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Flexible Passive NFC Tag for Multi-Gas Sensing

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ABSTRACT

In this work we present a full-passive flexible multi-gas sensing tag for the determination of oxygen, carbon dioxide, ammonia and relative humidity readable by a smartphone. This tag is based on NFC technology for energy harvesting and data transmission to a smartphone. The gas sensors show an optic response that is read through high-resolution digital colour detectors. A white LED is used as the common optical excitation source for all the sensors. Only a reduced electronics with very low power consumption is required for the reading of the optical responses and data transmission to a remote user. An application for Android operating system has been developed for the power supplying and data reception from the tag. The responses of the sensors have been calibrated and fitted to simple functions, allowing a fast prediction of the gases concentration. Cross-sensitivity has been also evaluated finding that in most of the cases is negligible or easily correctable using the rest of the readings. The election of the target gases has been due to their importance in the monitoring of modified atmosphere packaging. Resolutions and limits of detection measured are suitable for such kind of application.

Keywords: Passive tag; Optical multigas sensing; Colour detector; NFC; Android application; Smartphone.

The control of the conditions for food and beverage preservation in packaging systems has been widely studied in the last decade. The importance of guaranteeing the safe condition of the food, protecting it from external contamination, has led to an increasing interest of the companies in intelligent packaging technologies as well as the presence of this kind of systems on the markets. The research carried out on this subject has provided some innovations such as smart and active packaging, modified atmosphere

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3 packaging (MAP), and edible films/coatings.¹ Smart packaging is a system that allows
4 the monitoring of the properties of packaged foods and its environment, communicating
5 their state to the manufacturer, retailer and consumer.² Active packaging includes
6 additives or components that have an active participation in the preservation of the food
7 and beverage. MAP is used as a technique to modify the environmental conditions
8 inside the packaging in order to introduce some gas or gas mixtures to avoid the
9 spoilage of the contained food.^{1,3} Some of the traditional MAP technologies use
10 nitrogen flushing, vacuum packaging and carbon dioxide injection.^{4,5} In recent studies,
11 different gases have been introduced in the modified atmosphere such as argon for fruits
12 and vegetables,⁶ or carbon monoxide and high oxygen concentrations for red meats.⁷
13 MAP technology is often combined with smart packaging in order to inform the user if
14 the atmosphere within the package suffers any modification due to small breaks in the
15 envelope that might produce the spoilage of the content.
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20 For the reading and transmission to the user of the information regarding the
21 atmosphere conditions inside the package, electronic circuitry is often included in the
22 envelope.^{8,9} This electronics should be small size and low-power consumption.¹⁰ In this
23 field, radio frequency identification (RFID) and more recently near field communication
24 (NFC) has been adopted as a major technology for the development of tags included or
25 impressed on the packaging for the reading of the gas sensors and the transmission of
26 data to a remote RFID/NFC reader.¹¹⁻¹³ This short-range radio technology presents the
27 advantage of allowing the design of passive circuits that obtain the required power
28 supply for the operation of the electronics from the near field generated by a remote
29 reader, such as an NFC-enabled mobile device, when it is approached to the tag.^{14,15}
30 Therefore no battery is used in these tags, reducing the cost and enabling autonomous
31 operation.
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36 In the recent years, many passive RFID tags with sensing capabilities conceived for
37 monitoring the status of food in smart packaging have been reported.^{16,17} Most of them
38 are based on gases detection inside the package.^{18,19} Recently, the availability of NFC-
39 enabled mobile devices such as smartphones has avoided the necessity of a specific
40 RFID reader for data collection from the RFID tags. As a consequence, the smart
41 packaging based on this technology is being lately oriented to this protocol for data
42 transmission.^{20,21}
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46 Previous work of the authors presented the implementation of passive tags conceived to
47 be used in smart packaging for the monitoring of gases concentration in modified
48 atmospheres.^{14,22} In these papers, we proved the feasibility of the development of low
49 cost battery-free electronics systems based on optical sensors for the control of the gases
50 commonly presented in modified atmosphere composition and the rapid detection of the
51 envelope damages that can alter this composition producing the content spoilage.
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55 In this paper we propose a passive tag for multi-gas sensing based on RFID/NFC
56 technology for energy harvesting and data transmission with new sensing capabilities:
57 the number of gas sensors has been incremented to four. Furthermore, we have
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3 developed an Android application that allows in-situ measurement of the four gases
4 concentration using an NFC-enabled mobile phone. The analysed gases used for
5 evaluating the status of the inner modified atmosphere are oxygen and carbon dioxide,
6 which are two of the main gases used in MAPs.²³⁻²⁵ The other two gas sensors measured
7 by our prototype are aimed to detect and quantify the presence of ammonia and
8 humidity, two magnitudes that can reveal the spoilage of the food.²⁶⁻²⁸ The detection of
9 these four gases is based on the use of chemical sensors with optical response. This
10 approach allows a physical separation of the sensors, which can be placed inside the
11 package in contact with the inner atmosphere, whereas the reading and processing
12 electronics remain on the outside of the package. In addition, a temperature sensor is
13 included in order to compensate the temperature drifts of the gas sensors, as well as to
14 evaluate temperature variations of the environment than could also affect the content.²⁹
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21 **EXPERIMENTAL**

22 **Reagents and Materials**

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25 The chemicals used for the preparation of the sensing cocktails are: tributyl phosphate
26 (TBP), *o*-nitrophenyloctylether (NPOE), α -naphtholphthalein, crystal violet,
27 bromophenol blue sodium salt, 5,10,15,20-tetrakis(pentafluorophenyl)-21H,23H-
28 porphine palladium(II) (PdTFPP), tetraoctylammonium hydroxide (TOAOH),
29 cetyltrimethylammonium bromide (CTAB), ethanol, toluene, acetone, butyl acetate,
30 polystyrene, ethyl cellulose, cellulose acetate, and nafion 5%WT. All the reagents used
31 are analytical-reagent grade purchased from Sigma-Aldrich (Madrid, Spain). The tag is
32 screen printed on flexible substrate, specifically on 100 μm thick polyethylene
33 naphthalate (PEN, Kaladex PEN Film, Dupont Teijin Films, Tokyo, Japan), using silver
34 conductive ink model CRSN 2442 (Sun Chemical Corporation, Parsippany, New Jersey,
35 USA). PEN film was chosen because of its high light transmittance of 87% and good
36 adherence. The screen-printing machine was a Serfix III (Seglevint S.L., Barcelona,
37 Spain). The screen used to fabricate the single-layer pattern has a mesh density of 140
38 nylon threads per centimeter (T/cm). After printing, the pattern was sintered at a
39 constant temperature of 120 $^{\circ}\text{C}$ for 5 min in a convection oven (Venticell, Medcenter
40 Einrichtungen GmbH, Planegg, Germany). After sintering, four circles to contain the
41 four sensing membranes were screen printed using vinyl matt ink (Areny Color SL,
42 Alicante, Spain) on the other side of the tag. These circles act as barriers to prevent the
43 membranes from spreading. Finally, to assemble the chips and external components to
44 the substrate, a two-step process was carried out. First, the chips and silver pads were
45 interconnected using the conductive resin H20E (Epoxy Technology Inc., Billerica,
46 Massachusetts, USA). After this, the conductive resin was cured in the hot air oven at
47 120 $^{\circ}\text{C}$ for 20 min.
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Instruments and Software

The electrical characterization of the system was carried out using the following laboratory instrumentation: a mixed signal oscilloscope (MSO4101, Tektronix, Oregon, USA), an 8 1/2-bit Digital Multimeter 3158A (Agilent Technologies, Santa Clara, California, USA), a 15 MHz waveform generator 33120A (Agilent Technologies), a Precision Impedance Analyzer 4294A and an impedance probe kit (4294A1) (Agilent Technologies), a DC power supply E3630A (Agilent Technologies) and a balance DV215CD (Ohaus Co., Parsippany, New Jersey, USA). The standard mixtures for instrument calibration and characterization were prepared using N₂ as the inert gas by controlling the flow rates of the different high purity gases O₂, CO₂, NH₃ and N₂, entering a mixing chamber using a computer-controlled mass flow controller (Air Liquid España S.A., Madrid, Spain) operating at a total pressure of 760 Torr and a flow rate of 500 cm³ min⁻¹. Advanced Design Simulator (ADS, Agilent Technologies, Santa Clara, California, USA), a software based on the momentum method, has been used for the design and simulation of the printed antenna. To implement the Android application in the mobile phone, Android Studio 2.1.2 was chosen as the integrated development environment (IDE).

System Description

Membranes Preparation

The composition of the different sensing membranes and their preparation depends on the analyte that is going to be detected as well as the quantities of each one. The carbon dioxide sensing cocktail is prepared by the mixture of 64 μL of TBP, 320 μL of solution of 4.7 mg of α-naphtholphthalein in 4.27 mL of toluene/ethanol (80/20), 58.3 mg of ethyl cellulose in 1 ml of toluene and 600 μL of TOAOH.³⁰ Ammonia sensing cocktail is composed by 40 mg of cellulose acetate, 2 mg of bromophenol blue sodium salt, 37 mg of NPOE, 4.5 mg of CTAB in 2 mL of acetone.³¹ Oxygen sensing cocktail is prepared by the solution of 4.9 mg of PdTFPP in 5 mL of polystyrene 60 mg/mL in butyl acetate. Finally, the humidity sensing cocktail is prepared by the mixture of 1.27 mL of a solution of crystal blue 1.75 mM in methanol and 1 mL of nafion 5%WT.³²

Afterwards, 7 μL of each sensing solutions were dropped using a micropipette in the round designed area for that purpose and let it dry at room temperature for 2 hours in the darkness. Once the sensing membranes are dried, the tag can be used for the determination of the four gases.

Description of the Passive Sensing Tag

The proposed architecture consists of a RFID tag printed on a flexible substrate for the monitoring of four different gases by means of chemical sensors with optical response. The system is fully passive, therefore no battery is needed to supply the prototype. Instead, the power supply is obtained from the energy harvested from the near electromagnetic field induced by an external RFID reader. In this case, the reader is an

NFC-enabled mobile phone. Since the system is battery-free, it has been designed using very low consumption devices. Figure 1 shows a block diagram of the proposed system.

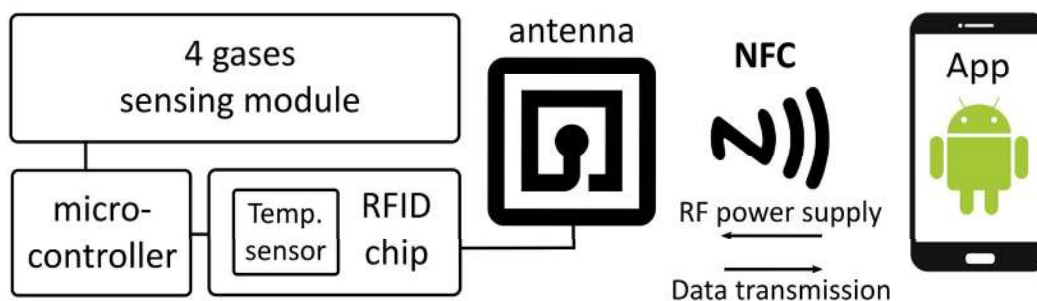


Figure 1. Block diagram of the complete system.

The analysis of the concentration of these gases is based on optical chemical sensors that are disposed on the inner face of tag in form of membranes. These membranes are optically excited and their optical responses are registered and related to the concentration of the objective gases. The printed interconnections and the required electronics for excitation and reading of the gas sensors and the data transmission is attached to the external face of tag, therefore the sensing membranes are the only elements that can be placed inside the package.

The sensing module is presented in the scheme of Figure 2. It consists of four gas sensors disposed in form of round membranes. These sensors are excited using a common white light-emitting diode (LED) situated in the centre of the sensing membranes (Figure 2(A)). In this way, the four sensors are excited together. For the reading of the optical response of the gas sensors, a digital colour detector is situated on the external surface of the flexible substrate directly facing each sensing membrane (Figure 2(B)).

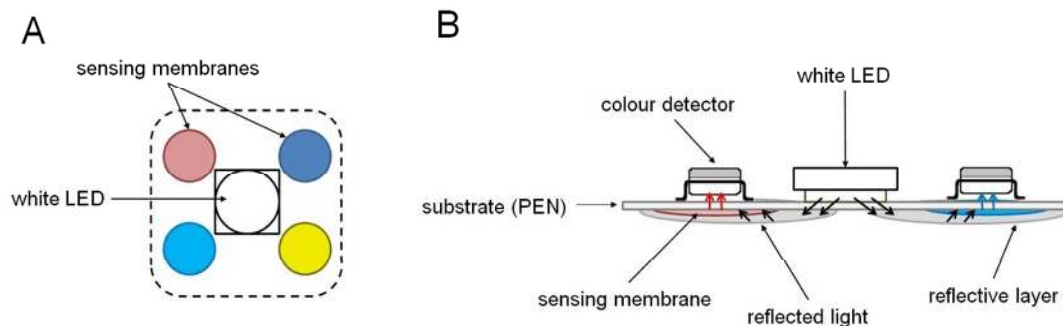


Figure 2. Bottom view (A) and lateral view (B) schemes of the sensing module.

In order to ensure that the emitted white light reaches by reflection the sensing membrane, a reflective layer permeable to gases consisting of white duct tape from 3M

(St. Paul, Minnesota, USA) is placed covering each membrane and part of the white LED. The optical response of each membrane, luminescent or colourimetric, is registered by the corresponding colour detector.

Figure 3 presents the complete system. A wide-surface diffused white LED model ASMT-MYH0-NDF00 (Avago Technologies, San José, California, USA) is used as the common optical excitation for the four sensing membranes. This LED has a very low power consumption of only 0.8 mW.

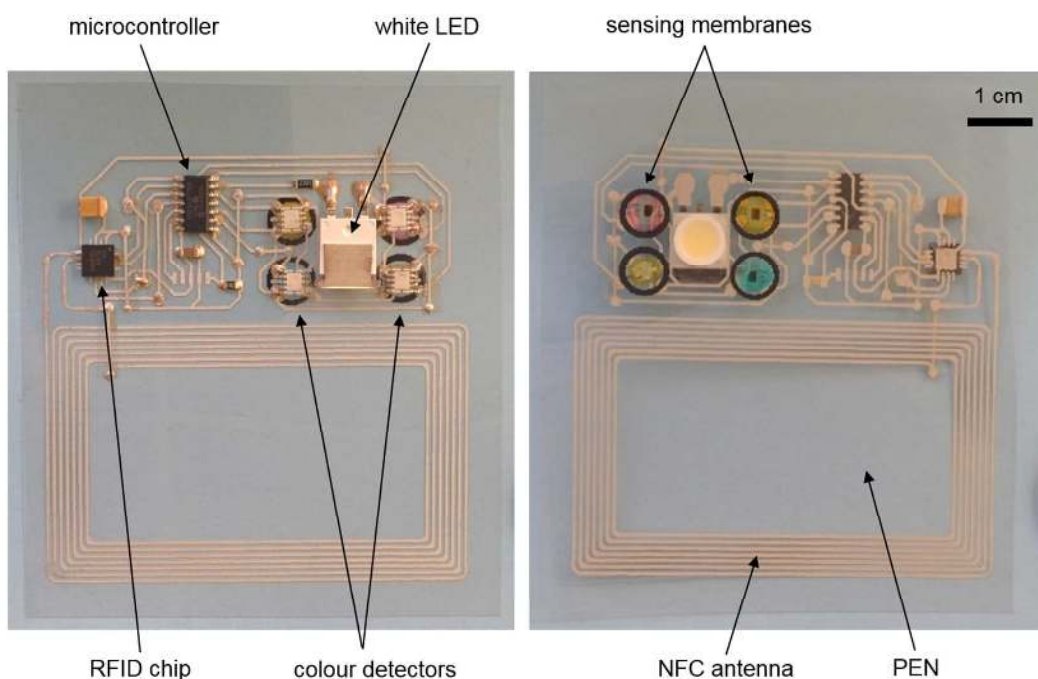


Figure 3. Photography of both sides of the developed tag.

The colour detector used in this design is the S11059-02DT (Hamamatsu Photonics, Hamamatsu, Japan), which is an I2C interface-compatible digital detector sensitive to red ($\lambda_{\text{peak}}=615$ nm), green ($\lambda_{\text{peak}}=530$ nm), blue ($\lambda_{\text{peak}}=460$ nm), and infrared ($\lambda_{\text{peak}}=855$ nm) radiation. The measured incident radiation is codified in four words of 16 bits, one for each colour. Besides its high resolution, it has been selected due to its very low power consumption of 250 μW , which makes this device optimal for passive designs. The digital outputs of the four colour detectors are directly transmitted by means of the I2C bus to the microcontroller model PIC16LF1703 (Microchip Technology Inc., Chandler, Arizona, USA), which also presents very good features regarding low power consumption. In this application, the consumption of the whole system is 8.5 mW in operation mode. The RFID chip is a device which integrates a radio-frequency (RF) interface that allows a wireless communication with an external RFID reader. The model selected here is the SL13A (IDS Microchip AG, Switzerland, since 2012 acquired by AMS AG, Unterpremstätten, Austria), which is a widely-used interface for the development of RFID/NFC tags.³³⁻³⁵ This device is compliant with the ISO15693

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3 RFID standard. It is also compatible with Android near-field communication (NfcV
4 standard). This component can be powered from the electromagnetic field induced in
5 the antenna by the external reader, which makes it suitable for the development of
6 passive tags. The SL13A integrates an on-chip 8kbit EEPROM and a built-in
7 temperature sensor. In addition, this device is able to power supply the rest of the
8 circuitry with a voltage output of 3.4 V and a maximum current of 4 mA, that is, a
9 maximum power of 13.2 mW, which is enough for this application. The antenna is a
10 custom-designed screen printed inductor. Resonance is achieved at $\omega_0 = \sqrt{LC}$, being
11 about 25 pF the capacitance of the RFID chip at the frequency of interest, 13.56 MHz.
12 Thus, the inductance value required for the resonation of the system at the frequency of
13 13.56 MHz is about 5.5 μ H. The designed printed inductor has seven turns and
14 dimensions of 65 mm \times 40 mm, being 500 μ m the width of the conductor and the
15 interspacing between the lines. The frequency response of the antenna as well as the
16 resonant frequency of the full system antenna-RFID chip has been evaluated. The
17 measured values of inductance and quality factor at the frequency of interest are 5.32
18 μ H and 1.43, respectively. The impedance of the tag reaches a value of 817 Ω at the
19 resonant frequency, in this case 13.68 MHz. Although this value is not exactly the
20 desired working frequency of 13.56 MHz, it is valid for a wireless operation following
21 the ISO15693 protocol specification.
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28 *Android Application*

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30 An Android application has been developed to use an NFC-enabled smartphone as the
31 external reader for the sensing tag. The application has been designed and tested against
32 API 23. However, to support different Android versions, the lowest API level
33 compatible with the application is API 16. The application user interface consists of
34 several text fields showing information about the tag identification number, current
35 temperature, values of each colour detector and gases concentration computed from
36 these values.
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40 When the smartphone is approached to the tag, it is detected, the Android application is
41 started and the system is powered up by the electromagnetic energy from the mobile
42 NFC link. After this, the white LED switches on, the microcontroller sequentially reads
43 the digital outputs of the four colour detectors by means of the I2C (Inter-Integrated
44 Circuit) protocol and it computes the different gases concentrations. Then, the
45 microcontroller saves all these measurements using the SPI (Serial Peripheral Interface)
46 protocol on specific locations of the RFID chip's non-volatile memory. These memory
47 locations are accessed by the Android application through the NFC interface using the
48 ISO 15693 NFC protocol, and the results are displayed on the screen of the smartphone,
49 as shown in Figure 4. The time required to perform a single reading of each colour
50 detector in the tag is 203 ms; therefore, the reading of the four detectors is accomplished
51 in 812 ms. The application also gets the temperature value measured by the RFID on-
52 chip temperature sensor. The explained procedure is repeated each time the user clicks
53 on the Measure button of the application user interface.
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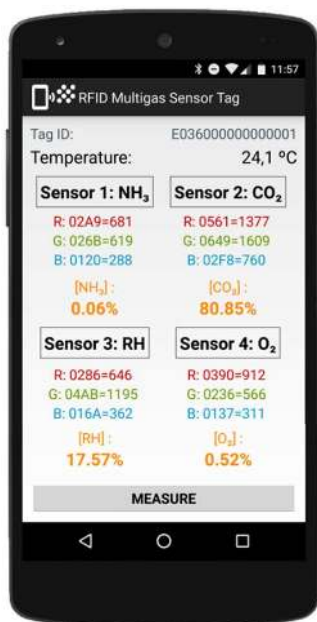


Figure 4. Smartphone running the Android application.

RESULTS AND DISCUSSION

The multi-gas sensing tag has been applied to monitor the concentrations of oxygen, carbon dioxide, ammonia and humidity. The concentration of O₂ in a MAP is very low, usually ranging from 0.05% to 2%, while the CO₂ is flushed into the package to obtain a high concentration above 60%.²² The concentration of ammonia will depend on the spoilage status of the food and it is found in low concentrations in the order of tens of ppm.³⁶ The relative humidity of the MAP can take both low and high values depending on the application.^{27,37}

The four gas sensors show an optical response to the presence of the corresponding gas, being the response of the O₂ sensor luminescent and the response of the rest of the sensors colourimetric. Previous work of the authors proved the feasibility of the structure shown in Figure 1(B) for the reading of the optical response of sensors both luminescent or colourimetric.²² There, a white LED was used as optical source for colourimetric sensors, and a specific LED for the excitation of luminescent sensors that require an optical source of a certain wavelength. In this work, we have been able to use a common white LED for the excitation of all sensors by means of a redesign and optimization of the sensing area. The spectrum of this LED contains the wavelengths necessary for the excitation of the luminescent sensor.

Stability of the Power Supply

The power supply of the tag sensing area provided by the RFID/NFC chip SL13A from the electromagnetic energy harvesting has been evaluated in order to prove its stability and analyze its possible influence on the response of the digital colour detectors. Two external parameters can affect the stability of the regulated voltage generated by the

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3 SL13A: the powering time and the position of the smartphone when it is approximated
4 to the tag antenna. Since the SL13A chip requires an induced electromagnetic field in
5 the antenna high enough to provide the regulated power supply, not every position of
6 the smartphone is able to activate the tag. When it is adequately placed, only a small
7 displacement is allowed to avoid the deactivation of the system. Within this accepted
8 range of positions of the smartphone, the voltage output of the SL13A presents a drop
9 of 5% of its nominal value. Since the colour detector is a digital device that can be
10 powered with a voltage from 2.25 to 3.6 V this variation in the power supply has no
11 effect on the output signals, according to the manufacturer.
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15 The influence of the powering time on the response of the colour detector is depicted on
16 Figure 5. This graphic shows the measurements of a stable incident light taken every 5
17 seconds from the moment of activation of the tag by the smartphone up to 5 minutes.
18 Each point in the curves is calculated as the mean value of six replicas, and the error
19 bars are obtained as the standard deviations of these replicas.
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22 As it can be seen, some fluctuation of the measured values is present. Nevertheless, the
23 dispersion of the data is very low with a maximum value of 0.25%, which is below the
24 maximum uncertainty obtained in the determination of each measurement from the set
25 of six replicas. Therefore, this fluctuation is assumed to be produced by uncertainty
26 inherent to the colour detector rather than due to the powering time.
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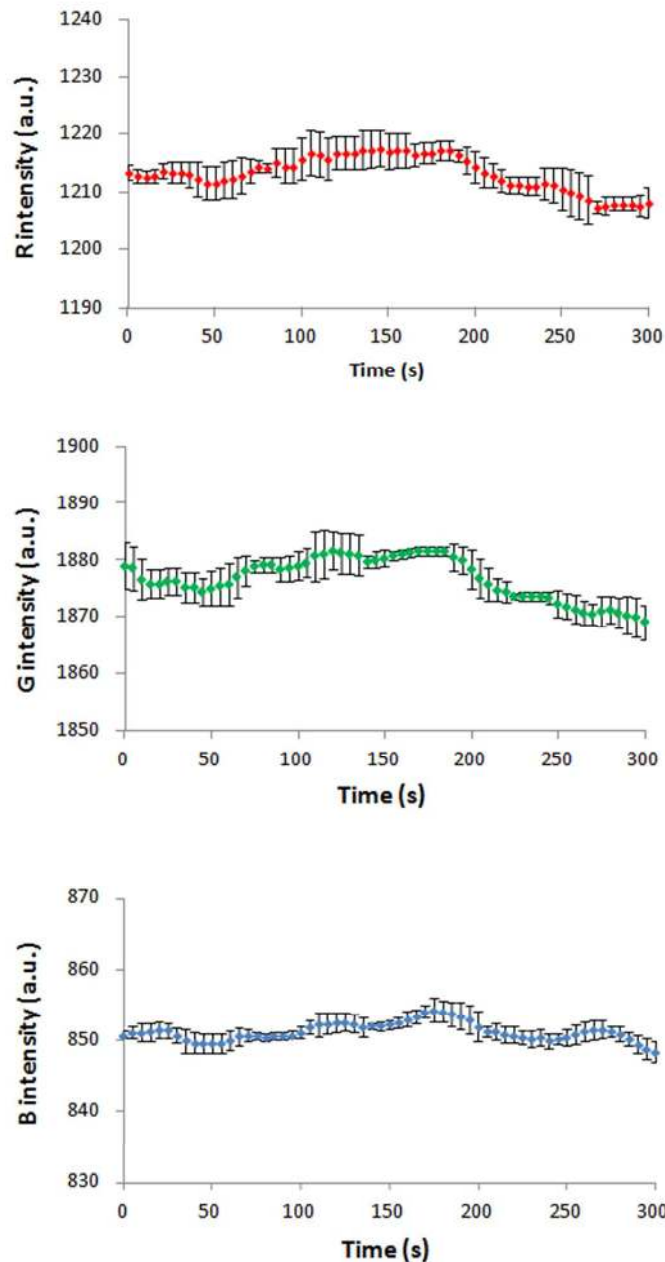


Figure 5. Output signals of the colour detector over time.

System Calibration

The multi-gas sensing tag has been calibrated obtaining the response of the different gas sensors to variations in the concentration of the corresponding sensed gas. All the measurements are carried out while the tag is powered by electromagnetic field coming from the smartphone NFC link; this energy is harvested by the tag antenna and conditioned by the RFID chip SL13A to power the rest of the electronics, therefore no other external power supply is used.

Figure 6A presents the calibration curve of the oxygen sensor. The response of the sensor is characterized by the intensity of the emitted red radiation that reaches the colour detector. This radiation corresponds to the luminescence generated by the complex PdTFPP when it is optically excited.³⁸ The output data word of the colour detector corresponding to red light is a direct measurement of this luminescence. The mean of 6 replicas at room temperature (21°C) is taken as the representative data for each concentration. As it is exposed above, the time required for the reading of one sensor is 203 ms; since the calibration data are generated from sets of 6 replicas, each calibration point is obtained in 1.22 seconds. An offset signal in the output of the colour detector is induced by the light emitted by the excitation white LED. Nevertheless, since it is a constant interference, it can be easily compensated or included in the calibration curve. As it was expected, the fitting equation is a potential function in the form $I = \alpha \cdot [\text{O}_2]^\beta$.³⁹

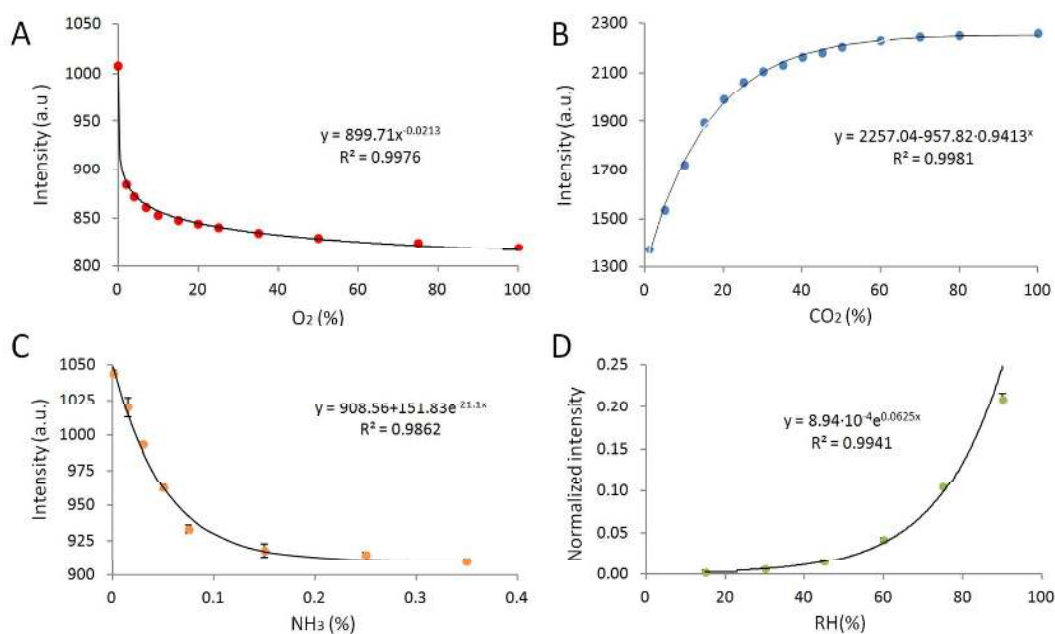


Figure 6. Calibration curves of the gas sensors.

The other three sensors are colourimetric-type. That means that the sensing membranes show a colour shift when the concentration of the surrounding target gas varies. Figures 6B to 6D show the calibration and fitting curves of the CO₂, NH₃ and humidity sensors, respectively. The response of these sensors is quantified by means of the colour intensity parameter given by⁴⁰:

$$I = \sqrt{R^2 + G^2 + B^2} \quad (1)$$

where R, G and B are the red, green and blue components of radiation measured by the digital colour detector, respectively. For the calibration curve of the CO₂ and NH₃

sensors, the intensity is fitted directly to a prediction function which is used to generate a value of the corresponding gas concentration from the colour measurements. Nevertheless, the data obtained from the calibration of the humidity sensor must be further processed to generate a simple fitting function as it is shown in Figure 6D, where a normalized value of the colour intensity in the form $\log(I_0/I)$ is presented, being I_0 the intensity measured for 0% relative humidity. Oxygen, carbon dioxide and relative humidity are calibrated in the full range 0 to 100%. Ammonia is measured from 0 to 0.35 %.

From the fitting functions presented in Figure 6 some technical specifications such as resolution and limit of detection (LOD) can be obtained. The resolution is calculated by taking derivatives in both sides of the equation and approximating these derivatives to increments⁴¹:

$$\Delta X = \frac{\partial f(I)}{\partial I} \Delta I \quad (2)$$

where X is the concentration of gas, $f(I)$ is the corresponding fitting function and ΔI is the error or uncertainty in the determination of the intensity I , which is taken as the standard deviation of the replicas made during the calibration processes. The LOD was obtained using the standard criteria: $\text{LOD} = y_b + 3s_b$, where y_b is the average blank signal and s_b is the standard deviation of the blank, which is determined using at least 10 replicas. Repeatability of the measurements is quantified through the coefficient of variation (CV) of the signal, defined as the ratio between the standard deviation of a set of replicas and its mean value.

Table 1 shows the results of the resolution, LOD and repeatability obtained for the four gas sensors. As it can be seen, these specifications allow the use of the developed tag for the monitoring of the selected gases taking into consideration the usual ranges found in MAPs.

Table 1. Technical specifications of the sensing tag.

Gas	Concentration (%)	Resolution (%)	CV (%)	LOD (%)
O ₂	0	$1.9 \cdot 10^{-4}$	0.09	$1.3 \cdot 10^{-3}$
	2	$9.4 \cdot 10^{-2}$	0.09	
	20	$9.1 \cdot 10^{-1}$	0.81	
CO ₂	5	$7.4 \cdot 10^{-2}$	0.21	0.23
	50	$9.4 \cdot 10^{-1}$	0.13	
	100	3.8	0.07	

NH ₃	$1.5 \cdot 10^{-2}$	$3.3 \cdot 10^{-3}$	0.71	$7.9 \cdot 10^{-4}$
	$5.0 \cdot 10^{-2}$	$2.0 \cdot 10^{-3}$	0.22	
	$3.5 \cdot 10^{-1}$	$1.6 \cdot 10^{-1}$	0.25	
RH	15	0.8	0.21	1.8
	45	1.1	0.24	
	90	0.1	0.44	

Cross-Sensitivity

The possible interferences of the gases in the response of the selective sensors have been evaluated. For this purpose, the maximum variation of the output signal of the sensors in the presence of the rest of gases is obtained for a fixed concentration of the target gas. In addition, the influence of the temperature on the response of the selective sensors has been also quantified as the variation of the output signal to an increment of 25 °C. Table 2 shows the obtained results.

Table 2. Cross-sensitivities between the sensors of the tag.

Selective sensor	Interferent	Signal variation (%)
O ₂ (0%)	CO ₂ (100%)	0.2
	NH ₃ (100%)	2.2
	RH (90%)	2.4
	T	14.1
CO ₂ (0%)	O ₂ (100%)	2.8
	NH ₃ (100%)	2.1
	RH (90%)	0.1
	T	2.6
NH ₃ (0%)	O ₂ (100%)	1.9
	CO ₂ (100%)	2.9
	RH (90%)	1.7
	T	1.8
RH (35%)	O ₂ (100%)	0.4
	CO ₂ (50%)	0.7
	NH ₃ (100%)	21.1
	T	2.3

As it can be seen, the interference produced by the gases on the response of the other gases selective sensors is very low, below the 3%, and the maximum deviation of the signal is always obtained when the interfering gas is present in a very high concentration near the 100%, which is not a realistic case in MAPs. This implies that in a practical case the cross-sensitivity can be neglected. There is only one exception, the

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3 influence of the ammonia on the response of the humidity sensor. The maximum
4 variation of the output signal of this sensor is above 21%. This means that an important
5 interference is produced by this gas and it should be corrected when the determination
6 of the gases concentration is carried out from the readings of the sensors.
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9 On the other hand, the temperature shows a strong influence in the response of the
10 oxygen sensor, which is a well-known effect.⁴² The reading of the oxygen sensor should
11 be also corrected with the value of the temperature,¹⁴ that is the reason for using a RFID
12 chip with a built-in temperature sensor.
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15 16 17 **CONCLUSIONS**

18 In this work, a passive multi-gas sensing RFID/NFC tag is presented for the
19 determination of a high number of parameters (oxygen, carbon dioxide, ammonia,
20 relative humidity and temperature) that are readable with a smartphone. The gases
21 concentrations are determined by means of chemical sensors with optical response. The
22 tag response to the different gases concentrations has been calibrated, obtaining very
23 good values for resolution, repeatability and limit of detection. This makes the proposed
24 system suitable for its use in smart packaging applications. Cross-sensitivity has been
25 also evaluated, obtaining an interference below the 3% in all cases with few exceptions,
26 where the measurements are easily corrected by software in the microcontroller from
27 the full set of readings.
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32 The tag is completely passive and the required power supply for its operation is
33 harvested from the near field generated by an NFC-enabled mobile phone. In this
34 application, the power consumption of the tag is only 8.5 mW in sensing mode. Thanks
35 to the use of digital colour detectors for the reading of the chemical sensors' response,
36 the system is robust against fluctuations in the power supply. In addition to powering
37 the system up, the mobile phone is used to collect and display the results on a custom
38 Android application in less than one second. The wireless communication between the
39 tag and the phone is achieved via the ISO 15693 standard. The use of a smartphone as
40 exciter/receiver instead of a specific RFID reader allows the operation of the tag by any
41 non-expert and non-trained user. This tag can be applied to a wide range of applications
42 in modified atmospheres where the monitoring of gases composition is required, or in
43 smart packaging applications where the control of the conditions for food and beverage
44 preservation needs to be guaranteed.
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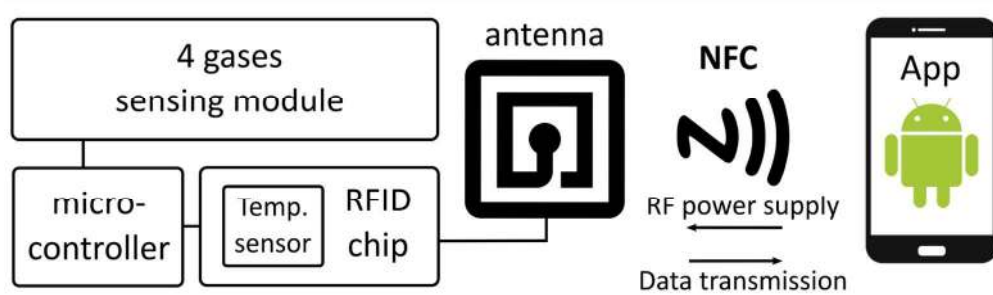


Figure 1. Block diagram of the complete system.

335x101mm (120 x 120 DPI)

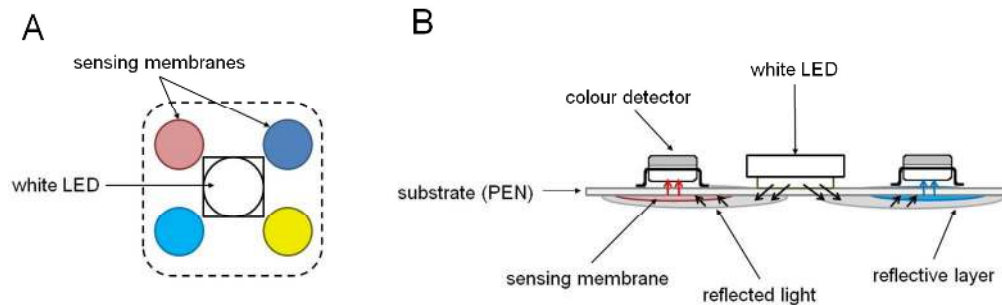


Figure 2. Bottom view (A) and lateral view (B) schemes of the sensing module.

338x108mm (120 x 120 DPI)

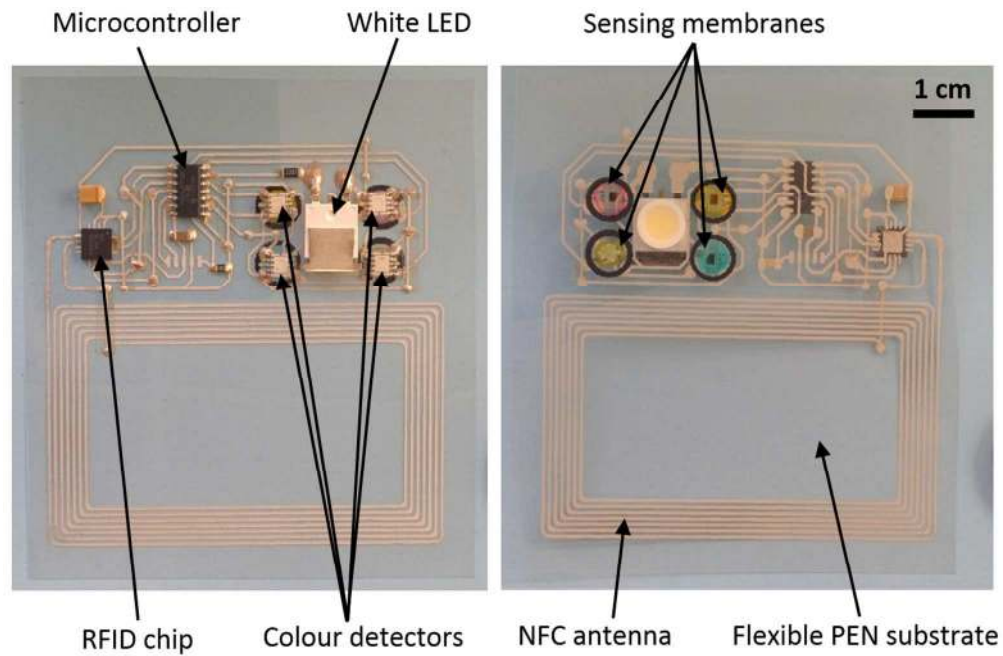


Figure 3. Photography of both sides of the developed tag.

354x229mm (96 x 96 DPI)

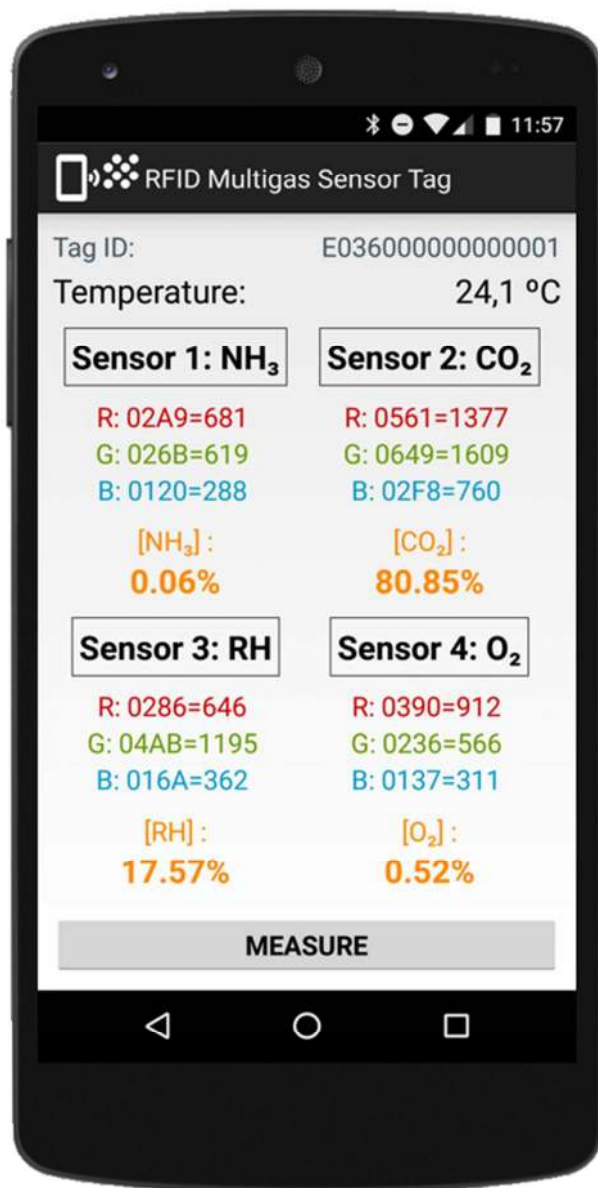


Figure 4. Smartphone running the Android application.

114x222mm (96 x 96 DPI)

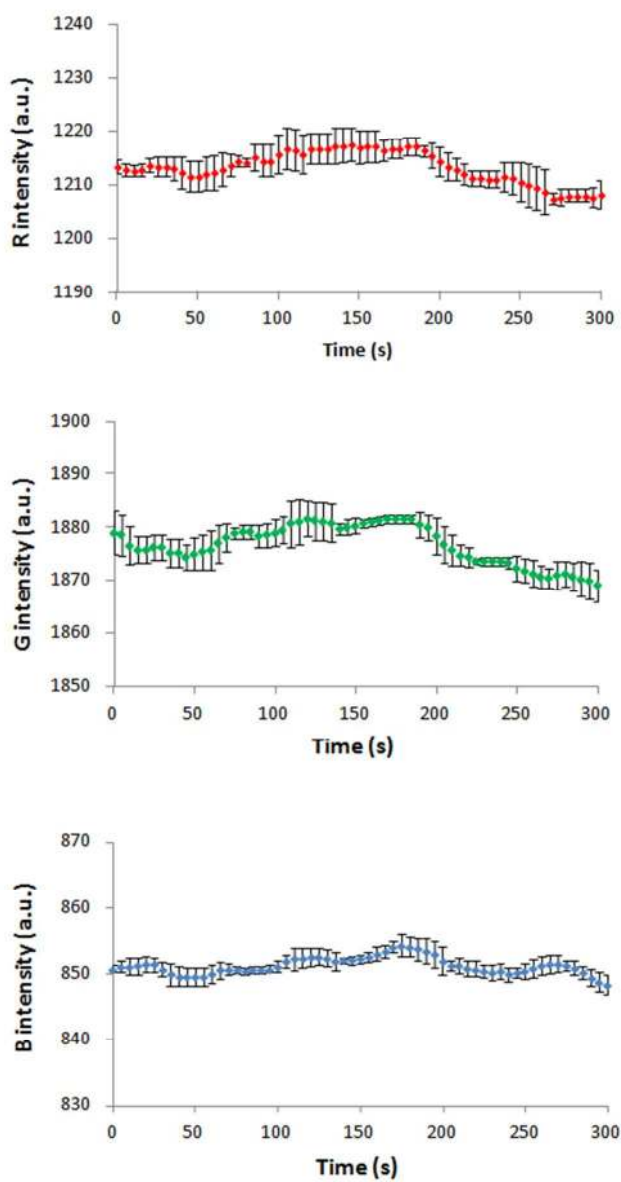


Figure 5. Output signals of the colour detector over time.

98x181mm (120 x 120 DPI)

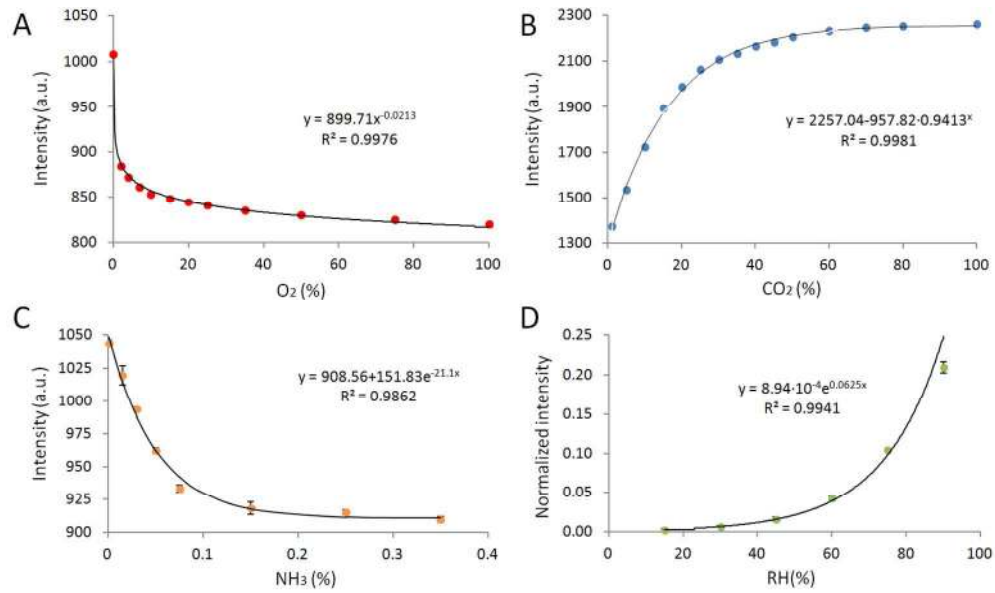


Figure 6. Calibration curves of the gas sensors.

321x187mm (120 x 120 DPI)