

Fracture Toughness of Phenol Formaldehyde Composites: Pilot Study

H Ku^{*#}, D Rogers^{*}, R Davey[#], F Cardona^{*}, and M Trada[#]

[#]Faculty of Engineering and Surveying,

University of Southern Queensland, Australia;

^{*}Centre of Excellence in Engineered Fibre Composites,

University of Southern Queensland, Australia.

Corresponding Author:

Title : Dr.

Name : Harry Siu-lung Ku

Affiliation : Faculty of Engineering and Surveying,
University of Southern Queensland.

Tel. No. : (07) 46 31-2919

Fax. No. : (07) 4631-2526

E-mail : ku@usq.edu.au

Address : Faculty of Engineering and Surveying,
University of Southern Queensland,
West Street, Toowoomba, 4350,
Australia.

Abstract: A commercial phenol formaldehyde based resole thermosetting resin (Hexion “J2027L”) was filled with ceramic-based fillers (Envirospheres “slg”) to increase its strength and fracture toughness. By testing viscosity, strength and fracture toughness at a range of filler addition levels, the optimal addition level of SLG was able to be determined in terms of workability, cost and performance. It was found that the fracture toughness of this resin could be significantly increased through the addition of the slg filler. The results show that composite with 20 % by weight of the slg produces the best balance between ease of casting and impact performance.

Keywords: Phenol formaldehyde, phenolic resin, envirospheres, SLG, short bar test and viscosity.

1. Introduction

Phenolic thermosetting materials were amongst the first major plastic material used by industry. They are still among the most widely used thermosetting resins due to their excellent high temperature and fire performance. Phenolics are formed from the condensation of polymerization reaction between phenol and formaldehyde. The condensation reaction for phenolics can be carried out under two different conditions, resulting in two different intermediate materials. One of the intermediates is called resoles and the other novolacs [1, 2].

In the resole process, the condensation polymerization is performed in an alkali solution with excess formaldehyde and is carefully controlled so that a linear, non-crosslinked polymer liquid, resole, is produced. The resole can then be molded.

When molding, the crosslinking is achieved by heating the viscous liquid. Since a crosslinked part can be obtained by simply heating the resoles, which are called one-stage resins. Alternatively, resole phenolic resins are cured at room temperature via the addition of acid catalysts, typically sulphonic acids [2].

Novolac phenolic resins are formed by reacting phenol and formaldehyde in an acid solution but with insufficient formaldehyde to complete the reaction at 100 °C (the opposite of forming resoles). About one mole of phenol is reacted with 0.70 to 0.85 mole of formaldehyde. This is the first stage of the reaction and a brittle thermoplastic resin is produced which can be melted but cannot crosslink to form a solid network.

The polymerization reaction is shown in Figure 1. The addition of hexamethylenetetramine (hexa), a basic catalyst, to the first stage phenolic resin makes it possible to create methylene crosses linkages to form a thermosetting material. When heat and pressure are applied to the hexa-containing novolac resin, the hexa decomposes, producing ammonia which provides methylene cross linkages to form a network structure. On account that hexa, a second material, must be added to novolacs, they are called two-stage resins. The temperature required for the cross-linking of the novolac resin ranges from 120 to 177 °C.

The various fillers used can vary from 50 to 80 % by weight. The fillers reduce shrinkage during molding, lower cost and improve strength. They are also used to improve electrical and thermal insulating properties and chemical resistance [1-4]. This research project is aimed at investigating the fracture toughness of a commercial resole phenol formaldehyde resin reinforced with ceramic microsphere

("Envirospheres slg") filler. Short bar testing has been used to determine the fracture toughness of the specimens in this work [5-7].

2. Materials

The commercial resole resin used in this study was J-2027L produced by Hexion Speciality Chemicals Pty Ltd. Its official name is Hexion Cellobond J2027L [8]. The acid catalyst used to crosslink the resin was Hexion Phencat 15 [9]. The ratio by weight of the resin to hardener for all samples in this work was chosen to be 20: 1. With reference to phenolic molecule of Figure 1, there are five 5 hydrogen atoms in the benzene ring but because of limited space, there are only three possible sites for reaction and the phenolic molecule is said to have a functionality of three and this is shown in Figure 2 [3, 10]. As the functionality of the phenolic molecules is greater than two, the molecules can react with formaldehyde molecules to form 3-D network polymer [1].

Envirospheres slg (E-spheres) is a commercial ceramic microsphere product obtained as a fly ash by-product. The particle size of this general purpose E-spheres ranges from 20 – 300 μm with approximate mean of 130 μm . The relative density of E-spheres is 0.7. E-spheres are a combination of Silica, SiO_2 (55-60%), Alumina, Al_2O_3 (36-44%), Iron Oxide, Fe_2O_3 (0.4-0.5%) and Titanium Dioxide, TiO_2 (1.4-1.6%).

3. Fracture toughness

Unlike the result of an impact test, it is a property that can be quantitatively measured. A typical fracture toughness test may be performed by applying a tensile stress to a specimen prepared with a flaw of known geometry and size and is shown in Figure 3. The stress applied to the material is intensified at the flaw [11]. For a simple test the stress intensity factor,

$$K = f\sigma\sqrt{\pi a} \quad (1)$$

where f is a geometry factor for the specimen and flaw. If the specimen is assumed to have 'infinite' width then $f \cong 1.0$; for 'semi-infinite' width, $f \cong 1.1$ [11, 12]

σ is the applied stress;

a is the flaw size.

The critical stress intensity factor is defined as fracture toughness, K_c is the K required for a crack to propagate and $K_c = f\sigma_c\sqrt{\pi a}$ (2)

K_c is a property that measures a material's resistance to brittle fracture when a crack is present and its unit is $\text{MPa}\sqrt{m}$. The value K_c for this thick-specimen situation is known as the plane strain fracture toughness K_{Ic} ; furthermore, it is also defined by [12]:

$$K_{Ic} = f\sigma\sqrt{\pi a} \quad (3)$$

4. Short Bar Test and the Composite Samples

Baker [7] described the background, selection criteria and specimen geometry options for short rod and short bar methods. Figures 4 and 5 show the short rod and short bar

specimens with straight chevron slots. The load line is the line along which the opening load is applied in the mouth of the specimen. The specimen parameter, B, is the specimen diameter (for short rod) or breath (for short bar). They also show two slot bottom geometries which result from two useful methods of machining the chevron slots. Figure 4 shows the straight slot geometry which results from feeding the saw or cutter through the specimen.

The reinforcer was E-sphere slg (ceramic hollow sphere) particulates and they were made 15 % to 35 % by weight in step of 5 % in the cured phenol formaldehyde composite PF/E-SPHERES (X %), where X is the percentage by weight of the filler; the 40% by weight was tried but it was found to be too viscous for mixing. As the raw materials of the composites are liquid and ceramic hollow spheres, the short bar specimens were cast to shape. The resin is mixed with the catalyst, after which the E-sphere slg is added to the mixture and they are then mixed to give the uncured composite. Table 1 shows the mass in grams of resin, catalyst and slg required respectively to make 300 grams of uncured composite of 20 % by weight of slg. The mould was made from PVC (poly vinyl chloride) sheets with six pieces of short bar specimen each. This is depicted in Figure 5. The slots were made by inserting plastic sheets of suitable thickness. Figure 6 shows some of the PF/E-SPHERES (X %) short bar specimens ready for the tests. After preliminary curing, the samples were taken out of the mould and post-cured in an oven at 50 °C for 2 hours followed by 80 °C for 4 hours and finally by 100 °C for 4 hours. They specimens were then subjected to short bar test.

5. Sample Size

The number of samples for each percentage by weight of E-spheres is six. An MTS 810 Material Testing Systems was used for the test. The rate of extension was made 1 mm per minute. The short bar tests involve an opening load being applied near the mouth of the specimen, causing a crack to initiate at the point of the chevron slot. Ideally, the opening load should be less than the load that will be required to further advance the crack. A continually increasing load must be supplied until the crack length reaches the critical crack length, a_c . Beyond a_c , the load should decrease, as shown in Figure 7.

The equation for fracture toughness in a short bar test can be derived from basic fracture mechanics using the assumptions of linear elastic fracture mechanics (LEFM). The equation for the material plane strain critical stress intensity factor, K_{ICSR} [13]:

$$K_{ICSB} = \frac{(F_{max} Y_m^*)}{B\sqrt{W}} \quad (4)$$

where F_{max} = Peak load

Y_m^* is the compliance calibration according to ASMT E-399-78 and

$$Y_m = 15.700$$

$$\omega = \frac{W}{H} = 1.671$$

$$\alpha_0 = \frac{a_0}{W} = 0.310$$

$$\alpha_1 = \frac{a_1}{W} = 0.969$$

All parameters like a_0 , a_1 , W and H are shown in Figure 8. Also, $B = 50$ (by design), and $F_{\max} = 356\text{N}$ (average peak load of six samples, 356 N was used in the calculation of K_{ICSB}).

Fracture toughness for 20% by weight of slg is calculated as:

$$K_{\text{ICSB}} = \frac{(F_{\max} Y_m^*)}{B\sqrt{W}} = 13.070\text{MPa}\sqrt{m}$$

6. Viscosity Measurements

Viscosity was measured using the Brookfield RDVD-II+ viscosity testing machine. Throughout the tests the viscosity was recorded at a constant temperature of 26 °C. The temperature of the composite (in liquid form) would rise as time went on due to the curing. Theoretically, one should allow the temperature to rise and viscosity to reduce (Figure 9) and then pour the liquid form composite into the moulds but this may not be achievable because the composite would have cured before one can properly cast the composite into the moulds. Viscosity has therefore to be measured as soon as the measuring probe was dipped into the composite.

7. Results and Discussion

Figure 10 shows the of fracture toughness J2027 specimens filled with varying weight percentages of E-spheres slg. Table 2 depicts the of fracture toughness PF/E-SPHERES with varying percentage by weight of slg with the standard deviation given in bracket. It was found that the fracture toughness is highest when the percentage by weight of the filler, slg is 20 %; its value is $12.47\text{MPa}\sqrt{m}$. As the standard deviation

is small, it can be argued that the values of fracture toughness obtained are reliable. Redjel [14] found that the fracture toughness of pure phenolic resin was $1.51 \text{ MPa}\sqrt{m}$; the fracture toughness of neat resin by weight of slg reinforced phenolic resin, PF/E-SHPERES (0%) in this study was $8.72 \text{ MPa}\sqrt{m}$, which is 5.78 times the fracture toughness of pure phenolic resin, an increase of 478%. This may be due to the improved resin used (the work was carried out eleven years later) and better post-curing method of the composite. Figure 11 shows the viscosity of 2027/E-sphere formulations as function of filler weight. This data shows that the viscosity increases with increasing percentage by weight of SLG. It has been found by experiment, and been confirmed by other researchers (Davey [15]), that there is a viscosity limit of resin/SLG mixtures above which casting is not possible. This is around 38-42% by weight and corresponds to viscosity in the range of 16,000 – 20,000 cps. This filler content is much higher than that previously determined to be best in terms of fracture toughness, 20% w/w. At 20% w/w, the viscosity of the resin/SLG mixture is around 3,140 cps. At this viscosity, workability of the filled resin would be good.

Figure 12 illustrates the scanning electron microscopy image of phenolic resin post-cured for 4 hours at 80 °C at a magnification of 3,500. There is evidence of the presence of voids of around 10 micron diameter that have been attributed to the water domains formed during the condensation cure of the resole resin. Its fracture toughness is less than those of phenolic resin reinforced with slg of 15 - 25 % by weight. Figure 13 enables one to view the voids of the above composite clearer as the magnification of the image was increased to 10,000 X.

Figure 14 illustrates the scanning electron microscopy image of phenolic resin reinforced by 20% by weight of slg and post-cured for 4 hours at 80 °C at a magnification of 15,000 X. It can be found that the voids were partially filled by the slg but the reinforcer did not fuse with the matrix and gap was found between them. Its fracture toughness is $12.50 \text{ MPa}\sqrt{m}$ and it can be argued that if the reinforcer and the matrix mix homogeneously, the fracture toughness will even be higher. Figure 15 enables one to view the more serious gap of the composite (15%) clearer as the magnification of the image was increased to 25,000 X. With this magnification, it is clear that there is no fusion between the reinforcer and the matrix. To improve the fusion between the reinforcer and the matrix, other fillers or resin will have to be added and this will also be research focus for us in the near future.

8. Conclusions

The project has proved that by adding 20 % by weight of slg to phenolic resin, the fracture toughness of the composite is 8.28 times of that of the pure resin. It has also proved that 20 % by weight of slg is the most suitable amount of slg added to attain maximum fracture toughness and has no fluidity problem for casting the composite into moulds. It can be argued that the fusion between phenolic resin (matrix) and slg (reinforcer) will be improved by adding some other fillers and resins to the composite.

References

1. Shackelford, J F, *Introduction to materials science for engineers*, 3rd edition, Macmillan, 1992, pp.435-437.

2. Smith, W F and Hashemir, J, *Foundations of material science and engineering*, 4th edition, McGraw-Hill, 2006, pp. 523-525.
3. Strong, A B, *Plastics: materials and processing*, 3rd edition, Pearson/Prentice-Hall, 2006, pp. 182-183, 304-309, 323-333, 620-621.
4. Clarke, J L (Editor), *Structural design of polymer composites*, E & FN Spon, U.K., 1996, pp.59-62, 343-5, 357.
5. Barker, L M, *Fracture mechanics applied to brittle materials*, ASTM, STP 678, American Society for Testing and Materials, 1979, pp.73-82.
6. Baker, L M, *Development of the short rod method of fracture toughness measurement*, Proceedings, Conference on Wear and Fracture Prevention, 21-22 May 1980, ASM, Metals Park, Ohio, pp. 163-180.
7. Baker, L M, *Short rod and short bar fracture toughness specimen geometries and test methods for metallic materials*, Proceedings, Fracture Mechanics: Thirteenth Conference, ASMT STP 743, 1981, pp. 456-475.
8. Chemwatch, *Material safety data sheet for Hexion Cellobond J2027L*, 2005a, pp. 1-14.
9. Chemwatch, *Material safety data sheet for Hexion Phencat 15*, 2005b, pp. 1-14.

10. Morgan, M J, *Engineering Materials –Study Book 1*, University of Southern Queensland, 2006, p.9.13.

11. Askeland, D R, *The science and engineering of materials*, Third Edition, Stanley Thornes, 1998, pp.163-164.

12. Callister, W D, *Materials science and engineering: an introduction*, 7th Ed., John Wiley and Sons, Inc., 2006, pp. 217-219.

13. Munz, D, *Determination of Fracture Toughness of High Strength Aluminum Alloys with Chevron Notched Short Rod and Short Bar Specimens*, *Engineering Fracture Mechanics*, Vol. 15, No. 1-2, 1981, pp. 231-236.

14. Redjel, B, *Mechanical Properties and Fracture Toughness of Phenolic Resin*, *Plastics, Rubber and Composites Processing and Applications*, 1995, Vol. 24, pp. 221-228.

15. Davey, S W, Heldt, T, Van Erp, G and Ayers, Stephen, *Vinyl Ester/Cenosphere Composite Materials for Civil and structural Engineering*, *FRP International*, Vol. 2, No. 3, 2005, pp. 2-5.

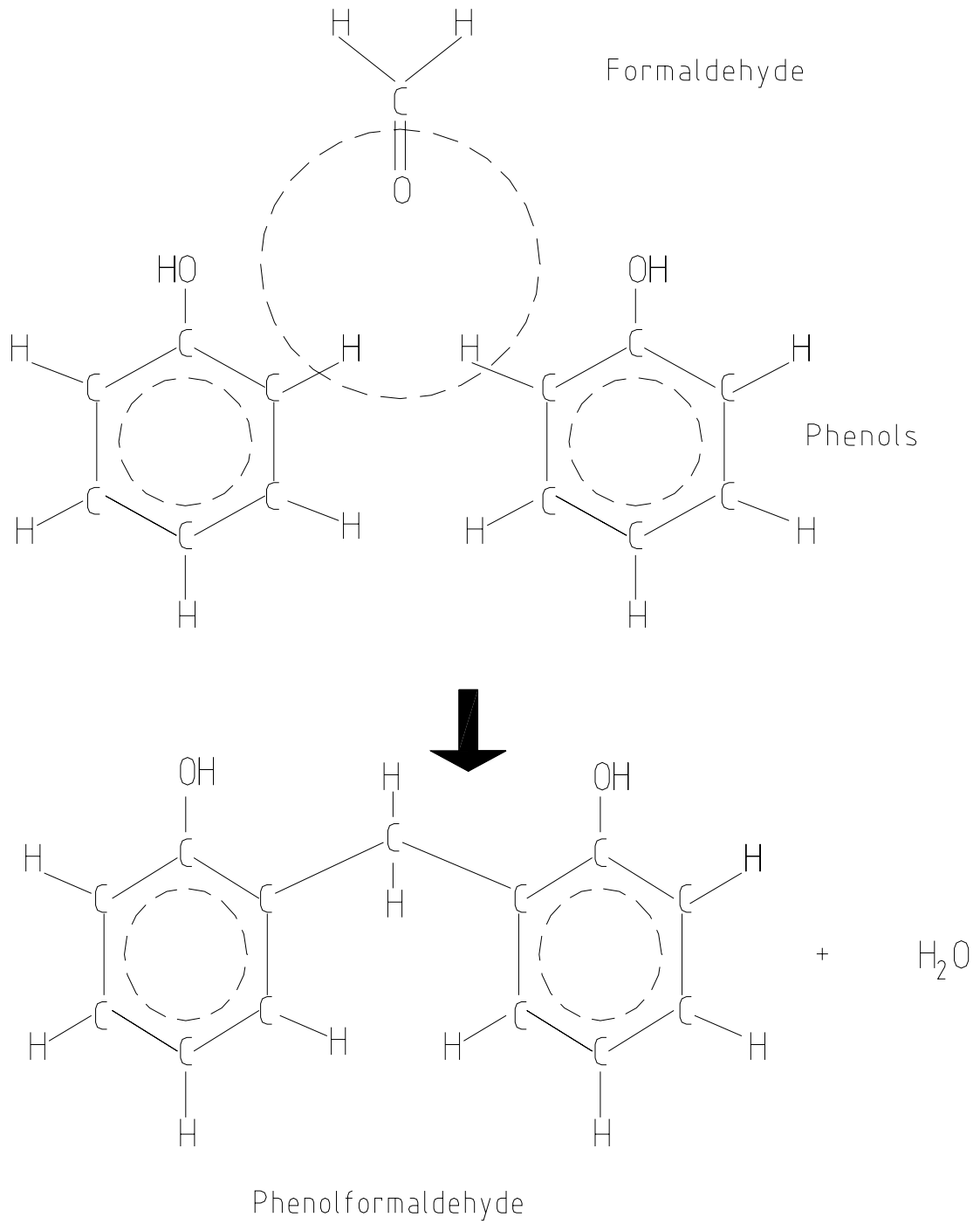


Figure 1: Formation of Phenol formaldehyde

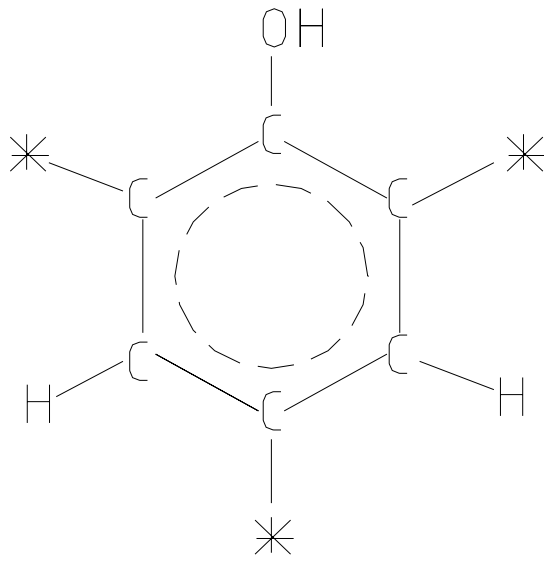


Figure 2: Phenol with active sites marked *

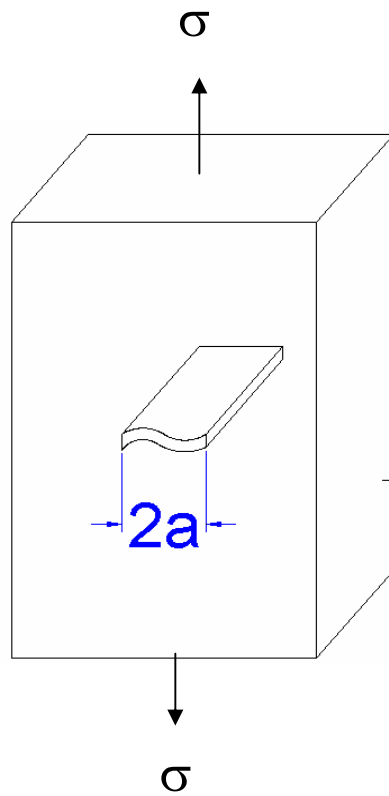
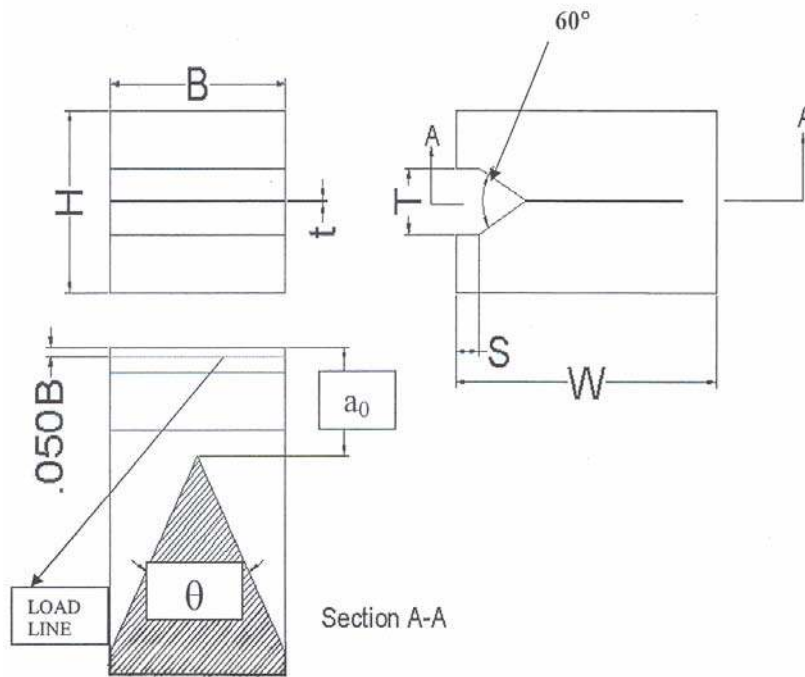


Figure 3: Schematic Drawing of Fracture Toughness Specimens with Edge and Internal Flaws



SYMBOL	DEFINITION	VALUE	TOLERANCE
B	BREADTH	B	
W	LENGTH	1.5B	$\pm .010B$
H	HEIGHT	.870B	$\pm .005B$
a_0	INITIAL CRACK LENGTH	.513B	$\pm .005B$
θ	SLOT ANGLE	55.2°	$\pm 1/2^\circ$
T	SLOT THICKNESS	SEE TABLE III (of Barker, 1981)	
S	GRIP GROOVE DEPTH	.130B	$\pm .010B$
T	GRIP GROOVE WIDTH	.313B	$\pm .005B$
R	RADIUS OF SLOT CUT	SEE FIG 4 (of Barker, 1981)	$\pm 2.5B$

Figure 4: Short Bar Specimen with Straight Chevron Slots. The LOAD LINE is the line along which the opening load is applied in the mouth of the specimen.



Figure 5: The mould for short bar specimens



Figure 6: The short bar specimens

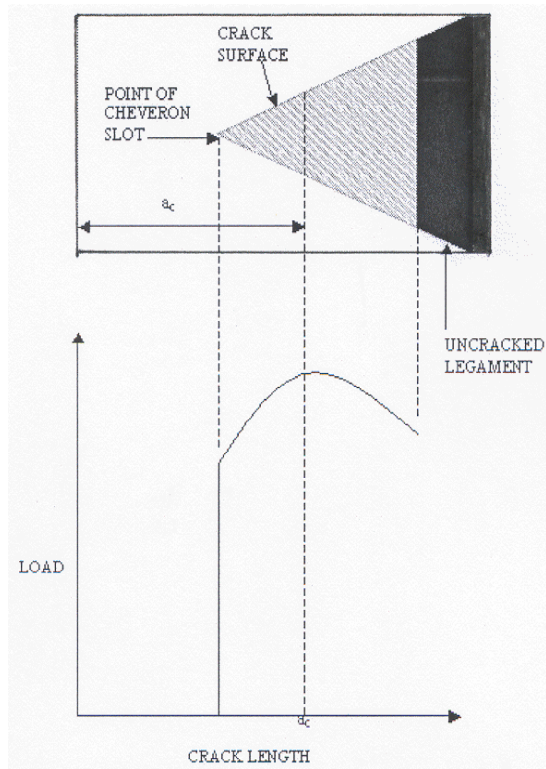


Figure 7: Variation of load versus crack length

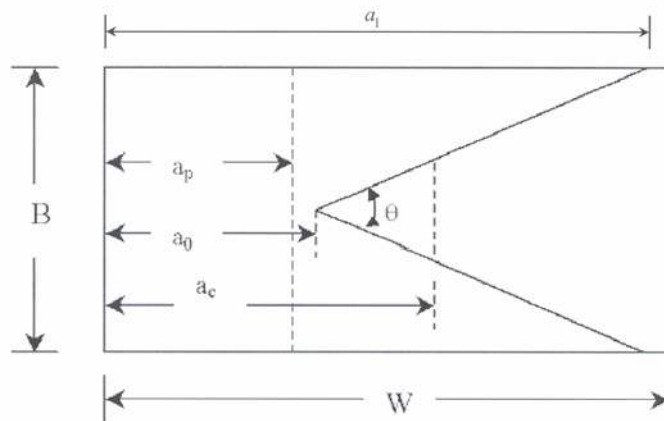


Figure 8: Cross-section dimensions of short bar specimen showing a_1

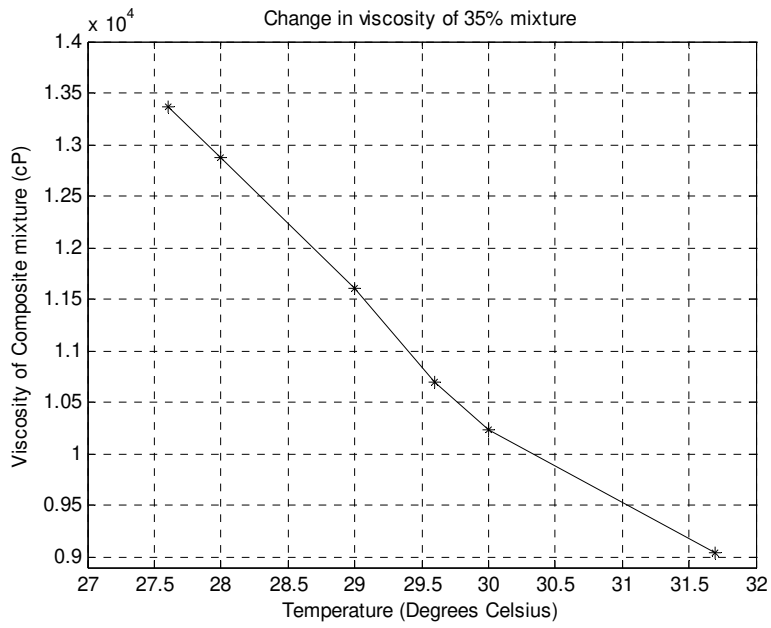


Figure 9: Viscosity change with temperature of 35% by weight of slg composite

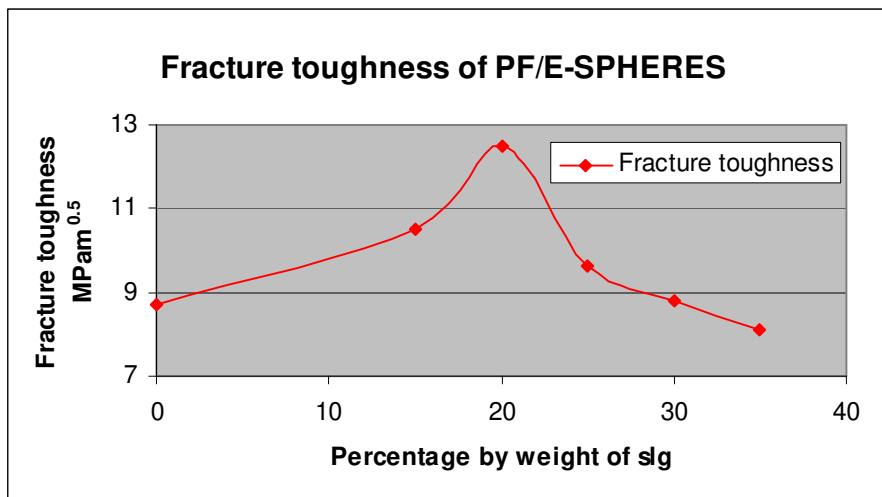


Figure 10: Fracture toughness of PF-E-SPHERES with varying percentage by weight of slg

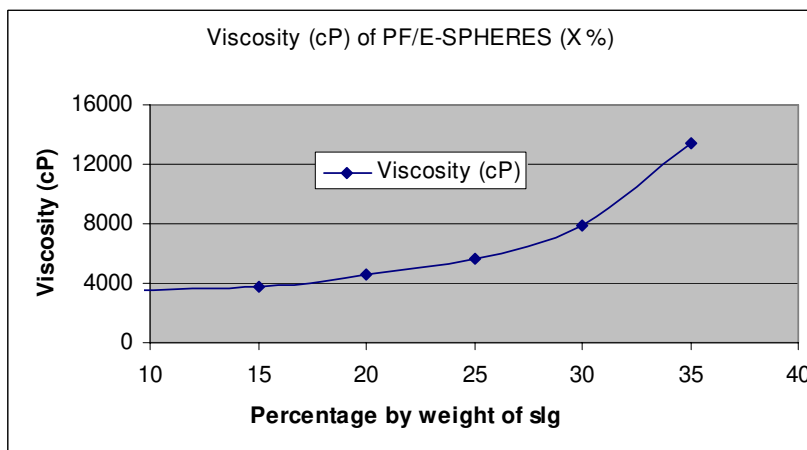


Figure 11: Viscosity of various composite mixtures at approximately 26°C

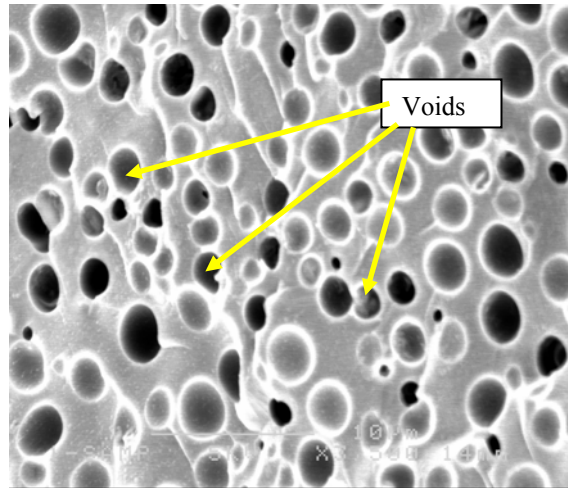


Figure 12: Phenolic resin post-cured for 4 hours at 80 °C at a magnification of 3,500 times

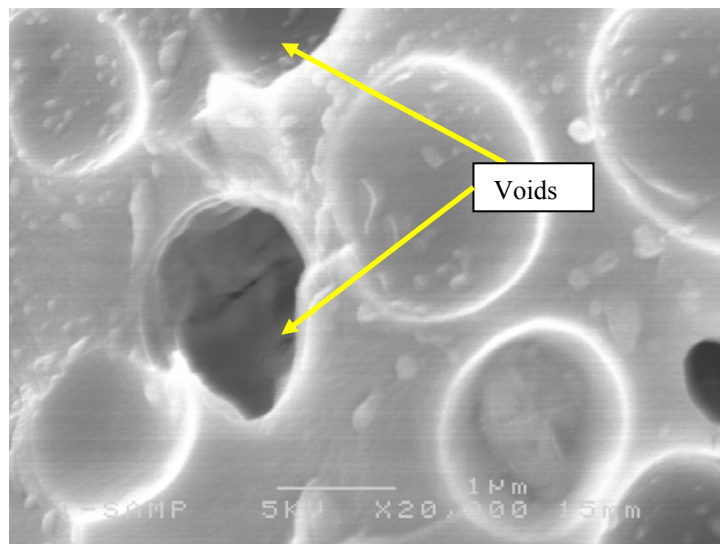


Figure 13: Phenolic resin post-cured for 4 hours at 80 °C at a magnification of 10,000 times

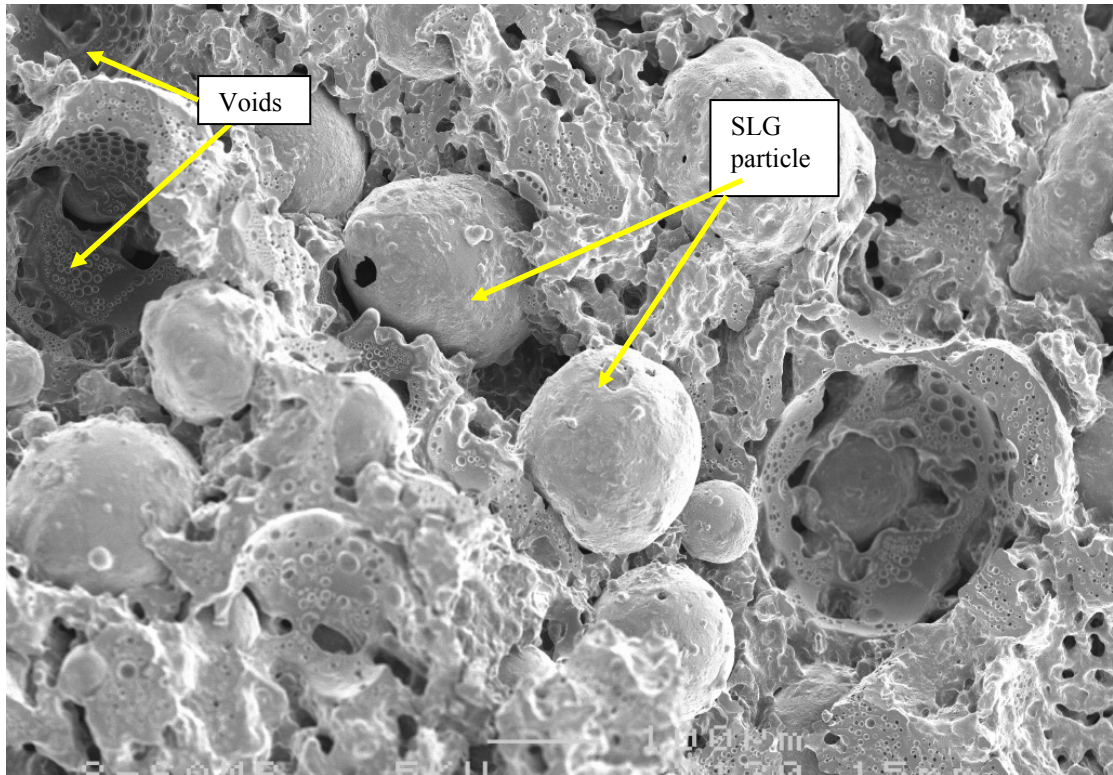


Figure 14: SEM image of phenolic resin reinforced by 20% by weight of slg and post-cured for 4 hours at 80 °C at a magnification of 15,000 X.

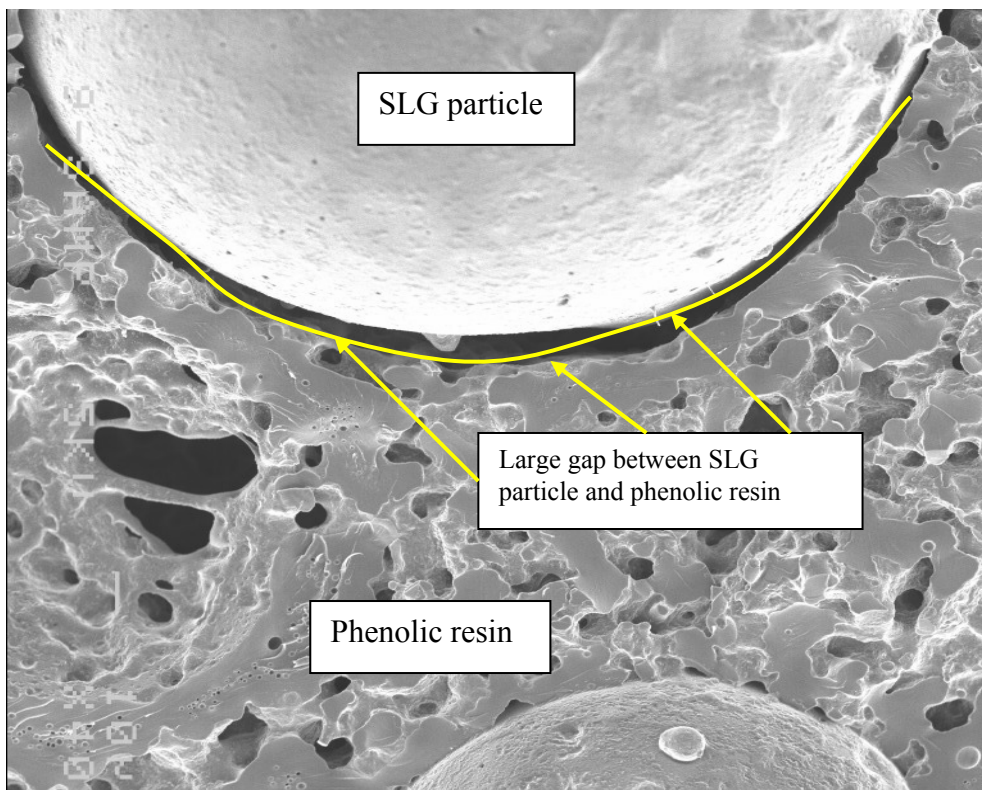


Figure 15: Closer look on more serious gap

Table 1: Weight of materials required to make 300 g of PF/SLG (20%)

Parameters	Materials	Resin (R)	Catalyst (C)	R + C	Slg	Composite
Percentage by weight		20	1	---	---	---
Percentage by weight		---	---	8	2	---
Weight of materials in 300 g of PF/SLG (10%)		229 (g)	11 (g)	240 (g)	60 (g)	300 (g)

Table 2: Fracture toughness of different percentage by weight of slg reinforced phenolic resin

Percentage by weight of slg	0	15	20	25	30	35
Fracture toughness $\text{MPa}\sqrt{m}$	8.72 (1.94) [#]	10.5 (0.80)	12.5 (0.16)	9.62 (0.24)	8.82 (0.36)	8.12 (0.67)

standard deviation