

Gen-Adler: The Generalized Adler's Equation for Injection Locking Analysis in Oscillators

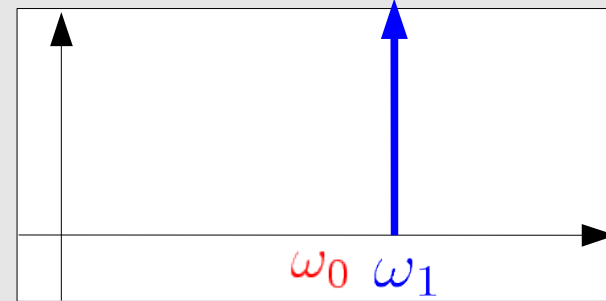
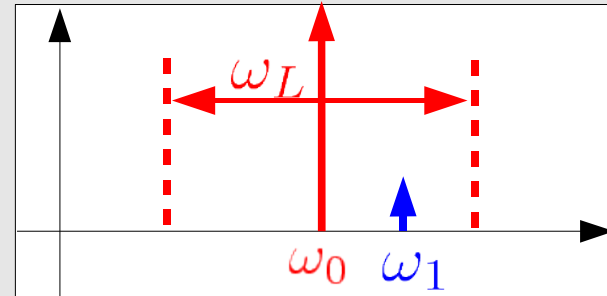
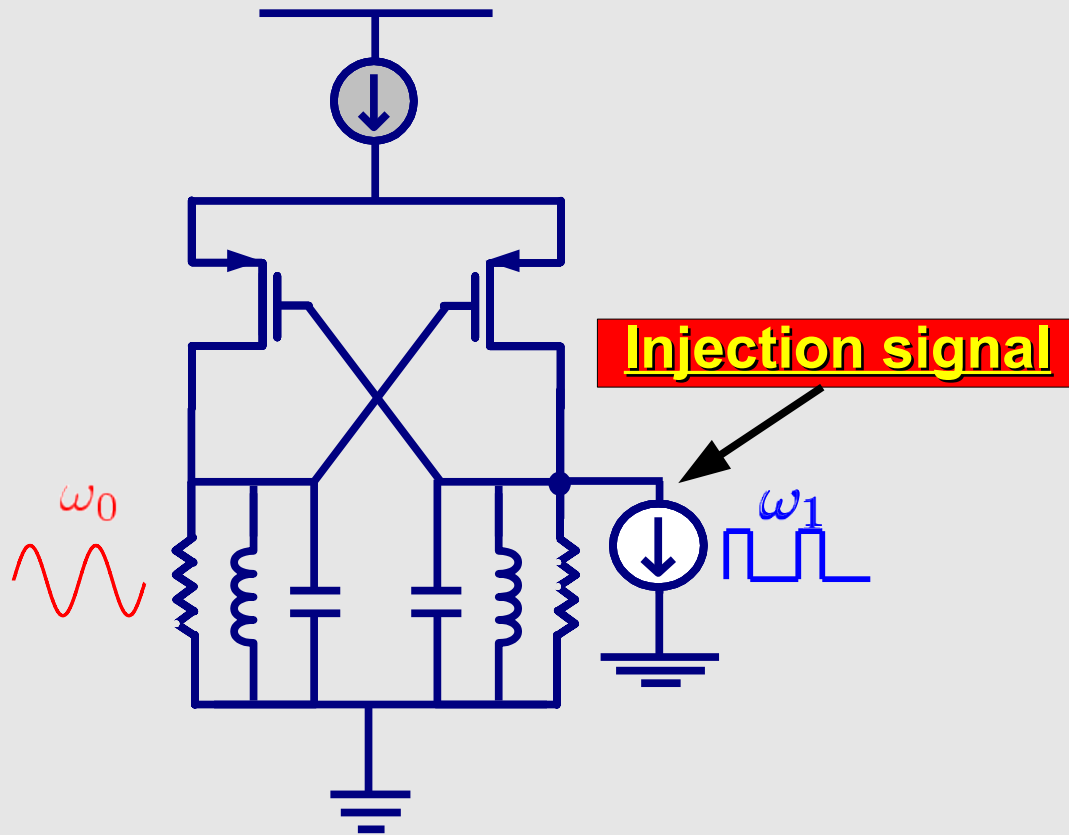
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Outline

- Introduction
 - Challenges involved
- Previous work
 - Adler's equation
- Gen-Adler injection locking equations
 - Ring oscillator
 - Sinusoidal, exponential, square injection signal
- Experimental results
- Conclusion

Introduction



- Injection locking
 - Frequency and phase are locked
- Engineering Applications
 - variable phase shifts, frequency multiplication, low power frequency dividers, precision quadrature generation

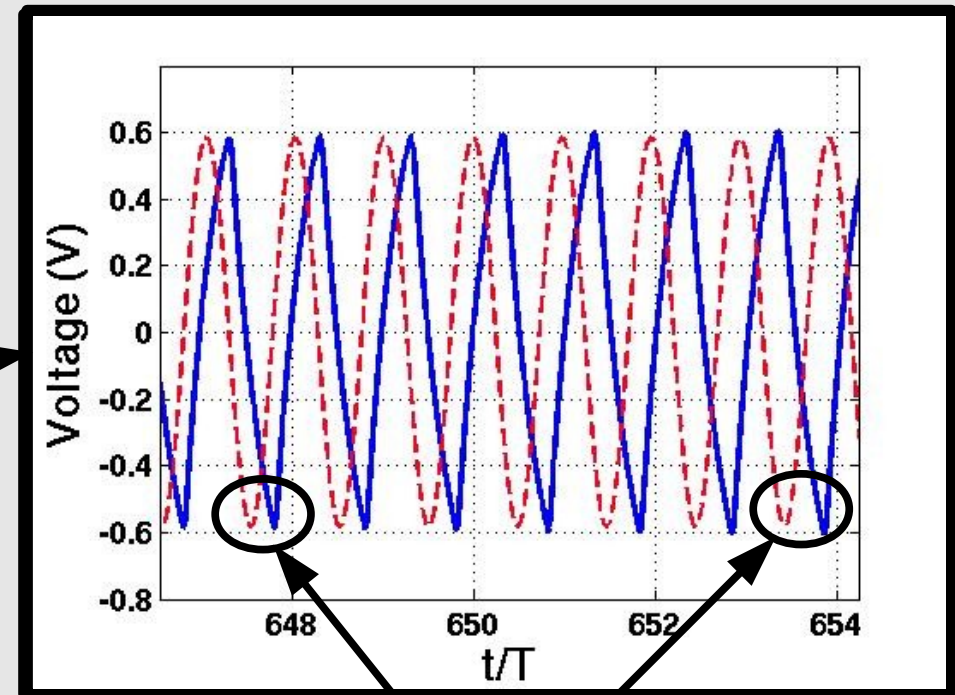
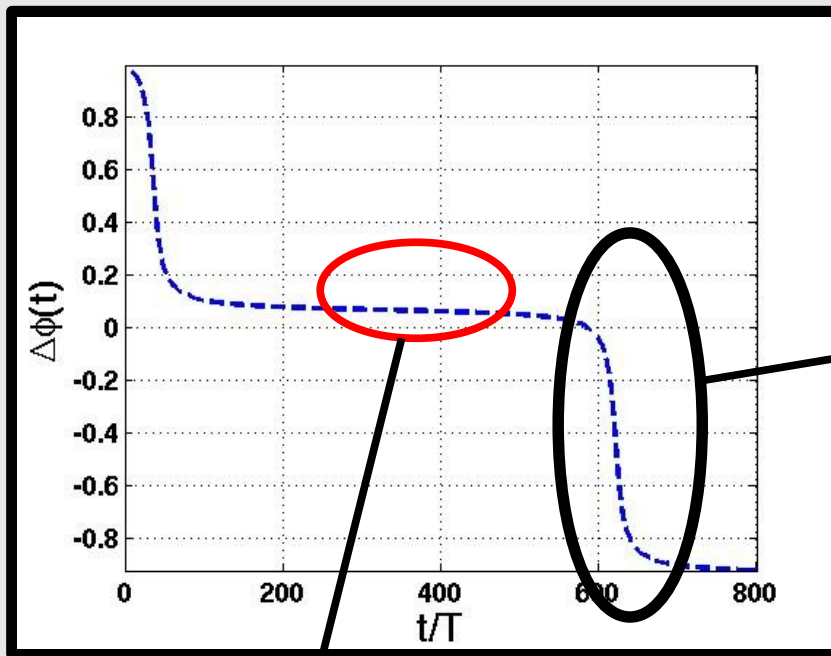
SPICE-level Simulation of Injection Locking

- **Inefficient and inaccurate**
 - Direct simulation of oscillators
 - Extremely small time steps are required
 - Accumulation of phase error
 - Difficult to extract phase and frequency information
 - Locking process can take several cycles
 - Simulation for hundreds of cycles to conclusively declare oscillator locked or unlocked.
 - Distinction between lock and quasi-lock, occurs when injection frequency is just outside the locking range

SPICE-level Simulation of Injection Locking (Cont'd)

Oscillator Waveform —

Injection Signal - - -



Oscillator "appears" to be locked

Not Locked

- Several number of simulations required to determine the oscillator's locking range

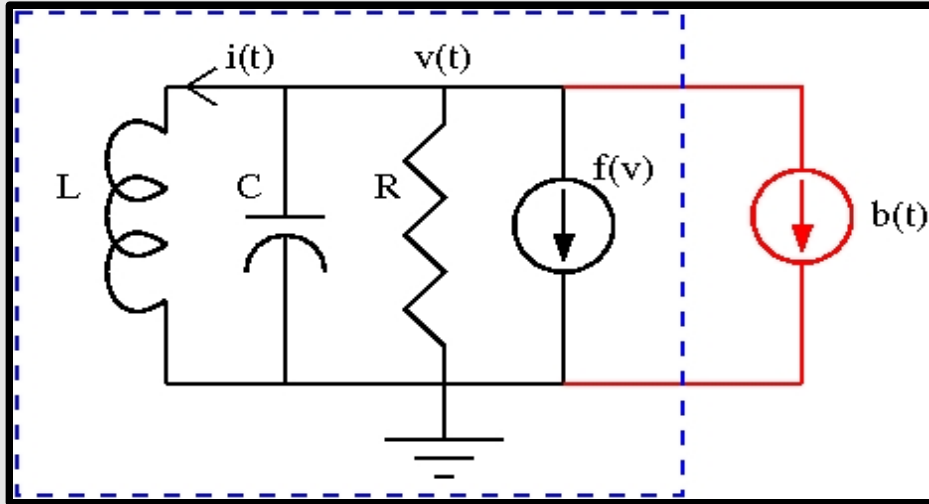
Alternative to SPICE-level simulation required

Previous Work on Injection Locking

1. Adler, R., "[A Study of Locking Phenomena in Oscillators](#)," Proceedings of the IRE , vol.34, no.6, pp. 351-357, June 1946
2. Razavi, B., "[A study of injection locking and pulling in oscillators](#)," Solid-State Circuits, IEEE Journal of , vol.39, no.9, pp. 1415-1424, Sept. 2004
3. Xiaolue Lai; Roychowdhury, J., "[Capturing oscillator injection locking via nonlinear phase-domain macromodels](#)," Microwave Theory and Techniques, IEEE Transactions on , vol.52, no.9, pp. 2251-2261, Sept. 2004
4. Xiaolue Lai; Roychowdhury, J., "[Analytical equations for predicting injection locking in LC and ring oscillators](#)," Custom Integrated Circuits Conference, 2005. Proceedings of the IEEE 2005 , vol., no., pp. 461-464, 18-21 Sept. 2005
5. Gourary, M.M.; Rusakov, S.G.; Ulyanov, S.L.; Zharov, M.M.; Mulvaney, B.J.; Gullapalli, K.K., "[Injection locking conditions under small periodic excitations](#)," Circuits and Systems, 2008. ISCAS 2008. IEEE International Symposium on , vol., no., pp.544-547, 18-21 May 2008
6. Gourary, M.M.; Rusakov, S.G.; Ulyanov, S.L.; Zharov, M.M.; Mulvaney, B.J.; Gullapalli, K.K., "[Smoothed form of nonlinear phase macromodel for oscillators](#)," Computer-Aided Design, 2008. ICCAD 2008. IEEE/ACM International Conference on , vol., no., pp.807-814, 10-13 Nov. 2008

Original Adler's Equation

Adler's Equation



Adler's Equation

$$\frac{d\Delta\phi(t)}{dt} = \Delta f_0 - \frac{I_i}{I_R} \frac{f_0}{2Q} \sin(2\pi\Delta\phi(t))$$

$$v(t) = A \cos(2\pi f_0 t)$$

$$b(t) = I_i \cos(2\pi f_1 t)$$

$\Delta\phi(t)$

Phase difference

Δf_0

Frequency difference

Q

Quality Factor

Injection Locking Dynamics

$$\frac{d\Delta\phi(t)}{dt} = \Delta f_0 - \frac{I_i}{I_R} \frac{f_0}{2Q} \sin(\Delta\phi(t))$$

- Adler's equation provides quick insight into locking dynamics
 - Instantaneous phase difference, $\Delta\phi(t)$
 - Instantaneous frequency of oscillator, $f_{inst} = f_1 + \frac{d\Delta\phi(t)}{dt}$
- In steady state, when oscillator is injection locked
 $\Delta\phi(t) = \text{constant}$

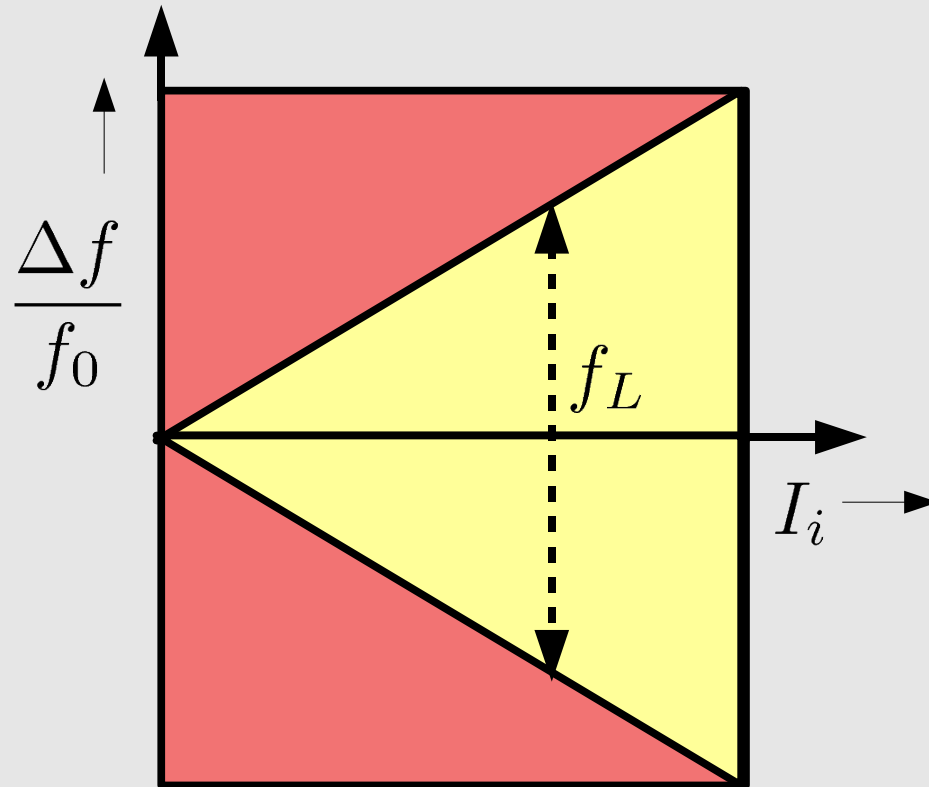
$$\Rightarrow \frac{d\Delta\phi(t)}{dt} = 0 \quad \Rightarrow \quad \frac{\Delta f_0}{f_0} = \frac{I_i}{I_R} \frac{1}{2Q} \sin(\Delta\phi_0)$$

- Analytical equation relating locking range and injection amplitude

Locking Range

$$f_L = 2 \left| \frac{\Delta f_0}{f_0} \right|_{max} = \frac{1}{Q} \frac{I_i}{I_R}$$

Locking Range



- Applicable only to **LC oscillator** (Q explicitly required) with **sinusoidal injection signal**

Review of Perturbation Projection Vector (PPV)

$$\frac{d\vec{x}}{dt} + \vec{f}(\vec{x}) = \vec{b}(t)$$

\vec{x}

Oscillator state variables

\vec{f}

Resistive components

\vec{b}

Perturbation to the oscillator

t

Time

$$\frac{d\vec{x}}{dt} + \vec{f}(\vec{x}) = 0$$

$$\vec{x}_{ss}(t) = [i_L(t), v_C(t)]^T$$

$$\frac{d\vec{x}}{dt} + \vec{f}(\vec{x}) = \vec{b}(t)$$

$$\vec{x}_p(t)$$

$$\vec{x}_p(t) = \vec{x}_{ss}(t + \alpha(t))$$

**Injection
signal**

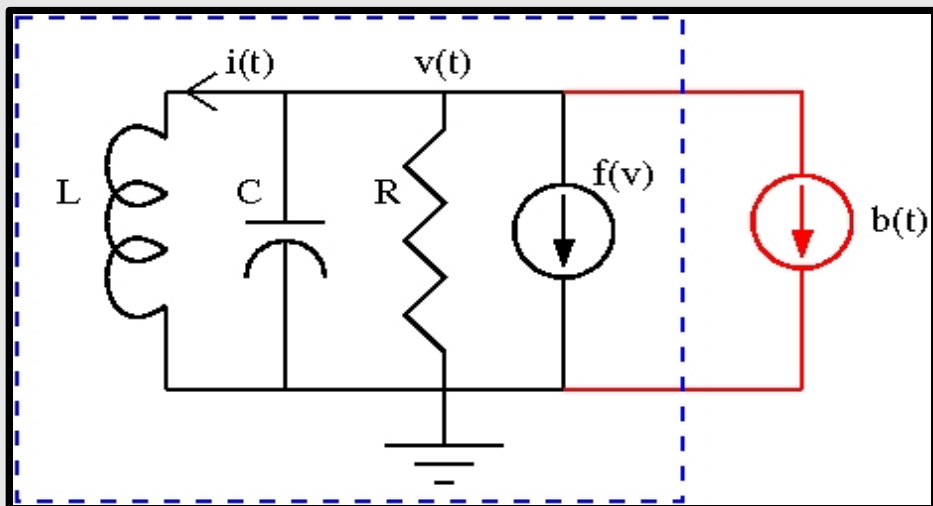
**PPV
equation**

$$\dot{\alpha}(t) = \vec{v}_1^T(t + \alpha(t)) \cdot \vec{b}(t)$$

$$\phi(t) = f_0(t + \alpha(t))$$

Oscillator phase

PPV Equation for LC Oscillator



$$v(t) = A \cos(2\pi f_0 t)$$

$$\vec{v}_1^T(t) = -\sqrt{\frac{L}{C}} \frac{1}{A} \sin(2\pi f_0 t)$$

$$b(t) = I_i \cos(2\pi f_1 t)$$

PPV equation

$$\frac{d\alpha(t)}{dt} = \vec{v}_1^T(t + \alpha(t)) \cdot \vec{b}(t)$$

$$\frac{d\alpha(t)}{dt} = -\sqrt{\frac{L}{C}} \frac{1}{A} \sin(2\pi f_0(t + \alpha(t))) \cdot I_i \cos(2\pi f_1 t)$$

$$\phi_1 = f_1 t$$

$$\alpha(t) = \frac{\Delta\phi}{f_0} + \frac{f_1 - f_0}{f_0} t$$

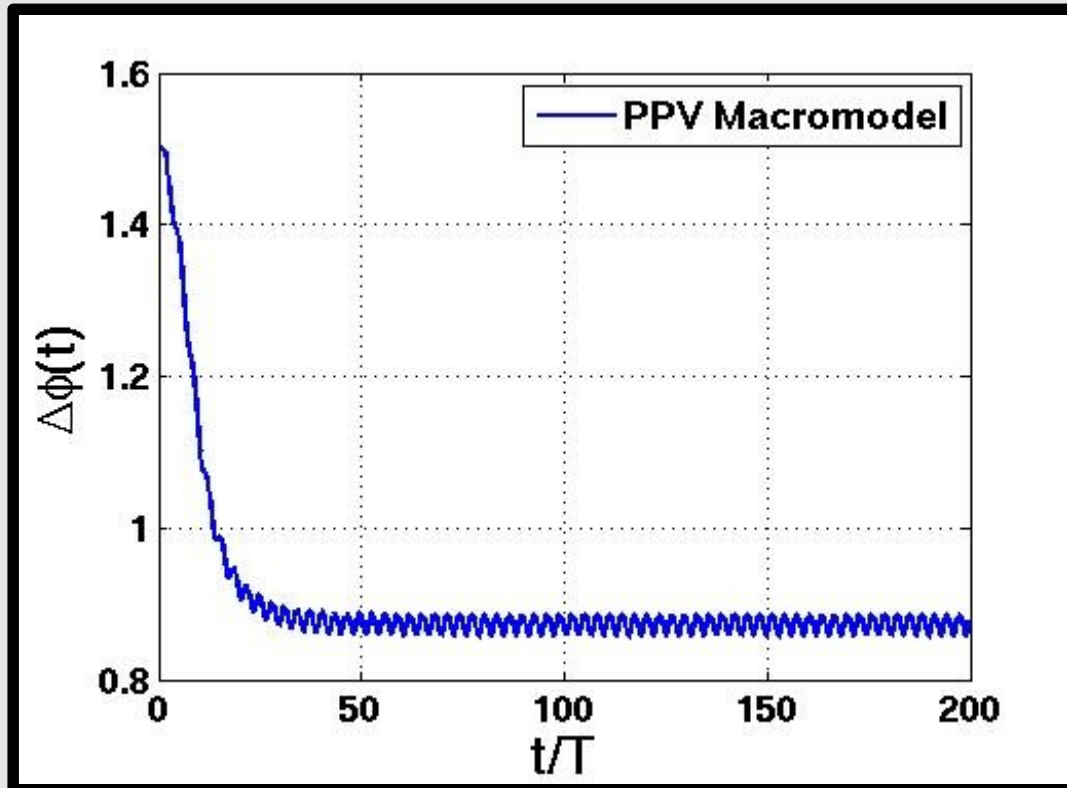
$$\phi = f_0(t + \alpha(t))$$

$$\frac{d\alpha(t)}{dt} = \frac{1}{f_0} \frac{d\Delta\phi}{dt} + \frac{f_1 - f_0}{f_0}$$

$$\Delta\phi(t) = \phi(t) - \phi_1(t)$$

PPV Equation and Phase Difference

$$\frac{d\Delta\phi(t)}{dt} = -(f_1 - f_0) - \frac{I_i}{I_R} \frac{f_0}{2Q} [\sin(2\pi\Delta\phi) + \sin(2\pi\Delta\phi + 2\pi f_1 t)]$$



PPV Equation and Adler's Equation

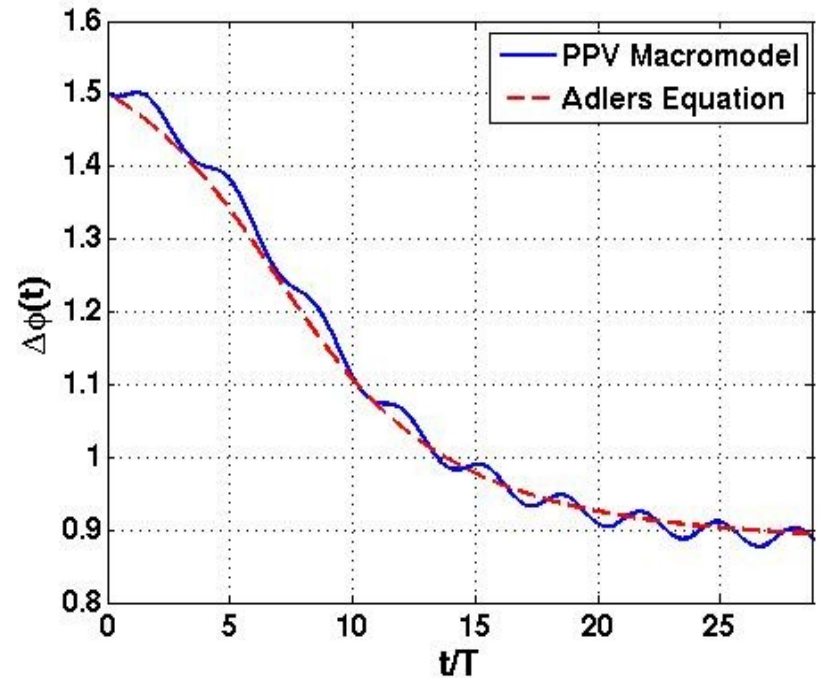
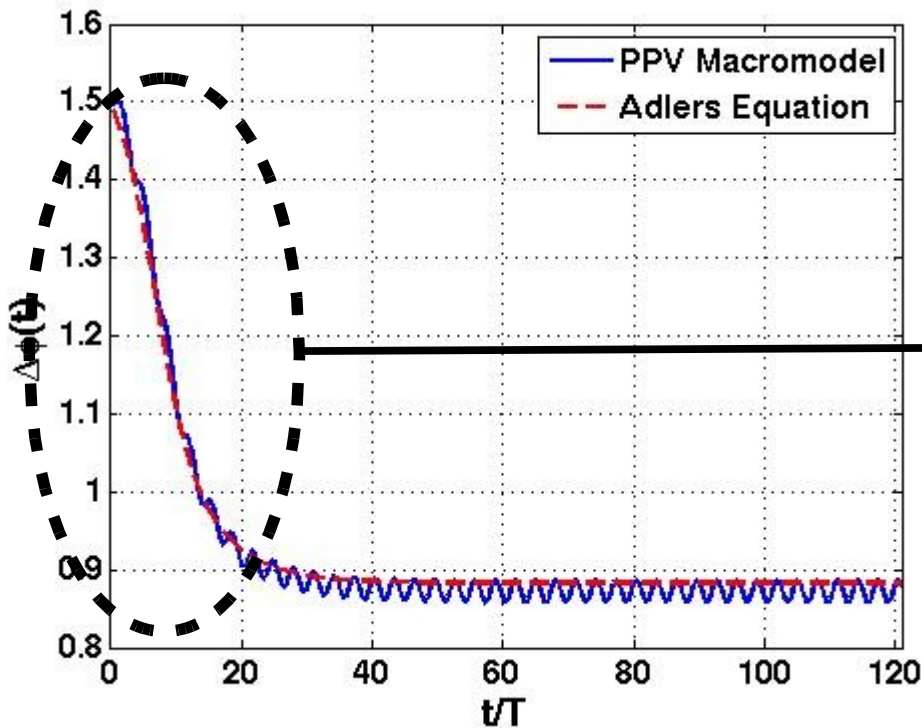
$$\frac{d\Delta\phi(t)}{dt} = -(f_1 - f_0) - \frac{I_i}{I_R} \frac{f_0}{2Q} [\sin(2\pi\Delta\phi)]$$

“fast” varying

$$\phi_1 = f_1 t$$



$$\frac{d\Delta\phi(t)}{dt} = -(f_1 - f_0) - \frac{I_i}{I_R} \frac{f_0}{2Q} [\sin(2\pi\Delta\phi) + \sin(2\pi\Delta\phi + 2\pi f_1 t)]$$



Adler's Equation from PPV Equation

PPV equation

$$\phi_1 = f_1 t$$

$$\frac{d\Delta\phi(t)}{dt} = -(f_1 - f_0) - \frac{I_i}{I_R} \frac{f_0}{2Q} [\sin(2\pi\Delta\phi) + \sin(2\pi\Delta\phi + 2\pi f_1 t)]$$

$$\frac{d\Delta\phi(t)}{dt} = -(f_1 - f_0) - f_0 g(\Delta\phi, \phi_1)$$

Average over "fast" varying variable $\phi_1 = f_1 t$

$$\frac{d\Delta\phi(t)}{dt} = -(f_1 - f_0) - f_0 g(\Delta\phi)$$

$$\frac{d\Delta\phi(t)}{dt} = -(f_1 - f_0) - f_0 \frac{I_i}{I_R} \frac{1}{2Q} [\sin(2\pi\Delta\phi)]$$

Adler's equation

Gen-Adler: Generalized Adler's Equation

Generalized Adler's Equation and PPV Equation

PPV equation

$$\frac{d\alpha(t)}{dt} = \vec{v}_1^T(t + \alpha(t)) \cdot \vec{b}(t) \quad (1)$$

Step 1: $\vec{v}_1^T(t) = \vec{\chi}(f_0 t)$

$$\frac{d\alpha(t)}{dt} = \vec{\chi}(f_0(t + \alpha(t))) \cdot \vec{b}(f_1 t) \quad (2)$$

Step 2: $\Delta\phi(t) = \phi(t) - \phi_1(t)$; $\phi(t) = f_0(t + \alpha(t))$; $\phi_1(t) = f_1 t$

$$\frac{d\Delta\phi(t)}{dt} = -(f_1 - f_0) + f_0 \vec{\chi}(\Delta\phi(t) + \phi_1(t)) \cdot \vec{b}(\phi_1(t))$$

Modified phase equation

Generalized Adler's Equation

$$\frac{d\Delta\phi(t)}{dt} = -(f_1 - f_0) + f_0 \underline{\chi(\Delta\phi(t) + \phi_1(t)) \cdot \vec{b}(\phi_1(t))}$$

Step 3: Average over the “fast” varying variable

$$g(\Delta\phi(t)) = \frac{1}{T_1} \int_0^{T_1} \chi(\Delta\phi(t) + \phi_1(t)) \cdot b(\phi_1(t)) d\phi_1(t)$$

where, $T_1 = \phi_1\left(\frac{1}{f_1}\right)$

$$\frac{d\Delta\phi(t)}{dt} = -(f_1 - f_0) + f_0 g(\Delta\phi(t))$$

$$\left(\frac{d\Delta\phi(t)}{dt}\right)_{max} = -(f_1 - f_0) + f_L/2$$

slow

\ll

$$\frac{d\phi_1(t)}{dt} = f_1$$

fast

Generalized Adler's Equation Contd. ...

$$\frac{d\Delta\phi(t)}{dt} = -(f_1 - f_0) + f_0 g(\Delta\phi(t))$$

- Same form as of original Adler's equation

$$\frac{d\Delta\phi(t)}{dt} = \Delta f_0 - f_0 \frac{I_i}{I_R} \frac{1}{2Q} \sin(\Delta\phi(t))$$

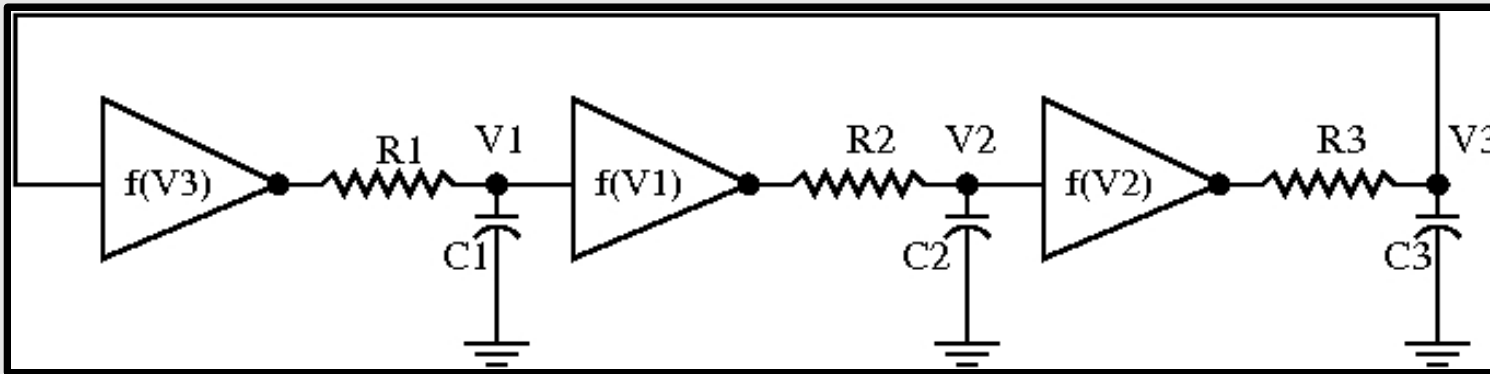
- Applicable for analysis of **any oscillator** unlike original Adler's Equation
- **Any** type of periodic **injection signal**: exponential, sinusoidal, square ...
- Obtained by averaging accurate PPV equation, but has Adler like simplicity

$$g(\Delta\phi(t)) = \frac{1}{T_1} \int_0^{T_1} \chi(\Delta\phi(t) + \phi_1(t)) \cdot b(\phi_1(t)) d\phi_1(t)$$

Analytical formulation

Analytical Formulation of Injection Locking Dynamics in Ring Oscillator

Injection Locking in Ring Oscillator



$$\frac{dv_1}{dt} = -\frac{v_1(t)}{R_1 C_1} + \frac{\tanh(Gm_3 v_3(t))}{R_1 C_1}$$

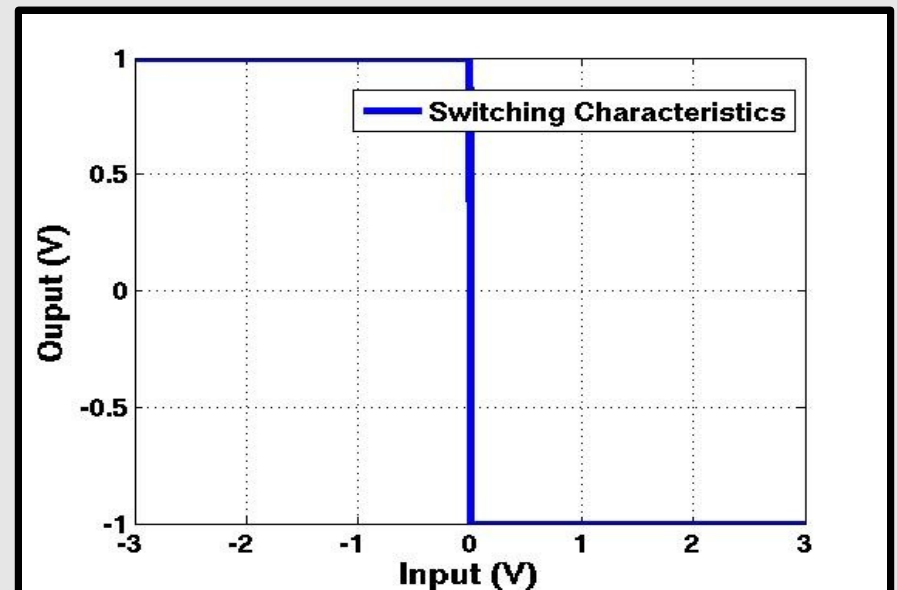
$$\frac{dv_2}{dt} = -\frac{v_2(t)}{R_2 C_2} + \frac{\tanh(Gm_1 v_1(t))}{R_2 C_2}$$

$$\frac{dv_3}{dt} = -\frac{v_3(t)}{R_3 C_3} + \frac{\tanh(Gm_2 v_2(t))}{R_3 C_3}$$

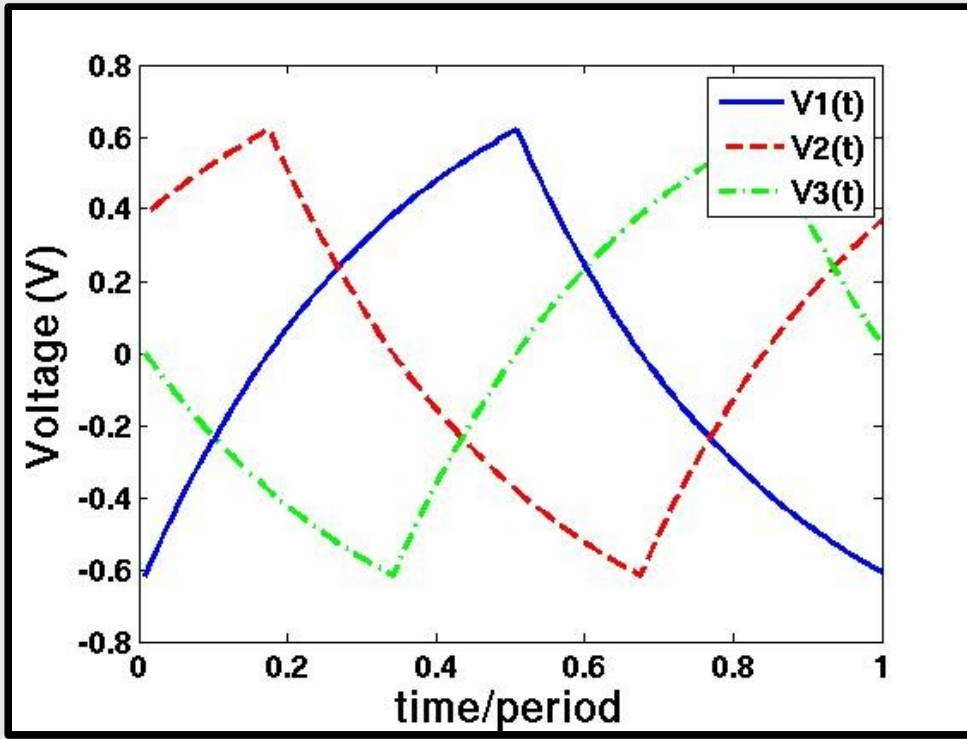
$$G_m \implies \infty$$

Ideal switching characteristics

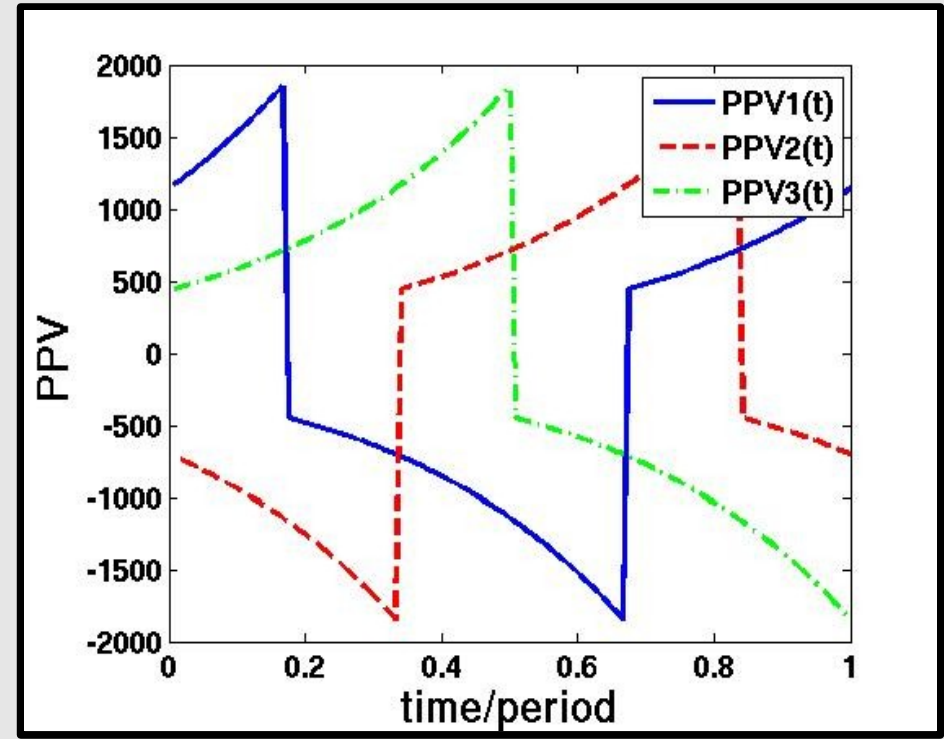
Three stage ring oscillator DEs



Ring Oscillator's PPV



Steady State Waveforms

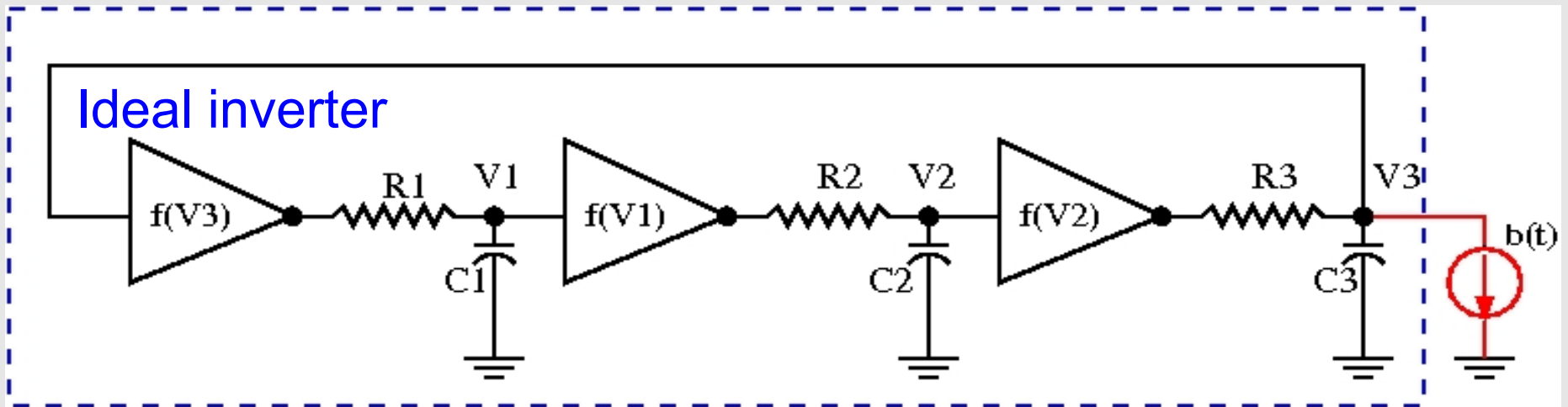


PPV Waveforms

$$v_1^T(t) = \begin{cases} \frac{1}{\sqrt{5}} \frac{R}{A} e^{\frac{t}{\tau}} & \text{if } 0 \leq t < \frac{T}{2} \\ \frac{R}{A} \left(\frac{2}{\sqrt{5}} - 1 \right) e^{\frac{t}{\tau}} & \text{if } \frac{T}{2} \leq t < T \end{cases}$$

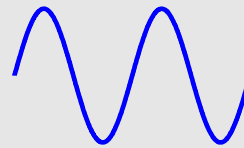
PPV at node V3

Gen-Adler for Ring Oscillator

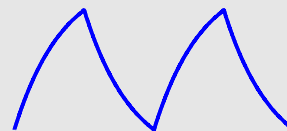


$$g(\Delta\phi(t)) = \frac{1}{T_1} \int_0^{T_1} \chi(\Delta\phi(t) + \phi_1(t)) \cdot b(\phi_1(t)) d\phi_1(t)$$

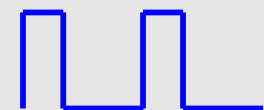
- Sinusoidal injection signal



- Exponential injection signal



- Square injection signal (with any duty cycle)



Analytical Injection Locking Dynamic Equations

$$\frac{d\Delta\phi(t)}{dt} = -(f_1 - f_0) + f_0 g(\Delta\phi(t))$$

Sinusoidal Injection to a ring oscillator

$$g(\Delta\phi(t)) = \frac{1}{\sqrt{4\pi^2 + K_0^2}} \frac{RI_i}{A} \sin(2\pi\Delta\phi(t) + \zeta) \times \left[K_1(e^{K_0/2} + 1) - K_2(e^{K_0} + e^{K_0/2}) \right]$$

$$\text{where, } \sin(\zeta) = \frac{2\pi}{\sqrt{4\pi^2 + K_0^2}}$$

$$K_0 = 2.887, \quad K_1 = \frac{1}{\sqrt{5}}, \quad K_2 = \left(\frac{2}{\sqrt{5}} - 1 \right)$$

Injection Locking Range

- In steady state, when oscillator is injection locked

$$\Delta\phi(t) = \Delta\phi_0(\text{constant}) \quad \longrightarrow \quad \frac{d\Delta\phi(t)}{dt} = 0$$

$$\frac{d\Delta\phi(t)}{dt} = -(f_1 - f_0) + f_0 g(\Delta\phi(t))$$

$$0 = -(f_1 - f_0) + f_0 g(\Delta\phi_0) \quad \longrightarrow \quad \frac{\Delta f_0}{f_0} = g(\Delta\phi_0)$$

$$\Delta f_{0max} = f_0 [g(\Delta\phi_0(t))]_{max}$$

$$|\Delta f_0|_{max} = \frac{f_0}{\sqrt{4\pi^2 + K_0^2}} \frac{RI_i}{A} \left[K_1(e^{K_0/2} + 1) - K_2(e^{K_0} + e^{K_0/2}) \right] = 0.6773 f_0 \frac{RI_i}{A}$$

$$f_L = 2\Delta f_{0max}$$

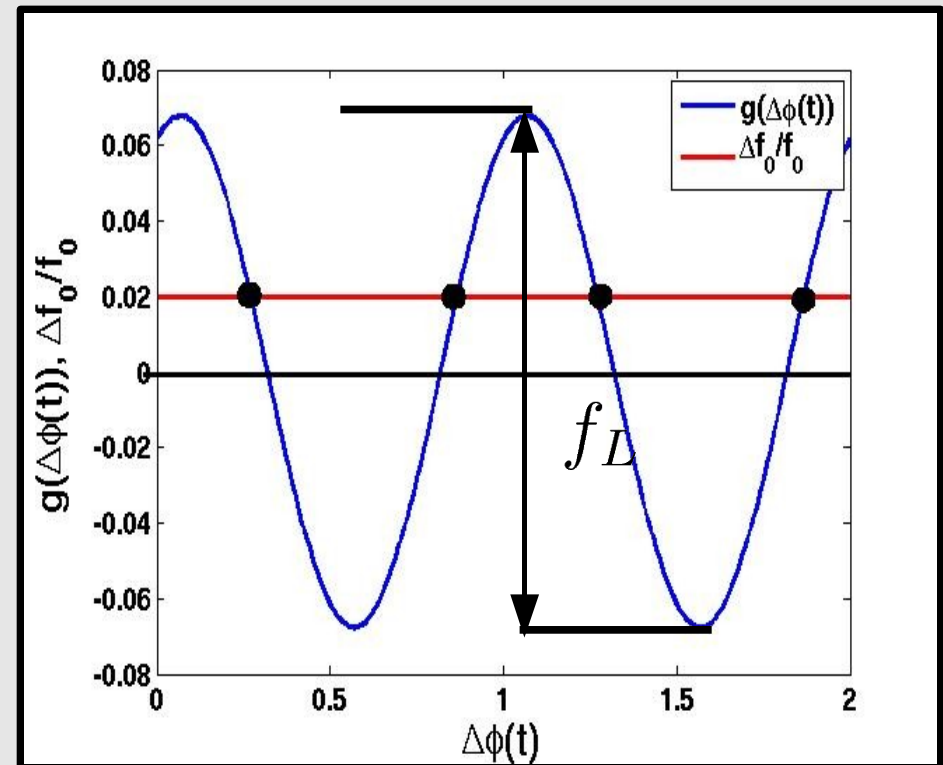
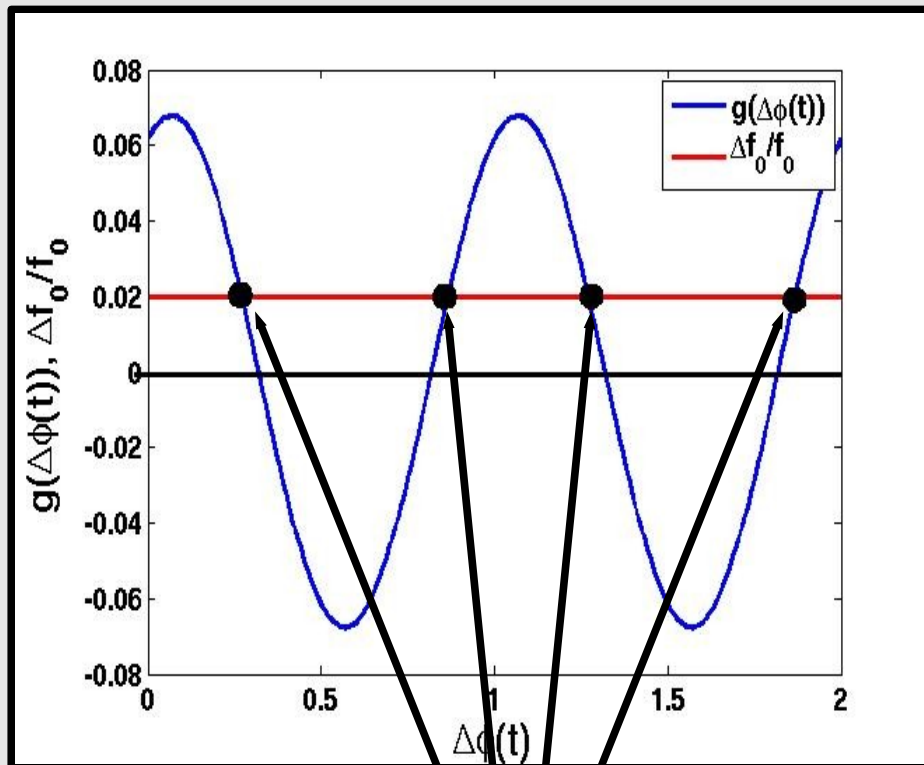
Lock Range

Graphical Injection Locking Analysis

$$\frac{d\Delta\phi(t)}{dt} = -(f_1 - f_0) + f_0 g(\Delta\phi(t))$$

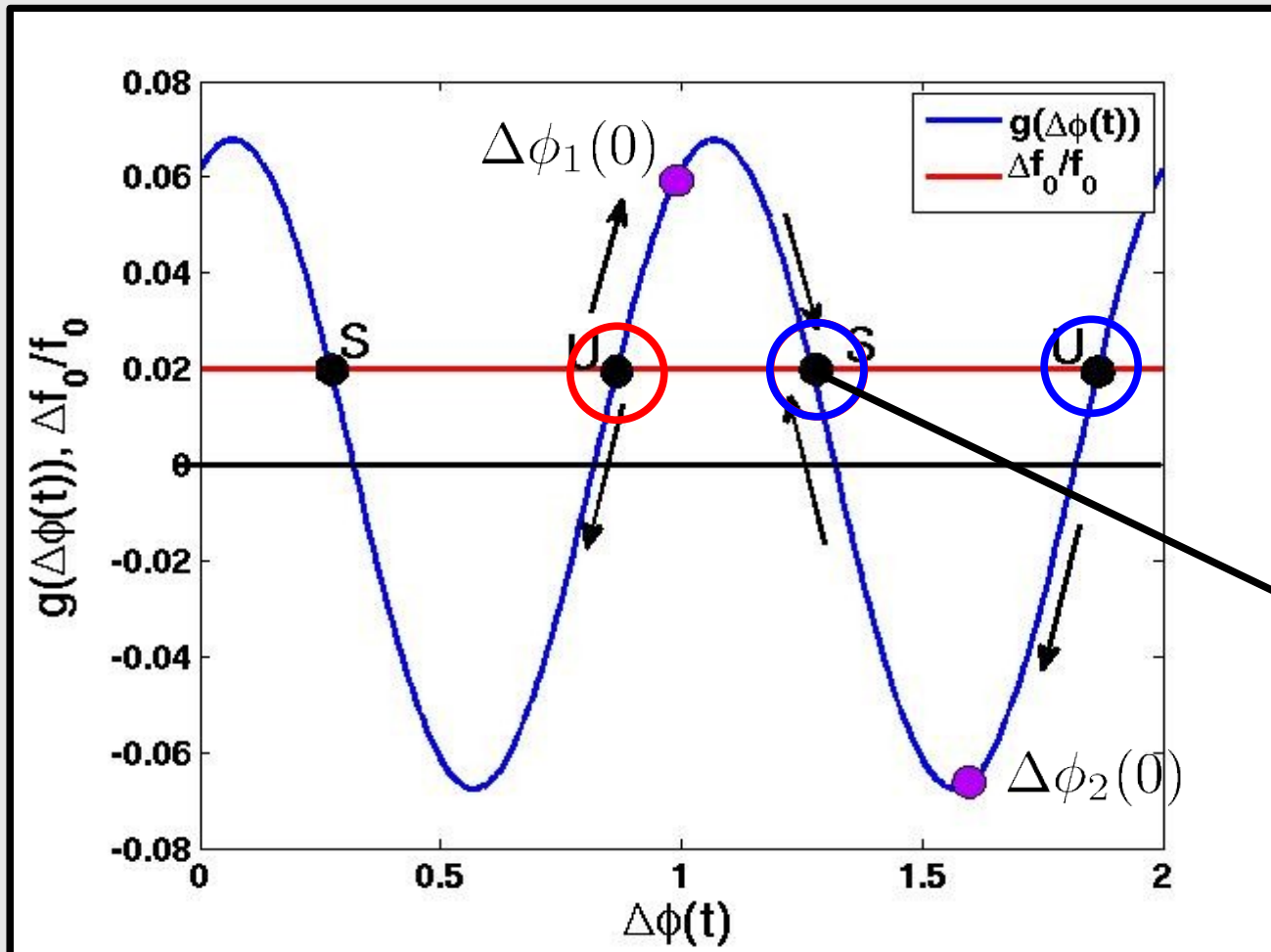
$$0 = -(f_1 - f_0) + f_0 g(\Delta\phi_0)$$

$$\frac{\Delta f_0}{f_0} = g(\Delta\phi_0)$$



Steady state phase

Graphical Injection Locking Analysis



$$\left(\frac{d\Delta\phi(t)}{dt} \right)_{\Delta\phi_1(0)} > 0$$

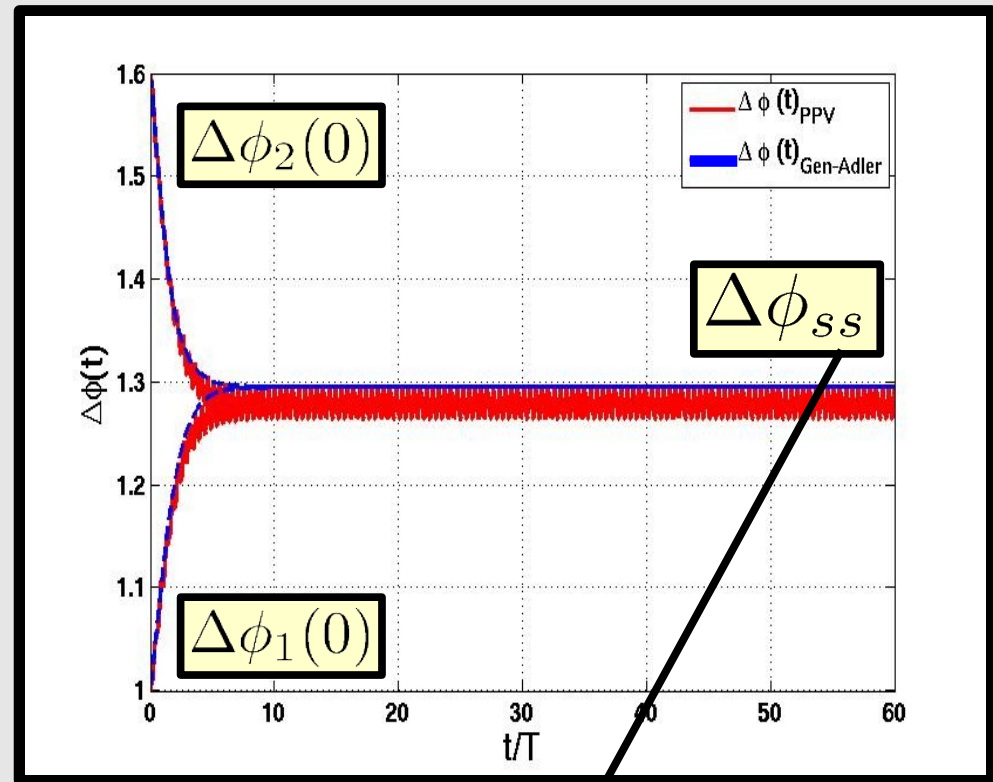
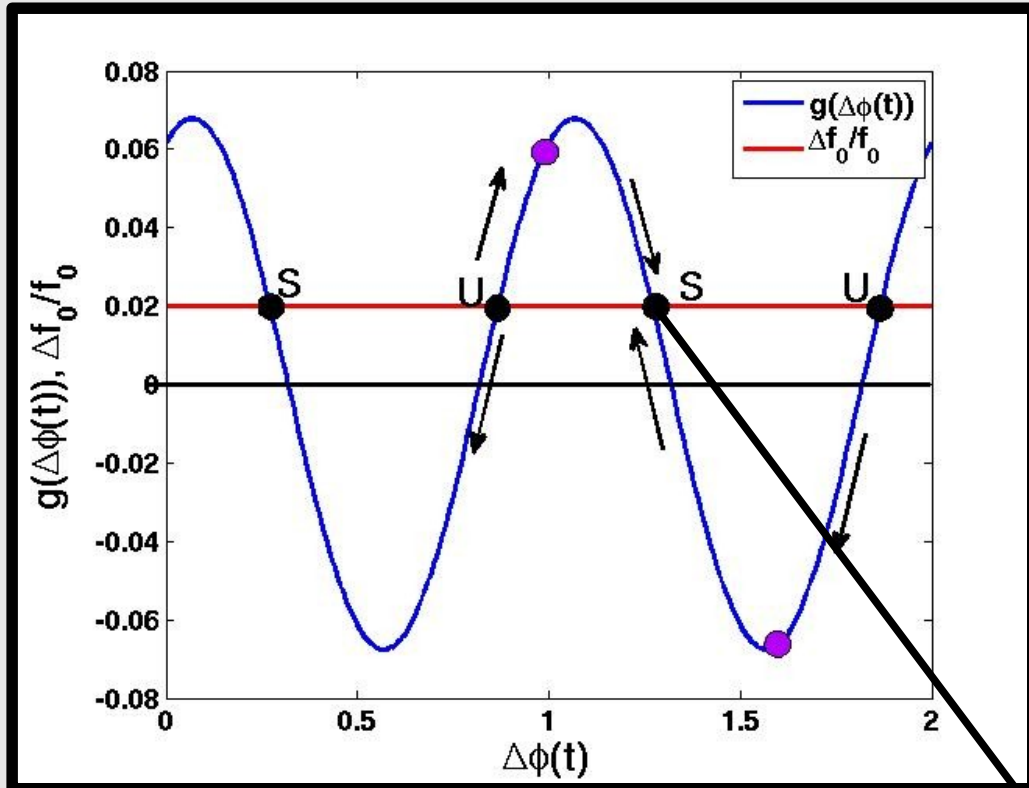
$$\Delta\phi_{ss} = 1.295$$

$$\left(\frac{d\Delta\phi(t)}{dt} \right)_{\Delta\phi_2(0)} < 0$$

$$\frac{d\Delta\phi(t)}{dt} = f_0 \left(g(\Delta\phi(t)) - \frac{\Delta f_0}{f_0} \right)$$

- **Unstable and stable steady state phase**

Graphical Injection Locking Analysis



$$\Delta\phi = 1.295$$

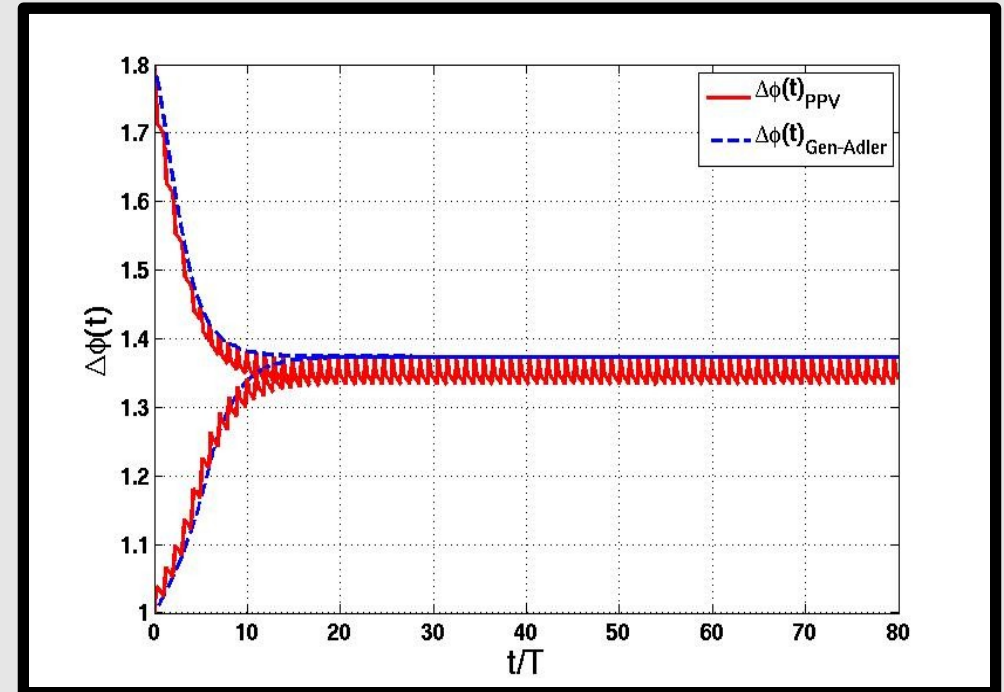
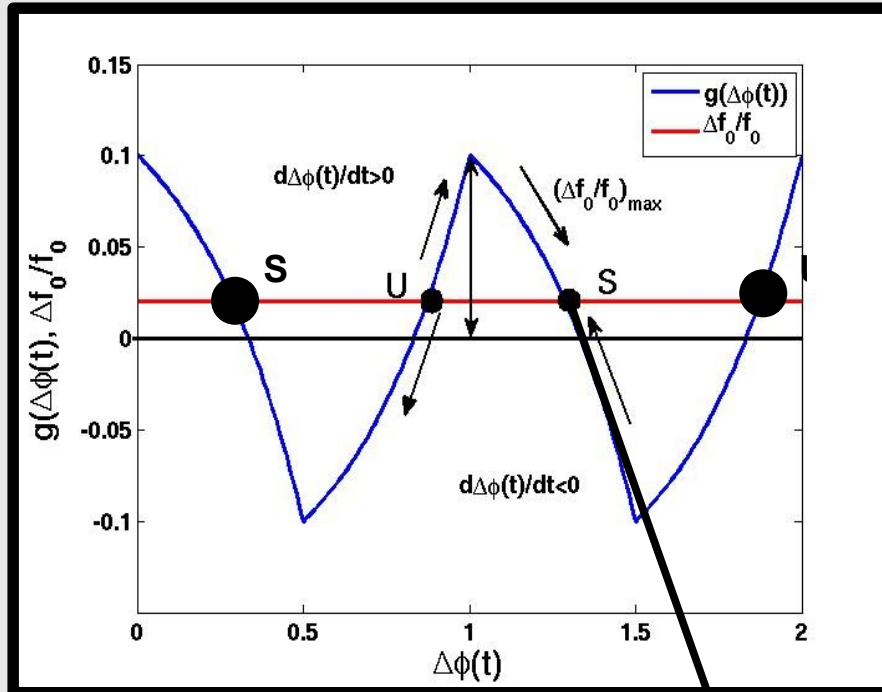
Square Wave Injection Signal

$$g(\Delta\phi(t)) = \begin{cases} \frac{RI_i}{A} \frac{K_1}{K_0} \left[e^{K_0\Delta\phi(t)} (e^{\eta K_0} - 1) \right] \\ \quad \text{if } 0 \leq \Delta\phi(t) < \frac{1}{2} - \eta \\ \\ \frac{RI_i}{A} \frac{1}{K_0} \left[(K_1 - K_2)e^{K_0/2} + e^{K_0\Delta\phi(t)} (K_2e^{\eta K_0} - K_1) \right] \\ \quad \text{if } \frac{1}{2} - \eta \leq \Delta\phi(t) < \frac{1}{2} \\ \\ \frac{RI_i}{A} \frac{K_2}{K_0} \left[e^{K_0\Delta\phi(t)} (e^{\eta K_0} - 1) \right] \\ \quad \text{if } \frac{1}{2} \leq \Delta\phi(t) < 1 - \eta \\ \\ \frac{RI_i}{A} \frac{1}{K_0} \left[(K_1 - K_2)e^{K_0/2} + e^{K_0\Delta\phi(t)} (K_2 - K_1e^{(\eta-1)K_0}) \right] \\ \quad \text{if } 1 - \eta \leq \Delta\phi(t) < 1 \end{cases}$$

$0 \leq \eta < 0.5 \quad \eta = \text{duty cycle of square wave}$

$$\frac{d\Delta\phi(t)}{dt} = -(f_1 - f_0) + f_0 g(\Delta\phi(t))$$

Square Wave Injection Signal

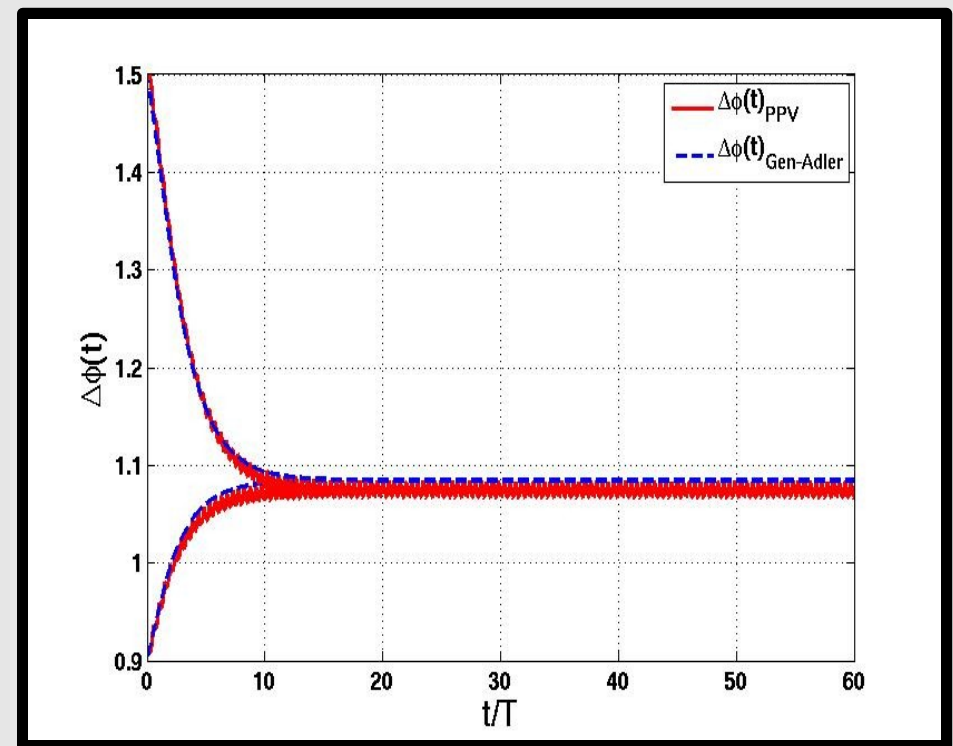
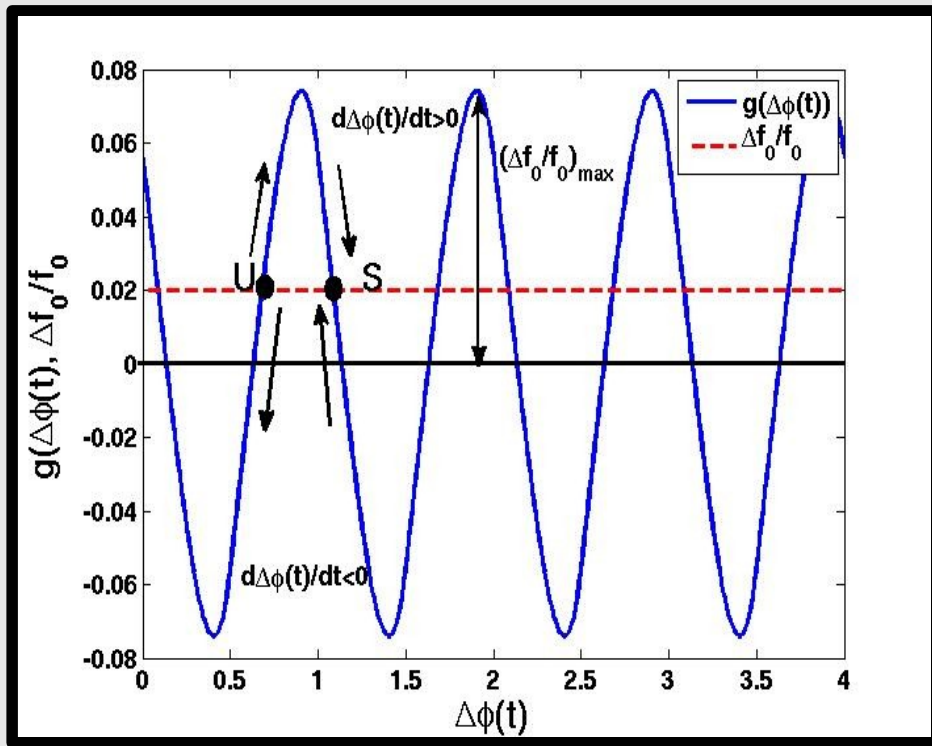


$$\Delta\phi = 1.3735$$

Lock Range

$$f_L = 2f_0 \frac{RI_i}{A} \frac{K_1}{K_0} \left[e^{K_0/2} (1 - e^{-\eta K_0}) \right]$$

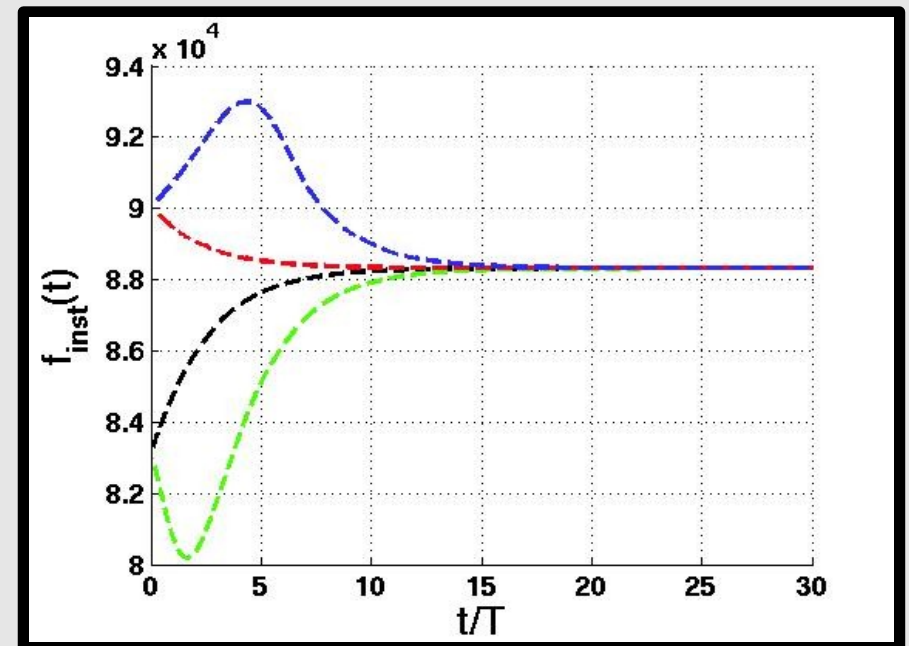
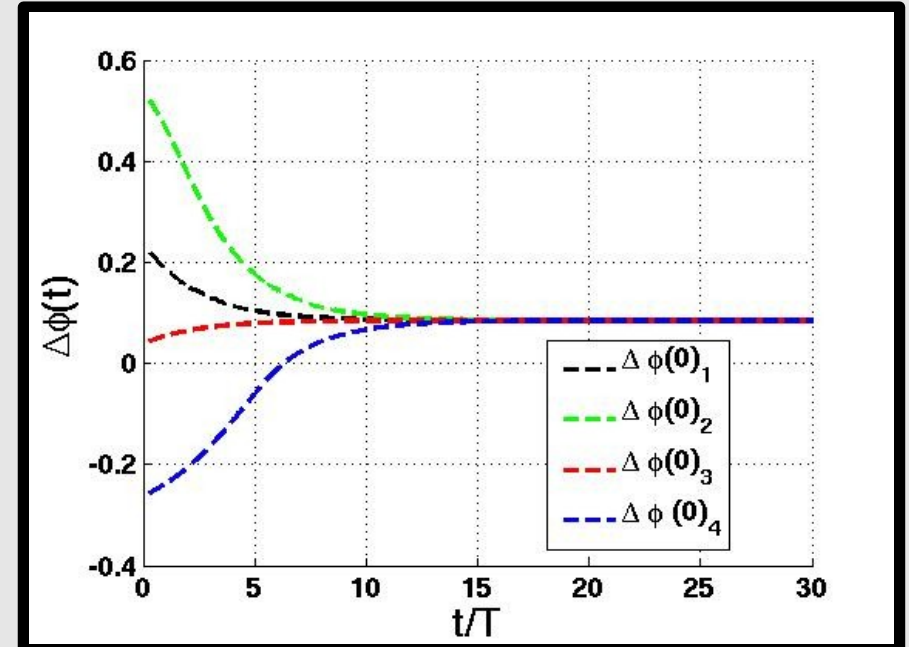
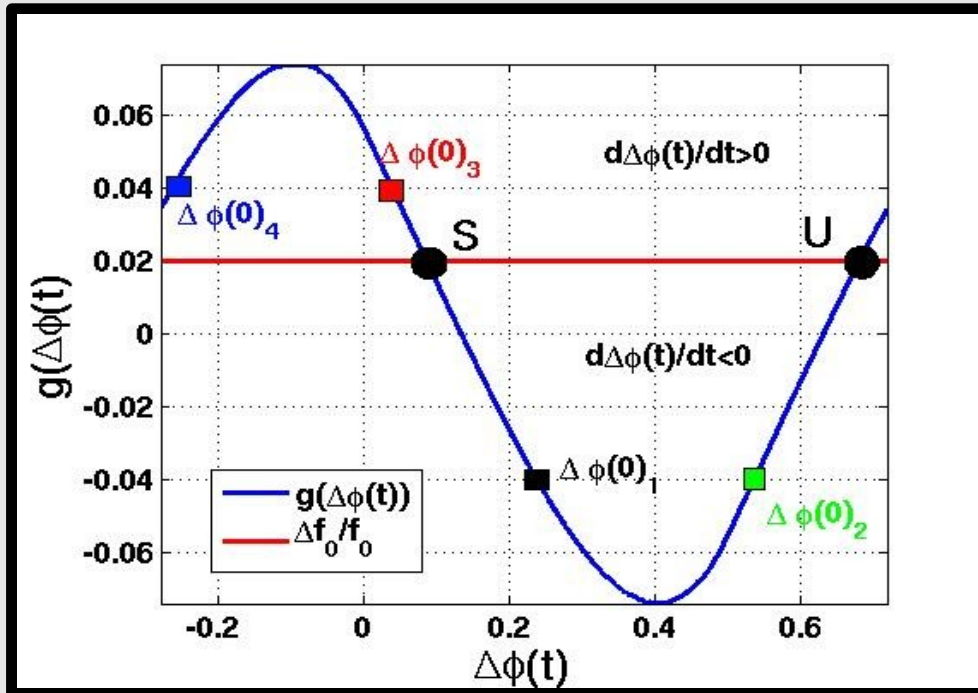
Exponential Injection Signal



Lock Range

$$f_L = 0.744 f_0 \frac{RI_i}{A}$$

Instantaneous Phase and Frequency

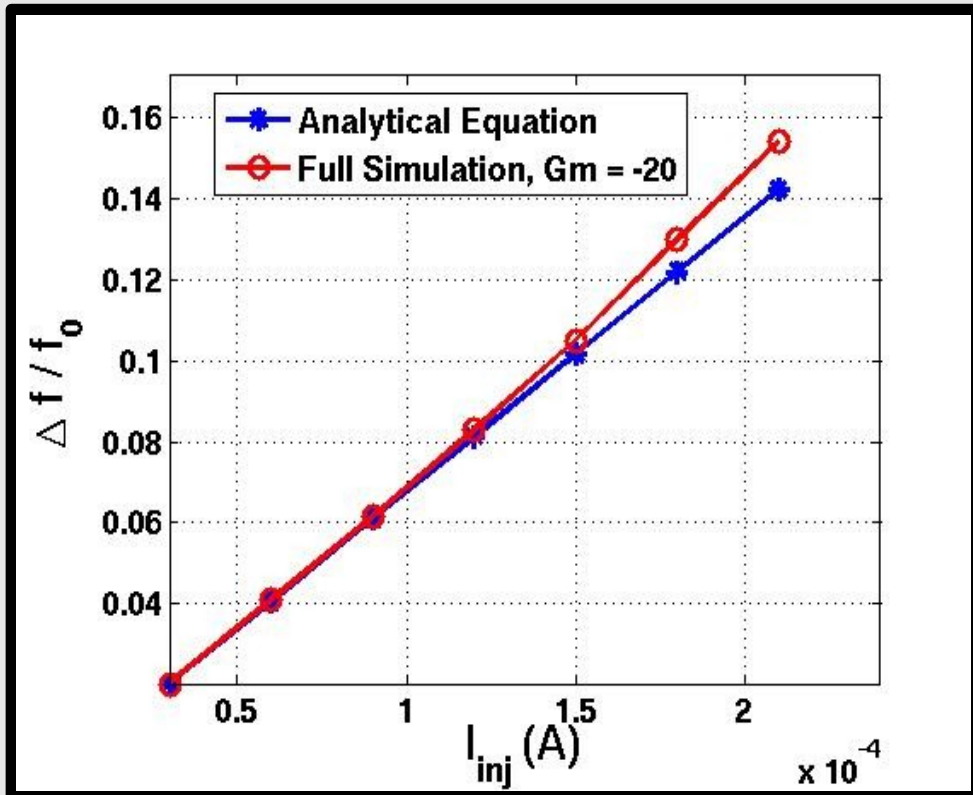


$$\frac{d\Delta\phi(t)}{dt} = -(f_1 - f_0) + f_0 g(\Delta\phi(t))$$

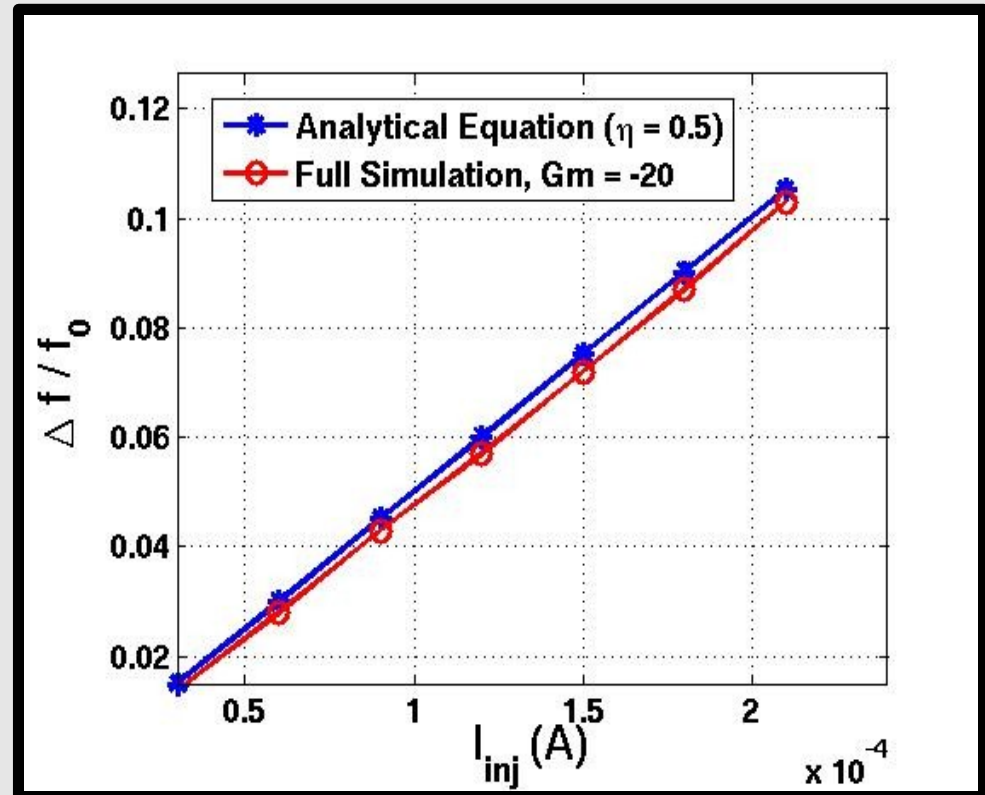
$$f_{inst} = \frac{d\Delta\phi(t)}{dt} + f_1$$

$$f_{inst} = f_0 + f_0 g(\Delta\phi(t))$$

Comparison with Full Simulation



Sinusoidal Injection



Square Wave Injection

Excellent match with the full simulation

Conclusion

- Simple analytical equations for injection locking analysis in ring oscillators
 - maintain Adler like **simplicity**
 - quick **insight** into injection locking process via graphical analysis
 - **hand analysis** of injection locking range for variety of injection signals
 - good match with the full simulation
- Gen-Adler is numerically applicable to any oscillator for injection locking analysis

End