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Hydrodynamic limits and numerical errors of isothermal lattice Boltzmann schemes

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ABSTRACT

With the aim of better understanding the numerical properties of the lattice Boltzmann method (LBM), a general methodology is proposed to derive its hydrodynamic limits in the discrete setting. It relies on a Taylor expansion in the limit of low Knudsen numbers. With a single asymptotic analysis, two kinds of deviations with the Navier-Stokes (NS) equations are explicitly evidenced: consistency errors, inherited from the kinetic description of the LBM, and numerical errors attributed to its space and time discretization. The methodology is applied to the Bhatnagar-Gross-Krook (BGK), the regularized and the multiple relaxation time (MRT) collision models in the isothermal framework. Deviation terms are systematically confronted to linear analyses in order to validate their expressions, interpret them and provide explanations for their numerical properties. The low dissipation of the BGK model is then related to a particular pattern of its error terms in the Taylor expansion. Similarly, dissipation properties of the regularized and MRT models are explained by a phenomenon referred to as *hyperviscous degeneracy*. The latter consists in an unexpected resurgence of high-order Knudsen effects induced by a large numerical prefactor. It is at the origin of over-dissipation and severe instabilities in the low-viscosity regime.

1. Introduction

Over the last three decades, the lattice Boltzmann method (LBM) has become a promising alternative to conventional methods in computational fluid dynamics (CFD) [1–4]. Inherited from lattice gas automata [5], it relies on a simplified statistical description of a gas inspired by the Boltzmann equation, encompassing a macroscopic flow behaviour usually modelled by the Navier-Stokes (NS) equations [6,7]. The great success of the LBM lies in the simplicity of its numerical scheme. It is based on a two-step Strang-like splitting method [8]: first a local collision step designed to mimic the effects of inter-particle collisions, followed by a node-to-node streaming of discrete populations on a Cartesian grid. The ensuing method offers an easy handling of complex geometries [9] together with an efficient and simply parallelizable algorithm [10]. However, in addition to a common athermal hypothesis required to preserve the narrow stencil of the method [11,12], standard lattice Boltzmann (LB) solvers suffer from a lack of robustness when the Mach number increases and in the inviscid limit [13,14]. This defect is often attributed to the presence of unstable non-hydrodynamic modes consequent of the kinetic fluid description [13,15,16].

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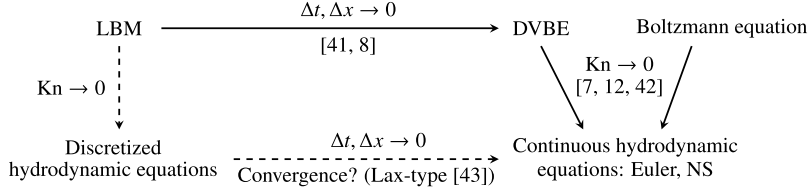


Fig. 1. Illustration, inspired from [44], of the asymptotic convergence of the LBM towards the Euler and NS equations, involving the time and space discretizations Δt and Δx and the Knudsen number Kn . Dashed arrows are scrutinized in the present work.

Historical attempts to enhance the numerical stability of LB solvers turned towards the pursuit of a more sophisticated collision kernel than the simple Bhatnagar–Gross–Krook (BGK) approximation [17]. The latter aims at relaxing distribution functions towards a discrete counterpart of the Maxwell-Boltzmann equilibrium with a single relaxation rate, eventually related to the kinematic viscosity. Noticing its stability issues, several authors proposed an extension of this approach using multiple relaxation times (MRT) in the aim of dissipating independently non-hydrodynamic modes, while preserving the correct macroscopic equations in the hydrodynamic limit [18,13,19]. Based on this idea, several models subsequently emerged, including the two-relaxation-time (TRT) scheme designed to reduce the large number of degrees of freedom allowed by the MRT [20,21], or the so-called cascaded models, performing the collision step in the local flow frame with a view to reduce Galilean invariance errors [22–24]. A second family of collision models, referred to as *regularized models*, aims at filtering out the non-hydrodynamic content of the distribution functions before the collision step [25–29]. They are built by analogy with a Chapman-Enskog expansion, showing that only first-order deviations from the equilibrium are required to recover the intended macroscopic behaviour in the hydrodynamic limit [7]. An equivalence can be drawn between some regularized and MRT models, indicating that they share similarities [30–32]. Another family of collision kernels is referred to as *entropic models*. Their purpose is to restore a discrete counterpart of Boltzmann’s H -theorem so as to increase the robustness of the collision step [33–38]. They might either enforce the existence of a Lyapunov functional by locally solving a minimization problem, or by ensuring the relaxation towards a numerical equilibrium defined as the maximum of a pseudo-entropy. An important feature of these models is that they are not obtained performing an expansion of the continuous Maxwellian, but that they are built *ab initio* enforcing a set of *a priori* constraints. In the same spirit, an enhanced robustness can be noted by simply changing the equilibrium distribution function of the BGK model to a numerical one [39], or by increasing the number of equilibrium moments imposed by the standard polynomial equilibrium [15,40,16,32].

Most of the aforementioned collision models share a common feature: they have been built upon physical considerations inherited from the kinetic theory of gases (hydrodynamic variables, Chapman-Enskog expansion, H -theorem and positivity of distribution functions). However, the stability problem can be raised from a different angle, noticing that the LBM is nothing but a numerical scheme solving a counterpart of the Boltzmann equation on a velocity lattice, namely the discrete-velocity Boltzmann equation (DVBE) [41]. Based on a sufficiently large lattice, the DVBE is precisely designed to recover the Navier-Stokes equations as hydrodynamic limit [12], as illustrated in Fig. 1. Linear analyses of the DVBE indicate that its stability is ensured for a large range of Mach numbers in the limit of low Knudsen numbers [42]. Therefore, there is some evidence that the instabilities of the LBM are solely induced by the time and space discretization of the numerical algorithm. As such, they might be investigated using common tools of numerical analyses like von Neumann linearizations or Taylor expansions to obtain equivalent equations.

In light of this, the relationship between the LBM and an intended macroscopic behaviour (Euler or NS equations) involves two asymptotic parameters as illustrated in Fig. 1: the discretization variables (Δx , Δt) indicating the numerical resolution of the DVBE, and the Knudsen number Kn , drawing a link between microscopic and macroscopic descriptions. The distinction between numerical and hydrodynamic expansions is the cornerstone of so-called *asymptotic preserving* (AP) schemes, which are designed to preserve the asymptotic limits from the microscopic to the macroscopic models in the discrete settings [44]. This topic is surprisingly poorly addressed in the LBM community. Yet, even though Δt and Δx can be related through a (diffusive or acoustic) scaling, the coexistence of two independent smallness parameters (Δt and Kn) makes Taylor expansions challenging in LBM. For instance, performing a Taylor expansion in Δt only yields an open system of macroscopic equations, which does not allow providing a clear physical interpretation to the numerical errors [45,46]. To overcome this issue, several authors assume an explicit relation between the discretization parameters and the Knudsen number [47–51]. In other words, deviations from the equilibrium allegedly scale as the mesh size or the time step. A single asymptotic analysis is then sufficient to recover the Euler and NS equations as a *consistency* study, *i.e.* in the limit $\Delta x, \Delta t \rightarrow 0$, rather than as a hydrodynamic limit [48]. In other works, a similar off-equilibrium scaling is obtained under the hypothesis that the collision does not involve the time step [52–57]. However, Kn and Δt are rigorously independent from each other, even though the spatial discretization might yield a maximal reachable Knudsen number [42], which acts as a numerical switch between the microscopic and macroscopic representations in AP schemes [44]. Unfortunately, supposing a systematic link between the Knudsen number and the discretization parameters prevents the distinction between numerical errors and hydrodynamic consistency.

The aim of the present work is to propose an original Taylor expansion of the LBM based on the Knudsen number, without assuming any relationship between the deviations from the equilibrium and the discretization parameters. For given mesh size and time step, the proposed methodology offers the benefit to make explicitly appear both numerical errors and

inconsistency with the desired physics, with a single asymptotic expansion. Such an analysis is also the opportunity to answer two questions, which are paramount for any AP scheme: 1) What are the hydrodynamic limits of the LBM in the discrete settings? 2) Are these limits stable and consistent (*i.e.* convergent in the sense of Lax [43]) with regards to the Navier-Stokes equations? Every error terms will be systematically confronted with linear stability analyses in order to validate their expression, to interpret them, as well as to provide explanations for the numerical errors observed in a previous work [32]. In particular, the present study exhibits a phenomenon referred to as *hyperviscous degeneracy*, consisting in a resurgence of unintended high-order Knudsen effects induced by a large numerical pre-factor.

The present article is structured as follows. In Sec. 2, the general methodology adopted in this work is described. A generic variable change is proposed regardless the form of the scheme, so that it can be applied to any collision model. In Sec. 3, it is applied to the BGK collision model, providing a theoretical rationale for its low numerical dissipation. A general form of regularized collision models is investigated in Sec. 4. Two particular regularizations are then scrutinized: a complete shear stress reconstruction (Sec. 5) and the more standard *projected* (PR) and *recursive* (RR) regularizations (Sec. 6). Finally, the analysis is extended to several forms of MRT models in Sec. 7. Even though the latter were historically developed earlier than the regularization, they are presented here as a generalization of the PR and RR models, for which the proposed methodology can be more directly applied. All the forthcoming work is conducted under the isothermal approximation in the context of an acoustic scaling, so as to investigate the asymptotic behaviour of LBM with regards to the isothermal weakly compressible NS equations.

2. Methodology

2.1. Isothermal discrete velocity Boltzmann equation (DVBE)

The aim of any LB scheme is to numerically solve a DVBE. In the present context, considering the BGK collision model [17] and including a general body-force term Ψ_i , it reads

$$\partial_t f_i + \xi_{i,\alpha} \partial_\alpha f_i = -\frac{1}{\tau} (f_i - f_i^{eq}) + \Psi_i, \quad \forall i \in \llbracket 0, V-1 \rrbracket, \quad (1)$$

where $(f_i)_{i \in \llbracket 0, V-1 \rrbracket}$ is the set of distribution functions, considered as unknowns of the DVBE, V is the number of velocities of the lattice composed of discrete velocities $(\xi_i)_{i \in \llbracket 0, V-1 \rrbracket}$, τ is the relaxation time of the BGK collision model and $(f_i^{eq})_{i \in \llbracket 0, V-1 \rrbracket}$ is the set of equilibrium distribution functions, yet to define. In the following, only one- and two-dimensional cases will be considered. In one dimension, $\alpha = x$, while in two dimensions, an implicit summation is performed in Eq. (1) on the index $\alpha \in \{x, y\}$. In the present context, and without loss of generality on the methodology, the equilibrium distribution function will be expressed as a Hermite polynomial expansion, as proposed by Grad [58] and Shan et al. [12]:

$$f_i^{eq} = \sum_{n=0}^N \frac{w_i}{n! c^{2n}} \mathbf{a}_{eq}^{(n)} : \mathcal{H}_i^{(n)}, \quad (2)$$

where w_i are the Gaussian weights of the lattice, c is a reference velocity, $\mathcal{H}_i^{(n)}$ are Hermite polynomials (n th-order tensors) defined by the Rodrigues' formula,

$$\mathcal{H}_{i,\alpha_1 \dots \alpha_n}^{(n)} = \frac{(-c^2)^n}{w(\xi_i)} \frac{\partial^n w}{\partial \xi_{\alpha_1} \dots \partial \xi_{\alpha_n}}(\xi_i), \quad w(\xi) = \frac{1}{(2\pi c^2)^{D/2}} \exp\left(-\frac{\xi^2}{2c^2}\right), \quad (3)$$

the symbol ':' stands for the Frobenius inner product, D is the spatial dimension and $\mathbf{a}_{eq}^{(n)}$ are Hermite equilibrium coefficients. Furthermore, N stands for the maximal order of equilibrium coefficients that can be imposed by Eq. (2). In order to recover the isothermal form of the Navier-Stokes equations as hydrodynamic limit of the DVBE, *e.g.* thanks to a Chapman-Enskog expansion [7], the first five coefficients have to be defined as

$$\begin{aligned} a_{eq}^{(0)} &= \rho, & a_{eq,\alpha}^{(1)} &= \rho u_\alpha, & a_{eq,\alpha\beta}^{(2)} &= \rho u_\alpha u_\beta + \rho c^2 (\theta - 1) \delta_{\alpha\beta}, \\ a_{eq,\alpha\beta\gamma}^{(3)} &= \rho u_\alpha u_\beta u_\gamma + \rho c^2 (\theta - 1) (u_\alpha \delta_{\beta\gamma} + u_\beta \delta_{\alpha\gamma} + u_\gamma \delta_{\alpha\beta}), \\ a_{eq,\alpha\beta\gamma\epsilon}^{(4)} &= \rho u_\alpha u_\beta u_\gamma u_\epsilon + \rho c^2 (\theta - 1) (\delta_{\alpha\beta} u_\gamma u_\epsilon + \delta_{\alpha\gamma} u_\beta u_\epsilon + \delta_{\alpha\epsilon} u_\beta u_\gamma + \delta_{\beta\gamma} u_\alpha u_\epsilon + \delta_{\beta\epsilon} u_\alpha u_\gamma + \delta_{\gamma\epsilon} u_\alpha u_\beta) \\ &\quad + \rho c^4 (\theta - 1)^2 (\delta_{\alpha\beta} \delta_{\gamma\epsilon} + \delta_{\alpha\gamma} \delta_{\beta\epsilon} + \delta_{\alpha\epsilon} \delta_{\beta\gamma}), \end{aligned} \quad (4)$$

where δ is the Kronecker symbol, ρ and \mathbf{u} are respectively the macroscopic density and velocity defined as

$$\rho = \sum_i f_i, \quad \rho u_\alpha = \sum_i \xi_{i,\alpha} f_i, \quad (5)$$

and θ is a dimensionless constant defined so that $c\sqrt{\theta}$ is the actual isothermal (Newtonian) sound speed [59]. In a thermal framework, θ can be viewed as the ratio between the local temperature and a reference one.

In the present work, two standard lattices are considered: the one-dimensional D1Q3 lattice and the two-dimensional D2Q9 one. Their discrete velocities and Gaussian weights read [11]:

$$\text{D1Q3} : \xi_x = [0, 1, -1]c/c_s, \quad w_i = [2/3, 1/6, 1/6], \quad (6)$$

$$\text{D2Q9} : \xi_x = [0, 1, 1, 0, -1, -1, -1, 0, 1]c/c_s, \quad \xi_y = [0, 0, 1, 1, 1, 0, -1, -1, -1]c/c_s, \\ w_i = [2/3, 1/9, 1/36, 1/9, 1/36, 1/9, 1/36, 1/9, 1/36], \quad (7)$$

where $c_s = 1/\sqrt{3}$ is called the lattice constant. Note that with both of these lattices, the quadrature order is not sufficiently large to correctly impose third-order Hermite equilibrium coefficients. The polynomial expansion of Eq. (2) has to be truncated at $N = 2$, leading to a weakly compressible assumption, where the isothermal NS equations are affected by a non-Galilean-invariant error in Mach number [60,12]. With the D2Q9 lattice, partial third-order ($a_{xy}^{(3)}$ and $a_{xyy}^{(3)}$) and fourth-order ($a_{xyyy}^{(4)}$) expansions can be considered, without, however, increasing the validity range of the macroscopic equations [45]. The latter equilibria will be denoted $N = 3^*$ and $N = 4^*$ in the following.

The body-force term Ψ_i can precisely be included to address this issue. In a previous work by Prasianakis and Karlin, this error is addressed by modifying the first-order moment of the DVBE, yielding a correct momentum equation [61]. However, this affects the computation of the macroscopic velocity, leading to an implicit problem to solve. In the present context, it is decided to adopt the strategy of Feng et al., which only affects the second-order moment of the DVBE [62]. With the D1Q3 lattice and the D2Q9 one with $N = 3^*, 4^*$, this correction reads

$$\Psi_i = -\frac{w_i}{2c^4} \mathcal{H}_{i,\alpha\alpha} \partial_\alpha a_{eq,\alpha\alpha}^{(3)}. \quad (8)$$

With the D2Q9 lattice with $N = 2$, the correction term has to fix the complete absence of third-order moments in f_i^{eq} and reads

$$\Psi_i = -\frac{w_i}{2c^4} \mathcal{H}_{i,\alpha\beta} \partial_\gamma a_{eq,\alpha\beta\gamma}^{(3)}, \quad (9)$$

where implicit summations are performed on α, β and γ . In the following, models for which Ψ_i intends to fix incorrect third-order moments in f_i^{eq} will be referred to as *corrected* models.

2.2. Dimensionless DVBE

The first step of the present methodology is to obtain a dimensionless form of the DVBE (1) in order to make characteristic non-dimensional numbers appear. This is done by considering a characteristic length l_p , defined as the length scale of a perturbation of a quantity X as

$$l_p \sim \frac{|X|}{|\nabla X|}, \quad (10)$$

where ∇ stands for the gradient operator. In the context of the linear analyses of Sec. 2.7, it can simply be reduced to $l_p = 1/k$, where k is the wavenumber of a considered perturbation. For the sake of consistency with the linear analyses, the characteristic length will be referred to as $1/k$ in the following. Furthermore, considering c/c_s as a characteristic velocity, a characteristic time can be defined as $c_s/(kc)$. This leads to the following dimensionless variables:

$$t^* = \frac{kc t}{c_s}, \quad x^* = kx, \quad y^* = ky. \quad (11)$$

With this non-dimensionalization, the DVBE can be re-written as

$$\partial_{t^*} f_i + e_{i,\alpha} \partial_{\alpha^*} f_i = -\frac{c_s}{k\tau c} (f_i - f_i^{eq}) + \Psi_i^*, \quad (12)$$

where $e_i = \xi_i c_s/c$ and $\Psi_i^* = \Psi_i c_s/(kc)$. Note that with these definitions and given the values of ξ_i for the D1Q3 and D2Q9 lattices, the dimensionless discrete velocities e_i are integers, which make them consistent with the dimensionless quantities of a LB solver. Finally, the relaxation coefficient appearing in Eq. (12) can be directly related to the Knudsen number Kn . The latter is indeed defined as the ratio between the mean free path of particles and a characteristic length. Considering $1/k$ as characteristic length and defining the mean free path as $\tau c/c_s$ following [42], the Knudsen number can be defined in the present formalism as

$$\text{Kn} = \frac{k\tau c}{c_s}. \quad (13)$$

The dimensionless DVBE finally reads

$$\partial_{t^*} f_i + e_{i,\alpha} \partial_{\alpha^*} f_i = -\frac{1}{\text{Kn}} (f_i - f_i^{eq}) + \Psi_i^* = -\frac{1}{\text{Kn}} (f_i - f_i^{eq} - \text{Kn} \Psi_i^*), \quad (14)$$

where the second equality can be very useful to interpret any body-force term as a change of equilibrium distribution function, which was, for instance, recently done by Saadat et al. [63]. This dimensionless equation will be considered as the target any LB solver intends to solve.

2.3. Taylor expansion of the dimensionless LB scheme

In a very general way, a LB scheme can be decomposed into two steps acting on a set of discrete distribution functions $(g_i)_{i \in [0, V-1]}$ (which are different from the f_i of the DVBE): a streaming step and a collision step. Since the collision step depends on the adopted model, a LB scheme can be systematically identified as a streaming step as

$$g_i(\mathbf{x} + \xi_i \Delta t, t + \Delta t) = g_i^c(\mathbf{x}, t), \quad (15)$$

where Δt is the time-step and g_i^c are the post-collision distribution functions, which can always be written as explicit functions of $(g_i)_{i \in [0, V-1]}$. Note that in presence of a body force term Ψ_i , it can be included under a discrete form (eventually evaluating spatial gradients with finite differences) in the collision step which makes Eq. (15) general. Regarding the time step Δt , it is here related to the mesh size Δx through the following acousting scaling: $c = c_s \Delta x / \Delta t$. As a consequence, the characteristic velocity defined in the previous section can be written as $c/c_s = \Delta x / \Delta t$, which is consistent with the conventional LB non-dimensionalization [3].

Following the same characteristic length, time and velocity as adopted in Sec. 2.2, a dimensionless LB scheme reads

$$g_i \left(\mathbf{x}^* + \mathbf{e}_i \text{Kn} \frac{\Delta t}{\tau}, t^* + \text{Kn} \frac{\Delta t}{\tau} \right) = g_i^c(\mathbf{x}^*, t^*). \quad (16)$$

In agreement with Fig. 1, two dimensionless parameters appear:

1. the Knudsen number Kn , which is the only parameter driving the flow physics since it is the only one appearing in the DVBE,
2. the ratio $\Delta t / \tau$, which is a purely numerical quantity representing the effects of the space and time discretization.

In particular, taking the limit $\Delta t / \tau \rightarrow 0$ should yield the DVBE providing that the LB scheme is consistent with it. In order to obtain the equivalent partial differential equations of the LB scheme, it seems tempting to perform a Taylor expansion of it for low values of $\Delta t / \tau$, by analogy with numerical analyses of common discrete schemes. This is for example the strategy adopted in [45,46]. As discussed in Sec. 1, many Taylor expansions of the literature assume a relationship between $\Delta t / \tau$ and Kn . In the present work, no such assumption is performed and an original Taylor expansion in the physical parameter Kn rather than the numerical parameter $\Delta t / \tau$ is preferred. This is motivated by several observations:

- In many applications of the LBM for simulations of air flows, e.g. in the aeronautical field, the common order of magnitude of $\tau / \Delta t$ is $[10^{-7} - 10^{-3}]$ [3]. The numerical parameter $\Delta t / \tau$ is then much greater than one in these cases, which makes a Taylor expansion for $\Delta t / \tau \rightarrow 0$ not convenient for the quantification of numerical errors.
- A Taylor expansion in $\Delta t / \tau$ is not sufficient to interpret any numerical error of the LBM as a deviation from the macroscopic equations, e.g. the Navier-Stokes (NS) equations. It would only exhibit numerical errors with respect to the DVBE, which is not a closed set of equations involving macroscopic variables (ρ and u_α) only. In any case, a supplementary investigation of the hydrodynamic limit of the equations would be mandatory [64].
- Since the Knudsen number is directly related to the flow physics, a Taylor expansion in Kn can evidence the effect of numerical errors at each physical scale (Euler, Navier-Stokes, Burnett,...). Furthermore, it will be shown in Sec. 2.5 that a Taylor expansion in Kn is sufficient to derive a closed set of macroscopic equations in a given hydrodynamic limit.
- In addition to remaining small for physical reasons, the constraint $\text{Kn} \ll 1$ is generally ensured for numerical reasons with the LB scheme. This is a consequence of the Nyquist-Shannon theorem [65,66], stipulating that no spatial fluctuations can be discretized with less than two points per wavelength. In other words, the characteristic length $1/k$ is limited by the mesh size Δx , so that $k \leq \pi / \Delta x$ for linear perturbations. Together with the relationship relating Δx with the acoustic scaling [3] ($c = c_s \Delta x / \Delta t$), this leads to

$$\text{Kn} \leq \text{Kn}_s = \pi \frac{\tau}{\Delta t}, \quad (17)$$

which ensures that the Knudsen number remains small in common simulations of air flows. The dimensionless number Kn_s has been referred to as the Knudsen-Shannon number by Masset and Wissocq [42]. This property is central for the numerical switch of AP schemes between microscopic and macroscopic descriptions [44].

A Taylor expansion of Eq. (16) for $\text{Kn} \rightarrow 0$ yields

$$\sum_{n \geq 0} \frac{\text{Kn}^n}{n!} \left(\frac{\Delta t}{\tau} \right)^n D_i^n g_i = g_i^c, \quad (18)$$

where D_i is the operator defined as $D_i = \partial_{t^*} + e_{i,\alpha} \partial_{\alpha^*}$ and D_i^n stands for n successive applications of this operator. To draw a parallel with the DVBE, Eq. (18) can then be re-written as

$$D_i g_i = -\frac{\tau}{\Delta t} \frac{1}{\text{Kn}} (g_i - g_i^c) - \sum_{n \geq 2} \frac{\text{Kn}^{n-1}}{n!} \left(\frac{\Delta t}{\tau} \right)^{n-1} D_i^n g_i. \quad (19)$$

2.4. Generic variable change

Noticing now that the first right-hand-side term of Eq. (19) is very close to the collision term of the DVBE (14), the following generic variable change can be assumed:

$$g_i - g_i^c = \frac{\Delta t}{\tau} (f_i - f_i^{eq} - \text{Kn} \Psi_i^*). \quad (20)$$

This variable change strongly depends on the collision model and it will be shown in Sec. 3 that, in the case of the BGK collision, it reduces to the well-known relation obtained by He et al. [41] in their *a priori* derivation of the BGK-LB scheme. However, when different collision models are adopted, other variable changes actually occur, which will be shown for both regularized models in Sec. 4 and MRT models in Sec. 7. Whatever the collision model, one has to check that the variable change is admissible, meaning that it does not affect the computation of macroscopic variables:

$$\sum_i g_i = \sum_i f_i = \rho, \quad \sum_i e_{i,\alpha} g_i = \sum_i e_{i,\alpha} f_i = \rho u_\alpha^* = \rho u_\alpha \frac{\Delta t}{\Delta x}, \quad (21)$$

which ensures that the variable change is completely transparent on the macroscopic quantities of interest.

In the following, the Taylor expansion in Kn will be re-written on the new variable f_i for several collision models, leading to the generic equation:

$$D_i f_i = -\frac{1}{\text{Kn}} (f_i - f_i^{eq} - \text{Kn} \Psi_i^*) + \sum_{n \geq 1} \text{Kn}^n E_i^{(n)}, \quad (22)$$

where $E_i^{(n)}$ are the deviations from the DVBE at each order in Knudsen number, which can be explicitly expressed as functions of $\Delta t/\tau$ and spatial derivatives of the macroscopic quantities of interest. In presence of a body-force term, $E_i^{(n)}$ can also account for the numerical errors induced by their numerical discretization (e.g. central or upwind finite differences). In particular, it will be shown that in the linear approximation, $E_i^{(n)}$ involves $(n+1)$ th-order spatial derivatives only.

The $*$ exponent will be dropped in the rest of the article for the time t , position \mathbf{x} and velocity \mathbf{u} . Note that a direct translation can be done between dimensional and lattice units by replacing the reference velocity c by the lattice constant c_s , as well as $\xi_{i,\alpha}$ by $e_{i,\alpha}$, in Eqs. (2)-(9).

2.5. Macroscopic equations at leading Knudsen orders

Once the deviation terms from the DVBE $E_i^{(n)}$ are found at given Knudsen orders, the next step of the analysis is to evidence their impact on the macroscopic evolution equations. After computing the moments of Eq. (22) and following the procedure detailed in Appendix A, the following equations are obtained:

$$\partial_t \rho + \partial_\alpha (\rho u_\alpha) = \text{Kn} E_\rho^{(1)} + \text{Kn}^2 E_\rho^{(2)} + \text{Kn}^3 E_\rho^{(3)} + O(\text{Kn}^4), \quad (23)$$

$$\partial_t (\rho u_\alpha) + \partial_\beta (\rho u_\alpha u_\beta) + c_s^2 \theta \partial_\alpha \rho = \text{Kn} \left(\rho c_s^2 \theta \partial_\beta S_{\alpha\beta} \right) + \text{Kn} E_{\rho u_\alpha}^{(1)} + \text{Kn}^2 E_{\rho u_\alpha}^{(2)} + \text{Kn}^3 E_{\rho u_\alpha}^{(3)} + O(\text{Kn}^4), \quad (24)$$

with $S_{\alpha\beta} = \partial_\alpha u_\beta + \partial_\beta u_\alpha$. This closed set of equations is obtained as a hydrodynamic limit (in the sense $\text{Kn} \rightarrow 0$) without performing the time-derivative expansion in smallness parameter proposed by Chapman and Enskog [7]. Hence, the Taylor expansion in Knudsen number is sufficient to exhibit the hydrodynamic limits of Eq. (22). In a certain manner, the procedure adopted here is similar to the Taylor expansion method proposed by Dubois [53], but with different notations yielding more straight physical interpretations thanks to the explicit appearance of Kn .

Defining a dynamic viscosity $\mu = \text{Kn} \rho c_s^2 \theta$, Eqs. (23)-(24) can be identified as the isothermal form of the NS equations including a bulk viscosity, as previously shown by Dellar [67]. As expected by a Chapman-Enskog expansion, viscous effects explicitly appear at first-order in Knudsen number. These equations are affected by the deviation terms $E_\rho^{(n)}$ and $E_{\rho u_\alpha}^{(n)}$. Like the $E_i^{(n)}$ terms of Eq. (22), they can be explicitly expressed as derivatives of macroscopic quantities, and *a priori* depend on the numerical parameter $\Delta t/\tau$. Moreover, they can be systematically decomposed into two contributions:

- Looking at the behaviour of $E_\rho^{(n)}$ and $E_{\rho u_\alpha}^{(n)}$ when $\Delta t/\tau \rightarrow 0$ highlights the *consistency* of the LB scheme with a desired physics (at a given Knudsen order).
- Looking at $(\Delta t/\tau)$ -dependent terms evidences the numerical errors induced by the time and space discretization of the LB scheme.

For instance, regarding the first-order deviation $E_{\rho u_\alpha}^{(1)}$, a consistency error is expected for non-corrected models with the D1Q3 and D2Q9 lattices, which is the well known Mach error in the shear stress tensor. Moreover, no first-order numerical error is expected for second-order accurate schemes, like the BGK one [53]. Since these terms appear at the same level (first-order in Kn) as the viscous effects, they can be directly interpreted as an additional viscosity arising in the macroscopic equations. A second-order accuracy is then mandatory if one wants to recover the Navier-Stokes behaviour in the asymptotic limit. Any first-order error would result in an incorrect viscosity, depending on the numerical model under consideration. In the linear approximation, it will be shown that these terms only involve second-order gradients. Throughout the rest of the article, the zeroth- and first-order contributions in Kn will be referred to as the *Navier-Stokes level*.

Regarding higher (second and third) orders in Kn, it can be shown that:

- second-order deviations $E_\rho^{(2)} - E_{\rho u_\alpha}^{(2)}$, involving third-order gradients only in the linear approximation, correspond to the leading *dispersion* errors,
- third-order deviations $E_\rho^{(3)} - E_{\rho u_\alpha}^{(3)}$, involving fourth-order gradients only in the linear approximation, can be interpreted as a *numerical hyperviscosity* in the macroscopic equations, yielding a *dissipation* error.

In the following, the deviations terms $E_\rho^{(n)}$ and $E_{\rho u_\alpha}^{(n)}$ will be computed for several models up to the third-order assuming a linear approximation, which is sufficient to exhibit their effective viscosity and hyperviscosity. For this purpose and given the complexity of the problems under consideration, the computer algebra system Maxima [68] is used following the methodology proposed in Appendix A.

2.6. Hyperviscous degeneracy

In the forthcoming investigations of several collision models, it will be shown that the $E_i^{(1)}$ term has no macroscopic contribution in most of the LB schemes of interest, meaning that they do not include any numerical viscosity. In order to explain their stability and dissipation properties, it is therefore required to focus on the $E_i^{(3)}$ term, related to hyperviscous effects, which is the purpose of the present section.

A particular quantity of interest is the order of magnitude of the ratio between the numerical hyperviscosity and the expected viscous effects, expressed as:

$$\Gamma = \frac{\text{Kn}^3 E_i^{(3)}}{\text{Kn}} = \text{Kn}^2 E_i^{(3)}. \quad (25)$$

In order to obtain a more explicit expression of this quantity, note that the definition of the Knudsen number yields

$$\text{Kn} = k\Delta x \frac{\tau}{\Delta t}. \quad (26)$$

$k\Delta x$ is directly related to the number of points used to discretize the characteristic length $l_p = 1/k$. Especially, for a plane monochromatic wave, the number of points per wavelength is $N_{ppw} = 2\pi/(k\Delta x)$. Furthermore, it will be shown that, in every analysis performed in the present article, the third-order deviation in Kn largely depends on the numerical parameter $\Delta t/\tau$, so that

$$E_i^{(3)} \sim \left(\frac{\Delta t}{\tau}\right)^n \quad \text{when} \quad \frac{\tau}{\Delta t} \ll 1, \quad (27)$$

where n , the maximal power of $(\Delta t/\tau)$ present in $E_i^{(3)}$, depends on the collision model under investigation. Hence, Eq. (25) becomes

$$\Gamma \sim (k\Delta x)^2 \left(\frac{\Delta t}{\tau}\right)^{n-2}. \quad (28)$$

For a given finite value of $k\Delta x$, *i.e.* for a given discretized phenomenon, three cases can now be distinguished:

1. $n < 2$: hyperviscous effects induced by $E_i^{(3)}$ are negligible compared to the expected viscous effects when the dimensionless relaxation time is low ($\tau/\Delta t \ll 1$),
2. $n = 2$: the ratio Γ between hyperviscous and viscous effects is not affected by the dimensionless relaxation time $\tau/\Delta t$,
3. $n > 2$: hyperviscous effects induced by $E_i^{(3)}$ become very large compared to the expected viscous effects when $\tau/\Delta t \ll 1$.

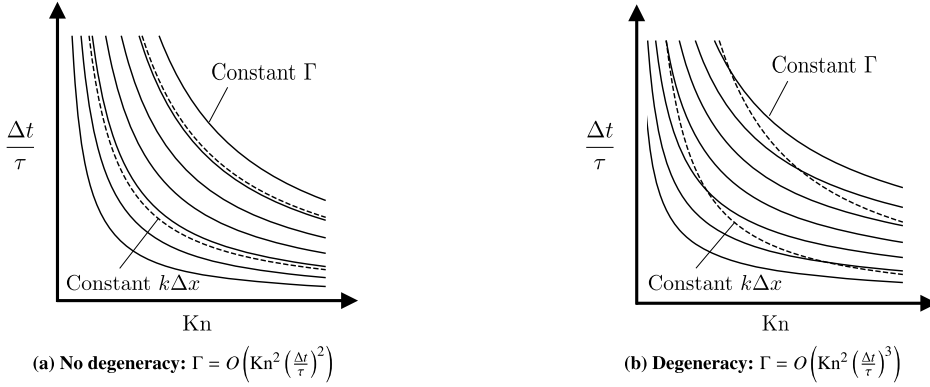


Fig. 2. Schematic plot of the link between numerical ($\Delta t/\tau$ -related) and asymptotic (Kn -related) errors for a discretized spatial phenomena described by a constant value of $k\Delta x = \text{Kn} \Delta t/\tau$.

The third case is referred to as a *hyperviscous degeneracy* in the rest of the article. It consists in a resurgence, unexpected from a physical point of view, of high-order Knudsen effects caused by a large numerical pre-factor ($E_i^{(3)}$ in this case). This phenomenon is illustrated in Fig. 2, where typical iso-contours of errors are represented in solid lines. For a given discretized spatial phenomena (represented by constant values of $k\Delta x$ in dashed lines), the error is independent of $\Delta t/\tau$ in the non-degenerated case, but only depends on the resolution $k\Delta x$. On the contrary, it increases as $\Delta t/\tau$ increases in the degenerated one.

In Sec. 3, it will be shown that the BGK model does not suffer from such a discrepancy. However, regularized models are subject to this phenomenon as shown in Sec. 4. In Sec. 7, it will be shown that any MRT model with constant relaxation times can *a priori* be subject to a degeneracy.

2.7. Numerical validation: linear analyses

Once the errors terms of a given LB collision model have been found, they can be systematically validated by performing a linear analysis of the mass and momentum equations (23)-(24) and comparing it with an analysis of the LB scheme of Eq. (15). As a reminder, linear (von Neumann) analyses are a powerful tool to exhibit the numerical properties of a linearized scheme [69,70], which has been largely used to analyse the properties of the LBM [71,72,13,73–76,16,77,78,32].

Applied to a system like Eqs. (23)-(24), the purpose of the von Neumann analysis is to seek linear solutions as

$$\Phi(\mathbf{x}, t) = \bar{\Phi} + \Phi'(\mathbf{x}, t), \quad \Phi' \ll \bar{\Phi}, \quad (29)$$

$$= \bar{\Phi} + \hat{\Phi} \exp\left(\frac{i}{k\Delta x}(\mathbf{k} \cdot \mathbf{x}\Delta x - \omega t \Delta t)\right), \quad (30)$$

for $\Phi \in \{\rho, \rho u_\alpha\}$, where $\bar{\Phi}$ are mean base quantities, constant in space and time and Φ' are small fluctuations with regards to $\bar{\Phi}$. In the von Neumann formalism, they are sought as plane monochromatic waves, involving the (complex) amplitudes $\hat{\Phi}$, the complex unity i defined such that $i^2 = -1$, the real wavenumber vector $\mathbf{k} = (k_x, k_y)$ and the complex pulsation ω . Note that in Eq. (30), time and space variables \mathbf{x} and t are dimensionless using the non-dimensionalization of Sec. 2.2, which explains the presence of the factor $1/(k\Delta x)$ in the equation. Moreover, k , related to the characteristic length of Sec. 2.2, is defined here as the norm of the wavenumber vector. Using the Nyquist-Shannon sampling theorem [65,66], the wavenumber vector is restricted to $k_x, k_y \leq \pi/\Delta x$. For this reason, the set of dimensionless parameters ($k_x\Delta x, k_y\Delta x, \tau/\Delta t$) will be adopted in the linear analyses, instead of the Knudsen number which is a combination of them.

A linearization of Eqs. (23)-(24) followed by the injection of plane monochromatic waves yield an eigenvalue problem

$$\omega^* \mathbf{U} = \mathbf{M}^{(p)} \mathbf{U} + O(k^{*p+2}). \quad (31)$$

where $\omega^* = \omega\Delta t$, $\mathbf{U} = [\rho', (\rho u_\alpha)']^T$, \mathbf{M} is a matrix of size $(D+1)$ and p is the order of truncation of the deviation terms. The explicit expression of this matrix, depending on \mathbf{k} , Δx , τ , Δt and the deviation terms, is provided in Appendix C. The complex pulsation ω can then be found as an eigenvalue of the matrix \mathbf{M} .

The eigenvalues of the linear system (31) will be systematically compared to that of the linearized LB scheme, which reads in the general form

$$e^{-i\omega_{\text{LBM}}^*} \mathbf{F} = \mathbf{M}^{\text{LBM}} \mathbf{F}, \quad (32)$$

where the matrix \mathbf{M}^{LBM} depends on the adopted collision model. The corresponding matrices are recalled in Appendix C for the collision models under consideration in the present work.

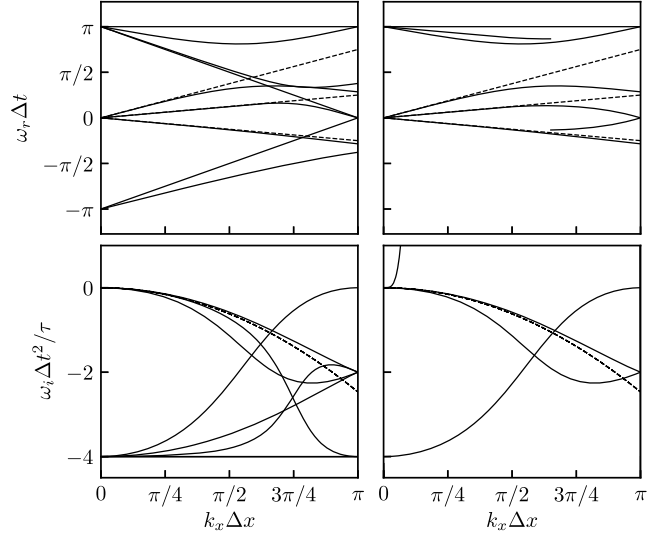


Fig. 3. Propagation (top) and dissipation (bottom) curves of the linear analyses performed on the isothermal NS equations (---) and the LB scheme with the non-corrected D2Q9 lattice and $N^* = 4$ (—). A horizontal mean flow is considered with $\bar{u}_x = 0.5c_s\sqrt{\theta}$, $\theta = 0.75$ and $\tau/\Delta t = 10^{-5}$. Left: BGK, right: PR collision models.

Such analyses are illustrated in Fig. 3, where the eigenvalues of both systems (31)–(32) are displayed for $k_x\Delta x \in [0, \pi]$, $k_y = 0$. In the case of Eq. (31), no deviation term is considered here, meaning that the isothermal NS equations are actually studied. Regarding Eq. (32), two models are displayed for the non corrected D2Q9 lattice with $N = 4^*$: the BGK and the projected regularization (PR). In-depth discussion of such analyses can be found for instance in [32]. Here, one can focus on two observations:

1. While the three eigenvalues of the isothermal NS equations tend towards zero when $k_x\Delta x \rightarrow 0$ (i.e. in the well-resolved limit), this is not the case of all the eigenvalues of the LBM. With the BGK (resp. PR) model, 6 modes (resp. 3 modes) tend towards π in this limit. The corresponding modes will be referred to as *non-hydrodynamic* (NH) modes.
2. The analysis of the PR model evidences an instability ($\omega_i/\tau > 0$) of a hydrodynamic mode, even in the low-wavenumber limit. Further analyses allow identifying this unstable mode as a shear wave [32]. This instability is not present with the BGK collision model, for which the dissipation of the hydrodynamic modes is close to that of the NS equations.

Note that because of modal interactions occurring in the LB scheme, the identification of NH modes as continuous functions $\omega^* = f(k^*)$ is not straightforward [16]. However, since the present work focuses on Taylor expansions for $\text{Kn} \rightarrow 0$, it is sufficient to adopt here the above definition of NH modes. The particular case of these modes is discussed in the next section. The fact that the BGK model induces a very low numerical dissipation will be theoretically explained in Sec. 3, and the instability of the PR model will be explained by a hyperviscous degeneracy in Sec. 6.

2.8. Particular case of non-hydrodynamic modes

The validity of the methodology proposed in the present work is actually ensured provided that distribution functions g_i are sufficiently continuous so that a Taylor expansion in Kn can be rigorously performed. One necessary condition is then

$$g_i\left(\mathbf{x} + \mathbf{e}_i \text{Kn} \frac{\Delta t}{\tau}, t + \text{Kn} \frac{\Delta t}{\tau}\right) = g_i^c(\mathbf{x}, t) \rightarrow g_i(\mathbf{x}, t) \quad \text{when} \quad \text{Kn} \rightarrow 0. \quad (33)$$

It is shown in the present section that this condition is not necessarily ensured, which further explains the behaviour of non-hydrodynamic modes evidenced in Fig. 3. For this purpose, let us consider the non-corrected BGK collision model [17], for which

$$g_i^c = g_i - \frac{\Delta t}{\tau + \Delta t/2} (g_i - f_i^{eq}). \quad (34)$$

With this model, the continuity condition (33) for a given ratio $\Delta t/\tau > 0$ is equivalent to

$$g_i(\mathbf{x}, t) \rightarrow f_i^{eq}(\mathbf{x}, t) \quad \text{when} \quad \text{Kn} \rightarrow 0. \quad (35)$$

Let us now consider a given set of non-zero distribution functions g_i verifying

$$\sum_i g_i = 0, \quad \sum_i e_{i,\alpha} g_i = 0. \quad (36)$$

Even if such a distribution function has no physical meaning, it can be used to model a non-hydrodynamic perturbation that does not project on density and velocity. By virtue of the rank-nullity theorem, the possible set of distribution functions verifying this condition is of dimension 6 with the D2Q9 lattice and of dimension 1 with the D1Q3 lattice. Given that zeroth- and first-order moments are both null with this choice, one has $f_i^{eq}(g_j) = 0$ so that the BGK-LB scheme reads

$$g_i \left(\mathbf{x} + \mathbf{e}_i \text{Kn} \frac{\Delta t}{\tau}, t + \text{Kn} \frac{\Delta t}{\tau} \right) = \frac{\tau - \Delta t/2}{\tau + \Delta t/2} g_i(\mathbf{x}, t), \quad (37)$$

which does not tend towards $g_i(\mathbf{x}, t)$ when $\text{Kn} \rightarrow 0$. As a consequence, the Taylor expansion in Knudsen number cannot be performed on distributions functions verifying Eq. (36). Looking now more carefully at Eq. (37), the linear modes \hat{g}_i ensuring this equation are those for which $\tau \neq \Delta t/2$ and

$$e^{-i\omega_{\text{LBM}}^*} = \frac{\tau - \Delta t/2}{\tau + \Delta t/2}, \quad (38)$$

when Kn tends towards zero. This leads to two cases:

$$\begin{aligned} \tau/\Delta t < 1/2 : \quad & \text{Re}(\omega_{\text{LBM}}^*) = \pi, \quad \text{Im}(\omega_{\text{LBM}}^*) = -\ln\left(\frac{\Delta t/2 - \tau}{\tau + \Delta t/2}\right), \\ \tau/\Delta t > 1/2 : \quad & \text{Re}(\omega_{\text{LBM}}^*) = 0, \quad \text{Im}(\omega_{\text{LBM}}^*) = -\ln\left(\frac{\tau - \Delta t/2}{\tau + \Delta t/2}\right). \end{aligned}$$

The first case corresponds to *over-relaxed* modes [3,79], whose amplitude is reversed at each iteration due to a real dimensionless pulsation close to π . They exactly match the non-hydrodynamic modes evidenced in the linear analyses of Sec. 2.7. This spurious numerical behaviour can be observed in practice, and may be very harmful for low-Reynolds and under-resolved simulations [80]. One of the aim of more sophisticated collision models is precisely to damp, or even filter out, these modes. The second case corresponds to *under-relaxed* modes [3].

As a consequence, non-hydrodynamic modes are *discontinuous* modes. The Taylor expansion method in Knudsen number, as proposed in this work, cannot be used to predict their numerical behaviour. The discontinuity of the deviation terms involved in these modes could even be simply guessed by looking at the linear analyses of Fig. 3: due to the phase-shift of π encountered by these modes, the deviation terms are necessarily discontinuous in Kn . Note that this discontinuity is not in disagreement with a consistency of the LB scheme with the DVBE, which requires an investigation of the limit $\tau/\Delta t \rightarrow 0$ as shown in Fig. 1.

Hence, the rest of the article will focus on hydrodynamic modes only, more precisely on the ability of the present methodology to predict and quantify their dispersion and dissipation properties. It is therefore sufficient to investigate the deviation terms of the macroscopic equations (23)-(24), for which only hydrodynamic modes are considered, contrary to the DVBE (22). Every analysis will have to be validated *a posteriori*, which will be performed thanks to the linear analyses introduced in Sec. 2.7.

2.9. Summary of the methodology

The methodology described in this section can be applied to any LB collision model. It is summarized as follows:

1. Non-dimensionalization of the LB scheme, so that two dimensionless numbers appear: the Knudsen number Kn and the numerical parameter $\Delta t/\tau$.
2. Taylor expansion in Kn , involving $\Delta t/\tau$ -dependent pre-factors.
3. A variable change $f_i = \psi(g_i)$ is then performed to mimic the DVBE, in particular its collision term. The admissibility of this variable change ($\sum_i f_i = \sum_i g_i$ and $\sum_i e_{i,\alpha} f_i = \sum_i e_{i,\alpha} g_i$) has to be checked. Deviation terms from the DVBE can then be exhibited, as shown in Eq. (22).
4. A closed set of macroscopic equations can then be obtained at a desired Knudsen order, in the linear approximation, following Appendix A. They can be identified as the isothermal form of NS equation with deviation terms. The latter include: (1) consistency errors with the NS equations, (2) $\Delta t/\tau$ -dependent numerical errors.
5. Validation of the macroscopic deviation terms using the linear analyses introduced in Sec. 2.7.

In all the analyses, a potential hyperviscous degeneracy will be scrutinized by looking at the numerical pre-factors of third-order deviations, as discussed in Sec. 2.6.

3. Application to the BGK collision model

This section aims at applying the Taylor expansion in Kn to the common BGK collision model, so as to quantify and validate the impacts of numerical errors on the intended physics. Given the poor practical interest of the BGK model, the

main goal of this section is rather pedagogical, since it provides a simple application of the above methodology. Moreover, the resulting deviation terms will be used as a reference when comparing other schemes.

Both D1Q3 and D2Q9 lattices will be considered in this section including different Hermite-based equilibria, with and without correction terms. In the former case, the effect of their discretization using finite differences, with upwind and central schemes, will be investigated.

3.1. General Taylor expansion of the BGK model

The general form of post-collision distribution functions involved in the BGK collision model reads:

$$g_i^c = g_i - \frac{\Delta t}{\tau + \Delta t/2} \left(g_i - f_i^{eq} - \text{Kn} \Psi_i^d \right), \quad (39)$$

where Ψ_i^d is a general discretized form of the body-force term. It can be either zero in the case of non-corrected LBM, or equal to the Ψ_i terms of Eqs. (8)-(9) with possible deviations induced by the finite-difference estimation of gradients. The latter will be further detailed for each case under consideration.

After performing the Taylor expansion of Sec. 2.3, the variable change suggested by Eq. (20) reads

$$\frac{\Delta t}{\tau + \Delta t/2} \left(g_i - f_i^{eq} - \text{Kn} \Psi_i^d \right) = \frac{\Delta t}{\tau} \left(f_i - f_i^{eq} - \text{Kn} \Psi_i^d \right), \quad (40)$$

which leads to

$$g_i = f_i + \frac{\Delta t}{2\tau} \left(f_i - f_i^{eq} - \text{Kn} \Psi_i^d \right). \quad (41)$$

This change of variable is in line with what can be found in the literature, especially in an *a priori* construction of the BGK-LB scheme [41]. Moreover, since the correction term of Feng et al. [62] involves a second-order Hermite moment only (if not null), its zeroth- and first-order moments vanish, which leads to

$$\sum_i g_i = \sum_i f_i = \rho, \quad \sum_i e_{i,\alpha} g_i = \sum_i e_{i,\alpha} f_i = \rho u_\alpha, \quad (42)$$

so that the variable change is admissible. The following equivalent partial differential equation is then obtained on f_i :

$$D_i f_i = -\frac{1}{\text{Kn}} f_i^{(1)} - \sum_{n \geq 2} \frac{\text{Kn}^{n-1}}{n!} \left(\frac{\Delta t}{\tau} \right)^{n-1} D_i^n f_i - \sum_{n \geq 1} \frac{\text{Kn}^{n-1}}{2n!} \left(\frac{\Delta t}{\tau} \right)^n D_i^n f_i^{(1)}, \quad (43)$$

where $f_i^{(1)}$ is defined as

$$f_i^{(1)} = f_i - f_i^{eq} - \text{Kn} \Psi_i^d. \quad (44)$$

In order to obtain a more convenient form of the deviation terms, one then needs to express the derivatives of $f_i^{(1)}$ appearing in Eq. (43) as function of f_i only. For this purpose, Eq. (43) can be written as:

$$f_i^{(1)} = -\sum_{n \geq 1} \frac{\text{Kn}^n}{n!} \left(\frac{\Delta t}{\tau} \right)^{n-1} D_i^n f_i - \sum_{n \geq 1} \frac{\text{Kn}^n}{2n!} \left(\frac{\Delta t}{\tau} \right)^n D_i^n f_i^{(1)}. \quad (45)$$

Let us now seek a series expansion of $f_i^{(1)}$ under the following form:

$$f_i^{(1)} = \sum_{n \geq 1} \frac{c_n}{n!} \text{Kn}^n \left(\frac{\Delta t}{\tau} \right)^{n-1} D_i^n f_i. \quad (46)$$

Injecting this expression in Eq. (45) yields

$$\begin{aligned} \sum_{n \geq 1} \frac{c_n}{n!} \text{Kn}^n \left(\frac{\Delta t}{\tau} \right)^{n-1} D_i^n f_i &= -\sum_{n \geq 1} \frac{\text{Kn}^n}{n!} \left(\frac{\Delta t}{\tau} \right)^{n-1} D_i^n f_i - \frac{1}{2} \sum_{n \geq 1} \sum_{m \geq 1} \frac{c_m}{n! m!} \text{Kn}^{n+m} \left(\frac{\Delta t}{\tau} \right)^{n+m-1} D_i^{n+m} f_i \\ &= -\sum_{n \geq 1} \frac{\text{Kn}^n}{n!} \left(\frac{\Delta t}{\tau} \right)^{n-1} D_i^n f_i - \frac{1}{2} \sum_{n \geq 2} \text{Kn}^n \left(\frac{\Delta t}{\tau} \right)^{n-1} \left(\sum_{k=1}^{n-1} \frac{c_k}{k!(n-k)!} \right) D_i^n f_i. \end{aligned}$$

This leads to the following recursive relation on the coefficients c_n :

Table 1

Expression of the ten firsts Bernoulli numbers B_n^- , Genocchi numbers G_n and the c_n coefficients involved in the series expansion of $f_i^{(1)}$.

n	0	1	2	3	4	5	6	7	8	9	10
B_n^-	-	-1/2	1/6	0	-1/30	0	1/42	0	-1/30	0	5/66
G_n	-	1	-1	0	1	0	-3	0	17	0	-155
c_n	2	-1	0	1/2	0	-1	0	17/4	0	-31	0

$$c_1 = -1, \quad \forall n \geq 2, \quad c_n = -1 - \frac{1}{2} \sum_{k=1}^{n-1} \binom{n}{k} c_k, \quad (47)$$

which can also be written as

$$c_0 = 2, \quad \forall n \geq 1, \quad c_n = - \sum_{k=0}^n \binom{n}{k} c_k. \quad (48)$$

In Appendix D, it is shown that these coefficients are related to both the Genocchi numbers G_n and the Bernoulli numbers B_n^- as

$$\forall n \geq 0, \quad c_n = 2 \frac{G_{n+1}}{n+1} = 4(1 - 2^{n+1}) \frac{B_{n+1}^-}{n+1}. \quad (49)$$

This relation is helpful since the Bernoulli numbers are well documented in the literature. The interested reader may refer to [81–84] for more informations on Genocchi and Bernoulli numbers. Some relations between Taylor expansions of the LB scheme and the Bernoulli polynomials have already been noticed in the literature [49], but no demonstration could be provided to the authors' knowledge. The first ten coefficients of this expansion are detailed in Table 1. An important feature is that every odd Bernoulli number is null, so that only odd coefficients remain in Eq. (46).

Finally, injecting these expressions into Eq. (46) and after some manipulations, a general form of the Taylor expansion is obtained for the BGK collision model

$$D_i f_i = -\frac{1}{\text{Kn}} (f_i - f_i^{eq}) + \Psi_i^d + \frac{\text{Kn}^2}{12} \left(\frac{\Delta t}{\tau} \right)^2 D_i^3 f_i - \frac{\text{Kn}^4}{5!} \left(\frac{\Delta t}{\tau} \right)^4 D_i^5 f_i + \sum_{p \geq 3} \frac{c_{2p+1}}{(2p+1)!} \text{Kn}^{2p} \left(\frac{\Delta t}{\tau} \right)^{2p} D_i^{2p+1} f_i. \quad (50)$$

This equation differs from the dimensionless DVBE of Eq. (14) by the discretization errors in Ψ_i^d and the deviation terms in $O(\text{Kn}^2)$. Note that no first-order term in Kn appear, which is a direct consequence of the second-order accuracy of the BGK-LB scheme [41,53,8]. Following the macroscopic interpretation of Sec. 2.5, it means that the BGK-LBM induces no numerical viscosity at the NS level.

In order to obtain an explicit expression of the deviation terms $E_i^{(n)}$ involved in Eq. (50), further development of the temporal and spatial derivatives included in $D_i^n f_i$ is required. This will be the purpose of Sec. 3.3 in the linear approximation. But before that, one can focus at the expression as it in order to explain the low-dissipation properties of the BGK collision model.

3.2. Low dissipation of the BGK collision model

An important feature of the BGK collision model directly appears in Eq. (50): when written under this form, only even orders in Knudsen number appear in the expansion. This is a direct consequence of the relation found between the c_n coefficients and the Bernoulli numbers. Let us recall here that even and odd Knudsen orders are directly related to dispersion and dissipation errors, respectively. Hence, no dissipation error appears in the above relation. As a matter of fact, a dissipation error is implicitly present in the $D_i^{2p} f_i$ terms of the even order errors. A first insight into these dissipative terms is provided in this section in absence of body-force term ($\Psi_i^d = 0$). For instance, let us focus on the second-order term of Eq. (50). Using the fact that $f_i = f_i^{eq} - \text{Kn} D_i f_i^{eq} + O(\text{Kn}^2)$, one has

$$\frac{\text{Kn}^2}{12} \left(\frac{\Delta t}{\tau} \right)^2 D_i^3 f_i = \frac{\text{Kn}^2}{12} \left(\frac{\Delta t}{\tau} \right)^2 D_i^3 f_i^{eq} - \frac{\text{Kn}^3}{12} \left(\frac{\Delta t}{\tau} \right)^2 D_i^4 f_i^{eq} + O(\text{Kn}^4), \quad (51)$$

so that a third-order error, related to the numerical hyperviscosity, actually arises. The latter involves the parameter $\Delta t/\tau$ at a power $n = 2$. Following Sec. 2.6, it means that the numerical hyperviscosity remains bounded and is not affected by the value of the dimensionless relaxation time. Hence, no hyperviscous degeneracy occurs. Given the parity of the deviation terms, this fundamental property of the BGK collision model may be extended to any error term of odd order, so that the numerical dissipation does not depend on the value of the dimensionless relaxation time. It is at the origin of the very low-dissipation properties of the model, despite its second-order accuracy, especially in comparison with other solvers [73].

3.3. Error terms in the linear approximation

Starting from Eq. (50), the purpose of the present section is to obtain an explicit expression of the deviation terms appearing in Eq. (22) involving spatial derivatives of macroscopic quantities only. This is a prerequisite for obtaining the explicit deviations from the macroscopic equations, as proposed in Appendix A. The focus is put here on the first-, second- and third-order terms, and linearity is assumed so as to simplify the expressions.

First, the discretized body-force term Ψ_i^d of Eq. (50) has to be considered. A general Taylor expansion in Kn is proposed for this term in Appendix B in the case of second-order central (referred to as DCO2) and first-order upwind (referred to as DU01) finite differences. Note that, while no first-order error is explicitly present in Eq. (50), such a term appears in the Taylor expansion of the body-force term with an upwind discretization.

Then, a second-order estimation of the $D_i^3 f_i$ terms appearing in Eq. (50) is required. It starts by writing

$$D_i^3 f_i = D_i^3 f_i^{eq} - \text{Kn} D_i^4 f_i^{eq} + \text{Kn} D_i^3 \Psi_i + O(\text{Kn}^2), \quad (52)$$

where the fact that $\Psi_i^d = \Psi_i + O(\text{Kn})$ has been used. The D_i terms can then be related to time and space derivatives as

$$D_i^3 = \partial_{ttt}^3 + 3e_{i,\alpha} \partial_{tt\alpha}^3 + 3e_{i,\alpha} e_{i,\beta} \partial_{t\alpha\beta}^3 + e_{i,\alpha} e_{i,\beta} e_{i,\gamma} \partial_{\alpha\beta\gamma}^3, \quad (53)$$

$$D_i^4 = \partial_{tttt}^4 + 4e_{i,\alpha} \partial_{ttt\alpha}^4 + 6e_{i,\alpha} e_{i,\beta} \partial_{tt\alpha\beta}^4 + 4e_{i,\alpha} e_{i,\beta} e_{i,\gamma} \partial_{t\alpha\beta\gamma}^4 + e_{i,\alpha} e_{i,\beta} e_{i,\gamma} e_{i,\delta} \partial_{\alpha\beta\gamma\delta}^4. \quad (54)$$

These terms can be related to derivatives of macroscopic quantities only since, for any function $\Phi(\rho, \mathbf{u})$, the following chain rule can be applied:

$$\partial_{\alpha_1 \dots \alpha_n}^n \Phi = \frac{\partial \Phi}{\partial \rho} \partial_{\alpha_1 \dots \alpha_n}^n \rho + \frac{\partial \Phi}{\partial (\rho u_\beta)} \partial_{\alpha_1 \dots \alpha_n}^n (\rho u_\beta), \quad (55)$$

for any combination of indices $\alpha_i \in \{t, x, y\}$. This chain rule can be applied to both f_i^{eq} and Ψ_i , which are explicit functions of ρ and \mathbf{u} . Note that the linear assumption is applied at this step since $\partial\Phi/\partial\rho$ and $\partial\Phi/\partial(\rho u_\beta)$ are assumed constant as the pre-factors of time/space derivatives. One can then dispose of time-derivatives of macroscopic quantities using the conservation equations at the desired Knudsen order, obtained by computing the zeroth- and first-order moments of Eq. (50):

$$\partial_t \rho = -\partial_\gamma (\rho u_\gamma) + O(\text{Kn}^2), \quad \partial_t (\rho u_\alpha) = -\partial_\beta \Pi_{\alpha\beta} + O(\text{Kn}^2), \quad (56)$$

where the fact that $\sum_i \Psi_i^d = \sum_i e_{i,\alpha} \Psi_i^d = 0$ has been used, and where

$$\Pi_{\alpha\beta} = \Pi_{\alpha\beta}^{eq} - \text{Kn} \left(\partial_t \Pi_{\alpha\beta}^{eq} + \partial_\gamma Q_{\alpha\beta\gamma}^{eq} \right) + \text{Kn} \sum_i e_{i,\alpha} e_{i,\beta} \Psi_i + O(\text{Kn}^2). \quad (57)$$

Time and space derivatives of Π^{eq} and Q^{eq} can finally be disposed thanks to the chain rule of Eq. (55). All these relations form a closed set of equations allowing an expression of $D_i^3 f_i$ involving spatial derivatives of macroscopic quantity only, at first-order in Kn. For this purpose, and given the complexity of the problems, the simplification of these equations is performed using the computer algebra system Maxima [68].

Finally, the explicit expressions of the $E_i^{(n)}$ terms being known, the macroscopic equations (23)-(24) are obtained following the general procedure detailed in Appendix A. Next sections provide the resulting deviation terms $E_\Phi^{(n)}$ obtained by these computations.

3.4. D1Q3 lattice

With the D1Q3 lattice, the following macroscopic equations are recovered:

$$\partial_t \rho + \partial_x (\rho u_x) = \text{Kn} E_\rho^{(1)} + \text{Kn}^2 E_\rho^{(2)} + \text{Kn}^3 E_\rho^{(3)} + O(\text{Kn}^4), \quad (58)$$

$$\partial_t (\rho u_x) + \partial_x (\rho u_x^2) + c_s^2 \theta \partial_x \rho = \text{Kn} \left(2\rho c_s^2 \theta \partial_{xx}^2 u_x \right) + \text{Kn} E_{\rho u_x}^{(1)} + \text{Kn}^2 E_{\rho u_x}^{(2)} + \text{Kn}^3 E_{\rho u_x}^{(3)} + O(\text{Kn}^4), \quad (59)$$

where the macroscopic deviation terms $E_\rho^{(n)}$ and $E_{\rho u_x}^{(n)}$ are provided below, involving consistency errors C_i and numerical errors N_i , whose explicit expressions are detailed in Appendix H.

3.4.1. Absence of correction

The mass and momentum equations (58)-(59) are obtained with

$$E_\rho^{(1)} = 0, \quad E_{\rho u_x}^{(1)} = -\frac{\partial^2 a_{eq,xxx}^{(3)}}{\partial x^2},$$

$$\begin{aligned}
E_\rho^{(2)} &= \left(\frac{\Delta t}{\tau}\right)^2 \frac{1}{12} \left(-\frac{\partial^3 a_{eq,xxx}^{(3)}}{\partial x^3} + 2\rho c_s^2 \theta \frac{\partial^3 u_x}{\partial x^3} \right), & E_{\rho u_x}^{(2)} &= C_1 + \left(\frac{\Delta t}{\tau}\right)^2 N_1, \\
E_\rho^{(3)} &= \left(\frac{\Delta t}{\tau}\right)^2 \frac{1}{12} \partial_x C_1, & E_{\rho u_x}^{(3)} &= C_2 + \left(\frac{\Delta t}{\tau}\right)^2 N_2.
\end{aligned} \tag{60}$$

The only first-order deviation from the isothermal NS equations is a modelling error related to $a_{eq,xxx}^{(3)}$ in the equation of momentum, which is the well-known Galilean invariance error induced by the lattice closure [60,12]. Similar consistency errors denoted with C_i , *i.e.* the remaining deviation terms when $\Delta t/\tau \rightarrow 0$, appear at second- and third-orders in Kn, but they may be neglected at the NS level. The only numerical errors arising at Kn^2 (dispersion error) and Kn^3 (numerical hyperviscosity) are proportional to $(\Delta t/\tau)^2$, which is in agreement with the second-order accuracy of the BGK-LBM. As mentioned in Sec. 3.2, no hyperviscous degeneracy occurs in this case. One can finally note that the numerical errors affecting the mass equation at a given order n (in Knudsen number) are directly related to the consistency error of the momentum equation at order $n-1$. It therefore seems that the numerical errors in the mass conservation originate from consistency errors multiplied by a numerical factor.

3.4.2. Analytically computed correction

Including now a correction term Ψ_i without considering its discretization errors, Eqs. (58)-(59) are recovered with

$$\begin{aligned}
E_\rho^{(1)} &= 0, & E_{\rho u_x}^{(1)} &= 0, \\
E_\rho^{(2)} &= \left(\frac{\Delta t}{\tau}\right)^2 \frac{1}{12} \left(-\frac{\partial^3 a_{eq,xxx}^{(3)}}{\partial x^3} + 2\rho c_s^2 \theta \frac{\partial^3 u_x}{\partial x^3} \right), & E_{\rho u_x}^{(2)} &= C_3 + \left(\frac{\Delta t}{\tau}\right)^2 N_1, \\
E_\rho^{(3)} &= \left(\frac{\Delta t}{\tau}\right)^2 \frac{1}{12} \partial_x C_3, & E_{\rho u_x}^{(3)} &= C_4 + \left(\frac{\Delta t}{\tau}\right)^2 N_3.
\end{aligned} \tag{61}$$

A direct consequence of the correction is that there is no more first-order deviation from the isothermal NS equations. First- and second-order terms only differ from the non-corrected case by the consistency terms, while the numerical errors remain the same. On the contrary, the third-order numerical error (numerical hyperviscosity) is affected by the correction. Furthermore, even though the first-order consistency error is corrected by the introduction of Ψ_i , the second-order numerical error appearing in the mass conservation equation is surprisingly still related to the deviation term $a_{eq,xxx}^{(3)}$ induced by the lattice closure. Except this observation, the numerical error $E_{\rho u_x}^{(3)}$ can still be related to the consistency error of $E_{\rho u_x}^{(2)}$.

3.4.3. Correction with a second-order central (DCO2) scheme

Including now a correction with a DCO2 discretization, Eqs. (58)-(59) are recovered with the exactly same deviation terms as with the analytically computed correction, except for the third-order term in the momentum equation:

$$E_{\rho u_x}^{(3)} = C_4 + \left(\frac{\Delta t}{\tau}\right)^2 \left(N_3 + \frac{1}{6} \frac{\partial^4 a_{eq,xxx}^{(3)}}{\partial x^4} \right). \tag{62}$$

Naturally, the discretization of Ψ_i only impacts the numerical error and does not affect the consistency of the scheme.

3.4.4. Correction with a first-order upwind (DUO1) scheme

When the correction term is discretized with a DUO1 scheme, the same deviation terms as with the analytically computed correction are obtained, except for

$$\begin{aligned}
E_{\rho u_x}^{(2)} &= C_3 + \left(\frac{\Delta t}{\tau}\right)^2 N_1 - \left(\frac{\Delta t}{2\tau}\right) \text{sgn}(u_x) \frac{\partial^3 a_{eq,xxx}^{(3)}}{\partial x^3}, \\
E_{\rho u_x}^{(3)} &= C_4 + \left(\frac{\Delta t}{\tau}\right)^2 \left(N_3 + \frac{1}{6} \frac{\partial^4 a_{eq,xxx}^{(3)}}{\partial x^4} \right) + \left(\frac{\Delta t}{2\tau}\right) \text{sgn}(u_x) N_4.
\end{aligned} \tag{63}$$

It only differs from the DCO2 case by numerical error terms in $\Delta t/\tau$, which is a direct consequence of the first-order accuracy of the upwind gradients. Note that, despite this first-order accuracy in Δt , the mass and momentum equations are recovered without error at the NS level, *i.e.* without error in $O(\text{Kn})$. This is a consequence of the fact that zeroth- and first-order moments of Ψ_i^d are null. Then, the discretization error only affects the macroscopic equations through the moments cascade, so that its contribution is at the order $O(\text{Kn}^2)$. As a consequence, no numerical viscosity originates from the choice of discretization of the correction term.

3.5. D2Q9 lattice

With the D2Q9 lattice, the macroscopic equations (23)-(24) are obtained with the deviation terms $E_\phi^{(n)}$ detailed in Appendix E. For the sake of simplicity, only the x-derivatives are provided in the deviation terms $E_{\rho u_x}^{(2)}$, $E_{\rho u_y}^{(2)}$, $E_\rho^{(3)}$, $E_{\rho u_x}^{(3)}$ and $E_{\rho u_y}^{(3)}$. The expressions of the other terms ($E_\rho^{(1)}$, $E_{\rho u_x}^{(1)}$, $E_{\rho u_y}^{(1)}$ and $E_\rho^{(2)}$) are much simpler, they are provided in their complete form.

From the expressions of deviation terms, the main observations are:

- the second-order numerical error in the mass equation ($E_\rho^{(2)}$) is always related to the cubic defect $a_{eq,\alpha\beta\gamma}^{(3)}$,
- this error can be reduced by a higher-order equilibrium (if possible), but not by including the correction Ψ_i ,
- the DCO2 and DUO1 discretizations of Ψ_i only affect the numerical errors of the momentum equation at $O(\text{Kn}^2)$: they do not add any numerical viscosity,
- the $N = 3^*$ - and $N = 4^*$ -equilibria yield similar deviation terms when x-derivatives only are considered.

3.6. Validation with linear analyses

The deviation terms provided in the previous section can now be validated by linear analyses. This is done here by comparing the eigenvalue problem of the macroscopic equations including deviation terms, given by Eq. (31), with that of the BGK-LB scheme, given by Eq. (32). If the truncated system of Eq. (31) correctly takes into consideration the deviation terms of the macroscopic equations up to the order p , then one necessarily has

$$\omega^* = \omega_{\text{LBM}}^* + O(k^{*p+2}), \quad (64)$$

for any eigenvalue associated to a physical wave: acoustics or shear. In the following, the latter are identified as the ones whose real part is the closest to that of the expected physical waves:

$$\text{Re}(\omega_{\text{shear}}^*) = k_\alpha^* \bar{u}_\alpha, \quad \text{Re}(\omega_{\text{ac}+}^*) = k_\alpha^* \bar{u}_\alpha + k^* c_s \sqrt{\theta}, \quad \text{Re}(\omega_{\text{ac}-}^*) = k_\alpha^* \bar{u}_\alpha - k^* c_s \sqrt{\theta}, \quad (65)$$

\bar{u} being the mean flow velocity of the linear analysis. For each of these waves, the validity of the deviation terms up to an order p is finally assessed by checking that

$$\frac{\Delta\omega^*}{k^*} \equiv \frac{|\omega^* - \omega_{\text{LBM}}^*|}{k^*} = O(k^{*p+1}) = O\left(\frac{1}{N_{ppw}^{p+1}}\right), \quad (66)$$

where $N_{ppw} = 2\pi/k^*$ is the number of points per wavelength of the considered monochromatic plane wave.

Real and imaginary parts of $\Delta\omega^*/k^*$ are displayed in Fig. 4 in log-scale for the two physical (acoustic) waves of the non-corrected D1Q3 lattice, as function of N_{ppw} . Four cases are considered: without considering any deviation term ($p = 0$), and with deviation terms truncated up to the order $p = 1$, $p = 2$ and $p = 3$, as provided by Eq. (60). The mean flow velocity is arbitrarily prescribed to $\bar{u} = 0.5c_s\sqrt{\theta}$ (corresponding to a Mach number $\overline{\text{Ma}} = 0.5$), the constant θ is set as $\theta = 0.8$ to avoid the particular case $\theta = 1$ and the dimensionless relaxation time is set to a commonly encountered value in aeronautic simulations: $\tau/\Delta t = 10^{-5}$. In any case, the adopted parameters do not impact the following conclusions:

- As expected by Eq. (66), an asymptotic behaviour of the remaining error terms is exhibited by the slope of the logarithmic curve for each physical eigenvalue.
- Real parts of the eigenvalues, highlighting dispersion errors, are associated to even error orders, while imaginary parts, highlighting dissipation errors, are associated to odd error orders. This is a consequence to the fact that linear dispersion (resp. dissipation) is related to odd (resp. even) spatial derivatives.
- When considering the deviations from the isothermal NS equations up to an order p , the predominant error is well recovered as $O(1/k^{*p+1})$, as predicted by Eq. (66).
- For $p = 0$ (without including deviation terms), the -1 slope exhibits the first-order deviation in Knudsen number, *i.e.* in viscosity, caused by the lattice closure defect $a_{eq,xxx}^{(3)}$.
- With the BGK collision model, the dissipation error is always smaller than the dispersion one, in agreement with the conclusions of previous work [73].

More importantly, the -4 slope recovered in the case $p = 3$ allows validating all the deviation terms obtained in the linear approximation up to the third-order in Kn, provided in Eq. (60).

Similarly, remaining errors $\Delta\omega^*/k^*$ are displayed for the analytically corrected D1Q3 model in Fig. 5 for $p = 0$ and $p = 3$. Two observations can be made from these curves. First, without including any deviation term in the isothermal NS equations ($p = 0$), a -2 slope is obtained for the remaining error, exhibiting an accuracy in $O(k^{*2})$, or equivalently $O(\text{Kn}^2)$. This indicates that the lattice defect $a_{eq,xxx}^{(3)}$ is well corrected thanks to the body-force term Ψ_i , so that no consistency error

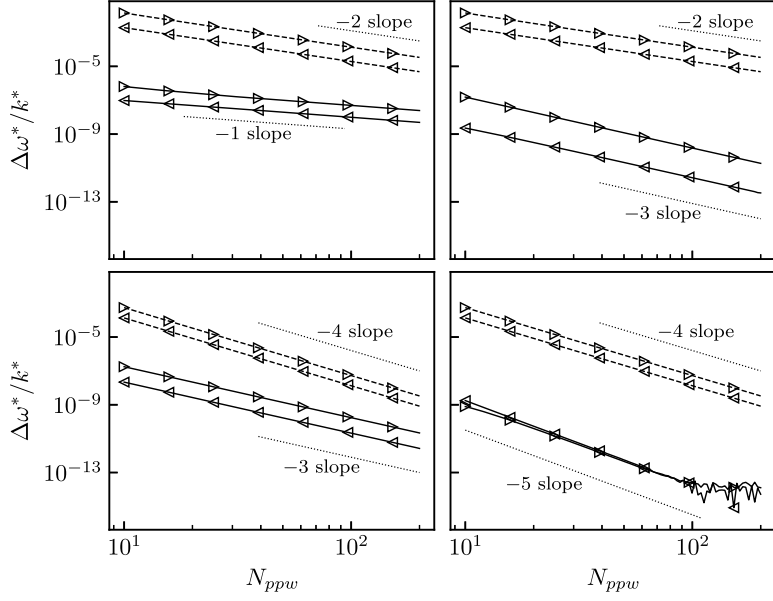


Fig. 4. Relative error between the eigenvalues of the BGK-LBM and that of the isothermal NS equations including deviation terms up to an order p provided in Eq. (60), for the non corrected D1Q3 lattice with $\bar{u} = 0.5c_s\sqrt{\theta}$, $\theta = 0.8$ and $\tau/\Delta t = 10^{-5}$. Top-left: $p = 0$ (no deviation term is considered), top-right: $p = 1$, bottom-left: $p = 2$, bottom-right: $p = 3$. $- \blacktriangleright -$: propagation error of the downstream acoustic eigenvalue, $- \blacktriangleleft -$: propagation error of the upstream acoustic eigenvalue, \blacktriangleright : dissipation error of the downstream acoustic eigenvalue, \blacktriangleleft : dissipation error of the upstream acoustic eigenvalue.

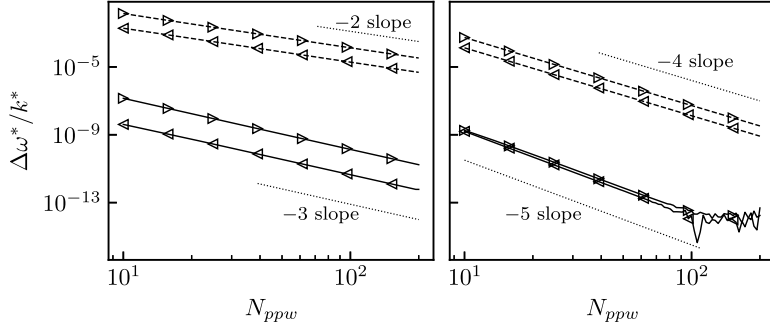


Fig. 5. Relative error between the eigenvalues of the BGK-LBM and that of the isothermal NS equations including deviation terms up to an order p provided in Eq. (61), for the analytically corrected D1Q3 lattice with $\bar{u} = 0.5c_s\sqrt{\theta}$, $\theta = 0.8$ and $\tau/\Delta t = 10^{-5}$. Left: $p = 0$ (no deviation term is considered), right: $p = 3$. $- \blacktriangleright -$: propagation error of the downstream acoustic eigenvalue, $- \blacktriangleleft -$: propagation error of the upstream acoustic eigenvalue, \blacktriangleright : dissipation error of the downstream acoustic eigenvalue, \blacktriangleleft : dissipation error of the upstream acoustic eigenvalue.

in viscosity occurs at the NS level. Secondly, the -4 slope exhibited in the case $p = 3$ allows validating all the deviation terms provided in the linear approximation in Eq. (61).

A similar work performed on all the deviation terms provided for the BGK-D1Q3 LB scheme in Sec. 3.4, as well as for the D2Q9 lattice in Appendix E further including a shear eigenvalue, allows validating them in the linear approximation. For the sake of compactness, these results are not provided here, the logarithmic curves of $\Delta\omega^*/k^*$ being very close to that of Figs. 4-5.

3.7. Summary of the numerical properties of the BGK collision model

In this section, the Taylor expansion in Knudsen number has been successfully applied to the BGK collision model for the D1Q3 and D2Q9 lattices, with and without body-force correction term. Even though the aim of such a work is mainly pedagogical, given the poor practical interest of the BGK collision model, one of its interesting features has been exhibited. Thanks to a close relationship linking the numerical errors of this model with the Bernoulli numbers, whose even terms are null, the numerical hyperviscosity remains bounded and does not degenerate when the dimensionless relaxation time $\tau/\Delta t$ is decreased. This property turns out to be fundamental to explain the very low dissipation of the BGK collision compared to other models.

Looking at the explicit expression of deviation terms with regards to the isothermal NS equations also underlines other interesting properties of the BGK collision model. The consistency errors exhibited in the present work are not problematic (except for the Mach error in the shear stress tensor): they are a simple consequence to the fact that a LB scheme does not intend to solve the NS equations, but a discrete counterpart of the Boltzmann equation. However, numerical errors exhibited in the mass equation are closely related to some consistency errors of the momentum equations. This observation might explain how enforcing the consistency of the LBM with the NS equations can improve the numerical behaviour of the scheme, as observed in a previous work [46].

Hence, with the BGK collision model, the numerical error in the mass equation involves the lattice closure defect $a_{eq,\alpha\beta\gamma}^{(3)}$. Interestingly, when the equilibrium distribution function is improved by recovering more equilibrium moments, as proposed with the D2Q9 lattice with $N = 3^*$ and $N = 4^*$ in Appendix E, the numerical error in the mass equation can be reduced, as a consequence of the improved consistency of the momentum equation. On the contrary, when the defect $a_{eq,\alpha\beta\gamma}^{(3)}$ is explicitly corrected thanks to a body-force term Ψ_i , the mass equation remains related to it even though the consistency of the momentum equation is recovered up to the first-order in Kn.

The main limitations of the BGK collision model remain its strong instability issues. The latter are caused by mode couplings arising in the linear approximation between hydrodynamic and non-hydrodynamic waves [16], whose behaviour cannot be investigated by the present Taylor expansion (*cf.* Sec. 2.8). For this reason, more sophisticated collision models are usually preferred in the aim of filtering out non-hydrodynamic modes. Among them, some regularized and MRT models are investigated in the next sections.

4. Regularized LBM: general case

4.1. Taylor expansion

In the general case and including a correction term Ψ_i , the regularization step affects the post-collision distribution functions as [25,26,28,29,85]:

$$g_i^c = f_i^{eq} + \left(1 - \frac{\Delta t}{\tau + \Delta t/2}\right) g_i^{(1)} + \frac{\Delta t}{2\tau} \text{Kn} \Psi_i^d, \quad (67)$$

where the non-dimensionalization of Sec. 2.2 has been applied, and $g_i^{(1)}$ is a recomputed (regularized) off-equilibrium part, whose explicit expression depends on the model under consideration. Note that the BGK collision model can also be written under this form with $g_i^{(1)} = g_i - f_i^{eq} + \text{Kn} \Delta t / (2\tau) \Psi_i^d = (\tau + \Delta t/2) / \tau (f_i - f_i^{eq})$. After performing the Taylor expansion of Sec. 2.3, the variable change suggested by Eq. (20) reads

$$g_i = h_i + \left(\frac{\Delta t}{\tau} - 1\right) f_i^{(1)}, \quad (68)$$

with

$$h_i = f_i + \frac{\tau - \Delta t/2}{\tau + \Delta t/2} g_i^{(1)} + \left(\frac{\Delta t}{2\tau} - 1\right) \text{Kn} \Psi_i^d, \quad f_i^{(1)} = f_i - f_i^{eq} - \text{Kn} \Psi_i^d. \quad (69)$$

A necessary and sufficient condition for the admissibility of this variable change is: $\sum_i g_i^{(1)} = \sum_i e_{i,\alpha} g_i^{(1)} = 0$, which is the case of all the regularization steps under consideration in this work. The following equivalent partial differential equation is then obtained:

$$\sum_{n \geq 1} \frac{\text{Kn}^{n-1}}{n!} \left(\frac{\Delta t}{\tau}\right)^{n-1} D_i^n h_i + \left(\frac{\Delta t}{\tau} - 1\right) \sum_{n \geq 1} \frac{\text{Kn}^{n-1}}{n!} \left(\frac{\Delta t}{\tau}\right)^{n-1} D_i^n f_i^{(1)} = -\frac{1}{\text{Kn}} f_i^{(1)}. \quad (70)$$

The latter can be re-written as

$$f_i^{(1)} = -\sum_{n \geq 1} \frac{\text{Kn}^n}{n!} \left(\frac{\Delta t}{\tau}\right)^{n-1} D_i^n h_i + \left(\frac{\tau}{\Delta t} - 1\right) \sum_{n \geq 1} \frac{\text{Kn}^n}{n!} \left(\frac{\Delta t}{\tau}\right)^n D_i^n f_i^{(1)}. \quad (71)$$

By analogy with the BGK model of Sec. 3, let us seek a series expansion of $f_i^{(1)}$ under the following form:

$$f_i^{(1)} = \sum_{n \geq 1} \frac{d_n}{n!} \text{Kn}^n \left(\frac{\Delta t}{\tau}\right)^{n-1} D_i^n h_i. \quad (72)$$

Injecting this expression in Eq. (71) yields

$$\sum_{n \geq 1} \frac{d_n}{n!} \text{Kn}^n \left(\frac{\Delta t}{\tau} \right)^{n-1} D_i^n h_i = - \sum_{n \geq 1} \frac{\text{Kn}^n}{n!} \left(\frac{\Delta t}{\tau} \right)^{n-1} D_i^n h_i + \left(\frac{\tau}{\Delta t} - 1 \right) \sum_{n \geq 1} \sum_{m \geq 1} \frac{d_m}{n! m!} \text{Kn}^{n+m} \left(\frac{\Delta t}{\tau} \right)^{n+m-1} D_i^{n+m} h_i \quad (73)$$

$$= - \sum_{n \geq 1} \frac{\text{Kn}^n}{n!} \left(\frac{\Delta t}{\tau} \right)^{n-1} D_i^n h_i + \left(\frac{\tau}{\Delta t} - 1 \right) \sum_{n \geq 2} \frac{\text{Kn}^n}{n!} \left(\frac{\Delta t}{\tau} \right)^{n-1} \left(\sum_{k=1}^{n-1} \binom{n}{k} d_k \right) D_i^n h_i, \quad (74)$$

where a Cauchy product is used to obtain the second equation. This leads to the following recurrence relation on the coefficients d_n :

$$d_1 = -1, \quad \forall n \geq 2, d_n = -1 + \left(\frac{\tau}{\Delta t} - 1 \right) \sum_{k=1}^{n-1} \binom{n}{k} d_k. \quad (75)$$

Contrary to the recurrence relation obtained in the BGK-case, the numerical parameter $\tau/\Delta t$ arises here, precluding the possibility to find an explicit relation between the d_i and a set of well-documented numbers such as the Bernoulli ones. Anyway, the first d_n coefficients can be easily computed using Eq. (75), leading to

$$d_2 = 1 - 2 \frac{\tau}{\Delta t}, \quad d_3 = -1 + 6 \frac{\tau}{\Delta t} - 6 \left(\frac{\tau}{\Delta t} \right)^2, \quad d_4 = 1 - 14 \frac{\tau}{\Delta t} + 36 \left(\frac{\tau}{\Delta t} \right)^2 - 24 \left(\frac{\tau}{\Delta t} \right)^3. \quad (76)$$

Similar coefficients were found by Holdych et al. [52] in their analysis of the BGK scheme, and were related to the polylogarithm function. Dong et al. [49] also noticed a similarity with the firsts Bernoulli polynomials.

Finally, one should note that with every regularization step considered in the present article, the distribution functions are reconstructed such that $g_i^{(1)} = O(\text{Kn})$. This allows defining a zeroth-order terms as

$$\hat{g}_i^{(1)} = \frac{1}{\text{Kn}} \left(\frac{\tau}{\tau + \Delta t/2} \right) g_i^{(1)}, \quad (77)$$

where the ratio $\tau/(\tau + \Delta t/2)$ simply appears for convenience. Together with this definition, injecting the d_n coefficients into Eq. (72) and collecting every terms in Kn up to the third-order yields

$$\begin{aligned} D_i f_i = & -\frac{1}{\text{Kn}} f_i^{(1)} + \text{Kn} \left(\frac{\Delta t}{2\tau} - 1 \right) \left[D_i^2 f_i + D_i \left(\hat{g}_i^{(1)} - \Psi_i^d \right) \right] \\ & + \text{Kn}^2 \left[\left(-1 + \frac{\Delta t}{\tau} - \frac{1}{6} \left(\frac{\Delta t}{\tau} \right)^2 \right) D_i^3 f_i - \left(1 - \frac{\Delta t}{2\tau} \right)^2 D_i^2 \left(\hat{g}_i^{(1)} - \Psi_i^d \right) \right] \\ & + \text{Kn}^3 \left[\left(-1 + \frac{3\Delta t}{2\tau} - \frac{7}{12} \left(\frac{\Delta t}{\tau} \right)^2 + \frac{1}{24} \left(\frac{\Delta t}{\tau} \right)^3 \right) D_i^4 f_i \right. \\ & \left. + \left(-1 + \frac{\Delta t}{\tau} - \frac{1}{6} \left(\frac{\Delta t}{\tau} \right)^2 \right) \left(1 - \frac{\Delta t}{2\tau} \right) D_i^3 \left(\hat{g}_i^{(1)} - \Psi_i^d \right) \right] + O(\text{Kn}^4). \end{aligned} \quad (78)$$

This equation will be the starting point for the forthcoming analyses of regularized models, especially to explicitly obtain the deviation terms $E_\Phi^{(n)}$. Before going further, one can notice that whatever the way regularized distribution functions are computed, the Euler equations are recovered provided that the zeroth- and first-order moments of $g_i^{(1)}$ are null. In particular, even with $g_i^{(1)} = 0$, the Euler equations can be recovered in the hydrodynamic limit. However, a first-order error in Kn can possibly lead to an unintended numerical viscosity, which will be particularly investigated.

4.2. Degenerating hyperviscosity with regularized models

Looking at Eq. (78) also allows a first estimation of the numerical hyperviscosity induced by the regularization, especially its ratio with the expected physical viscosity $\Gamma = \text{Kn}^2 E_i^{(3)}$. Neglecting the discretization errors of Ψ_i and keeping only the higher order in $\Delta t/\tau$ yields

$$\Gamma \sim \frac{\text{Kn}^2}{24} \left(\frac{\Delta t}{\tau} \right)^3 D_i^3 \left[D_i f_i + 2 \left(\hat{g}_i^{(1)} - \Psi_i \right) \right] = \frac{(k\Delta x)^2}{24} \frac{\Delta t}{\tau} D_i^3 \left[D_i f_i + 2 \left(\hat{g}_i^{(1)} - \Psi_i \right) \right]. \quad (79)$$

In the second equality, this ratio depends on $\Delta t/\tau$, as a consequence of the $(\Delta t/\tau)^3$ terms arising in Eq. (78). Hence, it is shown that for a given discretized spatial phenomenon characterized by a given value of $k\Delta x$, the unexpected effects of the numerical hyperviscosity can become predominant over the physical viscosity when $\tau/\Delta t$ is small. Since one usually has

$\tau/\Delta t < 10^{-3}$, the numerical hyperviscosity is then likely to degenerate. Looking at Eq. (79), this actually occurs for physical phenomena for which

$$k\Delta x > \sqrt{\frac{\tau}{\Delta t}}, \quad (80)$$

which might remain very small in practice compared to 1. This means that even well-resolved phenomena can be largely affected by the numerical hyperviscosity. Since the latter is *a priori* not controlled and strongly depends on the model under investigation, it can either lead to (1) over-dissipation or (2) instability. This explains the unexpected dissipation properties of regularized models exhibited in a previous work [32].

Note that with the BGK collision model, one has $\hat{g}_i^{(1)} = (f_i - f_i^{eq})/\text{Kn}$, so that

$$D_i f_i + 2\left(\hat{g}_i^{(1)} - \Psi_i^d\right) = D_i f_i + \frac{2}{\text{Kn}} f_i^{(1)} = -D_i f_i + O(\text{Kn}). \quad (81)$$

Injecting this expression into Eq. (78) allows, after some manipulation of the equations, recovering the Taylor expansion of the BGK collision model of Eq. (50), where no hyperviscous degeneracy occurs.

In order to exhibit the specific hyperviscous effects of the regularization, it is then necessary to focus on each model, which is the purpose of the following sections.

5. Regularization with a shear stress tensor reconstruction

In this section, the regularized model under consideration is referred to as a “shear stress tensor reconstruction”, where $g_i^{(1)}$ is computed using the knowledge of macroscopic quantities ρ and u_α only. It corresponds to the HRR collision model of Jacob et al. [29] in the particular case $\sigma = 0$. The main interest of this model is that it is the only regularization procedure that can be applied with the D1Q3 lattice. It is therefore first studied here to obtain reasonable expressions of deviation terms in 1D. This model is based on the relationship obtained by a Chapman-Enskog expansion [7], relating the off-equilibrium populations with the shear stress tensor. With the non-dimensionalization of Sec. 2.2 it reads

$$g_i^{(1)} = \text{Kn} \left(1 + \frac{\Delta t}{2\tau}\right) \hat{g}_i^{(1)} \quad \text{with} \quad \hat{g}_i^{(1)} = -\frac{w_i}{c_s^2} \left(e_{i,\alpha} e_{i,\beta} - c_s^2 \delta_{\alpha\beta}\right) \rho \theta \left(\partial_\alpha u_\beta + \partial_\beta u_\alpha\right). \quad (82)$$

Like the correction term Ψ_i , this off-equilibrium reconstruction involves space gradients which are, in practice, discretized by finite differences. The effects of a DCO2 and a DUO1 schemes will be investigated by comparison with the analytical gradients of Eq. (82) in the following.

5.1. First-order error term with the D1Q3 lattice

Let us focus on the first-order error term in Kn of Eq. (78), which is expected to be a source of numerical viscosity in the model. It can be re-written as

$$E_i^{(1)} = \left(\frac{\Delta t}{2\tau} - 1\right) D_i \left(D_i f_i + \hat{g}_i^{(1)} - \Psi_i\right). \quad (83)$$

The computation of this error term requires the computation of $D_i f_i$, which reads

$$\begin{aligned} D_i f_i &= D_i f_i^{eq} + O(\text{Kn}) = \partial_t f_i^{eq} + e_{i,x} \partial_x f_i^{eq} + O(\text{Kn}) \\ &= \frac{\partial f_i^{eq}}{\partial \rho} \partial_t \rho + \frac{\partial f_i^{eq}}{\partial(\rho u_x)} \partial_t(\rho u_x) + e_{i,x} \left(\frac{\partial f_i^{eq}}{\partial \rho} \partial_x \rho + \frac{\partial f_i^{eq}}{\partial(\rho u_x)} \partial_x(\rho u_x) \right) + O(\text{Kn}) \\ &= -\frac{\partial f_i^{eq}}{\partial \rho} \partial_x(\rho u_x) - \frac{\partial f_i^{eq}}{\partial(\rho u_x)} \partial_x \Pi_{xx}^{eq} + e_{i,x} \left(\frac{\partial f_i^{eq}}{\partial \rho} \partial_x \rho + \frac{\partial f_i^{eq}}{\partial(\rho u_x)} \partial_x(\rho u_x) \right) + O(\text{Kn}), \end{aligned} \quad (84)$$

where the fact that mass and momentum equations are recovered at first-order in Kn has been used. With the D1Q3 lattice, the equilibrium distribution can be written as

$$f_i^{eq} = w_i \left[\rho + \frac{\rho u_x e_{i,x}}{c_s^2} + \frac{(\rho u_x)^2 e_{i,x}^2}{2\rho c_s^4} - \frac{(\rho u_x)^2}{2\rho c_s^2} + \rho(\theta - 1) \frac{e_{i,x}^2 - c_s^2}{2c_s^2} \right], \quad (85)$$

so that

$$\frac{\partial f_i^{eq}}{\partial \rho} = w_i \left[1 - \frac{u_x e_{i,x}}{2c_s^4} + \frac{u_x^2}{2c_s^2} + (\theta - 1) \frac{e_{i,x}^2 - c_s^2}{2c_s^2} \right], \quad \frac{\partial f_i^{eq}}{\partial(\rho u_x)} = w_i \left[\frac{e_{i,x}}{c_s^2} + \frac{u_x e_{i,x}^2}{c_s^4} - \frac{u_x}{c_s^2} \right]. \quad (86)$$

Furthermore,

$$\partial_x \Pi_{xx}^{eq} = \partial_x (\rho u_x^2 + \rho c_s^2 \theta) = (u_x^2 + c_s^2 \theta) \partial_x \rho + 2\rho u_x \partial_x u_x. \quad (87)$$

Injecting these expressions in Eq. (84) yields after simplification

$$D_i f_i = \frac{w_i}{2c_s^2} (e_{i,x}^2 - c_s^2) \left[\left(-\frac{u_x^3}{c_s^2} + 3u_x(1-\theta) \right) \partial_x \rho + \left(-\frac{3\rho u_x^2}{c_s^2} + \rho(3-\theta) \right) \partial_x u_x \right] + O(\text{Kn}), \quad (88)$$

so that

$$D_i f_i + \hat{g}_i^{(1)} = -\frac{w_i}{2c_s^4} (e_{i,x}^2 - c_s^2) \partial_x (\rho u_x^3 + 3\rho c_s^2 (\theta - 1) u_x) + O(\text{Kn}). \quad (89)$$

Surprisingly, the right-hand-side term of this equation is exactly equal to the body-force term Ψ_i of Eq. (8). As a consequence, using the fact that $\Psi_i^d = \Psi_i + O(\text{Kn})$, one has in presence of correction

$$D_i f_i + \hat{g}_i^{(1)} - \Psi_i^d = O(\text{Kn}). \quad (90)$$

The first-order error in Kn of Eq. (78) then completely vanishes in presence of correction. Without any correction, a first-order error is expected, leading to undesired numerical viscosity, which can be cured thanks to the body-force term Ψ_i . It is therefore surprising that, while the correction term is designed to address a consistency error, it can be used to reduce a numerical error in the present case. This point can be interpreted as follows: the first-order error can be cancelled provided that the consistency of the viscous stress implicitly modelled by the LBM, and that explicitly imposed by $\hat{g}_i^{(1)}$, is ensured.

This important conclusion should be kept in mind when using a regularized model based on this reconstruction, such as the HRR model [29]. It has been demonstrated here with the D1Q3 lattice. It is shown in Sec. 5.4 that it remains true on the macroscopic equations of the D2Q9 lattice. This phenomenon explains why the correction had to be used in previous work based on the HRR collision model, even for low and moderate Mach numbers [80,86].

5.2. Corrected D1Q3 lattice: numerical properties of the degenerating hyperviscosity

The focus is now put on the corrected D1Q3 lattice, for which the numerical viscosity is cancelled. For the sake of simplicity, the numerical errors in Ψ_i are first neglected. The numerical dissipation is here mainly caused by the degenerating hyperviscosity characterized by Eq. (79). Using the conclusions of Eq. (90), it can be re-written as

$$\Gamma \sim \frac{\text{Kn}^2}{24} \left(\frac{\Delta t}{\tau} \right)^3 D_i^3 (\hat{g}_i^{(1)} - \Psi_i). \quad (91)$$

Studying the function $\hat{g}_i^{(1)} - \Psi_i$, which is explicitly known, should provide interesting properties on the degenerating hyperviscosity, *a fortiori* on the dissipation and stability properties of the model. It reads

$$\hat{g}_i^{(1)} - \Psi_i = \frac{w_i}{2c_s^4} (e_{i,x}^2 - c_s^2) \left[(u_x^3 + 3c_s^2(\theta - 1)u_x) \partial_x \rho + (3u_x^2 + c_s^2(\theta - 3)) \rho \partial_x u_x \right]. \quad (92)$$

In order to exhibit how this error can affect the dissipation of the acoustics, it is now possible to re-express it as function of the Riemann invariants, which are the characteristic quantities of a given physical phenomenon. For isothermal 1D cases, the two Riemann invariants R_+ and R_- are defined such that [87]

$$\rho \partial_x R_+ = \rho \partial_x u_x + c_s \sqrt{\theta} \partial_x \rho, \quad \rho \partial_x R_- = \rho \partial_x u_x - c_s \sqrt{\theta} \partial_x \rho, \quad (93)$$

where R_+ is the characteristic variable of the downstream acoustic wave, and R_- of the upstream one. Hence,

$$\partial_x u_x = \frac{1}{2} (\partial_x R_+ + \partial_x R_-), \quad \partial_x \rho = \frac{\rho}{2c_s \sqrt{\theta}} (\partial_x R_+ - \partial_x R_-). \quad (94)$$

Injecting them in Eq. (92) yields after simplification

$$\hat{g}_i^{(1)} - \Psi_i = \frac{w_i}{4c_s^2} (e_{i,x}^2 - c_s^2) \rho \theta \left[P_+(\text{Ma}) \partial_x R_+ + P_-(\text{Ma}) \partial_x R_- \right], \quad (95)$$

where $\text{Ma} = u_x / (c_s \sqrt{\theta})$ is the Mach number and

$$P_+(\text{Ma}) = \text{Ma}^3 + 3\text{Ma}^2 + 3\text{Ma} \left(1 - \frac{1}{\theta} \right) + 1 - \frac{3}{\theta}, \quad P_-(\text{Ma}) = P_+(-\text{Ma}). \quad (96)$$

This polynomial can be factorized as

$$P_+(\text{Ma}) = (\text{Ma} + 1) \left(\text{Ma} - \left(\frac{1}{c_s \sqrt{\theta}} - 1 \right) \right) \left(\text{Ma} + \left(\frac{1}{c_s \sqrt{\theta}} + 1 \right) \right), \quad (97)$$

which makes its three real roots clearly appear. For the downstream acoustic wave, $\text{Ma} = 1/(c_s \sqrt{\theta}) - 1$ is the only positive root of P_+ , which can be re-written as a Courant-Friedrich-Lewy condition [88],

$$\text{CFL} = 1, \quad \text{with} \quad \text{CFL} = u_x + c_s \sqrt{\theta} = c_s \sqrt{\theta} (\text{Ma} + 1). \quad (98)$$

Regarding the upstream acoustic wave, P_- has three positive roots: $\text{Ma} = 1$, $\text{Ma} = 1 + 1/(c_s \sqrt{\theta})$ and $\text{Ma} = 1 - 1/(c_s \sqrt{\theta})$, which is positive if $\theta > 3$.

As a consequence, the sign of the degenerating hyperviscosity is expected to theoretically change on a given wave for each of these roots, switching from a stabilizing error (over-dissipation) to a destabilizing one (negative dissipation). It can be summarized as follows:

- for the downstream acoustic wave, the hyperviscous error switches at $\text{CFL} = 1$,
- for the upstream acoustic wave, it switches at $\text{Ma} = 1$, at $\text{Ma} = 1 + 1/(c_s \sqrt{\theta})$ and at $\text{Ma} = 1 - 1/(c_s \sqrt{\theta})$ when $\theta > 3$.

This demonstration is in complete agreement with the stability limits of the HRR collision model observed by linear analyses in a previous work [89], namely $\text{Ma} < 1$ and $\text{CFL} < 1$. Note that similar limitations could even be recovered in a fully compressible framework, coupling the LB scheme with an additional energy equation.

In the following, this demonstration will be verified by explicitly computing the deviation terms of the D1Q3 lattice. Such conclusions will also be extended to the D2Q9 lattice in Sec. 5.4 and Appendix F.

5.3. Deviation terms of the D1Q3 lattice in the linear approximation

Starting from Eq. (78), an explicit expression of the deviation terms appearing in Eq. (22) involving spatial derivatives of macroscopic quantities has to be obtained. This is a prerequisite for obtaining the explicit deviations from the macroscopic equations, following Appendix A.

To this extent, an estimation of $D_i^2 f_i$, $D_i^3 f_i$ and $D_i^4 f_i$ is required with respectively a second-, first- and zeroth-order accuracy in Kn. The same goes for $D_i(\hat{g}_i^{(1)} - \Psi_i^d)$, $D_i^2(\hat{g}_i^{(1)} - \Psi_i^d)$ and $D_i^3(\hat{g}_i^{(1)} - \Psi_i^d)$. For this purpose, the computer algebra system Maxima [68] is used. Of considerable complexity, the procedure employed for these computations is not provided in details here. It is basically based on the following relations:

- the Taylor expansion of Ψ_i^d proposed in Appendix B, which makes Ψ_i explicitly appear,
- a Taylor expansion of the gradient terms involved in $\hat{g}_i^{(1)}$ depending on the discretization scheme (DCO2 or DUO1), similarly as in Appendix B,
- a second-order estimation of f_i as

$$f_i = f_i^{eq} + \text{Kn} (\Psi_i - D_i f_i^{eq}) + \text{Kn}^2 \left(D_i^2 f_i^{eq} - D_i \Psi_i + E_i^{(1)} \right) + O(\text{Kn}^3), \quad (99)$$

on which the derivation operator D_i^n can be applied,

- the chain rule of Eq. (55), that can be applied to f_i^{eq} , Ψ_i and $\hat{g}_i^{(1)}$,
- the macroscopic equations of Appendix A in order to transform any time-derivative to space-derivative.

Once the deviation terms $E_i^{(n)}$ obtained, their macroscopic counterpart $E_\Phi^{(n)}$ can be computed following the general procedure of Appendix A. The isothermal NS equations can finally be recovered as in Eqs. (23)-(24) with the deviation terms detailed below. All the consistency errors C_i and numerical terms N_i are provided in Appendix H.

5.3.1. Non corrected D1Q3, analytical reconstruction of $g_i^{(1)}$

In the non-corrected case and neglecting the discretization errors in $g_i^{(1)}$, the mass and momentum equations (23)-(24) are recovered with

$$\begin{aligned} E_\rho^{(1)} &= 0, & E_{\rho u_x}^{(1)} &= - \left(\frac{\Delta t}{2\tau} \right) \partial_{xx}^2 a_{eq,xxx}^{(3)}, \\ E_\rho^{(2)} &= \left(\frac{\Delta t}{\tau} \right)^2 \frac{1}{12} \left(- \frac{\partial^3 a_{eq,xxx}^{(3)}}{\partial x^3} + 2\rho c_s^2 \theta \frac{\partial^3 u_x}{\partial x^3} \right), & E_{\rho u_x}^{(2)} &= \left(\frac{\Delta t}{\tau} \right) \frac{C_3}{2} + \left(\frac{\Delta t}{\tau} \right)^2 N_{11}, \\ E_\rho^{(3)} &= \frac{1}{12} \left(\frac{\Delta t}{\tau} \right)^2 \partial_x C_3 + \left(\frac{\Delta t}{\tau} \right)^3 N_{12}, & E_{\rho u_x}^{(3)} &= \left(\frac{\Delta t}{\tau} \right) N_{13} + \left(\frac{\Delta t}{\tau} \right)^2 N_{14} + \left(\frac{\Delta t}{\tau} \right)^3 N_{16}. \end{aligned} \quad (100)$$

It is remarkable that there is no more consistency error with the isothermal NS equations in this model. In particular, even the well-known Mach error is removed thanks to the explicit computation of the off-equilibrium distribution functions based on a correct viscous stress tensor. Following a previous work [46], this indicates that the shear stress imposed *via* the reconstruction is the actual shear stress in the limit $\Delta t \rightarrow 0$. The only remaining terms are numerical errors which, contrary to the BGK model, include:

- a $\Delta t/\tau$ -dependent term in $E_{\rho u_x}^{(1)}$, indicating the numerical viscosity highlighted in Sec. 5.1,
- a $(\Delta t/\tau)^3$ -term in $E_{\rho}^{(3)}$ and $E_{\rho u_x}^{(3)}$, indicating the degenerating hyperviscosity of Sec. 5.2.

Also note that the numerical viscosity is directly related to the lattice defect $a_{eq.xxx}^{(3)}$. The ratio between this numerical viscosity and the physically expected one being of the order of $\Delta t/\tau$, this error is likely to have a very strong impact on the dissipation and the stability properties when the dimensionless relaxation time is small. For this reason, the correction term Ψ_i , which is expected to address this issue (*cf.* Sec. 5.1), is introduced in all the forthcoming analyses.

5.3.2. Analytically corrected D1Q3, analytical reconstruction of $g_i^{(1)}$

Introducing a correction term and neglecting the discretization errors in $g_i^{(1)}$ and Ψ_i , the mass and momentum equations (23)-(24) are recovered with

$$\begin{aligned} E_{\rho}^{(1)} &= 0, & E_{\rho u_x}^{(1)} &= 0, \\ E_{\rho}^{(2)} &= \left(\frac{\Delta t}{\tau}\right)^2 \frac{1}{12} \left(-\frac{\partial^3 a_{eq.xxx}^{(3)}}{\partial x^3} + 2\rho c_s^2 \theta \frac{\partial^3 u_x}{\partial x^3} \right), & E_{\rho u_x}^{(2)} &= \left(\frac{\Delta t}{2\tau}\right) C_3 + \left(\frac{\Delta t}{\tau}\right)^2 N_1, \\ E_{\rho}^{(3)} &= \frac{1}{12} \left(\frac{\Delta t}{\tau}\right)^2 \partial_x C_3, & E_{\rho u_x}^{(3)} &= \left(\frac{\Delta t}{\tau}\right) N_{13} + \left(\frac{\Delta t}{\tau}\right)^2 N_{17} + \left(\frac{\Delta t}{\tau}\right)^3 N_{18}. \end{aligned} \quad (101)$$

As predicted, the numerical viscosity is cancelled by the introduction of the correction term Ψ_i . An interesting feature of this term appears here: while it aims at correcting the first-order consistency error with the BGK collision model, it can be now used to correct a purely numerical error.

5.3.3. Correction with a DCO2 scheme, reconstruction of $g_i^{(1)}$ with a DCO2 scheme

Compared to Eq. (101), only the hyperviscous term is affected in the momentum equation as

$$E_{\rho u_x}^{(3)} = \left(\frac{\Delta t}{\tau}\right) N_{13} + \left(\frac{\Delta t}{\tau}\right)^2 \left(N_{17} + \frac{\rho\theta}{9} \frac{\partial^4 u_x}{\partial x^4} \right) + \left(\frac{\Delta t}{\tau}\right)^3 \left(N_{18} + \frac{1}{12} \frac{\partial^4 a_{eq.xxx}^{(3)}}{\partial x^4} - \frac{\rho\theta}{18} \frac{\partial^4 u_x}{\partial x^4} \right). \quad (102)$$

5.3.4. Correction with a DCO2 scheme, reconstruction of $g_i^{(1)}$ with a DUO1 scheme

Compared to Eq. (101), only the numerical errors in the momentum equation are affected as

$$\begin{aligned} E_{\rho u_x}^{(2)} &= \left(\frac{\Delta t}{\tau}\right) \left(\frac{C_3}{2} - \text{sgn}(u_x) \rho c_s^2 \theta \frac{\partial^3 u_x}{\partial x^3} \right) + \left(\frac{\Delta t}{\tau}\right)^2 \left(N_1 + \text{sgn}(u_x) \frac{\rho\theta}{6} \frac{\partial^3 u_x}{\partial x^3} \right), \\ E_{\rho u_x}^{(3)} &= \left(\frac{\Delta t}{\tau}\right) N_{13} + \left(\frac{\Delta t}{\tau}\right)^2 \left(N_{17} + \frac{\rho\theta}{9} \frac{\partial^4 u_x}{\partial x^4} - \text{sgn}(u_x) \frac{\partial_x C_3}{4} \right) \\ &\quad + \left(\frac{\Delta t}{\tau}\right)^3 \left(N_{18} + \frac{1}{12} \frac{\partial^4 a_{eq.xxx}^{(3)}}{\partial x^4} - \frac{\rho\theta}{18} \frac{\partial^4 u_x}{\partial x^4} + \text{sgn}(u_x) \frac{\partial_x C_3}{8} \right). \end{aligned} \quad (103)$$

Note that even if a first-order error in $\Delta t/\tau$ is introduced in the computation of $g_i^{(1)}$, it does not lead to numerical viscosity.

5.3.5. Correction with a DUO1 scheme, reconstruction of $g_i^{(1)}$ with a DCO2 scheme

Compared to Eq. (101), only the numerical errors in the momentum equation are affected as

$$\begin{aligned} E_{\rho u_x}^{(2)} &= \left(\frac{\Delta t}{2\tau}\right) C_3 + \left(\frac{\Delta t}{\tau}\right)^2 \left(N_1 - \frac{\text{sgn}(u_x)}{4} \frac{\partial^3 a_{eq.xxx}^{(3)}}{\partial x^3} \right), \\ E_{\rho u_x}^{(3)} &= \left(\frac{\Delta t}{\tau}\right) N_{13} + \left(\frac{\Delta t}{\tau}\right)^2 \left(N_{17} + \frac{\rho\theta}{9} \frac{\partial^4 u_x}{\partial x^4} \right) + \left(\frac{\Delta t}{\tau}\right)^3 \left(N_{18} + \frac{1}{12} \frac{\partial^4 a_{eq.xxx}^{(3)}}{\partial x^4} - \frac{\rho\theta}{18} \frac{\partial^4 u_x}{\partial x^4} + \text{sgn}(u_x) \frac{N_4}{8} \right). \end{aligned} \quad (104)$$

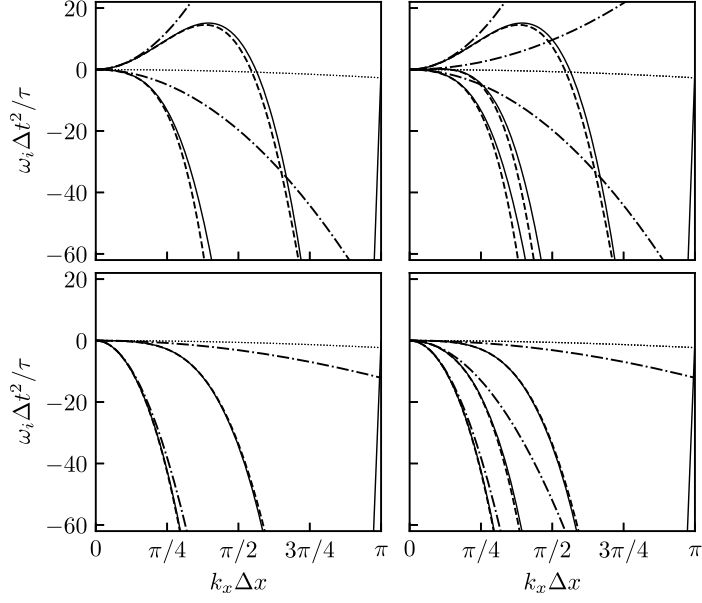


Fig. 6. Dissipation curves of the non-corrected D1Q3 lattice (left) and D2Q9 lattice with $N = 2$ (right) equipped with the shear stress reconstruction with an analytical computation of $g_i^{(1)}$. A horizontal mean flow is considered with $\bar{u}_x = 0.5c_s\sqrt{\theta}$ and $\tau/\Delta t = 10^{-3}$. Top: $\theta = 0.82$, bottom: $\theta = 0.7$. —: LB scheme,: isothermal NS equations, - · - · -: isothermal NS with numerical viscosity, - - -: isothermal NS with numerical viscosity and hyperviscosity.

5.3.6. Correction with a DUO1 scheme, reconstruction of $g_i^{(1)}$ with a DUO1 scheme

Compared to Eq. (101), only the numerical errors in the momentum equation are affected as

$$\begin{aligned}
 E_{\rho u_x}^{(2)} &= \left(\frac{\Delta t}{\tau}\right) \left(\frac{C_3}{2} - \text{sgn}(u_x) \rho c_s^2 \theta \frac{\partial^3 u_x}{\partial x^3}\right) + \left(\frac{\Delta t}{\tau}\right)^2 \left(N_1 - \frac{\text{sgn}(u_x)}{4} \frac{\partial^3 a_{eq,xxx}^{(3)}}{\partial x^3} + \text{sgn}(u_x) \frac{\rho \theta}{6} \frac{\partial^3 u_x}{\partial x^3}\right), \\
 E_{\rho u_x}^{(3)} &= \left(\frac{\Delta t}{\tau}\right) N_{13} + \left(\frac{\Delta t}{\tau}\right)^2 \left(N_{17} + \frac{\rho \theta}{9} \frac{\partial^4 u_x}{\partial x^4} - \text{sgn}(u_x) \frac{\partial_x C_3}{4}\right) \\
 &\quad + \left(\frac{\Delta t}{\tau}\right)^3 \left(N_{18} + \frac{1}{12} \frac{\partial^4 a_{eq,xxx}^{(3)}}{\partial x^4} - \frac{\rho \theta}{18} \frac{\partial^4 u_x}{\partial x^4} + \frac{\text{sgn}(u_x)}{8} (N_4 + \partial_x C_3)\right). \tag{105}
 \end{aligned}$$

5.4. Deviation terms of the D2Q9 lattice in the linear approximation

A similar work is performed on the D2Q9 lattice, for which deviation terms with the isothermal NS equations are provided in Appendix F in the linear approximation. Only the second-order equilibrium ($N = 2$) is considered, noticing that changing the order of the Hermite-based equilibrium has few impact on the general conclusions. Similar observations as with the D1Q3 lattice can be drawn: (1) the shear stress tensor reconstruction with $g_i^{(1)}$ allows recovering a perfect consistency with the NS equation in every case, (2) in absence of the body-force term correction Ψ_l , a numerical viscosity arises, (3) the latter can be cancelled by introducing the correction, eventually discretized, (4) in any case, a degenerating hyperviscosity occurs.

5.5. Linear analyses: impact of the numerical errors on the dissipation

All the expressions of error terms have been systematically validated by linear analyses, in the same way as with the BGK collision model of Sec. 3.6. Looking at the remaining errors $\Delta\omega^*/k^*$ between the eigenvalues of the LB scheme and that of the equivalent macroscopic equations allows for confirming the validity of the terms at every order in Kn. In this section, only the effect of error terms on the numerical dissipation is discussed.

Fig. 6 displays the dissipation curves of the non corrected D1Q3 and D2Q9 ($N = 2$) lattices with the shear stress tensor reconstruction. The parameters are arbitrarily chosen for the sake of readability at a horizontal Mach number $\text{Ma} = 0.5$, $\tau/\Delta t = 10^{-3}$ and two different values of θ : $\theta = 0.82$ and $\theta = 0.7$. The analyses of the LB schemes are compared to those of the isothermal NS equations without deviation terms ($p = 0$) and including the first-order deviation ($p = 1$) and up to the third-order one ($p = 3$). The last two cases emphasize the effects of the numerical viscosity and hyperviscosity, respectively.

In agreement with previous analyses, this particular regularization yields only two (resp. three) physical waves in 1D (resp. 2D), meaning that all the non-hydrodynamic modes are filtered out of a simulation [80,32]. With $\theta = 0.82$, the first-

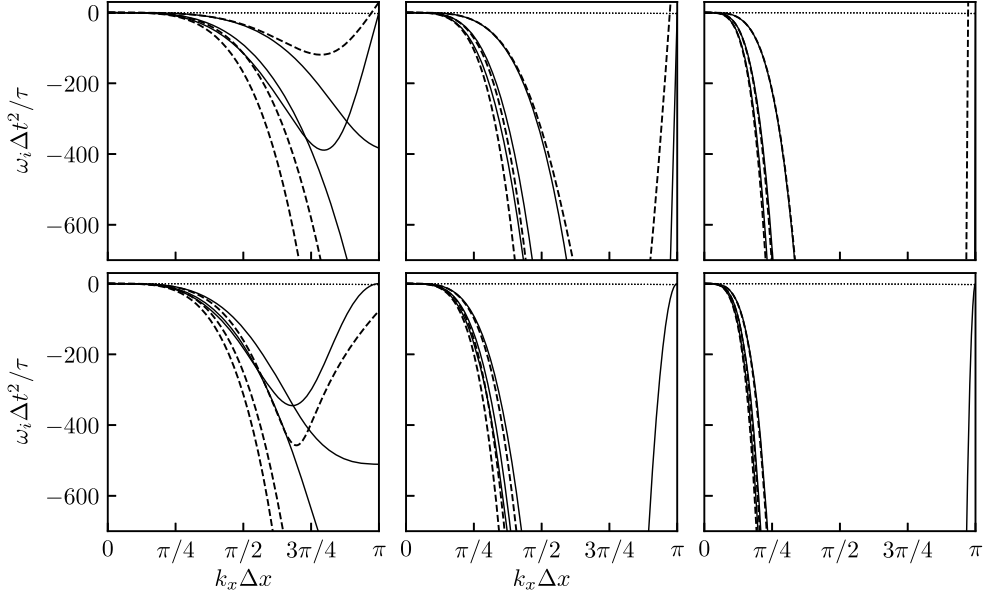


Fig. 7. Dissipation curves of the corrected D2Q9 lattice equipped with the shear stress reconstruction. A horizontal mean flow is considered with $\bar{u}_x = 0.5c_s\sqrt{\theta}$, $\theta = 0.8$ and three values of $\tau/\Delta t$: 10^{-3} (left), 10^{-4} (middle), 10^{-5} (right). Top: analytical computation of Ψ_i and $g_i^{(1)}$, bottom: a DCO2 scheme is used for their space-derivatives. —: LB scheme,: isothermal NS equations, ---: isothermal NS with numerical hyperviscosity.

order error is responsible for a destabilization of one acoustic wave with the D1Q3 lattice, as well as the additional shear wave of the D2Q9 lattice. These instabilities even occur in the well-resolved limit ($k_x \ll \Delta x$) and their order of magnitude can be very large compared to the isothermal NS equations. For all the waves, the numerical hyperviscosity has a stabilizing effect, which yet does not cancel the instability caused by the numerical viscosity for low wavenumbers. This competition between viscous and hyperviscous effects provides explanations to the instabilities observed in previous linear analyses of regularized models [32]. The bottom part of Fig. 6 ($\theta = 0.7$) highlights the strong impact of θ on the behaviour of the numerical error. In this particular case, both numerical viscosity and hyperviscosity induce an over-dissipation, leading to a stable model in the x -direction. Note that this does not allow drawing any conclusion on the linear stability of the scheme in other directions. Because of this large and unpredictable numerical viscosity, non-corrected models will no longer be discussed in the following, especially since this error can be simply addressed by introducing the body-force term Ψ_i .

Fig. 7 exhibits the dissipation properties of the corrected D2Q9 model with $N = 2$ for a horizontal mean flow at $Ma = 0.5$, $\theta = 0.8$ and three values of the dimensionless relaxation time: $\tau/\Delta t = 10^{-3}$, $\tau/\Delta t = 10^{-4}$ and $\tau/\Delta t = 10^{-5}$. The effect of the DCO2 discretization of Ψ_i and $g_i^{(1)}$ is also investigated. In any case and for the three expected physical waves, no more numerical viscosity is observed and the hyperviscosity induces a large over-dissipation compared to the isothermal NS equations. In addition to a qualitative validation of the error terms, the analyses performed at different values of $\tau/\Delta t$ exhibit the numerical origin of the error. The over-dissipation is all the more important as the dimensionless relaxation time is reduced, which further confirms the error in $\Delta t/\tau$ predicted by the hyperviscous degeneracy. Furthermore, the bottom part of Fig. 7 points out the impact of the discretization of Ψ_i and $g_i^{(1)}$ with a DCO2 scheme. Compared to their analytical computation, the numerical dissipation is further increased, but to a much lesser extent than that caused by the shear stress reconstruction. The over-dissipative character of this model, which was attributed to errors in the finite-difference estimation of the viscous stress tensor by previous authors [29], is therefore largely dominated by the degenerating hyperviscosity caused by the regularization procedure itself. This point is of paramount importance, since it is precisely this numerical dissipation that prevents from using this model as is. Instead, it is sometimes recommended to hybridize this shear stress reconstruction with a more standard regularization, such as the recursive one, as proposed in the so-called hybrid recursive regularized (HRR) model [29].

5.6. Impact of the degenerating hyperviscosity on the linear stability

Up to now, no clear discretization effect of Ψ_i and $g_i^{(1)}$ could be exhibited, which yet clearly affects the numerical error in hyperviscosity. In this section, the focus is put on its degenerating part, which may provide important conclusions on the choice of the discretization scheme. This is done here by considering the effect of the degenerating hyperviscosity only on the dissipation/amplification properties of the physical waves. For this purpose, the Euler equations are simply considered, onto which the $(\Delta/\tau)^3$ -related terms of $E_{\rho u_\alpha}^{(3)}$, referred to as H_α , are superimposed:

$$\partial_t \rho + \partial_\alpha (\rho u_\alpha) = 0, \quad \partial_t (\rho u_\alpha) + \partial_\beta (\rho u_\alpha u_\beta) + c_s^2 \theta \partial_\alpha \rho = H_\alpha. \quad (106)$$

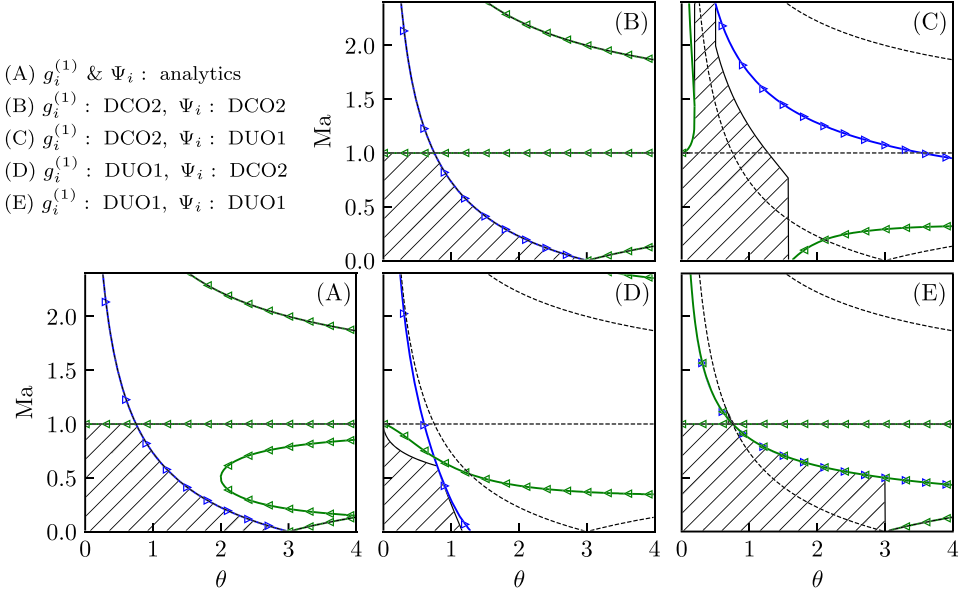


Fig. 8. Impact of the degenerating hyperviscosity on the linear stability of the corrected D1Q3 lattice equipped with the shear stress reconstruction. Contours of a null imaginary eigenvalue ω_i of Eq. (106) are displayed as: downstream acoustics (\rightarrow), upstream acoustics (\leftarrow). Dash lines represent the theoretical curves of Eq. (107). Hatched area: linear stability region of the LB scheme at $\tau/\Delta t = 10^{-5}$. (For interpretation of the colours in the figure(s), the reader is referred to the web version of this article.)

For instance, with the corrected D1Q3 lattice with analytical derivatives of Eq. (101), one has $H_x = N_{18}$. One interest of such a system is that it does not involve the dimensionless relaxation time anymore, which corresponds to the behaviour of the complete Eq. (101) in the limit of infinitely small values of $\tau/\Delta t$. Then, a linearization followed by a diagonalization of this reduced system, as proposed in Appendix C, leads to two acoustic eigenvalues. Studying the sign of their imaginary part ω_i in the low wavenumber limit provides information on the stabilizing or destabilizing effect of the degenerating hyperviscosity.

Fig. 8 displays the nullity curves of the two imaginary eigenvalues ω_i of the system (106) applied to the corrected D1Q3 lattice, for different values of the Mach number $Ma = u_x/(c_s\sqrt{\theta})$ and θ . Fives cases are considered depending on the way space gradients in $g_i^{(1)}$ and Ψ_i are discretized. These curves are compared with the theoretical values obtained in Sec. 5.2:

$$Ma = 1, \quad Ma = \frac{1}{c_s\sqrt{\theta}} - 1, \quad Ma = \frac{1}{c_s\sqrt{\theta}} + 1, \quad Ma = 1 - \frac{1}{c_s\sqrt{\theta}}. \quad (107)$$

Note that the second equation corresponds to the common condition CFL = 1.

Fig. 8 also displays hatched areas representing the linear stability regions obtained by performing a linear stability analysis of the isothermal LB scheme for $\tau/\Delta t = 10^{-5}$. In this case, stability is ensured provided that, for any value of $k_x\Delta x \in [-\pi, \pi]$ every eigenvalue ω is such that $\omega_i < 0$. The following observations can be made:

- Linear stability regions are always located below the annulment curves (\rightarrow) and (\leftarrow). In most of the cases, the instability is even encountered when crossing these curves. This confirms that the degenerating hyperviscosity is at the origin of the linear instability.
- The theoretical estimations of Sec. 5.2 (107) fit remarkably well the actual sign inversion of the degenerating hyperviscosity for the two acoustic waves when $g_i^{(1)}$ and Ψ_i are both analytically computed or estimated by a DCO2 discretization. However, using the DUO1 scheme in the estimation of Ψ_i or $g_i^{(1)}$, Eq. (107) cannot be used to predict its behaviour.
- With a DCO2 discretization, the stability limits are: $Ma = 1$ and $CFL = 1$, which is clearly caused by a sign inversion in the degenerating hyperviscosity. This is in complete agreement with previous observations [89].
- Evaluating Ψ_i with a DUO1 scheme and $g_i^{(1)}$ with a DCO2 one has an interesting effect on the stability: the theoretical limitations $Ma = 1$ and $CFL = 1$ can be overcome. This is done thanks to the modification of the hyperviscous error, which is now stabilizing for larger values of (Ma, θ) . This point is in agreement with an improved stability of the HRR collision model when the body-force term is evaluated by an upwind scheme, already observed in the literature [85,89, 90].

Similar studies are then performed on the D2Q9 lattice, considering the three possible Hermite-based equilibria. Fig. 9 displays the nullity curves of the degenerating hyperviscosity of the three physical eigenvalues, as well as the linear stability

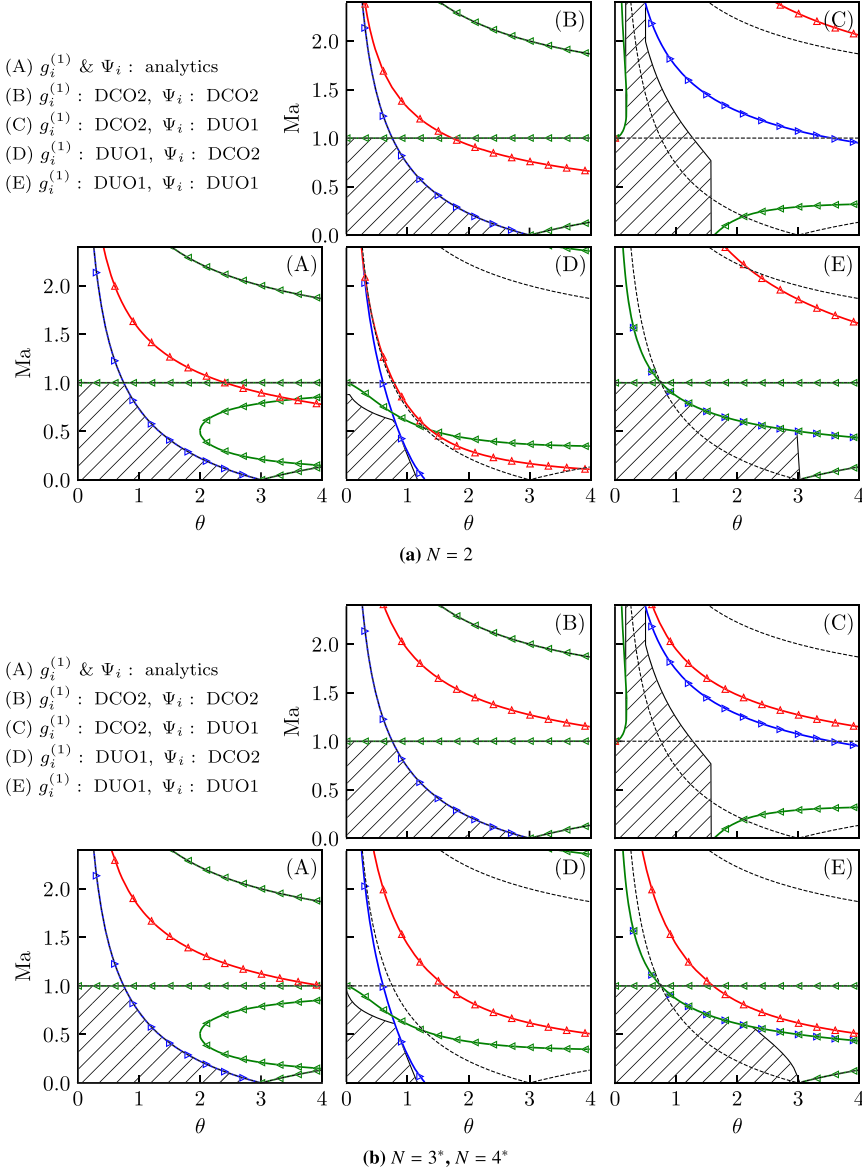


Fig. 9. Impact of the degenerating hyperviscosity on the linear stability of the corrected D2Q9 lattice equipped with the shear stress reconstruction, with a Hermite-based equilibrium at order N , considering the x -direction only. Contours of a null imaginary eigenvalue ω_i of Eq. (106) are displayed as: downstream acoustics (\blacktriangleright), upstream acoustics (\blacktriangleleft), shear wave (\blacktriangle). Dash lines represent the theoretical curves of Eq. (107). Hatched area: linear stability region of the LB scheme at $\tau/\Delta t = 10^{-5}$.

region, considering the x -direction only (for the gradients and the mean flow). Regarding the acoustics, the curves are identical to the D1Q3 lattice of Fig. 8. Only the appearance of a shear related eigenvalue can be noticed, whose behaviour is slightly affected by the order of the equilibrium distribution function. In any case, the stability of acoustic waves remains the more constraining one when looking at the x -direction only, and similar conclusions as with the D1Q3 lattice can be drawn. Also note that no difference is exhibited when comparing the $N = 3^*$ and $N = 4^*$ cases in the x -direction only.

Finally, every directions are considered with the D2Q9 lattice, and for the three Hermite-based equilibria, in Figs. 10-11. To this extent and following previous studies [32], the analyses are performed for any orientation of the mean flow $M_\theta \in [0^\circ, 45^\circ]$ and for $k_\theta \in [0^\circ, 180^\circ]$, where k_θ is the angle between \mathbf{k} and the x -axis. For each value of $\theta \in [0, 4]$, the minimal value of the Mach number ensuring a stabilizing degenerating hyperviscosity is retained. Note that, when performing studies in any direction, downstream and upstream acoustic waves cannot be distinguished from each other, they are simply referred to as acoustic waves. This time, every value of N leads to different results. In any case, no linear stability region can be observed when both $g_i^{(1)}$ and Ψ_i are computed with analytical gradients. This is due to an instability occurring for very large values of k , *i.e.* for under-resolved waves, which cannot be captured by the Taylor expansion. Same

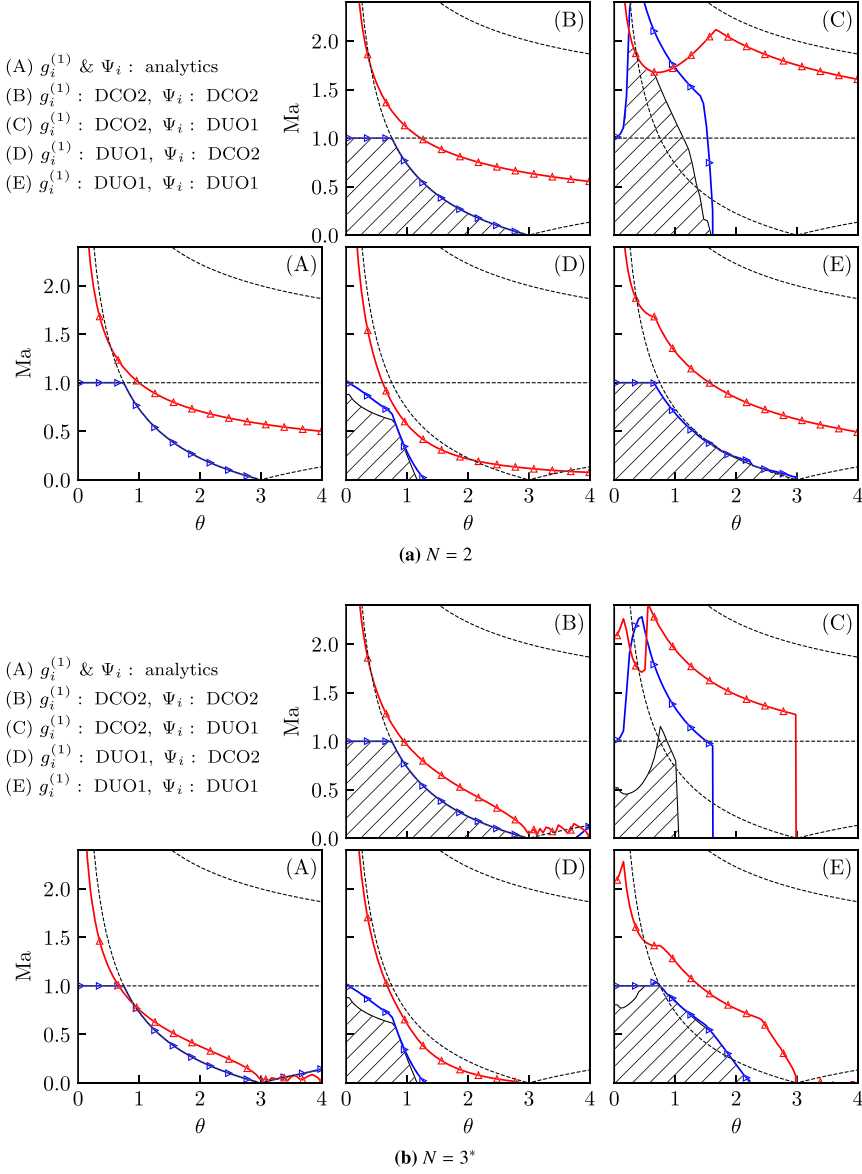


Fig. 10. Impact of the degenerating hyperviscosity on the linear stability of the corrected D2Q9 lattice equipped with the shear stress reconstruction, with a Hermite-based equilibrium at order N , considering all the possible directions. Contours of a null imaginary eigenvalue ω_i of Eq. (106) are displayed as: acoustic waves (\blacktriangleright), shear wave (\blacktriangleleft). Dash lines represent the theoretical curves of Eq. (107). Hatched area: linear stability region of the LB scheme at $\tau/\Delta t = 10^{-5}$.

phenomena explains all the discrepancies obtained between the linear stability areas (hatched areas) and the nullity curves of the hyperviscous degeneracy. Regarding the DCO2 discretization of $g_i^{(1)}$ and Ψ_i , similar stability limits as previously are observed in any case: $Ma < 1$ and $CFL < 1$. With $N = 2$, using a DUO1 discretization for Ψ_i still allows reaching Mach numbers $Ma > 1$, even though this effect is reduced compared to the D1Q3 case because of a destabilizing hyperviscosity affecting the shear wave. However, with $N = 3^*$ and $N = 4^*$, the stability region is much reduced, which is not due to the degenerating hyperviscosity but to an under-resolution effect.

5.7. Summary of the numerical properties of the shear stress tensor reconstruction

This comprehensive study of the shear stress tensor reconstruction highlights important properties shared by several LB schemes. The main interest of this model is that, since the regularized part $g_i^{(1)}$ is known as an explicit function of ρ and u_α , deviation terms of the regularized models can be deeply scrutinized and general conclusions can be drawn. Moreover,

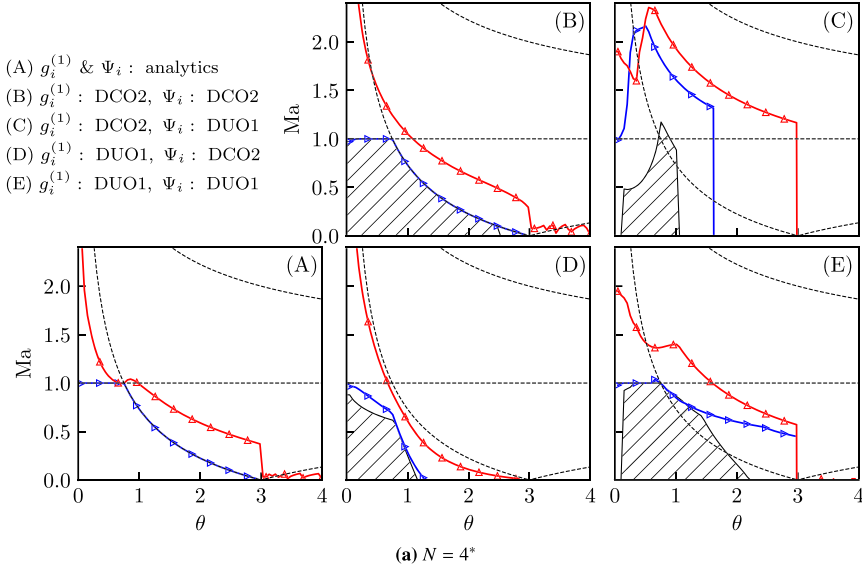


Fig. 11. Impact of the degenerating hyperviscosity on the linear stability of the corrected D2Q9 lattice equipped with the shear stress reconstruction, with a Hermite-based equilibrium at order N , considering all the possible directions. Contours of a null imaginary eigenvalue ω_i of Eq. (106) are displayed as: acoustic waves (\blacktriangleright), shear wave (\blacktriangleleft). Dash lines represent the theoretical curves of Eq. (107). Hatched area: linear stability region of the LB scheme at $\tau/\Delta t = 10^{-5}$.

Table 2

Summary of the nature of viscous deviations (Kn^1 -terms) affecting the BGK and HRR- $\sigma = 0$ collision models.

	BGK model	HRR- $\sigma = 0$
No Mach correction	Consistency error	Numerical error
Correction with Ψ_i	Correct viscosity	Correct viscosity

the analysis of the D1Q3 lattice is made possible, while PR and RR regularizations, as well as MRT models, are reduced to the BGK collision in the D1Q3 case. The following major conclusions can be drawn:

- The shear stress reconstruction is sufficient to recover a complete consistency with the NS equations. In particular, the Galilean invariance errors in the stress tensor are cured.
- In absence of correction term Ψ_i , a numerical viscosity is evidenced, consequent of the first-order accuracy of the numerical scheme. Surprisingly, introducing the correction term Ψ_i , designed to fix consistency errors, cancels this numerical viscosity. This property is summarized in Table 2.
- A degenerating numerical hyperviscosity is at the origin of over-dissipation and severe instabilities occurring for well resolved length scales, especially when the dimensionless relaxation time is low.
- With the DCO2 discretization for $g_i^{(1)}$ and Ψ_i , theoretical stability limits have been found as $Ma = 1$ and $CFL = 1$.
- Using a DUO1 discretization for Ψ_i allows increasing the range of stable Mach numbers, up to $Ma \approx 2$.

Obviously, the present study being restricted to isothermal LB methods, simulations of large Mach numbers would be unphysical. However, the present conclusions are in perfect agreement with previous observations drawn with compressible models based on a hybrid approach [85,89], indicating that the numerical properties of their LB part is mainly responsible for the overall behaviour. Especially, this confirms the benefits of an upwind estimation of the correction term.

This shear stress tensor reconstruction also provides the interest of filtering out any non-hydrodynamic mode [80,32]. Unfortunately, the aforementioned numerical errors in hyperviscosity yields an over-dissipation that makes it unusable as is. This is why one usually prefers to hybridize it with the more common projected and recursive regularizations. The latter are investigated in the next section.

6. Projected and recursive regularizations

This section aims at performing the Taylor expansion of two types of regularized models sharing strong similarities: the PR and RR models. Since these models are reduced to the BGK one in the D1Q3 case, only the D2Q9 lattice is considered here. One purpose of the present work is to provide some explanations to their unexpected dissipation properties exhibited in a previous work [32]. A unified formalism will be derived to simplify the analyses.

Table 3Coefficients of the matrix \mathbf{P} of Eq. (112) depending on the regularization scheme (PR or RR).

Regularization	λ_1	λ_2	λ_3	λ_4	λ_5	λ_6	λ_7	λ_8	λ_9
PR	0	0	0	0	0	0	0	0	0
RR, $N_r = 3^*$	u_y	$2u_x$	0	0	$2u_y$	u_x	0	0	0
RR, $N_r = 4^*$	u_y	$2u_x$	0	0	$2u_y$	u_x	u_y^2	$4u_x u_y$	u_x^2

6.1. Unified formalism

In the projected (PR) and the recursive regularization (RR) including a body-force term, off-equilibrium distribution functions read [25,26,28,62]

$$\text{PR: } g_i^{(1)} = \frac{w_i}{2c_s^4} a_{1,\alpha\beta}^{(2)} \mathcal{H}_{i,\alpha\beta}^{(2)} \quad \text{where} \quad a_{1,\alpha\beta}^{(2)} = \sum_j \mathcal{H}_{j,\alpha\beta}^{(2)} \left(g_j - f_j^{eq} + \text{Kn} \frac{\Delta t}{2\tau} \Psi_j^d \right), \quad (108)$$

$$\text{RR: } g_i^{(1)} = w_i \sum_{n=2}^{N_r} \frac{1}{n! c_s^{2n}} \mathbf{a}_1^{(n)} : \mathcal{H}_i^{(n)} \quad \text{where} \quad a_{1,\alpha_1 \dots \alpha_n}^{(n \geq 3)} = u_{\alpha_n} a_{1,\alpha_1 \dots \alpha_{n-1}}^{(n-1)} + \left[u_{\alpha_1} \dots u_{\alpha_{n-2}} a_{1,\alpha_{n-1} \alpha_n}^{(2)} + \text{perm}(\alpha_n) \right], \quad (109)$$

where N_r is the order of the recursive regularization, which obeys the same constraints as N , and $\text{perm}(\alpha_n)$ stands for all the cyclic permutations of indexes from α_1 to α_{n-1} . With the D2Q9 lattice, the off-equilibrium coefficients of interest read

$$a_{1,xy}^{(3)} = u_y a_{1,xx}^{(2)} + 2u_x a_{1,xy}^{(2)}, \quad a_{1,yy}^{(3)} = 2u_y a_{1,xy}^{(2)} + u_x a_{1,yy}^{(2)}, \quad a_{1,xyy}^{(4)} = u_y^2 a_{1,xx}^{(2)} + 4u_x u_y a_{1,xy}^{(2)} + u_x^2 a_{1,yy}^{(2)}. \quad (110)$$

In the D2Q9 case, regularized distribution functions can be equivalently written in a general way as

$$g_i^{(1)} = [\mathbf{H}^{-1} \mathbf{P} \mathbf{H}]_{ij} \left(g_j - f_j^{eq} + \text{Kn} \frac{\Delta t}{2\tau} \Psi_j^d \right), \quad (111)$$

where matrices \mathbf{H} and \mathbf{P} are defined as

$$\mathbf{H} = \begin{pmatrix} 1 & \dots & 1 \\ e_{0,x} & \dots & e_{8,x} \\ e_{0,y} & \dots & e_{8,y} \\ \mathcal{H}_{0,xx}^{(2)} & \dots & \mathcal{H}_{8,xx}^{(2)} \\ \mathcal{H}_{0,xy}^{(2)} & \dots & \mathcal{H}_{8,xy}^{(2)} \\ \mathcal{H}_{0,yy}^{(2)} & \dots & \mathcal{H}_{8,yy}^{(2)} \\ \mathcal{H}_{0,xyy}^{(3)} & \dots & \mathcal{H}_{8,xyy}^{(3)} \\ \mathcal{H}_{0,xyy}^{(3)} & \dots & \mathcal{H}_{8,xyy}^{(3)} \\ \mathcal{H}_{0,xyy}^{(4)} & \dots & \mathcal{H}_{8,xyy}^{(4)} \end{pmatrix}, \quad \mathbf{P} = \begin{pmatrix} 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & \lambda_1 & \lambda_2 & \lambda_3 & 0 & 0 & 0 \\ 0 & 0 & 0 & \lambda_4 & \lambda_5 & \lambda_6 & 0 & 0 & 0 \\ 0 & 0 & 0 & \lambda_7 & \lambda_8 & \lambda_9 & 0 & 0 & 0 \end{pmatrix}. \quad (112)$$

The coefficients λ_i depend on the regularization and are provided in Table 3.

Thanks to this equivalent matrix formulation of the PR and RR models, a straightforward link can be drawn with the MRT family of collision kernels, since

$$g_i^c = g_i + \underbrace{\left[\left(1 - \frac{\Delta t}{\tau + \Delta t/2} \right) [\mathbf{H}^{-1} \mathbf{P} \mathbf{H}]_{ij} + \delta_{ij} \right]}_{M_{ij}} \left(g_j - f_j^{eq} + \text{Kn} \frac{\Delta t}{2\tau} \Psi_j^d \right) + \frac{\Delta t}{\tau} \text{Kn} \Psi_i^d, \quad (113)$$

where M_{ij} can be interpreted as a matrix for a collision with multiple relaxation times. Previous relations between the PR model and Hermite-based MRT models have already been found in the literature [30,32], as well as between the RR scheme with $N = N_r = 4^*$ and a MRT model based on central Hermite moments [31]. Here, such a unified formalism is interesting since it allows an easy switch between the three models of interest.

6.2. Variable change

In order to incorporate this definition of $g_i^{(1)}$ into the generic Taylor expansion of regularized models of Eq. (78), a variable change has now to be performed so that the f_i variables explicitly appear. Combining Eq. (111) with the variable change of Eq. (68) yields

$$g_i^{(1)} = [\mathbf{H}^{-1}\mathbf{PH}]_{ij} \left(\left(1 - \frac{\Delta t}{\tau + \Delta t/2} \right) g_j^{(1)} + \frac{\Delta t}{\tau} (f_j - f_j^{eq}) \right) \quad (114)$$

$$\Rightarrow \left[\mathbf{I} + \left(\frac{\Delta t}{\tau + \Delta t/2} \right) \mathbf{H}^{-1}\mathbf{PH} \right]_{ij} g_j^{(1)} = \frac{\Delta t}{\tau} [\mathbf{H}^{-1}\mathbf{PH}]_{ij} (f_j - f_j^{eq}), \quad (115)$$

so that, by inverting this system, one finally has

$$g_i^{(1)} = \frac{\Delta t}{\tau} \mathbf{T}_{ij} (f_j - f_j^{eq}) \quad \text{with} \quad \mathbf{T} = \left[\mathbf{I} + \left(\frac{\Delta t}{\tau + \Delta t/2} \right) \mathbf{H}^{-1}\mathbf{PH} \right]^{-1} \mathbf{H}^{-1}\mathbf{PH}. \quad (116)$$

Regularized distribution functions are then directly related to the off-equilibrium populations $f_i - f_i^{eq}$, which is in the order of magnitude of the Knudsen number. Then, the definition of $\hat{g}_i^{(1)}$ of Eq. (77) makes sense in the context of PR and RR models, leading to

$$\hat{g}_i^{(1)} = \frac{1}{\text{Kn}} \frac{\Delta t}{\tau + \Delta t/2} \mathbf{T}_{ij} (f_j - f_j^{eq}). \quad (117)$$

6.3. Computation of error terms in the linear approximation

Once $\hat{g}_i^{(1)}$ is explicitly known for both models, the deviation terms with regards to the DVBE $E_i^{(n)}$ can be computed using the Taylor expansion of Eq. (78). This is done following the same procedure as with the shear stress reconstruction of Sec. 5.4. A particularity of the PR and RR models is that, given the matrix-shape of the regularized distributions, cross derivatives appear as

$$\begin{aligned} D_i D_j &= (\partial_t + e_{i,\alpha} \partial_\alpha) (\partial_t + e_{j,\beta} \partial_\beta), \quad D_i D_j D_k = (\partial_t + e_{i,\alpha} \partial_\alpha) (\partial_t + e_{j,\beta} \partial_\beta) (\partial_t + e_{k,\gamma} \partial_\gamma), \\ D_i D_j D_k D_l &= (\partial_t + e_{i,\alpha} \partial_\alpha) (\partial_t + e_{j,\beta} \partial_\beta) (\partial_t + e_{k,\gamma} \partial_\gamma) (\partial_t + e_{l,\delta} \partial_\delta). \end{aligned} \quad (118)$$

Here again, the computer algebra system Maxima [68] is used to compile the equations, providing the $E_i^{(n)}$ terms as well as the macroscopic deviations $E_\rho^{(n)}$ and $E_{\rho u_\alpha}^{(n)}$, following Appendix A. The latter are provided below in the D2Q9 case for the PR and RR models, for several equilibria and with different implementations of the correction terms. Note that similar deviation terms are obtained in the x direction for $N = 3^*$ and $N = 4^*$, as well as for $N_r = 3^*$ and $N_r = 4^*$ in the case of the RR collision model.

Below, only the modified error terms compared to the BGK counterpart are provided, considering derivatives in the x -direction for the sake of simplicity.

6.3.1. Non corrected PR model with $N = 2$

In this case, the y -momentum equation is affected with

$$\begin{aligned} E_{\rho u_y}^{(2)} &= \left(C_5 + 2c_s^2 \frac{\partial^3(\rho u_x u_y)}{\partial x^3} \right) - \left(\frac{\Delta t}{\tau} \right) c_s^2 \frac{\partial^3(\rho u_x u_y)}{\partial x^3} + \left(\frac{\Delta t}{\tau} \right)^2 N_5, \\ E_{\rho u_y}^{(3)} &= C_{11} + \left(\frac{\Delta t}{\tau} \right) N_{27} + \left(\frac{\Delta t}{\tau} \right)^2 (N_6 - N_{28}) + \left(\frac{\Delta t}{\tau} \right)^3 \frac{1}{4} N_{28}. \end{aligned} \quad (119)$$

Two types of numerical errors arise: a first-order error in time, in agreement with a first-order accuracy expected from a previous work [45,32], and a degenerating numerical hyperviscosity related to the N_{28} term. For a horizontal mean flow, the latter behaves as

$$N_{28} |_{(u_y=0)} = \frac{\rho u_x^2}{3} \frac{\partial^4 u_y}{\partial x^4}. \quad (120)$$

Let us recall here that a positive coefficient in front of a fourth-order gradient yields an anti-dissipation. Hence this numerical error is likely to be at the origin of the instability of the shear waves exhibited in a previous work [32], which will be further confirmed in Sec. 6.6.

6.3.2. Non corrected RR model with $N_r = 3^*, 4^*$ and $N = 2$

In this case, the y -momentum equation is affected with

$$E_{\rho u_y}^{(2)} = C_{13} + \left(\frac{\Delta t}{\tau} \right) N_{30} + \left(\frac{\Delta t}{\tau} \right)^2 N_5, \quad E_{\rho u_y}^{(3)} = C_{14} + \left(\frac{\Delta t}{\tau} \right) N_{31} + \left(\frac{\Delta t}{\tau} \right)^2 (N_6 + N_{32}) + \left(\frac{\Delta t}{\tau} \right)^3 N_{33}, \quad (121)$$

Exactly like the PR model, both first-order error in Δt and a degenerating hyperviscosity (N_{33}) are introduced. For a horizontal mean flow, the latter behaves as

$$N_{33}|_{(u_y=0)} = \frac{\rho u_x^4}{4} \frac{\partial^4 u_y}{\partial x^4}, \quad (122)$$

which is a destabilizing hyperviscosity affecting the shear wave only.

6.3.3. Non corrected PR model with $N = 3^*, 4^*$

In this case, the y -momentum equation is affected with

$$\begin{aligned} E_{\rho u_y}^{(2)} &= a_{eq,xxx}^{(3)} \frac{\partial^3 u_y}{\partial x^3} + C_{15} - \left(\frac{\Delta t}{2\tau}\right) C_{15} + \left(\frac{\Delta t}{\tau}\right)^2 N_{15}, \\ E_{\rho u_y}^{(3)} &= C_{16} + \left(\frac{\Delta t}{\tau}\right) N_{40} + \left(\frac{\Delta t}{\tau}\right)^2 (N_{10} + N_{41}) + \left(\frac{\Delta t}{\tau}\right)^3 N_{42}. \end{aligned} \quad (123)$$

Again, a first-order error in Δt together with a degenerating hyperviscosity, related to the N_{42} term, occur. For a horizontal mean flow, the latter behaves as

$$N_{42}|_{(u_y=0)} = -\frac{1}{8}\rho \left(u_x^4 + (c_s^2\theta - 1)u_x^2\right) \frac{\partial^4 u_y}{\partial x^4}. \quad (124)$$

6.3.4. Non corrected RR model with $N_r = 3^*, 4^*$ and $N = 3^*, 4^*$

In this case, the y -momentum equation is affected with

$$\begin{aligned} E_{\rho u_y}^{(2)} &= \left(\frac{\Delta t}{2\tau}\right) a_{eq,xxx}^{(3)} \frac{\partial^3 u_y}{\partial x^3} + \left(\frac{\Delta t}{\tau}\right)^2 N_{15}, \\ E_{\rho u_y}^{(3)} &= -\frac{\rho\theta^2}{9} \frac{\partial^4 u_y}{\partial x^4} - \left(\frac{\Delta t}{6\tau}\right) (3\theta u_x^2 + c_s^2\theta^2 - \theta)\rho \frac{\partial^4 u_y}{\partial x^4} + \left(\frac{\Delta t}{\tau}\right)^2 \left(N_{10} + \rho u_x a_{eq,xxx}^{(3)} \frac{\partial^4 u_y}{\partial x^4}\right) + \left(\frac{\Delta t}{\tau}\right)^3 N_{44}. \end{aligned} \quad (125)$$

The degenerating hyperviscosity is here similar to the PR model for a horizontal mean flow.

6.4. Corrected models

Deviation terms of corrected PR and RR models are provided in Appendix G. The correction term Ψ_i is either computed analytically, or discretized with a DCO2 and a DUO1 scheme.

6.5. Hyperviscous degeneracy of PR and RR models

Expliciting the deviation terms of the PR and RR models allows highlighting three specific features of the regularization. First, the scheme is globally first-order accurate in time, as prospected in a previous work [32], but the corresponding errors do not affect the recovery of the NS equations. This first-order accuracy in Δt could be guessed from the general Taylor expansion of regularized models of Eq. (78). It is now clearly exhibited for each model. The fact that the NS level remains second-order accurate is in agreement with past convergence studies [30,26,91–94]. Secondly, the regularization step induces a degenerating hyperviscosity in each model. The latter remains uncontrolled as an unexpected consequence of time and space discretization errors. This point could also be guessed from the general form of Eq. (78). This uncontrolled error is as large as the dimensionless relaxation time is low, and causes an unintended dissipation or instability, depending on the sign of the numerical hyperviscosity. Thirdly, while the add of a correction term Ψ_i affects the degenerating hyperviscosity, the way it is discretized (DCO2 or DUO1 schemes) has no effect on it when the x direction is considered only.

A summary of the degenerating hyperviscous terms affecting the PR and RR models is provided in Table 4 for different equilibria, corrected or not, when only the x -derivatives are considered together with the assumption of a horizontal mean flow. In any case, only a space derivative of the transverse velocity (u_y) affects the conservation equation of the y -momentum, which means that this numerical error has an impact on the shear waves only. These errors terms are provided here along the x -direction only for the sake of simplicity, without questioning the generalities of the methodology. When other directions are considered, far more complex phenomena occur which prevent from drawing such simple conclusions. In particular, an anisotropy of both acoustic and shear phenomena is expected in two dimensions [32].

Table 4

Summary of the degenerating hyperviscous terms arising in $E_{\rho u_y}^{(3)}$ with the PR and RR models on the D2Q9 lattice, when only x -derivatives are considered and with a horizontal mean flow assumption.

	PR model	RR model with $N_r = 3^*, 4^*$
$N = 2$, non corrected	$\frac{\rho u_x^2}{12} \frac{\partial^4 u_y}{\partial x^4}$ (destabilizing)	$\frac{\rho u_x^4}{4} \frac{\partial^4 u_y}{\partial x^4}$ (destabilizing)
$N = 2$, corrected	$\frac{\rho u_x^2}{12} \frac{\partial^4 u_y}{\partial x^4}$ (destabilizing)	$(1 - \theta) \frac{\rho u_x^2}{12} \frac{\partial^4 u_y}{\partial x^4}$ (stabilizing when $\theta > 1$)
$N = 3^*, 4^*$, non corrected	$-\frac{1}{8} \rho (u_x^4 + (c_s^2 \theta - 1) u_x^2) \frac{\partial^4 u_y}{\partial x^4}$ (stabilizing when $\text{Ma}^2 \geq 1/(c_s^2 \theta) - 1$)	$-\frac{1}{8} \rho (u_x^4 + (\theta - 1) u_x^2) \frac{\partial^4 u_y}{\partial x^4}$ (stabilizing when $\text{Ma}^2 \geq (1 - \theta)/(c_s^2 \theta)$)
$N = 3^*, 4^*$, corrected	$-\frac{1}{8} \rho (u_x^4 + (c_s^2 \theta - 1) u_x^2) \frac{\partial^4 u_y}{\partial x^4}$ (stabilizing when $\text{Ma}^2 \geq 1/(c_s^2 \theta) - 1$)	$-\frac{1}{8} \rho (u_x^4 + (\theta - 1) u_x^2) \frac{\partial^4 u_y}{\partial x^4}$ (stabilizing when $\text{Ma}^2 \geq (1 - \theta)/(c_s^2 \theta)$)

6.6. Validation with linear analyses

As previously, the error terms provided above have been quantitatively validated by comparing the linear analyses of the regularized LB schemes with that of the macroscopic equations obtained by the Taylor expansion, following the methodology detailed in Sec. 3.6. In the present section, a more qualitative study is proposed to investigate the impact of the numerical error on the dissipation properties in the linear approximation.

Fig. 12 displays the dissipation curves obtained from linear analyses of the PR and RR models in the x -direction, with a horizontal mean flow at $\text{Ma} = 0.25$. In the present case, the discretization effects of the correction term Ψ_i are not considered since they do not affect the hyperviscous degeneracy. These curves are compared with the analyses of the isothermal NS equations including the deviation terms up to the third-order in Kn . The analytical estimation of the degenerating hyperviscosity from Table 4 is also presented. For the latter, the dimensionless amplification rate is simply obtained by replacing the fourth-order derivative of u_y by $(k_x \Delta x)^4$, e.g. for the non corrected PR model with $N = 2$:

$$\omega_i \Delta t = \frac{\rho u_x^2}{12} (k_x \Delta x)^4. \quad (126)$$

Analyses with a fourth-order equilibrium and a fourth-order regularization show no difference, in the x -direction, with the third-order cases. Therefore, only combinations of $N = 2, 3^*$ and $N_r = 2, 3^*$ are displayed on the figure.

A very good agreement is obtained between all the curves, except a supplementary non-hydrodynamic wave, whose behaviour cannot be predicted by Taylor expansions in Kn . As expected, only one wave (the shear wave) is greatly affected by the regularization in the x -direction. Especially, the analytical estimation of the numerical hyperviscosity provides an accurate estimation of its behaviour. This indicates that the hyperviscous degeneracy is responsible for the large instabilities and over-dissipation of this wave compared to the theoretically expected curves, for a dimensionless relaxation time $\tau/\Delta t = 10^{-5}$. As a consequence, every models are unstable at low Mach number when $\theta < 1$, even though stability can be recovered for large wavenumbers with the RR model, which is due to uncontrolled higher Knudsen effects. For $3 > \theta \geq 1$, only three models can ensure a stable shear wave in the x -direction for a non zero Mach number: the corrected RR model with $N = 2$ and the RR model with $N = 3^*$, corrected or not.

Unfortunately, other studies of the hyperviscous degeneracy performed in any direction (not shown here) indicate that, whatever the considered model (PR or RR), there still exists a combination of directions for which it is destabilizing even at very low Mach number ($\text{Ma} = 0.01$). Hence, the degenerating hyperviscosity is globally destabilizing for both the PR and RR models on the D2Q9 lattice. As a consequence, the numerical scheme becomes unstable when the dimensionless relaxation time decreases, even for very low Mach numbers. This explains why the critical Mach numbers obtained by linear stability analyses conducted in previous work tend to zero in the zero-viscosity limit [40,45,78,32].

6.7. Summary

In summary, the Taylor expansions performed on the PR and RR models lead to the following general conclusions:

- Even if the scheme is globally first-order accurate in Δt , no first-order error affects the isothermal NS level. In particular, these schemes induce no numerical viscosity.
- A degenerating hyperviscosity has been exhibited, which, when only the x -direction is considered, affects the shear wave only. Its analytical expression could be obtained and validated with linear analyses.
- Considering all the possible directions, the degenerating hyperviscosity is destabilizing for both PR and RR models.

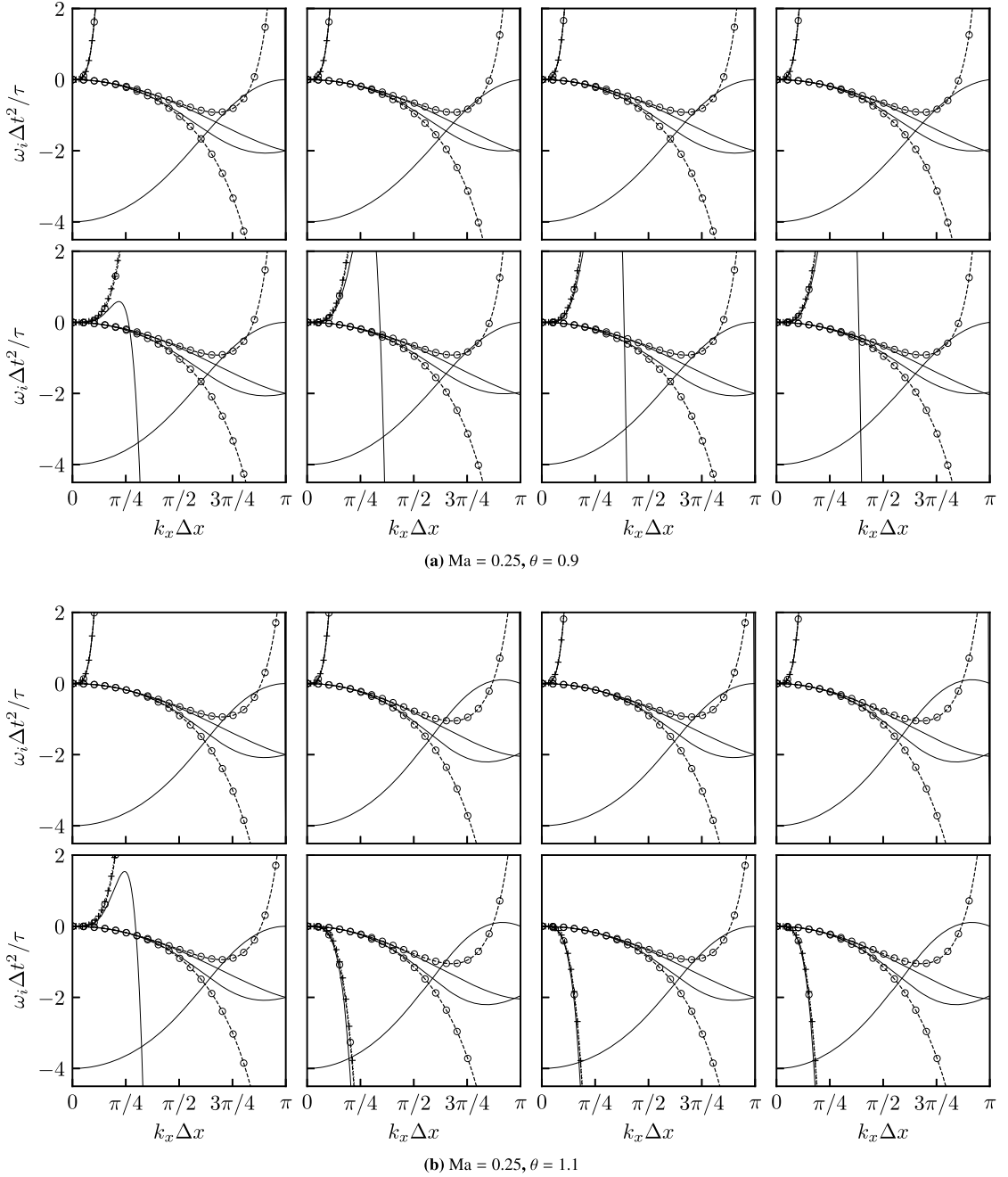


Fig. 12. Dissipation curves of the PR and RR models with the D2Q9 lattice considering horizontal plane waves ($k_y = 0$), a horizontal mean flow at $Ma = 0.25$ and $\tau/\Delta t = 10^{-5}$. Top: PR model, bottom: RR model with $N_r = 3^*$. From left to right: $N = 2$ non corrected, $N = 2$ with analytical correction, $N = 3^*$ non corrected, $N = 3^*$ with analytical correction. Three linear analyses are compared: the LB scheme (—), the NS equations including deviation terms up to Kn^3 (-○-○-), and the estimated degenerating hyperviscosity of Table 4 (⋯+⋯).

In addition to the instabilities, the numerical error in hyperviscosity results in a strong anisotropy of the dissipation properties of the PR and RR models, exhibited in a previous work [32].

In practice, the instabilities can be of relatively low amplitude, such as with the non corrected RR model with $N = 2$ of Fig. 12b. But the scheme remains linearly unstable, and the instabilities are all the more pronounced as the dimensionless relaxation time decreases. As a consequence, there is no combination of parameters (Ma, θ) for which the hyperviscosity is stabilizing in any direction, unlike the shear stress reconstruction of Sec. 5. This is the main reason why these models are sometimes coupled with each other with a parameter σ , giving birth to the so-called hybrid recursive regularized (HRR) scheme [29]. Unfortunately, its numerical errors are unlikely to be a simple linear combination of that of the RR

and the shear stress reconstruction. This is due to three reasons: (1) the complex moment cascade, (2) the fact that the variable change of the PR/RR model is also affected by σ , (3) the fact that, in the original model of Jacob et al. [29], the recurrence also applies to the complete reconstruction of the shear stress tensor, which has not been considered here. A Taylor expansion of this model could be the purpose of future work.

7. Application to MRT models

Given the strong analogy that can be drawn between PR/RR schemes and MRT models, one can finally wonder how the latter behave in terms of numerical error, more precisely regarding their dissipation properties. In this regard, an increasing numerical error of some athermal MRT models has already been exhibited in the incompressible limit by Dellar [79]. Noticing that reducing the Mach number of a simulation for a fixed Reynolds number comes down to decreasing the dimensionless relaxation time related to the kinematic viscosity, it is likely that a degenerating hyperviscosity is at the origin of such an error. To shed some light on these phenomena, a Taylor expansion in Kn is proposed here for some MRT models of interest. For the sake of simplicity, the correction term Ψ_i is not considered in this section. As a consequence, $\theta = 1$ is adopted here, since a value of $\theta \neq 1$ would yield a very large error (linear in Mach number) in the shear stress tensor. Moreover, only the D2Q9 lattice is considered in this section.

7.1. Description of the MRT models under consideration

Post-collision population of MRT models can generally be written as

$$g_i^c = g_i - \mathbf{C}_{ij} (g_j - f_j^{eq}), \quad (127)$$

where \mathbf{C} , the collision matrix, is supposed to be diagonal when written in a certain basis of moments, which means that every moments are relaxed independently towards an equilibrium state. The collision matrix then reads

$$\mathbf{C} = \mathbf{M}^{-1} \mathbf{S} \mathbf{M}, \quad (128)$$

where \mathbf{S} is a diagonal matrix of relaxation rates and \mathbf{M} is the matrix of the considered moments. In the present work, four bases of moments are considered: the so-called raw-moments (RM), the central moments (CM), the Hermite moments (HM) and the central Hermite moments (CHM). More information on these bases can be found in [31]. The MRT model based on central moments is sometimes referred to as *cascaded* model [22,23]. In the present context, the choice of second-order moments is slightly modified so that the bulk viscosity can be freely adjusted only changing one diagonal value of \mathbf{S} . The moments matrices read

$$\mathbf{M}^{\text{RM}} = \begin{pmatrix} 1 & \dots & 1 \\ e_{0,x} & \dots & e_{8,x} \\ e_{0,y} & \dots & e_{8,y} \\ e_{0,x}^2 - e_{0,y}^2 & \dots & e_{8,x}^2 - e_{8,y}^2 \\ e_{0,x}e_{0,y} & \dots & e_{8,x}e_{8,y} \\ e_{0,x}^2 + e_{0,y}^2 & \dots & e_{8,x}^2 + e_{8,y}^2 \\ e_{0,x}^2 e_{0,y} & \dots & e_{8,x}^2 e_{8,y} \\ e_{0,x}e_{0,y}^2 & \dots & e_{8,x}e_{8,y}^2 \\ e_{0,x}^2 e_{0,y}^2 & \dots & e_{8,x}^2 e_{8,y}^2 \end{pmatrix}, \quad \mathbf{M}^{\text{CM}} = \begin{pmatrix} 1 & \dots & 1 \\ c_{0,x} & \dots & c_{8,x} \\ c_{0,y} & \dots & c_{8,y} \\ c_{0,x}^2 - c_{0,y}^2 & \dots & c_{8,x}^2 - c_{8,y}^2 \\ c_{0,x}c_{0,y} & \dots & c_{8,x}c_{8,y} \\ c_{0,x}^2 + c_{0,y}^2 & \dots & c_{8,x}^2 + c_{8,y}^2 \\ c_{0,x}^2 c_{0,y} & \dots & c_{8,x}^2 c_{8,y} \\ c_{0,x}c_{0,y}^2 & \dots & c_{8,x}c_{8,y}^2 \\ c_{0,x}^2 c_{0,y}^2 & \dots & c_{8,x}^2 c_{8,y}^2 \end{pmatrix}, \quad (129)$$

$$\mathbf{M}^{\text{HM}} = \begin{pmatrix} 1 & \dots & 1 \\ e_{0,x} & \dots & e_{8,x} \\ e_{0,y} & \dots & e_{8,y} \\ \mathcal{H}_{0,xx}^{(2)} - \mathcal{H}_{0,yy}^{(2)} & \dots & \mathcal{H}_{8,xx}^{(2)} - \mathcal{H}_{8,yy}^{(2)} \\ \mathcal{H}_{0,xy}^{(2)} & \dots & \mathcal{H}_{8,xy}^{(2)} \\ \mathcal{H}_{0,xx}^{(2)} + \mathcal{H}_{0,yy}^{(2)} & \dots & \mathcal{H}_{8,xx}^{(2)} + \mathcal{H}_{8,yy}^{(2)} \\ \mathcal{H}_{0,xx}^{(3)} & \dots & \mathcal{H}_{8,xx}^{(3)} \\ \mathcal{H}_{0,xy}^{(3)} & \dots & \mathcal{H}_{8,xy}^{(3)} \\ \mathcal{H}_{0,xy}^{(4)} & \dots & \mathcal{H}_{8,xy}^{(4)} \end{pmatrix}, \quad \mathbf{M}^{\text{CHM}} = \begin{pmatrix} 1 & \dots & 1 \\ c_{0,x} & \dots & c_{8,x} \\ c_{0,y} & \dots & c_{8,y} \\ \mathcal{H}_{0,xx}^{*(2)} - \mathcal{H}_{0,yy}^{*(2)} & \dots & \mathcal{H}_{8,xx}^{*(2)} - \mathcal{H}_{8,yy}^{*(2)} \\ \mathcal{H}_{0,xy}^{*(2)} & \dots & \mathcal{H}_{8,xy}^{*(2)} \\ \mathcal{H}_{0,xx}^{*(2)} + \mathcal{H}_{0,yy}^{*(2)} & \dots & \mathcal{H}_{8,xx}^{*(2)} + \mathcal{H}_{8,yy}^{*(2)} \\ \mathcal{H}_{0,xx}^{*(3)} & \dots & \mathcal{H}_{8,xx}^{*(3)} \\ \mathcal{H}_{0,xy}^{*(3)} & \dots & \mathcal{H}_{8,xy}^{*(3)} \\ \mathcal{H}_{0,xy}^{*(4)} & \dots & \mathcal{H}_{8,xy}^{*(4)} \end{pmatrix}, \quad (130)$$

where $c_{i,\alpha} = e_{i,\alpha} - u_\alpha$ and $\mathcal{H}_i^{*(n)}$ are central Hermite polynomials built using $c_{i,\alpha}$ instead of $e_{i,\alpha}$. A fundamental property of \mathbf{C} is that it preserves collision invariants which are the mass density ρ and the momentum ρu_x and ρu_y . As a consequence, the sub-space spanned by $(1, 1, 1, 1, 1, 1, 1, 1, 1)^T$, \mathbf{e}_x and \mathbf{e}_y forms an eigenspace of the collision matrix. Its corresponding

eigenvalues have no influence on the collision and can be arbitrarily set to 1, so that $\mathbf{S} = \text{diag}(1, 1, 1, s_4, s_5, s_6, s_7, s_8, s_9)$. With these definitions, the dimensionless kinematic viscosity ν and bulk viscosity ν_b are related to s_4, s_5 and s_6 as:

$$s_4 = s_5 = \frac{\Delta t}{\tau + \Delta t/2}, \quad s_6 = \frac{\Delta t}{\tau_b + \Delta t/2}, \quad \nu = k^* \frac{\tau}{\Delta t} c_s^2, \quad \nu_b = k^* \frac{\tau_b}{\Delta t} c_s^2. \quad (131)$$

Even though several relaxation times appear, a Taylor expansion in Knudsen number is still possible, provided that Kn is based on the relaxation time τ related to the shear viscosity ν . Such a work is performed below for a fixed ratio $\tau_b/\tau = \nu_b/\nu$ and for fixed additional relaxation rates s_7, s_8 and s_9 . Regarding the latter, they are related to the dissipation properties of non-hydrodynamic modes which might have a strong impact on stability. One can re-write these relaxation rates as

$$s_i = \frac{\Delta t}{\tau_i + \Delta t/2}, \quad i \in \{7, 8, 9\}, \quad (132)$$

where τ_i is the relaxation time associated to a non-hydrodynamic moment. Here, the condition $s_i < 2$ clearly appears for ensuring a positive relaxation time τ_i . This is why the relaxation rates s_i are usually prescribed between 0 and 2 [13]. However, in the present work, no hypothesis will be assumed on these coefficients, so as to obtain the most general possible conclusions regarding their impact on hydrodynamic modes.

7.2. General Taylor expansion of MRT models

A Taylor expansion of the general expression of MRT models given by Eq. (127) yields

$$D_i g_i = -\frac{1}{\text{Kn}} \frac{\tau}{\Delta t} \mathbf{C}_{ij} (g_j - f_j^{eq}) - \frac{\text{Kn}}{2} \frac{\Delta t}{\tau} D_i^2 g_i - \frac{\text{Kn}^2}{6} \left(\frac{\Delta t}{\tau} \right)^2 D_i^3 g_i - \frac{\text{Kn}^3}{24} \left(\frac{\Delta t}{\tau} \right)^3 D_i^4 g_i + O(\text{Kn}^4). \quad (133)$$

The following change of variable is then performed:

$$-\frac{1}{\text{Kn}} \frac{\Delta t}{\tau} \mathbf{C}_{ij} (g_j - f_j^{eq}) = -\frac{1}{\text{Kn}} (f_i - f_i^{eq}), \quad (134)$$

which leads to

$$g_i = f_i + \mathbf{A}_{ij} (f_j - f_j^{eq}), \quad \mathbf{A} = \frac{\Delta t}{\tau} \mathbf{C}^{-1} - \mathbf{I}, \quad (135)$$

where \mathbf{I} is the Identity matrix. Since ρ and ρu_α are collision invariants, the equalities $\sum_i g_i = \sum_i f_i = \rho$ and $\sum_i e_{i,\alpha} g_i = \sum_i e_{i,\alpha} f_i = \rho u_\alpha$ are ensured, so that the variable change is admissible. Injecting it in Eq. (133) yields

$$D_i f_i = -\frac{1}{\text{Kn}} (f_i - f_i^{eq}) - \frac{\text{Kn}}{2} \frac{\Delta t}{\tau} D_i^2 f_i - \frac{\text{Kn}^2}{6} \left(\frac{\Delta t}{\tau} \right)^2 D_i^3 f_i - \frac{\text{Kn}^3}{24} \left(\frac{\Delta t}{\tau} \right)^3 D_i^4 f_i \\ - \mathbf{A}_{ij} D_i f_j^{(1)} - \frac{\text{Kn}}{2} \frac{\Delta t}{\tau} \mathbf{A}_{ij} D_i^2 f_j^{(1)} - \frac{\text{Kn}^2}{6} \left(\frac{\Delta t}{\tau} \right)^2 \mathbf{A}_{ij} D_i^3 f_j^{(1)} - \frac{\text{Kn}^3}{24} \left(\frac{\Delta t}{\tau} \right)^3 \mathbf{A}_{ij} D_i^4 f_j^{(1)} + O(\text{Kn}^4), \quad (136)$$

with $f_j^{(1)} = f_j - f_j^{eq}$. Note that the choice is made here to compare the MRT-LB scheme with the BGK-DVBE. The deviations should not be interpreted as numerical errors only, since the MRT-LB scheme is not supposed to converge towards the BGK-DVBE, but to its *a priori* unknown MRT counterpart. In particular, some deviations between the two equations are physically expected, such as a change of bulk viscosity enabled by s_6 .

To obtain a general equation in the same form as that of the BGK collision model (50) or the regularized ones (78), one then needs to express the derivatives of $f_j^{(1)}$ as derivatives of f_i only. To this extent, Eq. (136) can be re-written as

$$f_j^{(1)} = -\text{Kn} \left(D_j f_j + \mathbf{A}_{jk} D_j f_k^{(1)} \right) - \frac{\text{Kn}^2}{2} \frac{\Delta t}{\tau} \left(D_j^2 f_j + \mathbf{A}_{jk} D_j^2 f_k^{(1)} \right) - \frac{\text{Kn}^3}{6} \left(\frac{\Delta t}{\tau} \right)^2 \left(D_j^3 f_j + \mathbf{A}_{jk} D_j^3 f_k^{(1)} \right) + O(\text{Kn}^4). \quad (137)$$

After successive derivations of this equation with respect to D_i , injecting these expressions into Eq. (136) leads to

$$D_i f_i = -\frac{1}{\text{Kn}} (f_i - f_i^{eq}) + \text{Kn} \left[\mathbf{A}_{ij} D_i D_j f_j - \frac{\Delta t}{2\tau} D_i^2 f_i \right] \\ + \text{Kn}^2 \left[-\mathbf{A}_{ij} \mathbf{A}_{jk} D_i D_j D_k f_k + \frac{\Delta t}{2\tau} \mathbf{A}_{ij} \left(D_i D_j^2 f_j + D_i^2 D_j f_j \right) - \frac{1}{6} \left(\frac{\Delta t}{\tau} \right)^2 D_i^3 f_i \right] \\ + \text{Kn}^3 \left[\mathbf{A}_{ij} \mathbf{A}_{jk} \mathbf{A}_{kl} D_i D_j D_k D_l f_l - \frac{\Delta t}{2\tau} \mathbf{A}_{ij} \mathbf{A}_{jk} \left(D_i D_j D_k^2 f_k + D_i D_j^2 D_k f_k + D_i^2 D_j D_k f_k \right) + \frac{1}{4} \left(\frac{\Delta t}{\tau} \right)^2 \mathbf{A}_{ij} D_i^2 D_j^2 f_j \right]$$

$$+ \frac{1}{6} \left(\frac{\Delta t}{\tau} \right)^2 \mathbf{A}_{ij} \left(D_i D_j^3 f_j + D_i^3 D_j f_j \right) - \frac{1}{24} \left(\frac{\Delta t}{\tau} \right)^3 D_i^4 f_i \Big] + O(\text{Kn}^4). \quad (138)$$

Looking at this equation, several observations can be drawn:

- In the case of the BGK collision, the matrix \mathbf{A} is reduced to $\mathbf{A} = \Delta t/(2\tau)\mathbf{I}$. Replacing this expression into Eq. (138) allows recovering the general Taylor expansion of the BGK model of Eq. (50).
- Like regularized models, a first-order error in Kn appear. Its impact on the macroscopic equations in terms of potential numerical viscosity will be investigated.
- Similarly, a first-order error in time arises like with regularized models. This is in agreement with a previous demonstration of the first-order accuracy of the PR model based on a MRT formalism [32].
- A degeneracy of the numerical hyperviscosity is exhibited by the presence of $(\Delta t/\tau)^3$ -related terms in the third order in Kn. Noticing that the matrix \mathbf{A} involves $(\Delta t/\tau)$ itself, the pre-factor of this term cannot be estimated in a general way. Analyses adapted to each MRT model are performed in the next section to interpret the effects of the degeneracy.

Starting from Eq. (138), the same procedure as with the BGK and regularized models can be followed to obtain the deviation terms $E_i^{(n)}$, which are function of space gradients only. Then, deviation terms with the isothermal NS equations $E_\Phi^{(n)}$ can be obtained following Appendix A. Here again, the computer algebra system Maxima [68] is used to simplify the equations.

7.3. Error terms in the linear approximation

In this section, deviation terms with the isothermal NS equations are provided for each MRT model of interest, in the linear approximation. Contrary to Eqs. (23)-(24), an adjustable bulk viscosity has to be considered here. The adopted formalism for the macroscopic equations is then

$$\partial_t \rho + \partial_\alpha (\rho u_\alpha) = \text{Kn} E_\rho^{(1)} + \text{Kn}^2 E_\rho^{(2)} + \text{Kn}^3 E_\rho^{(3)} + O(\text{Kn}^4), \quad (139)$$

$$\begin{aligned} \partial_t (\rho u_\alpha) + \partial_\beta (\rho u_\alpha u_\beta) + c_s^2 \partial_\alpha \rho = \text{Kn} \rho c_s^2 \partial_\beta \left(S_{\alpha\beta} + \left(\frac{\tau_b}{\tau} - \frac{2}{D} \right) \partial_\gamma u_\gamma \delta_{\alpha\beta} \right) + \text{Kn} E_{\rho u_\alpha}^{(1)} + \text{Kn}^2 E_{\rho u_\alpha}^{(2)} \\ + \text{Kn}^3 E_{\rho u_\alpha}^{(3)} + O(\text{Kn}^4). \end{aligned} \quad (140)$$

Because of the large size of the error terms involved in the MRT models (due to the large numbers of free parameters), only two informations will be provided below:

1. the first-order deviation terms $E_\rho^{(1)}$ and $E_{\rho u_\alpha}^{(1)}$ (Navier-Stokes level), including consistency errors and possible numerical errors, in every direction,
2. the degenerating hyperviscosity, *i.e.* $(\Delta t/\tau)^3$ -related terms in $E_\rho^{(3)}$ and $E_{\rho u_\alpha}^{(3)}$, considering the x -direction only.

7.3.1. First-order deviations in Kn (NS-level)

Let us first focus on the deviation terms affecting the mass and momentum equations at the NS level, *i.e.* at first-order in Knudsen number.

In common with all the models investigated up to now, there is no deviation from the mass equation at the NS level with MRT models: $E_\rho^{(1)} = 0$. Furthermore, the momentum equations are affected in the same way (still at the NS level), whatever the MRT model tested in the present work (RM, CM, HM, CHM). For a second-order equilibrium ($N = 2$), their first-order deviations read:

$$\begin{aligned} E_{\rho u_x}^{(1)} &= - \left(\frac{\kappa + 1}{2} \right) \partial_{xx}^2 a_{eq,xxx}^{(3)} - \left(\frac{\kappa - 1}{2} \right) \partial_{xx}^2 a_{eq,xyy}^{(3)} - \left(\frac{\kappa + 3}{2} \right) \partial_{xy}^2 a_{eq,xyy}^{(3)} - \left(\frac{\kappa - 1}{2} \right) \partial_{xy}^2 a_{eq,yyy}^{(3)} - \partial_{yy}^2 a_{eq,xyy}^{(3)}, \\ E_{\rho u_y}^{(1)} &= - \partial_{xx}^2 a_{eq,xyy}^{(3)} - \left(\frac{\kappa - 1}{2} \right) \partial_{xy}^2 a_{eq,xxx}^{(3)} - \left(\frac{\kappa + 3}{2} \right) \partial_{xy}^2 a_{eq,xyy}^{(3)} - \left(\frac{\kappa - 1}{2} \right) \partial_{yy}^2 a_{eq,xyy}^{(3)} - \left(\frac{\kappa + 1}{2} \right) \partial_{yy}^2 a_{eq,yyy}^{(3)}, \end{aligned} \quad (141)$$

where $\kappa = \tau_b/\tau$. This results in a consistency error only, which is due to the truncation of the equilibrium distribution function to the second-order. Like the PR and the RR model, there is no numerical viscosity even if the scheme is first-order accurate.

When the equilibrium distribution is enriched with third- and/or fourth-order terms ($N = 3^*$ or $N = 4^*$), they read

$$E_{\rho u_x}^{(1)} = - \left(\frac{\kappa + 1}{2} \right) \partial_{xx}^2 a_{eq,xxx}^{(3)} - \left(\frac{\kappa - 1}{2} \right) \partial_{xy}^2 a_{eq,yyy}^{(3)}, \quad E_{\rho u_y}^{(1)} = - \left(\frac{\kappa + 1}{2} \right) \partial_{yy}^2 a_{eq,yyy}^{(3)} - \left(\frac{\kappa - 1}{2} \right) \partial_{xy}^2 a_{eq,xxx}^{(3)}. \quad (142)$$

All the error terms related to $a_{eq,xy}^{(3)}$ and $a_{eq,xy}^{(3)}$ have been cancelled thanks to the improved equilibrium.

The fact that the deviations at the NS level (first-order in Kn) remain unaffected by the moment basis has a strong importance, especially for the CM and CHM based MRT models. This means that, contrary to a common intuition, performing the collision step in the local basis of central moments does not lead to a correction of the Galilean invariance error at the NS level. This observation is in line with previous studies of the linearized DVBE with multiple relaxation times [42]. However, higher orders in Kn are affected by the choice of the basis and may have a strong impact on stability, as shown below.

7.3.2. Degenerating hyperviscosity considering the x -direction only

For all the aforementioned MRT models, when only the x -direction is considered, there is no hyperviscous degeneracy on the mass equation nor on the x -momentum equation. However, the y -momentum equation is affected in different ways, depending on the equilibrium order or the moment basis. For $N = 2$, the deviations read:

$$\text{RM, HM: } E_{\rho u_y}^{(3)} \sim - \left(\frac{\Delta t}{\tau} \right)^3 \frac{s_7 - 2}{36s_7} \left((3u_x^2 + 1)u_y \frac{\partial^4 \rho}{\partial x^4} + 6\rho u_x u_y \frac{\partial^4 u_x}{\partial x^4} + 3\rho u_x^2 \frac{\partial^4 u_y}{\partial x^4} \right). \quad (143)$$

$$\text{CM, CHM: } E_{\rho u_y}^{(3)} \sim - \left(\frac{\Delta t}{\tau} \right)^3 \frac{s_7 - 2}{24s_7} \left(9(u_x^4 + u_x^2)u_y \frac{\partial^4 \rho}{\partial x^4} + (30u_x^3 + 2u_x)\rho u_y \frac{\partial^4 u_x}{\partial x^4} + 6\rho u_x^4 \frac{\partial^4 u_y}{\partial x^4} \right). \quad (144)$$

For $N = 3^*$ or $N = 4^*$, they read

$$\text{RM, HM: } E_{\rho u_y}^{(3)} \sim \left(\frac{\Delta t}{\tau} \right)^3 \frac{s_7 - 2}{72s_7} \left((9u_x^4 + 9u_x^2 - 2)u_y \frac{\partial^4 \rho}{\partial x^4} + (36u_x^3 - 6u_x)\rho u_y \frac{\partial^4 u_x}{\partial x^4} + (9u_x^4 - 6u_x^2)\rho \frac{\partial^4 u_y}{\partial x^4} \right), \quad (145)$$

$$\text{CM, CHM: } E_{\rho u_y}^{(3)} \sim \left(\frac{\Delta t}{\tau} \right)^3 \frac{s_7 - 2}{8s_7} \rho u_x^4 \frac{\partial^4 u_y}{\partial x^4}. \quad (146)$$

As can be seen, this hyperviscous term is similar for the RM- and HM-MRT models, as well as for the CM- and CHM-MRT ones. Also note that when $s_7 = 1$, the error terms of the projected regularization (PR) are recovered with the HM-MRT (and *a fortiori* the RM-MRT) model. Similarly, the hyperviscosity of the CM and CHM based models are reduced to that of the RR model with $N_r = 3^*, 4^*$ and $N = 3^*, 4^*$, when $s_7 = 1$, as prospected by Coreixas et al. [31].

The effect of this hyperviscosity on the stability of hydrodynamic modes is investigated in the next section.

7.4. Hyperviscous degeneracy of MRT models

Looking at the form of the degenerating error in hyperviscosity allows drawing general conclusions for all the MRT models of interest. When only the x -direction is considered:

- the degenerating hyperviscosity does not involve the bulk viscosity, but only the relaxation rate s_7 ,
- when $s_7 = 2$, the degeneracy is cancelled.

These conclusions can even be generalized in every direction, expanding them to the three relaxation rates related to non-hydrodynamic variables: s_7 , s_8 and s_9 . The particular case $s_7 = s_8 = s_9 = 2$ will be further discussed in Sec. 7.6.

Exactly like PR and RR models, the hyperviscous degeneracy only affects the dissipation of the shear wave when the x -direction is considered together with a horizontal mean flow ($u_y = 0$). A summary of their analytical expression is compiled in Table 5. Let us recall here that a positive hyperviscosity yields a negative dissipation, which can lead to an instability. To this regards, the drastic effects of a simple change of equilibrium distribution function on the linear stability are exhibited. In any case, a change of the dissipation properties is expected at the critical value $s_7 = 2$.

It might be surprising to observe a stabilizing property for several models when $s_7 > 2$, which yields a negative relaxation time τ_7 (cf. Eq. (132)), and is out of the common stability bounds found in the literature [13]. Yet, one should keep in mind that the results exhibited in the present work regard the dissipation properties of the hydrodynamic modes only. They are not sufficient to conclude on the linear stability of a scheme because of two limitations of the methodology: 1) it cannot predict the stability of non-hydrodynamic modes as discussed in Sec. 2.8, and 2) the behaviour of under-resolved phenomena may require higher-order expansions to be accurately captured. Thus, only the stabilizing or destabilizing effect of the hyperviscosity on hydrodynamic modes is studied in Table 5. Even though observing a destabilizing hyperviscosity is sufficient to conclude on an unstable scheme, the converse is not generally true.

Yet, when confronting the results of Table 5 with the fact that $s_7 > 2$ yields unstable non-hydrodynamic modes, a general conclusion can be drawn: among the studied MRT schemes, the CM- and CHM-MRT models with $N = 3^*, 4^*$ are the only ones likely to be stable in the low-viscosity regime, in which the degeneracy becomes predominant.

Table 5

Summary of the degenerating hyperviscous terms arising in $E_{\rho u_y}^{(3)}$ with the non corrected MRT models on the D2Q9 lattice, when only x derivatives are considered and with a horizontal mean flow assumption.

	$N = 2$	$N = 3^*, 4^*$
RM, HM	$-\left(\frac{s_7 - 2}{12s_7}\right)\rho u_x^2 \frac{\partial^4 u_y}{\partial x^4}$ (stabilizing when $s_7 > 2$)	$\left(\frac{s_7 - 2}{24s_7}\right)(3u_x^2 - 2)\rho u_x^2 \frac{\partial^4 u_y}{\partial x^4}$ (stabilizing when $s_7 > 2$ while $\text{Ma} < \sqrt{2}$)
CM, CHM	$-\left(\frac{s_7 - 2}{4s_7}\right)\rho u_x^4 \frac{\partial^4 u_y}{\partial x^4}$ (stabilizing when $s_7 > 2$)	$\left(\frac{s_7 - 2}{8s_7}\right)\rho u_x^4 \frac{\partial^4 u_y}{\partial x^4}$ (stabilizing when $s_7 < 2$)

7.5. Validation with linear analyses

The hyperviscous degeneracy exhibited in the above section is now confronted to the linear analyses of the real MRT LB schemes. To this purpose, the eigenvalue problem corresponding to the general MRT scheme is provided in Appendix C.

Fig. 13 displays the dissipation curves of the four MRT models with $N = 2$ and $N = 3^*$, in comparison with the analytical estimation of the degenerating hyperviscosity affecting x -aligned shear waves of Table 5. For instance, for the MRT-RM model with $N = 2$, this estimation reads

$$\omega_i \Delta t = -\left(\frac{s_7 - 2}{12s_7}\right)\rho u_x^2 (k_x \Delta x)^4. \quad (147)$$

In every case, waves travelling along the x -direction are investigated ($k_y = 0$) with a horizontal mean flow at Mach number $\text{Ma} = 0.5$, together with a dimensionless relaxation time $\tau/\Delta t = 10^{-5}$. The bulk relaxation time is set to $\tau_b = 2\tau$ to avoid the particular case of the BGK collision model $\tau_b = \tau$, and two parameters are evaluated for the relaxation rate of third- and fourth-order moments: $s_7 = s_8 = s_9 = 1.5$ and $s_7 = s_8 = s_9 = 2.5$. Note that the second case is above the bounds proposed by Lallemand & Luo ($0 < \tau_N < 2$) [13].

The numerical prediction of the behaviour of the three physical waves provided by the Taylor expansion is in very good agreement with the linear analyses. In particular, two waves, which are actually acoustic waves, seem unaffected by the choice of MRT model and compared to the BGK collision. This is in agreement with the estimation of the degenerating hyperviscosity in the x -direction, only affecting the shear wave. Regarding the latter, it is, exactly like the PR and RR models of Sec. 6, either over-dissipated or anti-dissipated, *i.e.* leading to linear instabilities. The results from Table 5 allow an accurate estimation of this behaviour, indicating that the degenerating hyperviscosity is responsible for these phenomena. Notably, the change of behaviour above the critical value $s_7 = 2$ is recovered for all models.

Looking at these linear analyses is also the opportunity to focus on the behaviour of non-hydrodynamic modes, which cannot be predicted by the Taylor expansions in Kn . Even if only two of them are visible in Fig. 13, six non-hydrodynamic modes are actually present. The four remaining modes are severely damped, so that they cannot be observed on the figure. Note that, with every MRT model except the RM formulation, one non-hydrodynamic mode is largely dissipated when $s_7 < 2$, and amplified for $s_7 > 2$. The latter is at the origin of a strong instability in the x -direction.

7.6. Cancelling the degeneracy with MRT models

Two particular cases, for which the degeneracy is cancelled, can be exhibited. Denoting here $s_N = s_7 = s_8 = s_9$ for a generalization in every direction:

1. In the case of the BGK collision model, one has

$$s_N = \frac{\Delta t}{\tau + \Delta t/2} \Rightarrow \frac{s_N - 2}{s_N} = -\frac{2\tau}{\Delta t}, \quad (148)$$

so that every $(\Delta t/\tau)^3$ -related terms are removed from the numerical hyperviscosity. A result of Sec. 3 is recovered: there is no hyperviscous degeneracy with the BGK collision model. This observation can even be extended to a BGK collision with adaptive bulk viscosity, since the degenerating hyperviscosity does not depend on $\kappa = \tau_b/\tau$.

2. With $s_N = 2$, the degenerating hyperviscosity is cancelled in any direction. Considering fixed relaxation parameters (independent of $\tau/\Delta t$), this is the only value that leads to such a property.

The second case is in line with several linear stability analyses of MRT models aiming at finding optimal sets of free parameters, which often result in some values close to the critical parameter $\tau_N = 2$ [13,19,74,75,64]. Using Eq. (132), this particular case is equivalent to $\tau_N = 0$, meaning that high-order moments are immediately imposed to their equilibrium value by the collision model, without relaxation.

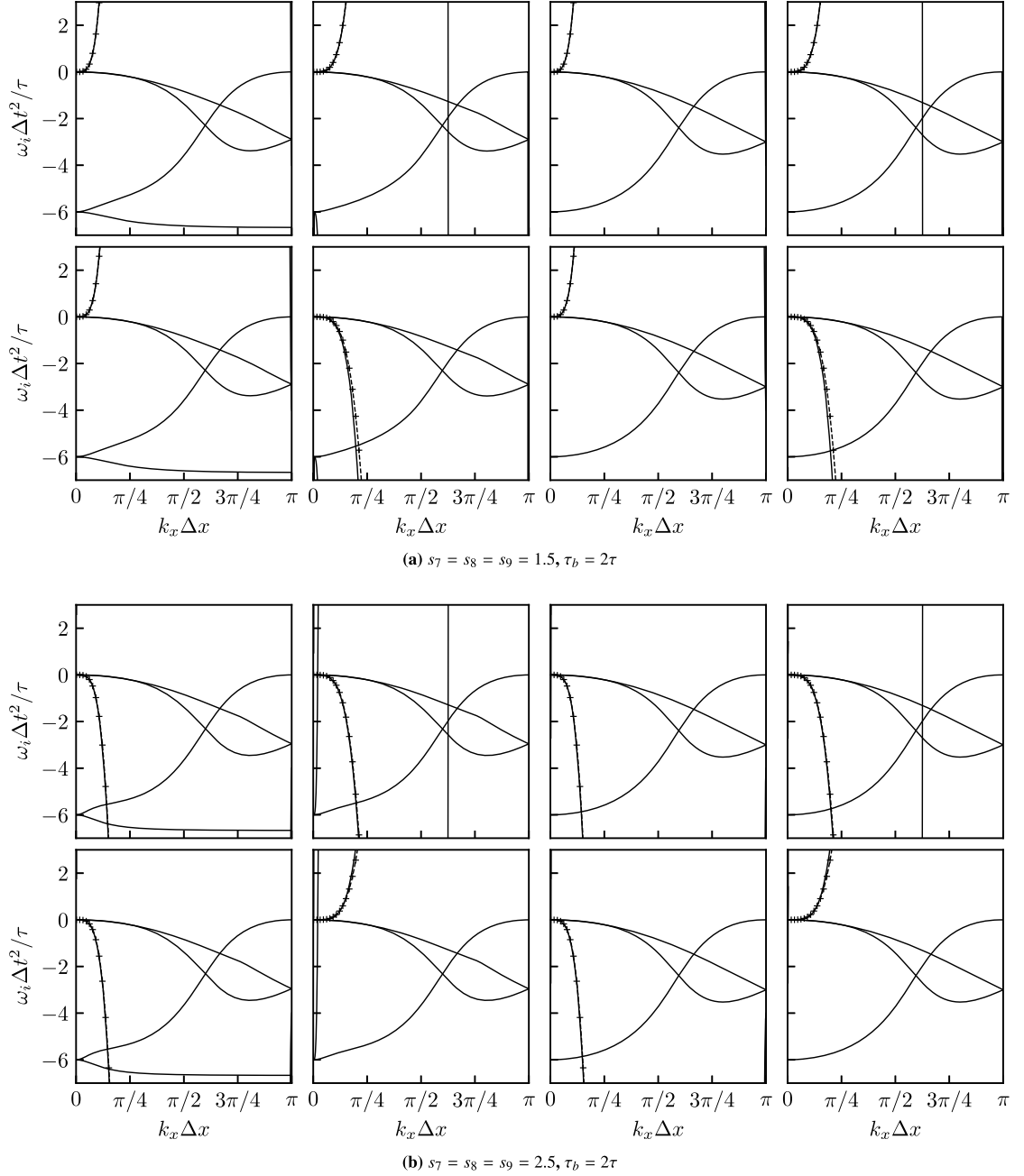


Fig. 13. Dissipation curves of the MRT models with the D2Q9 lattice considering horizontal plane waves ($k_y = 0$), a horizontal mean flow at $Ma = 0.5$ and $\tau/\Delta t = 10^{-5}$. Top: $N = 2$, bottom: $N = 3^*$ (similar results with $N = 4^*$). From left to right: MRT-RM, MRT-CM, MRT-HM and MRT-CHM. The linear analyses of the LB scheme (—) are compared to the estimated degenerating hyperviscosity of Table 5 (---).

Interestingly, imposing higher-order moments to their equilibrium value is precisely the purpose of the PR model (in the Hermite basis) and the RR one (in the central Hermite basis). This fact seems in disagreement with the above observation. To shed the light on this property, let us re-write the collision step affecting these moments as

$$\mathbf{m}^{(n),coll} = \mathbf{m}^{(n)} - s_N \left(\mathbf{m}^{(n)} - \mathbf{m}_{eq}^{(n)} \right) = \mathbf{m}_{eq}^{(n)} - (s_N - 1) \left(\mathbf{m}^{(n)} - \mathbf{m}_{eq}^{(n)} \right), \quad (149)$$

where $\mathbf{m}^{(n)}$ and $\mathbf{m}_{eq}^{(n)}$ are respectively moments and equilibrium moments of order $n \geq 3$, no matter the definition of moments (RM, CM, HM or CHM). With this notation, the regularization procedure is equivalent to setting $s_N = 1$. Hence, by denoting $\mathbf{m}_{neq}^{(n),coll} = \mathbf{m}^{(n),coll} - \mathbf{m}_{eq}^{(n)}$, two cases are noticeable:

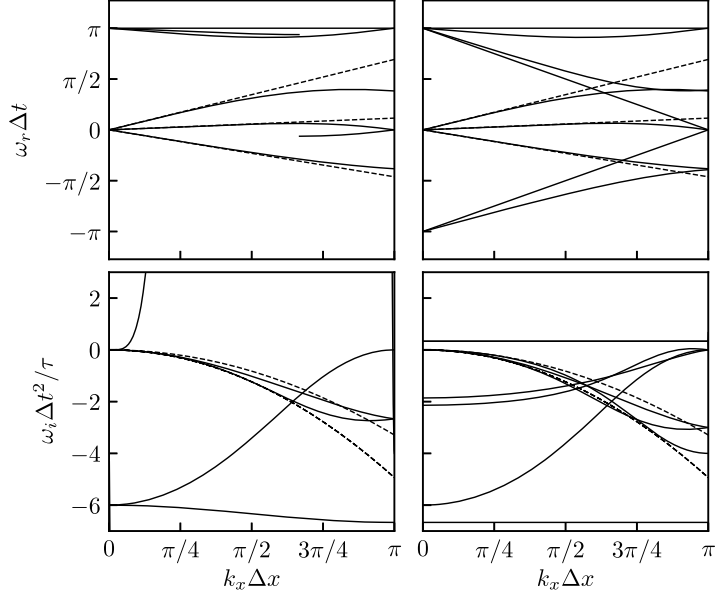


Fig. 14. Propagation (top) and dissipation (bottom) curves of the linear analyses performed on the non-corrected MRT-RM scheme with $N = 2$ (—) and the isothermal NS equations (---). A horizontal mean flow is considered at $\text{Ma} = 0.2$, with $\tau/\Delta t = 10^{-5}$ and $\tau_b/\tau = 2$. Left: $s_N = 1$, right: $s_N = 2$.

$$\text{MRT with } \tau_N = 0 \ (s_N = 2) : \quad \mathbf{m}_{neq}^{(n),coll} = -\mathbf{m}_{neq}^{(n)}, \quad (150)$$

$$\text{Regularization } (s_N = 1) : \quad \mathbf{m}_{neq}^{(n),coll} = 0. \quad (151)$$

The first case has the advantage of cancelling the degenerating hyperviscosity thanks to the particular value $s_N = 2$. However, this value enforces an over-relaxation of the corresponding moments resulting in a sign inversion of their off-equilibrium parts, as shown by Eq. (150). It is at the origin of spurious oscillations [3], also interpreted as an amplitude inversion of the non-hydrodynamic modes at each time step [80]. The second case (regularization) allows filtering out these non-hydrodynamic modes as shown in [32], which is done at the cost of the degeneracy.

These properties are confirmed by Fig. 14, displaying dispersion and dissipation curves of the MRT-RM model with $\tau_b/\tau = 2$ and the characteristic values $s_N = 1$ and $s_N = 2$. With $s_N = 1$, three modes are filtered out (six modes remain), which can clearly be visible on the dispersion curve. Unfortunately, a physical wave is amplified because of the hyperviscous degeneracy. The behaviour of the PR model is well recovered here. With $s_N = 2$ the degeneracy is cancelled, so that the expected dissipation of physical waves can be correctly recovered. However, the non-hydrodynamic modes are not filtered any more. A careful study of this model might lead to three kinds of stability issues caused by the particular value $s_N = 2$:

1. A non-hydrodynamic mode is surprisingly amplified whatever the considered wavenumber. The latter is related to the bulk viscosity and can only be attenuated by setting $\tau_b < \tau$.
2. Other non-hydrodynamic modes are slightly unstable, even in the x -direction, for large values of $k_x \Delta x$.
3. Due to the large number of non-hydrodynamic modes, eigenvalue collisions are likely to occur in every direction, so that this model is concerned by similar stability issues as the BGK one.

7.7. Note on the bulk viscosity and the trace of the shear stress tensor

The above remark on the values $s_N = 1$ (regularization) and $s_N = 2$ (no degeneracy) can equivalently be applied to the bulk viscosity regarding the relaxation rate s_6 . In the present section, the relationship between the bulk viscosity and the trace of $\mathbf{\Pi}^{neq} = \mathbf{\Pi} - \mathbf{\Pi}^{eq}$, which can be obtained thanks to a Chapman-Enskog expansion, is particularly considered. More precisely, the focus is put here on several collision models enforcing a traceless $\mathbf{\Pi}^{neq}$ in the aim of cancelling the bulk viscosity [95,46].

Without loss of generality, the MRT-RM model described in Sec. 7.1 is considered here. The collision affects the trace of $\mathbf{\Pi}^{neq}$ as

$$\text{Tr}(\mathbf{\Pi}^{neq,coll}) = -(s_6 - 1) \text{Tr}(\mathbf{\Pi}^{neq}). \quad (152)$$

With this formulation, imposing a traceless $\mathbf{\Pi}^{neq}$ tensor during the collision step is equivalent to setting $s_6 = 1$ in the MRT collision model. However, using Eq. (131), a null bulk viscosity can only be obtained with $s_6 = 2$. The particular value $s_6 = 1$ actually leads to

$$\tau_b = \frac{\Delta t}{2}, \quad (153)$$

so that τ_b/τ may be very large for low values of the dimensionless relaxation time. This non-desired bulk viscosity may be at the origin of an improved stability when enforcing a traceless $\mathbf{\Pi}^{neq}$, already noticed in the literature [95,46].

Like in the previous section, two cases are then noticeable:

$$\text{Traceless } \mathbf{\Pi}^{neq} (s_6 = 1) : \quad \text{Tr}(\mathbf{\Pi}^{neq, coll}) = 0, \quad (154)$$

$$\text{Zero bulk viscosity } (s_6 = 2) : \quad \text{Tr}(\mathbf{\Pi}^{neq, coll}) = -\text{Tr}(\mathbf{\Pi}^{neq}). \quad (155)$$

The first case can be viewed as a new regularization, imposing another moment to its equilibrium value, leading to the filtering of another non-hydrodynamic mode. However, this is done at the cost of an additional numerical bulk viscosity. The second case effectively cancels the bulk viscosity.

7.8. Particular case of the TRT model

Studying the linearized error terms of MRT models is the opportunity to investigate the properties of the two-relaxation-time (TRT) scheme, especially regarding the role of the so-called magic parameter Λ [20,96,21]. The purpose of the TRT collision model is to relax, with two different relaxation parameters λ^+ and λ^- , the symmetric and anti-symmetric parts of the distribution functions. Equivalently, it can be viewed as a MRT model relaxing even moments with the parameter λ^+ and odd ones with λ^- [3]. Without loss of generality, the MRT-RM formulation is adopted here with

$$s_4 = s_5 = s_6 = s_9 = \lambda^+ = \frac{\Delta t}{\tau + \Delta t/2}, \quad s_7 = s_8 = \lambda^- = \frac{\Delta t}{\tau^- + \Delta t/2}. \quad (156)$$

Note that with these definitions, the bulk viscosity cannot be tuned any more. The great interest of this model is that only one free parameter remains: λ^- , or equivalently τ^- . It is usually related to λ^+ as

$$\Lambda \equiv \lambda^+ \lambda^- = \left(\frac{\Delta t}{\tau + \Delta t/2} \right) \left(\frac{\Delta t}{\tau^- + \Delta t/2} \right) \Rightarrow \lambda^- = \frac{1}{\Lambda} \left(\frac{\tau}{\Delta t} + \frac{1}{2} \right), \quad (157)$$

where Λ is referred to as the magic parameter of the TRT model. For a fixed value Λ (independent of $\tau/\Delta t$), the relaxation rate of odd-moments behaves as $\lambda^- \sim \tau/\Delta t$. Given the form of the degenerating hyperviscosity exhibited with the MRT-RM model, especially the appearance of $(1/s_7)$ -related terms in the degenerating hyperviscosity of Table 5, the degeneracy is expected to be even more prominent with the TRT model with a fixed magic parameter.

When x -derivatives only are considered for the sake of simplicity, a computation of the linearized deviation terms of the TRT model yields, for a second-order equilibrium distribution function,

$$\begin{aligned} E_\rho^{(3)} &= O((\Delta t/\tau)^2), & E_{\rho u_x}^{(3)} &= O((\Delta t/\tau)^2), \\ E_{\rho u_y}^{(3)} &= -\left(\frac{\Delta t}{\tau}\right)^4 \frac{\Lambda(\Lambda - 1/4)}{9} \left((6u_x^2 + 2)u_y \frac{\partial^4 \rho}{\partial x^4} + 12\rho u_x u_y \frac{\partial^4 u_x}{\partial x^4} + 6\rho u_x^2 \frac{\partial^4 u_y}{\partial x^4} \right) + O((\Delta t/\tau)^2). \end{aligned} \quad (158)$$

Exactly like the MRT-RM model with fixed high-order relaxation parameters, no degeneracy is obtained on the mass and x -momentum equations. However, a $(\Delta t/\tau)^4$ -related term arises in the y -momentum equation which, as predicted, increases the degeneracy when the dimensionless relaxation time is small. Also note that no $(\Delta t/\tau)^3$ -term arises, which remains true in any direction. It is also noteworthy that this degeneracy is cancelled when $\Lambda = 1/4$, which is precisely the optimal parameter found by d'Humières and Ginzburg by derivation of steady recurrence equations [96]. However, this property is not true when considering all the possible directions.

In order to investigate the effects of this degeneracy, linear stability analyses of the TRT scheme are provided in Fig. 15. Dispersion and dissipation curves of two systems are displayed: (1) the TRT-LB scheme following Appendix C and (2) the isothermal NS-equations including deviation terms up to the third-order in Knudsen number. Two values of the magic parameter are considered: $\Lambda = 1$ and $\Lambda = 1/4$. These analyses are performed along the x -direction, with a horizontal mean flow at $\text{Ma} = 0.1$, a second-order equilibrium distribution function and with a dimensionless relaxation time $\tau/\Delta t = 10^{-3}$. For the sake of completeness, the complete form of the error terms in that case (x -aligned mean flow and x -derivatives only) is provided below:

$$\begin{aligned} E_\rho^{(1)} &= 0, & E_{\rho u_x}^{(1)} &= -\frac{\partial^2 a_{eq,xxx}^{(3)}}{\partial x^2}, & E_{\rho u_y}^{(1)} &= -\rho u_x^2 \frac{\partial^2 u_y}{\partial x^2}, \\ E_\rho^{(2)} &= -\left(\frac{\Delta t}{\tau}\right)^2 \frac{1}{36} \left(3u_x^3 \frac{\partial^3 \rho}{\partial x^3} + (9u_x^2 - 2)\rho \frac{\partial^3 \rho}{\partial x^3} \right), \end{aligned}$$

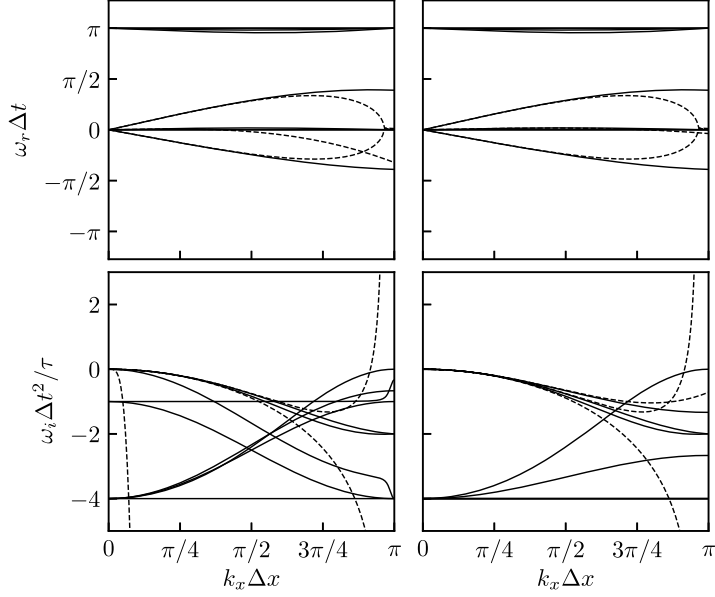


Fig. 15. Propagation (top) and dissipation (bottom) curves of the linear analyses performed on the TRT scheme with $N = 2$ (—) and the isothermal NS equations including deviation terms up to Kn^3 (---). A horizontal mean flow is considered at $\text{Ma} = 0.1$ with $\tau/\Delta t = 10^{-3}$. Left: $\Lambda = 1$, right: $\Lambda = 1/4$.

$$\begin{aligned}
E_{\rho u_x}^{(2)} &= -\frac{1}{9} \left((27u_x^4 + 9u_x^2 - 2) \frac{\partial^3 \rho}{\partial x^3} + (90u_x^3 - 18u_x) \rho \frac{\partial^3 u_x}{\partial x^3} \right) \\
&\quad + \left(\frac{\Delta t}{\tau} \right)^2 \frac{1}{54} \left((9u_x^4 + 9u_x^2 - 2) \frac{\partial^3 \rho}{\partial x^3} + (36u_x^3 - 6u_x) \rho \frac{\partial^3 u_x}{\partial x^3} \right), \\
E_{\rho u_y}^{(2)} &= -2u_x(u_x^2 - c_s^2) \frac{\partial^3 u_y}{\partial x^3} + \left(\frac{\Delta t}{\tau} \right)^2 \frac{1}{6} (u_x^3 - 4\Lambda u_x) \rho \frac{\partial^3 u_y}{\partial x^3}, \\
E_{\rho}^{(3)} &= -\left(\frac{\Delta t}{\tau} \right)^2 \frac{1}{108} \left((27u_x^4 + 9u_x^2 - 2) \frac{\partial^4 \rho}{\partial x^4} + (90u_x^3 - 18u_x) \frac{\partial^4 u_x}{\partial x^4} \right), \\
E_{\rho u_x}^{(3)} &= -\frac{1}{9} \left((108u_x^5 + 51u_x^3 - 12u_x) \frac{\partial^4 \rho}{\partial x^4} + (378u_x^4 - 81u_x^2 + 2) \rho \frac{\partial^4 u_x}{\partial x^4} \right) \\
&\quad + \left(\frac{\Delta t}{\tau} \right)^2 \frac{1}{108} \left((162u_x^5 + 129u_x^3 - 28u_x) \frac{\partial^4 \rho}{\partial x^4} + (612u_x^4 - 99u_x^2 - 2) \rho \frac{\partial^4 u_x}{\partial x^4} \right), \\
E_{\rho u_y}^{(3)} &= -\frac{1}{9} (45u_x^4 - 18u_x^2 + 1) \rho \frac{\partial^4 u_y}{\partial x^4} + \left(\frac{\Delta t}{\tau} \right)^2 \frac{1}{36} (27u_x^4 - 72\Lambda u_x^2 + (8\Lambda - 1)) \rho \frac{\partial^4 u_y}{\partial x^4} \\
&\quad - \left(\frac{\Delta t}{\tau} \right)^4 \frac{\Lambda(\Lambda - 1/4)}{3} 2\rho u_x^2 \frac{\partial^4 u_y}{\partial x^4}. \tag{159}
\end{aligned}$$

Surprisingly, and unlike all the other models investigated in the present work, the dissipation of the vorticity wave is not accurately predicted by the Taylor expansion when $\Lambda \neq 1/4$. More precisely, the degeneracy predicted by the Taylor expansion expects an over-dissipation of this wave, which is not noticed on the linear analysis. Such a discrepancy is also observed when all the directions are considered. Regarding the acoustic waves, they do not suffer from any large error in dissipation, which is in agreement with the Taylor expansion. It is also noticeable that, looking on the dispersion curves, only four non-hydrodynamic modes have $\omega_r \approx \pi$, and two other ones have a phase velocity close to 0. Let us recall here that, with the BGK collision model, all the non-hydrodynamic modes have a real pulsation shifted of π , which is attributed to an over-relaxation of non-hydrodynamic variables in Sec. 2.8. With the TRT model, the very large relaxation time applied to the two odd moments ($\tau^-/\Delta t$) leads to an under-relaxation of these quantities instead of an over-relaxation [3]. This is at the origin of the observed phenomena.

Given the discrepancies observed in the behaviour of the vorticity wave of Fig. 15, and in order to ensure that the Taylor expansions have been properly performed, convergence plots of the linearized error terms are proposed in Fig. 16. Exactly like for the validation of the deviation terms of the BGK collision model proposed in Sec. 3.6, this figure displays the behaviour of $\Delta\omega^*/k^*$ when the resolution of the wave increases, where $\Delta\omega^*$ is the difference in the eigenvalues of the TRT-

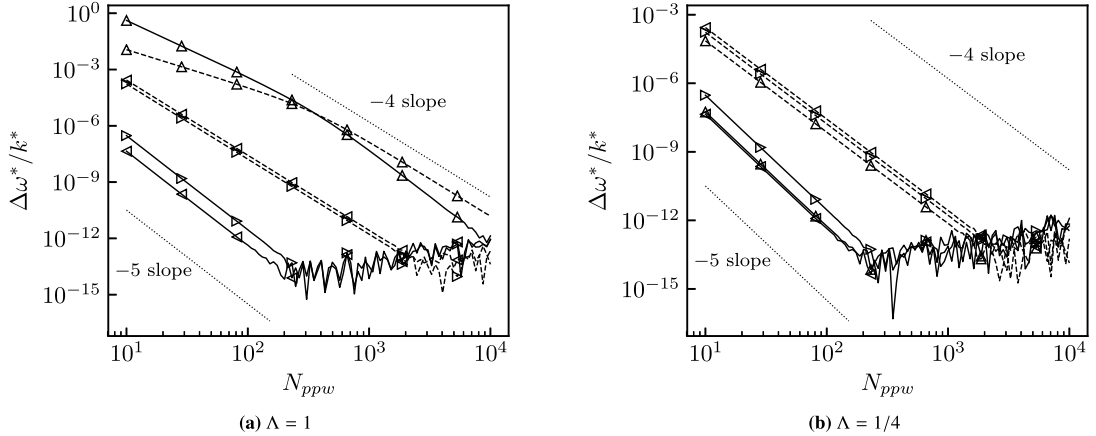


Fig. 16. Relative error between the eigenvalues of the TRT-LBM and that of the isothermal NS equations including deviation terms up to the fourth-order, with $Ma = 0.1$, $\tau/\Delta t = 10^{-3}$. Dispersion errors are plotted as: $-\triangleright-$ (downstream acoustic eigenvalue), $-\triangleleft-$ (upstream acoustic eigenvalue), $-\blacktriangle-$ (shear eigenvalue). Dissipation errors are plotted as: $\rightarrow\blacktriangleright$ (downstream acoustic eigenvalue), $\leftarrow\blacktriangleleft$ (upstream acoustic eigenvalue), \blacktriangle (shear eigenvalue).

LB scheme and that of the isothermal NS equations including the computed error terms. Displayed in log-scale, a -4 -slope in the asymptotic limit of the dispersion properties (real part of $\Delta\omega^*/k^*$), as well as a -5 -slope in the dissipation properties (imaginary part of $\Delta\omega^*/k^*$) theoretically validate the accuracy of the Taylor expansion in Kn . With $\Lambda = 1$ (Fig. 16a), such a behaviour is correctly recovered on the two acoustic waves travelling in the x -direction, up to the machine precision. However, regarding the vorticity, such an agreement is only obtained for very well resolved waves, with $N_{ppw} > 200$. With a lower resolution, a -3 -slope (resp. a -2 -slope) is observed in the dissipation (resp. dispersion) properties. This indicates that, even though the deviation terms obtained by the Taylor expansion are theoretically validated as suggested by the asymptotic behaviour of the remaining error, they cannot accurately predict the numerical properties of waves discretized with less than 200 points. This observation is in agreement with the incorrect prediction provided by the Taylor expansion in Fig. 15. The only explanation for such a behaviour is that high-order Kn deviation terms, that have been neglected in the present work, are subject to a degeneracy that compensates the dissipation error induced by the numerical hyperviscosity. This phenomenon, still not understood by the present authors, might be related to the fact that no $(\Delta t/\tau)^3$ -related term arises in the hyperviscosity error. A better understanding of this surprising property may be the purpose of future work.

Finally note that with $\Lambda = 1/4$ (Fig. 16b), a correct slope is obtained up to the machine precision for all the waves discretized with more than ten points. This is in line with the fact that the degeneracy is cancelled in the x -direction for this value of the magic parameter.

7.9. Summary of the numerical errors of MRT models

The Taylor expansion performed on several forms of MRT collision models provides important conclusions regarding their numerical errors. Every formulation investigated in the present work, depending on the choice of moments (RM, CM, HM, CHM), lead to a common result: for fixed values of the non-hydrodynamic relaxation parameters, the numerical hyperviscosity is subject to a degeneracy similar to that of regularized models. Changing the moment basis or the value of the relaxation parameter s_N would eventually affect the sign of the numerical hyperviscosity, switching from a stabilizing to a destabilizing effect. However, this effect cannot be predicted *a priori*, which prevents from finding any physical argument in favour of one model from another. In the present study, it is theoretically shown that the central moment formulation can yield a stabilizing hyperviscosity, while the raw and Hermite bases cannot.

The particular value $s_N = 2$, which is equivalent to a null relaxation time for high-order moments, allows cancelling the degeneracy for all models. However, unlike the regularization which comes down to setting $s_N = 1$, this does not filter out any non-hydrodynamic mode, so that the advantage compared to the BGK collision remains unclear. This is probably why these relaxation parameters are usually prescribed to a value between 1 and 2 in the literature, usually tuned by linear analyses or academic test cases [18,13,19,74,75,64].

The degenerating hyperviscosity is likely to be at the origin of the numerical errors exhibited by Dellar in the incompressible limit with a relaxation parameter $s_N = 1$ [79]. In this work, simulations of a Kelvin-Helmholtz instability were performed for decreasing Mach numbers with a constant Reynolds number and spatial resolution. This is equivalent to decreasing the dimensionless relaxation time $\tau/\Delta t$ which, according to the Taylor expansions, lead to an increasing numerical error compared to the BGK collision model.

Finally, an investigation of the TRT model exhibits an interesting feature of its numerical errors. Even though, for a fixed magic parameter Λ , the degeneracy is still present and even amplified, it does not lead to any strong error in dissipation compared to BGK and MRT models with fixed relaxation parameters. Furthermore, the under-relaxation of odd moments may reduce spurious oscillations which can lead to an increased stability.

8. Conclusion

In this paper, a thorough asymptotic analysis is proposed to derive the hydrodynamic limits of some isothermal LB schemes in the discrete setting. Since such a Taylor expansion in Knudsen number is not mathematically rigorous because of the presence of discontinuous NH modes, it is then systematically validated by linear analyses. In a sense, the mathematical developments performed in this work are quite close to other Taylor expansions of the literature, such as the work of Holdych et al. [52], Dubois [53] or more recently Fucik and Straka [57]. In these articles, the Taylor expansion is performed assuming that it does not affect the collision step, which comes down to keeping a constant value of $\Delta t/\tau$. Given the two independent dimensionless numbers defined in Sec. 2, namely Kn and $\Delta t/\tau$, these expansions can be interpreted in terms of Knudsen number as well. In this regard, one purpose of the present work is to restore, in a discrete setting, the recovery of macroscopic equations as hydrodynamic limits of the LBM, instead of a consistency limit as it is commonly assumed in the LBM community [48].

An interest of the present methodology is to discriminate consistency errors, inherited from the kinetic modelling of the DVBE, and numerical errors attributed to the time and space discretization. Applied to different collision models and confronted to linear analyses, it leads to the following conclusions:

- The low dissipation of the BGK collision model is explained by the appearance of the Bernoulli numbers in the Taylor expansion (*cf.* Sec. 3).
- Both regularized and MRT models with fixed relaxations suffer from a degenerating hyperviscosity, which consists in a resurgence of high-Kn phenomena induced by a large numerical pre-factor. This phenomenon is at the origin of an over-dissipation and instability of hydrodynamic modes, even in well-resolved conditions.
- The shear stress reconstruction of the HRR model induces a numerical viscosity which can be addressed by introducing the physical correction Ψ_i . In the latter case, the hyperviscosity is stabilizing for $Ma < 1$ and $CFL < 1$. The finite-difference scheme adopted in the computation of space gradients can affect these limits.
- The correction term of Feng et al. [62] can efficiently restore a correct dissipation at the Navier-Stokes level, whatever the way it is discretized.
- With the TRT collision model, even though a degeneracy is theoretically present, it surprisingly does not considerably affect the dissipation properties.

More generally, an important result of the moment cascade in the discrete setting is to translate consistency errors to numerical ones, by introducing $(\Delta t/\tau)$ pre-factors. This observation may be at the origin of a better numerical behaviour when the consistency of the scheme is improved [46].

Even if the analysis has been performed in an isothermal context, several conclusions seem to be directly transposed to a compressible framework. Especially, the $Ma < 1$ and $CFL < 1$ conditions of the HRR model are in line with recent linear stability analyses of hybrid LBM [89]. Further investigations of the hydrodynamic limits and numerical errors of compressible LBM may be the purpose of future work. Furthermore, to complete the analysis, a particular attention may be paid to the behaviour of non-hydrodynamic modes which have been neglected in the present work. Last but not least, error terms being explicitly known at each Knudsen order, a benefit of the present work is to pave the way for possible numerical corrections.

CRedit authorship contribution statement

Gauthier Wissocq: Conceptualization, Methodology, Software, Validation, Writing – original draft. **Pierre Sagaut:** Supervision, Writing – review & editing.

Declaration of competing interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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Appendix A. Macroscopic equations

Let us start with the following DVBE with deviation terms,

$$\partial_t f_i + e_{i,\alpha} \partial_\alpha f_i = -\frac{1}{Kn} (f_i - f_i^{eq} - Kn \Psi_i) + \sum_{n \geq 1} Kn^n E_i^{(n)}, \quad (\text{A.1})$$

where it is supposed that every deviation term $E_i^{(n)}$ is explicitly expressed as space-gradients of macroscopic quantities ρ and u_α . Taking the first five moments of this equation yields

$$\partial_t \rho + \partial_\alpha (\rho u_\alpha) = \sum_i \Psi_i + \text{Kn} \sum_i E_i^{(1)} + \text{Kn}^2 \sum_i E_i^{(2)} + \text{Kn}^3 \sum_i E_i^{(3)} + O(\text{Kn}^4), \quad (\text{A.2})$$

$$\partial_t (\rho u_\alpha) + \partial_\beta \Pi_{\alpha\beta} = \sum_i e_{i,\alpha} \Psi_i + \text{Kn} \sum_i e_{i,\alpha} E_i^{(1)} + \text{Kn}^2 \sum_i e_{i,\alpha} E_i^{(2)} + \text{Kn}^3 \sum_i e_{i,\alpha} E_i^{(3)} + O(\text{Kn}^4), \quad (\text{A.3})$$

$$\partial_t \Pi_{\alpha\beta} + \partial_\gamma Q_{\alpha\beta\gamma} = -\frac{1}{\text{Kn}} \left(\Pi_{\alpha\beta} - \Pi_{\alpha\beta}^{\text{eq}} \right) + \sum_i e_{i,\alpha} e_{i,\beta} \Psi_i + \text{Kn} \sum_i e_{i,\alpha} e_{i,\beta} E_i^{(1)} + \text{Kn}^2 \sum_i e_{i,\alpha} e_{i,\beta} E_i^{(2)} + O(\text{Kn}^3), \quad (\text{A.4})$$

$$\partial_t Q_{\alpha\beta\gamma} + \partial_\delta R_{\alpha\beta\gamma\delta} = -\frac{1}{\text{Kn}} \left(Q_{\alpha\beta\gamma} - Q_{\alpha\beta\gamma}^{\text{eq}} \right) + \sum_i e_{i,\alpha} e_{i,\beta} e_{i,\gamma} \Psi_i + \text{Kn} \sum_i e_{i,\alpha} e_{i,\beta} e_{i,\gamma} E_i^{(1)} + O(\text{Kn}^2), \quad (\text{A.5})$$

$$\partial_t R_{\alpha\beta\gamma\delta} + \partial_\epsilon S_{\alpha\beta\gamma\delta\epsilon} = -\frac{1}{\text{Kn}} \left(R_{\alpha\beta\gamma\delta} - R_{\alpha\beta\gamma\delta}^{\text{eq}} \right) + \sum_i e_{i,\alpha} e_{i,\beta} e_{i,\gamma} e_{i,\delta} \Psi_i + O(\text{Kn}), \quad (\text{A.6})$$

where

$$\begin{aligned} \Pi_{\alpha\beta} &= \sum_i e_{i,\alpha} e_{i,\beta} f_i, & Q_{\alpha\beta\gamma} &= \sum_i e_{i,\alpha} e_{i,\beta} e_{i,\gamma} f_i, \\ R_{\alpha\beta\gamma\delta} &= \sum_i e_{i,\alpha} e_{i,\beta} e_{i,\gamma} e_{i,\delta} f_i, & S_{\alpha\beta\gamma\delta\epsilon} &= \sum_i e_{i,\alpha} e_{i,\beta} e_{i,\gamma} e_{i,\delta} e_{i,\epsilon} f_i, \end{aligned} \quad (\text{A.7})$$

and $\Pi_{\alpha\beta}^{\text{eq}}$, $Q_{\alpha\beta\gamma}^{\text{eq}}$, $R_{\alpha\beta\gamma\delta}^{\text{eq}}$ and $S_{\alpha\beta\gamma\delta\epsilon}^{\text{eq}}$ are their equilibrium counterpart. Note that an aliasing error can occur on these moments because of the lattice closure, so that they may not be independent from each other [97]. For example, with the D1Q3 and D2Q9 lattices, one has $Q_{xxx} = Q_{xxx}^{\text{eq}} = \rho u_x$. The stress tensor Π appearing in the momentum equation (A.3) can be expressed using Eq. (A.4):

$$\Pi_{\alpha\beta} = \Pi_{\alpha\beta}^{\text{eq}} - \text{Kn} \left(\partial_t \Pi_{\alpha\beta} + \partial_\gamma Q_{\alpha\beta\gamma} - \sum_i e_{i,\alpha} e_{i,\beta} \Psi_i \right) + \text{Kn}^2 \sum_i e_{i,\alpha} e_{i,\beta} E_i^{(1)} + \text{Kn}^3 \sum_i e_{i,\alpha} e_{i,\beta} E_i^{(2)} + O(\text{Kn}^4). \quad (\text{A.8})$$

In the above equation, two terms remain to be expressed at $O(\text{Kn}^3)$: $\partial_t \Pi_{\alpha\beta}$ and $\partial_\gamma Q_{\alpha\beta\gamma}$. For the first one, by successive derivations of Eqs. (A.8)-(A.5) one has

$$\partial_t \Pi_{\alpha\beta} = \partial_t \Pi_{\alpha\beta}^{\text{eq}} - \text{Kn} \left(\partial_{tt}^2 \Pi_{\alpha\beta} + \partial_{\gamma t}^2 Q_{\alpha\beta\gamma} - \sum_i e_{i,\alpha} e_{i,\beta} \partial_t \Psi_i \right) + \text{Kn}^2 \sum_i e_{i,\alpha} e_{i,\beta} \partial_t E_i^{(1)} + O(\text{Kn}^3) \quad (\text{A.9})$$

$$\begin{aligned} &= \partial_t \Pi_{\alpha\beta}^{\text{eq}} - \text{Kn} \left(\partial_{tt}^2 \Pi_{\alpha\beta}^{\text{eq}} + \partial_{\gamma t}^2 Q_{\alpha\beta\gamma}^{\text{eq}} - \sum_i e_{i,\alpha} e_{i,\beta} \partial_t \Psi_i \right) + \text{Kn}^2 \left(\partial_{ttt}^3 \Pi_{\alpha\beta}^{\text{eq}} + 2\partial_{tt\gamma}^3 Q_{\alpha\beta\gamma}^{\text{eq}} + \partial_{t\gamma\delta}^3 R_{\alpha\beta\gamma\delta}^{\text{eq}} \right. \\ &\quad \left. - \sum_i e_{i,\alpha} e_{i,\beta} \partial_{tt}^2 \Psi_i - \sum_i e_{i,\alpha} e_{i,\beta} e_{i,\gamma} \partial_{\gamma t}^2 \Psi_i + \sum_i e_{i,\alpha} e_{i,\beta} \partial_t E_i^{(1)} \right) + O(\text{Kn}^3). \end{aligned} \quad (\text{A.10})$$

Similarly, the second term can be evaluated as

$$\partial_\gamma Q_{\alpha\beta\gamma} = \partial_\gamma Q_{\alpha\beta\gamma}^{\text{eq}} - \text{Kn} \left(\partial_{\gamma t}^2 Q_{\alpha\beta\gamma} + \partial_{\gamma\delta}^2 R_{\alpha\beta\gamma\delta} - \sum_i e_{i,\alpha} e_{i,\beta} e_{i,\gamma} \partial_\gamma \Psi_i \right) + \text{Kn}^2 \sum_i e_{i,\alpha} e_{i,\beta} e_{i,\gamma} \partial_\gamma E_i^{(1)} + O(\text{Kn}^3) \quad (\text{A.11})$$

$$\begin{aligned} &= \partial_\gamma Q_{\alpha\beta\gamma}^{\text{eq}} - \text{Kn} \left(\partial_{\gamma t}^2 Q_{\alpha\beta\gamma}^{\text{eq}} + \partial_{\gamma\delta}^2 R_{\alpha\beta\gamma\delta}^{\text{eq}} - \sum_i e_{i,\alpha} e_{i,\beta} e_{i,\gamma} \partial_\gamma \Psi_i \right) \\ &\quad + \text{Kn}^2 \left(\partial_{\gamma tt}^3 Q_{\alpha\beta\gamma}^{\text{eq}} + 2\partial_{\gamma\delta t}^3 R_{\alpha\beta\gamma\delta}^{\text{eq}} + \partial_{\gamma\delta\epsilon}^3 S_{\alpha\beta\gamma\delta\epsilon}^{\text{eq}} \right. \\ &\quad \left. - \sum_i e_{i,\alpha} e_{i,\beta} e_{i,\gamma} \partial_{\gamma t}^2 \Psi_i - \sum_i e_{i,\alpha} e_{i,\beta} e_{i,\gamma} e_{i,\delta} \partial_{\gamma\delta}^2 \Psi_i + \sum_i e_{i,\alpha} e_{i,\beta} e_{i,\gamma} \partial_\gamma E_i^{(1)} \right) + O(\text{Kn}^3). \end{aligned} \quad (\text{A.12})$$

The flux in the momentum equation (A.3) can then be written as

$$\begin{aligned}
\partial_\beta \Pi_{\alpha\beta} = & \partial_\beta \Pi_{\alpha\beta}^{eq} - \text{Kn} \left(\partial_{\beta t}^2 \Pi_{\alpha\beta}^{eq} + \partial_{\beta\gamma}^2 Q_{\alpha\beta\gamma}^{eq} - \sum_i e_{i,\alpha} e_{i,\beta} \partial_\beta \Psi_i \right) \\
& + \text{Kn}^2 \left(\partial_{\beta t t}^3 \Pi_{\alpha\beta}^{eq} + 2 \partial_{\beta\gamma t}^3 Q_{\alpha\beta\gamma}^{eq} + \partial_{\beta\gamma\delta}^3 R_{\alpha\beta\gamma\delta}^{eq} - \sum_i e_{i,\alpha} e_{i,\beta} \partial_{\beta t}^2 \Psi_i \right. \\
& \left. - \sum_i e_{i,\alpha} e_{i,\beta} e_{i,\gamma} \partial_{\beta\gamma}^2 \Psi_i + \sum_i e_{i,\alpha} e_{i,\beta} \partial_\beta E_i^{(1)} \right) \\
& - \text{Kn}^3 \left(\partial_{\beta t t t}^4 \Pi_{\alpha\beta}^{eq} + 3 \partial_{\beta\gamma t t}^4 Q_{\alpha\beta\gamma}^{eq} + 3 \partial_{\beta\gamma\delta t}^4 R_{\alpha\beta\gamma\delta}^{eq} + \partial_{\beta\gamma\delta\epsilon}^4 S_{\alpha\beta\gamma\delta\epsilon}^{eq} \right. \\
& \left. - \sum_i e_{i,\alpha} e_{i,\beta} \partial_{\beta t t}^3 \Psi_i - 2 \sum_i e_{i,\alpha} e_{i,\beta} e_{i,\gamma} \partial_{\beta\gamma t}^3 \Psi_i - \sum_i e_{i,\alpha} e_{i,\beta} e_{i,\gamma} e_{i,\delta} \partial_{\beta\gamma\delta}^3 \Psi_i \right. \\
& \left. + \sum_i e_{i,\alpha} e_{i,\beta} \partial_{\beta t}^2 E_i^{(1)} + \sum_i e_{i,\alpha} e_{i,\beta} e_{i,\gamma} \partial_{\beta\gamma}^2 E_i^{(1)} - \sum_i e_{i,\alpha} e_{i,\beta} \partial_\beta E_i^{(2)} \right) + O(\text{Kn}^4). \tag{A.13}
\end{aligned}$$

In this expression, any n th-order derivative can be expressed in the linear approximation with the chain rule

$$\partial_{\alpha_1 \dots \alpha_n}^n \Phi = \frac{\partial \Phi}{\partial \rho} \partial_{\alpha_1 \dots \alpha_n}^n \rho + \frac{\partial \Phi}{\partial (\rho u_\alpha)} \partial_{\alpha_1 \dots \alpha_n}^n (\rho u_\alpha), \quad \alpha_i \in \{x, y, t\}, \tag{A.14}$$

which can be used to express the derivatives of $\Pi_{\alpha\beta}^{eq}$, $Q_{\alpha\beta\gamma}^{eq}$, $R_{\alpha\beta\gamma\delta}^{eq}$, $S_{\alpha\beta\gamma\delta\epsilon}^{eq}$, Ψ_i , $E_i^{(1)}$ and $E_i^{(2)}$ as function of derivatives of the macroscopic quantities ρ and ρu_α only. Their time-derivatives can then be disposed using the mass and momentum equations (A.2)-(A.3) at the correct order in Kn. Applying this technique iteratively to dispose of the second-order time-derivatives and above, the following closed set of equations are obtained

$$\partial_t \rho + \partial_\alpha (\rho u_\alpha) = \text{Kn} E_\rho^{(1)} + \text{Kn}^2 E_\rho^{(2)} + \text{Kn}^3 E_\rho^{(3)} + O(\text{Kn}^4), \tag{A.15}$$

$$\partial_t (\rho u_\alpha) + \partial_\beta (\rho u_\alpha u_\beta) + c_s^2 \theta \partial_\alpha \rho = \text{Kn} \left(\rho c_s^2 \theta \partial_\beta S_{\alpha\beta} \right) + \text{Kn} E_{\rho u_\alpha}^{(1)} + \text{Kn}^2 E_{\rho u_\alpha}^{(2)} + \text{Kn}^3 E_{\rho u_\alpha}^{(3)} + O(\text{Kn}^4), \tag{A.16}$$

with $S_{\alpha\beta} = \partial_\alpha u_\beta + \partial_\beta u_\alpha$ and where the fact that $\Pi_{\alpha\beta}^{eq} = \rho u_\alpha u_\beta + \rho c_s^2 \theta \delta_{\alpha\beta}$ has been used. $E_\rho^{(n)}$ and $E_{\rho u_\alpha}^{(n)}$ are deviation terms from the mass and momentum equations of the isothermal Navier-Stokes equations, respectively. They both include:

- the effects of the moments cascade of the DVBE, which can be viewed as errors in consistency with the isothermal NS equations,
- the macroscopic effects of the deviations from the DVBE $E_i^{(n)}$, which include the numerical errors of the model.

Explicit expressions of these deviation terms are obtained using the computer algebra system Maxima [68]. Numerical errors can then be clearly identified as $\Delta t/\tau$ -dependent terms, while consistency errors are the remaining terms when $\Delta t/\tau \rightarrow 0$.

Appendix B. Discretized correction terms

In the case of corrected LB models, the body-force term Ψ_i is usually discretized thanks to finite differences. The aim of this appendix is to focus on the numerical errors performed during their discretization in the context of Taylor expansions in Knudsen number Kn. Starting from the general expression of Eq. (9), it can be re-written in its dimensionless form using a chain rule as:

$$\Psi_i = -\frac{w_i}{2c_s^4} \mathcal{H}_{i,\alpha\beta}^{(2)} \left(\frac{\partial a_{eq,\alpha\beta\gamma}^{(3)}}{\partial \rho} \partial_\gamma \rho + \frac{\partial a_{eq,\alpha\beta\gamma}^{(3)}}{\partial (\rho u_\delta)} \partial_\gamma (\rho u_\delta) \right). \tag{B.1}$$

The discrete form of the correction term Ψ_i^d is then obtained by using a finite-difference scheme for the evaluation of space gradients ∂_γ . Note that the choice of variables used for this discretization, e.g. (ρ, \mathbf{u}) or $(\rho, \rho \mathbf{u})$, has no impact in the linear approximation, and the second one is arbitrarily adopted here. Two kinds of discretizations are considered: a first-order upwind scheme (DUO1) and a second-order central scheme (DCO2):

$$\text{DCO2: } (\partial_\gamma \Phi)^{\text{DCO2}} = \frac{\Phi(\mathbf{x} + k\Delta x \mathbf{e}_\gamma) - \Phi(\mathbf{x} - k\Delta x \mathbf{e}_\gamma)}{2k\Delta x}, \quad (\text{B.2})$$

$$\text{DUO1: } (\partial_\gamma \Phi)^{\text{DUO1}} = \frac{\Phi(\mathbf{x} + d^+ k\Delta x \mathbf{e}_\gamma) - \Phi(\mathbf{x} - d^- k\Delta x \mathbf{e}_\gamma)}{k\Delta x} \quad \text{with} \quad \begin{cases} d^+ = |\text{sgn}(u_\gamma) - 1|/2 \\ d^- = |\text{sgn}(u_\gamma) + 1|/2 \end{cases}, \quad (\text{B.3})$$

for any function Φ , where \mathbf{e}_γ is the unit vector in the direction γ . A Taylor series expansion of these expressions yields

$$\text{DCO2: } (\partial_\gamma \Phi)^{\text{DCO2}} = \partial_\gamma \Phi + \frac{\text{Kn}^2}{6} \left(\frac{\Delta t}{\tau} \right)^2 \partial_{\gamma\gamma\gamma}^3 \Phi + O(\text{Kn}^4), \quad (\text{B.4})$$

$$\begin{aligned} \text{DUO1: } (\partial_\gamma \Phi)^{\text{DUO1}} &= \partial_\gamma \Phi - \text{sgn}(u_\gamma) \frac{\text{Kn}}{2} \frac{\Delta t}{\tau} \partial_{\gamma\gamma}^2 \Phi + \frac{\text{Kn}^2}{6} \left(\frac{\Delta t}{\tau} \right)^2 \partial_{\gamma\gamma\gamma}^3 \Phi \\ &\quad - \text{sgn}(u_\gamma) \frac{\text{Kn}^3}{24} \left(\frac{\Delta t}{\tau} \right)^3 \partial_{\gamma\gamma\gamma\gamma}^4 \Phi + O(\text{Kn}^4). \end{aligned} \quad (\text{B.5})$$

This leads to the following Taylor series expansions for the linearized Ψ_i^d with a DCO2 discretization:

$$\Psi_i^{\text{DCO2}} = \Psi_i - \frac{w_i}{2c_s^4} \mathcal{H}_{i,\alpha\beta}^{(2)} \frac{\text{Kn}^2}{6} \left(\frac{\Delta t}{\tau} \right)^2 \left(\frac{\partial a_{\text{eq},\alpha\beta\gamma}^{(3)}}{\partial \rho} \partial_{\gamma\gamma\gamma}^3 \rho + \frac{\partial a_{\text{eq},\alpha\beta\gamma}^{(3)}}{\partial (\rho u_\delta)} \partial_{\gamma\gamma\gamma}^3 (\rho u_\delta) \right) + O(\text{Kn}^4), \quad (\text{B.6})$$

and with a DUO1 discretization:

$$\begin{aligned} \Psi_i^{\text{DUO1}} &= \Psi_i^{\text{DCO2}} + \text{sgn}(u_\gamma) \frac{w_i}{2c_s^4} \mathcal{H}_{i,\alpha\beta}^{(2)} \left(\frac{\text{Kn}}{2} \frac{\Delta t}{\tau} \left(\frac{\partial a_{\text{eq},\alpha\beta\gamma}^{(3)}}{\partial \rho} \partial_{\gamma\gamma}^2 \rho + \frac{\partial a_{\text{eq},\alpha\beta\gamma}^{(3)}}{\partial (\rho u_\delta)} \partial_{\gamma\gamma}^2 (\rho u_\delta) \right) \right. \\ &\quad \left. + \frac{\text{Kn}^3}{24} \left(\frac{\Delta t}{\tau} \right)^3 \left(\frac{\partial a_{\text{eq},\alpha\beta\gamma}^{(3)}}{\partial \rho} \partial_{\gamma\gamma\gamma\gamma}^4 \rho + \frac{\partial a_{\text{eq},\alpha\beta\gamma}^{(3)}}{\partial (\rho u_\delta)} \partial_{\gamma\gamma\gamma\gamma}^4 (\rho u_\delta) \right) \right). \end{aligned} \quad (\text{B.7})$$

Appendix C. Matrices of the linear analyses

C.1. Macroscopic equations with deviation terms

To perform analyses of Eqs. (23)-(24), the linearized deviation terms $E_\Phi^{(n)}$ can be written under the following general form:

$$E_\Phi^{(n)} = A_{\Phi,\alpha_1 \dots \alpha_{n+1}}^{(n+1)} \frac{\partial^{n+1} \rho}{\partial \alpha_1 \dots \partial \alpha_{n+1}} + B_{\Phi,\alpha_1 \dots \alpha_{n+1}}^{(n+1)} \frac{\partial^{n+1} (\rho u_x)}{\partial \alpha_1 \dots \partial \alpha_{n+1}} + C_{\Phi,\alpha_1 \dots \alpha_{n+1}}^{(n+1)} \frac{\partial^{n+1} (\rho u_y)}{\partial \alpha_1 \dots \partial \alpha_{n+1}}, \quad \Phi \in \{\rho, \rho u_\alpha\}, \quad (\text{C.1})$$

where implicit summations are performed on indices $\alpha_1, \dots, \alpha_{n+1} \in \{x, y\}$ and $\mathbf{A}_\Phi^{(n)}$, $\mathbf{B}_\Phi^{(n)}$ and $\mathbf{C}_\Phi^{(n)}$ are constant coefficients involving the mean base (space- and time-averaged) density and velocity. In 1D, every index is equal to x and $\mathbf{C}_\Phi^{(n)} = 0$ so that, for instance, the first-order deviation of the mass equation $E_\rho^{(1)}$ can be written as

$$E_\rho^{(1)} = A_{\rho,xx}^{(2)} \frac{\partial^2 \rho}{\partial x^2} + B_{\rho,xx}^{(2)} \frac{\partial^2 (\rho u_x)}{\partial x^2}. \quad (\text{C.2})$$

A linear analysis of Eqs. (23)-(24) yields the following system of equations

$$\omega^* \hat{\rho} = k_\alpha^* \hat{j}_\alpha - \sum_{n \geq 1} i^n \left(\frac{\tau}{\Delta t} \right)^n k_{\alpha_1}^* \dots k_{\alpha_{n+1}}^* \left(A_{\rho,\alpha_1 \dots \alpha_{n+1}}^{(n+1)} \hat{\rho} + B_{\rho,\alpha_1 \dots \alpha_{n+1}}^{(n+1)} \hat{j}_x + C_{\rho,\alpha_1 \dots \alpha_{n+1}}^{(n+1)} \hat{j}_y \right), \quad (\text{C.3})$$

$$\begin{aligned} \omega^* \hat{j}_\alpha &= k_\beta^* \left(\overline{u_\beta} \hat{j}_\alpha + \overline{u_\alpha} \hat{j}_\beta - \overline{u_\alpha u_\beta} \hat{\rho} \right) + k_\alpha^* c_s^2 \theta \hat{\rho} - i \frac{\tau}{\Delta t} c_s^2 \theta k_\beta^* \left(k_\alpha^* \hat{j}_\beta + k_\beta^* \hat{j}_\alpha - \overline{u_\beta} k_\alpha^* \hat{\rho} - \overline{u_\alpha} k_\beta^* \hat{\rho} \right) \\ &\quad - \sum_{n \geq 1} i^n \left(\frac{\tau}{\Delta t} \right)^n k_{\alpha_1}^* \dots k_{\alpha_{n+1}}^* \left(A_{\rho u_\alpha, \alpha_1 \dots \alpha_{n+1}}^{(n+1)} \hat{\rho} + B_{\rho u_\alpha, \alpha_1 \dots \alpha_{n+1}}^{(n+1)} \hat{j}_x + C_{\rho u_\alpha, \alpha_1 \dots \alpha_{n+1}}^{(n+1)} \hat{j}_y \right), \end{aligned} \quad (\text{C.4})$$

where $j_\alpha = \rho u_\alpha$. The eigenvalue problem of Eq. (31) is then recovered with

$$M_{00}^{(p)} = -\sum_{n=1}^p i^n \left(\frac{\tau}{\Delta t}\right)^n k_{\alpha_1}^* \dots k_{\alpha_{n+1}}^* A_{\rho, \alpha_1 \dots \alpha_{n+1}}^{(n+1)}, \quad M_{01}^{(p)} = k_x^* - \sum_{n=1}^p i^n \left(\frac{\tau}{\Delta t}\right)^n k_{\alpha_1}^* \dots k_{\alpha_{n+1}}^* B_{\rho, \alpha_1 \dots \alpha_{n+1}}^{(n+1)}, \quad (\text{C.5})$$

$$M_{02}^{(p)} = k_y^* - \sum_{n=1}^p i^n \left(\frac{\tau}{\Delta t}\right)^n k_{\alpha_1}^* \dots k_{\alpha_{n+1}}^* C_{\rho, \alpha_1 \dots \alpha_{n+1}}^{(n+1)}, \quad (\text{C.6})$$

$$M_{10}^{(p)} = -k_x^* \overline{u_x^2} - k_y^* \overline{u_x u_y} + k_x^* c_s^2 \theta + i \frac{\tau}{\Delta t} c_s^2 \theta \left(2k_x^{*2} \overline{u_x} + k_x^* k_y^* \overline{u_y} + k_y^{*2} \overline{u_x}\right) - \sum_{n=1}^p i^n \left(\frac{\tau}{\Delta t}\right)^n k_{\alpha_1}^* \dots k_{\alpha_{n+1}}^* A_{\rho u_x, \alpha_1 \dots \alpha_{n+1}}^{(n+1)}, \quad (\text{C.7})$$

$$M_{11}^{(p)} = 2k_x^* \overline{u_x} + k_y^* \overline{u_y} - i \frac{\tau}{\Delta t} c_s^2 \theta \left(2k_x^{*2} + k_y^{*2}\right) - \sum_{n=1}^p i^n \left(\frac{\tau}{\Delta t}\right)^n k_{\alpha_1}^* \dots k_{\alpha_{n+1}}^* B_{\rho u_x, \alpha_1 \dots \alpha_{n+1}}^{(n+1)}, \quad (\text{C.8})$$

$$M_{12}^{(p)} = k_y^* \overline{u_x} - i \frac{\tau}{\Delta t} c_s^2 \theta \left(k_x^* k_y^*\right), \quad (\text{C.9})$$

$$M_{20}^{(p)} = -k_x^* \overline{u_x u_y} - k_y^* \overline{u_y^2} + k_y^* c_s^2 \theta + i \frac{\tau}{\Delta t} c_s^2 \theta \left(k_x^* k_y^* \overline{u_x} + k_x^{*2} \overline{u_y} + 2k_y^{*2} \overline{u_y}\right) - \sum_{n=1}^p i^n \left(\frac{\tau}{\Delta t}\right)^n k_{\alpha_1}^* \dots k_{\alpha_{n+1}}^* A_{\rho u_y, \alpha_1 \dots \alpha_{n+1}}^{(n+1)}, \quad (\text{C.10})$$

$$M_{21}^{(p)} = k_x^* \overline{u_y} - i \frac{\tau}{\Delta t} c_s^2 \theta \left(k_x^* k_y^*\right) - \sum_{n=1}^p i^n \left(\frac{\tau}{\Delta t}\right)^n k_{\alpha_1}^* \dots k_{\alpha_{n+1}}^* B_{\rho u_y, \alpha_1 \dots \alpha_{n+1}}^{(n+1)}, \quad (\text{C.11})$$

$$M_{22}^{(p)} = k_x^* \overline{u_x} + 2k_y^* \overline{u_y} - i \frac{\tau}{\Delta t} c_s^2 \theta \left(k_x^{*2} + 2k_y^{*2}\right) - \sum_{n=1}^p i^n \left(\frac{\tau}{\Delta t}\right)^n k_{\alpha_1}^* \dots k_{\alpha_{n+1}}^* C_{\rho u_y, \alpha_1 \dots \alpha_{n+1}}^{(n+1)}, \quad (\text{C.12})$$

where p is the order of truncation of the Taylor expansion in Kn. Note that the error done on the eigenvalue problem is of the order $O(k^{*p+2})$ for a given value of the dimensionless relaxation time $\tau/\Delta t$. This is an important observation for validating the deviation terms by comparison with the eigenvalues of the linearized LB scheme.

C.2. LBM with BGK collision

The linear stability analysis of the LB scheme with the BGK collision model can be found in previous references [71,72,13,15,73,16,77,78,32]. The eigenvalue problem of Eq. (32) is recovered with

$$\mathbf{M}_{ij}^{\text{LBM}} = e^{-ik_\alpha^* e_{i,\alpha}} \left(\delta_{ij} - \frac{\Delta t}{\tau + \Delta t/2} \left(\delta_{ij} - \mathbf{J}_{ij}^{eq,N} \right) + \frac{\tau}{\tau + \Delta t/2} \left(D_\gamma^{\text{FD}} \psi_{ij,\gamma} \right) \right), \quad (\text{C.13})$$

where $\mathbf{J}^{eq,N}$ is the Jacobian matrix of the equilibrium distribution, which can be analytically computed as [32]

$$\mathbf{J}_{ij}^{eq,N} = \sum_{n=0}^N \frac{w_i}{n! c_s^{2n}} \mathbf{\Lambda}_{eq,j}^{(n)} : \mathcal{H}_i^{(n)}, \quad (\text{C.14})$$

where

$$\mathbf{\Lambda}_{eq,j}^{(0)} = 1, \quad \left(\mathbf{\Lambda}_{eq,j}^{(1)} \right)_\alpha = e_{j,\alpha}, \quad \left(\mathbf{\Lambda}_{eq,j}^{(2)} \right)_{\alpha\beta} = \overline{u_\alpha} e_{j,\beta} + \overline{u_\beta} e_{j,\alpha} - \overline{u_\alpha u_\beta}, \quad (\text{C.15})$$

$$\left(\mathbf{\Lambda}_{eq,j}^{(3)} \right)_{\alpha\beta\gamma} = \overline{u_\alpha u_\beta} e_{j,\gamma} + \overline{u_\alpha u_\gamma} e_{j,\beta} + \overline{u_\beta u_\gamma} e_{j,\alpha} - 2\overline{u_\alpha u_\beta u_\gamma}, \quad (\text{C.16})$$

$$\left(\mathbf{\Lambda}_{eq,j}^{(4)} \right)_{\alpha\beta\gamma\delta} = \overline{u_\alpha u_\beta u_\gamma} e_{j,\delta} + \overline{u_\alpha u_\beta u_\delta} e_{j,\gamma} + \overline{u_\alpha u_\gamma u_\delta} e_{j,\beta} + \overline{u_\beta u_\gamma u_\delta} e_{j,\alpha} - 3\overline{u_\alpha u_\beta u_\gamma u_\delta}. \quad (\text{C.17})$$

The last right-hand-side term of Eq. (C.13) aims at considering the body-force term Ψ_i of Eq. (9) in the linear analysis, with

$$\psi_{ij,\gamma} = -\frac{w_i}{2c_s^4} \mathcal{H}_{i,\alpha\beta}^{(2)} \left(\mathbf{\Lambda}_{eq,j}^{(3)} \right)_{\alpha\beta\gamma}, \quad (\text{C.18})$$

and where D_γ^{FD} accounts for the linearized space gradients in the direction γ , depending on the way they are discretized:

$$\text{Analytical gradients : } D_{\gamma}^{\text{FD}} = ik_{\gamma}^*, \quad (\text{C.19})$$

$$\text{DCO2 : } D_{\gamma}^{\text{FD}} = i \sin(k_{\gamma}^*), \quad (\text{C.20})$$

$$\text{DUO1 : } D_{\gamma}^{\text{FD}} = \text{sgn}(\overline{u_{\gamma}}) \left(1 - \exp(-\text{sgn}(\overline{u_{\gamma}}) ik_{\gamma}^*) \right) \quad (\text{C.21})$$

C.3. LBM with regularized collision

Linear stability analyses of the regularized LBM can be found in [32,89]. The eigenvalue problem of Eq. (32) is generally recovered with

$$\mathbf{M}_{ij}^{\text{LBM}} = e^{-ik_{\alpha}^* e_{i,\alpha}} \left(\mathbf{J}_{ij}^{\text{eq},N} + \left(1 - \frac{\Delta t}{\tau + \Delta t/2} \right) \mathbf{J}_{ij}^{(1)} + \frac{1}{2} D_{\gamma}^{\text{FD}} \psi_{ij,\gamma} \right), \quad (\text{C.22})$$

where $\mathbf{J}_{ij}^{(1)}$ is the Jacobian matrix of the off-equilibrium distribution functions. It depends on the regularized scheme:

$$\text{Shear stress reconstruction: } \mathbf{J}_{ij}^{(1)} = -\frac{w_i}{c_s^2} \left(\frac{\tau}{\Delta t} + \frac{1}{2} \right) \left(e_{i,\alpha} e_{i,\beta} - c_s^2 \delta_{\alpha\beta} \right) \theta \left(D_{\alpha}^{\text{FD}} (e_{j,\beta} - \overline{u_{\beta}}) + D_{\beta}^{\text{FD}} (e_{j,\alpha} - \overline{u_{\alpha}}) \right), \quad (\text{C.23})$$

$$\text{PR/RR: } \mathbf{J}_{ij}^{(1)} = [\mathbf{H}^{-1} \mathbf{P} \mathbf{H}]_{ik} \left[\delta_{kj} - \mathbf{J}_{kj}^{\text{eq},N} + \frac{1}{2} D_{\gamma}^{\text{FD}} \psi_{kj,\gamma} \right], \quad (\text{C.24})$$

where \mathbf{H} and \mathbf{P} are defined in Sec. 6.1.

C.4. MRT models

For MRT models in absence of body-force term as considered in Sec. 7, the eigenvalue problem of Eq. (32) is recovered with

$$\mathbf{M}_{ij}^{\text{LBM}} = e^{-ik_{\alpha}^* e_{i,\alpha}} \left(\delta_{ij} - \overline{\mathbf{C}}_{ik} \left(\delta_{kj} - \mathbf{J}_{kj}^{\text{eq},N} \right) \right), \quad (\text{C.25})$$

where $\overline{\mathbf{C}}$ is the collision matrix evaluated at the mean base flow.

Appendix D. Relations with Genocchi and Bernoulli numbers for the BGK collision model

Let us consider the coefficients c_n defined by the following recurrence relation

$$c_0 = 2, \quad \forall n \geq 1, \quad c_n = - \sum_{k=0}^n \binom{n}{k} c_k. \quad (\text{D.1})$$

In order to find out any interesting property in the Taylor expansion of f_i^{neq} with the BGK collision model, let us focus on the generating function of c_n :

$$f(x) = \sum_{n \geq 0} c_n \frac{x^n}{n!}. \quad (\text{D.2})$$

Multiplying Eq. (D.1) by $x^n/n!$ and doing a summation over $n \geq 1$ yield

$$\sum_{n \geq 1} c_n \frac{x^n}{n!} = - \sum_{n \geq 1} \sum_{k=0}^n \binom{n}{k} c_k \frac{x^n}{n!} \Rightarrow \sum_{n \geq 0} c_n \frac{x^n}{n!} - c_0 = - \sum_{n \geq 0} \sum_{k=0}^n \binom{n}{k} c_k \frac{x^n}{n!} + c_0 \quad (\text{D.3})$$

$$\Rightarrow \underbrace{\sum_{n \geq 0} c_n \frac{x^n}{n!}}_{f(x)} - 2 = - \left(\underbrace{\sum_{n \geq 0} c_n \frac{x^n}{n!}}_{f(x)} \right) \left(\underbrace{\sum_{n \geq 0} \frac{x^n}{n!}}_{\exp(x)} \right) + 2. \quad (\text{D.4})$$

Hence, the generating function of c_n is given by

$$f(x) = \frac{4}{\exp(x) + 1}. \quad (\text{D.5})$$

Then, knowing that $f(x) + f(-x) = 4$, one has

$$\sum_{n \geq 0} c_n \frac{x^n}{n!} (1 + (-1)^n) = 4, \quad (\text{D.6})$$

so that any even coefficient is null:

$$\forall p \geq 1, c_{2p} = 0. \quad (\text{D.7})$$

Note that, given the generating function f of c_n , these coefficients can be related to the Genocchi numbers G_n defined by their generating function g [82]:

$$g(x) = \sum_{n \geq 1} G_n \frac{x^n}{n!} = \frac{2x}{\exp(x) + 1} = \frac{x}{2} f(x). \quad (\text{D.8})$$

Hence,

$$\forall n \geq 0, c_n = 2 \frac{G_{n+1}}{n+1}. \quad (\text{D.9})$$

Genocchi numbers can also be related to the Bernoulli numbers B_n^- as [81,82]

$$\forall n \geq 1, G_n = 2(1 - 2^n) B_n^-, \quad (\text{D.10})$$

so that

$$\forall n \geq 0, c_n = 4(1 - 2^{n+1}) \frac{B_{n+1}^-}{n+1}. \quad (\text{D.11})$$

Appendix E. Deviation terms of the BGK model with the D2Q9 lattice

This appendix provides the deviation terms $E_\phi^{(n)}$ of the BGK-D2Q9 model, from the isothermal NS equations. For the sake of simplicity, only the x -derivatives will be provided in the deviation terms $E_{\rho u_x}^{(2)}$, $E_{\rho u_y}^{(2)}$, $E_\rho^{(3)}$, $E_{\rho u_x}^{(3)}$ and $E_{\rho u_y}^{(3)}$. The expression of the other terms ($E_\rho^{(1)}$, $E_{\rho u_x}^{(1)}$, $E_{\rho u_y}^{(1)}$ and $E_\rho^{(2)}$) is much simpler, they will be provided in their complete form. Three equilibrium are considered: $N = 2$, $N = 3^*$ and $N = 4^*$, with and without correction term Ψ_i .

Note that deviation terms are completely equivalent in the x -direction with the partial third-order ($N = 3^*$) and the partial fourth-order ($N = 4^*$) equilibria, they are therefore only provided once.

E.1. Second-order equilibrium ($N = 2$)

No correction:

$$\begin{aligned} E_\rho^{(1)} &= 0, & E_{\rho u_x}^{(1)} &= -\partial_{xx}^2 a_{eq,xxx}^{(3)} - 2\partial_{xy}^2 a_{eq,xyx}^{(3)} - \partial_{yy}^2 a_{eq,xyy}^{(3)}, & E_{\rho u_y}^{(1)} &= -\partial_{xx}^2 a_{eq,xyx}^{(3)} - 2\partial_{xy}^2 a_{eq,xyy}^{(3)} - \partial_{yy}^2 a_{eq,yyy}^{(3)}, \\ E_\rho^{(2)} &= \left(\frac{\Delta t}{\tau}\right)^2 \frac{1}{12} \left(-\partial_{xxx}^3 a_{eq,xxx}^{(3)} - 3\partial_{xxy}^3 a_{eq,xyx}^{(3)} - 3\partial_{xyy}^3 a_{eq,xyy}^{(3)} - \partial_{yyy}^3 a_{eq,yyy}^{(3)} + \rho c_s^2 \theta (\partial_{xx}^2 S_{xx} + 2\partial_{xy}^2 S_{xy} + \partial_{yy}^2 S_{yy}) \right), \\ E_{\rho u_x}^{(2)} &= C_1 + \left(\frac{\Delta t}{\tau}\right)^2 N_1, & E_{\rho u_y}^{(2)} &= C_5 + \left(\frac{\Delta t}{\tau}\right)^2 N_5, & E_\rho^{(3)} &= \left(\frac{\Delta t}{\tau}\right)^2 \frac{1}{12} \partial_x C_1, \\ E_{\rho u_x}^{(3)} &= C_2 + \left(\frac{\Delta t}{\tau}\right)^2 N_2, & E_{\rho u_y}^{(3)} &= C_6 + \left(\frac{\Delta t}{\tau}\right)^2 N_6. \end{aligned} \quad (\text{E.1})$$

Including now a correction term Ψ_i without considering its discretization errors, one has

$$\begin{aligned} E_\rho^{(1)} &= 0, & E_{\rho u_x}^{(1)} &= 0, & E_{\rho u_y}^{(1)} &= 0, \\ E_\rho^{(2)} &= \left(\frac{\Delta t}{\tau}\right)^2 \frac{1}{12} \left(-\partial_{xxx}^3 a_{eq,xxx}^{(3)} - 3\partial_{xxy}^3 a_{eq,xyx}^{(3)} - 3\partial_{xyy}^3 a_{eq,xyy}^{(3)} - \partial_{yyy}^3 a_{eq,yyy}^{(3)} + \rho c_s^2 \theta (\partial_{xx}^2 S_{xx} + 2\partial_{xy}^2 S_{xy} + \partial_{yy}^2 S_{yy}) \right), \\ E_{\rho u_x}^{(2)} &= C_3 + \left(\frac{\Delta t}{\tau}\right)^2 N_1, & E_{\rho u_y}^{(2)} &= C_7 + \left(\frac{\Delta t}{\tau}\right)^2 N_5, & E_\rho^{(3)} &= \left(\frac{\Delta t}{\tau}\right)^2 \frac{1}{12} \partial_x C_3, \\ E_{\rho u_x}^{(3)} &= C_4 + \left(\frac{\Delta t}{\tau}\right)^2 N_3, & E_{\rho u_y}^{(3)} &= C_8 + \left(\frac{\Delta t}{\tau}\right)^2 N_7. \end{aligned} \quad (\text{E.2})$$

Including the discretization effects of the DCO2 scheme, only third-order errors in the momentum equation are affected:

$$E_{\rho u_x}^{(3)} = C_4 + \left(\frac{\Delta t}{\tau}\right)^2 \left(N_3 + \frac{1}{6} \frac{\partial^4 a_{eq,xxx}^{(3)}}{\partial x^4}\right), \quad E_{\rho u_y}^{(3)} = C_8 + \left(\frac{\Delta t}{\tau}\right)^2 \left(N_7 + \frac{1}{6} \frac{\partial^4 a_{eq,xyy}^{(3)}}{\partial x^4}\right). \quad (E.3)$$

Finally, with the DU01 scheme, the numerical errors of the momentum equations are altered as

$$\begin{aligned} E_{\rho u_x}^{(2)} &= C_3 + \left(\frac{\Delta t}{\tau}\right)^2 N_1 - \left(\frac{\Delta t}{2\tau}\right) \text{sgn}(u_x) \frac{\partial^3 a_{eq,xxx}^{(3)}}{\partial x^3}, & E_{\rho u_y}^{(2)} &= C_7 + \left(\frac{\Delta t}{\tau}\right)^2 N_5 - \left(\frac{\Delta t}{2\tau}\right) \text{sgn}(u_x) \frac{\partial^3 a_{eq,xyy}^{(3)}}{\partial x^3}, \\ E_{\rho u_x}^{(3)} &= C_4 + \left(\frac{\Delta t}{\tau}\right)^2 \left(N_3 + \frac{1}{6} \frac{\partial^4 a_{eq,xxx}^{(3)}}{\partial x^4}\right) + \left(\frac{\Delta t}{2\tau}\right) \text{sgn}(u_x) N_4, \\ E_{\rho u_y}^{(3)} &= C_8 + \left(\frac{\Delta t}{\tau}\right)^2 \left(N_7 + \frac{1}{6} \frac{\partial^4 a_{eq,xyy}^{(3)}}{\partial x^4}\right) + \left(\frac{\Delta t}{2\tau}\right) \text{sgn}(u_x) N_9. \end{aligned} \quad (E.4)$$

E.2. Partial third- and fourth-order equilibria ($N = 3^*, 4^*$)

No correction:

$$\begin{aligned} E_{\rho}^{(1)} &= 0, & E_{\rho u_x}^{(1)} &= -\frac{\partial^2 a_{eq,xxx}^{(3)}}{\partial x^2}, & E_{\rho u_y}^{(1)} &= -\frac{\partial^2 a_{eq,yyy}^{(3)}}{\partial y^2}, \\ E_{\rho}^{(2)} &= \left(\frac{\Delta t}{\tau}\right)^2 \frac{1}{12} \left(-\frac{\partial^3 a_{eq,xxx}^{(3)}}{\partial x^3} - \frac{\partial^3 a_{eq,yyy}^{(3)}}{\partial y^3} + \rho c_s^2 \theta \left(\frac{\partial^2 S_{xx}}{\partial x^2} + 2 \frac{\partial^2 S_{xy}}{\partial x \partial y} + \frac{\partial^2 S_{yy}}{\partial y^2}\right)\right), \\ E_{\rho u_x}^{(2)} &= C_1 + \left(\frac{\Delta t}{\tau}\right)^2 N_1, & E_{\rho u_y}^{(2)} &= a_{eq,xxx}^{(3)} \frac{\partial^3 u_y}{\partial x^3} + \left(\frac{\Delta t}{\tau}\right)^2 N_{15}, \\ E_{\rho}^{(3)} &= \left(\frac{\Delta t}{\tau}\right)^2 \frac{1}{12} \partial_x C_1, & E_{\rho u_x}^{(3)} &= C_2 + \left(\frac{\Delta t}{\tau}\right)^2 N_2, & E_{\rho u_y}^{(3)} &= C_9 + \left(\frac{\Delta t}{\tau}\right)^2 N_{10}. \end{aligned} \quad (E.5)$$

Analytically computed correction:

$$\begin{aligned} E_{\rho}^{(1)} &= 0, & E_{\rho u_x}^{(1)} &= 0, & E_{\rho u_y}^{(1)} &= 0, \\ E_{\rho}^{(2)} &= \left(\frac{\Delta t}{\tau}\right)^2 \frac{1}{12} \left(-\frac{\partial^3 a_{eq,xxx}^{(3)}}{\partial x^3} - \frac{\partial^3 a_{eq,yyy}^{(3)}}{\partial y^3} + \rho c_s^2 \theta \left(\frac{\partial^2 S_{xx}}{\partial x^2} + 2 \frac{\partial^2 S_{xy}}{\partial x \partial y} + \frac{\partial^2 S_{yy}}{\partial y^2}\right)\right), \\ E_{\rho u_x}^{(2)} &= C_3 + \left(\frac{\Delta t}{\tau}\right)^2 N_1, & E_{\rho u_y}^{(2)} &= \frac{\partial^3}{\partial x^3} (u_y a_{eq,xxx}^{(3)}) + \left(\frac{\Delta t}{\tau}\right)^2 N_{15}, \\ E_{\rho}^{(3)} &= \left(\frac{\Delta t}{\tau}\right)^2 \frac{1}{12} \partial_x C_3, & E_{\rho u_x}^{(3)} &= C_4 + \left(\frac{\Delta t}{\tau}\right)^2 N_3, & E_{\rho u_y}^{(3)} &= C_{10} + \left(\frac{\Delta t}{\tau}\right)^2 N_8. \end{aligned} \quad (E.6)$$

Including the discretization effects of the DCO2 scheme, only the third-order error in the x -momentum equation is affected:

$$E_{\rho u_x}^{(3)} = C_4 + \left(\frac{\Delta t}{\tau}\right)^2 \left(N_3 + \frac{1}{6} \frac{\partial^4 a_{eq,xxx}^{(3)}}{\partial x^4}\right). \quad (E.7)$$

Finally, with the DU01 scheme, the numerical errors of the momentum equations are altered as

$$\begin{aligned} E_{\rho u_x}^{(2)} &= C_3 + \left(\frac{\Delta t}{\tau}\right)^2 N_1 - \left(\frac{\Delta t}{2\tau}\right) \text{sgn}(u_x) \frac{\partial^3 a_{eq,xxx}^{(3)}}{\partial x^3}, \\ E_{\rho u_x}^{(3)} &= C_4 + \left(\frac{\Delta t}{\tau}\right)^2 \left(N_3 + \frac{1}{6} \frac{\partial^4 a_{eq,xxx}^{(3)}}{\partial x^4}\right) + \left(\frac{\Delta t}{2\tau}\right) \text{sgn}(u_x) N_4, \\ E_{\rho u_y}^{(3)} &= C_{10} + \left(\frac{\Delta t}{\tau}\right)^2 N_8 - \left(\frac{\Delta t}{2\tau}\right) \text{sgn}(u_x) u_y \frac{\partial^4 a_{eq,xxx}^{(3)}}{\partial x^4}. \end{aligned} \quad (E.8)$$

Appendix F. Deviation terms of the shear stress reconstruction (HRR- $\sigma = 0$) with the D2Q9 lattice

This appendix provides the deviation terms (with the athermal NS equations) of the D2Q9 lattice with the shear stress reconstruction of Sec. 5, also referred to as HRR- $\sigma = 0$, in the linear approximation. Only the equilibrium at second-order ($N = 2$) is considered here, noticing that changing the order of the Hermite-based equilibrium has very few impact on the general conclusions. Furthermore, for the sake of simplicity, only x -derivatives are provided for $E_{\rho u_y}^{(2)}$, $E_{\rho}^{(3)}$ and $E_{\rho u_x}^{(3)}$.

F.1. Non corrected D2Q9 lattice, analytical reconstruction of $g_i^{(1)}$

$$\begin{aligned}
E_{\rho}^{(1)} &= 0, & E_{\rho u_x}^{(1)} &= -\left(\frac{\Delta t}{2\tau}\right) \left(\partial_{xx}^2 a_{eq,xxx}^{(3)} + 2\partial_{xy}^2 a_{eq,xyx}^{(3)} + \partial_{yy}^2 a_{eq,xyy}^{(3)}\right), \\
E_{\rho u_y}^{(1)} &= -\left(\frac{\Delta t}{2\tau}\right) \left(\partial_{xx}^2 a_{eq,xyx}^{(3)} + 2\partial_{xy}^2 a_{eq,xyy}^{(3)} + \partial_{yy}^2 a_{eq,yyy}^{(3)}\right), \\
E_{\rho}^{(2)} &= \left(\frac{\Delta t}{\tau}\right)^2 \frac{1}{12} \left(-\partial_{xxx}^3 a_{eq,xxx}^{(3)} - 3\partial_{xxy}^3 a_{eq,xyx}^{(3)} - 3\partial_{xyy}^3 a_{eq,xyy}^{(3)} - \partial_{yyy}^3 a_{eq,yyy}^{(3)} + \rho c_s^2 \theta (\partial_{xx}^2 S_{xx} + 2\partial_{xy}^2 S_{xy} + \partial_{yy}^2 S_{yy})\right), \\
E_{\rho u_x}^{(2)} &= \left(\frac{\Delta t}{\tau}\right) \frac{C_3}{2} + \left(\frac{\Delta t}{\tau}\right)^2 N_{11}, & E_{\rho u_y}^{(2)} &= \left(\frac{\Delta t}{\tau}\right) N_{19} + \left(\frac{\Delta t}{\tau}\right)^2 N_{20}, \\
E_{\rho}^{(3)} &= \frac{1}{12} \left(\frac{\Delta t}{\tau}\right)^2 \partial_x C_3 + \left(\frac{\Delta t}{\tau}\right)^3 N_{12}, \\
E_{\rho u_x}^{(3)} &= \left(\frac{\Delta t}{\tau}\right) N_{13} + \left(\frac{\Delta t}{\tau}\right)^2 N_{14} + \left(\frac{\Delta t}{\tau}\right)^3 N_{16}, & E_{\rho u_y}^{(3)} &= -\left(\frac{\Delta t}{\tau}\right) \frac{\rho \theta^2}{18} \frac{\partial^4 u_y}{\partial x^4} + \left(\frac{\Delta t}{\tau}\right)^2 N_{21} + \left(\frac{\Delta t}{\tau}\right)^3 N_{22}.
\end{aligned} \tag{F.1}$$

F.2. $N = 2$, analytically corrected D2Q9 lattice, analytical reconstruction of $g_i^{(1)}$

$$\begin{aligned}
E_{\rho}^{(1)} &= 0, & E_{\rho u_x}^{(1)} &= 0, & E_{\rho u_y}^{(1)} &= 0, \\
E_{\rho}^{(2)} &= \left(\frac{\Delta t}{\tau}\right)^2 \frac{1}{12} \left(-\partial_{xxx}^3 a_{eq,xxx}^{(3)} - 3\partial_{xxy}^3 a_{eq,xyx}^{(3)} - 3\partial_{xyy}^3 a_{eq,xyy}^{(3)} - \partial_{yyy}^3 a_{eq,yyy}^{(3)} + \rho c_s^2 \theta (\partial_{xx}^2 S_{xx} + 2\partial_{xy}^2 S_{xy} + \partial_{yy}^2 S_{yy})\right), \\
E_{\rho u_x}^{(2)} &= \left(\frac{\Delta t}{2\tau}\right) C_3 + \left(\frac{\Delta t}{\tau}\right)^2 N_1, & E_{\rho u_y}^{(2)} &= \left(\frac{\Delta t}{\tau}\right) N_{19} + \left(\frac{\Delta t}{\tau}\right)^2 N_{23}, & E_{\rho}^{(3)} &= \frac{1}{12} \left(\frac{\Delta t}{\tau}\right)^2 \partial_x C_3, \\
E_{\rho u_x}^{(3)} &= \left(\frac{\Delta t}{\tau}\right) N_{13} + \left(\frac{\Delta t}{\tau}\right)^2 N_{17} + \left(\frac{\Delta t}{\tau}\right)^3 N_{18}, & E_{\rho u_y}^{(3)} &= -\left(\frac{\Delta t}{\tau}\right) \frac{\rho \theta^2}{18} \frac{\partial^4 u_y}{\partial x^4} + \left(\frac{\Delta t}{\tau}\right)^2 N_{24} + \left(\frac{\Delta t}{\tau}\right)^3 N_{25}.
\end{aligned} \tag{F.2}$$

F.3. $N = 2$, correction with a DCO2 scheme, reconstruction of $g_i^{(1)}$ with a DCO2 scheme

Compared to Eq. (F.2), only the numerical errors in the momentum equation are affected as

$$\begin{aligned}
E_{\rho u_x}^{(3)} &= \left(\frac{\Delta t}{\tau}\right) N_{13} + \left(\frac{\Delta t}{\tau}\right)^2 \left(N_{17} + \frac{\rho \theta}{9} \frac{\partial^4 u_x}{\partial x^4}\right) + \left(\frac{\Delta t}{\tau}\right)^3 \left(N_{18} + \frac{1}{12} \frac{\partial^4 a_{eq,xxx}^{(3)}}{\partial x^4} - \frac{\rho \theta}{18} \frac{\partial^4 u_x}{\partial x^4}\right), \\
E_{\rho u_y}^{(3)} &= -\left(\frac{\Delta t}{\tau}\right) \frac{\rho \theta^2}{18} \frac{\partial^4 u_y}{\partial x^4} + \left(\frac{\Delta t}{\tau}\right)^2 \left(N_{24} + \frac{\rho \theta}{18} \frac{\partial^4 u_y}{\partial x^4}\right) + \left(\frac{\Delta t}{\tau}\right)^3 \left(N_{25} + \frac{1}{12} \frac{\partial^4 a_{eq,xyy}^{(3)}}{\partial x^4} - \frac{\rho \theta}{36} \frac{\partial^4 u_y}{\partial x^4}\right).
\end{aligned} \tag{F.3}$$

F.4. $N = 2$, correction with a DCO2 scheme, reconstruction of $g_i^{(1)}$ with a DUO1 scheme

Compared to Eq. (F.2), only the numerical errors in the momentum equation are affected as

$$\begin{aligned}
E_{\rho u_x}^{(2)} &= \left(\frac{\Delta t}{\tau}\right) \left(\frac{C_3}{2} - \text{sgn}(u_x) \rho c_s^2 \theta \frac{\partial^3 u_x}{\partial x^3}\right) + \left(\frac{\Delta t}{\tau}\right)^2 \left(N_1 + \text{sgn}(u_x) \frac{\rho \theta}{6} \frac{\partial^3 u_x}{\partial x^3}\right), \\
E_{\rho u_y}^{(2)} &= \left(\frac{\Delta t}{\tau}\right) \left(N_{19} - \text{sgn}(u_x) \frac{\rho \theta}{6} \frac{\partial^3 u_y}{\partial x^3}\right) + \left(\frac{\Delta t}{\tau}\right)^2 \left(N_{23} + \text{sgn}(u_x) \frac{\rho \theta}{12} \frac{\partial^3 u_y}{\partial x^3}\right),
\end{aligned}$$

$$\begin{aligned}
E_{\rho u_x}^{(3)} &= \left(\frac{\Delta t}{\tau}\right) N_{13} + \left(\frac{\Delta t}{\tau}\right)^2 \left(N_{17} + \frac{\rho\theta}{9} \frac{\partial^4 u_x}{\partial x^4} - \text{sgn}(u_x) \frac{\partial_x C_3}{4} \right) \\
&\quad + \left(\frac{\Delta t}{\tau}\right)^3 \left(N_{18} + \frac{1}{12} \frac{\partial^4 a_{eq,xxx}^{(3)}}{\partial x^4} - \frac{\rho\theta}{18} \frac{\partial^4 u_x}{\partial x^4} + \text{sgn}(u_x) \frac{\partial_x C_3}{8} \right), \\
E_{\rho u_y}^{(3)} &= -\left(\frac{\Delta t}{\tau}\right) \frac{\rho\theta^2}{18} \frac{\partial^4 u_y}{\partial x^4} + \left(\frac{\Delta t}{\tau}\right)^2 \left(N_{24} + \frac{\rho\theta}{18} \frac{\partial^4 u_y}{\partial x^4} - \text{sgn}(u_x) \frac{N_{19}}{2} \right) \\
&\quad + \left(\frac{\Delta t}{\tau}\right)^3 \left(N_{25} + \frac{1}{12} \frac{\partial^4 a_{eq,xy}^{(3)}}{\partial x^4} - \frac{\rho\theta}{36} \frac{\partial^4 u_y}{\partial x^4} + \text{sgn}(u_x) \frac{N_{19}}{4} \right). \tag{F.4}
\end{aligned}$$

F.5. $N = 2$, correction with a DUO1 scheme, reconstruction of $g_i^{(1)}$ with a DCO2 scheme

Compared to Eq. (F.2), only the numerical errors in the momentum equation are affected as

$$\begin{aligned}
E_{\rho u_x}^{(2)} &= \left(\frac{\Delta t}{2\tau}\right) C_3 + \left(\frac{\Delta t}{\tau}\right)^2 \left(N_1 - \frac{\text{sgn}(u_x)}{4} \frac{\partial^3 a_{eq,xxx}^{(3)}}{\partial x^3} \right), \\
E_{\rho u_y}^{(2)} &= \left(\frac{\Delta t}{\tau}\right) N_{19} + \left(\frac{\Delta t}{\tau}\right)^2 \left(N_{23} - \frac{\text{sgn}(u_x)}{4} \frac{\partial^3 a_{eq,xy}^{(3)}}{\partial x^3} \right), \\
E_{\rho u_x}^{(3)} &= \left(\frac{\Delta t}{\tau}\right) N_{13} + \left(\frac{\Delta t}{\tau}\right)^2 \left(N_{17} + \frac{\rho\theta}{9} \frac{\partial^4 u_x}{\partial x^4} \right) + \left(\frac{\Delta t}{\tau}\right)^3 \left(N_{18} + \frac{1}{12} \frac{\partial^4 a_{eq,xxx}^{(3)}}{\partial x^4} - \frac{\rho\theta}{18} \frac{\partial^4 u_x}{\partial x^4} + \text{sgn}(u_x) \frac{N_4}{8} \right), \\
E_{\rho u_y}^{(3)} &= -\left(\frac{\Delta t}{\tau}\right) \frac{\rho\theta^2}{18} \frac{\partial^4 u_y}{\partial x^4} + \left(\frac{\Delta t}{\tau}\right)^2 \left(N_{24} + \frac{\rho\theta}{18} \frac{\partial^4 u_y}{\partial x^4} \right) \\
&\quad + \left(\frac{\Delta t}{\tau}\right)^3 \left(N_{25} + \frac{1}{12} \frac{\partial^4 a_{eq,xy}^{(3)}}{\partial x^4} - \frac{\rho\theta}{36} \frac{\partial^4 u_y}{\partial x^4} + \text{sgn}(u_x) N_{26} \right). \tag{F.5}
\end{aligned}$$

F.6. $N = 2$, correction with a DUO1 scheme, reconstruction of $g_i^{(1)}$ with a DUO1 scheme

Compared to Eq. (F.2), only the numerical errors in the momentum equation are affected as

$$\begin{aligned}
E_{\rho u_x}^{(2)} &= \left(\frac{\Delta t}{\tau}\right) \left(\frac{C_3}{2} - \text{sgn}(u_x) \rho c_s^2 \theta \frac{\partial^3 u_x}{\partial x^3} \right) + \left(\frac{\Delta t}{\tau}\right)^2 \left(N_1 - \frac{\text{sgn}(u_x)}{4} \frac{\partial^3 a_{eq,xxx}^{(3)}}{\partial x^3} + \text{sgn}(u_x) \frac{\rho\theta}{6} \frac{\partial^3 u_x}{\partial x^3} \right), \\
E_{\rho u_y}^{(2)} &= \left(\frac{\Delta t}{\tau}\right) \left(N_{19} - \text{sgn}(u_x) \frac{\rho\theta}{6} \frac{\partial^3 u_y}{\partial x^3} \right) + \left(\frac{\Delta t}{\tau}\right)^2 \left(N_{23} + \text{sgn}(u_x) \frac{\rho\theta}{12} \frac{\partial^3 u_y}{\partial x^3} - \frac{\text{sgn}(u_x)}{4} \frac{\partial^3 a_{eq,xy}^{(3)}}{\partial x^3} \right), \\
E_{\rho u_x}^{(3)} &= \left(\frac{\Delta t}{\tau}\right) N_{13} + \left(\frac{\Delta t}{\tau}\right)^2 \left(N_{17} + \frac{\rho\theta}{9} \frac{\partial^4 u_x}{\partial x^4} - \text{sgn}(u_x) \frac{\partial_x C_3}{4} \right) \\
&\quad + \left(\frac{\Delta t}{\tau}\right)^3 \left(N_{18} + \frac{1}{12} \frac{\partial^4 a_{eq,xxx}^{(3)}}{\partial x^4} - \frac{\rho\theta}{18} \frac{\partial^4 u_x}{\partial x^4} + \frac{\text{sgn}(u_x)}{8} (N_4 + \partial_x C_3) \right), \\
E_{\rho u_y}^{(3)} &= -\left(\frac{\Delta t}{\tau}\right) \frac{\rho\theta^2}{18} \frac{\partial^4 u_y}{\partial x^4} + \left(\frac{\Delta t}{\tau}\right)^2 \left(N_{24} + \frac{\rho\theta}{18} \frac{\partial^4 u_y}{\partial x^4} - \text{sgn}(u_x) \frac{N_{19}}{2} \right) \\
&\quad + \left(\frac{\Delta t}{\tau}\right)^3 \left(N_{25} + \frac{1}{12} \frac{\partial^4 a_{eq,xy}^{(3)}}{\partial x^4} - \frac{\rho\theta}{36} \frac{\partial^4 u_y}{\partial x^4} + \text{sgn}(u_x) \left(\frac{N_{19}}{4} + N_{26} \right) \right). \tag{F.6}
\end{aligned}$$

Appendix G. Deviation terms of corrected PR and RR models

This appendix details the deviation terms of corrected PR and RR models. For the sake of simplicity, only modifications from their BGK counterpart are provided with x -derivatives only.

G.1. PR model with $N = 2$

Analytical correction:

$$E_{\rho u_y}^{(2)} = \left(C_7 + 2c_s^2 \frac{\partial^3(\rho u_x u_y)}{\partial x^3} \right) - \left(\frac{\Delta t}{\tau} \right) c_s^2 \frac{\partial^3(\rho u_x u_y)}{\partial x^3} + \left(\frac{\Delta t}{\tau} \right)^2 N_5,$$

$$E_{\rho u_y}^{(3)} = C_{12} + \left(\frac{\Delta t}{\tau} \right) N_{29} + \left(\frac{\Delta t}{\tau} \right)^2 (N_7 - N_{28}) + \left(\frac{\Delta t}{\tau} \right)^3 \frac{1}{4} N_{28}. \quad (G.1)$$

Correction with a DCO2 scheme:

$$E_{\rho u_y}^{(2)} = \left(C_7 + 2c_s^2 \frac{\partial^3(\rho u_x u_y)}{\partial x^3} \right) - \left(\frac{\Delta t}{\tau} \right) c_s^2 \frac{\partial^3(\rho u_x u_y)}{\partial x^3} + \left(\frac{\Delta t}{\tau} \right)^2 N_5,$$

$$E_{\rho u_y}^{(3)} = C_{12} + \left(\frac{\Delta t}{\tau} \right) N_{29} + \left(\frac{\Delta t}{\tau} \right)^2 \left(N_7 + \frac{1}{6} \frac{\partial^4 a_{eq,xy}^{(3)}}{\partial x^4} - N_{28} \right) + \left(\frac{\Delta t}{\tau} \right)^3 \frac{1}{4} N_{28}. \quad (G.2)$$

Correction with a DUO1 scheme:

$$E_{\rho u_y}^{(2)} = \left(C_7 + 2c_s^2 \frac{\partial^3(\rho u_x u_y)}{\partial x^3} \right) - \left(\frac{\Delta t}{\tau} \right) c_s^2 \frac{\partial^3(\rho u_x u_y)}{\partial x^3} + \left(\frac{\Delta t}{\tau} \right)^2 N_5 - \left(\frac{\Delta t}{2\tau} \right) \text{sgn}(u_x) \frac{\partial^3 a_{eq,xy}^{(3)}}{\partial x^3},$$

$$E_{\rho u_y}^{(3)} = C_{12} + \left(\frac{\Delta t}{\tau} \right) N_{29} + \left(\frac{\Delta t}{\tau} \right)^2 \left(N_7 + \frac{1}{6} \frac{\partial^4 a_{eq,xy}^{(3)}}{\partial x^4} - N_{28} \right) + \left(\frac{\Delta t}{2\tau} \right) \text{sgn}(u_x) N_9 + \left(\frac{\Delta t}{\tau} \right)^3 \frac{1}{4} N_{28}. \quad (G.3)$$

G.2. RR model with $N_r = 3^*, 4^*$ and $N = 2$

Analytical correction:

$$E_{\rho u_y}^{(2)} = \left(\frac{\Delta t}{3\tau} \right) N_{34} + \left(\frac{\Delta t}{\tau} \right)^2 N_{35}, \quad E_{\rho u_y}^{(3)} = -\frac{\rho\theta^2}{9} \frac{\partial^4 u_y}{\partial x^4} + \left(\frac{\Delta t}{\tau} \right) N_{36} + \left(\frac{\Delta t}{\tau} \right)^2 (N_7 - N_{37}) + \left(\frac{\Delta t}{\tau} \right)^3 N_{38}, \quad (G.4)$$

where

$$N_{38} |_{(u_y=0)} = (1 - \theta) \frac{\rho u_x^2}{12} \frac{\partial^4 u_y}{\partial x^4}. \quad (G.5)$$

Correction with a DCO2 scheme:

$$E_{\rho u_y}^{(2)} = \left(\frac{\Delta t}{3\tau} \right) N_{34} + \left(\frac{\Delta t}{\tau} \right)^2 N_{35},$$

$$E_{\rho u_y}^{(3)} = -\frac{\rho\theta^2}{9} \frac{\partial^4 u_y}{\partial x^4} + \left(\frac{\Delta t}{\tau} \right) N_{36} + \left(\frac{\Delta t}{\tau} \right)^2 \left(N_7 + \frac{1}{6} \frac{\partial^4 a_{eq,xy}^{(3)}}{\partial x^4} - N_{37} \right) + \left(\frac{\Delta t}{\tau} \right)^3 N_{38}. \quad (G.6)$$

Correction with a DUO1 scheme:

$$E_{\rho u_y}^{(2)} = \left(\frac{\Delta t}{3\tau} \right) N_{34} + \left(\frac{\Delta t}{\tau} \right)^2 N_{35} - \left(\frac{\Delta t}{2\tau} \right) \text{sgn}(u_x) \frac{\partial^3 a_{eq,xy}^{(3)}}{\partial x^3},$$

$$E_{\rho u_y}^{(3)} = -\frac{\rho\theta^2}{9} \frac{\partial^4 u_y}{\partial x^4} + \left(\frac{\Delta t}{\tau} \right) (N_{36} + \text{sgn}(u_x) \partial_x C_{13}) + \left(\frac{\Delta t}{\tau} \right)^2 \left(N_7 + \frac{1}{6} \frac{\partial^4 a_{eq,xy}^{(3)}}{\partial x^4} - N_{37} + \text{sgn}(u_x) N_{39} \right) + \left(\frac{\Delta t}{\tau} \right)^3 N_{38}. \quad (G.7)$$

G.3. PR model with $N = 3^*, 4^*$

Analytical correction:

$$E_{\rho u_y}^{(2)} = 2\rho c_s^2 \theta \frac{\partial^3(u_x u_y)}{\partial x^3} - \left(\frac{\Delta t}{2\tau}\right) C_{15} + \left(\frac{\Delta t}{\tau}\right)^2 N_{15},$$

$$E_{\rho u_y}^{(3)} = C_{17} + \left(\frac{\Delta t}{\tau}\right) N_{43} + \left(\frac{\Delta t}{\tau}\right)^2 (N_8 + N_{41}) + \left(\frac{\Delta t}{\tau}\right)^3 N_{42}. \quad (\text{G.8})$$

Correction with a DCO2 scheme:

$$E_{\rho u_y}^{(2)} = 2\rho c_s^2 \theta \frac{\partial^3(u_x u_y)}{\partial x^3} - \left(\frac{\Delta t}{2\tau}\right) C_{15} + \left(\frac{\Delta t}{\tau}\right)^2 N_{15},$$

$$E_{\rho u_y}^{(3)} = C_{17} + \left(\frac{\Delta t}{\tau}\right) N_{43} + \left(\frac{\Delta t}{\tau}\right)^2 (N_8 + N_{41}) + \left(\frac{\Delta t}{\tau}\right)^3 N_{42}. \quad (\text{G.9})$$

Correction with a DUO1 scheme:

$$E_{\rho u_y}^{(2)} = 2\rho c_s^2 \theta \frac{\partial^3(u_x u_y)}{\partial x^3} - \left(\frac{\Delta t}{2\tau}\right) C_{15} + \left(\frac{\Delta t}{\tau}\right)^2 N_{15},$$

$$E_{\rho u_y}^{(3)} = C_{17} + \left(\frac{\Delta t}{\tau}\right) N_{43} - \left(\frac{\Delta t}{2\tau}\right) \text{sgn}(u_x) u_y \frac{\partial^4 a_{eq.xxx}^{(3)}}{\partial x^4} + \left(\frac{\Delta t}{\tau}\right)^2 (N_8 + N_{41}) + \left(\frac{\Delta t}{\tau}\right)^3 N_{42}. \quad (\text{G.10})$$

G.4. RR model with $N_r = 3^*, 4^*$ and $N = 3^*, 4^*$

Analytical correction:

$$E_{\rho u_y}^{(2)} = \left(\frac{\Delta t}{2\tau}\right) \frac{\partial^3(u_y a_{eq.xxx}^{(3)})}{\partial x^3} + \left(\frac{\Delta t}{\tau}\right)^2 N_{15},$$

$$E_{\rho u_y}^{(3)} = -\frac{\rho\theta^2}{9} \frac{\partial^4 u_y}{\partial x^4} + \left(\frac{\Delta t}{\tau}\right) N_{45} + \left(\frac{\Delta t}{\tau}\right)^2 (N_8 + N_{46}) + \left(\frac{\Delta t}{\tau}\right)^3 N_{47}. \quad (\text{G.11})$$

For a horizontal mean flow, the degenerating hyperviscosity behaves as

$$N_{47}|_{(u_y=0)} = N_{44} = -\frac{1}{8} \rho (u_x^4 + (\theta - 1)u_x^2) \frac{\partial^4 u_y}{\partial x^4}. \quad (\text{G.12})$$

Correction with a DCO2 scheme:

$$E_{\rho u_y}^{(2)} = \left(\frac{\Delta t}{2\tau}\right) \frac{\partial^3(u_y a_{eq.xxx}^{(3)})}{\partial x^3} + \left(\frac{\Delta t}{\tau}\right)^2 N_{15},$$

$$E_{\rho u_y}^{(3)} = -\frac{\rho\theta^2}{9} \frac{\partial^4 u_y}{\partial x^4} + \left(\frac{\Delta t}{\tau}\right) N_{45} + \left(\frac{\Delta t}{\tau}\right)^2 (N_8 + N_{46}) + \left(\frac{\Delta t}{\tau}\right)^3 N_{47}. \quad (\text{G.13})$$

Correction with a DUO1 scheme:

$$E_{\rho u_y}^{(2)} = \left(\frac{\Delta t}{2\tau}\right) \frac{\partial^3(u_y a_{eq.xxx}^{(3)})}{\partial x^3} + \left(\frac{\Delta t}{\tau}\right)^2 N_{15},$$

$$E_{\rho u_y}^{(3)} = -\frac{\rho\theta^2}{9} \frac{\partial^4 u_y}{\partial x^4} + \left(\frac{\Delta t}{\tau}\right) N_{45} + \left(\frac{\Delta t}{\tau}\right)^2 (N_8 + N_{46}) - \text{sgn}(u_x) \left(\frac{\Delta t}{\tau}\right)^2 \frac{u_y}{4} \frac{\partial^4 a_{eq.xxx}^{(3)}}{\partial x^4} + \left(\frac{\Delta t}{\tau}\right)^3 N_{47}. \quad (\text{G.14})$$

Appendix H. Deviation terms

H.1. Consistency errors with the isothermal NS equations

$$C_1 = -\left(3u_x^4 + (4\theta - 3)u_x^2 + \theta^2/9 - \theta/3\right) \frac{\partial^3 \rho}{\partial x^3} - \left(10\rho u_x^3 + (2\theta - 4)\rho u_x\right) \frac{\partial^3 u_x}{\partial x^3},$$

$$\begin{aligned}
C_2 &= -\frac{1}{3} \left(36u_x^5 + (56\theta - 39)u_x^3 + (4\theta^2 - 11\theta + 3)u_x \right) \frac{\partial^4 \rho}{\partial x^4} \\
&\quad - \frac{1}{9} \left(378u_x^4 + (108\theta - 189)u_x^2 + 2\theta^2 - 9\theta + 9 \right) \rho \frac{\partial^4 u_x}{\partial x^4}, \\
C_3 &= \frac{2\theta^2}{9} \frac{\partial^3 \rho}{\partial x^3} + 2\rho\theta u_x \frac{\partial^3 u_x}{\partial x^3}, \quad C_4 = \frac{4}{3}\theta^2 u_x \frac{\partial^4 \rho}{\partial x^4} + \frac{1}{9} \left(54\theta u_x^2 - 2\theta^2 \right) \rho \frac{\partial^4 u_x}{\partial x^4}, \\
C_5 &= - \left(3u_x^3 + (7c_s^2\theta - 1)u_x \right) u_y \frac{\partial^3 \rho}{\partial x^3} - \left(8u_x^2 + 2c_s^2(\theta - 1) \right) \rho u_y \frac{\partial^3 u_x}{\partial x^3} - 2\rho u_x^3 \frac{\partial^3 u_y}{\partial x^3}, \\
C_6 &= -\frac{1}{9} \left(108u_x^4 + (123\theta - 57)u_x^2 + 3\theta^2 - 2\theta - 1 \right) u_y \frac{\partial^4 \rho}{\partial x^4} \\
&\quad - \frac{1}{3} \left(111u_x^3 + (19\theta - 19)u_x \right) \rho u_y \frac{\partial^4 u_x}{\partial x^4} - \frac{1}{9} \left(45u_x^4 + 6u_x^2 - 1 \right) \rho \frac{\partial^4 u_y}{\partial x^4}, \\
C_7 &= \frac{2}{3} \left(-u_x u_y \frac{\partial^3 \rho}{\partial x^3} + \rho(\theta - 1) \left(u_y \frac{\partial^3 u_x}{\partial x^3} + u_x \frac{\partial^3 u_y}{\partial x^3} \right) \right), \\
C_8 &= -\frac{1}{9} \left(18u_x^2 - 4\theta^2 + 4\theta \right) u_y \frac{\partial^4 \rho}{\partial x^4} + 10\rho c_s^2(\theta - 1)u_x u_y \frac{\partial^4 u_x}{\partial x^4} + \frac{1}{9} \left((12\theta - 18)u_x^2 - \theta^2 + 2\theta \right) \rho \frac{\partial^4 u_y}{\partial x^4}, \\
C_9 &= \left(3u_x^4 + (2\theta - 3)u_x^2 - 2c_s^4\theta^2 + c_s^2\theta \right) \rho \frac{\partial^4 u_y}{\partial x^4}, \\
C_{10} &= \frac{1}{3} \left(9u_x^4 + (15\theta - 9)u_x^2 + 2\theta^2 - 2\theta \right) u_y \frac{\partial^4 \rho}{\partial x^4} + (11u_x^3 + 5(\theta - 1)u_x) \rho u_y \frac{\partial^4 u_x}{\partial x^4} \\
&\quad + \frac{1}{9} \left(27u_x^4 + (18\theta - 27)u_x^2 - 2\theta^2 + 3\theta \right) \rho \frac{\partial^4 u_y}{\partial x^4}, \\
C_{11} &= C_6 + \frac{1}{9} \left((24u_x^2 + 6\theta - 2)u_y \frac{\partial^4 \rho}{\partial x^4} + 42\rho u_x u_y \frac{\partial^4 u_x}{\partial x^4} + (24u_x^2 - 2)\rho \frac{\partial^4 u_y}{\partial x^4} \right), \\
C_{12} &= C_8 + \frac{1}{9} \left((18u_x^2 + 4\theta)u_y \frac{\partial^4 \rho}{\partial x^4} + 30\rho u_x u_y \frac{\partial^4 u_x}{\partial x^4} + (18u_x^2 - 2\theta)\rho \frac{\partial^4 u_y}{\partial x^4} \right), \\
C_{13} &= -2c_s^2\theta u_x u_y \frac{\partial^3 \rho}{\partial x^3} - (u_x^2 + c_s^2(\theta - 1))\rho u_y \frac{\partial^3 u_x}{\partial x^3}, \\
C_{14} &= -\frac{1}{9} (27u_x^4 + (24\theta - 24)u_x^2 + \theta^2 - 2\theta + 1) u_y \frac{\partial^4 \rho}{\partial x^4} - \frac{1}{3} (24u_x^3 + (4\theta - 8)u_x) \rho u_y \frac{\partial^4 u_x}{\partial x^4} \\
&\quad - \frac{1}{9} (9u_x^4 - 6u_x^2 + 1) \rho \frac{\partial^4 u_y}{\partial x^4}, \\
C_{15} &= -(u_x^3 + (\theta - 1)u_x) u_y \frac{\partial^3 \rho}{\partial x^3} - (3u_x^2 + c_s^2\theta - 1) \rho u_y \frac{\partial^3 u_x}{\partial x^3} - (u_x^3 + (c_s^2\theta - 1)u_x) \rho \frac{\partial^3 u_y}{\partial x^3}, \\
C_{16} &= \frac{1}{3} \left((-15u_x^4 + (15 - 21\theta)u_x^2 - 2c_s^2\theta^2 + 2\theta) u_y \frac{\partial^4 \rho}{\partial x^4} + ((21 - 11\theta)u_x - 51u_x^3) \rho u_y \frac{\partial^4 u_x}{\partial x^4} \right. \\
&\quad \left. + (4\theta u_x^2 - c_s^2\theta^2) \rho \frac{\partial^4 u_y}{\partial x^4} \right), \\
C_{17} &= \frac{4}{9}\theta^2 u_y \frac{\partial^4 \rho}{\partial x^4} + 10\rho c_s^2\theta u_x u_y \frac{\partial^4 u_x}{\partial x^4} + \frac{1}{9} (12\theta u_x^2 - \theta^2) \rho \frac{\partial^4 u_y}{\partial x^4},
\end{aligned}$$

H.2. Numerical errors

$$\begin{aligned}
N_1 &= \frac{1}{54} \left(9u_x^4 + (18\theta - 9)u_x^2 + \theta^2 - 3\theta \right) \frac{\partial^3 \rho}{\partial x^3} + \frac{1}{9} \left(6u_x^3 + (2\theta - 3)u_x \right) \rho \frac{\partial^3 u_x}{\partial x^3}, \\
N_2 &= \frac{1}{108} \left((162u_x^5 + (300\theta - 171)u_x^3 + (26\theta^2 - 63\theta + 9)u_x) \frac{\partial^4 \rho}{\partial x^4} \right. \\
&\quad \left. + (612u_x^4 + (216\theta - 315)u_x^2 + 4\theta^2 - 15\theta + 9) \rho \frac{\partial^4 u_x}{\partial x^4} \right),
\end{aligned}$$

$$\begin{aligned}
N_3 &= \frac{1}{108} \left((54u_x^5 + (108\theta - 45)u_x^3 + (-10\theta^2 - 9\theta - 9)u_x) \frac{\partial^4 \rho}{\partial x^4} + (216u_x^4 - 81u_x^2 - 8\theta^2 + 15\theta - 9) \rho \frac{\partial^4 u_x}{\partial x^4} \right), \\
N_4 &= (-3u_x^4 + (3 - 4\theta)u_x^2 - \theta^2/3 + \theta/3) \frac{\partial^4 \rho}{\partial x^4} + (-10u_x^3 + (4 - 4\theta)u_x) \rho \frac{\partial^3 u_x}{\partial x^3}, \\
N_5 &= \frac{1}{6} \left((u_x^3 + \theta u_x) u_y \frac{\partial^3 \rho}{\partial x^3} + (3u_x^2 + c_s^2 \theta) \rho u_y \frac{\partial^3 u_x}{\partial x^3} + \rho u_x^3 \frac{\partial^3 u_y}{\partial x^3} \right), \\
N_6 &= \frac{1}{36} \left((54u_x^4 + (71\theta - 21)u_x^2 + 7c_s^2 \theta^2 - 2c_s^2 \theta - 1) u_y \frac{\partial^4 \rho}{\partial x^4} + (177u_x^3 + (37\theta - 21)u_x) \rho u_y \frac{\partial^4 u_x}{\partial x^4} \right. \\
&\quad \left. + (27u_x^4 + 6u_x^2 - 1) \rho \frac{\partial^4 u_y}{\partial x^4} \right), \\
N_7 &= \frac{1}{108} (54u_x^4 + (81\theta + 9)u_x^2 - \theta^2 + 6\theta - 3) u_y \frac{\partial^4 \rho}{\partial x^4} + \frac{1}{12} (21u_x^3 + (\theta + 3)u_x) \rho u_y \frac{\partial^4 u_x}{\partial x^4} \\
&\quad + \frac{1}{36} (9u_x^4 + (12 - 6\theta)u_x^2 - 1) \rho \frac{\partial^4 u_y}{\partial x^4}, \\
N_8 &= -\frac{1}{108} (27u_x^4 + (54\theta - 27)u_x^2 + 7\theta^2 - 9\theta) u_y \frac{\partial^4 \rho}{\partial x^4} - \frac{1}{6} (6u_x^3 + (2\theta - 3)u_x) \rho u_y \frac{\partial^4 u_x}{\partial x^4} \\
&\quad - \frac{1}{36} (18u_x^4 + (12\theta - 18)u_x^2 - \theta^2 + 2\theta) \rho \frac{\partial^4 u_y}{\partial x^4}, \\
N_9 &= -\frac{1}{3} \left((9u_x^3 + (7\theta - 5)u_x) u_y \frac{\partial^4 \rho}{\partial x^4} + (24u_x^2 + 4\theta - 4) \rho u_y \frac{\partial^4 u_x}{\partial x^4} + (6u_x^3 + 2(\theta - 1)u_x) \rho \frac{\partial^4 u_y}{\partial x^4} \right), \\
N_{10} &= -\frac{1}{108} (27u_x^4 + (36\theta - 27)u_x^2 + \theta^2 - 3\theta) u_y \frac{\partial^4 \rho}{\partial x^4} - \frac{1}{6} (5u_x^3 + (\theta - 2)u_x) \rho u_y \frac{\partial^4 u_x}{\partial x^4} \\
&\quad - \frac{1}{36} (18u_x^4 + (12\theta - 18)u_x^2 - \theta^2 + 2\theta) \rho \frac{\partial^4 u_y}{\partial x^4}, \\
N_{11} &= -\frac{1}{108} (63u_x^4 + (72\theta - 63)u_x^2 + 7\theta^2 - 3\theta) \frac{\partial^3 \rho}{\partial x^3} - \frac{1}{18} (33u_x^3 + (14\theta - 12)u_x) \rho \frac{\partial^3 u_x}{\partial x^3}, \\
N_{12} &= -\frac{1}{72} \left((9u_x^4 + (12\theta - 9)u_x^2 + \theta^2 - \theta) \frac{\partial^4 \rho}{\partial x^4} + (30u_x^3 + (12\theta - 12)u_x) \rho \frac{\partial^4 u_x}{\partial x^4} \right), \\
N_{13} &= -\frac{2}{9} \rho \theta^2 \frac{\partial^4 u_x}{\partial x^4}, \quad N_{14} = \frac{1}{54} \left((9\theta u_x^2 + 19\theta^2 - 9\theta) u_x \frac{\partial^4 \rho}{\partial x^4} + (99\theta u_x^2 + 17\theta^2 - 12\theta) \rho \frac{\partial^4 u_x}{\partial x^4} \right), \\
N_{15} &= -\frac{1}{36} \left((3u_x^3 + 3(\theta - 1)u_x) u_y \frac{\partial^3 \rho}{\partial x^3} + (9u_x^2 + \theta - 3) \rho u_y \frac{\partial^3 u_x}{\partial x^3} + (3u_x^3 + 3(\theta - 1)u_x) \rho \frac{\partial^3 u_y}{\partial x^3} \right), \\
N_{16} &= -\frac{1}{36} \left((27u_x^5 + (37\theta - 30)u_x^3 + (8\theta^2 - 9\theta + 3)u_x) \frac{\partial^4 \rho}{\partial x^4} + (87u_x^4 + (51\theta - 42)u_x^2 + 4\theta^2 - 6\theta + 3) \rho \frac{\partial^4 u_x}{\partial x^4} \right), \\
N_{17} &= \frac{1}{54} \left(10\theta^2 u_x \frac{\partial^4 \rho}{\partial x^4} + (45\theta u_x^2 - \theta^2 + 6\theta) \rho \frac{\partial^4 u_x}{\partial x^4} \right), \\
N_{18} &= \frac{1}{72} \left((18u_x^5 + (36\theta - 15)u_x^3 + (2\theta^2 - 3\theta - 3)u_x) \frac{\partial^4 \rho}{\partial x^4} + (72u_x^4 + (24\theta - 27)u_x^2 + \theta - 3) \rho \frac{\partial^4 u_x}{\partial x^4} \right), \\
N_{19} &= \rho c_s^2 \theta \frac{\partial^3 (u_x u_y)}{\partial x^3}, \\
N_{20} &= -\frac{1}{12} (7u_x^3 + (5\theta - 3)u_x) u_y \frac{\partial^3 \rho}{\partial x^3} - \frac{1}{18} (27u_x^2 + 5\theta - 3) \rho u_y \frac{\partial^3 u_x}{\partial x^3} - \frac{1}{6} (2u_x^3 + \theta u_x) \rho \frac{\partial^3 u_y}{\partial x^3}, \\
N_{21} &= \frac{1}{108} (9\theta u_x^2 + 11\theta^2 - 3\theta) u_y \frac{\partial^4 \rho}{\partial x^4} + \rho \theta u_x u_y \frac{\partial^4 u_x}{\partial x^4} + \frac{1}{18} (6\theta u_x^2 + \theta^2) \rho \frac{\partial^4 u_y}{\partial x^4}, \\
N_{22} &= -\frac{1}{216} (162u_x^4 + (165\theta - 108)u_x^2 + 13\theta^2 - 7\theta) u_y \frac{\partial^4 \rho}{\partial x^4} - \frac{1}{18} (39u_x^3 + (14\theta - 9)u_x) \rho u_y \frac{\partial^4 u_x}{\partial x^4}
\end{aligned}$$

$$\begin{aligned}
& -\frac{1}{72}(18u_x^4 + 12\theta u_x^2 + \theta^2)\rho \frac{\partial^4 u_y}{\partial x^4}, \\
N_{23} &= \frac{1}{6}(u_x^3 + (\theta - 1)u_x)u_y \frac{\partial^3 \rho}{\partial x^3} + \frac{1}{18}(9u_x^2 + \theta - 3)\rho u_y \frac{\partial^3 u_x}{\partial x^3} + \frac{1}{6}(u_x^3 - u_x)\rho \frac{\partial^3 u_y}{\partial x^3}, \\
N_{24} &= \frac{2}{27}\theta^2 u_y \frac{\partial^4 \rho}{\partial x^4} + \frac{\rho\theta}{2}u_x u_y \frac{\partial^4 u_x}{\partial x^4} + \frac{\rho\theta}{18}(3u_x^2 + 1) \frac{\partial^4 u_y}{\partial x^4}, \\
N_{25} &= \frac{1}{72}\left((18u_x^4 + (27\theta - 15)u_x^2 + \theta^2 - 2\theta - 1)u_y \frac{\partial^4 \rho}{\partial x^4} + (63u_x^3 + (15\theta - 21)u_x)\rho u_y \frac{\partial^4 u_x}{\partial x^4}\right. \\
& \quad \left.+ (9u_x^4 - 6u_x^2 - 1)\rho \frac{\partial^4 u_y}{\partial x^4}\right), \\
N_{26} &= -\frac{1}{24}\left((9u_x^3 + (7\theta - 5)u_x)u_y \frac{\partial^4 \rho}{\partial x^4} + (24u_x^2 + 4(\theta - 1))\rho u_y \frac{\partial^4 u_x}{\partial x^4} + (6u_x^3 + 2(\theta - 1)u_x)\rho \frac{\partial^4 u_y}{\partial x^4}\right), \\
N_{27} &= -\frac{1}{9}\left((9u_x^2 + 2\theta - 1)u_y \frac{\partial^4 \rho}{\partial x^4} + 15\rho u_x u_y \frac{\partial^4 u_x}{\partial x^4} + (9u_x^2 - 1)\rho \frac{\partial^4 u_y}{\partial x^4}\right), \\
N_{28} &= \frac{1}{9}\left((3u_x^2 + \theta)u_y \frac{\partial^4 \rho}{\partial x^4} + 6\rho u_x u_y \frac{\partial^4 u_x}{\partial x^4} + 3\rho u_x^2 \frac{\partial^4 u_y}{\partial x^4}\right), \\
N_{29} &= -\frac{1}{9}\left((6u_x^2 + \theta)u_y \frac{\partial^4 \rho}{\partial x^4} + 9\rho u_x u_y \frac{\partial^4 u_x}{\partial x^4} + (6u_x^2 - \theta)\rho \frac{\partial^4 u_y}{\partial x^4}\right), \\
N_{30} &= -\frac{1}{6}\left((9u_x^3 + (5\theta - 3)u_x)u_y \frac{\partial^3 \rho}{\partial x^3} + (21u_x^2 + \theta - 1)\rho u_y \frac{\partial^3 u_x}{\partial x^3} + 6\rho u_x^3 \frac{\partial^3 u_y}{\partial x^3}\right), \\
N_{31} &= \frac{1}{18}\left(-((33\theta - 6)u_x^2 + \theta^2 + \theta - 2)u_y \frac{\partial^4 \rho}{\partial x^4} - (45u_x^3 + (21\theta - 15)u_x)\rho u_y \frac{\partial^4 u_x}{\partial x^4} + (18u_x^4 - 12u_x^2 + 2)\rho \frac{\partial^4 u_y}{\partial x^4}\right), \\
N_{32} &= \frac{1}{18}\left((-54u_x^4 + (-51\theta + 18)u_x^2 - \theta^2 + \theta)u_y \frac{\partial^4 \rho}{\partial x^4} + (-153u_x^3 + (-21\theta + 15)u_x)\rho u_y \frac{\partial^4 u_x}{\partial x^4} - 36\rho u_x^4 \frac{\partial^4 u_y}{\partial x^4}\right), \\
N_{33} &= \frac{1}{72}\left((27u_x^4 + (36\theta - 9)u_x^2 + \theta^2 - \theta)u_y \frac{\partial^4 \rho}{\partial x^4} + (90u_x^3 + (18\theta - 12)u_x)\rho u_y \frac{\partial^4 u_x}{\partial x^4} + 18\rho u_x^4 \frac{\partial^4 u_y}{\partial x^4}\right), \\
N_{34} &= -u_x u_y \frac{\partial^3 \rho}{\partial x^3} + (\theta - 1)\rho u_y \frac{\partial^3 u_x}{\partial x^3} + (\theta - 1)\rho u_x \frac{\partial^3 u_y}{\partial x^3}, \\
N_{35} &= \frac{1}{6}\left((u_x^3 + \theta u_x)u_y \frac{\partial^3 \rho}{\partial x^3} + (3u_x^2 + c_s^2 \theta)\rho u_y \frac{\partial^3 u_x}{\partial x^3} + \rho u_x^3 \frac{\partial^3 u_y}{\partial x^3}\right), \\
N_{36} &= \frac{1}{9}(\theta^2 - \theta)u_y \frac{\partial^4 \rho}{\partial x^4} + \frac{1}{3}(2\theta - 1)\rho u_x u_y \frac{\partial^4 u_x}{\partial x^4} + \frac{1}{9}(1 - 3u_x^2)\rho \theta \frac{\partial^4 u_y}{\partial x^4}, \\
N_{37} &= \frac{1}{9}(6u_x^2 - \theta^2 + \theta)u_y \frac{\partial^4 \rho}{\partial x^4} + \frac{1}{3}(-2\theta + 3)\rho u_x u_y \frac{\partial^4 u_x}{\partial x^4} + \frac{2}{3}(1 - \theta)\rho u_x^2 \frac{\partial^4 u_y}{\partial x^4}, \\
N_{38} &= \frac{1}{36}(3u_x^2 - \theta^2 + \theta)u_y \frac{\partial^4 \rho}{\partial x^4} + \frac{1}{12}(2 - \theta)\rho u_x u_y \frac{\partial^4 u_x}{\partial x^4} + (1 - \theta)\frac{\rho u_x^2}{12} \frac{\partial^4 u_y}{\partial x^4}, \\
N_{39} &= -\frac{1}{12}\left((9u_x^3 + (5\theta - 5)u_x)u_y \frac{\partial^4 \rho}{\partial x^4} + (21u_x^2 + 3(\theta - 1))\rho u_y \frac{\partial^4 u_x}{\partial x^4} + (6u_x^3 + 2(\theta - 1)u_x)\rho \frac{\partial^4 u_y}{\partial x^4}\right), \\
N_{40} &= \frac{1}{6}\left((12u_x^4 + (15\theta - 12)u_x^2 + c_s^2 \theta^2 - \theta)u_y \frac{\partial^4 \rho}{\partial x^4} + (39u_x^3 + (7\theta - 15)u_x)\rho u_y \frac{\partial^4 u_x}{\partial x^4}\right. \\
& \quad \left.+ (6u_x^4 + (\theta - 6)u_x^2 - c_s^2 \theta^2 + \theta)\rho \frac{\partial^4 u_y}{\partial x^4}\right), \\
N_{41} &= \frac{1}{18}\left((9u_x^4 + (18\theta - 9)u_x^2 + \theta^2 - 3\theta)u_y \frac{\partial^4 \rho}{\partial x^4} + (36u_x^3 + (12\theta - 18)u_x)\rho u_y \frac{\partial^4 u_x}{\partial x^4}\right)
\end{aligned}$$

$$\begin{aligned}
& + (9u_x^4 + (3\theta - 9)u_x^2)\rho \frac{\partial^4 u_y}{\partial x^4} \Big), \\
N_{42} = & \frac{1}{24} \left((-3u_x^4 + (-6\theta + 3)u_x^2 - c_s^2\theta^2 + \theta)u_y \frac{\partial^4 \rho}{\partial x^4} + (-12u_x^3 + (-4\theta + 6)u_x)\rho u_y \frac{\partial^4 u_x}{\partial x^4} \right. \\
& \left. + (-3u_x^4 + (3 - \theta)u_x^2)\rho \frac{\partial^4 u_y}{\partial x^4} \right), \\
N_{43} = & \frac{1}{18} \left(\frac{\partial^4 \rho}{\partial x^4} (18u_x^4 + (27\theta - 18)u_x^2 + \theta^2 - 3\theta)u_y + (63u_x^3 + (3\theta - 27)u_x)\rho u_y \frac{\partial^4 u_x}{\partial x^4} \right. \\
& \left. + (18u_x^4 + (3\theta - 18)u_x^2 - \theta^2 + 3\theta)\rho \frac{\partial^4 u_y}{\partial x^4} \right), \\
N_{44} = & -\frac{1}{8}\rho(u_x^4 + (\theta - 1)u_x^2) \frac{\partial^4 u_y}{\partial x^4}, \\
N_{45} = & \frac{1}{6} \left((3\theta u_x^2 + \theta^2 - \theta)u_y \frac{\partial^4 \rho}{\partial x^4} + (3u_x^3 + 3(\theta - 1)u_x)\rho u_y \frac{\partial^4 u_x}{\partial x^4} + (-3\theta u_x^2 - c_s^2\theta^2 + \theta)\rho \frac{\partial^4 u_y}{\partial x^4} \right), \\
N_{46} = & \frac{1}{2} \left((2u_x^4 + (3\theta - 2)u_x^2 + c_s^2\theta^2 - c_s^2\theta)u_y \frac{\partial^4 \rho}{\partial x^4} + (7u_x^3 + 3(\theta - 1)u_x)u_y \frac{\partial^4 u_x}{\partial x^4} + (2u_x^4 + 2(\theta - 1)u_x^2)\rho \frac{\partial^4 u_y}{\partial x^4} \right), \\
N_{47} = & \frac{1}{8} \left((-u_x^4 + (-2\theta + 1)u_x^2 - c_s^2\theta^2 + c_s^2\theta)u_y \frac{\partial^4 \rho}{\partial x^4} + (-4u_x^3 + (-2\theta + 2)u_x)\rho u_y \frac{\partial^4 u_x}{\partial x^4} \right. \\
& \left. - (u_x^4 + (\theta - 1)u_x^2)\rho \frac{\partial^4 u_y}{\partial x^4} \right).
\end{aligned}$$

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