

Imaging of coherent fields through lenslike systems

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I derive the imaging condition for the complex amplitude of a monochromatic field by a sequence of lenslike elements.

In this Letter I consider the problem of imaging a *coherent* electromagnetic field by a general axisymmetric lenslike system, as illustrated in Fig. 1. The individual elements that compose the system are each describable by an *ABCD* ray matrix, and the propagation between the input plane (x_0, y_0) and the output plane (x_1, y_1) is thus governed by the overall system matrix:

$$\begin{vmatrix} A & B \\ C & D \end{vmatrix} = \begin{vmatrix} A_n & B_n \\ C_n & D_n \end{vmatrix} \cdots \begin{vmatrix} A_1 & B_1 \\ C_1 & D_1 \end{vmatrix}. \quad (1)$$

In an important extension of the eikonal formalism, Baues¹ and Collins² showed that the output and input complex fields in our problem are related by

$$f_1(x_1, y_1) = \frac{ik}{2\pi B} \exp(-ikL) \iint_{x_0} f_0(x_0, y_0) \exp\left[\left(-\frac{ik}{2B}\right) \left[D(x_1^2 + y_1^2) - 2x_1x_0 - 2y_1y_0 + A(x_0^2 + y_0^2) \right]\right] dx_0 dy_0. \quad (2)$$

By rearranging and manipulating the exponent we can rewrite Eq. (2) as

$$\begin{aligned} f_1(x_1, y_1) &= \frac{ik}{2\pi B} \exp\left[\left(-\frac{ik}{2B}\right) \left(D - \frac{1}{A}\right) (x_1^2 + y_1^2)\right] \\ &\times \int \int_{x_0} f_0(x_0, y_0) \exp\left[\left(-\frac{ik}{2B}\right) \right. \\ &\times \left. \left[A\left(x_0 - \frac{x_1}{A}\right)^2 + A\left(y_0 - \frac{y_1}{A}\right)^2 \right]\right] dx_0 dy_0. \end{aligned} \quad (3)$$

Here I consider the function $\exp[-(ikA/2B)(x_0 - x_1/A)^2]$.

I will show formally, at the end of this Letter, that

$$Y(x) \equiv \lim_{B \rightarrow 0} \sqrt{\frac{i}{2\pi B}} \exp\left(-i\frac{x^2}{2B}\right) = \delta(x), \quad (4)$$

where $\delta(x)$ is the Dirac delta function, so that in the limit $B \rightarrow 0$

$$\begin{aligned} f_1(x_1, y_1) &= \frac{\exp(-ikL)}{A} f_0\left(\frac{x_1}{A}, \frac{y_1}{A}\right) \\ &\times \exp\left[-i\frac{k(DA-1)}{2AB} (x_1^2 + y_1^2)\right]. \end{aligned} \quad (5)$$

In the case of a lossless system, $AD - BC = 1$, so that Eq. (5) can be written as

$$\begin{aligned} f_1(x_1, y_1) &= \frac{\exp(-ikL)}{A} f_0\left(\frac{x_1}{A}, \frac{y_1}{A}\right) \\ &\times \exp\left[-i\frac{kC}{2A} (x_1^2 + y_1^2)\right]. \end{aligned} \quad (6)$$

Equation (6) is the central result of this Letter. It shows that when $B = 0$ the output is an exact, scaled replica of the input field except for a quadratic phase factor.^{3,4} The image magnification is A . The generalized imaging condition is thus $B = 0$.^{5,6}

As an example, I apply the formalism to the simple case of imaging by a single thin lens, as illustrated in Fig. 2. In this case,

$$\begin{aligned} \begin{vmatrix} A & B \\ C & D \end{vmatrix} &= \begin{vmatrix} 1 & d_i \\ 0 & 1 \end{vmatrix} \begin{vmatrix} -\frac{1}{f} & 0 \\ 0 & 1 \end{vmatrix} \begin{vmatrix} 1 & d_o \\ 0 & 1 \end{vmatrix} \\ &= \begin{vmatrix} 1 - \frac{d_i}{f} & d_o d_i \left(\frac{1}{d_o} + \frac{1}{d_i} - \frac{1}{f}\right) \\ -\frac{1}{f} & 1 - \frac{d_o}{f} \end{vmatrix}. \end{aligned} \quad (7)$$

The imaging condition $B = 0$ in this case assumes the familiar form of geometrical optics,

$$\frac{1}{f} = \frac{1}{d_o} + \frac{1}{d_i}, \quad (8)$$

from which it follows directly that $A = 1 - d_i/f = -d_i/d_o = -M$, where $M \equiv d_i/d_o$ is the magnification factor. In a similar fashion I show that $C/A = M/f$ and $D = -M^{-1}$, so that

$$\begin{aligned} f_1(x, y) &= -\frac{1}{M} \exp\left[-i\left[kL + \frac{k(x^2 + y^2)}{2Mf}\right]\right] \\ &\times f_0\left(-\frac{x}{M}, -\frac{y}{M}\right). \end{aligned} \quad (9)$$

This special case reduces to a result given by Goodman.⁷ Another special case of imaging by a quadratic index fiber is considered in Ref. 5. I have thus derived the imaging relation for a coherent electromagnetic field by a system of lenslike elements.

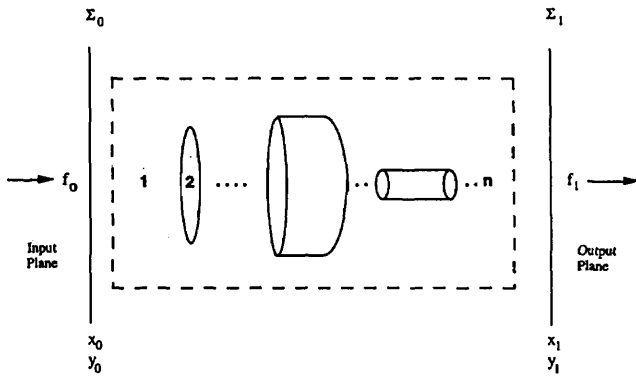


Fig. 1. Generalized lenslike system.

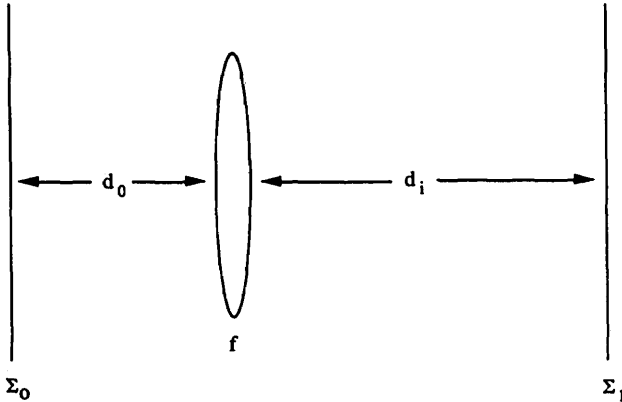


Fig. 2. Imaging by a thin lens.

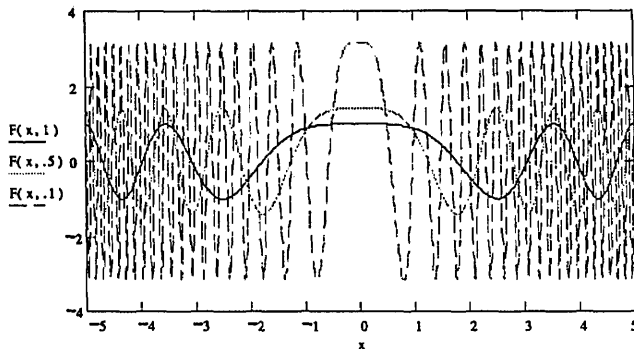


Fig. 3. Function $F(x, B) = (2\pi B)^{-1/2} \cos(x^2/2B)$ for $B = 1, 0.5, 0.1$.

To prove, as claimed above, that

$$Y(t) \equiv \lim_{B \rightarrow 0} \left(\frac{i}{2\pi B} \right)^{1/2} \exp\left(-i \frac{2t^2}{2B}\right) = \delta(t), \quad (10)$$

we need to show that

$$\int_{-\infty}^{\infty} Y(t) dt = 1 \quad (11)$$

and that

$$\int_{t_1}^{t_2} Y(t) dt = 0 \quad (12)$$

for any interval $t_1 \dots t_2$ that does not contain the origin. To appreciate qualitatively the nature of the function $(i/2\pi B)^{1/2} \exp(-ix^2/2B)$, consider its projection,

$$F(x, B) \equiv \left(\frac{1}{2\pi B} \right)^{1/2} \cos\left(\frac{x^2}{2B}\right). \quad (13)$$

Figure 3 shows plots of $F(x, B)$ for $B = 1, 0.5, 0.1$. Equation (11) reflects the fact that the main contribution to the integral is from the first few oscillations near the origin (the area under a given number of peaks is independent of B), whereas Eq. (12) follows from the fact that, when $B \rightarrow 0$, t_1 and t_2 in the normalized variable $x = t/\sqrt{B}$ of Fig. 3 tend to infinity. More rigorously, I employ the definition of the Fresnel cosine and sine integrals⁸ $C(\omega)$ and $S(\omega)$, respectively,

$$\begin{aligned} C(\omega) &= \int_0^\omega \cos\left(\frac{\pi}{2} \tau^2\right) d\tau, \\ S(\omega) &= \int_0^\omega \sin\left(\frac{\pi}{2} \tau^2\right) d\tau, \\ C(\infty) &= S(\infty) = 0.5, \end{aligned}$$

to express Eq. (11) as

$$\begin{aligned} \int_{t_1}^{t_2} Y(t) dt &= \frac{1}{2} (1 + i) \lim_{B \rightarrow 0} \left\{ C\left(\frac{t_2}{\sqrt{\pi B}}\right) - C\left(\frac{t_1}{\sqrt{\pi B}}\right) \right. \\ &\quad \left. - i \left[S\left(\frac{t_2}{\sqrt{\pi B}}\right) - S\left(\frac{t_1}{\sqrt{\pi B}}\right) \right] \right\} \\ &= \frac{1}{2} (1 + i) \{ C(\infty) - C(\infty) \\ &\quad - i[S(\infty) - S(\infty)] \} = 0 \end{aligned}$$

when t_1 and t_2 have the same sign.

In a similar fashion I show that

$$\int_{-\infty}^{\infty} Y(t) dt = (1 + i) [C(\infty) - iS(\infty)] = 1.$$

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