

In situ grown bifacial graphene stabilizes composite electrode for efficient perovskite solar cells

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In situ grown bifacial graphene stabilizes composite electrode for efficient perovskite solar cells

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Instability of rear electrodes undermines the long-term operational durability of efficient perovskite solar cells (PSCs). Here, a composite electrode of copper-nickel (Cu-Ni) alloy stabilized by in situ grown bifacial graphene is designed. The alloying makes the work function of Cu suitable for regular PSCs and Cu-Ni is the ideal substrate for preparing high-quality graphene *via* chemical vapor deposition, which simultaneously protects the device from oxygen, water and internal components reaction. To rivet the composite electrode with semi-device, a thermoplastic copolymer is employed as an adhesive layer during hot pressing. The resultant device achieved power conversion efficiency of 24.34% with significantly improved stability; the devices without encapsulation retained 97% of their initial efficiency after the damp heat test at 85°C with relative humidity of 85% for 1440 hours and the encapsulated devices maintained 95% of their initial efficiencies after maximum power point tracking under continuous 1 sun illumination for 5000 hours.

Metal halide perovskite solar cells (PSCs) have attracted great attention in both academia and industry owing to their excellent optoelectronic performance and low manufacturing costs¹⁻⁶. However, for PSCs to realize commercialization, they must survive the long-term natural erosion imposed by oxygen, moisture, light and heat^{7,8}. Thanks to the optimization of the perovskite materials, charge transport materials and the interface layers⁹⁻¹², the

operational stability of PSCs has made a great progress, but one of the key functional layers, rear electrode, is still prone to fail, which limits the overall durability of efficient PSCs¹³⁻¹⁴.

Silver (Ag) and aluminum (Al) are commonly used rear electrodes, whereas they tend to react with migrated halide anions from perovskite to form resistive compounds such as AgI and AlI₃¹⁵⁻¹⁷. In the case of gold (Au), although the formation enthalpy of Au-I is much higher, Au atoms can diffuse into the perovskite to form deep-level defects of Au_{Pb}, which act as efficient non-radiative recombination centers¹⁸. In addition, the use of noble metals comes at a high price and implies more stringent requirements for vacuum and temperature, which will significantly increase the manufacturing costs. To suppress the interaction between perovskite and metal atoms, introducing a thin buffer layer to separate them without hindering the charge transport has been reported as a successful strategy^{19,20}. However, materials from the perovskite or the electrode tend to penetrate that buffer layer on a long timescale because achieving a thin but uniform and compact coverage on a large area with buffer layers that are usually formed by solution-processable small molecules or polymers is hard²¹, calling for an increased intrinsic chemical stability of rear electrodes for PSCs.

Copper (Cu) is a potential candidate due to its relative inertness to migrated perovskite components and has been widely used in inverted PSCs²². However, its work function (WF) of 4.65 eV limits its application in efficient regular PSCs, which usually use 2,2',7,7'-

tetrakis(*N,N*-dip-methoxyphenylamine)-9,9'-spirobifluorene (spiro-OMeTAD) or poly[bis(4-phenyl)(2,4,6-trimethylphenyl)amine] (PTAA) with a highest occupied molecular orbital (HOMO) of around -5.2 eV²³. In addition, Cu can be oxidized by oxygen and moisture to generate products such as Cu₂(OH)₂CO₃ and Cu atoms were reported to diffuse into perovskite at 85°C²⁴. Besides metal electrodes, intrinsically stable carbon electrodes have also been applied to PSCs and 9000 hours of operational stability at the maximum power point tracking (MPPT) and 55°C was recently reported with no obvious change in the power conversion efficiency (PCE)²⁵. However, big challenges exist for them to obtain high efficiencies because of the severe potential losses²⁶. Therefore, it is still an open issue to develop a low-cost rear electrode with a tunable WF that combines chemical stability and high efficiency.

Herein, we report a composite electrode that consists of (i) Cu-nickel (Ni) alloy and (ii) in situ grown bifacial graphene. The microalloying of Cu with Ni (125:1/v:v) improves its electrochemical stability without compromising the electrical properties and makes it possible to tune the WF of Cu to fit the requirements of regular PSCs by simply varying the content of Ni. Moreover, Cu-Ni alloy is an ideal substrate for preparing high-quality graphene on both sides by chemical vapor deposition (CVD), which acts as natural barrier and substantially strengthens the stability of Cu-Ni alloy because the outer graphene can block the penetration of water and oxygen while the inner graphene can suppress the migration of perovskite components or metal atoms caused by light and heat. The

composite electrode is hot pressed on the semi-device with the assistance of a thermoplastic copolymer, which ensures the efficient charge collection at the interface of semi-device/electrode. As a result, a PCE of 24.34% was achieved for the regular device using graphene/Cu-Ni/graphene composite as rear electrode (CNG device) with an aperture area of 0.09 cm², comparable to that of the device using Ag electrode. After the optimization of the thermoplastic copolymer with conductive graphene nanoflake (GN), we obtained a PCE of over 20.76% for CNG device with an aperture area of 1.02 cm². The CNG devices without encapsulation retained 97% of their initial PCEs after the aging test of heating at 85°C with relative humidity (RH) of *ca.* 85% for 1440 hours and the encapsulated devices maintained 95% of their initial PCEs after operating at the MPPT under continuous 1 sun illumination for 5000 hours.

Fabrication and characterization of CNG electrodes

The fabrication process of CNG composite electrode and the assembly of the whole device (Extended Data Fig. 1) are detailed in Methods. The thickness of the sputtered Ni before annealing is set at 200 nm to obtain a WF for Cu-Ni that is compatible with the HOMOs of spiro-OMeTAD or PTAA (Extended Data Fig. 2, A to D). The cross-sectional scanning electron microscopy (SEM) of Cu-Ni and the corresponding energy dispersive spectroscopy (EDS) elemental mapping images confirm the uniform distribution of Ni in Cu foil after thermal annealing under reducing atmosphere (Extended Data Fig. 2, E to G). This process also smoothens the surface of the substrate, thereby preparing it for in situ

growth of graphene, as demonstrated by the atomic force microscopy (AFM) (Extended Data Fig. 2, H).

A uniform but thin layer of graphene is required here to meet the demand of being an efficient barrier without introducing extra defects or hindering the carrier transport.²⁷ We focus on the characterization of one side since the quality of graphene on both sides should be identical in a CVD method. Using CH₄ as the carbon source, with respective flow rates of 5, 10 and 15 standard cubic centimeter per minute (sccm), diluted in 100 sccm Ar/H₂, we arm both sides of the Cu-Ni alloy with graphene with varying number of layers and quality, denoted as CNG-5, CNG-10 and CNG-15, respectively. Their optical microscope (OM) images are provided in Fig. 1, A to C. Obviously, due to the difference in the content of carbon source, the graphene on CNG-5 and CNG-15 form a non-uniform monolayer and coexisting monolayer and bilayer, respectively. In contrast, a uniform monolayer graphene is observed on CNG-10. To further determine the quality and layer numbers of graphene, Raman spectra are measured for the three samples. The full width at half maximum (FWHM) for 2D peak at *ca.* 2680 cm⁻¹ are shown in Fig. 1, D to F; the graphene of CNG-10 exhibits the most uniform distribution of FWHM for 2D peak with an average value of below 45 cm⁻¹. Coupled with the intensity ratios of 2D peak and G peak at *ca.* 1584 cm⁻¹ (I_{2D}/I_G), as shown in Fig. 1, G to I, the layer numbers of graphene on CNG-5, CNG-10 and CNG-15 can be deduced²⁸. The graphene of CNG-5 contains regions of $I_{2D}/I_G > 2.5$, which represents discontinuous monolayer graphene film and is consistent with the OM image in

Fig. 1A. The I_{2D}/I_G for CNG-10 almost locates between 1.5 and 2.5, indicating the formation of monolayer graphene. Further increase in the content of CH_4 leads to blue regions for CNG-15 ($0.8 < I_{2D}/I_G < 1.2$), which is indicative of the formation of non-uniform bilayer and agrees well with the FWHM of 60 cm^{-1} in Fig. 1F. Incomplete coverage may weaken the function of being the barrier for water, oxygen and migrated components, whereas overlapped graphene not only enlarges the defect density at this interface (Extended Data Fig. 3, A to C) but also increases the series resistance (R_s) of PSCs. Therefore, CNG-10 is expected to be the most suitable composite electrode among the three samples.

Assembly and performance of CNG devices

Before the assembly of an integral device, the effect of graphene on the WFs of Cu-Ni alloy is measured by ultraviolet photoelectron spectroscopy (UPS). As shown in Extended Data Fig. 4, A to D, the WFs of CNG-5, CNG-10 and CNG-15 composite electrodes are 5.15, 5.11 and 4.99 eV, respectively, which are also compatible with the HOMOs of the commonly used HTMs in regular PSCs. The integral devices are fabricated by hot pressing CNG electrodes on the semi-device with the structure of fluorine-doped tin oxide (FTO)/ SnO_2 /perovskite/HTM. A thin adhesive layer of thermoplastic ethylene vinyl acetate (EVA) copolymer is employed at the interface to assist the combination of HTMs and CNG electrodes and to fill the possible gaps left after hot pressing, which is beneficial for realizing efficient carrier tunneling and thereby the enhanced ohmic contact²⁹. The

temperature of hot pressing is set at 130°C, which is a conventional value for EVA-based materials. In addition, the pressure and time are optimized to be 0.3 MPa and 60 seconds, respectively, after the measurement of the resistance of CNG electrodes/EVA/spiro-OMeTAD/FTO (Extended Data Fig. 4, E and F).

Fig. 2A shows the cross-sectional SEM image of a CNG device; EVA is too thin to be distinguishable so that it can realize efficient carrier tunneling. The current density-voltage ($J-V$) curves of PSCs using CNG-5, CNG-10, CNG-15 and Ag electrodes (CNG-5, CNG-10, CNG-15, Ag device) under forward scan are presented in Fig. 2B. The CNG-10 device obtained a PCE of 24.34% with an aperture area of 0.09 cm², which is comparable with that of the Ag device (best PCE = 24.65%). The detailed photovoltaic parameters of Fig. 2B are summarized in Extended Data Table 1. The inferior performance of CNG-5 and CNG-15 devices can be attributed to the lower quality of graphene, leading to the charge accumulation at the HTM/electrode interface. This effect can be verified by capacitance-voltage ($C-V$) measurements *via* searching the characteristic peaks in capacitance at a specific region of bias under light³⁰. As shown in Extended Data Fig. 5, A to D, the $C-V$ curve of the CNG-10 device shows no obvious peaks, indicating the fast charge transport in the device, whereas the CNG-5 device shows a peak at *ca.* -1.1 V and the CNG-15 device shows peaks at both *ca.* -0.3 V and -1.1 V, respectively, indicating the charge accumulation in those devices. Twenty devices of each batch were fabricated and the histogram of average PCE values are shown in Extended Data Fig. 6; the CNG-10 devices exhibit a

narrower distribution of PCE compared with other CNG devices and thereby a higher reproducibility due to the uniform and high-quality graphene layer, as demonstrated in Fig. 1.

We further fabricated CNG device with an aperture area of 1.02 cm². However, a much lower PCE of 15.43% was achieved (Extended Data Fig. 7, A), probably due to the nonuniformity of hot pressing, which may cause larger gaps at the interface beyond the thickness of EVA. In this case, we slowed down the rotation speed of EVA from 6000 to 5500 and 5000 r.p.m and the R_s of the corresponding devices first reduces and then suddenly increases to a much higher value (Extended Data Fig. 7, B), which means that the choice of 5000 r.p.m leads to the formation of an insulating layer too thick to allow charge tunneling. To allow for higher EVA thickness in localized areas with larger gaps, we mitigated resistive losses *via* addition of GN in EVA to boost the conductivity. The carbonyl group on the branch chain of EVA can interact with GN *via* Van der Waals force, as confirmed by the small blue shift (*ca.* 0.33 eV) of C=O peak measured by x-ray photoelectron spectroscopy (XPS) in Extended Data Fig. 7, C, which helps the formation of conductive network of GN in EVA matrix³¹. As is shown in Extended Data Fig. 7, D, the volume resistance of EVA goes through a sudden drop when the mass ratio of GN reaches 1.6 wt% and further increase to 2.4 wt% barely improves the conductivity, indicating the formation of a stable conductive network. The J - V curves of the devices with 0.8 wt%, 1.6 wt% and 2.4 wt% GN in EVA are shown in Fig. 2C (0.8%-, 1.6%- and 2.4%-

device). Obviously, the PCE of the device is greatly improved to 20.76% when the network is constructed (1.6%-device) and the corresponding incident photon-electron conversion efficiency (IPCE) is provided in Extended Data Fig. 7, E, showing a minimal mismatch with the J_{SC} from the $J-V$ scan (<3%). In addition, no obvious hysteresis was observed (Extended Data Fig. 7, F). However, a drop in the optoelectronic performance is found for 2.4%-device, especially in the open-circuit voltage and the fill factor. To disclose the reason, we measured the transient photovoltage (TPV) decay to analyze the charge carrier dynamics in the devices (Fig. 2D). The faster decay of TPV for 2.4%-device suggests a shorter charge carrier lifetime than that for 1.6% device, which may be related to the aggregation of GN³². The distribution of GN in EVA is characterized by Raman spectra (Fig. 2E and F); apparent aggregation of GN represented by the red regions is found in EVA with 2.4 wt% GN, which may bring about higher concentration of defects that cause extra non-radiative losses at the interface. It should be noted that a variety of conductive additives can be chosen to boost the conductivity of the copolymer. However, to guarantee the stability of the interface, stable materials with good dispersity will be the priority selection.

Stabilizing mechanism of CNG electrode

To reveal the stabilizing mechanism of CNG, we first studied their resistance to water and oxygen. As shown in Extended Data Fig. 8, A to E, the contact angle with water in air rises from 74.9° for Ag electrode to 102° for CNG-10, which should be beneficial for

repelling water. Even if water is dropped and stays at the surface of CNG-10 for 24 hours, the color of perovskite remains black, while the perovskite under Ag turns yellow (Extended Data Fig. 8, F and G). To exclude the effect of electrode thickness, the permeation rates of water and oxygen for CNG-10 electrodes are measured and drop to 3.32% and 5.38% of the initial values for Cu-Ni alloy after equipped with air-tight and hydrophobic graphene (Extended Data Fig. 9, A and B). The reduced permeability meets the requirements for encapsulation³³. To study this encapsulation effect of CNG electrodes on devices, in Fig. 3A, we conducted the gas chromatography-mass spectrometry (GC-MS) to compare the volatile products escaping from Ag and CNG-10 devices after aging tests at 85°C and 85% RH in the air for 500 hours³⁴. As a result, barely no volatile products are found for CNG device, except for a small quantity of NH₃ and NO. By contrast, a variety of products are detected for Ag device, including the additive 4-tert-butylpyridine from spiro-OMeTAD. The GC-MS results demonstrate superior damp heat stability of CNG device. To investigate the electrochemical corrosion of CNG electrodes, Tafel curves for Cu, Cu-Ni and CNG-10 are measured (Fig. 3B). Compared with Cu, the corrosion current is lower at the anodic section for Cu-Ni, implying slower corrosion rate due to the microalloying with Ni. For the sample of CNG-10, the self-corrosion potential (E_{corr}) positively shifts from -0.34 V (Cu and Cu-Ni) to -0.29 V, representing much higher resistance to chemical corrosion, which is owed to not only the blocking of water and oxygen, but also the decrease in the migration rate of ionic species that can trigger oxidation and reduction³⁵.

The effect of CNG-10 electrode on the suppression of migrated ions and metal atoms in the devices is further demonstrated. After removing the package and peeling off the electrodes of the devices that were aged under MPPT for 1000 hours, XPS measurement reveals an I⁻ signal much lower inside CNG-10 than that inside Ag (Extended Data Fig. 10, A and B), which preserves the morphologies of spiro-OMeTAD and perovskite, as shown in Extended Data Fig. 10, C and D. The spatial distribution of I⁻, Ag⁻ and Cu⁻ for the aged Ag and CNG devices are analyzed by time-of-flight secondary ion mass spectroscopy (ToF-SIMS, Extended Data Fig. 10, E and F). Obviously, the I⁻ (Fig. 3C) and Ag⁻ (Fig. 3E) in the aged Ag device have migrated over the whole depth of the device while I⁻ (Fig. 3D) and Cu⁻ (Fig. 3F) in the aged CNG-10 device are almost confined to their original layers.

Stabilizing effect of CNG electrode on devices

CNG-10 devices without encapsulation retained 97% of their initial efficiency after the aging test of heating at 85°C with *ca.* 85% RH for 1440 hours, whereas the PCEs of the control devices dropped to 56.5% of their initial PCEs after 936 hours (Fig. 4A). For the operational stability test, another control sample using Cu-Ni alloy with bifacial sprayed graphene as the electrode (SG device) was tested. All the encapsulated devices were measured under MPPT with continuous 1 sun illumination; the CNG-10 devices retained 95% of their initial PCEs after 5000 hours with a small deviation across five individual cells, while the PCEs of the SG and Au devices dropped to 59% and 30% of their initial PCEs after 2500 and 1250 hours, respectively, with much larger deviations (Fig. 4B). The

inferior performance of SG device may be ascribed to numerous pores in overlapped graphene.

Online content

Any methods, additional references, Nature Research reporting summaries, source data, statements of data availability and associated accession codes are available.

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Additional information:

Supplementary information is available for this paper.

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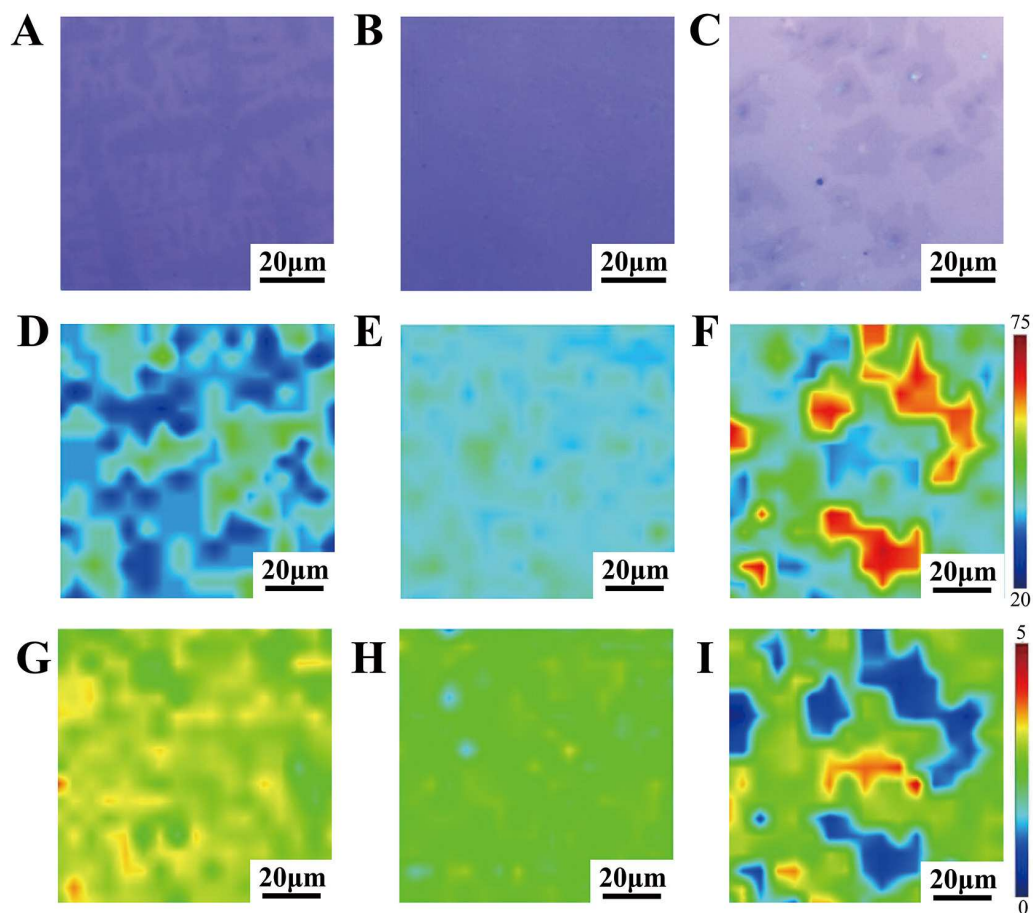


Fig. 1. The quality and layer number of graphene of CNG composite electrodes characterized by OM and Raman spectra. (A to C) OM images, (D to F) Raman mapping of 2D FWHM and (G to I) I_{2D}/I_G of graphene on CNG-5, CNG-10 and CNG-15. The transfer method of graphene used for the measurement of OM and Raman spectra is based on previous work ²⁸.

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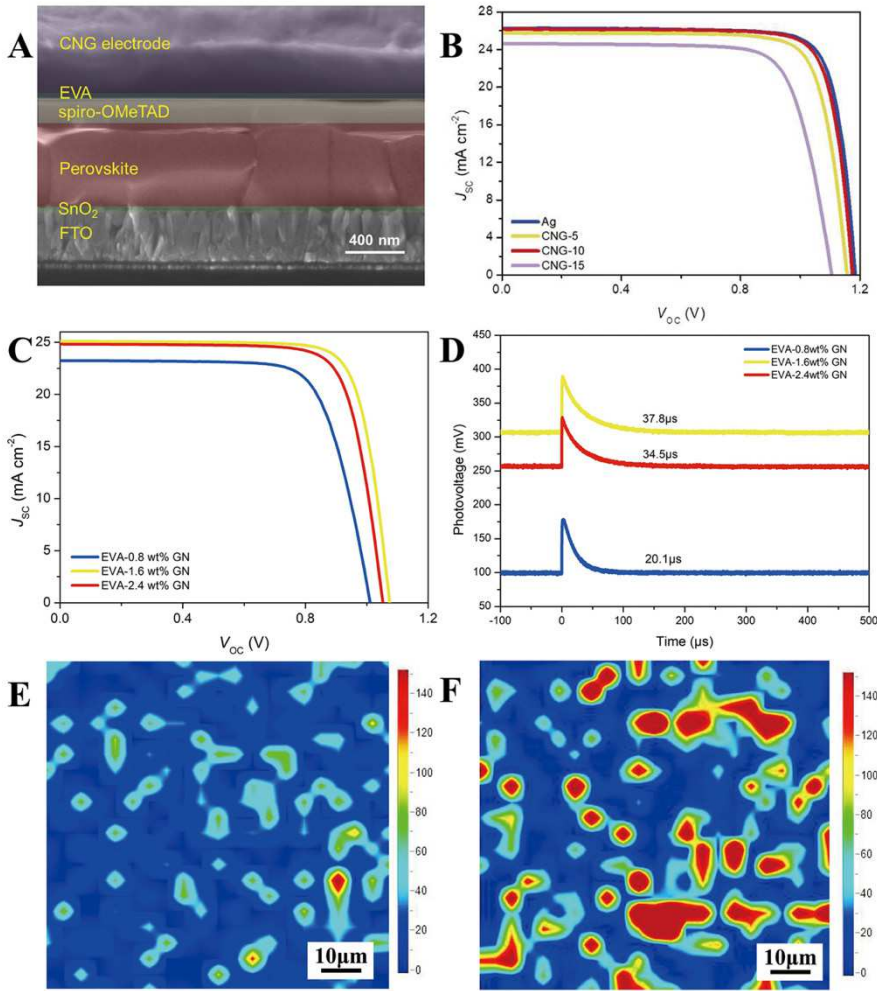


Fig. 2. The structure and performance of PSCs with aperture areas of 0.09 and 1.02 cm². (A) Cross-sectional SEM image of CNG-10 device. (B) J - V curves of CNG and Ag devices with an aperture area of 0.09 cm² under forward scan. (C) J - V curves and (D) corresponding TPV results of 1.02 cm² CNG devices with different modified adhesive layers in the mass ratio of GN in EVA. Raman mapping of G peak for (E) 1.6 wt% and (F) 2.4 wt% GN in EVA, respectively.

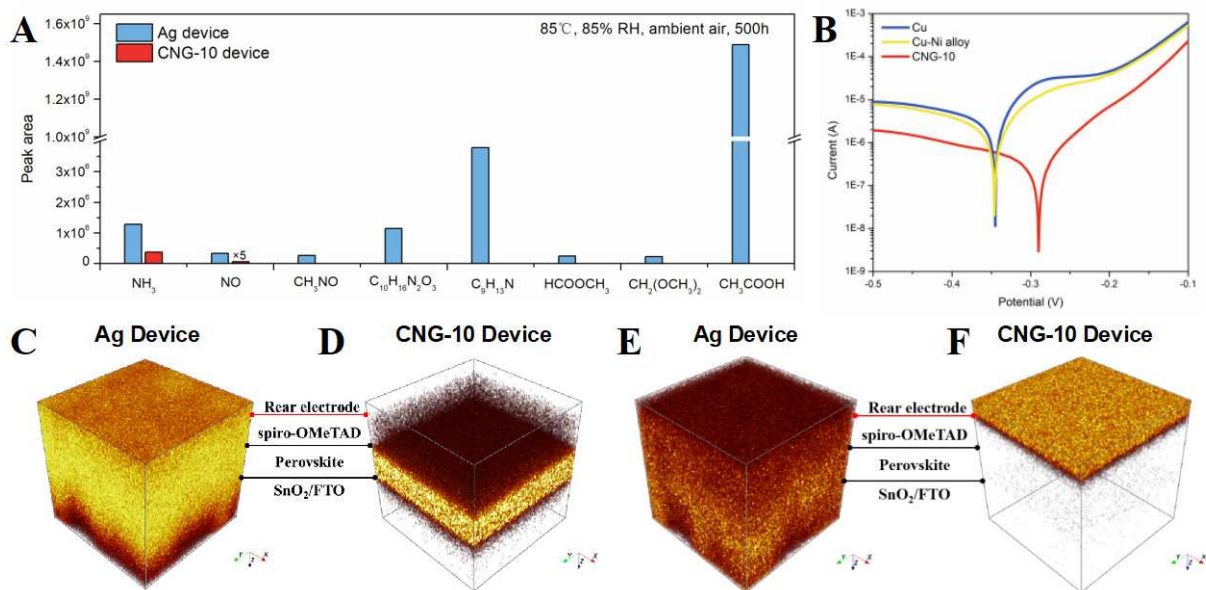


Figure 3. The stabilizing mechanism of CNG electrodes. (A) GC-MS peak areas of products for the aged Ag and CNG-10 devices. (B) Tafel curves for Cu, Cu-Ni and CNG-10 electrodes in NaCl solution (3.5 wt%). The spatial distribution of I⁻ in the aged (C) Ag and (D) CNG devices, respectively. The spatial distribution of (E) Ag⁺ and (F) Cu⁺ in the aged Ag and CNG devices, respectively.

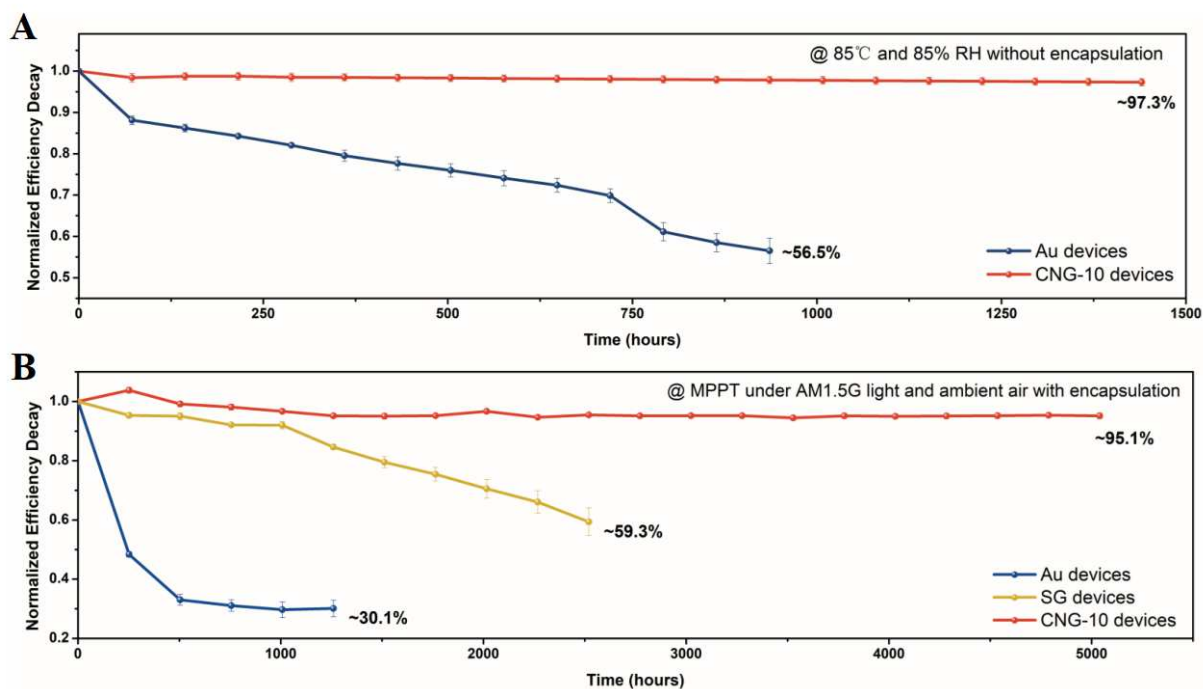


Figure 4. The stabilizing effect of CNG electrodes on devices. (A) The damp heat stability of the Au and CNG-10 devices without encapsulation. (B) The operational stability of the encapsulated Au, SG and CNG-10 devices. The error bars denote standard deviations for five individual devices.

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Methods

Materials. All the chemicals were used without further purification, including (1) SnO₂ electron transport material (ETM): dispersing SnO₂, 15% in H₂O colloidal dispersion (Alfa Aesar), deionized water (Sigma Aldrich); (2) perovskite precursor: CH(NH₂)₂I (FAI, 98%, TCI), CH₃NH₃Cl (MAcI, 98%, TCI), PbI₂ (99.99%, TCI), dimethylformamide (DMF, 99.8%, Sigma Aldrich), dimethyl sulfoxide (DMSO, 99.9%, Sigma Aldrich), isopropanol (IPA, Sigma Aldrich); (3) spiro-OMeTAD HTM: spiro-OMeTAD (99.8%, Ningbo Borun New Material Technology Co., LTD.), 4-tert-butylpyridine (tBP, Xi'an Polymer Light Technology), bis(trifluoromethane)sulfonimide lithium salt (Li-TFSI, 99.95%, Sigma Aldrich), acetonitrile (99.8%, Sigma Aldrich), chlorobenzene (CB, 99.8%, Sigma Aldrich), PTAA (Sigma Aldrich), toluene (99.8%, Sigma Aldrich); (4) Electrode: Ag, Au (99.999%, Beijing Dream Material Technology Co. LTD.), Cu foil (99.8%, Alfa Aesar), Ni target (99.995%, Beijing ZhongNuo Advanced Material Technology Co., LTD.), EVA (with 40% ethenyl acetate, Sigma Aldrich), GN (Alfa Aesar) for adhesive, xylene (99%, Aladdin), graphene for SG device (99%, Alfa Aesar). Chlorinated graphene oxide (Cl-GO) is synthesized according to previous work ¹¹.

Synthesis of EVA-based adhesives. Different amount of GN from 0 to 6 mg were added into 10 mL xylene and sonicated for 1 hour to form a homogeneous GN dispersion. 0.25 g of EVA was then added into the dispersions. The samples were placed on a drying oven at 80°C to swell for 1 hour. The swelled sample was further stirred for 10 hours to form homogeneous EVA adhesive and EVA-GN adhesive.

Fabrication of CNG and SG electrodes. For the fabrication of CNG electrodes, the Cu foil was first chemically polished on both sides and sonicated with detergent, deionized water, ethanol, acetone and IPA for 15 minutes, respectively. Ni with respective thicknesses of 100, 200 and 300 nm were then sputtered on the Cu foil using the magnetron sputtering method followed by thermal annealing under 100 sccm Ar/H₂ reducing atmosphere at 1000°C for 1 hour to form uniform Cu-Ni alloys. By employing 5, 10 and 15 sccm of CH₄ diluted in 100 sccm Ar/H₂ as carbon source at 1000°C for 30 minutes, both-sides of Cu-Ni alloy were protected by graphene with varying number of layers and quality, denoted as CNG-5, CNG-10 and CNG-15, respectively. For the fabrication of SG electrode, 20 mg graphene was dispersed into 5 mL IPA through ball-milling for 12 hours to obtain a homogeneous dispersion. Then, 150 µL dispersion was sprayed onto both sides of Cu-Ni alloy followed by annealing at 85°C³⁶.

Fabrication of PSCs with different electrodes. The FTO substrates were etched with zinc powder and 6M HCl for 15 seconds to obtain patterned substrates, followed by sonication with detergent, deionized water, ethanol, acetone and IPA for 15 minutes, respectively. Before use, the substrates were cleaned with ultraviolet ozone for 20 minutes to remove the organic residues. Then a thin layer of SnO₂ was prepared by spin-coating a SnO₂ dispersion (1:8.5/v:v in deionized water) at 3000 r.p.m for 30 seconds, followed by annealing in the ambient air at 150°C for 30 minutes. After the 20-minute treatment by ultraviolet ozone, the substrates were transferred to the glove box. 1.5M PbI₂ in DMF:DMSO (9:1/v:v) was spin-coated on SnO₂ at 1500 r.p.m for 40 seconds and then a

solution of FAI:MAI:MACl (90:9:9 mg mL⁻¹) in IPA was spin-coated on PbI₂ at 1500 r.p.m for 30 seconds, followed by thermal annealing at 150°C for 15 minutes in the ambient air (*ca.* 30% humidity). The substrates were then transferred to the nitrogen glove box and a layer of spiro-OMeTAD or PTAA was spin-coated on perovskite film at 3000 r.p.m for 30 seconds. The spiro-OMeTAD was dissolved in chlorobenzene (72.3 mg mL⁻¹) with additives of 17.5 µL Li-TFSI/acetonitrile (520 mg mL⁻¹) and 28.8 µL tBP. The PTAA was dissolved in toluene (10 mg mL⁻¹) with additives of 7.5 µL Li-TFSI/acetonitrile (170 mg mL⁻¹) and 4 µL tBP. For PSCs with CNG electrodes, the EVA or EVA-GN adhesives was spin-coated on one side of CNG at 5000, 5500 or 6000 r.p.m for 30 seconds, followed with thermal treatment at 70°C for 30 minutes to remove the solvent and form a thin and uniform bonding layer. The CNG electrodes were hot-pressed with semi-device (Glass/FTO/SnO₂/perovskite/HTM) at 130°C under a pressure of 0-0.5 MPa for 0-100 seconds (TH-XC601-H, Shenzhen XOTECH Co., LTD.). For PSCs with control electrodes, 80 nm thick of Ag or Au was thermally evaporated using a black metal shading mask. The 0.09 and 1.02 cm² masks were used to define the aperture areas during measurement.

Damp heat and operational stability tests of the control and CNG devices. For the stability tests of Fig. 4, A and B, Au electrode is used for the control devices to increase the comparability. In addition, to rule out the thermal degradation from the HTM layer, thermally stable Cl-GO/PTAA is used for control and CNG devices ¹¹.

Characterization. The Raman mapping spectroscopy was performed on an inVia spectroscope (Renishaw, UK) to assess the morphology and quality of the graphene with

an excitation source of 532 nm Ar ion laser. Field emission SEM (JEOL JSM-7800F Prime) equipped with EDS was employed to observe the morphology and element distribution of the samples. An atomic force microscopy (AFM, TT2-AFM, USA) was employed to measure the roughness of Cu-Ni substrates. The electrochemical impedance spectroscopy (EIS) and $C-V$ measurements were characterized by a multifunctional electrochemical analysis instrument (Zahner, Germany) under dark or white light (60 mW cm^{-2}), respectively. The TPV measurements were carried out by the TranPVC instrument with a 640 nm laser under light-emitting diode (LED) white light bias. The $J-V$ curves of PSCs were measured under simulated solar illumination at 100 mW cm^{-2} , AM 1.5G (WXS-155S-10, Wacom Denso, recorded by a digital source meter Keithley 2400). The solar simulator was calibrated by standard silicon reference cell, which was certified by the Calibration, Standards and Measurement Team at the Research Center for Photovoltaics in AIST, Japan. The spectral mismatch is $<3\%$. The $J-V$ measurements were measured under forward scan (-0.2 to 1.2 V) or reverse scan (1.2 to -0.2 V). The IPCE spectrum was characterized by a monochromatic incident light of $1 \times 10^{16} \text{ photon cm}^{-2}$ ³⁷. The ToF-SIMS were based on ION ToF SIMS 5-100 (Germany). A stable Cs^+ ion beam was utilized as the ion beam to peel off the PSCs with an analysis area of $100 \times 100 \text{ }\mu\text{m}^2$. The XPS and UPS were measured with a Kratos AXIS UltraDLD by Al $\text{K}\alpha$ X-ray source. The static contact angle tests were characterized by water droplet with a DSA100 instrument (Germany). The volume resistivity of bonding layer (EVA or EVA-GN) on glass was measured on a high resistance meter (Agilent 4339B, USA) to identify the percolation threshold of graphene in EVA

polymer. The permeation rates of water vapor and oxygen for Cu-Ni alloy and CNG electrodes were measured by a gas transmission rate tester followed by ISO 2556. Tafel polarization curves were obtained by an electrochemical workstation (CHI660D) with a three-electrode system. The GC-MS data was recorded by headspace GC-MS analytical methods based on a previous work ³⁴. Rt-QPLOT column (30 m×0.32 mm) or Rtx-VolatileAmine column (30 m×0.32 mm) was connected to the PTV inlet. The helium carrier gas was set to a constant flow, and oven equilibration time to 10 minutes.

Data availability

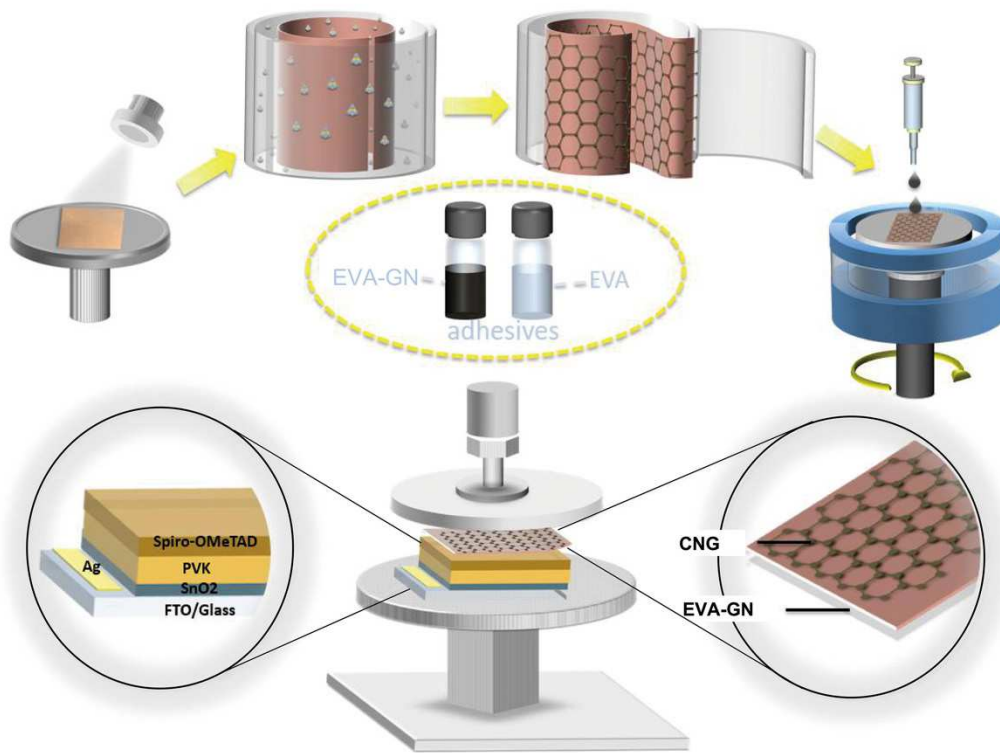
The data that support the findings of this study are available from the corresponding authors upon reasonable request.

Code availability

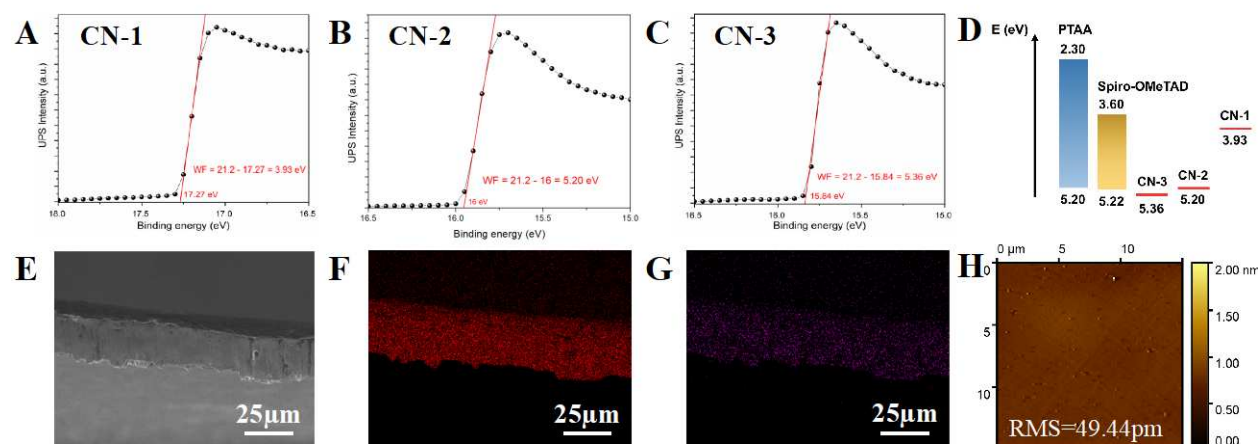
The codes used in this work are available from the corresponding authors upon reasonable request.

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- 37 Wang, Y. *et al.* Reliable Measurement of perovskite solar cells. *Adv. Mater.* **31**, 1803231, doi:10.1002/adma.201803231 (2019).
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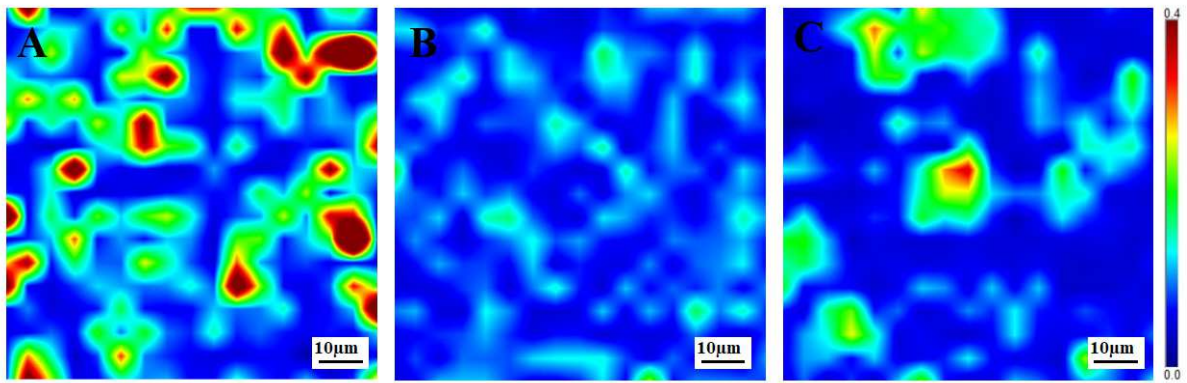
- comprising acryloyl groups. JP2015185802-A.
- 39 Tanabe, J., Tanaka, A. & Kawasaki, M. Sealing film for forming solar cell module, is obtained by carrying out thermal reaction of ethylene-vinyl acetate copolymer, organic peroxide, crosslinking adjuvant as crosslinking agent and additive with self-polymerization property. JP2016092353-A.



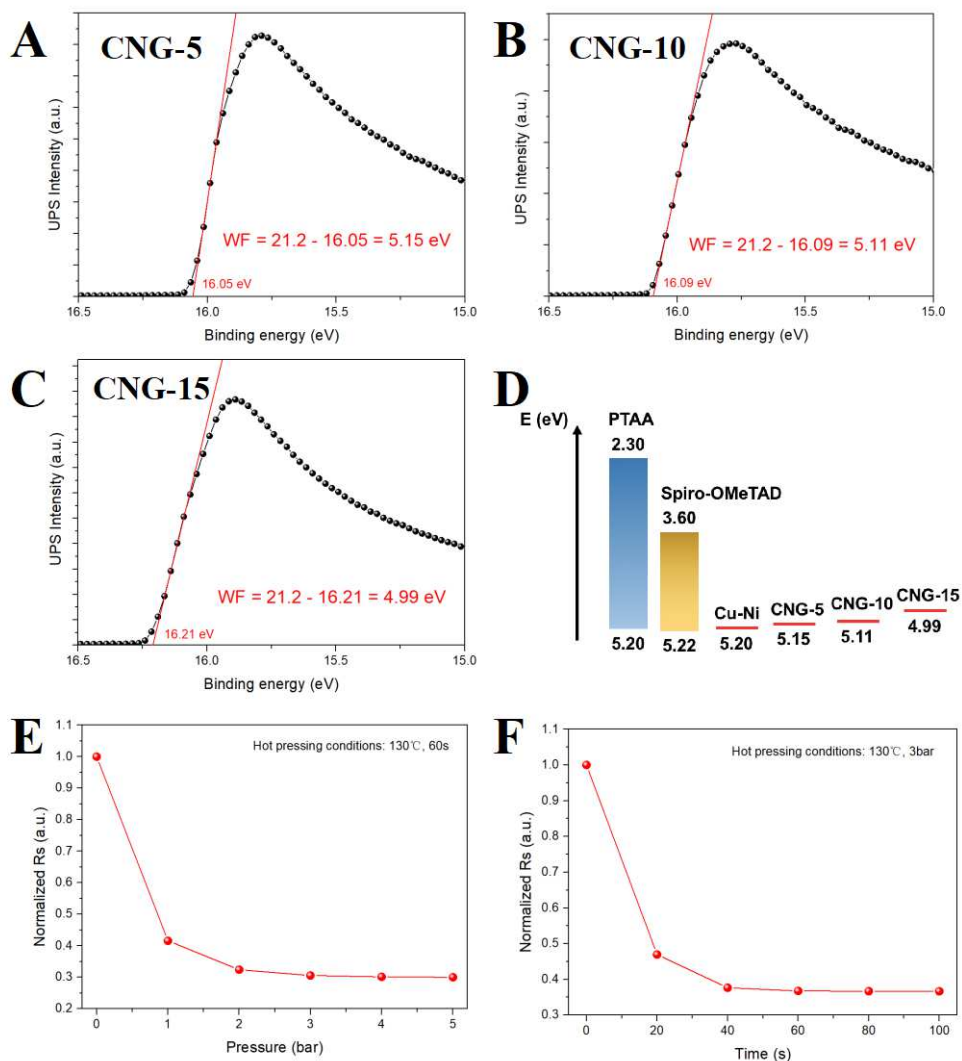
Extended Data Fig. 1. Schematic of the fabrication process of CNG electrodes and the assembly of the integral device.



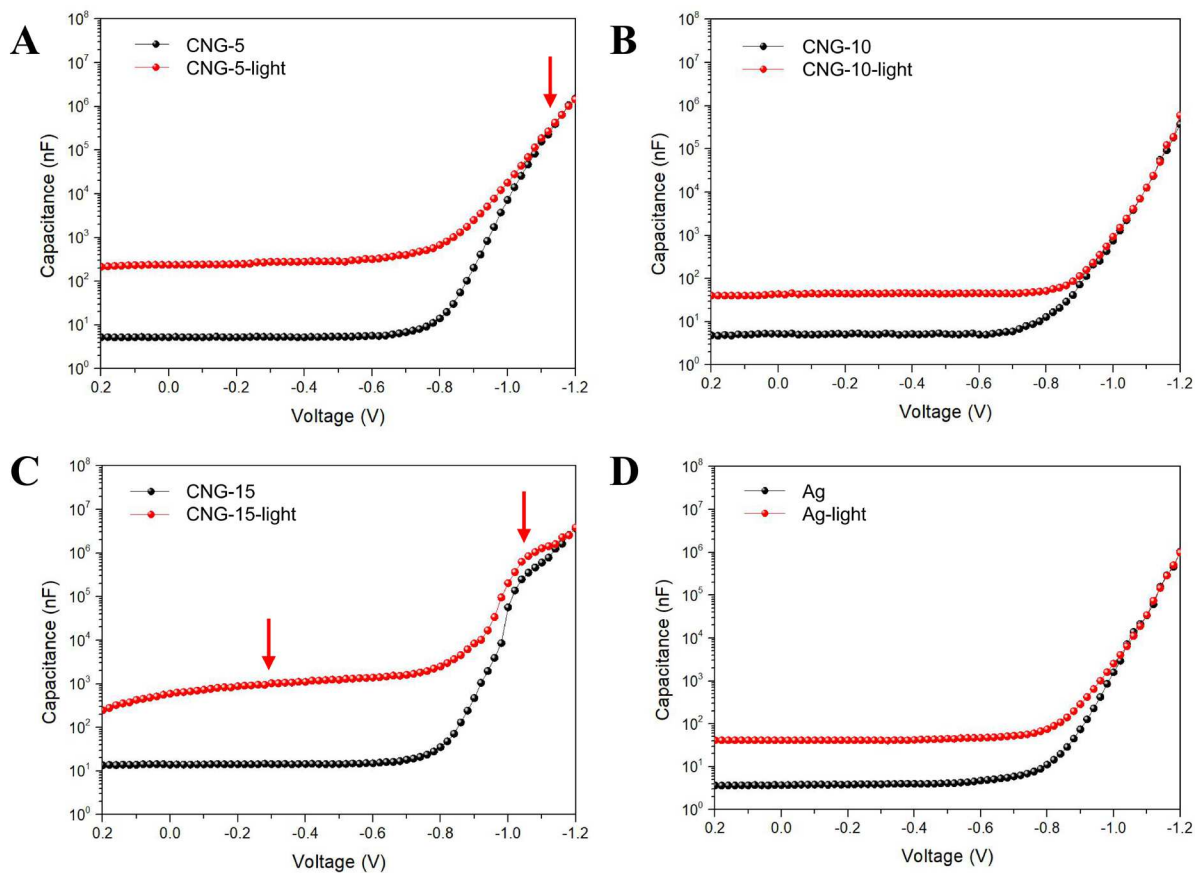
Extended Data Fig. 2. The formation and characterization of Cu-Ni alloy. The WFs of the Cu-Ni alloys fabricated by sputtering (A) 100, (B) 200 and (C) 300 nm thickness of Ni on Cu foil, denoted as CN-1, CN-2 and CN-3. (D) The relative energy level alignment of CN-1, CN-2, CN-3 and the commonly used HTMs in regular PSCs. The energy band structures of HTMs are based on the previous work¹⁹. (E) Cross-sectional SEM images of CNG electrodes with EDS mapping of (F) Ni and (G) Cu elements. (H) AFM xy-plane film morphology of Cu-Ni substrate. The roughness in (E) is caused by the preparation process of samples, which requires cutting to expose the cross section.



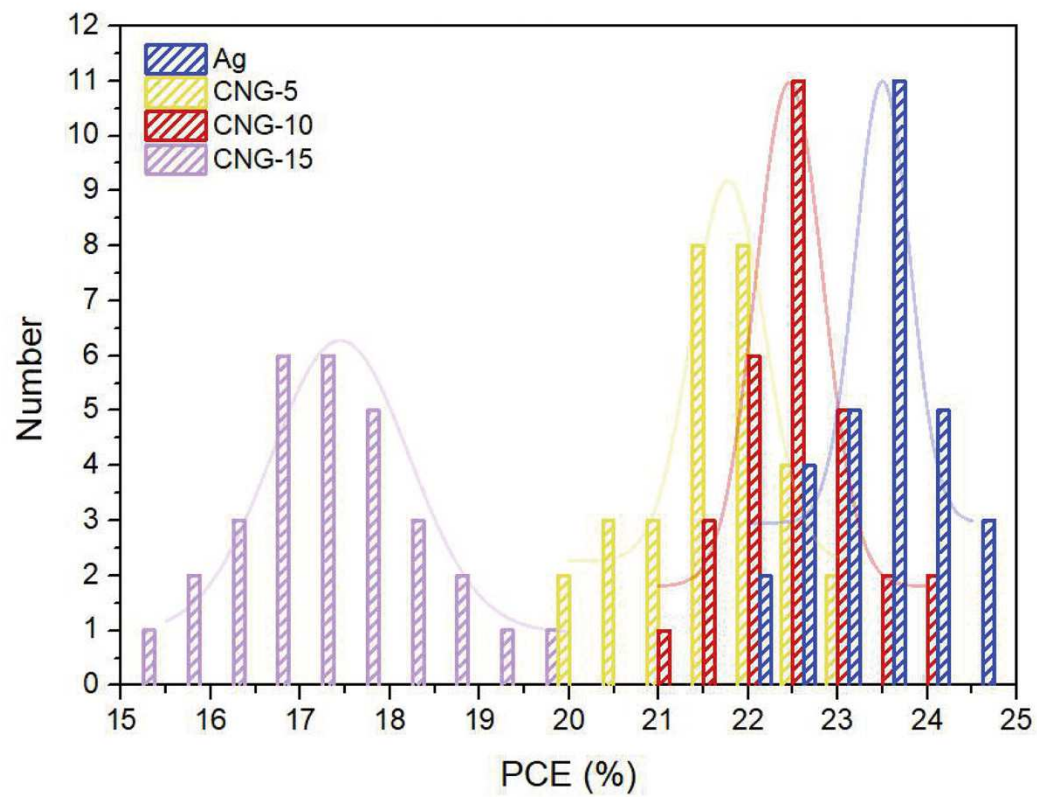
Extended Data Fig. 3. The defect density of graphene on (A) CNG-5, (B) CNG-10 and (C) CNG-15, reflected by I_D/I_G .



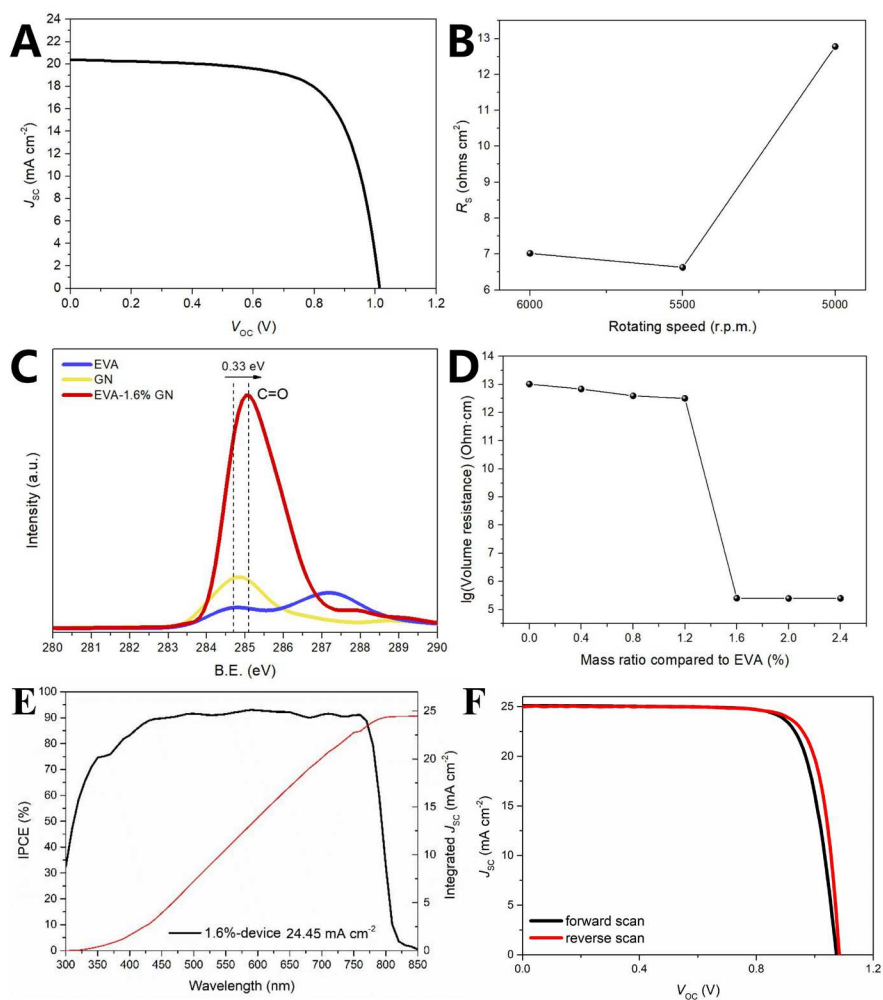
Extended Data Fig. 4. The assembly of integral CNG devices. The WFs of (A) CNG-5, (B) CNG-10 and (C) CNG-15 electrodes measured by UPS. (D) The energy level alignment for CNG electrodes and the commonly used HTMs in regular PSCs. The WF of Cu-Ni alloy in (D) is extracted from the result in Extended Data Fig. 2. The relationship between the resistance of CNG electrodes/EVA/spiro-OMeTAD/FTO and the (E) pressure and (F) time for hot pressing. The temperature is set to 130°C according to previous reports^{38,39}.



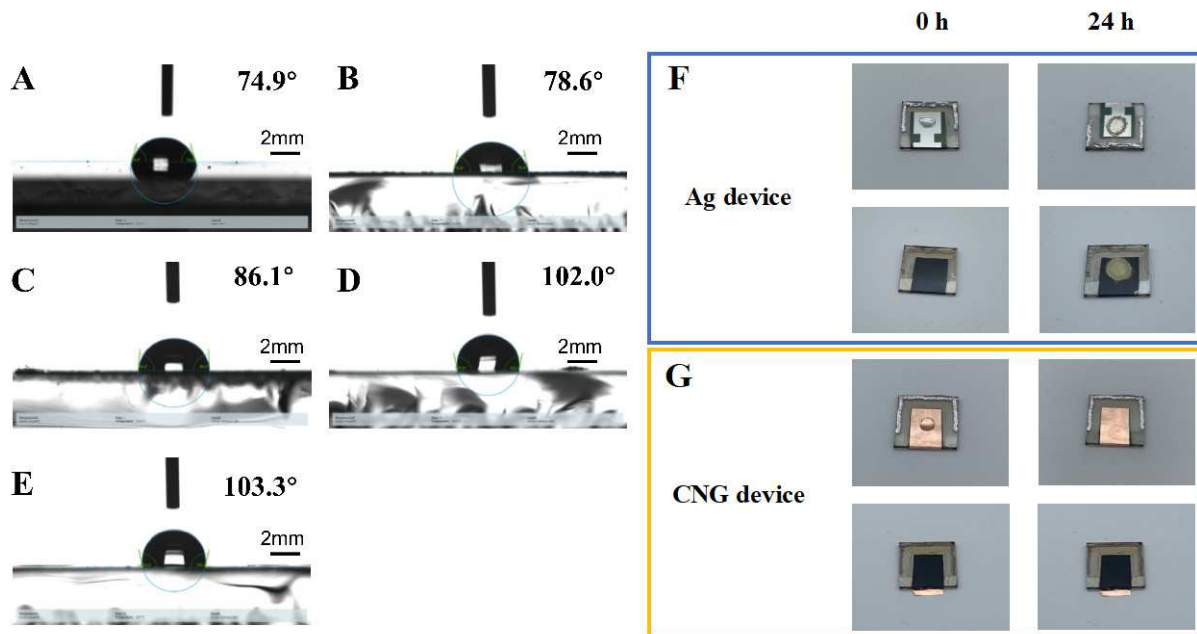
Extended Data Fig. 5. The charge carrier accumulation in CNG and Ag devices. C - V characteristics of (A) CNG-5, (B) CNG-10, (C) CNG-15 and (D) Ag devices under dark or illumination (LED, white light, 60 mW cm^{-2}) with the frequency of 1 kHz.



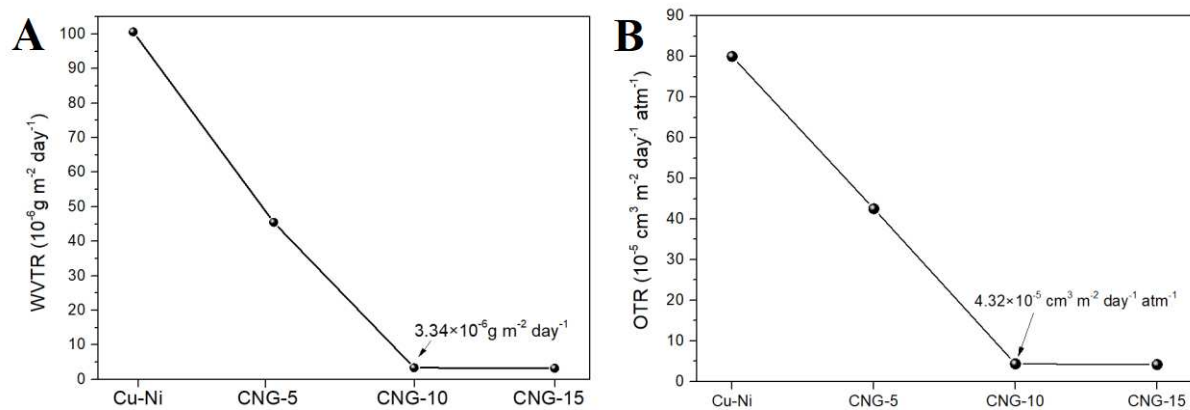
Extended Data Fig. 6. Histogram of average PCEs of PSCs using different electrodes.



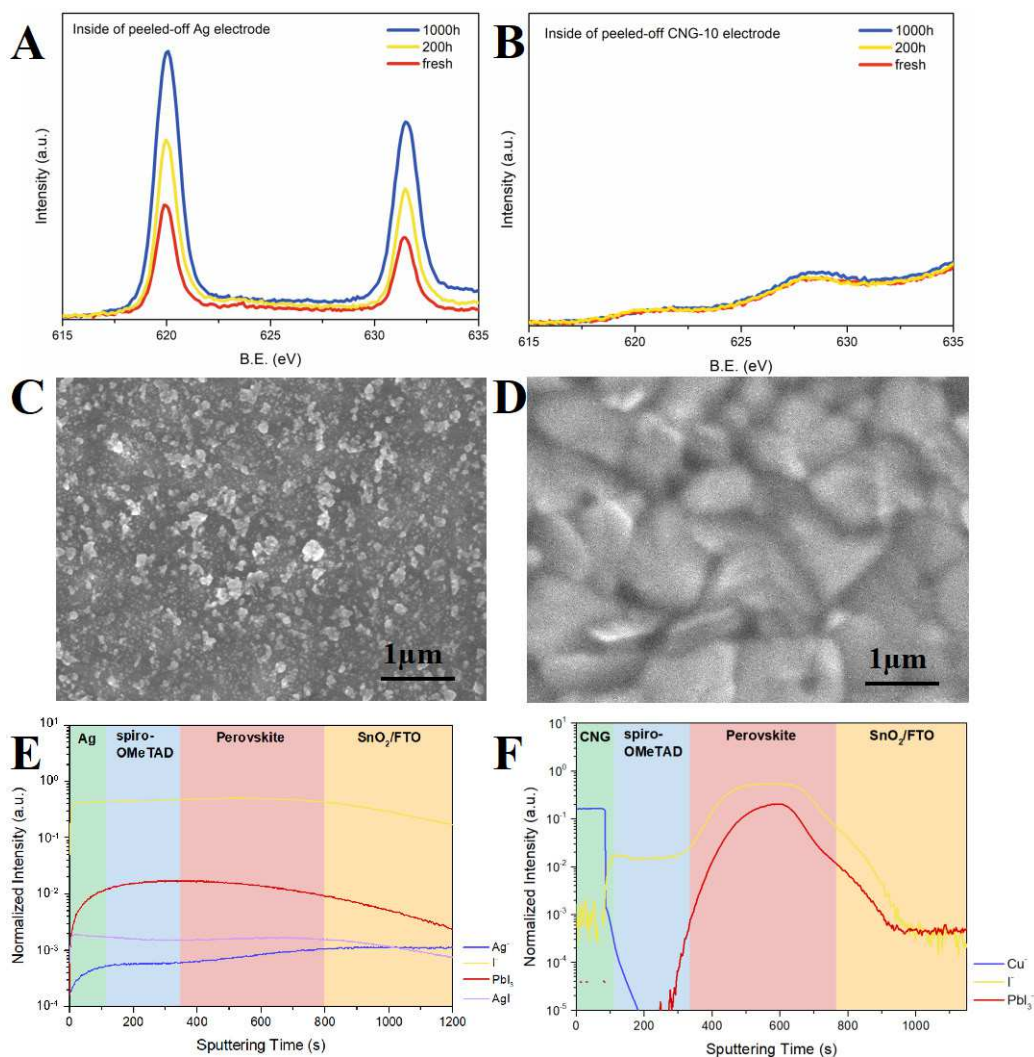
Extended Data Fig. 7. The fabrication of CNG device with an aperture area of 1.02 cm² and the modification of the adhesive layer. (A) The J - V curve of CNG-10 device under forward scan with EVA as the adhesive layer. (B) The R_s of CNG-10 device using EVA as the adhesive layer with different rotation speeds. (C) The interaction between EVA and GN. C=O peak in EVA, GN and EVA-1.6 wt% GN composite, measured by XPS. (D) The percolation threshold of GN in EVA adhesive. (E) The IPCE spectrum and (F) the J - V curves under forward and reverse scan for 1.6%-device.



Extended Data Fig. 8. The hydrophobic property of CNG electrodes. The static contact angle with water in air for (A) Ag, (B) Cu-Ni alloy, (C) CNG-5, (D) CNG-10 and (E) CNG-15, respectively. The top and bottom photographs of PSCs with (F) Ag and (G) CNG-10 electrodes before (left) and after (right) being exposed to water droplet for 24 hours.



Extended Data Fig. 9. The effect of graphene on the resistance of CNG electrodes to water vapor and oxygen. The permeation rates of (A) water vapor and (B) oxygen for Cu-Ni alloy and CNG electrodes.



Extended Data Fig. 10. The suppression of halide ions and metal atoms diffusion by CNG-10 electrode. The XPS spectra of I 3d core levels of the inside of (A) Ag and (B) CNG-10 electrodes of PSCs with different aging time. The top-view SEM images of spiro-OMeTAD/perovskite/SnO₂/FTO/glass after peeling off the electrodes of aged (C) Ag and (D) CNG-10 devices. The depth profiles of ToF-SIMS for aged (E) Ag and (F) CNG-10 devices.

Extended Data Table 1. The champion performance of Ag and CNG devices with an aperture area of 0.09 cm².

Rear electrode	V_{OC} (V)	J_{SC} (mA cm ⁻²)	FF (%)	PCE (%)	R_S (Ohm cm ²)	R_{sh} (Ohm cm ²)
Ag	1.162	26.23	80.91	24.65	2.61	16198.52
CNG-5	1.136	25.75	79.53	23.27	3.46	10067.85
CNG-10	1.154	26.16	80.66	24.34	2.88	13503.61
CNG-15	1.081	24.60	75.30	20.03	4.16	9489.08