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Kinetic modeling: a predictive tool for the adsorption of zinc ions onto calcium alginate beads

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Abstract

Background: The main purpose of this study is to develop a nonlinear model of a batch adsorption and to evaluate the model's capability in the prediction of experimental adsorption data. Additionally, results of the nonlinear model were compared with data of pseudo first- and second-order models. Experimental data were extracted from the adsorption of zinc ions using calcium alginate beads prepared via electrospray method. In order to study the effects of biosorbent porosity and the initial concentration of the zinc solution on adsorption kinetics, calcium alginate beads were prepared with two different porosities and zinc concentrations.

Results: The results revealed that the nonlinear model offers a much more accurate prediction compared with other models as the average root mean square deviation of the nonlinear model was calculated to be only 2.66%, which was smaller at least four times than that of others. Furthermore, the nonlinear model showed that diffusive transport through beads was limited by pore diffusion.

Conclusions: The nonlinear model provided a good fit to the experimental data as the calculated equilibrium adsorptions were shown to be in good agreement with their experimental counterparts.

Keywords: Nonlinear kinetic model, Pseudo-kinetic models, Zinc adsorption, Calcium alginate beads

Background

In certain industries, the adsorption of heavy metals from various waste streams which are cleaned using a sorbent is a crucial separation process [1]. Although there are numerous commercial adsorbents that are available for this purpose, biodegradable polymers such as chitosan and sodium alginate can be considered to be more beneficial, cost-effective, and more abundant in nature than others [2,3]. Sodium alginate extracted from brown algae is a linear copolymer of α -L-guluronate and α -D-mannuronate [4]. In addition, sodium alginate could be ionically gelled by the divalent cations such as Ca^{2+} and be converted to a stable and cross-linked structure [5], which has been used for the removal of some heavy metals such as cadmium [6,7], chromium [8], lead [6], cobalt [9], iron, copper [7], mercury [6], and zinc [10] from aqueous solutions. Furthermore, prediction of the adsorptive behavior of sorbents is important as a

consequence of the investigation of adsorption mechanism [11-17]. In order to investigate the mechanisms of the adsorption of heavy metals into adsorbents, pseudo first- and second-order models have been usually used to assess experimental data [2,12]. Since the model should be fitted by existing experimental data due to the model's nature, they can only predict the rate-controlling steps [2]. On the other hand, in almost all previous research in the adsorption processes, no mathematical model such as nonlinear ones has been applied [18,19] as the adsorption data have been extracted and undergone a simple investigation in their mechanisms via some pseudo models. The nonlinear model is instrumental and rational for the modeling and predicting of adsorption systems. The physiochemical conditions such as the type of ionic solutions (liquid diffusion coefficient), bead size, agitation rate, and porosity of beads are effective factors in an adsorption process that can be considered in the nonlinear model while their effects could be investigated in detail [14,20]. Implementing the mathematical model, once it has been endorsed, has the advantages of minimizing the number of experiments related to new operating

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conditions. In the nonlinear model, the interactive behavior between solutes and adsorbent is certainly described using essential isotherm equations such as that of Freundlich and Langmuir for modeling an adsorption system [2,3,9,21].

In the present study, biosorbents were produced with sodium alginate using the electrospray method, and their capability in removing zinc ions from an aqueous solution under batch adsorption was investigated. The main objectives were to investigate the zinc adsorption mechanism onto the calcium alginate beads, to develop a mathematical model for description of the adsorption, and to assess the flexibility of the mathematical model in comparison with some pseudo-kinetic models in the prediction of absorptive behavior. In addition, some effective parameters such as porosity and concentration of aqueous solution could not be clearly investigated on adsorption processes with pseudo models; on the contrary, the nonlinear model is able to provide a framework of analysis of these parameters. Therefore, the effects of some parameters such as porosity of the beads and initial zinc concentration in the adsorption process were considered on the adsorptive behavior of the models.

Methods

General assumptions

For quantitative depiction of the sorption process, the following assumptions have been made:

- 1 Each prepared calcium alginate bead was idealized as a sphere.
- 2 The mass transfer into calcium alginate beads was only considered in the radius direction, and other directions were deemed negligible.
- 3 Transport of the ions was from the bulk solution to the bead surface and across the boundary layer.
- 4 Adsorption was considered at the inner site of the beads.
- 5 The physical properties of the calcium alginate beads and the solutions' properties were constant in the isotherm of the adsorption processes.
- 6 Pore diffusion was considered onto calcium alginate sorbent.
- 7 Radius of the beads was constant with the adsorption of the water and the heavy metal (i.e., no swelling).
- 8 Bulk convection was neglected onto the beads.

Model description

Mass balance development

Based on the assumptions, the nonlinear model for the prepared sphere beads is as follows [7,20]:

$$\frac{\partial C}{\partial t} + \frac{\rho_b}{\varepsilon} \frac{\partial P}{\partial t} = \frac{D_l}{\tau} \left(\frac{\partial^2 C}{\partial r^2} + \frac{2}{r} \frac{\partial C}{\partial r} \right), \quad (1)$$

where C (mg-solute/L) is the concentration of the dissolved solute inside the porous beads, t (s) is the time, ρ_b

(g-alginate/L) is the medium bulk density, ε (dimensionless) is the porosity, P (mg-solute/g-alginate) is the adsorbed concentration, D_l is the liquid diffusion coefficient (m^2/s), τ (dimensionless) is the tortuosity factor, and r (m) is the radial distance. The characteristics of calcium alginate beads and initial zinc solution are presented in Table 1. The adsorbed concentration can be defined using the Freundlich and Langmuir isotherm [2,22].

Langmuir isotherm

The Langmuir isotherm assumes that the monolayer coverage of sorption of each molecule onto the surface has equal sorption activation energy [13]. It has been usually applied to determine the quantity and compare the performance of different biosorbents and is expressed as follows:

$$P = \frac{P_{\max} K_f C}{1 + K_f C}, \quad (2)$$

where P_{\max} (mg/g) is the maximum amount of adsorption, and K_f (L/mg) is the sorption equilibrium constant. Substitution of the Langmuir isotherm into Equation 1, the nonlinear model for a solute inside a porous bead becomes Equation 3:

$$\frac{\partial C}{\partial t} = D_a \left(\frac{\partial^2 C}{\partial r^2} + \frac{2}{r} \frac{\partial C}{\partial r} \right), \quad (3)$$

where D_a is the apparent diffusion coefficient, which is determined as follows:

$$D_a = \frac{D_l}{\tau \left(1 + \frac{\rho_b P_{\max} K_f}{\varepsilon (1 + K_f C)^2} \right)} \quad (4)$$

Table 1 Characteristics of calcium alginate beads and initial zinc solutions

Characteristic	Sample number			
	I	II	III	IV
Solid density (g/cm^3) [23]			0.8755	
Sodium alginate concentration (w/v,%)	1	2	1	2
Average wet weight (mg)	2.5	2.75	2.5	2.75
Average dry weight (mg)	0.335	0.5	0.335	0.5
Porosity	0.85	0.794	0.85	0.794
Average radius (cm)			0.055	
Initial zinc concentration (ppm)	100	100	300	300
Agitation rate (rpm)			250	
Diffusion coefficient (m^2/s) [24]			3.6×10^{-10}	
Solution bulk density (g-alginate/ cm^3)			≈ 1	
Water density (g/cm^3)			≈ 1	
Solution pH			4.5	
Temperature ($^{\circ}\text{C}$)			27	

Solution technique

Boundary and initial conditions, which were determined based on general assumptions and experimental conditions, were needed to solve Equation 1. Accordingly, the following boundary and initial conditions were used:

$$C(r, 0) = 0 \rightarrow \text{at } t = 0, \quad (5)$$

$$D_a \frac{\partial C}{\partial r} = 0 \text{ at } r = 0, \text{ at the center of the sphere,} \quad (6)$$

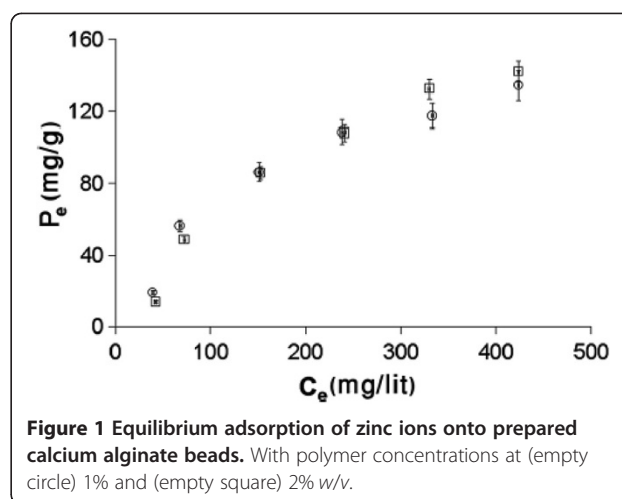
$$D_a \frac{\partial C}{\partial r} \Big|_{r=R} = k_c (C_b - C_R) \text{ at the outside boundary.} \quad (7)$$

In the derived model, the bead radius was divided into N stages using implicit finite difference method. According to the initial condition, it was considered that the prepared calcium alginate beads were devoid of zinc at the initial time of adsorption. Concentration of the center was parallelized to the next stage that was shown in Equation 6. As shown in Equation 7, the flow of solute onto the bead on the surface and the flow through the boundary layer into the bead as k_c which is the mass transfer coefficient (m/s), and C_b and C_R are the bulk solute concentration and the solute concentration at the bead surface, respectively [14,20]. Because the nonlinear model was applied to calculate solution concentration at different times, the implicit method was used to find the concentration profiles in the bead. Solving the numerical equation needs an assumption of the value of fitting parameters in Equation 3. The fitting parameters are τ and k_c which depend on the bead size, initial concentration of heavy metal in the solution, and agitation rate [14,20]. The mass transfer coefficient (k_c) can be regulated using the amount of equilibrium adsorption. In order to adjust the fitting parameters, k_c was first determined by calculating the minimum deviation between experimental and calculated adsorption equilibrium data at a constant τ , and then τ was estimated as the last and only remaining fitting parameter, which is independent from the calculated data of k_c as the estimated amount of equilibrium adsorption was constant during the determination of τ . The satisfied amount of tortuosity factor was confirmed when the deviation between experimental and calculated data was minimum.

Results and discussion

Adsorption isotherm

The adsorption capacities of the calcium alginate beads were compared at different concentrations in Figure 1. The beads were prepared with two different polymer concentrations, 1% and 2% w/v. It indicates that the saturation adsorption capacity increases with the increasing amount of initial zinc concentration at both



polymer concentrations. On the other hand, regarding to the same diameter of all beads, the change in the polymer concentration was effective on the porousness. Therefore, the saturation adsorption capacities of the prepared beads with the different concentrations were slightly dissimilar, owing to their near porosities. The Langmuir model was adaptively applied to describe the equilibrium data of zinc adsorption onto the beads. Results show that Langmuir isotherm has been much perfectly fitted to the equilibrium data compared with other isotherms. The Langmuir equilibrium constants and corresponding R^2 adjustment coefficients, which were calculated through the application of the least squares method, are shown in Table 2.

Pseudo first- and second-order models

The pseudo first- and second-order models were applied to test the experimental data for investigating the mechanism of the adsorption. The first-order rate expression of Lagergren [22] is given as follows:

$$\log(P_e - P) = \log P_e - \frac{k_1 t}{2.303}, \quad (8)$$

where P_e and P (mg/g) are the amounts of zinc ions, which were adsorbed into the adsorbents at equilibrium and at the time t , respectively, and k_1 (1/min) is the rate

Table 2 Langmuir isotherm constants for the prepared beads with the different polymer concentrations

Concentration	K_f (L/mg)	P_{\max} (mg/g)	R^2
Alginate 1% w/v	0.0058	200	0.991
Alginate 2% w/v	0.0035	250	0.994

constant of the pseudo first-order model. The experimental data could be fitted with a straight line of $\log(P_e - P)$ versus t , which can determine the flexibility of the model to predict the data. On the other hand, the second-order kinetic model is expressed as follows [22]:

$$\frac{t}{P} = \frac{1}{k_2 P_e^2} - \frac{t}{P_e}, \quad (9)$$

where k_2 (g/mg min) is the rate constant of the pseudo second-order model. There should be a linear relationship in the plot of t/P versus t if second-order kinetics is applicable. The slopes and intercepts of the plots give the second-order rate constant k_2 and P_e . The model is capable of predicting the behavior of all range of adsorption data without any parameters in advance and to show a rapport with chemical adsorptions, which are the rate-controlling steps [2,22,25]. Table 3 represents the calculated results obtained from the first- and second-order kinetic models and a comparison of the results with correlation coefficients (R^2). The correlation coefficients for the first-order model were low. Figure 2 shows both pseudo-model behaviors in prediction of the experimental data.

The pseudo-kinetic models are not in good agreement with the pre-equilibrium times of adsorptions, but the prediction of the second-order model shows a better convergence at equilibrium time rather than the first-order model.

The second-order kinetic model generally presents a more or less rational prediction as it showed high correlation coefficients in certain samples. The calculated P_e values resulted from second-order kinetic model were in a good fit with the experimental P_e values.

Furthermore, the first-order model of Lagergren could not support perfectly all ranges of contact time and was not generally adjustable in the initial stage of the adsorption processes [2,22,25]. Figure 2 illustrates that second-order model tends to follow the experimental data better than first-order model as the correlation coefficients for the second-order kinetic model (that are displayed in Table 3) are higher than those of first-order adsorption model. In order to

determine the deviations between all calculated and experimental data, root mean square deviation (σ_{RMSD}) was calculated as follows:

$$\sigma_{\text{RMSD}} = \left[\frac{1}{n} \sum_{i=1}^n \left(\frac{P_{\text{Exp}} - P_{\text{Cal}}}{P_{\text{Exp}}} \right)^2 \right]^{0.5} \times 100. \quad (10)$$

Table 4 shows that the first-order model could not follow the data as it has an average σ_{RMSD} of 15.61%, but the second-order model has a comparatively more rational agreement. Although a better agreement was shown for samples I and II, the average σ_{RMSD} was calculated to be 10.59%. Overall, Table 4 shows a high value of σ_{RMSD} of the models, indicating a poor agreement with the experimental data. It is obviously alleged that the adsorption of zinc ions onto the prepared calcium alginate beads could be the rate-limiting step, owing to the better agreement of the second-order model [2].

Nonlinear model

The nonlinear diffusion model was applied to model the experimental data. The adsorption behavior has been described with the Langmuir adsorption equation. The Langmuir equation constants are shown in Table 2. Therefore, the results indicate a single molecule layer adsorption [2,22]. The nonlinear model was numerically solved with the implicit, finite difference approximation using the Newton-Raphson's method [26]. The data were fitted using τ and k_c as a lumped parameter applied to describe the boundary layer effect as the fitting parameters. Figure 2a shows that the calculated amount of adsorbed zinc ions increased as the time increases and reached an equilibrium value after 130 min, which is approximately equal to the experimental equilibrium time. In addition, a reasonable agreement is shown in the following experimental data and in fitting the balanced adsorption amount. The fitting parameters (which depend on some effective conditions such as the agitation rate and initial concentration of the solutions [14,20]) were determined with the calculation of σ_{RMSD} between the predicted and experimental data. Furthermore, Figure 2b,c,d shows the same adaptive behaviors in estimating the experimental data with high accuracies as the predicted data are fitted

Table 3 Comparison of first- and second-order adsorption rate constant and calculated/experimental P_e values at different samples

Sample number	$P_{e, \text{Exp}}$ (mg/g)	First-order kinetic model			Second-order kinetic model		
		k_1 (1/min)	$P_{e, \text{Cal}}$ (mg/g)	R^2	k_2 (g/mg min)	$P_{e, \text{Cal}}$ (mg/g)	R^2
I	53.4	0.032	54.70	0.959	0.0025	53.66	0.9984
II	38.87	0.019	37.58	0.964	0.0011	38.22	0.9911
III	96.14	0.024	89.53	0.964	0.0011	97.12	0.9953
IV	94.74	0.028	96.2	0.995	0.0008	96.98	0.995

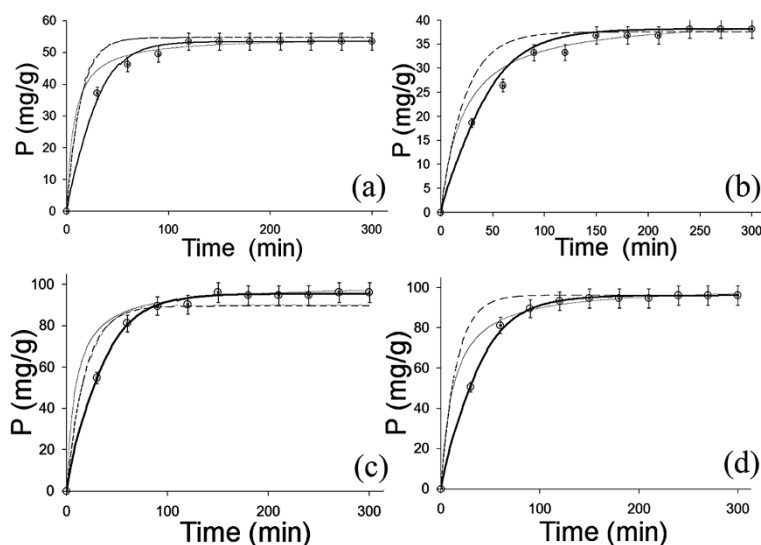


Figure 2 Comparison of first-order (dotted line), second-order (thin line), and the non-linear (thick line) adsorption kinetics. These are zinc ions onto the prepared calcium alginate beads with experimental data (empty circle): (a) sample I, (b) sample II, (c) sample III, and (d) sample IV.

at the balanced adsorption data. Table 5 shows the estimated fitting parameters and the equilibrium adsorption data in different conditions. The factor of tortuosity was calculated from 9.52 to 16.8 with the changing of porosity and initial concentration of the zinc solution. The value of τ depends on the characteristics of the beads, and the high value of τ indicates a slow diffusion into the adsorbent. It is worth mentioning that the calculated τ is independent on the conditions of initial solution and sorbent loading characteristics [14,20]. It is important to notice that increasing the porosity of the beads from 0.794 to 0.85 decreases the factor of tortuosity, but the changes of porosity do not have any significant effect on the τ values at high zinc concentration in the initial solution (300 mg/L). The fitted values of k_c were estimated to be 1.39×10^{-7} to 2.21×10^{-7} m/s, showing the independence of the uptake kinetics on agitation rate. Therefore, the diffusive transport in the prepared calcium alginate beads at high-speed agitation rate (250 rpm) was limited by pore diffusion that indicated the rate-limiting step [14,20]. Although it seems

that the kinetic pseudo models are flexible for the data, the nonlinear model comes with lower σ_{RMSD} values compared with the pseudo models. The calculated σ_{RMSD} values of the pseudo models showed a disparity in the prediction of experimental data (Table 4). Interestingly, the nonlinear model has an average σ_{RMSD} value of 2.66% which is at least four times smaller than that of the pseudo models, indicating a more reliable prediction capability of the nonlinear model in the adsorption process. In all samples, the mathematical model provided an adjustable behavior and perfectly fitted the data.

Experimental

Materials

Sodium alginate (medium viscosity, 3,500 cps, 2% w/v aqueous solution at 25°C) was purchased from Sigma-Aldrich Corporation (St. Louis, MO, USA). Zinc sulfate pentahydrate ($\text{ZnSO}_4 \cdot 5\text{H}_2\text{O}$), sodium hydroxide (NaOH), hydrochloric acid (HCl), and calcium chloride (CaCl_2)

Table 4 Comparison of the calculated σ_{RMSD} of the kinetic models for the different samples

Kinetic models	σ_{RMSD} samples				
	I	II	III	IV	Average
First-order kinetic model	11.68	18.71	11.39	20.67	15.61
Second-order kinetic model	6.46	9.82	13.11	12.96	10.59
Nonlinear Model	2.85	5.11	1.35	1.31	2.66

Table 5 Calculated fitting parameters of the nonlinear model in adsorption of zinc ions

Fitting parameters in the nonlinear model	Sample number			
	I	II	III	IV
τ	9.52	14.54	16.53	16.8
k_c (m/s)	2.21×10^{-7}	1.39×10^{-7}	1.44×10^{-7}	1.92×10^{-7}
$P_{e, \text{Cal}}$ (mg/g)	53.454	38.217	95.496	96.099

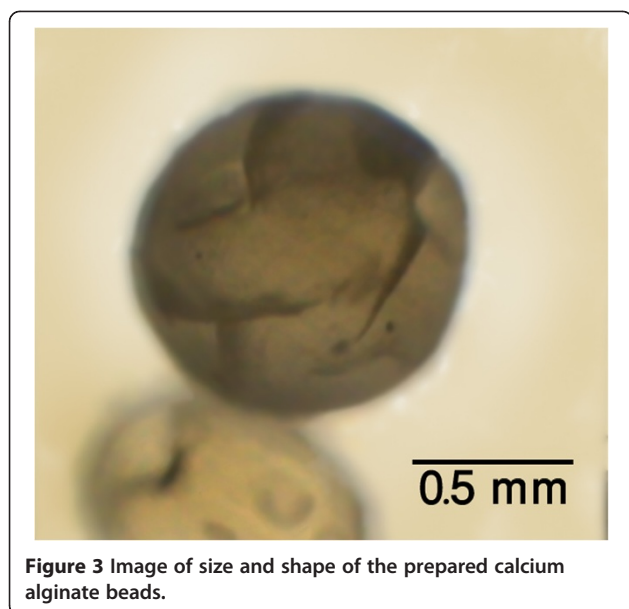


Figure 3 Image of size and shape of the prepared calcium alginate beads.

were purchased from Merck AG (Darmstadt, Germany) and were used as received without further purification.

Preparation of the porous calcium alginate beads

Calcium alginate beads were prepared according to the method of Moghadam et al. [27]. Briefly, sodium alginate solution was prepared by dissolving 1 and 2 g of the polymer in 99 and 98 mL of distilled water, respectively. The solution of the sodium alginate flowed through a stainless steel nozzle via a syringe pump at a 100-mL/h flow rate. Electric field strength was set using a high voltage, DC power supply. The liquid meniscus at the tip of the nozzle was affected by the adjusted electric field where droplets were formed and inundated. The droplet was dripped into a container where ionotropic gelation occurred. The solution made in the container was calcium chloride (3% w/v). The solution was gently stirred for 5 min while the droplets were cured. The prepared calcium alginate beads were washed with distilled water and acetone and dried until the water completely evaporated. The size of the dried calcium alginate beads was measured randomly using the images processor (SAIRAN Co., Iran). Figure 3 shows the size and shape of the prepared calcium alginate beads.

Calculation of the porosity of calcium alginate beads

Porosity of the calcium alginate beads was calculated from the density of the alginate and the weight change before and after drying [1]; the following formula was applied:

$$\varepsilon = \frac{(W_W - W_D)/\rho_W}{W_D/\rho_{AL} + (W_W - W_D)/\rho_W}, \quad (11)$$

where ε is the porosity of the calcium alginate beads, W_W

(g) is the weight of the wet calcium alginate bead before drying, W_D (g) is the weight of the dried calcium alginate bead, ρ_W is the density of water, and ρ_{AL} is the density of the alginate (Table 1).

Adsorption process

Standard zinc solutions with certain concentrations were prepared by dissolving $ZnSO_4 \cdot H_2O$ into 500 mL of distilled water. In experiments of the batch kinetic adsorption, 50 mL of standard solution with an adjusted pH (4.5) and 25 mg of the calcium alginate beads were shaken with the use of a shaker (250 rpm) in a thermostat water bath. The concentration of zinc was determined by an atomic absorption spectrophotometer (SPCA-626D, Shimadzu Corporation, Kyoto, Japan). The amount of zinc absorbed onto the calcium alginate beads, P (mg/g dried beads), was calculated using the following equation:

$$P = \frac{V(C_0 - C)}{W_D}, \quad (12)$$

where V (L) is the volume of the zinc solution, C_0 (mg/L) is the initial zinc concentration, C (mg/L) is the zinc concentration at a certain time, and W_D (g) is the weight of the dried calcium alginate beads [2,3].

Conclusions

In this study, calcium alginate beads were prepared using the electrospray method as a biosorbent, and adsorption of zinc ions was investigated using the batch equilibrium method. In addition, the effective parameters on adsorption such as porosity were analyzed with the suggested nonlinear model, and the predicted behavior of the nonlinear model in the prediction of experimental data was compared with that of the pseudo-kinetic models. The pseudo models could not follow the experimental data at pre-equilibrium time spans of the adsorption processes as high deviations from the experimental data were observed by the calculation of σ_{RMSD} .

The fitting parameters (τ and k_c) of the nonlinear model were estimated using minimum σ_{RMSD} between the experimental and calculated data. According to porosity and solution concentration, τ and k_c (m/s) were calculated from 9.52 to 16.8 and from 1.39×10^{-7} to 2.21×10^{-7} m/s, respectively. The nonlinear model demonstrated that diffusive transport through the beads was limited by pore diffusion. The nonlinear model was shown to possess a superb adaptive behavior in the prediction of zinc adsorption in the different samples as its average σ_{RMSD} was calculated to be 2.66%, which was the lowest σ_{RMSD} compared to all other models. The nonlinear model provided a good fit to the experimental data as the calculated equilibrium adsorptions were shown to be in good agreement with their experimental counterparts.

Abbreviations

C: Zinc concentration (mg/L); C_b : Bulk solute concentration (mg/L); C_e : Equilibrium zinc concentration (mg/L); C_s : Solute concentration at the surface of the sphere (mg/L); C_0 : Initial zinc concentration (mg/L); D_a : Apparent diffusion coefficient; D : Diffusion coefficient (m^2/s); k_1 : Rate constant of pseudo first-order model (1/min); k_2 : Rate constant of pseudo second-order model (g/mg·min); k_c : Mass transfer coefficient (m/s); K_f : Langmuir constant (mg/g); n : The number of experimental data; P : Adsorbed concentration (mg/g); P_{cal} : Calculated adsorbed concentration (mg/g); P_e : Equilibrium adsorbed concentration (mg/g); P_{Exp} : Experimental adsorbed concentration (mg/g); P_{max} : Maximum monolayer amount of adsorption (mg/g); R : Radius (m); R^2 : Correlation coefficient; T : Time (s); W_D : Weight of dried calcium alginate bead (g); W_W : Weight of wet calcium alginate bead before drying (g); V : Volume of zinc solution (L); τ : Tortuosity factor; ρ_b : Bulk density (g/cm³); ϵ : Porosity; ρ_w : Density of water; ρ_{AL} : Density of sodium alginate; σ_{RMSD} : Root mean square deviation.

Competing interests

The authors declare that they have no competing interests.

Authors' contributions

MHK carried out the experiments, studied the mechanisms of the adsorption, wrote the adsorption nonlinear model program, analyzed the data, and drafted the manuscript. MM helped in some parts of the experiments. MK participated in the interpretation of results. SRK read and edited the manuscript and commented on it. All the authors read and approved the final manuscript.

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