

# Knot Tightening by Constrained Gradient Descent

Ted Ashton, Jason Cantarella, Michael Piatek, and Eric J. Rawdon

## CONTENTS

1. Introduction
  2. A Discretization for the Ropelength Problem
  3. Bridging Theory and Computation
  4. Program Design
  5. Results of Computations
  6. Future Directions
  7. Appendix: Ropelength Data
- References

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We present new computations of approximately length-minimizing polygons with fixed thickness. These curves model the centerlines of “tight” knotted tubes with minimal length and fixed circular cross-section. Our curves approximately minimize the ropelength (or quotient of length and thickness) for polygons in their knot types. While previous authors have minimized ropelength for polygons using simulated annealing, the new idea in our code is to minimize length over the set of polygons of thickness at least one using a version of constrained gradient descent.

We rewrite the problem in terms of minimizing the length of the polygon subject to an infinite family of differentiable constraint functions. We prove that the set of variations of a polygon of thickness one that does not decrease thickness to first order is a finitely generated polyhedral cone, and give an explicit set of generators. Using this cone, we give a first-order minimization procedure and a Karush–Kuhn–Tucker criterion for polygonal-ropelength criticality.

Our main numerical contribution is a set of 379 almost-critical knots and links, including all prime knots with ten and fewer crossings and all prime links with nine and fewer crossings. For links, these are the first published ropelength figures, and for knots they improve on existing figures. We give new maps of the self-contacts of these knots and links, and discover some highly symmetric tight knots with particularly simple-looking self-contact maps.

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## 1. INTRODUCTION

### 1.1. Overview

Knots tied in rope are flexible machines that organize tensions and contact forces to bind tightly and resist unraveling. As a technology, knots have proved remarkably effective. For this reason there is a vast body of knowledge about their practical uses. Yet in many ways, the design of these machines remains mysterious. As early as 1987, Maddocks and Keller were able to study different types of hitches and predict their holding power by an analysis of their equilibrium shapes [Maddocks and Keller 87]. But these shapes were rather simple, and there was no way

2000 AMS Subject Classification: 49M25, 49Q10, 53A04, 57M25  
Keywords: ropelength, tight knots, ideal knots, constrained gradient descent, sparse nonnegative least-squares problem (snls), knot-tightening

to infer the structures of more complicated knots from these examples. It was obvious that what was needed was data, and by the end of the century, a series of numerical experiments in knot-tightening was underway [Rawdon 97, Pierański 98, Laurie 98, Sullivan 02]. This paper describes a new computational approach to knot-tightening that yields improved numerical results (a preliminary report on some of our findings appeared in the conference proceedings [Cantarella et al. 05]). To build our method, we derive some new results in the theory of ropelength for polygonal knots.

### 1.2. Defining the Problem

Given any space curve  $\gamma$ , we can define the *thickness*  $\text{Thi}(\gamma)$  of  $\gamma$  to be the supremal  $\epsilon$  for which any point in an  $\epsilon$ -neighborhood of  $\gamma$  has a unique nearest neighbor on the curve.<sup>1</sup> Any curve with nonzero thickness is  $C^{1,1}$  (that is, it is  $C^1$  with a Lipschitz first derivative) [Federer 59, Cantarella et al. 02]. Given this, the following proposition has been proved.

**Proposition 1.1.** [Litherland et al. 99] *If  $\gamma$  is a  $C^1$  curve, then the thickness  $\text{Thi}(\gamma)$  is given by the supremal radius of all embedded tubes formed by taking the union of disks of uniform radius centered on  $\gamma(s)$  in the planes normal to  $\gamma'(s)$ .*

This idea of thickness was first proposed in [Krötenheerdt and Veit 76], see also [Krötenheerdt and Veit 05], and was rediscovered in the 1990s [Nabutovsky 95, Buck and Orloff 95]. The thickness can be used to define a scale-invariant quantity called *ropelength*:

**Definition 1.2.** The *ropelength* of a curve  $\gamma$  is defined by

$$\text{Rop}(\gamma) = \frac{\text{Len}(\gamma)}{\text{Thi}(\gamma)},$$

where  $\text{Len}(\gamma)$  is the length of  $\gamma$ . The *minimal ropelength*  $\text{Rop}(L)$  of a knot or link type  $L$  is the minimal ropelength of all curves in that knot or link type.

The knot-tightening problem is to find and describe the minimal-ropelength curves in a given knot type. It is known that such curves exist, but very few examples are known explicitly (see [Gonzalez and de la Llave 03, Gonzalez et al. 02, Cantarella et al. 02]). Once found (or

computed to sufficient accuracy), these configurations have been used to predict the relative speed of DNA knots under gel electrophoresis [Katritch 96], the pitch of double-helical DNA [Micheletti et al. 99], the average values of different spatial measurements of random knots [Dobay et al. 03], and the breaking points of knots [Pierański et al. 01]. They also provide a model for the structure of a class of subatomic particles known as glueballs [Buniy and Kephart 03].

### 1.3. Another Form of the Problem

Let  $\gamma: S^1 \rightarrow \mathbb{R}^3$  now be a  $C^2$  parameterized curve, and define the self-distance function  $d: S^1 \times S^1 \rightarrow \mathbb{R}$  of  $\gamma$  by  $d(s, t) := \|\gamma(s) - \gamma(t)\|$ . As usual, let  $\kappa(s)$  denote the curvature of  $\gamma$ . We then define the set  $\text{dcsd}(\gamma)$  of *doubly critical self-distances* to be the set of critical points of  $d$  with  $s \neq t$ . Taking the partial derivatives of  $d$ , we see that  $(s, t) \in \text{dcsd}(\gamma)$  if and only if

$$\langle \gamma(s) - \gamma(t), \gamma'(s) \rangle = 0 \quad \text{and} \quad \langle \gamma(s) - \gamma(t), \gamma'(t) \rangle = 0.$$

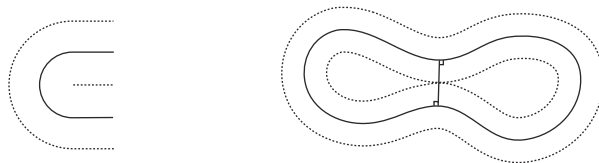
A key idea in [Litherland et al. 99] is that for any  $\tau < \text{Thi}(\gamma)$ , the surface of the tube of radius  $\tau$  around  $\gamma$  has no self-intersections and is  $C^2$  smooth. But when  $\tau = \text{Thi}(\gamma)$ , the tube is pinched or has a tangential self-intersection. This leads to an alternative characterization of thickness:

**Theorem 1.3.** [Litherland et al. 99] *The thickness of  $\gamma$  is the minimum of*

$$\min_s \frac{1}{\kappa(s)} \quad \text{and} \quad \min_{(s,t) \in \text{dcsd}(\gamma)} \frac{d(s,t)}{2}.$$

Figure 1 shows curves in which the first and second of these terms control the thickness.

Since length and thickness scale together, minimizing ropelength is the same as minimizing length over the set of curves with thickness at least one. Since thickness is a min-function, the condition  $\text{Thi}(\gamma) \geq 1$  can be viewed as an infinite family of inequality constraints on  $\gamma$ . These



**FIGURE 1.** The thickness of a smooth curve  $\gamma$  is controlled by curvature (as in the left-hand picture) and the length of chords in  $\text{dcsd}(\gamma)$  (as in the right-hand picture).

<sup>1</sup>Federer referred to this number as the *reach* of  $\gamma$  [Federer 59].

constraints are active at places where the tube around  $\gamma$  forms kinks (where  $1/\kappa$  is in control of the minimum in Theorem 1.3) or has self-contacts (where the self-distance  $d(s, t)/2$  is in control of the minimum).

#### 1.4. Numerical Approaches to the Knot-Tightening Problem

Previous authors have defined discretized versions of thickness for polygons or spline curves and viewed the problem as one of minimizing the nonsmooth quotient of length and thickness. The advantage of this approach is that it is a very simple and robust way to obtain approximately ropelength-minimizing curves. The disadvantage is that it is very difficult to take advantage of the fact that thickness (as given in Theorem 1.3) is a min-function.

Our approach is to define a discrete version of thickness as a min-function and think of the problem as one of minimizing a differentiable function  $\text{Len}(\mathcal{V})$  subject to a family of differentiable constraints  $\text{Thi}_p(\mathcal{V}) \geq 1$ . While our approach will not quite fit into the standard framework of constrained optimization (our family of constraints is infinite), we will be able to define a version of constrained gradient descent that minimizes polygonal ropelength effectively.

#### 1.5. Theoretical Framework

For an equilateral space polygon  $\mathcal{V}$  we first prove that our function  $\text{Thi}_p(\mathcal{V})$  can be written as a minimum over a fixed compact family of differential functions. From here we use Clark’s theorem to show that  $\text{Thi}_p$  has a one-sided derivative in the direction of any variation  $W$  of  $\mathcal{V}$ . For a polygon with  $\text{Thi}_p(\mathcal{V}) = 1$  we use these derivatives to define a cone of infinitesimal variations  $I(\mathcal{V})$  that do not decrease  $\text{Thi}_p$  to first order and the dual cone of “resolvable” variations  $R(\mathcal{V})$ . Our next main theorem is that  $R(\mathcal{V})$  is a finitely generated polyhedral cone whose generators are the gradients of the lengths of certain chords of the polygon (called *struts*) and of a function of certain turning angles of the polygon (called *kinks*). We give explicit formulas for these gradients in terms of the vertex positions.

We then compute the gradient of  $\text{Len}(\mathcal{V})$  and define the constrained gradient of length to be the projection of  $\text{Len}(\mathcal{V})$  onto the polyhedral cone  $I(\mathcal{V})$ . At this point we give the expected result that a polygon is critical for polygonal ropelength if and only if the constrained gradient of length is zero. Equivalently, a polygon is critical for polygonal ropelength if there is a set of positive Lagrange multipliers on the struts and kinks that combine to equal

the negative of the length gradient. The theory section ends with a discussion of how to compute the constrained gradient numerically.

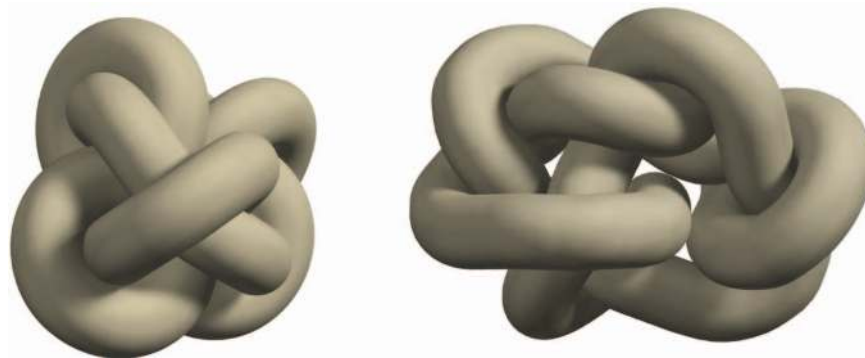
#### 1.6. Numerical Methods

Sections 3 and 4 describe the design of our polygonal-ropelength-minimizing software. Our algorithm essentially consists in computing the constrained gradient of length and taking small steps in this direction until the constrained gradient is sufficiently small. However, the details of the process are not quite so simple. Since the constraint functions are nonlinear, even steps that are in the direction of the constrained gradient violate some constraints to second order. Further, newly active constraints are discovered throughout the run as previously distant sections of tube come into contact with one another. As a result, we must choose step sizes carefully and correct errors periodically. It is also important that the algorithm run efficiently, since the size of our problem (a few thousand variables and a similar number of active constraints) is fairly large.

We have solved these technical and engineering problems and used our software to minimize all prime knots with ten or fewer crossings and all prime links with nine or fewer crossings, for a total of 379 different knot and link types. We intend to address the ropelength of composite knots and links in a future publication.

#### 1.7. New Ropelength Bounds

We check our figures against previous computations of the minimum ropelength of knots and links and against some of the few known theoretical results for the lengths of tight links. Our results improve on all previously published computational results except for the trefoil knot. For example, we improve the best known upper bound for the ropelength of the well-studied figure-eight knot  $4_1$  by 0.06 to 42.0887 (as compared to the bound of [Carlen et al. 05]) and improve the best known upper bound for the ropelength of the  $9_{20}$  knot by 8.12% to 80.2219 (compared to the bound of [Rawdon 03]). To get a sense of the difference between the configurations produced by our method and the configurations produced by the simulated annealer of [Rawdon 03], we show both configurations in Figure 2. For links, our figures are the first computational results to appear in print, but compare well to known theoretical results. For example, the upper bound provided by our computation of the Borromean rings link  $6_2^3$  is 58.0070—within 0.0017% of the exact value around 58.0060 suggested by



**FIGURE 2.** These two images of the  $9_{20}$  knot show the tightest configurations obtained by our algorithm (left) and by the TOROS algorithm described in [Rawdon 03] (right). It is clear that our algorithm performs better once there are many self-contacts in the knot. In fact, the ropelength of the left-hand configuration is bounded by 80.2219, while the configuration on the right has ropelength bounded by 87.31. (Figure is available in color online)

[Cantarella et al. 06], while our computation of the tight shape of the “simple chain” link is 41.7086588—within 0.02% of the correct value of  $6\pi + 2$  [Cantarella et al. 02].

We also compared our results to those of [Gilbert 11], which are unpublished but available on Bar-Natan’s *Knot Atlas* wiki. Gilbert provides Fourier coefficients and instructions for reconstructing the vertices of his configurations from those data. We followed his instructions, but our software did not verify his claimed ropelength numbers.<sup>2</sup> According to our measurement of the ropelength of Gilbert’s configurations, our knots are tighter in all cases but  $2_1^2$  by an average of 3.714%, with some outliers, such as our  $9_{37}^2$  link, which is 71% shorter. If we compare our results to Gilbert’s claimed ropelengths, our knots and links are tighter in 309 cases and less tight in 33. Overall, our knots and links are (on average) 1.104% tighter than the bounds claimed by Gilbert, with our  $9_{28}^2$  link about 4% shorter than Gilbert’s claim.

### 1.8. Self-Contact Maps

The authors of [Schuricht and von der Mosel 04] and [Cantarella et al. 06] have given versions of a ropelength criticality criterion for knots without kinks that state roughly that a knot  $\gamma$  is ropelength-critical when the elastic force given by the gradient of the length of the curve is balanced by a system of Lagrange multipliers on the self-contacts of the tube around  $\gamma$ . The latter au-

thors used their condition to derive a ropelength-critical configuration of the Borromean rings and a surprising ropelength-critical configuration of a clasp formed by two tubes stretched across each other.

In both of these examples, the most difficult part of the result was the deduction of the structure of the set of self-contacts for the tight configuration. Since these contact maps are very sensitive to small perturbations of the centerline, it has been difficult to resolve them using previous numerical methods.<sup>3</sup> These contacts and the system of Lagrange multipliers on them are explicitly computed by our algorithm, allowing us to give medium-quality contact maps for a large number of knots and links. The contact maps offer some support for the hypothesis that a relatively small number of structures may reappear often in tight knots and links.

### 1.9. Previous Work

This is not the first time gradient-like methods have been attempted for the knot-tightening problem. Our work has been inspired by Piotr Pierański’s SONO algorithm [Pierański 98], which follows a version of the length gradient, but does not include an explicit resolution of this vector against the active constraints. Our thinking is also informed by John Sullivan’s “energy-ropelength method” [Sullivan 02], which optimizes thickness instead of length, estimating the maximum diameter of a uniform embedded tube around the core curve by an  $L^p$  average of the radii of embedded cross-sectional disks

<sup>2</sup>Our measurement of curvature by MinRad is sensitive to edge length and seems to come out much larger than his ropelengths would indicate. This is probably a discretization effect, and it is certainly possible that the Fourier knots defined by Gilbert’s data have ropelengths corresponding to Gilbert’s claimed numbers.

<sup>3</sup>The notable exception to this rule has been the “biarc” spline-annealing method of [Carlen et al. 05], which has produced well-resolved contact maps for the  $3_1$  and  $4_1$  knots.

and minimizing the resulting smooth functional using the conjugate-gradient implementation in Brakke’s `evolvr` [Brakke 92].

## 2. A DISCRETIZATION FOR THE ROPELENGTH PROBLEM

### 2.1. Polygonal Thickness

Consider a closed space polygon  $\mathcal{V}$  with vertices  $v_1, \dots, v_V$  and edges  $e_1, \dots, e_V$ . We will think of  $\mathcal{V}$  as the vector  $(v_1, \dots, v_V)$  in  $(\mathbb{R}^3)^V = \mathbb{R}^{3V}$ , and assume that all subscripts on vertices and edges are taken modulo  $V$ . The unit tangent vector  $T_i$  to each edge of a polygon is well defined on the interior of the edge. At the vertex  $v_i$  joining edges  $e_{i-1}$  and  $e_i$ , there are two tangent vectors  $T_{i-1}$  and  $T_i$ . The curvature of  $\mathcal{V}$  at  $v_i$  is usually thought of as a delta function whose mass is given by the turning angle  $\theta_i$  from  $T_{i-1}$  to  $T_i$ . We will use a somewhat different definition of curvature for polygons:

**Definition 2.1.** The *minimum radius of curvature* (or  $\text{MinRad}$ ) of  $\mathcal{V}$  at  $v_i$  is given by the radius of the unique circle that is tangent to the two edges meeting at  $v_i$  and that touches the midpoint of the shorter one.

It is shown in [Rawdon 97] that if  $\theta_i$  is the turning angle of  $\mathcal{V}$  at  $v_i$ , then we can give  $\text{MinRad}(v_i)$  (and define  $\text{MinRad}^\pm(v_i)$ ) by the expressions

$$\begin{aligned} \min \left\{ \frac{|e_{i-1}|}{2 \tan(\theta_i/2)}, \frac{|e_i|}{2 \tan(\theta_i/2)} \right\} \\ = \min\{\text{MinRad}^-(v_i), \text{MinRad}^+(v_i)\}. \end{aligned} \quad (2-1)$$

It is clear that while  $\text{MinRad } v_i$  is not necessarily a differentiable function, the two functions  $\text{MinRad}^\pm v_i$  are differentiable when they are defined. The motivation for this definition is that we can round off all the corners of  $\mathcal{V}$  by splicing in these circle arcs, generating a  $C^{1,1}$  curve with radii of curvature equal to the  $\text{MinRad}(v_i)$ . We could have defined  $\text{Thi}_p(\mathcal{V})$  to be the thickness of this curve. It turns out, however, that there is no closed-form computation for that number (although it can be computed approximately, as we will see in Section 5.3).

We now define a set corresponding to  $\text{dcsd}$  for polygons:

**Definition 2.2.** Let  $\text{dcsd}(\mathcal{V})$  be the set of  $(p, q)$  on  $\mathcal{V}$  with  $p \neq q$  that are local minima of the self-distance function on  $\mathcal{V}$ .

There are several possible cases for  $(p, q)$  in  $\text{dcsd}(\mathcal{V})$ , since the polygon might have a vertex at one or both of the endpoints of the chord. These are shown in Figure 3.

We can then define Rawdon’s polygonal thickness:

**Definition 2.3.** The polygonal thickness  $\text{Thi}_p(\mathcal{V})$  of a space polygon  $\mathcal{V}$  without self-intersections is given by the minimum

$$\text{Thi}_p(\mathcal{V}) := \min \left\{ \min_i \text{MinRad}(v_i), \min_{(p,q) \in \text{dcsd}(\mathcal{V})} \frac{d(p,q)}{2} \right\}.$$

We have carefully constructed this definition so that when polygons  $\mathcal{V}_n$  with increasing numbers of edges are inscribed in a space curve  $\gamma$  under some mild geometric hypotheses, then  $\text{Thi}_p(\mathcal{V}_n) \rightarrow \text{Thi}(\gamma)$  [Rawdon 97, Rawdon 98, Rawdon 03].

### 2.2. The Problem with $\text{Thi}_p$

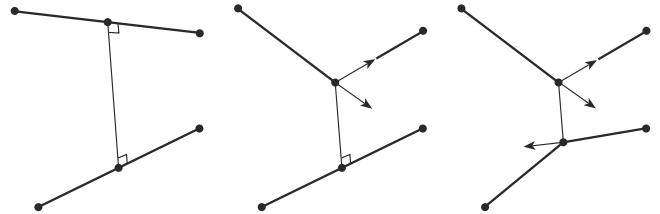
Definition 2.3 allows us to define the set of polygons with  $\text{Thi}_p(\mathcal{V}) \geq 1$  as the polygons obeying a family of constraints of the form  $\text{MinRad}(v_i) \geq 1$  and  $d(p, q) \geq 2$  for  $(p, q) \in \text{dcsd}(\mathcal{V})$ . This is almost the standard form for constrained optimization problems

$$\min_{\mathcal{V} \in \mathbb{R}^{3V}} f(\mathcal{V}) \quad \text{subject to } g_i(\mathcal{V}) \geq 0, \quad (2-2)$$

where  $f$  and the  $g_i$  are differentiable. The problem is that the set of constraint functions  $d(p, q)$  for  $(p, q) \in \text{dcsd}(\mathcal{V})$  depends on the polygon. We will need a common set of constraint functions for all polygons in a neighborhood of a solution.

### 2.3. Constraint Thickness

To solve this problem, we will define a new thickness measure for polygons called the *constraint thickness* that is given in the form 2-2. We will then prove that for



**FIGURE 3.** We see three types of local minima of the self-distance function on a space polygon  $\mathcal{V}$  in the three-dimensional drawings above. From left to right, these are an *edge-edge* pair, a *vertex-edge* pair, and a *vertex-vertex* pair.

equilateral polygons, the new constraint thickness defines the same set of polygons as the old polygonal thickness.

We first define a subset of the pairs of points on a polygon:

**Definition 2.4.** For a given positive  $\tau$  and  $\ell$ , let  $\theta(\tau, \ell)$  be the turning angle of a pair of edges of length  $\ell$  with  $\text{MinRad} = \tau$ . We set

$$\text{VB}(\tau, \ell) = \left\{ (p, q) \in \mathcal{V} \times \mathcal{V} : \text{vb}(p, q) \geq \frac{\pi}{\theta(\tau, \ell)} \right\},$$

where  $\text{vb}(p, q)$  is the smaller number of vertices between points  $p$  and  $q$  (counting  $p$  and/or  $q$  if they are vertices and remembering that there are two ways to determine this number, depending on which way we go from  $p$  to  $q$  around the closed polygon  $\mathcal{V}$ ).

We note that an easy computation shows that  $\theta(\tau, \ell) = 2 \arctan(\ell/2\tau)$ . We can now define our new thickness measure. If  $p$  and  $q$  are on different components, we take  $\text{vb}(p, q) = \infty$ .

**Definition 2.5.** The  $(\tau, \ell)$ -constraint thickness  $\text{CThi}(\tau, \ell, \mathcal{V})$  of a polygon  $\mathcal{V}$  is given by

$$\begin{aligned} & \text{CThi}(\tau, \ell, \mathcal{V}) \\ &= \min \left\{ \min \frac{\text{MinRad}(v_i)}{\tau}, \min_{(p,q) \in \text{VB}(\tau, \ell)} \frac{d(p, q)}{2} \right\}. \end{aligned}$$

We note that  $\mathcal{V}$  need not be equilateral or have edge length  $\ell$  to define the constraint thickness. We can view  $\tau$  as the “stiffness” of the rope (compare the definition of  $\lambda$ -thickness in [Cantarella et al. 11] and [Buck and Rawdon 04]), since it provides a lower bound on the radius of curvature of a tube of unit radius. Although our theory (and our code) should work for any  $\tau \geq 1$ , we have not experimented with values for  $\tau$  other than 1 and so will write the  $(1, \ell)$ -constraint thickness  $\text{CThi}(1, \ell, \mathcal{V})$  as  $\text{CThi}(\ell, \mathcal{V})$ .

We can now prove that  $\text{CThi}(\ell, \mathcal{V})$  is an equivalent thickness to  $\text{Thi}_p$  for equilateral polygons of edge length  $\ell$ .

**Theorem 2.6.** If  $\mathcal{V}$  is an equilateral polygon of edge length  $\ell$ , then  $\text{Thi}_p(\mathcal{V}) \geq 1 \iff \text{CThi}(\ell, \mathcal{V}) \geq 1$ .

To prove the theorem we will need a lemma (cf. [Rawdon 00, Lemma 13]):

**Lemma 2.7.** If  $\mathcal{V}$  is an equilateral polygon of edge length  $\ell$  and  $\text{MinRad} \geq \tau$ , then  $\text{dcsd}(\mathcal{V}) \subset \text{VB}(\tau, \ell)$ .

*Proof:* The proof has two parts. In the first, we show that the shorter of the two arcs between any  $(p, q) \notin \text{VB}(\tau, \ell)$  has total curvature  $t$  less than  $\pi$ , while in the second we will show that any pair joined by such an arc cannot be in  $\text{dcsd}(\mathcal{V})$ . So suppose that  $t \geq \pi$ . We will prove that  $(p, q) \in \text{VB}(\tau, \ell)$ .

Since  $\text{MinRad}(\mathcal{V}) \geq \tau$ , we know that each turning angle of  $\mathcal{V}$  is less than  $\theta(\tau, \ell)$ . If the total curvature of the arc joining  $p$  and  $q$  is at least  $\pi$ , then  $\text{vb}(p, q) \cdot \theta(\tau, \ell) \geq \pi$ , so

$$\text{vb}(p, q) \geq \frac{\pi}{\theta(\tau, \ell)}$$

and  $(p, q) \in \text{VB}(\tau, \ell)$ , proving the claim.

Now suppose that  $(p, q) \in \text{dcsd}(\mathcal{V})$ . We claim that the total curvature  $t$  of each arc joining  $p$  and  $q$  is at least  $\pi$ , and hence that  $(p, q) \in \text{VB}(\tau, \ell)$ . Suppose not. The arc of  $\mathcal{V}$  joining  $p$  and  $q$  together with the chord from  $p$  to  $q$  forms a closed space polygon  $\mathcal{V}'$ . The total curvature of this polygon is equal to  $t$  plus the turning angles at  $p$  and  $q$ . By Fenchel’s theorem [do Carmo 76], that total curvature is at least  $2\pi$ . So the angle at  $p$  and the angle at  $q$  must sum to more than  $\pi$ . Thus either the angle at  $p$  or the angle at  $q$  must exceed  $\pi/2$ . But in that case, we could reduce  $d(p, q)$  to first order by moving  $p$  or  $q$  along an edge from the arc that connects  $p$  and  $q$ , contradicting our assumption that  $(p, q) \in \text{dcsd}(\mathcal{V})$ .  $\square$

We are now ready to prove Theorem 2.6:

*Proof:* Suppose that  $\text{CThi}(\ell, \mathcal{V}) \geq 1$ . This implies that  $\min_i \text{MinRad}(v_i) \geq 1$  by the definition of  $\text{CThi}$ . Lemma 2.7 tells us that  $\text{dcsd}(\mathcal{V}) \subset \text{VB}(1, \ell)$ , so we know that

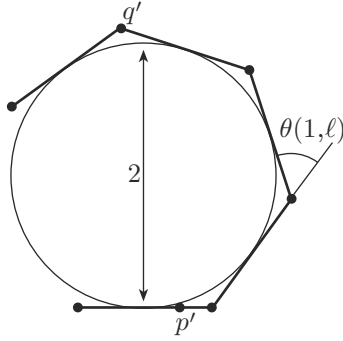
$$\min_{(p,q) \in \text{dcsd}(\mathcal{V})} d(p, q) \geq \min_{(p,q) \in \text{VB}(1, \ell)} d(p, q). \tag{2-3}$$

Together, these facts imply that  $\text{Thi}_p(\mathcal{V}) \geq 1$ , proving one direction of the theorem.

Suppose that  $\text{Thi}_p(\mathcal{V}) \geq 1$ . As above, this means that  $\min_i \text{MinRad}(v_i) \geq 1$ , so Lemma 2.7 applies and (2-3) holds. If the minimum on the right-hand side of (2-3) is achieved on the interior of  $\text{VB}(1, \ell)$ , then it is a local minimum of  $d(p, q)$  where  $p \neq q$  and so is in  $\text{dcsd}(\mathcal{V})$ . In this case, (2-3) is an equality and  $\text{CThi}(\ell, \mathcal{V}) \geq 1$ , completing the proof.

We are left with the case that the minimum of  $d(p, q)$  over  $\text{VB}(1, \ell)$  is realized by some  $(p, q)$  on the boundary of  $\text{VB}(1, \ell)$ . We claim that  $d(p, q)/2 \geq 1$ . This will complete the proof that  $\text{CThi}(\ell, \mathcal{V}) \geq 1$ .

By definition,  $(p, q)$  is on the boundary of  $\text{VB}(1, \ell)$  only if  $\text{vb}(p, q) = \lceil \pi/\theta(1, \ell) \rceil$ . And since  $\text{vb}(p, q)$  is constant on the interiors of edges, one of  $p$  and  $q$  (without loss



**FIGURE 4.** The key step in the proof of Theorem 2.6 is the proof that points  $p'$  and  $q'$  on an arc  $\mathcal{P}$  are at least distance 2 apart. This arc has equal edge lengths  $\ell$ , each turning angle equal to  $\theta(1, \ell) := 2 \arctan(\ell/2)$ , and  $n := \lceil \pi/\theta(1, \ell) \rceil$  edges. We see above that these conditions imply that  $\mathcal{P}$  has an inscribed circle of unit radius. Further, the marked point  $q'$  must have a larger  $y$ -coordinate than the top of the circle, providing the required lower bound on the distance from  $p'$  to  $q'$ .

of generality,  $q$ ) must be a vertex. Since each turning angle of the arc of  $\mathcal{V}$  between  $p$  and  $q$  is bounded by  $\theta(1, \ell)$ , Schur's theorem [Chern 67] implies that  $d(p, q)$  is bounded below by the distance between the endpoints of  $p', q'$  of a planar polygonal arc  $\mathcal{P}$  with the same edge lengths and each turning angle equal to  $\theta(1, \ell)$ . We depict the situation in Figure 4.

We know that  $\mathcal{P}$  has  $n = \text{vb}(p, q)$  edges and total curvature  $(n - 1)\theta(1, \ell)$ . Since  $n = \text{vb}(p, q) = \lceil \pi/\theta(1, \ell) \rceil$ , we have

$$n - 1 < \frac{\pi}{\theta(1, \ell)} \leq n,$$

and so

$$(n - 1)\theta(1, \ell) < \pi \leq n\theta(1, \ell).$$

Thus if we add an edge to  $\mathcal{P}$  at  $q'$  with turning angle  $\theta(1, \ell)$  to form an arc  $\mathcal{P}^+$ , the total curvature of  $\mathcal{P}$  is less than  $\pi$ , while the total curvature of  $\mathcal{P}^+$  is at least  $\pi$ . These facts imply that if the first edge of  $\mathcal{P}$  lies along the  $x$ -axis, the point  $q'$  has the largest  $y$ -coordinate on  $\mathcal{P}^+$ . But our turning-angle and edge-length conditions imply that  $\mathcal{P}^+$  has an inscribed circle of unit radius, so the  $y$ -coordinate of  $q'$  is at least two. This implies that  $d(p', q') \geq 2$ , completing the proof.  $\square$

These proofs imply an obvious corollary, which will be useful in practice:

**Corollary 2.8.** *If  $\text{dcsd}(\mathcal{V}) \subset \text{VB}(\tau, \ell)$  and the distance between any two vertices on the boundary of  $\text{VB}$  is strictly*

*greater than  $\text{Thi}_p(\mathcal{V})$ , then  $\text{CThi} = \text{Thi}_p$  for polygons in a neighborhood of  $\mathcal{V}$  (regardless of whether  $\mathcal{V}$  is equilateral with edge length  $\ell$ ).*

*Proof:* The argument is the same as that of Theorem 2.6, using the hypotheses instead of Lemma 2.7 and the argument about turning angles.  $\square$

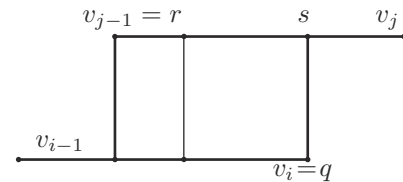
## 2.4. Struts and Kinks

In our definition of  $\text{Thi}_p$ , we saw that pairs of points in  $\text{dcsd}$  and vertices with minimum  $\text{MinRad}$  were in control of thickness. We now want to develop similar sets of ‘‘controlling’’ pairs of points and vertices for  $\text{CThi}$ . This will require a bit of care.

Given any two line segments  $e_1$  and  $e_2$  in space, a calculation reveals that the minimum distance between them is attained at a single point except in some special cases in which  $e_1$  and  $e_2$  are parallel. In that case, the minimum is attained at an interval of corresponding pairs (as in Figure 5). The endpoints of these intervals are self-distances measured from an endpoint of one segment to a point on the other. Following this line of argument we see that for any space polygon the local minima of the self-distance function  $d(p, q)$  are isolated unless there are pairs of parallel edges, in which case there may be families of local minima as above. Using these observations we make the following definition:

**Definition 2.9.** The *strut set*  $\text{Strut}(\mathcal{V})$  is the set of pairs  $(p, q)$  in  $\text{VB}(1, \ell)$  with  $d(p, q)/2 = 1$  and either

- $(p, q)$  is an isolated local minimum of  $d(p, q)$ , or
- $(p, q)$  is an *endpoint* of a family of local minima of  $d(p, q)$ .



**FIGURE 5.** When the edges  $e_i$  and  $e_j$  are parallel, many chords realize the minimum distance between the segments. In this case, we show that the minimum derivative of distance between any of these pairs occurs at one end or the other. We name the endpoints of this family of chords  $p$  and  $q$  on  $e_i$  and  $r$  and  $s$  on  $e_j$ . One of each of these pairs must be an endpoint—in this case it is  $q = v_i$  and  $r = v_{j-1}$  that are endpoints.



In the second case,  $(p, q)$  must be a vertex–edge pair joining two parallel edges of  $\mathcal{V}$ .

We note that  $\text{Strut}(\mathcal{V})$  is a finite subset of  $\text{dcsd}(\mathcal{V})$  ( $\text{dcsd}(\mathcal{V})$  may be infinite if two edges are parallel). It is much easier to define the *kink set*:

**Definition 2.10.** The *kink set*  $\text{Kink}(\mathcal{V})$  is the set of vertices  $v_i$  and signs  $\pm$  with  $\text{MinRad}^\pm v_i = 1$ .

The strut and kink sets are both empty if we have  $\text{CThi}(\ell, \mathcal{V}) > 1$ .

### 2.5. Polygon Space and Variations of CThi

We now want to describe the space of variations of a polygon that preserve or increase CThi to first order. Given a polygon  $\mathcal{V} \in \mathbb{R}^{3V}$  we can define a variation of  $\mathcal{V}$  by any  $W = (w_1, \dots, w_V) \in \mathbb{R}^{3V}$ . This variation generates a family of polygons

$$\mathcal{V}_t = \mathcal{V} + tW = (v_1 + tw_1, \dots, v_V + tw_V).$$

This specifies a variation of the *vertices* of the polygon, but we will actually need to extend this to a variation of the entire polygon. We do so by writing each point  $p$  on  $\mathcal{V}$  as a convex combination of adjacent vertices  $p = sv_i + (1 - s)v_{i+1}$  and defining

$$p_t = s(v_i + tw_i) + (1 - s)(v_{i+1} + tw_{i+1}). \tag{2-4}$$

We can now define the distance between  $p$  and  $q$  as a function of the vertex positions of  $\mathcal{V}$  by writing  $p = sv_i + (1 - s)v_{i+1}$  and  $q = s'v_j + (1 - s')v_{j+1}$ , where  $v_i, v_{i+1}$ , and  $v_j, v_{j+1}$  are the endpoints of the edges containing  $p$  and  $q$  and letting

$$d(p, q) = d(sv_i + (1 - s)v_{i+1}, s'v_j + (1 - s')v_{j+1})$$

be a function from  $\mathbb{R}^{3V}$  to  $\mathbb{R}$ . The gradient of this function with respect to the vertex positions (that is, holding  $s$  and  $s'$  constant), denoted by  $\nabla d(p, q)$ , is then a vector in  $\mathbb{R}^{3V}$ . For any vertex  $v_i \in \mathcal{V}$ , the functions  $\text{MinRad}^\pm v_i$  are also functions of the vertex positions, with corresponding gradient vectors  $\nabla \text{MinRad}^\pm v_i$ .

We now want to prove that  $\text{CThi}(\ell, \mathcal{V})$  has a one-sided derivative as we vary  $\mathcal{V}$  according to any variation  $W$  and to give a finite procedure for computing that variation. This will require some setup.

**Proposition 2.11.** *Suppose that  $\text{CThi}(\ell, \mathcal{V}) = 1$ . Then viewing every pair of points  $(p, q)$  on  $\mathcal{V}$  and every  $\text{MinRad}^\pm v_i$  as functions of  $t$ , the forward time deriva-*

*tive exists and satisfies*

$$\begin{aligned} D_W \text{CThi}(\ell, \mathcal{V}) & \tag{2-5} \\ &= \frac{d}{dt^+} \text{CThi}(\mathcal{V}_t) \Big|_{t=0} \\ &= \min \left\{ \min_{(v_i, \pm) \in \text{Kink}(\mathcal{V})} \frac{d}{dt^+} (\text{MinRad}^\pm v_i)(t) \Big|_{t=0}, \right. \\ & \quad \left. \min_{\text{Strut}(\mathcal{V})} \frac{d}{dt^+} \frac{d(p(t), q(t))}{2} \Big|_{t=0} \right\}. \end{aligned}$$

*Proof:* We begin by ignoring any  $\text{MinRad} v_i$  functions that are not defined (which happens when  $v_{i-1}, v_i$ , and  $v_{i+1}$  are collinear). Since  $\text{CThi}(\ell, \mathcal{V})$  is equal to 1, the  $\text{MinRad}$  of these vertices will not affect  $\text{CThi}(\mathcal{V} + tW)$  for small enough  $t$ . The function  $\text{CThi}$  is then the minimum of a set of differentiable functions  $\text{MinRad}^\pm v_i$  and  $d(p, q)/2$  indexed by the (compact) disjoint union of compact sets  $\{v_1, \pm\} \sqcup \dots \sqcup \{v_V, \pm\} \sqcup \text{VB}(1, \ell)$  (where we assume that any  $v_i$  with  $\text{MinRad} v_i$  undefined are missing). Clark’s theorem for min-functions [Clarke 75] tells us immediately that the derivative in (2-5) exists.

However, Clark’s theorem tells us that

$$\begin{aligned} D_W \text{CThi}(\ell, \mathcal{V}) & \\ &= \min \left\{ \min_{\substack{(v_i, \pm) \\ \text{MinRad}^\pm v_i = 1}} \frac{d}{dt^+} \Big|_{t=0} (\text{MinRad}^\pm v_i)(t), \right. \\ & \quad \left. \min_{\substack{(p, q) \in \text{VB}(1, \ell) \\ d(p, q)/2 = 1}} \frac{d}{dt^+} \Big|_{t=0} \frac{d(p(t), q(t))}{2} \right\}. \end{aligned}$$

The first set  $\{(i, \pm) \mid \text{MinRad}^\pm v_i = 1\}$  is the kink set, which matches (2-5). But if a pair of edges in  $\mathcal{V}$  are parallel and at distance 2 from one another, then  $\text{Strut}(\mathcal{V})$  is only a subset of  $\{(p, q) \in \text{VB}(1, \ell) \mid d(p, q)/2 = 1\}$ . We must prove that

$$\begin{aligned} \min_{\substack{(p, q) \in \text{VB}(1, \ell) \\ d(p, q)/2 = 1}} \frac{d}{dt^+} \frac{d(p(t), q(t))}{2} \Big|_{t=0} & \tag{2-6} \\ &= \min_{(p, q) \in \text{Strut}(\mathcal{V})} \frac{d}{dt^+} \frac{d(p(t), q(t))}{2} \Big|_{t=0}. \end{aligned}$$

For any pair of parallel edges with distance 2, we may assume that the situation is as in Figure 5.

We label points  $p, q, r$ , and  $s$  as in the figure, and parameterize the line segments between  $p$  and  $q$  and between  $r$  and  $s$  by  $\eta \in [0, 1]$ . The pairs with  $\eta = 0$  and  $\eta = 1$  are in the strut set of  $\mathcal{V}$ , but the pairs given by all other values of  $\eta$  are not. To prove (2-6) we must find

$$\min_{\eta \in [0, 1]} \frac{d}{dt^+} \|\eta p + (1 - \eta)q - \eta r - (1 - \eta)s\|,$$



and show that it is attained at  $\eta = 0$  or  $\eta = 1$ . If we view  $p, q, r$ , and  $s$  as functions of time, then for any given  $\eta$ , the time derivative of the corresponding length is given by

$$\frac{1}{2} \langle \eta p + (1 - \eta)q - \eta r - (1 - \eta)s, \eta p' + (1 - \eta)q' - \eta r' - (1 - \eta)s' \rangle,$$

where we have used the fact that  $d(e_i, e_j)/2 = 1$ . Re-grouping, we can rewrite this as

$$\frac{1}{2} \langle \eta(p - r) + (1 - \eta)(q - s), \eta(p - r)' + (1 - \eta)(q - s)' \rangle,$$

and using the fact that  $p - r = q - s$  at time 0, we can again rewrite this as

$$\eta \langle p - r, p' - r' \rangle + (1 - \eta) \langle q - s, q' - s' \rangle.$$

Now as  $\eta$  varies between 0 and 1, we note that the  $\eta$  derivative of the above quantity is

$$\langle p - r, p' - r' \rangle - \langle q - s, q' - s' \rangle.$$

In particular, this derivative is nonzero for all  $\eta \in [0, 1]$  unless  $\langle p - r, p' - r' \rangle = \langle q - s, q' - s' \rangle$ , in which case it vanishes identically. This means that the minimum value of this expression is always realized when  $\eta = 0$  or  $\eta = 1$ . This completes the proof.  $\square$

We can use Proposition 2.11 to define two sets of variations that will be of particular interest to us. The first set consists of variations that are tangent to the boundary or pointing into the interior of the set of polygons  $\text{CThi}(\ell, \mathcal{V}) \geq 1$ . We will allow our polygons to move in these directions.

**Definition 2.12.** Suppose we have a polygon  $\mathcal{V}$  and a variation  $W$  of  $\mathcal{V}$ . If  $\text{CThi}(\ell, \mathcal{V}) = 1$ , we say that  $W$  is an *infinitesimal motion* of  $\mathcal{V}$  if the forward directional derivative

$$D_W \text{CThi}(\ell, \mathcal{V})$$

is greater than or equal to zero. If  $\text{CThi}(\ell, \mathcal{V}) > 1$ , we call every variation  $W$  an infinitesimal motion. The set of all infinitesimal motions of  $\mathcal{V}$  is denoted by  $I(\mathcal{V})$ .

Given our definitions of  $\nabla d(p, q)$  and  $\nabla \text{MinRad}^\pm v_i$  above, the following corollary follows directly from Proposition 2.11.

**Corollary 2.13.** *The set  $I(\mathcal{V})$  is the dual cone of the set  $-\nabla d(p, q)/2$  for  $(p, q) \in \text{Strut}(\mathcal{V})$  and  $-\nabla \text{MinRad}^\pm v_i$  for  $(v_i, \pm) \in \text{Kink}(\mathcal{V})$ .*

*Proof:* We need only recall that the dual cone  $A^+$  to a set of vectors  $A$  is the set of vectors  $X$  for which  $\langle X, W \rangle \leq 0$  for all  $W \in A$ . Since the directional derivatives of  $d(p, q)/2$  and  $\text{MinRad}^\pm v_i$  in the direction  $X$  are the dot products of  $X$  with  $-\nabla d(p, q)/2$  and  $-\nabla \text{MinRad}^\pm v_i$ ,  $X$  is in the dual cone if and only if all these directional derivatives are nonnegative. But by the proposition, this implies that  $D_X \text{CThi}(\ell, \mathcal{V})$  is nonnegative as well.  $\square$

The second set of variations of interest will be the normal cone of the boundary of the set of polygons with  $\text{CThi}(\ell, \mathcal{V}) \geq 1$ . We will forbid our polygons from moving in these directions.

**Definition 2.14.** The convex cone of *resolvable motions*  $R(\mathcal{V})$  of  $\mathcal{V}$  is the cone generated by the set  $-\nabla d(p, q)/2$  for  $(p, q) \in \text{Strut}(\mathcal{V})$  and  $-\nabla \text{MinRad}^\pm v_i$  for  $(v_i, \pm) \in \text{Kink}(\mathcal{V})$ . Here  $R(\mathcal{V})$  is the set of vectors  $R \in \mathbb{R}^{3V}$  that can be expressed in the form

$$R = \sum_{(p,q) \in \text{Strut}(\mathcal{V})} -\lambda_i^2 \nabla \frac{d(p,q)}{2} + \sum_{v_j \in \text{Kink}(\mathcal{V})} -\lambda_j^2 \nabla \text{MinRad } v_j. \quad (2-7)$$

Here the indices  $i$  and  $j$  just number the elements of the strut and kink sets. The constants  $\lambda_i^2$  and  $\lambda_j^2$  are nonnegative numbers, as suggested by the notation.

It is a standard fact from optimization theory that  $R(\mathcal{V}) = I(\mathcal{V})^+$ , since for any set of vectors  $\{v\}$ , the double dual  $\{v\}^{++}$  is the cone generated by  $\{v\}$ .

## 2.6. Theory of Constrained Optimization

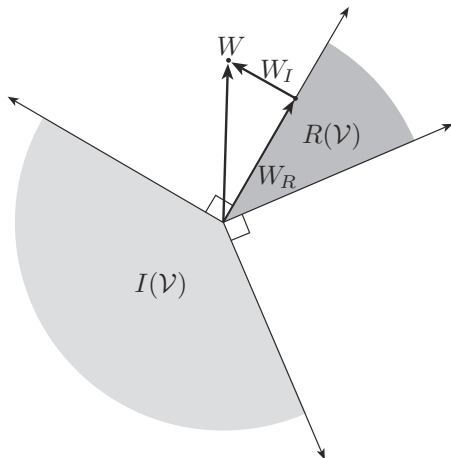
Given a function  $f(\mathcal{V})$  on the space of polygons  $\mathbb{R}^{3V}$ , we can compute the negative gradient  $-\nabla f$ , which is a variation vector in  $\mathbb{R}^{3V}$ . We are now interested in understanding how this gradient is modified by the constraint  $\text{CThi}(\ell, \mathcal{V}) \geq 1$ . This thickness constraint models the effect of an embedded tube around the polygon: it allows some motions of  $\mathcal{V}$  and blocks others.

**Definition 2.15.** The *constrained gradient*  $(-\nabla f)_I$  of  $-f$  is the closest vector in  $I(\mathcal{V})$  to  $-\nabla f(\mathcal{V})$ .

We now recall that any convex cone and its dual cone provide a kind of orthogonal decomposition of their ambient vector space, as shown in Figure 6.

**Proposition 2.16.** [Stoer and Witzgall 70, Theorem 2.8.7] *Any vector  $W \in \mathbb{R}^{3V}$  may be uniquely written*

$$W = W_R + W_I,$$



**FIGURE 6.** The infinitesimal motions  $I(\mathcal{V})$  and the resolvable motions  $R(\mathcal{V})$  of  $\mathcal{V}$  form dual convex cones. Hence, although these are not orthogonal subspaces of  $\mathbb{R}^{3V}$ , a similar decomposition property holds: any vector  $W$  may be written uniquely as a sum of a vector  $W_I \in I(\mathcal{V})$  and a vector  $W_R \in R(\mathcal{V})$ .

where  $\langle W_R, W_I, \rangle = 0$ ,  $W_R \in R(\mathcal{V})$  is the closest resolvable motion to  $W$ , and  $W_I \in I(\mathcal{V})$  is the closest infinitesimal motion to  $W$ .

We note that this proposition shows that the constrained gradient of  $-f$  is well defined. Further, it is easy to show that the constrained gradient is the direction of steepest descent for  $f$  within  $I(\mathcal{V})$ . This makes us guess that the constrained gradient should vanish at a critical point for minimizing  $f$ . To prove it, we define critical points more carefully:

**Definition 2.17.** We say that  $\mathcal{V}$  is *thickness-critical* for minimizing  $f$  if either

- $D_W f = 0$ , or
- $C\text{Thi}(\ell, \mathcal{V}) = 1$  and for any  $W$  with  $D_W f(\mathcal{V}) < 0$ , we have  $D_W C\text{Thi}(\ell, \mathcal{V}) < 0$ .

In the first case, we are at an unconstrained critical point of the objective function  $f$ . In the second, we are at a constrained critical point where motion in the direction of the negative gradient of  $f$  is blocked by active constraints. We then have a version of the Kuhn–Tucker Theorem (restated in our language from the original form in [Cantarella et al. 06]), which gives a verifiable condition for thickness-criticality.

**Theorem 2.18.** *The polygon  $\mathcal{V}$  is thickness-critical for minimizing  $f$  if and only if  $-\nabla f$  is in  $R(\mathcal{V})$  if and only if the constrained gradient  $(-\nabla f)_I$  vanishes.*

*Proof:* It suffices to show that the first two statements are equivalent, since the second and third are clearly equivalent by Proposition 2.16.

If  $-\nabla f$  is not in  $R(\mathcal{V})$ , then Farkas’s theorem implies that there exists some  $W$  with  $\langle W, \nabla f \rangle = D_W f < 0$  and  $\langle W, R \rangle \leq 0$  for all  $R \in R(\mathcal{V})$  [Panik 93, p. 118]. Using the definition of  $R(\mathcal{V})$  and Proposition 2.11, this implies  $D_W C\text{Thi}(\ell, \mathcal{V}) \geq 0$ . Thus  $\mathcal{V}$  is not thickness-critical for minimizing  $f$ .

If  $-\nabla f$  is in  $R(\mathcal{V})$ , we will prove that  $\mathcal{V}$  is thickness-critical for minimizing  $f$ . We first observe that the dual cone of  $-\nabla f$  contains the dual cone  $R^+(\mathcal{V})$ . Now suppose we have some  $W$  with  $D_W f < 0$ . Then  $\langle W, -\nabla f \rangle > 0$ , so  $W \notin (-\nabla f)^+$ , and in particular,  $W \notin R^+(\mathcal{V})$ . But this means that  $\langle W, R \rangle > 0$  for some  $R \in R(\mathcal{V})$ , so  $D_W C\text{Thi}(\ell, \mathcal{V}) < 0$ . Hence  $\mathcal{V}$  is thickness-critical for minimizing  $f$ .  $\square$

We can give a natural interpretation of this theorem in mathematical and physical terms by considering the condition  $-\nabla f \in R(\mathcal{V})$ . By definition, this means that

$$-\nabla f + \sum_{(p,q) \in \text{Strut}(\mathcal{V})} \lambda_i^2 \nabla \frac{d(p,q)}{2} + \sum_{v_j \in \text{Kink}(\mathcal{V})} \lambda_j^2 \nabla \text{MinRad } v_j = 0. \tag{2-8}$$

Mathematically, the  $\lambda_i^2$  and  $\lambda_j^2$  are Lagrange multipliers. If we think of the thickness constraint as an embedded tube around  $\mathcal{V}$ , we can interpret these scalars as magnitudes of compression forces transmitted by tube contacts (for struts) and angles where the polygon resists further bending (for kinks).

In general, we cannot expect every local minimum of a constrained function to be a constrained critical point in the sense of Definition 2.17. If the set of polygons defined by  $C\text{Thi}(\ell, \mathcal{V})$  had an outward-pointing cusp, we might reach a point where some  $W$  with  $D_W f < 0$  had  $D_W C\text{Thi} = 0$ . For example, the constrained system

$$\begin{aligned} &\text{minimize } f(x, y) = -x, \\ &\text{subject to } g(x, y) = \min\{x^3 - y, y\} \geq 0, \end{aligned}$$

has this property at the local minimum  $(0, 0)$  for  $W = (1, 0)$ . The problem here is simply that  $D_W g \leq 0$  for all  $W$ . This does not happen for thickness-constrained polygons, but we will need another idea to prove it:

**Definition 2.19.** We say that  $\mathcal{V}$  is *constraint-qualified* (in the sense of [Mangasarian and Fromovitz 67]) if there exists some  $W$  such that  $D_W \text{CThi} > 0$ .

It is then standard to show the following:

**Proposition 2.20.** [Cantarella et al. 06] *Any constraint-qualified local minimum of  $f$  is a thickness-critical point for minimizing  $f$ .*

In our case, scaling  $\mathcal{V}$  provides the desired motion, so we have the following corollary.

**Corollary 2.21.** *If the polygon  $\mathcal{V}$  is a local minimum for  $f$ , then it is a thickness-critical point for minimizing  $f$ .*

We make a final note that in general, our criticality theory works equally well for  $\text{CThi}$  and  $\text{Thi}_p$  (even for polygons  $\mathcal{V}$  that are not equilateral), as long as they obey the hypotheses of Corollary 2.8. This is true in practice in all of our numerically computed configurations.

### 3. BRIDGING THEORY AND COMPUTATION

#### 3.1. Overview of the Algorithm

We have now derived enough theory to describe our algorithm in general terms. We wish to minimize the function  $\text{Len}(\mathcal{V})$  subject to the constraint  $\text{CThi}(\ell, \mathcal{V}) \geq 1$ . We will do so by computing the constrained gradient  $(-\text{Len } \mathcal{V})_I$  and stepping in this direction. These steps will reduce  $\text{Len}(\mathcal{V})$  while keeping  $\mathcal{V}$  close to the set  $\text{CThi}(\ell, \mathcal{V}) \geq 1$  (since the constraints are nonconvex, we cannot stay entirely inside this set). When  $(-\text{Len } \mathcal{V})_I$  vanishes, the algorithm will terminate. By Theorem 2.18, if the constrained gradient were exactly zero, the resulting configuration would be a thickness-critical point for minimizing length. We note that our algorithm will attempt to maintain an approximately equilateral polygon  $\mathcal{V}$ , but it is not required to: constant edge length  $\ell$  is not a hypothesis of Theorem 2.18. Our only caveat is that we must remember that  $\text{CThi}(\mathcal{V})$  may not be equal to  $\text{Thi}_p(\mathcal{V})$  if the final configuration fails to obey the hypotheses of Corollary 2.8. We also note that there is nothing special about choosing  $\text{Len}(\mathcal{V})$  as the function to minimize—both our theory and our code would work just as well for any other function.

#### 3.2. Computing the Constrained Gradient

To implement this algorithm, we must be able to compute the constrained gradient  $(-\nabla f)_I$ . This is a standard

problem in linear algebra. By definition, if  $-\nabla f$  is written as  $(-\nabla f)_R + (-\nabla f)_I$  using Proposition 2.16, the constrained gradient is equal to  $(-\nabla f)_I$ . We can compute this by computing  $(-\nabla f)_R$ , which is easy to do, since we know the generators of the cone  $R(\mathcal{V})$ .

**Definition 3.1.** If  $\text{CThi}(\ell, \mathcal{V}) = 1$ , the *rigidity matrix*  $A$  of  $\mathcal{V}$  is the matrix whose columns are the gradients  $-\nabla d(p, q)/2$  for  $(p, q) \in \text{Strut}(\mathcal{V})$  and  $-\nabla \text{MinRad}^\pm v_i$  for  $(v_i, \pm) \in \text{Kink}(\mathcal{V})$ .

We can construct the rigidity matrix by finding the members of  $\text{Strut}(\mathcal{V})$  and  $\text{Kink}(\mathcal{V})$ . It follows from the definition that  $R(\mathcal{V})$  is the image of the positive orthant under the matrix  $A$ . By Proposition 2.16,  $(-\nabla f)_R$  is the closest vector in that image to  $-\nabla f$ . So if we solve the nonnegative least-squares (NNLS) problem

$$\min_{\Lambda \geq 0} \|\Lambda A - (-\nabla f)\|, \quad (3-1)$$

then  $(-\nabla f)_R = \Lambda A$  and  $(-\nabla f)_I = -\nabla f - \Lambda A$ . This least-squares problem is a special kind of quadratic programming problem that has been well studied in numerical linear algebra (see [Björck 96]). In our case, the problem is much easier because  $A$  is extremely sparse—the gradients of the  $d(p, q)/2$  involve no more than four vertices (and so 12 variables), while the gradients of the  $\text{MinRad}^\pm$  involve only three vertices (and nine variables). So each column of  $A$ , which is typically 1000 or more entries long, contains at most 12 nonzero entries.

#### 3.3. The Gradient of Length

We can now compute  $(-\nabla \text{Len})_I$  if we can compute  $-\nabla \text{Len}$ , build the rigidity matrix  $A$  from the strut and kink sets, and solve the NNLS problem in (3-1). We will take these problems in order.

Length is a differentiable function of polygons  $\mathcal{V} \in \mathbb{R}^{3V}$ , whose gradient is given by a straightforward calculation:

**Proposition 3.2.** *The gradient of length of a polygon  $\mathcal{V}_n$  is given by the collection of  $n$  vectors*

$$\nabla \text{Len}(\mathcal{V})_k = \frac{v_{k-1} - v_k}{\|v_{k-1} - v_k\|} + \frac{v_{k+1} - v_k}{\|v_{k+1} - v_k\|}.$$

#### 3.4. The Gradient of $d(p, q)/2$

Given a pair of points  $(p, q)$  on  $\mathcal{V}$ , the gradient of the distance between them is a set of four vectors located at the endpoints of the edges on which  $p$  and  $q$  lie. These vectors are given by a calculation:

**Proposition 3.3.** *Suppose that  $(p, q) \in \text{Strut}(\mathcal{V})$ . If  $p = \alpha v_i + (1 - \alpha)v_{i+1}$  and  $q = \beta v_j + (1 - \beta)v_{j+1}$ , then*

$$\nabla \frac{d(p, q)}{2} = \frac{1}{2d(p, q)} \left\{ \alpha(p - q), (1 - \alpha)(p - q), \beta(q - p), (1 - \beta)(q - p) \right\},$$

where these three vectors are applied to  $v_i, v_{i+1}, v_j$ , and  $v_{j+1}$  in order.

### 3.5. The Gradient of $\text{MinRad}^\pm$

As we noted above, the  $\text{MinRad}^\pm$  are differentiable where they are defined. We now compute the gradient on  $\text{MinRad}^+$ , noting that the gradient of  $\text{MinRad}^-$  is similar.

**Proposition 3.4.** *Given a vertex  $i$  on  $\mathcal{V}_n$  with finite  $\text{MinRad}^\pm(v_i)$ , we let  $n$  denote the oriented normal vector to the plane defined by  $v_{i-1}, v_i, v_{i+1}$  and define the scalar constant*

$$K = \frac{\|v_{i+1} - v_i\|}{2 \cos \theta - 2}$$

and the vector constants

$$\begin{aligned} V &= \frac{v_{i+1} - v_i}{2 \tan(\theta/2) \|v_{i+1} - v_i\|}, \\ W &= K \frac{(v_{i-1} - v_i) \times n}{\|v_{i-1} - v_i\|^2}, \\ X &= K \frac{n \times (v_{i+1} - v_i)}{\|v_{i+1} - v_i\|^2}. \end{aligned}$$

Then if we write the gradient of  $\text{MinRad}^+$  as a triple of vectors located at  $v_{i-1}, v_i$ , and  $v_{i+1}$ , we have

$$\nabla \text{MinRad}^+(v_i) = \{W, -W - X - V, X + V\}.$$

*Proof:* The proof is a lengthy calculation. We want to compute the gradient of

$$\text{MinRad}^+(v_i) = \frac{\|v_{i+1} - v_i\|}{2 \tan(\theta/2)},$$

where  $\theta$  is the turning angle at vertex  $v_i$ . We start with a change of variables. Let  $A = v_{i-1} - v_i$  and  $B = v_{i+1} - v_i$ . We can rewrite  $\text{MinRad}^+$  in terms of these variables and compute its gradient as follows:

$$\begin{aligned} \nabla \frac{\|B\|}{2 \tan(\theta/2)} &= \frac{1}{2 \tan(\theta/2)} \left( 0, \frac{B}{\|B\|} \right) \\ &\quad - \frac{1}{2} \left[ \frac{\|B\|}{\tan^2(\theta/2)} \cdot \frac{d}{d\theta} \tan(\theta/2) \right] \nabla \theta. \end{aligned} \tag{3-2}$$

Now

$$\frac{d}{d\theta} \tan(\theta/2) = \frac{1}{2 \cos^2(\theta/2)} = \frac{1}{2 \frac{1 + \cos \theta}{2}} = \frac{1}{1 + \cos \theta}, \tag{3-3}$$

$$\tan^2(\theta/2) = \frac{1 - \cos \theta}{1 + \cos \theta}.$$

So we can rewrite (3-2) as

$$\begin{aligned} \nabla \frac{\|B\|}{2 \tan(\theta/2)} &= \frac{1}{2 \tan(\theta/2)} \left( 0, \frac{B}{\|B\|} \right) - \frac{\|B\|}{2 - 2 \cos \theta} \nabla \theta \\ &= (0, V) + K \nabla \theta. \end{aligned}$$

Keeping track of the sign of the exterior angle, we see that if  $n$  is the oriented unit normal to the plane containing  $A$  and  $B$ , we have

$$\nabla \theta = \left( \frac{A \times n}{\|A\|^2}, \frac{n \times B}{\|B\|^2} \right),$$

and so

$$\nabla \frac{\|B\|}{2 \tan(\theta/2)} = (W, X + V).$$

Using the definition of  $A$  and  $B$  to change back to the original variables completes the proof.  $\square$

The function  $\text{MinRad}(v_i)$  provides a discrete analogue to the radius of curvature for the polygonal curve  $\mathcal{V}$  at  $v_i$ . Since this is a numerical computation of a second derivative, we expect the function to be quite sensitive to small changes in the positions of the vertices of  $\mathcal{V}$ . This sensitivity will limit the accuracy of our computations, so we record an estimate of the norm of the gradient of  $\text{MinRad}^+(v_i)$ .

**Corollary 3.5.** *If  $\mathcal{V}$  is an equilateral polygon with edge length  $\ell$  and  $\text{MinRad} v_i = 1$ , then*

$$\|\nabla \text{MinRad}^\pm v_i\| \geq \frac{2}{\ell^2}.$$

*Proof:* Consider

$$\|W\| = \frac{\|v_{i+1} - v_i\| \|(v_{i-1} - v_i) \times n\|}{|2 \cos \theta - 2| \|v_{i-1} - v_i\|^2}.$$

Since the polygon is equilateral and  $n$  is a unit vector normal to  $v_{i-1} - v_i$ , this is just  $\|W\| = 1/|2 \cos \theta - 2|$ . If  $\text{MinRad} = 1$ , then (squaring  $\text{MinRad}$  and using both half-angle formulas for the tangent), we see that  $\|W\| = |2 + 2 \cos \theta|/\ell^2$ . Since  $W$  appears alone in the formula for  $\nabla \text{MinRad}^+$ , this is a lower bound for the norm of the entire gradient.  $\square$

## 4. PROGRAM DESIGN

### 4.1. Issues of Scale

The design and implementation of our algorithm `ridgerunner` were shaped by the scale of the knot-minimizing problems we intended to solve and the amount of computer power we had on hand to solve them. To inform the discussion that follows, we will now take a moment to consider the dimensions of our problems. In a typical run, we started by minimizing the length of a low-resolution version of our knot or link with two vertices per unit of ropelength (80 to 150 vertices).

Once that configuration was minimized, a medium-resolution run at four vertices per unit of ropelength was performed. A final run followed at eight vertices per unit of ropelength. Most of the runtime was spent during the final run, which took 20–40 CPU hours on a desktop computer. During the final run, the average edge length  $\ell$  for our curves was approximately 0.061, which meant that there were 658 edges. The average size of the strut set was 892 pairs of points, while the average size of the kink set was 19 vertices. The rigidity matrix was then on average a  $911 \times 1974$  matrix that was 99.4% sparse (no more than 10875 of its 1798314 entries were nonzero). A typical run contained several hundred thousand steps.

### 4.2. The Algorithm

Our method is based loosely on the method of constrained gradient descent. The basic idea is to generate a series of polygons  $\mathcal{V}_i$  that converge to a limit polygon that is thickness-critical for minimizing a function  $f(\mathcal{V})$  by taking a series of steps in the form

$$\mathcal{V}_{k+1} = \mathcal{V}_k + \alpha(-\nabla f)_I,$$

where  $\alpha$  is chosen by a search algorithm. When  $\text{CThi}(\ell, \mathcal{V}) > 1$ , this is just the method of steepest descent, since  $(-\nabla f)_I = -\nabla f$ . When  $\text{CThi}(\ell, \mathcal{V}) = 1$ , these steps are tangent to the boundary of  $\text{CThi}(\ell, \mathcal{V}) \geq 1$  and in principle decrease  $\text{CThi}$  by no more than  $O(\alpha^2)$ .

In some circumstances, such as when two sections of tube touch for the first time, we can decrease  $\text{CThi}$  by  $O(\alpha)$  (which is much larger, since  $\alpha \ll 1$ ). We control this error by searching for an  $\alpha$  that keeps  $\text{CThi}(\ell, \mathcal{V}_k + \alpha(-\nabla f)_I)$  within acceptable bounds. When  $\text{CThi}(\ell, \mathcal{V}_k)$  becomes too small, we correct the accumulated error using a Newton’s-method-type solver. The code terminates when the constrained gradient is small enough to convince us that we are near a point that is thickness-critical for minimizing  $f$ . This procedure is summarized in Algorithm 1.

---

**Algorithm 1:** The outline of the `ridgerunner` algorithm.

---

```

input : A polygon  $\mathcal{V}_0$  and an error bound  $\text{MaxErr}$ .
output: A sequence of positions  $\mathcal{V}_k$  with
          $\text{CThi}(\ell, \mathcal{V}_k) \geq 1 - \text{MaxErr}$ .

1  repeat
2      Compute  $-\nabla f = -\nabla \text{Len}(\mathcal{V}_k) + -\nabla \text{Eq}(\mathcal{V}_k)$ ;
3      Find  $\text{Strut}(\mathcal{V})$  and  $\text{Kink}(\mathcal{V})$  and construct the
         rigidity matrix  $A$ ;
4      Compute constrained gradient  $(-\nabla f)_I$ ;
5      Search for  $\alpha$  such that  $\mathcal{V}_k + \alpha(-\nabla f)_I$ 
         minimizes ropelength and is computationally
         acceptable and set  $\mathcal{V}_{k+1} = \mathcal{V}_k + \alpha(-\nabla f)_I$ ;
6      if  $\text{CThi}(\ell, \mathcal{V}_{k+1}) < 1 - \text{MaxErr}$  then
7          Correct  $\text{CThi}(\ell, \mathcal{V}_{k+1})$  by Newton’s
             method;
8      end
9  until  $\|(-\nabla f)_I\| / \|\nabla f\|$  is sufficiently small;
```

---

In the rest of this section, we will comment on each of these steps in turn.

### 4.3. Line 2. Equilateral Polygons, $\text{CThi}$ and $\text{Thi}_p$

We have proved that  $\text{CThi} \geq 1 \iff \text{Thi}_p \geq 1$  only for equilateral polygons. It is therefore important that our  $\mathcal{V}_k$  remain at least approximately equilateral during a run. We enforce this constraint by defining a penalty function  $\text{Eq}(\mathcal{V})$  that is minimized when  $\mathcal{V}_k$  is equilateral and minimizing the sum  $\text{Len}(\mathcal{V}) + \text{Eq}(\mathcal{V})$ . This is quite effective (a typical run recorded an average error in edge length of about 0.385%) in practice. We note that while  $\text{CThi}$  and  $\text{Thi}_p$  might not be equal for nonequilateral polygons, we avoid any problems that might result by performing all of our final ropelength calculations with respect to the original  $\text{Thi}_p$  thickness.

### 4.4. Line 3. Finding $\text{Strut}(\mathcal{V})$ and $\text{Kink}(\mathcal{V})$

In principle, the strut and kink sets could be found by direct inspection of all pairs of edges and all vertices of  $\mathcal{V}$ . But since there are usually  $10^6$  such pairs, this naive method is too slow. So to find the strut and kink sets, we used the clustering code `octrope` described in [Ashton and Cantarella 05].

### 4.5. Line 4. Finding the Constrained Gradient

Once we have  $\text{Strut}(\mathcal{V})$  and  $\text{Kink}(\mathcal{V})$ , we can use the gradient formulas given in Propositions 3.3 and 3.4 to construct the rigidity matrix  $A$ . We must then solve the sparse nonnegative least-squares (SNNLS) problem  $\min_{\Lambda \geq 0} \|A\Lambda - (-\nabla f)\|$ , which we recall as equation (3–1).

We use the freely available `tsnnls` library [Cantarella et al. 08], which is an implementation of the block-pivoting algorithm of [Portugal et al. 94]. The PJV algorithm solves a sequence of unconstrained least-squares problems to find a partition of the variables of  $\Lambda$  into complementary sets  $F$  and  $G$  representing variables that will be nonzero and zero in the solution to (3–1). It is very important to take advantage of the sparsity of  $A$  in order to solve these (rather large) problems in an acceptable amount of time, since this step makes the dominant contribution to our overall runtime in most cases. To this end, `tsnnls` solves the least-squares problem  $Ax = b$  by solving the “normal equations”  $A^T Ax = A^T b$ . Since  $A^T A$  is symmetric, we can solve this system using a Cholesky factorization. This is done very quickly using the multifrontal supernodal sparse Cholesky code `TAUCS` of [Toledo et al. 03].

We have sacrificed some accuracy in favor of speed, since the condition number of  $A^T A$  is the square of the condition number of  $A$ . A standard “rule of thumb” in such situations is that the error in the solution is on the order of machine epsilon ( $10^{-16}$ ) multiplied by the condition number. To verify that this was small in practice, we used the `rcond` function in `LAPACK` to estimate the condition number of the rigidity matrices of all of our final configurations. The average condition number was on the order of  $10^4$ , with none being worse than  $8 \times 10^5$ . Thus we expect to have an average error on the order of  $10^{-8}$  and a worst-case error of  $10^{-6}$  in our final computations of the constrained gradient.

It is also worth noting that the `TAUCS` code will fail if the rigidity matrix is singular, which will occur when there is more than one way to balance the gradient force. This is expected for very complicated knots, but seems to be rare among knots in our data set. A more advanced version of `tsnnls` would calculate a minimum-norm solution to the least-squares problem in this case.

#### 4.6. Line 5. Choosing a Step Size

When  $C\text{Thi}(\mathcal{V}) > 1$ , our code sets a small maximum step size of  $10^{-2}$  and proceeds by Euler integration.<sup>4</sup> Once  $C\text{Thi}(\mathcal{V}) = 1$ , thickness typically decreases by a small amount at each step. We choose  $\alpha$  by a line search algorithm, finding the minimum ropelength of configura-

tions in the given direction using Brent’s method with a relatively low precision.

However, we do not always accept the ropelength-minimizing  $\alpha$ . Instead, we apply a collection of ad hoc conditions, which we describe as  $\alpha$  being “computationally acceptable.” These include an upper bound on the step size of  $10^{-2}$ , a lower bound of  $10^{-6}$ , and the requirement that the linear algebra solver of Step 4 be able to compute a new direction  $-\nabla f_I$  at the new location. These are motivated by several practical considerations. If the step size is permitted to be too large, loose configurations will often form large kinked regions before the tube contacts itself. Kinks reduce step sizes by orders of magnitude. In practice, this means that such a run takes an unacceptably long time to converge. If the step size is permitted to be too small, the solver can stall just before discovering a new self-contact. In these cases it has proved better to take the risk of a slight increase in ropelength in order to improve the strut set.

Finally, even when the step size is less than  $10^{-2}$ , if an arc of the knot suddenly contacts another arc, introducing too many new struts into the rigidity matrix, the matrix can become numerically singular, defeating the `tsnnls` solver of Step 4. Thus, we must look ahead and make sure that the next position will be acceptable to `tsnnls` before locking in a step size.

#### 4.7. Line 7. Error Correction

When the error bound  $\text{MaxErr} = 10^{-4}$  is reached, we use Newton’s method to return  $\mathcal{V}_k$  to a configuration with larger thickness. For any given variation  $W$  of  $\mathcal{V}$  we can estimate the change in the  $d(p, q)/2$  for  $(p, q) \in \text{Strut}(\mathcal{V})$  and in  $\text{MinRad}^\pm v_i$  for  $(v_i, \pm) \in \text{Kink}(\mathcal{V})$  by  $A^T W$ , where  $A$  is the rigidity matrix we have already computed.

We use this observation in a straightforward way. We construct a vector  $C$  of desired corrections that is equal to  $(1 - \text{MaxErr}/2) - d(p, q)/2$  for  $(p, q) \in \text{Strut}(\mathcal{V})$  and  $(1 - \text{MaxErr}/2) - \text{MinRad}^\pm v_i$  for  $(v_i, \pm) \in \text{Kink}(\mathcal{V})$ . Having done so, we find a minimum-norm solution to  $A^T W = C$ . We then step according to  $W$ , using a search algorithm to decide the step size, rebuild the rigidity matrix in case we have changed the strut or kink set in the correction step, and iterate.

We note that we do not attempt to correct all of the error in  $C\text{Thi}(\mathcal{V})$  during this procedure. If we did so, we would risk losing struts and kinks when we rebuild the rigidity matrix. In that case, the next Newton step, ignoring those pairs or vertices, might rediscover them as struts and kinks. In principle, this cycling behavior could

<sup>4</sup>We could improve the accuracy and speed of this portion of the computation by using a smarter ODE solving method. But these steps have no linear algebra involved, so they are already orders of magnitude faster than those to come. In practice, this portion of the run consumes less than one percent of the total runtime.

delay or prevent convergence of the Newton procedure, as noted in [Fletcher 01]. Our method does not eliminate this possibility entirely (in the current version of the code, we have observed occasional failures of the Newton solver), but in practice, the Newton solver almost always converges in only a few iterations.

The main problem with the Newton solver is that it is slow for large problems. The matrix  $A^T$  is mapping from a high-dimensional space of variations to a relatively low-dimensional space of struts and kinks, so it has a large kernel. Hence the matrix  $AA^T$  is not positive definite, and so we cannot solve  $A^TW = C$  using the method of normal equations and the fast Cholesky decomposition of TAUCS. Instead, we must use the older `lsqr` code of [Paige and Saunders 82] to find a minimum-norm solution to the problem. This can be as much as a hundred times slower than a regular step.

We always have the option of sidestepping Newton correction by simply scaling the knot (as in Pierański’s SONO algorithm). This preserves ropelength but destroys the strut set completely, requiring us to rebuild the strut set during subsequent steps. Our experience has been that this can improve performance during the middle stages of a run, when a fairly large number of struts and kinks have formed but the knot is still far from tight, but it is better to use Newton correction in the final stages of a run when one is trying to adjust a converged strut set to improve the final results.

At the moment, the speed of `lsqr` controls the overall performance of our code. We hope to find an improved error-correction procedure in future versions of the software.

#### 4.8. Modified Versions of the Algorithm

We have also modified our algorithm to handle some special cases, such as open curves with fixed endpoints or endpoints constrained to lie in planes. In these cases, the gradients of the endpoint constraints are added to the rigidity matrix and the gradient of length is resolved against them in Step 4. In addition, a specialized error-correction algorithm enforces the constraints after each step to prevent numerical error from causing the endpoints to drift away from their positions over time. The general Newton’s method algorithm for error-correction is also modified in these cases to take endpoint constraints into account.

In addition, we have found that curves whose final tight positions have long segments with no struts or kinks as well as tightly curved regions with many struts and

kinks often take a very large number of steps to tighten completely. Sections of the curve with no struts or kinks simply minimize length with no constraints and must therefore end up as straight lines. But as they approach this position, the gradient of length approaches zero, while regions where the gradient of length is balanced by struts and kinks have comparatively large length gradients. Since the step size is controlled by the tightly curved regions, it may take a very long time for the strut- and kink-free regions to finish straightening. We have had some success in these cases with a modified version of our algorithm that detects sections of curve with no struts or kinks and scales up the length gradient on those portions of the curve alone.

## 5. RESULTS OF COMPUTATIONS

We now present the main results of our computations. To summarize, we have significantly extended the range and quality of existing computations of tight knots and links. The new data support some interesting conjectures about the geometric structure of these configurations.

### 5.1. Validation of `ridgerunner` Computations

To verify that the system works, we checked the results of `ridgerunner` against some theoretical results. The results of the comparison appear in Table 1. As we can see from the table, the relative error in these ropelength computations is as small as 0.0017%.

The paper [Cantarella et al. 06] also gives an explicit strut set for the Borromean rings. To compare the numerically computed strut set to the theoretical one, we plot them together in Figure 7. The figure shows that the numerically computed strut set is quite close to the actual one. Figure 8 shows a similar comparison between theoretical results and a `ridgerunner` computation for the strut set of the “simple clasp” formed by two strands looped over one another. The theoretical results in [Cantarella et al. 06] for this clasp assume that the curvature of the clasp is not bounded, so we compare with the results of a run of our software that did not enforce curvature constraints.

### 5.2. Computing Polygonal-Ropelength Minimizers for Many Knots and Links

We minimized polygonal ropelength for all prime knots of ten and fewer crossings and all prime links of nine and fewer crossings (a total of 379 knot and link types) at resolutions of at least eight vertices per unit of





Link Name	Clasp	Hopf Link ( $2_1^2$ )	$2_1^2 \# 2_1^2$	Borromean Rings ( $6_2^3$ )
Vertices	332	216	384	930
Rop <sub>p</sub> bound	4.2841	25.1406	41.7131	58.0192
Rop bound	4.2837	25.1334	41.7086588	58.0070
Smooth length	4.2629	$8\pi$	$12\pi + 4$	58.0060
	[Cantarella et al. 06]	[Cantarella et al. 02]	[Cantarella et al. 02]	[Cantarella et al. 06]
Relative error	0.4%	0.02%	0.02%	0.0017%

**TABLE 1.** Numerical results from `ridgerunner` compared to the minimum ropelength values from [Cantarella et al. 02] and [Cantarella et al. 06]. The relative errors in the computations are quite small.

ropelength (several hundred vertices in total). For a few knots and links of special interest, we computed high-resolution runs with 16, 32, or 74 vertices per unit ropelength. The largest runs in our data set contain about 2400 vertices.

The computations were performed on clusters at the University of St. Thomas, the University of Georgia, and the ACCRE cluster at Vanderbilt University. We began our computations with an initial low-resolution (200 vertices or fewer) polygon, which we ran until the residual ( $\|(-\nabla f)_I\|/\|-\nabla f\|$ ) was sufficiently low. We then increased resolution by a minrad-preserving version of spline interpolation and minimized again from the resulting new starting configurations.

Our initial goal was a residual less than 0.01, which we achieved for 375 of the 379 knots and links in our data set. We were able to reach a residual of 0.001 for 286 of the knots and links in our data set, proving that our knots are close to being critical for the  $C\text{Thi}$  thickness. While our knots are not quite equilateral, they all satisfy the hypotheses of Corollary 2.8 and are hence also close to critical for the original  $\text{Thi}_p$  thickness. Because of this corollary, we know that both thicknesses are equal for our configurations, so we have computed and reported the  $\text{Thi}_p$  thickness and ropelength below.

We started each knot from at least five initial configurations, including the configurations from Knot-

Plot<sup>5</sup> (similar to the configurations in Rolfsen's table), the TOROS simulated annealer [Rawdon 03], Gilbert's minimized configurations from the online *Knot Atlas* [Gilbert 11], hand-drawn configurations from Kawauchi's *A Survey of Knot Theory* [Kawauchi 96], and positions generated from KnotPlot's `diagram` command. The results shown describe the lowest ropelength we achieved from any of these starting configurations.

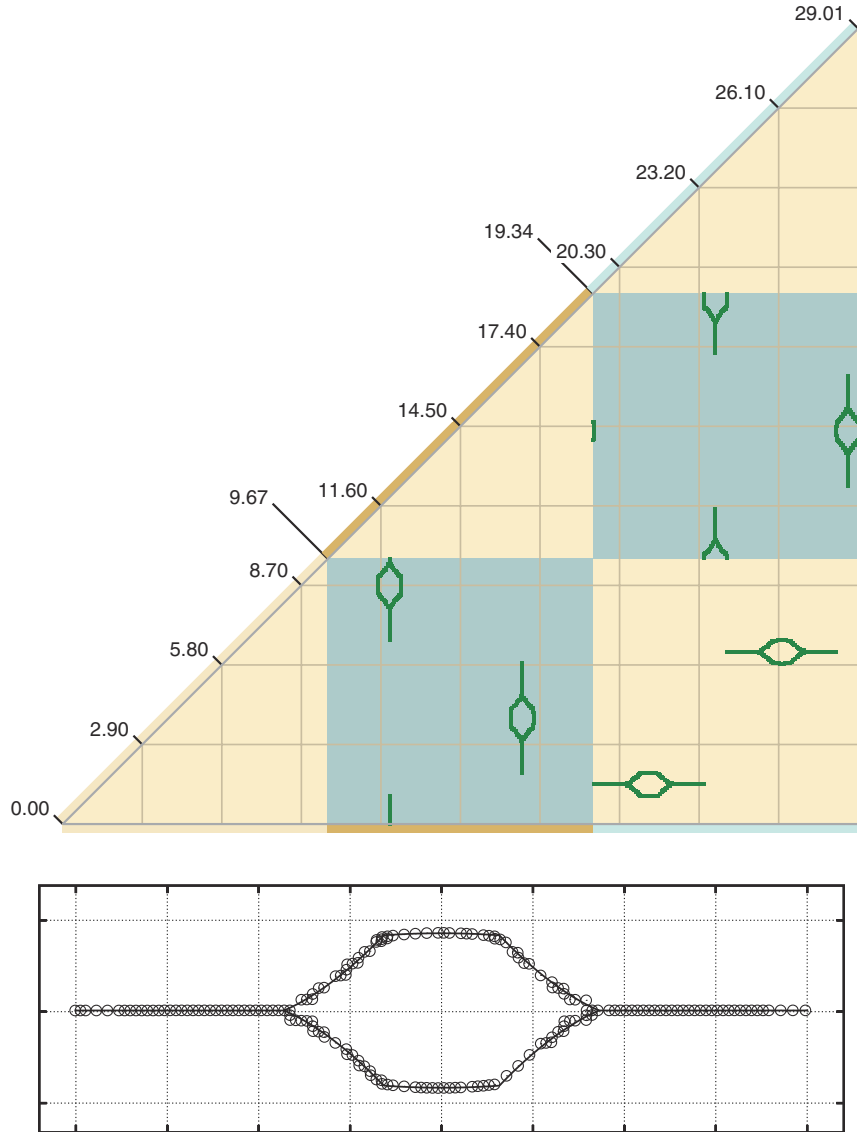
The polygonal ropelengths for our curves appear in the column  $\text{Rop}_p$  of Tables 3–5 of the appendix (Section 7), while a plot of the ropelengths organized by crossing number appears in Figure 10.

### 5.3. Generating Upper Bounds for Smooth Ropelength

Our computations yielded a large set of approximate minimizers of  $\text{Len}(\mathcal{V})/\text{Thi}_p(\mathcal{V})$ . From these, we wanted to generate upper bounds on the minimum (smooth) ropelength of these knots and links. Rawdon has given general bounds [Rawdon 98, Rawdon 03] on the rate at which  $\text{Thi}_p \rightarrow \text{Thi}$ , which we could have used for this purpose. But we were interested in small improvements in ropelength, so we used a more careful approach.

Our procedure for constructing smooth ropelength bounds from polygonal data is as follows. Beginning with

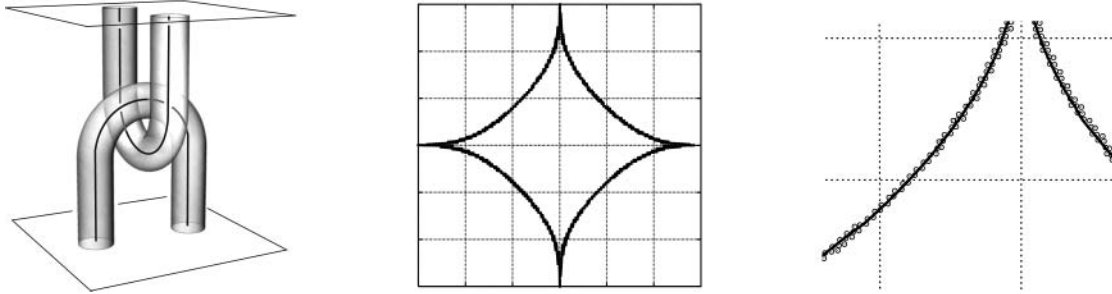
<sup>5</sup> Available at <http://www.knotplot.com>.



**FIGURE 7.** The diagonal above is labeled with arc-length values along the three components of the Borromean rings link, which is numbered  $6_3^3$  in Rolfsen’s table. Every pair  $(s, t) \in \text{Strut}(\mathcal{V})$  is represented by a dark green square centered on  $(s, t)$ . As we see from the top plot, no tube around a component of the link is in contact with itself (so the three triangles near the diagonal are empty). But each of the components makes contact with the other two, as shown by the boxes plotted in the rectangles forming the remainder of the plot. We can see that the contacts break up naturally into “lantern-shaped” structures. In the bottom plot, we compare one “lantern” to the self-contact set predicted by [Cantarella et al. 06], which is represented by a black line (Figure is available in color online).

$\mathcal{V}$ , we splice circle arcs of radius  $\text{MinRad}(v_i)$  into the corners at vertices  $v_i$  as shown on the left-hand side of Figure 9 to create a piecewise  $C^2$  curve  $V(s)$ . The minimal radius of curvature for this curve is equal to  $\text{MinRad}(\mathcal{V})$ . But the self-distances of  $V(s)$  may be different from those of the polygon  $\mathcal{V}$  if they involve the new circle arcs.

We must therefore compute the self-distances of  $\mathcal{V}(s)$ . This poses a problem:  $\mathcal{V}(s)$  is composed of arcs of circles and line segments, and Neff has shown that there is no simple formula for the distance between two arbitrary circle arcs in 3-space [Neff 90]. So we estimate the self-distances of the smooth curve  $V(s)$  by taking distances between a finite number of sample points on the curve



**FIGURE 8.** The left-hand picture shows a (loose) configuration of the “simple clasp”—a simple two-strand tangle that serves as an interesting model for the interaction between two ropes passing over each other at right angles. A ropelength-critical configuration of this tangle has been derived and studied extensively in [Cantarella et al. 06] and [Cantarella et al. 11]. Since this derivation included an explicit strut set, it is natural to compare *ridgerunner*’s results to this theoretical picture. This comparison is shown in the two plots center and right, which plot the positions of struts in arc-length coordinates with the origin located where each curve first begins to turn. The enlarged plot (right) shows the agreement between theoretical and computational results. The data shown are from a 332-edge polygonal clasp.

separated from one another by some  $\epsilon$ . These distances are presumably larger than the minimum self-distance along the curve, but we can use them to bound the minimum self-distance using the following proposition.

**Proposition 5.1.** *Suppose that  $c(s)$  and  $d(t)$  are each unit-speed piecewise  $C^2$  arcs with curvature bounded above by  $K$ . Further, suppose that  $\|c(0) - d(0)\| > 1/2$  is the minimum distance between  $c$  and  $d$ . Then for any  $0 \leq s, t \leq \epsilon$ ,*

$$\|c(0) - d(0)\| \geq \|c(s) - d(t)\| - (1 + K)\epsilon^2. \quad (5-1)$$

*Proof:* Since  $\|c(s) - d(t)\|$  has a local minimum at  $(0, 0)$ , we know that

$$\langle c'(0), c(0) - d(0) \rangle = 0 \quad \text{and} \quad \langle d'(0), c(0) - d(0) \rangle = 0.$$

Further, the curvature bound tells us that  $\|c''\|, \|d''\| < K$ . We will use these facts to estimate  $\|c(s) - d(t)\|^2$ . If we let  $C(s) = \int_0^s c'(x) dx$  and  $D(t) = \int_0^t d'(y) dy$ , then we

have  $c(s) = C(s) + c(0)$  and  $d(t) = D(t) + d(0)$ , so

$$\|c(s) - d(t)\|^2 = \|C(s) - D(t)\|^2 - 2\langle C(s) - D(t), c(0) - d(0) \rangle + \|c(0) - d(0)\|^2. \quad (5-2)$$

Since  $c(s)$  and  $d(t)$  are unit-speed curves and  $0 \leq s, t \leq \epsilon$ , we know that  $\|C(s)\|, \|D(t)\| < \epsilon$ , and so the first term is bounded above by  $4\epsilon^2$ .

The middle term is more interesting. As before, we can let  $CC(s) = \int_0^s c''(x) dx$  and  $DD(t) = \int_0^t d''(y) dy$ , so  $c'(s) = CC(s) + c'(0)$  and  $d'(t) = DD(t) + d'(0)$ . Since  $c'(0)$  and  $d'(0)$  are normal to  $c(0) - d(0)$ , we can then write this middle term as

$$\begin{aligned} & -\langle C(s) - D(t), c(0) - d(0) \rangle \\ &= -\left\langle \int_0^s CC(x) dx - \int_0^t DD(y) dy, c(0) - d(0) \right\rangle. \end{aligned}$$

Since  $\|c''\|, \|d''\| < K$ , we know that  $\|CC(s)\| < Ks$ ,  $\|DD(t)\| < Kt$ . Thus (recalling that  $s, t < \epsilon$ ) the norms of the integrals on the right above are each bounded above by  $K\epsilon^2/2$ , and the entire dot product is bounded above by  $K\epsilon^2\|c(0) - d(0)\|$ .



**FIGURE 9.** On the left, we see the curve constructed from splicing a circular arc of radius  $\text{MinRad}(v_i)$  into  $v_{i-1}v_iv_{i+1}$ . This curve is  $C^1$ , but not  $C^2$  at the splice points. On the right, we see the setup for Proposition 5-1. On the left and right are arcs  $c$  and  $d$  with curvature  $\leq K$  and length  $\leq \epsilon$ . The minimum distance  $x$  between them occurs at  $c(0), d(0)$ . We prove that this distance is bounded below by the distance between any other pair of points  $c(s)$  and  $d(t)$  minus  $(1 + K)\epsilon^2$ .

Cr	Rop	Links
3	32.74	$3_1$
4	[40.0122, 42.0887]	$4_1^2, 4_1$
5	[47.2016, 49.7716]	$5_1, 5_1^2$
6	[50.5539, 58.1013]	$6_3^3, 6_3^2$
7	[55.5095, 66.3147]	$7_7^2, 7_6^2$
8	[60.5754, 75.2592]	$8_7^3, 8_1^4$
9	[66.0311, 83.6092]	$9_{49}^2, 9_{42}^2$
10	[71.0739, 92.3565]	$10_{124}, 10_{123}$

**TABLE 2.** This table shows the links of smallest and largest minimum ropelength for each crossing number (according to our data). Recall that we did not minimize ten-crossing links, so it is likely that some ten-crossing link type has larger or smaller minimum ropelength than the  $10_{123}$  and  $10_{124}$  knots.

Thus the right-hand side of (5–2) is bounded by  $\|c(0) - d(0)\|^2 + 4\epsilon^2 + 2K\epsilon^2\|c(0) - d(0)\|$ . Since  $1/2 < \|c(0) - d(0)\|$ , we have  $4\epsilon^2 < 2\epsilon^2\|c(0) - d(0)\|$ . Using this, we see that

$$\begin{aligned} & 4\epsilon^2 + 2K\epsilon^2\|c(0) - d(0)\| + \|c(0) - d(0)\|^2 \\ & < \|c(0) - d(0)\|^2 + (2 + 2K)\epsilon^2\|c(0) - d(0)\| \\ & < (\|c(0) - d(0)\| + (1 + K)\epsilon^2)^2. \end{aligned}$$

This completes the proof.  $\square$

Our code, named `roundout_r1`,<sup>6</sup> establishes a coarse net of points on  $V(s) \times V(s) \simeq [0, 1] \times [0, 1]$  and then eliminates subsquares of this square from consideration using Proposition 5–1. The remaining squares are then subdivided and searched in turn. The process terminates once we have computed the local minima of  $d(p, q)$  on the square with whatever accuracy we require.

Using `roundout_r1` in double-precision machine arithmetic, we found upper bounds for the ropelengths of our 379-minimized configurations. These figures appear in column Rop of Tables 3 through 5, in Section 7. These figures constitute the best known data set on the lengths of tight knots and links. The data are summarized in Figure 10 and Table 2.

To test how accurate these final results are likely to be, we computed the relative residual  $\|(-\nabla f)_I\|/\|-\nabla f\|$  for all these knots and links. The average residual of knots in our tabulation is about 0.00289. We have

achieved residuals as low as  $2.54 \times 10^{-5}$  for knots and links of special interest, such as  $8_{18}$ ,  $10_{123}$ , the trefoil, and the Borromean rings. A table of these residuals appears in Section 7. We achieved residuals  $< 0.01$  for all the minimum ropelength positions of knots and links in our catalog except  $8_3^4$ , where a configuration built by hand from stadium curves proved slightly better than the best `ridgerunner` configuration.

#### 5.4. Generation of Tightening Animations, Pictures, and Strut Sets

We have saved the minimization runs for each of these knots and links as an animation showing the tightening knot.<sup>7</sup>

We have also generated images of the polygonal strut sets and approximately tight configurations for each of the 379 knots and links in our data set. Space considerations prevent us from including all of these data in this paper, so they are enclosed in the associated *Atlas of Tight Links* [Ashton et al. 11]. Figure 11 shows a typical page from the *Atlas*. All of our tight knot and link data, including coordinates for the tight configurations, are publicly available with the publication of this paper. We note that for technical reasons, our minimized configurations have thickness close to 1/2 (rather than 1, as in the discussion above), and hence their maximum curvature is 2.

#### 5.5. Discovery of Symmetric Tight Knots

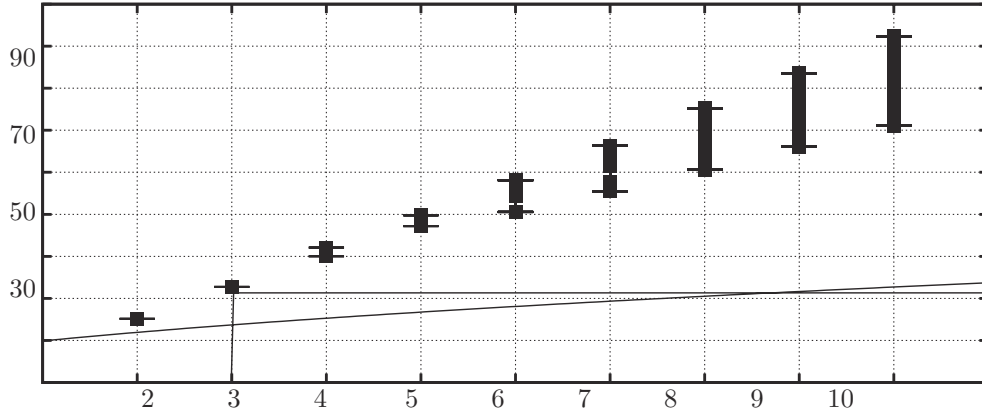
An interesting feature of the ropelength function is that minimizing ropelength usually breaks any symmetry enjoyed by the original configuration of a given knot. For instance, while the minimizing configuration for the (3, 2) torus knot  $3_1$  appears to be threefold symmetric (as expected), the minimizing configuration for the (5, 2) torus knot  $5_1$  is not fivefold symmetric. It was therefore somewhat surprising to discover two knots in our data set,  $8_{18}$  and  $10_{123}$ , for which the tight configurations are highly symmetric. These knots are shown in Figure 12. Their self-contact sets (which appear on pages 67 and 358 of the *Atlas*, and are reproduced in Section 7 of this paper as Figures 15 and 16) are highly suggestive, resembling those of the Borromean rings (page 29), and appearing to consist of a single element repeated several times. This feature implies that these knots may be better candidates for explicit solution than the seemingly simpler trefoil knot.

<sup>6</sup>The source code for `roundout_r1` is freely available as part of the `octrope` library.

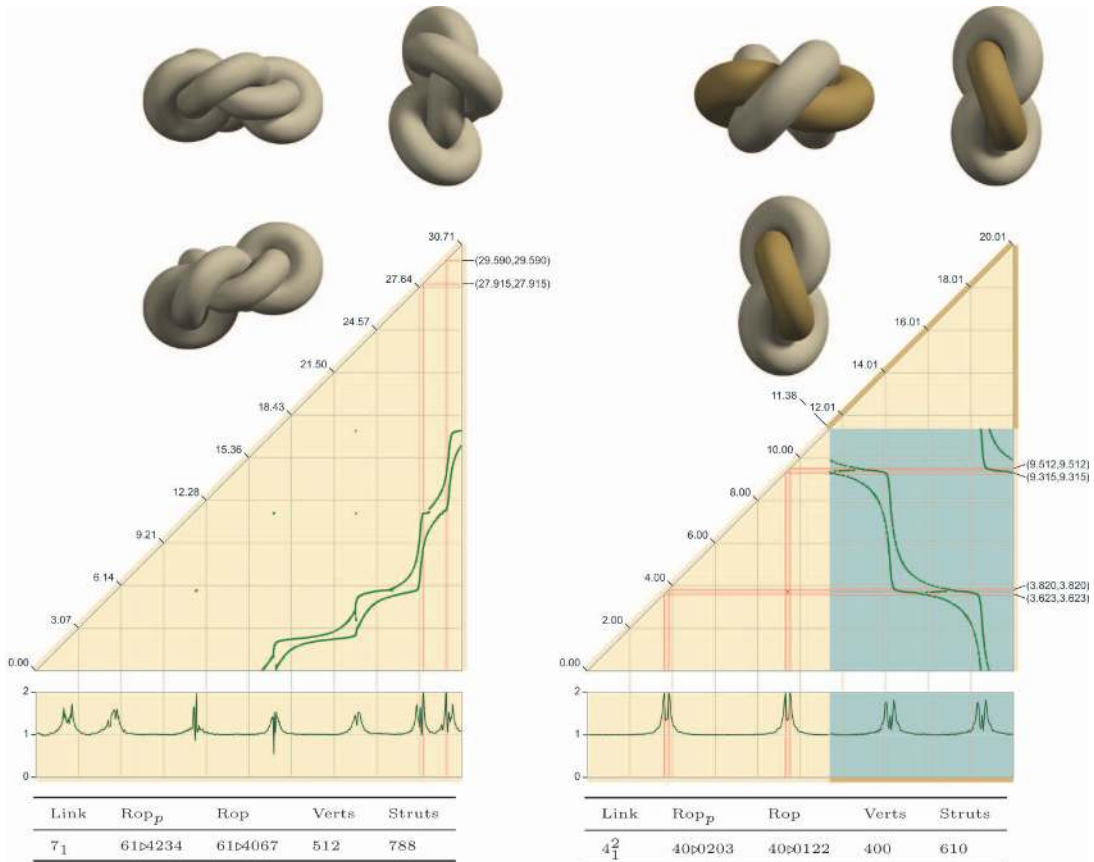
<sup>7</sup>These animations are posted on the web at <http://www.jasoncantarella.com/movs/>.

Link	Rop <sub>p</sub>	Rop	Link	Rop <sub>p</sub>	Rop	Link	Rop <sub>p</sub>	Rop
2 <sub>1</sub> <sup>2</sup>	25.1415	25.1334	8 <sub>2</sub>	71.4141	71.3985	8 <sub>8</sub> <sup>3</sup>	65.0195	65.0042
3 <sub>1</sub>	32.7437	32.7436	8 <sub>3</sub>	71.1736	71.1575	8 <sub>9</sub> <sup>3</sup>	66.7076	66.6936
4 <sub>1</sub>	42.0971	42.0887	8 <sub>4</sub>	71.4872	71.4704	8 <sub>10</sub> <sup>3</sup>	65.4704	65.4580
4 <sub>1</sub> <sup>2</sup>	40.0203	40.0122	8 <sub>5</sub>	72.1519	72.1344	8 <sub>1</sub> <sup>4</sup>	75.2748	75.2592
5 <sub>1</sub>	47.2149	47.2016	8 <sub>6</sub>	72.4903	72.4725	8 <sub>2</sub> <sup>4</sup>	67.4087	67.3937
5 <sub>2</sub>	49.4820	49.4701	8 <sub>7</sub>	72.2292	72.2137	8 <sub>3</sub> <sup>4</sup>	66.2969	66.2865
5 <sub>1</sub> <sup>2</sup>	49.7864	49.7716	8 <sub>8</sub>	72.7438	72.7241	9 <sub>1</sub>	75.5663	75.5461
6 <sub>1</sub>	56.7178	56.7058	8 <sub>9</sub>	72.4568	72.4399	9 <sub>2</sub>	78.1231	78.1066
6 <sub>2</sub>	57.0381	57.0235	8 <sub>10</sub>	72.9580	72.9379	9 <sub>3</sub>	78.2040	78.1892
6 <sub>3</sub>	57.8531	57.8392	8 <sub>11</sub>	72.9110	72.8966	9 <sub>4</sub>	78.2793	78.2665
6 <sub>1</sub> <sup>2</sup>	54.3919	54.3768	8 <sub>12</sub>	73.9707	73.9518	9 <sub>5</sub>	78.6615	78.6447
6 <sub>2</sub> <sup>2</sup>	56.7087	56.7000	8 <sub>13</sub>	72.8194	72.8000	9 <sub>6</sub>	79.5802	79.5597
6 <sub>3</sub> <sup>2</sup>	58.1142	58.1013	8 <sub>14</sub>	73.7784	73.7612	9 <sub>7</sub>	79.6924	79.6731
6 <sub>1</sub> <sup>3</sup>	57.8286	57.8141	8 <sub>15</sub>	73.9076	73.8977	9 <sub>8</sub>	80.0276	80.0080
6 <sub>2</sub> <sup>3</sup>	58.0112	58.0070	8 <sub>16</sub>	73.5207	73.5054	9 <sub>9</sub>	79.8965	79.8778
6 <sub>3</sub> <sup>3</sup>	50.5602	50.5539	8 <sub>17</sub>	74.5075	74.4912	9 <sub>10</sub>	79.8009	79.7855
7 <sub>1</sub>	61.4234	61.4067	8 <sub>18</sub>	74.9114	74.9063	9 <sub>11</sub>	80.1355	80.1180
7 <sub>2</sub>	63.8684	63.8556	8 <sub>19</sub>	60.9970	60.9858	9 <sub>12</sub>	80.0997	80.0834
7 <sub>3</sub>	63.9430	63.9285	8 <sub>20</sub>	63.1066	63.0929	9 <sub>13</sub>	80.2657	80.2498
7 <sub>4</sub>	64.2836	64.2687	8 <sub>21</sub>	65.5387	65.5248	9 <sub>14</sub>	80.0193	80.0001
7 <sub>5</sub>	65.2705	65.2560	8 <sub>1</sub> <sup>2</sup>	68.4208	68.4045	9 <sub>15</sub>	80.8941	80.8725
7 <sub>6</sub>	65.7068	65.6924	8 <sub>2</sub> <sup>2</sup>	71.0493	71.0311	9 <sub>16</sub>	80.1334	80.1143
7 <sub>7</sub>	65.6235	65.6086	8 <sub>3</sub> <sup>2</sup>	72.7292	72.7133	9 <sub>17</sub>	80.4718	80.4530
7 <sub>1</sub> <sup>2</sup>	64.2484	64.2345	8 <sub>4</sub> <sup>2</sup>	72.5995	72.5855	9 <sub>18</sub>	81.5816	81.5673
7 <sub>2</sub> <sup>2</sup>	65.0363	65.0204	8 <sub>5</sub> <sup>2</sup>	73.9503	73.9331	9 <sub>19</sub>	80.9196	80.9004
7 <sub>3</sub> <sup>2</sup>	65.3414	65.3257	8 <sub>6</sub> <sup>2</sup>	73.2133	73.1955	9 <sub>20</sub>	80.2421	80.2219
7 <sub>4</sub> <sup>2</sup>	65.0759	65.0602	8 <sub>7</sub> <sup>2</sup>	74.3917	74.3752	9 <sub>21</sub>	81.1083	81.0920
7 <sub>5</sub> <sup>2</sup>	66.2068	66.1915	8 <sub>8</sub> <sup>2</sup>	73.7714	73.7540	9 <sub>22</sub>	81.0587	81.0390
7 <sub>6</sub> <sup>2</sup>	66.3281	66.3147	8 <sub>9</sub> <sup>2</sup>	73.2196	73.2038	9 <sub>23</sub>	81.2922	81.2733
7 <sub>7</sub> <sup>2</sup>	55.5177	55.5095	8 <sub>10</sub> <sup>2</sup>	73.6729	73.6548	9 <sub>24</sub>	80.9626	80.9451
7 <sub>8</sub> <sup>2</sup>	57.7714	57.7631	8 <sub>11</sub> <sup>2</sup>	72.9786	72.9608	9 <sub>25</sub>	81.1348	81.1198
7 <sub>1</sub> <sup>3</sup>	65.8157	65.8062	8 <sub>12</sub> <sup>2</sup>	73.8018	73.7846	9 <sub>26</sub>	80.9241	80.9053
8 <sub>1</sub>	70.9833	70.9669	8 <sub>13</sub> <sup>2</sup>	74.1522	74.1369	9 <sub>27</sub>	81.1838	81.1813
8 <sub>2</sub>	71.4141	71.3985	8 <sub>14</sub> <sup>2</sup>	73.6878	73.6695	9 <sub>28</sub>	81.0878	81.1352
			8 <sub>15</sub> <sup>2</sup>	64.3105	64.2996	9 <sub>29</sub>	81.2019	81.1821
			8 <sub>16</sub> <sup>2</sup>	66.8148	66.8046	9 <sub>30</sub>	81.4811	81.4883
			8 <sub>1</sub> <sup>3</sup>	72.2765	72.2603	9 <sub>31</sub>	81.6751	81.6581
			8 <sub>2</sub> <sup>3</sup>	72.9357	72.9181	9 <sub>32</sub>	81.5343	81.5175
			8 <sub>3</sub> <sup>3</sup>	74.8824	74.8656	9 <sub>33</sub>	82.7691	82.7541
			8 <sub>4</sub> <sup>3</sup>	75.0026	74.9866	9 <sub>34</sub>	82.1884	82.1706
			8 <sub>5</sub> <sup>3</sup>	73.4072	73.3932	9 <sub>35</sub>	79.2390	79.2165
			8 <sub>6</sub> <sup>3</sup>	74.7320	74.7159	9 <sub>36</sub>	80.2275	80.2064
			8 <sub>7</sub> <sup>3</sup>	60.5897	60.5754	9 <sub>37</sub>	81.1744	81.1674
			8 <sub>8</sub> <sup>3</sup>	65.0195	65.0042	9 <sub>38</sub>	81.7858	81.7697

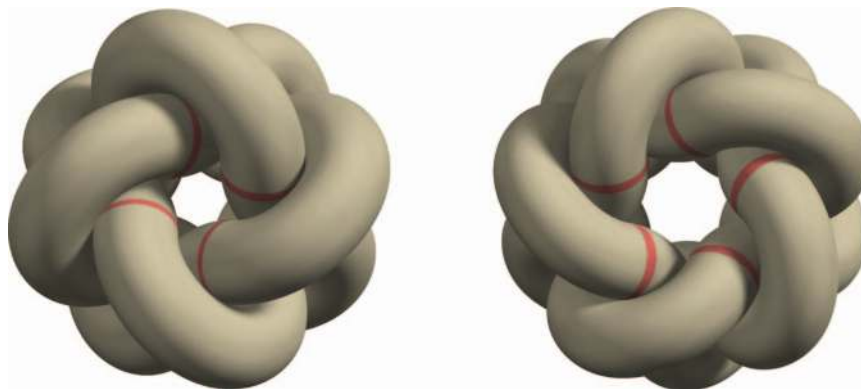
TABLE 3. Part 1 of Ropelengths of tight knots and links by knot type.



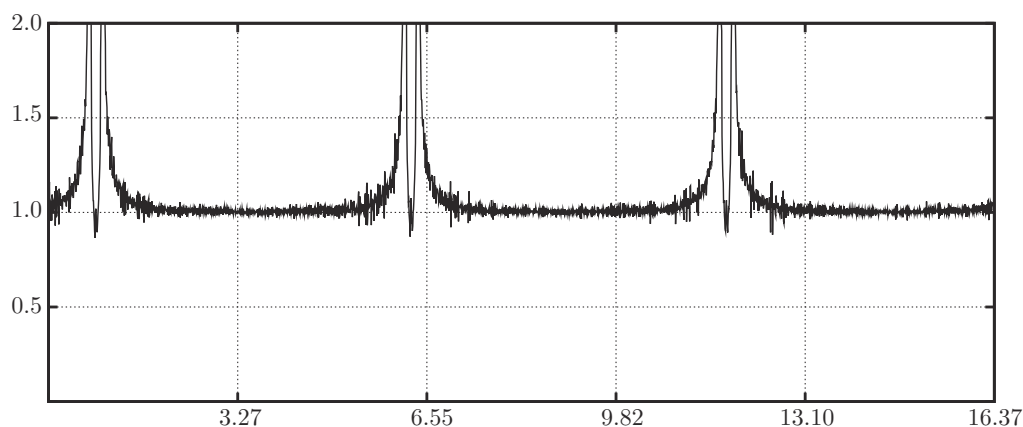
**FIGURE 10.** This graph shows the relationship between ropelength ( $y$ -axis) and crossing number ( $x$ -axis) for knots and links in our data set. The bottom lines show the bound of [Denne et al. 06] for ropelength of a nontrivial knot (horizontal line, dropping to zero below crossing number 3) and Diao’s bound [Diao 03] for ropelength in terms of crossing number (curve). We can see that there is a substantial overlap of ropelength values between different crossing numbers. This is reflected in Tables 6–7 of Section 7, which show the knots in ropelength order. Table 2 shows the links of least and greatest ropelength for each crossing number.



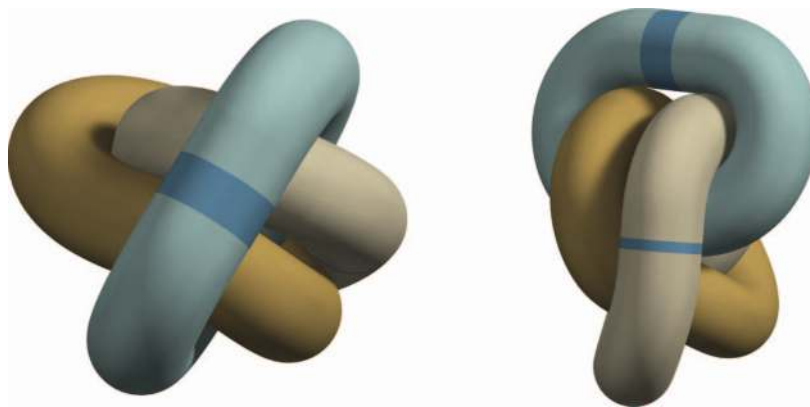
**FIGURE 11.** This figure shows simplified versions of two pages from the *Atlas of Tight Links* for the knot  $7_1$  and the link  $4_1^2$ . On each page, the top left pictures show three views of the link. The triangular graphic shows the struts of the link as found by `ridgerunner` plotted as points  $(s, t)$  in arc-length coordinates along the link. The background of each plot changes color to indicate the change from one component to the next. The key along the left-to-right diagonal is given in arc-length units and color-coded with the pictures at upper left to show which component is referred to by the plot. Recall that these configurations have thickness  $1/2$ , so the maximum arc-length value is half the ropelength. (Figure is available in color online)



**FIGURE 12.** Two highly symmetric tight knots are the  $8_{18}$  knot shown above left and the  $10_{123}$  knot shown above right. Rounding the corners of these curves yields ropelength upper bounds of 74.9063 and 92.3565, respectively. Because their strut sets break into a particularly simple form (see Figures 15 and 16), these knots may be better candidates for an explicit solution than the trefoil. (Figure is available in color online)



**FIGURE 13.** This plot shows the computed  $1/\text{MinRad}$  values as a function of arc length along the polygon for a 2400-edge trefoil with thickness close to  $1/2$ , residual 0.0018, and polygonal ropelength 32.743663 (rounding out the corners as described above gives a smooth ropelength upper bound of 32.74352 for this configuration). The value at each vertex is plotted above with no numerical smoothing. Although there is some noise in the portions of the plot where curvature is not constrained, the six kinked regions are clearly resolved. A total of 117 vertices are involved in these regions.



**FIGURE 14.** This figure shows two views of our computed tight configuration of the link  $6_3^3$  (ropelength upper bound 50.5539). Straight segments on the blue and white components, which occur when these components lose contact with the other components of the link, are highlighted in darker blue. (Figure is available in color online)



Link	Rop <sub>p</sub>	Rop	Link	Rop <sub>p</sub>	Rop	Link	Rop <sub>p</sub>	Rop
9 <sub>38</sub>	81.7858	81.7697	9 <sub>33</sub> <sup>2</sup>	82.1790	82.1612	9 <sub>16</sub> <sup>3</sup>	75.0113	75.0003
9 <sub>39</sub>	81.8439	81.8264	9 <sub>34</sub> <sup>2</sup>	81.8490	81.8320	9 <sub>17</sub> <sup>3</sup>	72.8831	72.8705
9 <sub>40</sub>	81.6652	81.6474	9 <sub>35</sub> <sup>2</sup>	81.2508	81.2318	9 <sub>18</sub> <sup>3</sup>	72.4529	72.4382
9 <sub>41</sub>	81.3687	81.3540	9 <sub>36</sub> <sup>2</sup>	80.7066	80.6866	9 <sub>19</sub> <sup>3</sup>	72.6412	72.6275
9 <sub>42</sub>	69.4867	69.4756	9 <sub>37</sub> <sup>2</sup>	81.9102	81.8927	9 <sub>20</sub> <sup>3</sup>	75.9995	75.9845
9 <sub>43</sub>	71.5050	71.4901	9 <sub>38</sub> <sup>2</sup>	82.6750	82.6561	9 <sub>21</sub> <sup>3</sup>	74.8967	74.8908
9 <sub>44</sub>	71.5587	71.5427	9 <sub>39</sub> <sup>2</sup>	81.8972	81.8758	9 <sub>1</sub> <sup>4</sup>	81.6096	81.5927
9 <sub>45</sub>	74.0861	74.0761	9 <sub>40</sub> <sup>2</sup>	81.9680	81.9460	10 <sub>1</sub>	85.1146	85.0947
9 <sub>46</sub>	68.6330	68.6169	9 <sub>41</sub> <sup>2</sup>	83.6038	83.5878	10 <sub>2</sub>	85.6050	85.5850
9 <sub>47</sub>	74.8935	74.8785	9 <sub>42</sub> <sup>2</sup>	83.6304	83.6092	10 <sub>3</sub>	85.4483	85.4278
9 <sub>48</sub>	74.0317	74.0228	9 <sub>43</sub> <sup>2</sup>	66.2549	66.2398	10 <sub>4</sub>	85.8181	85.7974
9 <sub>49</sub>	73.9403	73.9286	9 <sub>44</sub> <sup>2</sup>	72.2072	72.1896	10 <sub>5</sub>	86.4952	86.4741
9 <sub>1</sub> <sup>2</sup>	78.6049	78.5862	9 <sub>45</sub> <sup>2</sup>	71.0815	71.0726	10 <sub>6</sub>	86.8353	86.8125
9 <sub>2</sub> <sup>2</sup>	79.5287	79.5152	9 <sub>46</sub> <sup>2</sup>	73.8347	73.8215	10 <sub>7</sub>	87.2979	87.2775
9 <sub>3</sub> <sup>2</sup>	79.9495	79.9312	9 <sub>47</sub> <sup>2</sup>	69.9130	69.8983	10 <sub>8</sub>	85.8620	85.8428
9 <sub>4</sub> <sup>2</sup>	78.6961	78.6764	9 <sub>48</sub> <sup>2</sup>	73.6563	73.6426	10 <sub>9</sub>	86.8410	86.8222
9 <sub>5</sub> <sup>2</sup>	79.6569	79.6384	9 <sub>49</sub> <sup>2</sup>	66.0444	66.0311	10 <sub>10</sub>	87.2060	87.1870
9 <sub>6</sub> <sup>2</sup>	80.1200	80.1017	9 <sub>50</sub> <sup>2</sup>	69.3353	69.3284	10 <sub>11</sub>	86.9848	86.9630
9 <sub>7</sub> <sup>2</sup>	81.1437	81.1261	9 <sub>51</sub> <sup>2</sup>	70.5455	70.5299	10 <sub>12</sub>	87.1055	87.0824
9 <sub>8</sub> <sup>2</sup>	80.9964	80.9766	9 <sub>52</sub> <sup>2</sup>	72.8271	72.8106	10 <sub>13</sub>	88.9148	88.8989
9 <sub>9</sub> <sup>2</sup>	80.3174	80.2999	9 <sub>53</sub> <sup>2</sup>	68.0154	68.0082	10 <sub>14</sub>	88.3232	88.3023
9 <sub>10</sub> <sup>2</sup>	80.3218	80.3036	9 <sub>54</sub> <sup>2</sup>	71.0240	71.0089	10 <sub>15</sub>	87.4787	87.4606
9 <sub>11</sub> <sup>2</sup>	82.0329	82.0140	9 <sub>55</sub> <sup>2</sup>	73.8129	73.7998	10 <sub>16</sub>	87.4946	87.4684
9 <sub>12</sub> <sup>2</sup>	81.9602	81.9414	9 <sub>56</sub> <sup>2</sup>	72.9013	72.8833	10 <sub>17</sub>	87.0473	87.0277
9 <sub>13</sub> <sup>2</sup>	79.3468	79.3280	9 <sub>57</sub> <sup>2</sup>	72.2115	72.1922	10 <sub>18</sub>	88.4257	88.4092
9 <sub>14</sub> <sup>2</sup>	80.7276	80.7104	9 <sub>58</sub> <sup>2</sup>	74.1685	74.1499	10 <sub>19</sub>	87.5311	87.5099
9 <sub>15</sub> <sup>2</sup>	80.5659	80.5458	9 <sub>59</sub> <sup>2</sup>	72.3285	72.3130	10 <sub>20</sub>	86.8731	86.8514
9 <sub>16</sub> <sup>2</sup>	81.3758	81.3565	9 <sub>60</sub> <sup>2</sup>	73.5589	73.5442	10 <sub>21</sub>	87.0497	87.0343
9 <sub>17</sub> <sup>2</sup>	80.3223	80.3022	9 <sub>61</sub> <sup>2</sup>	69.3751	69.3636	10 <sub>22</sub>	87.2417	87.2182
9 <sub>18</sub> <sup>2</sup>	81.7563	81.7461	9 <sub>1</sub> <sup>3</sup>	81.1522	81.1333	10 <sub>23</sub>	88.7048	88.6901
9 <sub>19</sub> <sup>2</sup>	79.4706	79.4491	9 <sub>2</sub> <sup>3</sup>	81.7304	81.7190	10 <sub>24</sub>	88.4160	88.3963
9 <sub>20</sub> <sup>2</sup>	80.1357	80.1147	9 <sub>3</sub> <sup>3</sup>	82.2498	82.2346	10 <sub>25</sub>	88.7767	88.7587
9 <sub>21</sub> <sup>2</sup>	80.6010	80.5824	9 <sub>4</sub> <sup>3</sup>	82.5202	82.5029	10 <sub>26</sub>	88.4564	88.4328
9 <sub>22</sub> <sup>2</sup>	81.0964	81.0794	9 <sub>5</sub> <sup>3</sup>	80.2664	80.2456	10 <sub>27</sub>	89.8944	89.8795
9 <sub>23</sub> <sup>2</sup>	80.2592	80.2379	9 <sub>6</sub> <sup>3</sup>	80.9434	80.9258	10 <sub>28</sub>	87.5276	87.5061
9 <sub>24</sub> <sup>2</sup>	81.7913	81.7691	9 <sub>7</sub> <sup>3</sup>	82.0540	82.0378	10 <sub>29</sub>	89.2410	89.2238
9 <sub>25</sub> <sup>2</sup>	81.7810	81.7630	9 <sub>8</sub> <sup>3</sup>	81.1278	81.1107	10 <sub>30</sub>	88.3731	88.3558
9 <sub>26</sub> <sup>2</sup>	82.1031	82.0859	9 <sub>9</sub> <sup>3</sup>	81.5469	81.5295	10 <sub>31</sub>	88.2624	88.2401
9 <sub>27</sub> <sup>2</sup>	81.0288	81.0141	9 <sub>10</sub> <sup>3</sup>	82.3146	82.2964	10 <sub>32</sub>	88.6809	88.6597
9 <sub>28</sub> <sup>2</sup>	81.3352	81.3222	9 <sub>11</sub> <sup>3</sup>	82.0023	81.9867	10 <sub>33</sub>	88.2952	88.2744
9 <sub>29</sub> <sup>2</sup>	82.1606	82.1445	9 <sub>12</sub> <sup>3</sup>	82.4811	82.4608	10 <sub>34</sub>	87.0322	87.0101
9 <sub>30</sub> <sup>2</sup>	82.2155	82.1987	9 <sub>13</sub> <sup>3</sup>	71.9210	71.9119	10 <sub>35</sub>	88.0891	88.0697
9 <sub>31</sub> <sup>2</sup>	80.5732	80.5561	9 <sub>14</sub> <sup>3</sup>	74.4319	74.4205	10 <sub>36</sub>	88.0424	88.0233
9 <sub>32</sub> <sup>2</sup>	81.4151	81.3990	9 <sub>15</sub> <sup>3</sup>	74.2998	74.2810	10 <sub>37</sub>	88.1319	88.1153
9 <sub>33</sub> <sup>2</sup>	82.1790	82.1612	9 <sub>16</sub> <sup>3</sup>	75.0113	75.0003			

TABLE 4. Part 2 of ropelengths of tight knots and links by knot type.

Link	Rop <sub>p</sub>	Rop	Link	Rop <sub>p</sub>	Rop	Link	Rop <sub>p</sub>	Rop
10 <sub>37</sub>	88.1319	88.1153	10 <sub>80</sub>	89.1669	89.1556	10 <sub>123</sub>	92.3646	92.3565
10 <sub>38</sub>	88.3478	88.3257	10 <sub>81</sub>	90.0181	90.0007	10 <sub>124</sub>	71.0894	71.0739
10 <sub>39</sub>	88.3562	88.3323	10 <sub>82</sub>	88.7011	88.6801	10 <sub>125</sub>	74.9907	74.9778
10 <sub>40</sub>	89.2659	89.2464	10 <sub>83</sub>	89.5544	89.5314	10 <sub>126</sub>	77.6202	77.6026
10 <sub>41</sub>	89.0725	89.0553	10 <sub>84</sub>	89.6518	89.6788	10 <sub>127</sub>	80.0235	80.0124
10 <sub>42</sub>	89.9013	89.8857	10 <sub>85</sub>	87.8403	87.8164	10 <sub>128</sub>	76.4187	76.4026
10 <sub>43</sub>	89.3512	89.3366	10 <sub>86</sub>	88.7050	88.6851	10 <sub>129</sub>	78.5739	78.5553
10 <sub>44</sub>	88.8714	88.8515	10 <sub>87</sub>	89.1363	89.1173	10 <sub>130</sub>	78.8499	78.8356
10 <sub>45</sub>	89.4836	89.4621	10 <sub>88</sub>	89.5638	89.5461	10 <sub>131</sub>	81.2871	81.2678
10 <sub>46</sub>	86.4718	86.4487	10 <sub>89</sub>	89.4343	89.4178	10 <sub>132</sub>	74.7441	74.7330
10 <sub>47</sub>	87.3043	87.2821	10 <sub>90</sub>	88.9330	88.9115	10 <sub>133</sub>	77.1813	77.1631
10 <sub>48</sub>	87.3814	87.3643	10 <sub>91</sub>	88.9611	88.9435	10 <sub>134</sub>	78.6521	78.6377
10 <sub>49</sub>	88.2914	88.2705	10 <sub>92</sub>	89.6200	89.6011	10 <sub>135</sub>	81.2305	81.2157
10 <sub>50</sub>	87.3876	87.3716	10 <sub>93</sub>	88.3962	88.3773	10 <sub>136</sub>	78.0398	78.0276
10 <sub>51</sub>	88.3209	88.3002	10 <sub>94</sub>	88.8514	88.8306	10 <sub>137</sub>	79.6352	79.6185
10 <sub>52</sub>	88.0719	88.0565	10 <sub>95</sub>	90.0056	89.9848	10 <sub>138</sub>	82.5504	82.5320
10 <sub>53</sub>	88.8361	88.8180	10 <sub>96</sub>	89.5493	89.5284	10 <sub>139</sub>	72.9001	72.8944
10 <sub>54</sub>	87.5336	87.5127	10 <sub>97</sub>	89.4340	89.4163	10 <sub>140</sub>	73.8610	73.8477
10 <sub>55</sub>	88.3760	88.3699	10 <sub>98</sub>	89.7172	89.6969	10 <sub>141</sub>	76.9687	76.9543
10 <sub>56</sub>	89.0160	88.9973	10 <sub>99</sub>	88.8926	88.8734	10 <sub>142</sub>	75.8951	75.8754
10 <sub>57</sub>	89.6126	89.5946	10 <sub>100</sub>	88.7124	88.6927	10 <sub>143</sub>	78.2422	78.2307
10 <sub>58</sub>	88.9623	88.9445	10 <sub>101</sub>	89.7344	89.7210	10 <sub>144</sub>	81.4378	81.4275
10 <sub>59</sub>	89.2228	89.2090	10 <sub>102</sub>	88.7969	88.7734	10 <sub>145</sub>	75.9194	75.9076
10 <sub>60</sub>	89.3397	89.3190	10 <sub>103</sub>	88.7971	88.7914	10 <sub>146</sub>	79.7416	79.7322
10 <sub>61</sub>	86.3754	86.3571	10 <sub>104</sub>	91.7476	91.7280	10 <sub>147</sub>	79.1666	79.1571
10 <sub>62</sub>	87.5318	87.5071	10 <sub>105</sub>	89.8260	89.8055	10 <sub>148</sub>	79.0893	79.0742
10 <sub>63</sub>	88.4046	88.3861	10 <sub>106</sub>	89.1546	89.1319	10 <sub>149</sub>	81.0500	81.0318
10 <sub>64</sub>	87.4878	87.4742	10 <sub>107</sub>	89.7525	89.7356	10 <sub>150</sub>	80.1392	80.1219
10 <sub>65</sub>	88.3918	88.3725	10 <sub>108</sub>	88.5137	88.4932	10 <sub>151</sub>	81.8414	81.8207
10 <sub>66</sub>	89.0275	89.0047	10 <sub>109</sub>	91.1966	91.1789	10 <sub>152</sub>	79.1715	79.1556
10 <sub>67</sub>	88.4741	88.4534	10 <sub>110</sub>	89.6275	89.6114	10 <sub>153</sub>	80.4764	80.4648
10 <sub>68</sub>	88.1199	88.1013	10 <sub>111</sub>	89.6677	89.6438	10 <sub>154</sub>	81.5405	81.5218
10 <sub>69</sub>	89.0983	89.0778	10 <sub>112</sub>	89.5744	89.5529	10 <sub>155</sub>	78.0648	78.0503
10 <sub>70</sub>	89.2068	89.1846	10 <sub>113</sub>	90.2239	90.2141	10 <sub>156</sub>	79.5639	79.5443
10 <sub>71</sub>	89.0853	89.0699	10 <sub>114</sub>	89.3062	89.2856	10 <sub>157</sub>	81.4731	81.4568
10 <sub>72</sub>	89.1974	89.1779	10 <sub>115</sub>	90.4340	90.4176	10 <sub>158</sub>	81.6398	81.6220
10 <sub>73</sub>	89.5332	89.5130	10 <sub>116</sub>	90.2703	90.2583	10 <sub>159</sub>	79.8863	79.8692
10 <sub>74</sub>	88.1285	88.1077	10 <sub>117</sub>	89.5335	89.5245	10 <sub>160</sub>	78.1529	78.1472
10 <sub>75</sub>	88.9725	88.9524	10 <sub>118</sub>	89.5261	89.5094	10 <sub>161</sub>	74.5460	74.5302
10 <sub>76</sub>	88.3673	88.3479	10 <sub>119</sub>	90.1394	90.1226	10 <sub>162</sub>	81.0033	80.9838
10 <sub>77</sub>	88.5689	88.5471	10 <sub>120</sub>	90.1862	90.1674	10 <sub>163</sub>	82.6629	82.6548
10 <sub>78</sub>	88.5548	88.5322	10 <sub>121</sub>	89.9375	89.9240	10 <sub>164</sub>	82.1862	82.1698
10 <sub>79</sub>	88.9647	88.9488	10 <sub>122</sub>	89.8258	89.8094	10 <sub>165</sub>	82.8211	82.8040
10 <sub>80</sub>	89.1669	89.1556	10 <sub>123</sub>	92.3646	92.3565			

TABLE 5. Part 3 of ropelengths of tight knots and links by knot type.

## 6. FUTURE DIRECTIONS

Several directions for future research suggest themselves from these experiments. First, we note that while we have given finite strut sets for several polygonal knots and observed that they are close to the 1-dimensional strut sets for the corresponding smooth tight configurations, we have not proved a theorem explaining how our polygonal strut sets converge to the strut sets of a critical polygon. We conjecture that this is part of a larger theorem that would show that if a family of polygonal-ropelength critical configurations  $\mathcal{V}_n$  converges to a  $C^{1,1}$  curve  $V$ , then  $V$  is ropelength-critical in the sense of [Cantarella et al. 11], the strut sets of the  $\mathcal{V}_n$  converge in Hausdorff distance to the self-contact set of  $V$ , and the kink sets of the  $\mathcal{V}_n$  converge to the portion of  $V$  at maximum curvature.

There are several features of the tight knot data set that we have discovered that seem worthy of further investigation. Carlen, Smutny, and Maddocks noted in [Carlen et al. 05] that curvature constraints seemed to be “within a rather small tolerance of being active” at several points on their numerical approximations of the tight trefoil and figure-eight knots. Baranska et al. provided plots of the curvature of their approximately tight trefoil in [Baranska et al. 08] that appear to confirm this observation (in fact, these authors even provide approximate plots of the *torsion* of their tight trefoil obtained by numerical smoothing).

We have noticed the same phenomenon in our data sets. Our computation of the curvature for the trefoil appears in Figure 13. In the *Atlas of Tight Knots*, we highlight the active curvature constraints found by `ridgerunner` as part of the minimization process by red lines on the plot of strut sets. These active curvature constraints occur in 359 of the 379 knots and links minimized. This provides suggestive numerical evidence that kinks are rather common in tight knots. We intend to provide better evidence for this conjecture in an upcoming publication.

Several authors have proved versions of the theorem that an interval of a tight knot with curvature less than the maximum allowed and no struts must be a straight line segment [Gonzalez and Maddocks 99, Schuricht and von der Mosel 04, Durumeric 07, Cantarella et al. 11]. We see this phenomenon 325 times in the *Atlas*, for instance in the link  $6_3^3$  on page 28 (see also Figure 14), which appears to have three straight segments of arc lengths 2.1, 1.14, and 0.56. We highlight these segments in blue on the plots in the *Atlas*. These segments are almost as common as kinked regions in our data set, suggesting that

they are generic features of tight configurations. Gonzalez has conjectured that every composite knot formed from joining a knot to its mirror image has a critical configuration with a pair of straight segments. We do not address this conjecture here, since we consider only prime knots and links, but we do intend to compute approximately minimizing composite knots and links in a future publication.

The paper [Cantarella et al. 11] (as well as [Maddocks and Keller 87] under very different hypotheses) shows that a pair of arcs in a tight knot coparameterized by a single family of struts and having curvature less than the maximum bound form a standard double helix. As far as we can tell, this phenomenon occurs only a few times in the *Atlas*, for instance in the  $6_3^3$  link on page 28, the  $7_7^2$  link on page 43, the  $8_{19}$  knot on page 66, and possibly in the  $8_7^3$  link on page 91. It would be interesting to look for more critical configurations with double-helix sections.

We also contemplate further improvements to our numerical knot-tightening methods. The constrained gradient descent method presented in this paper is a significant improvement over simulated annealing—in practice, it has proved to be an effective minimizer for both knots and links. But this is surely not the last word in numerical ropelength minimization. Our method is a member of the class of “projected-gradient” methods introduced by Rosen and Zoutendijk in the early 1960s [Rosen 61, Zoutendijk 59]. These algorithms are subject to a number of well-known numerical problems, such as a tendency to “wobble” when confronted with a steep-sided valley and the problem of “zigzagging,” which occurs when elements repeatedly enter and leave the strut and kink sets on successive minimization or error-correction steps. Our implementation seems to suffer from both these problems during some difficult minimizations. We have experimented with adding conjugate-gradient features to our existing code to solve these problems, but so far, the results seem to yield only a slight improvement.

For these reasons, more modern methods such as sequential quadratic programming (SQP) have become the norm [Fletcher 01]. Codes implementing these methods require the user to specify a set of constraint functions in advance. Unfortunately, in our formulation of the constraint thickness, an  $n$ -vertex polygon has  $O(n^2)$  self-distance constraints and  $O(n)$  turning angle or MinRad constraints. For a typical polygon with  $10^3$  vertices, this would mean a set of  $10^6$  constraints—too many to be practical. However, if we know approximately which self-distance constraints will be active in the final

Link	Link	Link	Link	Link	Link	Link	Link
$2_1^2$	$8_1^2$	$9_{48}^2$	$9_3$	$9_{15}^2$	$9_{18}^2$	$10_{21}$	$10_{23}$
$3_1$	$8_{10}^3$	$8_{10}^2$	$10_{143}$	$9_{31}^2$	$9_{25}^2$	$10_{12}$	$10_{100}$
$4_1^2$	$9_{46}$	$8_{14}^2$	$9_4$	$9_{21}^2$	$9_{24}^2$	$10_{10}$	$10_{25}$
$4_1$	$9_{50}^2$	$8_8^2$	$10_{129}$	$9_{36}^2$	$9_{38}$	$10_{22}$	$10_{102}$
$5_1$	$9_{61}^2$	$8_{14}$	$9_1^2$	$9_{14}^2$	$10_{151}$	$10_7$	$10_{103}$
$5_2$	$9_{42}$	$8_{12}^2$	$10_{134}$	$9_{15}$	$9_{39}$	$10_{47}$	$10_{53}$
$5_1^2$	$9_{47}^2$	$9_{55}^2$	$9_5$	$9_{19}$	$9_{34}^2$	$10_{48}$	$10_{94}$
$6_3^3$	$9_{51}^2$	$9_{46}^2$	$9_4^2$	$9_{26}$	$9_{39}^2$	$10_{50}$	$10_{44}$
$6_1^2$	$8_1$	$10_{140}$	$10_{130}$	$9_6^3$	$9_{37}^2$	$10_{15}$	$10_{99}$
$7_7^2$	$9_{54}^2$	$8_{15}$	$10_{148}$	$9_{24}$	$9_{12}^2$	$10_{16}$	$10_{13}$
$6_2^2$	$8_2^2$	$9_{49}$	$10_{152}$	$9_8^2$	$9_{40}^2$	$10_{64}$	$10_{90}$
$6_1$	$9_{45}^2$	$8_5^2$	$10_{147}$	$10_{162}$	$9_{11}^3$	$10_{28}$	$10_{91}$
$6_2$	$10_{124}$	$8_{12}$	$9_{35}$	$9_{27}^2$	$9_{11}^2$	$10_{62}$	$10_{58}$
$7_8^2$	$8_3$	$9_{48}$	$9_{13}^2$	$10_{149}$	$9_7^3$	$10_{19}$	$10_{79}$
$6_1^3$	$8_2$	$9_{45}$	$9_{19}^2$	$9_{22}$	$9_{26}^2$	$10_{54}$	$10_{75}$
$6_3$	$8_4$	$9_{17}^3$	$9_2^2$	$9_{22}^2$	$9_{29}^2$	$10_{85}$	$10_{56}$
$6_2^3$	$9_{43}$	$8_{13}^2$	$10_{156}$	$9_{21}$	$9_{33}^2$	$10_{36}$	$10_{66}$
$6_3^2$	$9_{44}$	$9_{58}^2$	$9_6$	$9_8^3$	$10_{164}$	$10_{52}$	$10_{41}$
$8_7^3$	$8_5$	$9_{15}^3$	$10_{137}$	$9_{25}$	$9_{34}$	$10_{35}$	$10_{71}$
$8_{19}$	$9_{44}^2$	$8_7^2$	$9_5^2$	$9_7^2$	$9_{30}^2$	$10_{68}$	$10_{69}$
$7_1$	$9_{57}^2$	$9_{14}^3$	$9_7$	$9_1^3$	$9_3^3$	$10_{74}$	$10_{87}$
$8_{20}$	$9_{13}^3$	$8_{17}$	$10_{146}$	$9_{28}$	$9_{10}^3$	$10_{37}$	$10_{106}$
$7_2$	$8_7$	$10_{161}$	$9_{10}$	$9_{37}$	$9_{12}^3$	$10_{31}$	$10_{80}$
$7_3$	$8_1^3$	$8_6^3$	$10_{159}$	$9_{27}$	$9_4^3$	$10_{49}$	$10_{72}$
$7_1^2$	$9_{59}^2$	$10_{132}$	$9_9$	$9_{29}$	$10_{138}$	$10_{33}$	$10_{70}$
$7_4$	$9_{18}^3$	$8_3^3$	$9_3^2$	$10_{135}$	$10_{163}$	$10_{51}$	$10_{59}$
$8_{15}^2$	$8_9$	$9_{47}$	$9_{14}$	$9_{35}^2$	$9_{38}^2$	$10_{14}$	$10_{29}$
$8_8^3$	$8_6$	$9_{21}^3$	$9_8$	$10_{131}$	$9_{33}$	$10_{38}$	$10_{40}$
$7_2^2$	$8_4^2$	$8_{18}$	$10_{127}$	$9_{23}$	$10_{165}$	$10_{39}$	$10_{114}$
$7_4^2$	$9_{19}^3$	$10_{125}$	$9_{12}$	$9_{28}^2$	$9_{41}^2$	$10_{76}$	$10_{60}$
$7_5$	$8_3^3$	$8_4^3$	$9_6^2$	$9_{41}$	$9_{42}^2$	$10_{30}$	$10_{43}$
$7_3^2$	$8_8$	$9_{16}^3$	$9_{16}$	$9_{16}^2$	$10_1$	$10_{55}$	$10_{97}$
$8_{21}$	$8_{13}$	$8_1^4$	$9_{20}^2$	$9_{32}^2$	$10_3$	$10_{65}$	$10_{89}$
$7_7$	$9_{52}^2$	$9_1$	$9_{11}$	$10_{144}$	$10_2$	$10_{93}$	$10_{45}$
$7_6$	$9_{56}^2$	$10_{142}$	$10_{150}$	$10_{157}$	$10_4$	$10_{63}$	$10_{118}$
$7_1^3$	$10_{139}$	$10_{145}$	$9_{36}$	$9_{30}$	$10_8$	$10_{24}$	$10_{73}$
$9_{49}^2$	$8_{11}$	$9_{20}^3$	$9_{20}$	$9_{32}$	$10_{61}$	$10_{18}$	$10_{117}$
$7_5^2$	$8_2^3$	$10_{128}$	$9_{23}^2$	$10_{154}$	$10_{46}$	$10_{26}$	$10_{96}$
$9_{43}^2$	$8_{10}$	$10_{141}$	$9_5^3$	$9_9^3$	$10_5$	$10_{67}$	$10_{83}$
$8_3^4$	$8_{11}^2$	$10_{133}$	$9_{13}$	$9_{18}$	$10_6$	$10_{108}$	$10_{88}$
$7_6^2$	$8_6^2$	$10_{126}$	$9_9^2$	$9_1^4$	$10_9$	$10_{78}$	$10_{112}$
$8_9^3$	$8_9^2$	$10_{136}$	$9_{17}^2$	$10_{158}$	$10_{20}$	$10_{77}$	$10_{57}$
$8_{16}^2$	$8_5^3$	$10_{155}$	$9_{10}^2$	$9_{40}$	$10_{11}$	$10_{32}$	$10_{92}$
$8_2^4$	$8_{16}$	$9_2$	$9_{17}$	$9_{31}$	$10_{34}$	$10_{82}$	$10_{110}$
$9_{53}^2$	$9_{60}^2$	$10_{160}$	$10_{153}$	$9_3^2$	$10_{17}$	$10_{86}$	$10_{111}$
$8_1^2$	$9_{48}^2$	$9_3$	$9_{15}^2$	$9_{18}^2$	$10_{21}$	$10_{23}$	$10_{84}$

TABLE 6. Part 1 of knot and link types sorted by ropelength.

Link	Link	Link	Link	Link	Link	Link
10 <sub>84</sub>	10 <sub>107</sub>	10 <sub>27</sub>	10 <sub>95</sub>	10 <sub>120</sub>	10 <sub>115</sub>	10 <sub>123</sub>
10 <sub>98</sub>	10 <sub>105</sub>	10 <sub>42</sub>	10 <sub>81</sub>	10 <sub>113</sub>	10 <sub>109</sub>	—
10 <sub>101</sub>	10 <sub>122</sub>	10 <sub>121</sub>	10 <sub>119</sub>	10 <sub>116</sub>	10 <sub>104</sub>	—
10 <sub>107</sub>	10 <sub>27</sub>	10 <sub>95</sub>	10 <sub>120</sub>	10 <sub>115</sub>	10 <sub>123</sub>	—

TABLE 7. Part 2 of knot and link types sorted by ropelength.

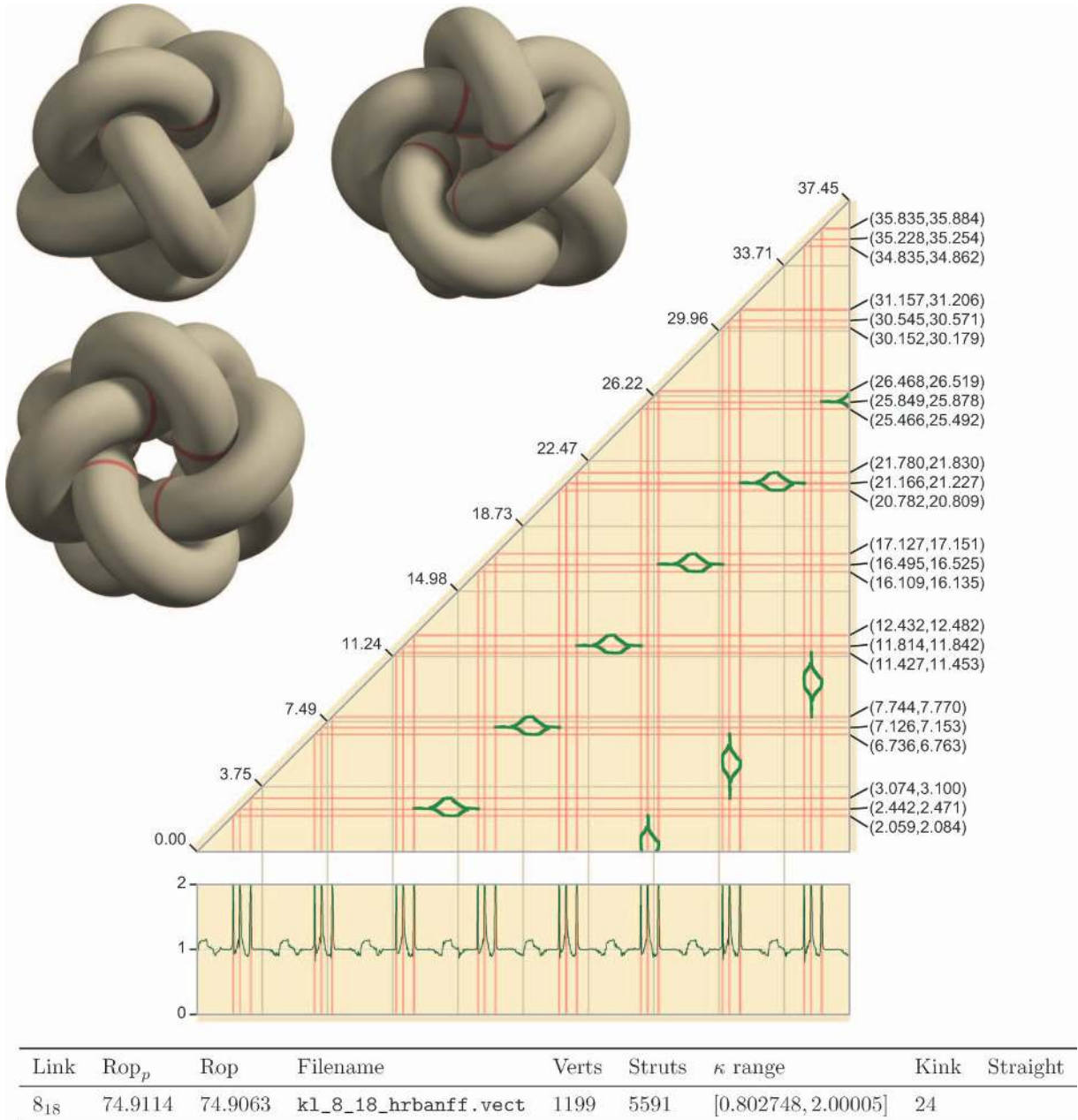


FIGURE 15. This reproduction of the entry for 8<sub>18</sub> in the *Atlas of Tight Knots and Links* shows that the strut and kink sets for this knot are highly symmetric. The *Atlas* provides similar information for all our computed tight knots and links. (Figure is available in color online)

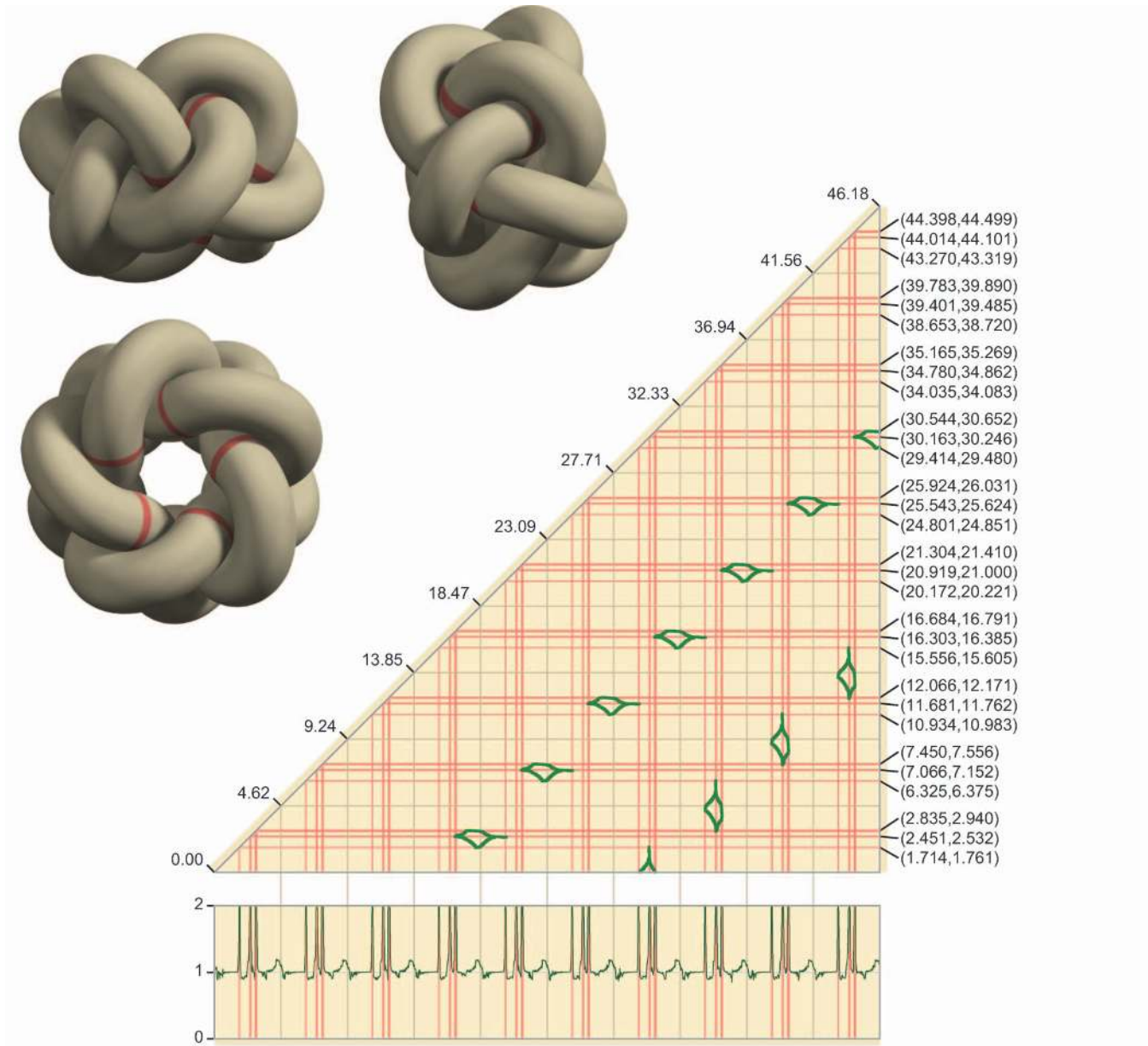
Link	Residual	Link	Residual	Link	Residual	Link	Residual
$2_1^2$	$2.45124e - 05$	$8_2$	0.000982684	$8_8^3$	0.00100655	$9_{38}$	0.000978978
$3_1$	0.00621792	$8_3$	0.00100028	$8_9^3$	0.000980533	$9_{39}$	0.000999482
$4_1$	0.000996335	$8_4$	0.00100103	$8_{10}^3$	0.0074908	$9_{40}$	0.000999343
$4_1^2$	0.000999549	$8_5$	0.00100033	$8_1^4$	0.00100006	$9_{41}$	0.00899161
$5_1$	0.00981995	$8_6$	0.000999848	$8_2^4$	0.000999682	$9_{42}$	0.000999996
$5_2$	0.00994775	$8_7$	0.00101551	$8_3^4$	0.780186	$9_{43}$	0.00898749
$5_1^2$	0.00998078	$8_8$	0.000981272	$9_1$	0.00802077	$9_{44}$	0.000999789
$6_1$	0.000999592	$8_9$	0.000999932	$9_2$	0.00997484	$9_{45}$	0.0099754
$6_2$	0.00897204	$8_{10}$	0.000978418	$9_3$	0.00998254	$9_{46}$	0.00099973
$6_3$	0.000979541	$8_{11}$	0.000979921	$9_4$	$8.64059e - 05$	$9_{47}$	0.000998991
$6_1^2$	0.000999952	$8_{12}$	0.00998976	$9_5$	0.00999417	$9_{48}$	0.00998933
$6_2^2$	0.000999833	$8_{13}$	0.000993117	$9_6$	0.000980197	$9_{49}$	0.00099957
$6_3^2$	0.00999004	$8_{14}$	0.000981486	$9_7$	0.000979897	$9_1^2$	0.00107787
$6_1^3$	0.00998537	$8_{15}$	0.0099948	$9_8$	0.00101007	$9_2^2$	0.00100115
$6_2^3$	0.000705159	$8_{16}$	0.000981316	$9_9$	0.000999938	$9_3^2$	0.00100055
$6_3^3$	0.00627026	$8_{17}$	0.00999085	$9_{10}$	0.00113523	$9_4^2$	0.00099991
$7_1$	0.00105833	$8_{18}$	0.000900015	$9_{11}$	0.000981742	$9_5^2$	0.00100118
$7_2$	0.00998149	$8_{19}$	0.000998339	$9_{12}$	0.000981742	$9_6^2$	0.00126944
$7_3$	0.00999358	$8_{20}$	0.00099998	$9_{13}$	0.000979842	$9_7^2$	0.00104121
$7_4$	0.00100877	$8_{21}$	0.000999988	$9_{14}$	0.00999582	$9_8^2$	0.00100133
$7_5$	0.000999532	$8_1^2$	0.00100142	$9_{15}$	0.000984327	$9_9^2$	0.000999724
$7_6$	0.000979869	$8_2^2$	0.000979836	$9_{16}$	0.000979831	$9_{10}^2$	0.00140283
$7_7$	0.00100393	$8_3^2$	0.000999961	$9_{17}$	0.000999818	$9_{11}^2$	0.000999221
$7_1^2$	0.000999487	$8_4^2$	0.00216462	$9_{18}$	0.00100032	$9_{12}^2$	0.00100137
$7_2^2$	0.00101952	$8_5^2$	0.00999516	$9_{19}$	0.00992217	$9_{13}^2$	0.00100112
$7_3^2$	0.000999871	$8_6^2$	0.00100295	$9_{20}$	0.000981217	$9_{14}^2$	0.000999788
$7_4^2$	0.00099954	$8_7^2$	0.000999802	$9_{21}$	0.00100005	$9_{15}^2$	0.000999236
$7_5^2$	0.000999894	$8_8^2$	0.000999762	$9_{22}$	0.0010001	$9_{16}^2$	0.00605
$7_6^2$	0.00100556	$8_9^2$	0.000979774	$9_{23}$	0.000998846	$9_{17}^2$	0.00899775
$7_7^2$	0.00320787	$8_{10}^2$	0.000999858	$9_{24}$	0.000979562	$9_{18}^2$	0.000999648
$7_8^2$	0.0018494	$8_{11}^2$	0.00997927	$9_{25}$	0.000999907	$9_{19}^2$	0.00100405
$7_1^3$	0.000999748	$8_{12}^2$	0.000999968	$9_{26}$	0.000977105	$9_{20}^2$	0.000999853
$8_1$	0.00898769	$8_{13}^2$	0.0010008	$9_{27}$	0.00100048	$9_{21}^2$	0.00898977
$8_2$	0.000982684	$8_{14}^2$	0.00101123	$9_{28}$	0.00999324	$9_{22}^2$	0.00943088
		$8_{15}^2$	0.00099994	$9_{29}$	0.00996501	$9_{23}^2$	0.000998181
		$8_{16}^2$	0.000997563	$9_{30}$	0.000979844	$9_{24}^2$	0.000999946
		$8_1^3$	0.00100589	$9_{31}$	0.000979942	$9_{25}^2$	0.0009999
		$8_2^3$	0.000999904	$9_{32}$	0.000979062	$9_{26}^2$	0.00100243
		$8_3^3$	0.00100014	$9_{33}$	0.000997746	$9_{27}^2$	0.00099997
		$8_4^3$	0.00999606	$9_{34}$	0.00100114	$9_{28}^2$	0.000998883
		$8_5^3$	0.000995844	$9_{35}$	0.000999697	$9_{29}^2$	0.00100157
		$8_6^3$	0.00099824	$9_{36}$	0.000981383	$9_{30}^2$	0.00099989
		$8_7^3$	0.00119532	$9_{37}$	0.000978472	$9_{31}^2$	0.000999523
		$8_8^3$	0.00100655	$9_{38}$	0.00999228	$9_{32}^2$	0.00100012
					0.000978978	$9_{33}^2$	0.000999711

TABLE 8. Part 1 of residuals of tight knots and links by knot type.

Link	Residual	Link	Residual	Link	Residual	Link	Residual
$9_{33}^2$	0.000999711	$9_{16}^3$	0.000999575	$10_{37}$	0.000999835	$10_{82}$	0.000978946
$9_{34}^2$	0.00100169	$9_{17}^3$	0.00749982	$10_{38}$	0.000979821	$10_{83}$	0.00999433
$9_{35}^2$	0.000999778	$9_{18}^3$	0.000999841	$10_{39}$	0.000986038	$10_{84}$	0.0099812
$9_{36}^2$	0.00100172	$9_{19}^3$	0.00101035	$10_{40}$	0.00100863	$10_{85}$	0.000981325
$9_{37}^2$	0.000999058	$9_{20}^3$	0.00100002	$10_{41}$	0.00999693	$10_{86}$	0.000978499
$9_{38}^2$	0.000999748	$9_{21}^3$	0.00100039	$10_{42}$	0.000999751	$10_{87}$	0.000979621
$9_{39}^2$	0.000999888			$10_{43}$	0.000980157	$10_{88}$	0.000979845
$9_{40}^2$	0.000999835	$9_1^4$	0.000979958	$10_{44}$	0.00322255	$10_{89}$	0.0010019
$9_{41}^2$	0.00100037			$10_{45}$	0.000982692	$10_{90}$	0.000980234
$9_{42}^2$	0.000998679	$10_1$	0.00101691	$10_{46}$	0.00997656	$10_{91}$	0.000977397
$9_{43}^2$	0.00100109	$10_2$	0.00100023	$10_{47}$	0.000980999	$10_{92}$	0.00100005
$9_{44}^2$	0.00100838	$10_3$	0.000991435	$10_{48}$	0.00999602	$10_{93}$	0.000979652
$9_{45}^2$	0.00997492	$10_4$	0.00100846	$10_{49}$	0.000998073	$10_{94}$	0.00097991
$9_{46}^2$	0.00100042	$10_5$	0.00100194	$10_{50}$	0.000981787	$10_{95}$	0.000979668
$9_{47}^2$	0.00999831	$10_6$	0.000979506	$10_{51}$	0.00098231	$10_{96}$	0.00018365
$9_{48}^2$	0.000999984	$10_7$	0.0097283	$10_{52}$	0.000999419	$10_{97}$	0.000999872
$9_{49}^2$	0.000999984	$10_8$	0.000980356	$10_{53}$	0.00101025	$10_{98}$	0.00999481
$9_{50}^2$	0.000999226	$10_9$	0.000979784	$10_{54}$	0.00999263	$10_{99}$	0.0099926
$9_{51}^2$	0.000999443	$10_{10}$	0.00999688	$10_{55}$	0.00998728	$10_{100}$	0.00101003
$9_{52}^2$	0.000999958	$10_{11}$	0.00760935	$10_{56}$	0.00999185	$10_{101}$	0.00999705
$9_{53}^2$	0.00996962	$10_{12}$	0.000991292	$10_{57}$	0.000999798	$10_{102}$	0.000979674
$9_{54}^2$	0.000999703	$10_{13}$	0.000999947	$10_{58}$	0.000999966	$10_{103}$	0.00999479
$9_{55}^2$	0.00100064	$10_{14}$	0.0010261	$10_{59}$	0.00995441	$10_{104}$	0.00999683
$9_{56}^2$	0.000979788	$10_{15}$	0.000979185	$10_{60}$	0.000980266	$10_{105}$	0.000979902
$9_{57}^2$	0.00255237	$10_{16}$	0.000985699	$10_{61}$	0.00787098	$10_{106}$	0.000979055
$9_{58}^2$	0.000999155	$10_{17}$	0.00998848	$10_{62}$	0.00105699	$10_{107}$	0.000980096
$9_{59}^2$	0.00108631	$10_{18}$	0.000979621	$10_{63}$	0.00998227	$10_{108}$	0.00127554
$9_{60}^2$	0.000999312	$10_{19}$	0.00098045	$10_{64}$	0.00997603	$10_{109}$	0.000979798
$9_{61}^2$	0.00100091	$10_{20}$	0.000979959	$10_{65}$	0.00135295	$10_{110}$	0.000979638
		$10_{21}$	0.000999057	$10_{66}$	0.000999872	$10_{111}$	0.000979851
$9_1^3$	0.000999763	$10_{22}$	0.000991413	$10_{67}$	0.000979823	$10_{112}$	0.00104599
$9_2^3$	0.000999746	$10_{23}$	0.00999682	$10_{68}$	0.00100695	$10_{113}$	0.00999934
$9_3^3$	0.00100525	$10_{24}$	0.00166886	$10_{69}$	0.000999786	$10_{114}$	0.00100087
$9_4^3$	0.000999641	$10_{25}$	0.000994731	$10_{70}$	0.000980057	$10_{115}$	0.000978725
$9_5^3$	0.00100042	$10_{26}$	0.00098015	$10_{71}$	0.00999226	$10_{116}$	0.00998661
$9_6^3$	0.000999746	$10_{27}$	0.000999869	$10_{72}$	0.000999942	$10_{117}$	0.00998396
$9_7^3$	0.000999935	$10_{28}$	0.00996703	$10_{73}$	0.00998888	$10_{118}$	0.000999987
$9_8^3$	0.000999751	$10_{29}$	0.00116525	$10_{74}$	0.000978382	$10_{119}$	0.000999834
$9_9^3$	0.000996684	$10_{30}$	0.000999376	$10_{75}$	0.000981812	$10_{120}$	0.00100037
$9_{10}^3$	0.00099985	$10_{31}$	0.000979897	$10_{76}$	0.000980892	$10_{121}$	0.00099989
$9_{11}^3$	0.0010755	$10_{32}$	0.000979993	$10_{77}$	0.00999768	$10_{122}$	0.000999203
$9_{12}^3$	0.00100439	$10_{33}$	0.000979857	$10_{78}$	0.000981017	$10_{123}$	0.0016528
$9_{13}^3$	0.00749431	$10_{34}$	0.00098555	$10_{79}$	0.0010001	$10_{124}$	0.00100133
$9_{14}^3$	0.00900147	$10_{35}$	0.000982115	$10_{80}$	0.000979926	$10_{125}$	0.00998345
$9_{15}^3$	0.00112426	$10_{36}$	0.000979692	$10_{81}$	0.000981576	$10_{126}$	0.00999723
$9_{16}^3$	0.000999575	$10_{37}$	0.000999835	$10_{82}$	0.000978946	$10_{127}$	0.00998882

TABLE 9. Part 2 of residuals of tight knots and links by knot type.





Link	Rop <sub>p</sub>	Rop	Filename	Verts	Struts	$\kappa$ range	Kink	Straight
10 <sub>123</sub>	92.3646	92.3565	k1_10_123_handcrafted.vect	1498	7189	[0.84917, 2.00008]	30	

**FIGURE 16.** This reproduction of the entry for 10<sub>123</sub> in the *Atlas of Tight Knots and Links* shows that it has a similar structure to 8<sub>18</sub>. We do not believe that the repeated structures are the same (note, for instance, the different spacing of the kinked regions). (Figure is available in color online)

configuration, we can ignore constraints that we expect to be inactive, resulting in a reduced constraint set of size  $O(n)$ . Our approximately minimized polygons provide exactly this information. For this reason we imagine an important use of our data will be in formulating input problems for a future SQP-based knot-minimizer. Our polygons are already serving as input for the biarc-based annealer of [Carlen et al. 05].

While our data set is detailed and suggestive, solving explicitly for the structure of ropelength-minimizing (smooth) knots and links is likely to require even better data. It is shown in [Cantarella et al. 11] that a critical shape for the simple clasp formed when ropes pass over one another at right angles contains tiny straight segments of length a few thousandths of the total length of the curves. Resolving these features will require

Link	Residual	Link	Residual	Link	Residual	Link	Residual
10 <sub>127</sub>	0.00998882	10 <sub>137</sub>	0.000979856	10 <sub>147</sub>	0.000999813	10 <sub>157</sub>	0.000979535
10 <sub>128</sub>	0.000988223	10 <sub>138</sub>	0.00899453	10 <sub>148</sub>	0.000981385	10 <sub>158</sub>	0.000980822
10 <sub>129</sub>	0.00902523	10 <sub>139</sub>	0.000979731	10 <sub>149</sub>	0.00100026	10 <sub>159</sub>	0.000979791
10 <sub>130</sub>	0.000999987	10 <sub>140</sub>	0.0099924	10 <sub>150</sub>	0.000979903	10 <sub>160</sub>	0.00998455
10 <sub>131</sub>	0.00959976	10 <sub>141</sub>	0.00100144	10 <sub>151</sub>	0.000979813	10 <sub>161</sub>	0.00899311
10 <sub>132</sub>	0.000980876	10 <sub>142</sub>	0.000980204	10 <sub>152</sub>	0.00999625	10 <sub>162</sub>	0.000985909
10 <sub>133</sub>	0.000980018	10 <sub>143</sub>	0.00993363	10 <sub>153</sub>	0.0091785	10 <sub>163</sub>	0.00899697
10 <sub>134</sub>	0.00999485	10 <sub>144</sub>	0.00995796	10 <sub>154</sub>	0.00115132	10 <sub>164</sub>	0.000979519
10 <sub>135</sub>	0.00100006	10 <sub>145</sub>	0.00102699	10 <sub>155</sub>	0.00998753	10 <sub>165</sub>	0.000979783
10 <sub>136</sub>	0.00999149	10 <sub>146</sub>	0.00998505	10 <sub>156</sub>	0.0009799		
10 <sub>137</sub>	0.000979856	10 <sub>147</sub>	0.000999813	10 <sub>157</sub>	0.000979535		

TABLE 10. Part 3 of residuals of tight knots and links by knot type.

converged runs for polygonal-rope-length minimizers with tens of thousands of vertices, an ambitious goal that will keep this area of experimental mathematics active for some time to come.

## 7. APPENDIX: ROPELENGTH DATA

We present three sets of tables of ropelength data. The first set, Tables 3–5, show the polygonal ropelength ( $\text{Rop}_p$ ) and ropelength upper bounds ( $\text{Rop}$ ) that we have obtained for each of the knot types that we have considered. The knots and links are organized according to their position in Rolfsen’s table, with the link  $X_z^y$  being the  $z$ th example of a prime  $X$ -crossing link of  $y$  components in the table. We have identified the two “Perko pair” knots 10<sub>161</sub> and 10<sub>162</sub> and renumbered the subsequent knots accordingly, so there are only 165 ten-crossing knots in our results.

The second set, Tables 6 and 7, show the same knot and link types ordered by ropelength upper bound. These tables are to be read down each column from the top left to the bottom right. We can see that this order is quite different from the one in Rolfsen’s table with (for instance) the 2-component link  $7_7^2$  occurring before any 6- or 7-crossing knot and the 10<sub>124</sub> knot occurring before many 8- and 9-crossing links.

The third set of tables, Tables 8–10, give the residual of each of our computed configurations. The low residuals show that they are close to critical in the sense of Theorem 2.18. We include these data as a measure of the relative quality of each of our minimized configurations.

Figures 15 and 16 are reproductions of the pages from the *Atlas of Tight Knots* for the approximately tight 8<sub>18</sub> and 10<sub>123</sub> knots. On the top left of each page are three views of the tight configurations, with kinked regions highlighted in red. On the top right is a plot of the self-contact map of the configuration. Each of these plots consists of a triangular region with the hypotenuse labeled with arc-length values on the knot. A box is plotted at  $(s, t)$  on the plot if there is a strut connecting  $L(s)$  and  $L(t)$ . Below the graph appears a plot of  $1/\text{MinRad}(v_i)$  for the polygon (to the same scale). Kinked regions of maximum curvature are highlighted on the graph. Each such region has a key on the right-hand side of the plot showing the arc-length positions of the start and end of the kink (in order to give a sense of the relative scale of the kinked region). At the bottom of the page is a line of data giving the polygonal ropelength  $\text{Rop}_p$  (as measured by `octrope`), ropelength upper bound  $\text{Rop}$  (from `roundout_rl`), filename, number of vertices and struts, maximum and minimum curvature values, and number of kinked regions. The last entry shows the total arc length of straight regions in the curves (0 for these two knots, but nonzero for many knots and links in the *Atlas*).

## 8. ACKNOWLEDGMENTS

The authors would like to mention the hard work of Sivan Toledo, whose TAUCS library made `tlsqr` and `tsnnls` possible. Our code was made much faster by Toledo’s carefully written supernodal multifrontal Cholesky factorization code. We are similarly indebted to Portugal,

Judice, and Vicente for developing the block principal pivoting algorithm. Many colleagues provided helpful conversations and insights about these and similar problems, including Joe Fu, Rob Kusner, John Sullivan, Piotr Pierański, John Maddocks, and Andrzej Stasiak. The authors would also like to acknowledge the support of the National Science Foundation through the University of Georgia VIGRE grant (DMS-00-89927), DMS-02-04826 (to Cantarella and Fu), and DMS-08-10415 (to Rawdon).

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Ted Ashton, Linthicum Heights, MD 21090 (ashted@ashtonfam.org)

Jason Cantarella, Department of Mathematics, University of Georgia, Athens, GA 30602 (cantarel@math.uga.edu)

Michael Piatek, Department of Computer Science, University of Washington, Seattle, WA 98195 (piatek@cs.washington.edu)

Eric J. Rawdon, Department of Mathematics, University of St. Thomas, St. Paul, MN (ejrawdon@stthomas.edu)

Received February 5, 2010; accepted April 19, 2010.