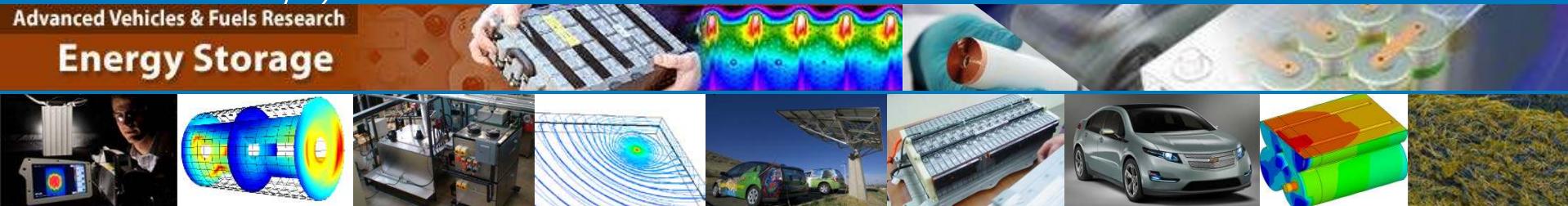


Life Prediction Model for Grid-Connected Li-ion Battery Energy Storage System

Advanced Vehicles & Fuels Research
Energy Storage



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NREL/ PR-5400-68759

Applications of Energy Storage (ES) on the Grid

Focus of present ES system life study

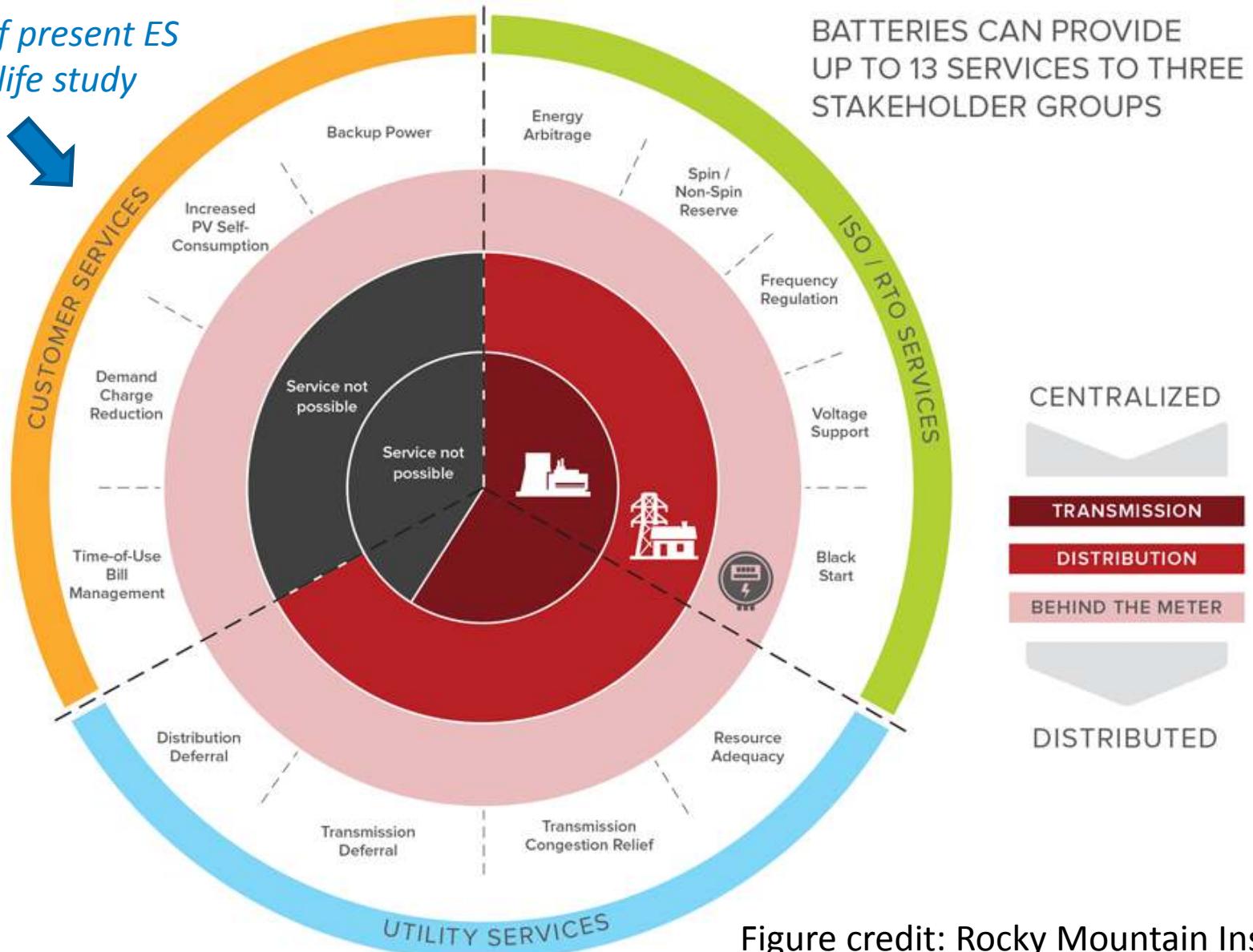


Figure credit: Rocky Mountain Institute

Example Application: Behind-the-meter ES enables PV use in locations such as Hawaii (where power export is prohibited)

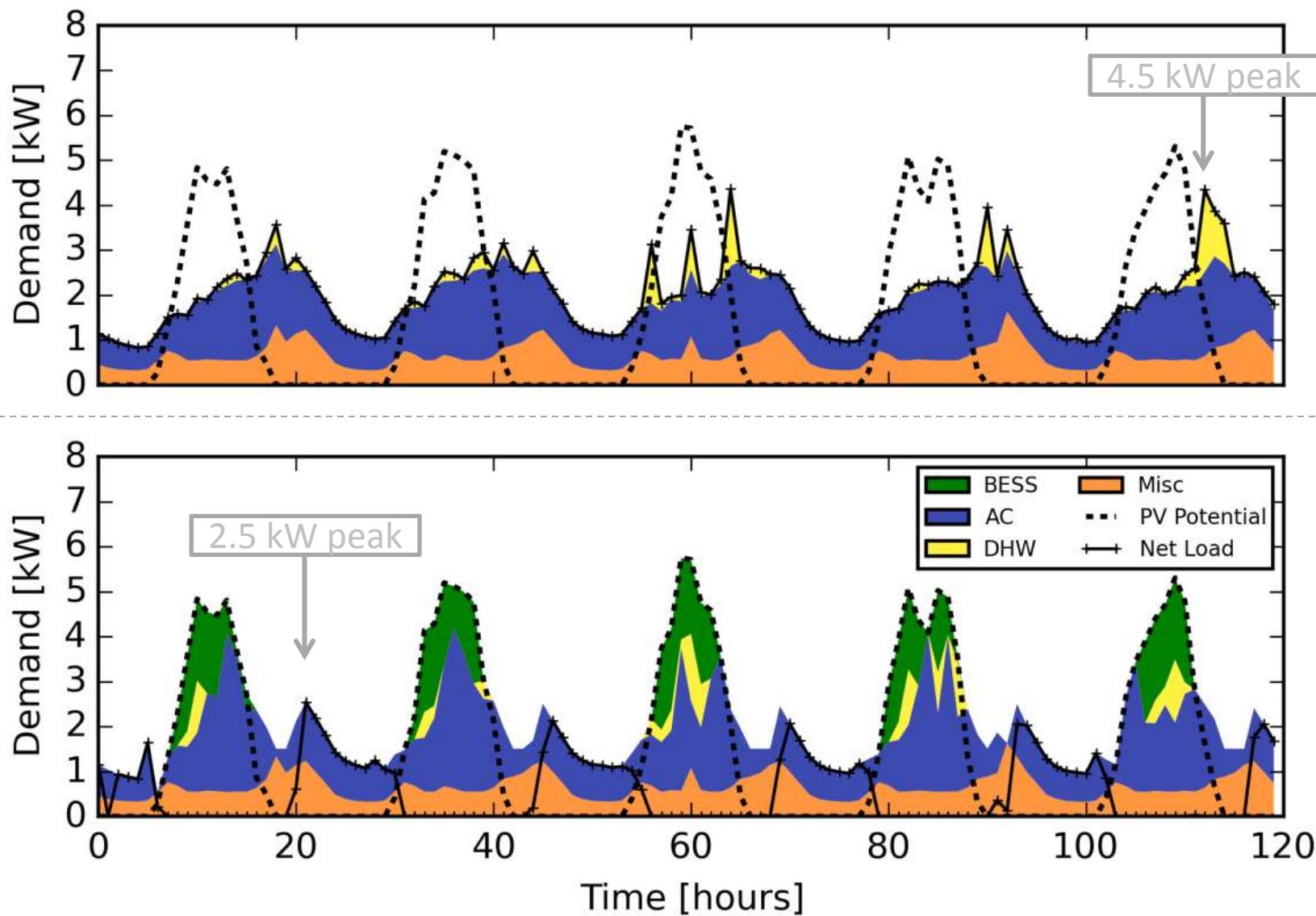


Figure: "Solar Plus: An Holistic Approach to Distributed Solar PV" Eric O'Shaughnessy, Kristen Ardani, Dylan Cutler, Robert Margolis (NREL Pub #68371)

Outline

- Degradation mechanisms
- Modeling approach
- Aging tests
- Model and parameter identification
- Example life prediction

Li-ion Working Principles

Neg. Electrode

Graphite

Hard carbon

Silicon

Titanate

Li metal

Pos. Electrode

LiXO_2 ,

$\text{X} = \text{NiMnCo}$

Co

NiCoAl

LiMn_2O_4 ,

LiFePO_4

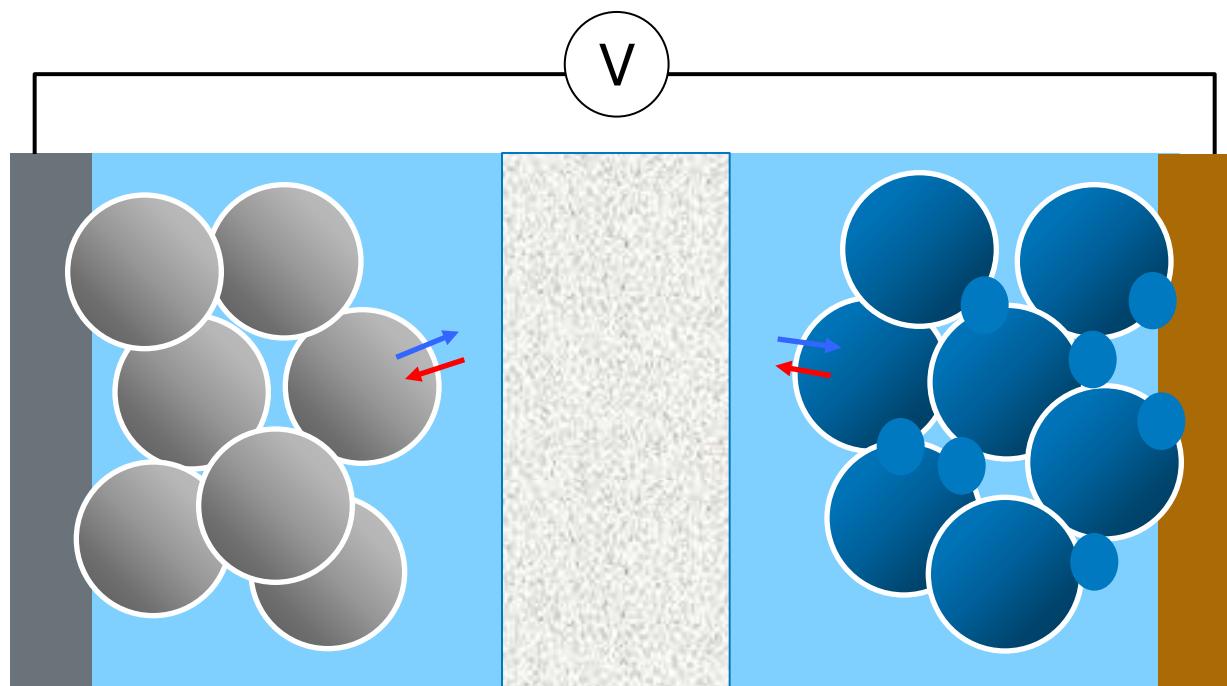
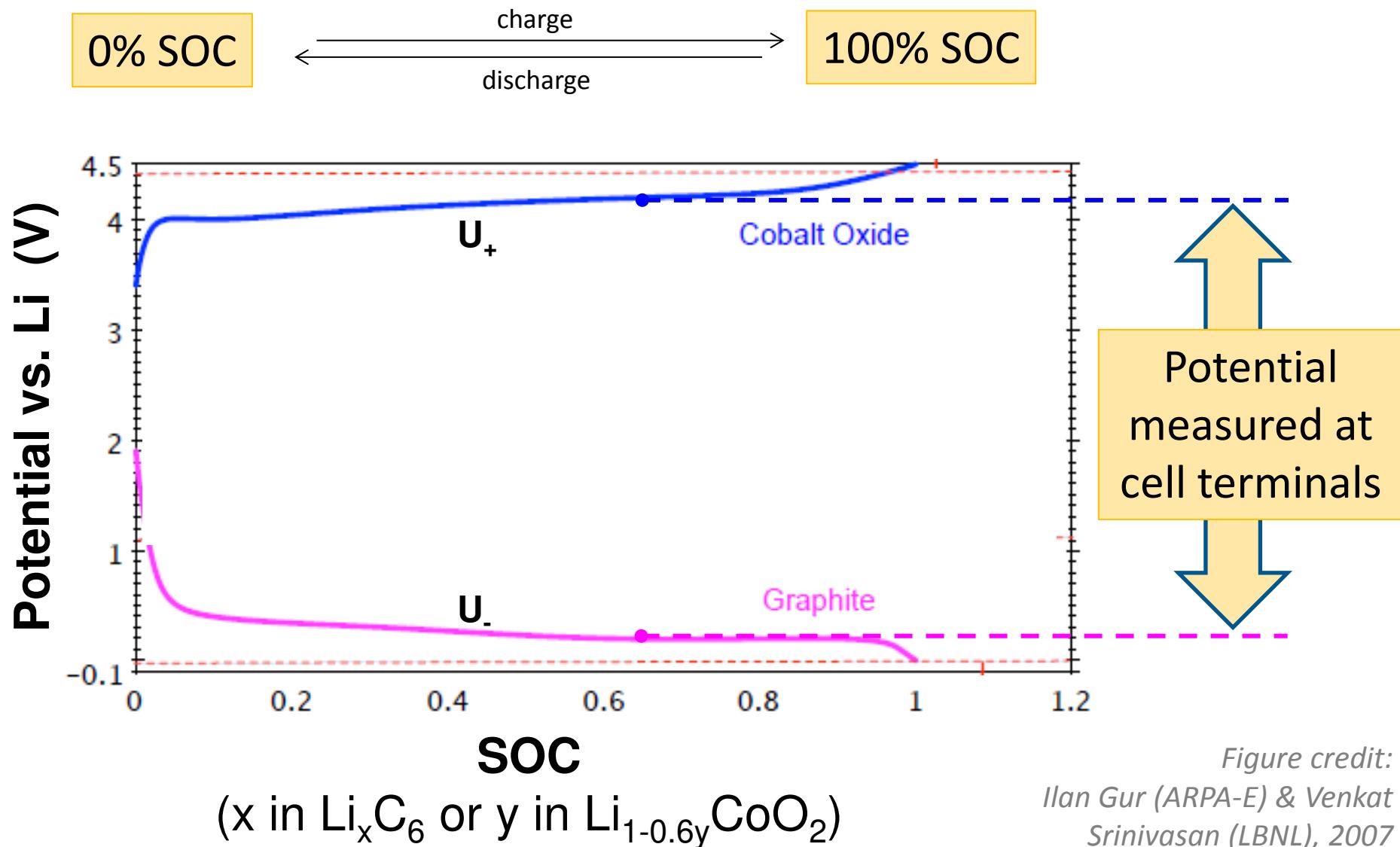


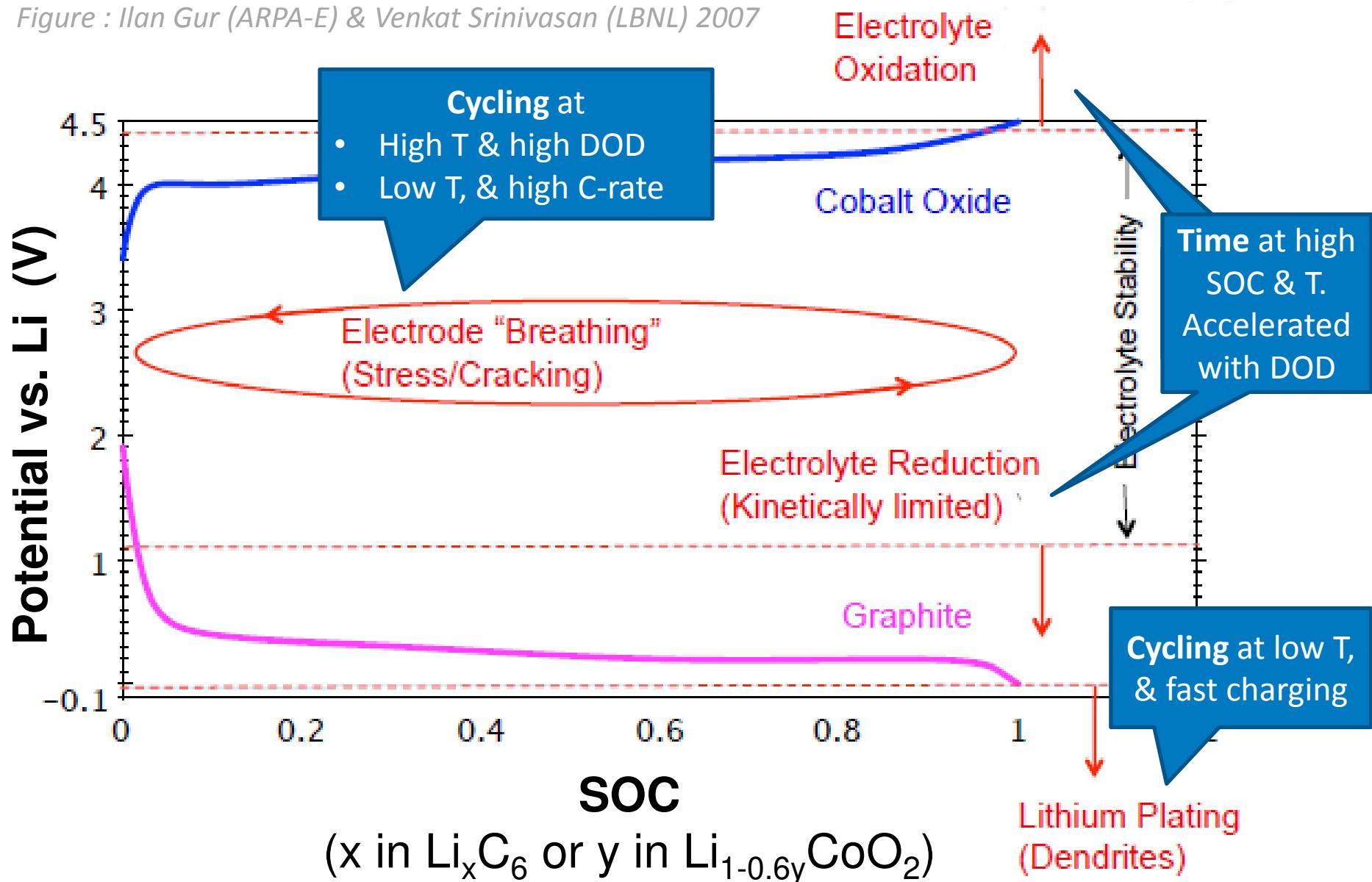
Figure credit: Gi-Heon Kim

Electrochemical Operating Window



Electrochemical Window – Degradation

Figure : Ilan Gur (ARPA-E) & Venkat Srinivasan (LBNL) 2007



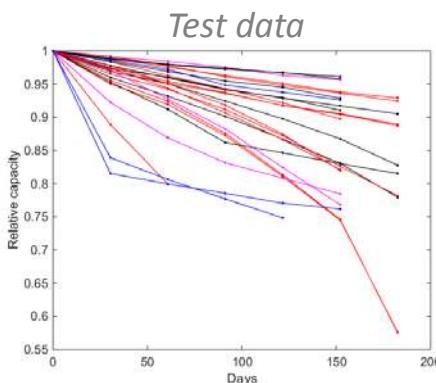
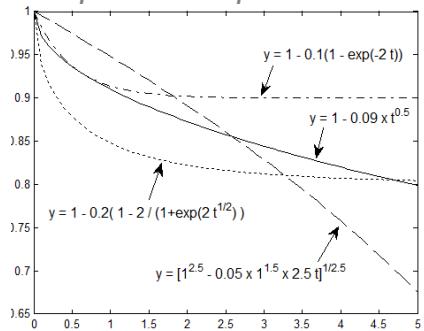
NREL Battery Life Predictive Model Framework

Reduced-order models for physical fade mechanisms, e.g.

- SEI growth & damage
- Particle fracture
- Electrode isolation
- Electrolyte decomposition
- Gas generation, delamination
- Li plating

Semi-automated software aids model equation selection and parameter identification

Equations + parameters



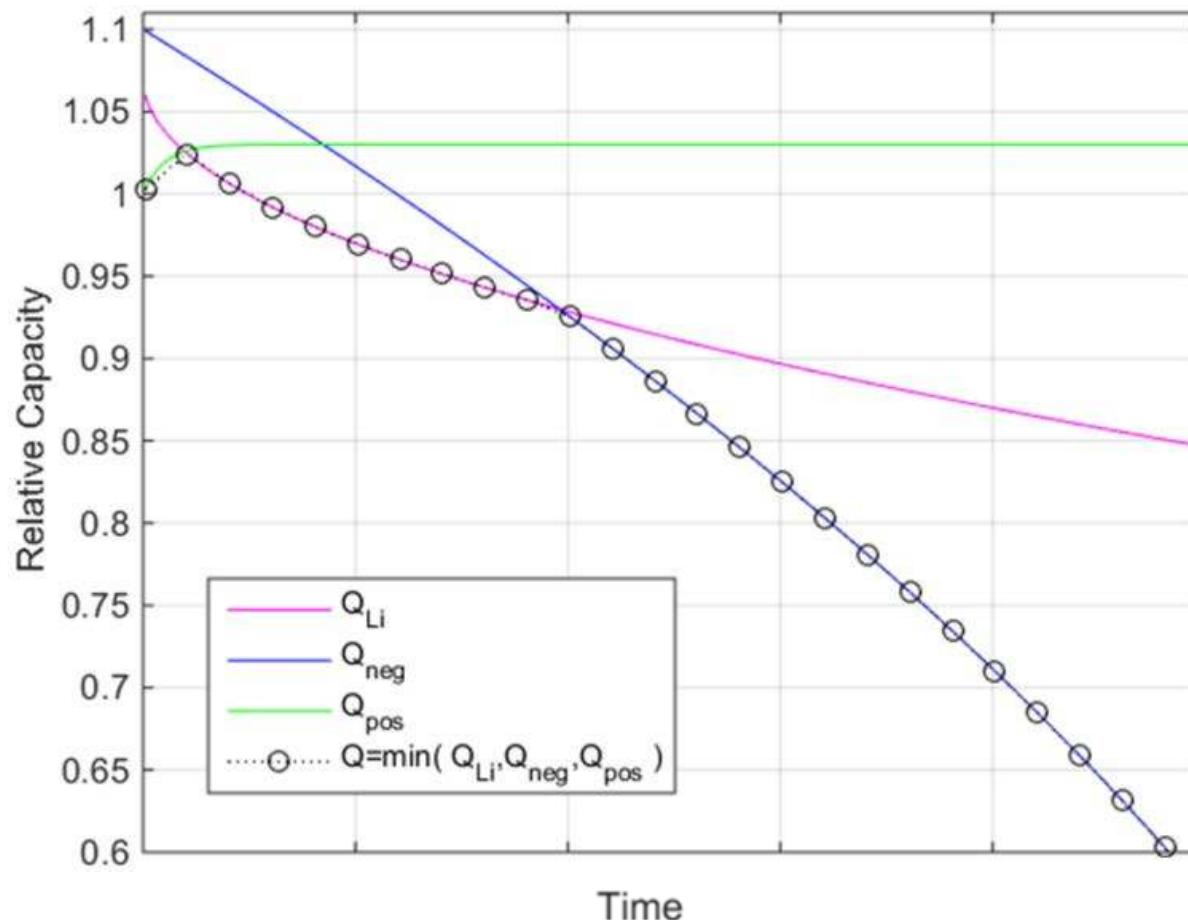
Mechanism	Trajectory equation	State equation	Parameters
Diffusion-controlled reaction	$x(t) = kt^{1/2}$	$\dot{x}(t) = \frac{k}{2} \left(\frac{k}{x(t)} \right)$	k – rate ($p=1/2$)
Kinetic-controlled reaction	$x(t) = kt$	$\dot{x}(t) = k$	k – rate ($p=1$)
Mixed diffusion/kinetic	$x(t) = kt^p$	$\dot{x}(t) = kp \left(\frac{k}{x(t)} \right)^{\frac{1-p}{p}}$	k – rate p – order, $0.3 < p < 1$
Diffusion controlled reaction with mechanical damage	See Appendix A	$\dot{N} = \frac{dN}{dt} = k_D \cdot (\sqrt{D})^p$ $\dot{x}_0(t) = \frac{k}{2} \left(\frac{k}{x(t)} \right)$ $\dot{x}_j(t) = D \frac{k}{2} \left(\frac{k}{x(t)} \right)$	k – rate p – order
Cyclic fade – linear	$x(N) = kN$	$\dot{x}(N) = k$	k – rate ($p=0$)
Cyclic fade – accelerating	$x(N) = [x_0^{1+p} + kx_0^p(1+p)N]^{\frac{1}{1+p}}$	$\dot{x}(N) = k \left(\frac{x_0}{x(N)} \right)^p$	k – rate p – order, $0 \geq p > 3$
Break-in process	$x(t) = M(1 - \exp(-kt))$ or $x(N) = \dots$	$\dot{x}(t) = k(M - x(t))$	M – maximum fade k – rate
Sigmoidal reaction	$x(t) = M \left[1 - \frac{2}{1 + \exp(kt^p)} \right]$ or $x(N) = \dots$	$\dot{x}(t) = \frac{2MkpX(t)\exp(kX(t))}{[1 + \exp(kX(t))]^2}$ $X(t) = \left\{ \frac{1}{k} \ln \left(\frac{2}{1 - x(t)/M} - 1 \right) \right\}^{\frac{1}{p}}$	M – maximum fade k – rate p – order

x, D : state variables
 k, k_D : fade rates
 p : order
 M : maximum extent of fade

S. Santhanagopalan, K. Smith, J. Neubauer, G.-H. Kim, A. Pesaran, M. Keyser, Design and Analysis of Large Lithium-Ion Battery Systems, Artech House, 2015.

Model assumes measured capacity is minimum of:

1. Cycleable lithium, Q_{Li}
2. Negative electrode sites, Q_{neg}
3. Positive electrode sites, Q_{pos}



Aging tests – Kokam 75Ah Gr/NMC Li-ion cells

- **Tests design to include both benign and highly accelerated aging**
 - Some real-world, some reaching 30% capacity fade in 6-9 months
- **Pure storage (0%), partial cycling (50% DC*), & fully accelerated cycling (100% DC)**
 - Separate calendar from cycling fade
- **Capacity check run at test temperature**
 - Simplifies testing but makes model ID more difficult
- **Ideal test matrix would include more aging conditions**

Cycling tests				
Temperature	DOD	Dis./charge rate	Duty-cycle*	# of cells
23°C	80%	1C/1C	100%	2
30°C	100%	1C/1C	100%	1
30°C	80%	1C/1C	50%	1
0°C	80%	1C/0.3C	100%	2
45°C	80%	1C/1C	100%	1

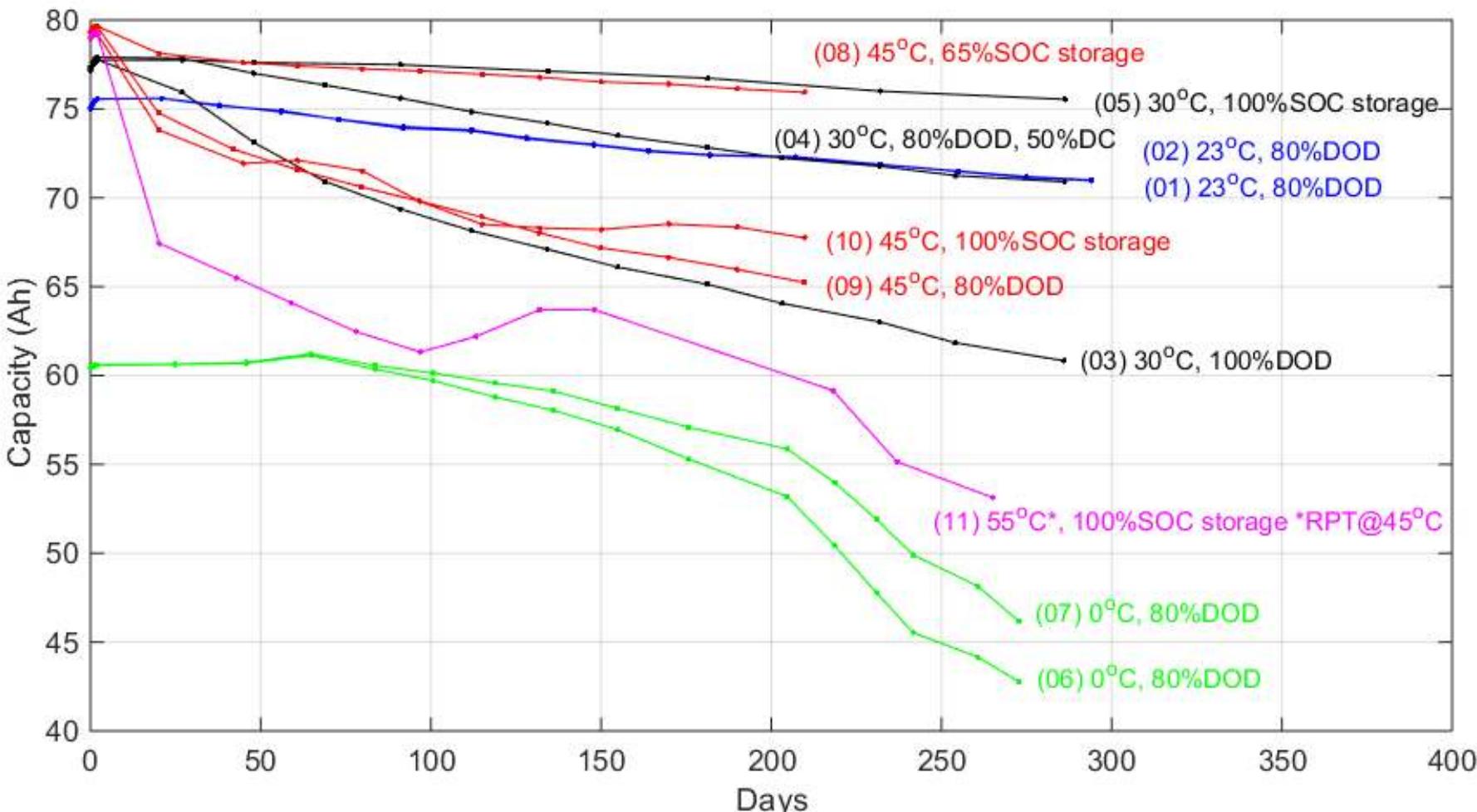
Storage tests		
Temperature	SOC	# of cells
30°C	100%	1
45°C	65%	1
45°C	100%	1
55°C	100%	1

Gr = Graphite negative electrode

NMC = Nickel-Manganese-Cobalt positive electrode

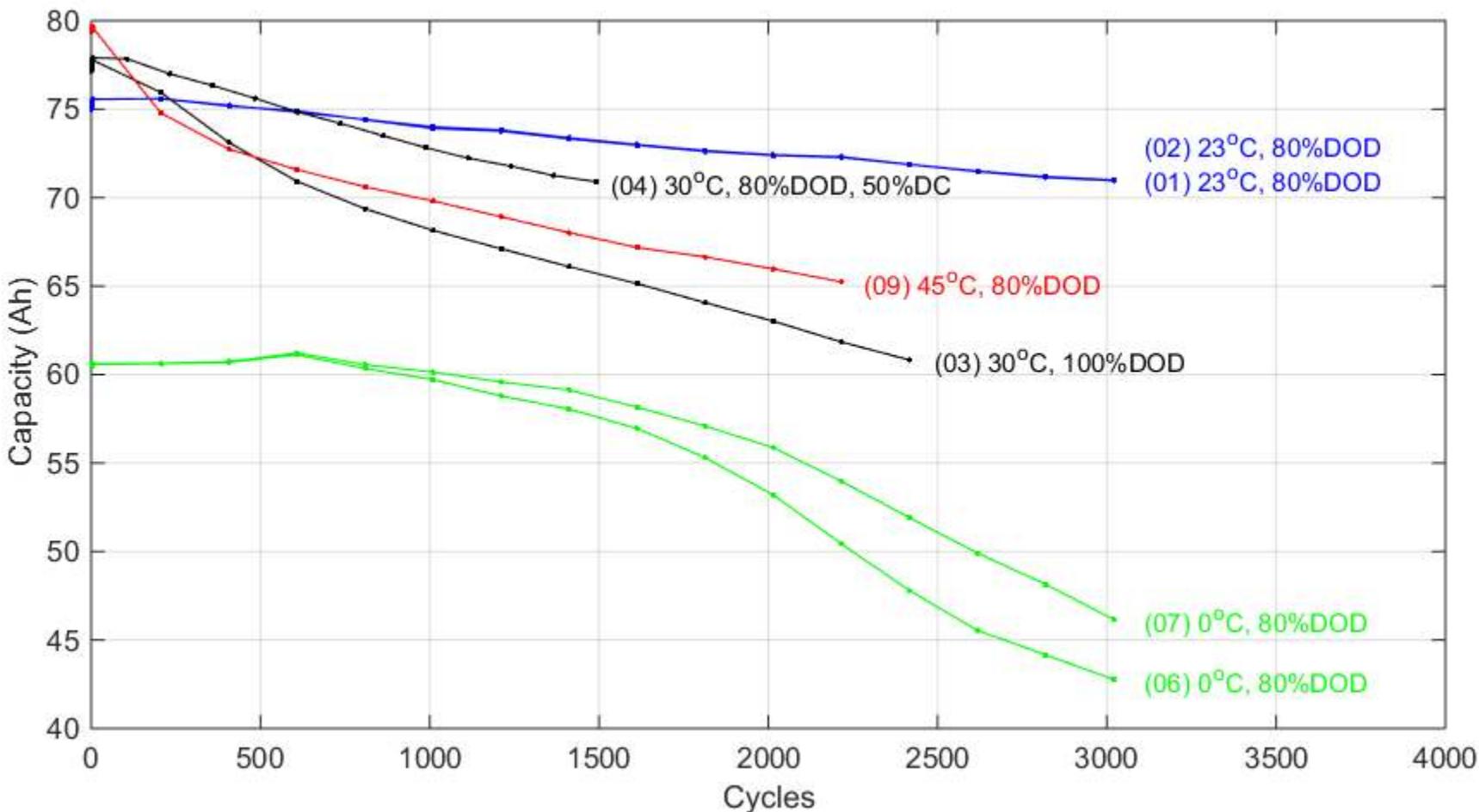
C/5 Capacity vs. Time

- Tight agreement for replicate cells 1&2 at 23°C
- Some divergence for replicate cells 6&7 at 0°C
- Unexplained temporary capacity increase for 55°C storage cell

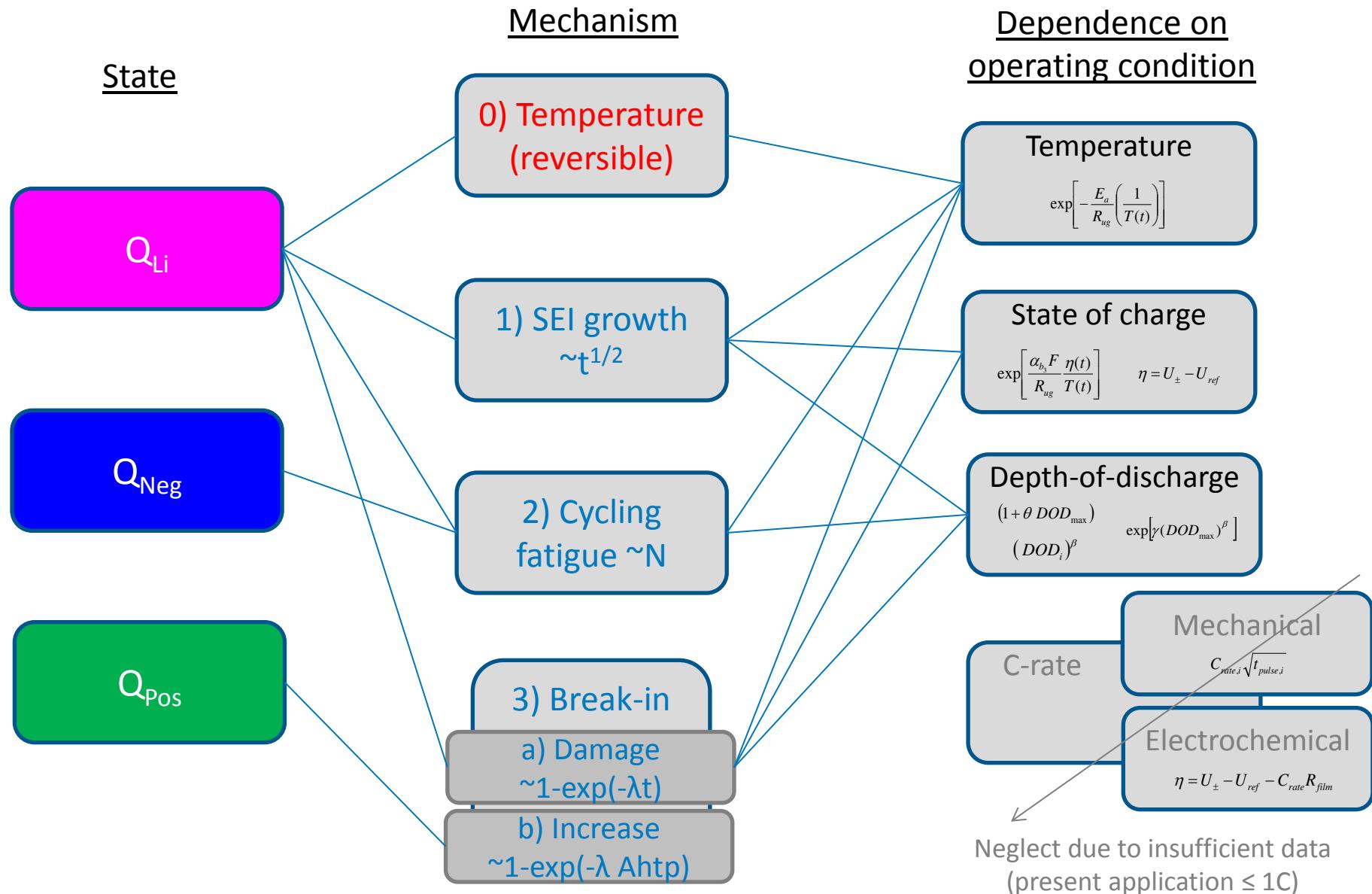


C/5 Capacity vs. Cycles

- Storage data omitted
- Just 6% capacity loss after 3000 cycles at 23°C, 80% DOD



Capacity Evolution–Reversible and Irreversible



Q_{Pos} Capacity Break-in & Initial Temperature Dependence

- Hypothesize initial cycles induce microcracks in NMC particles, increasing electrolyte wetting and surface area

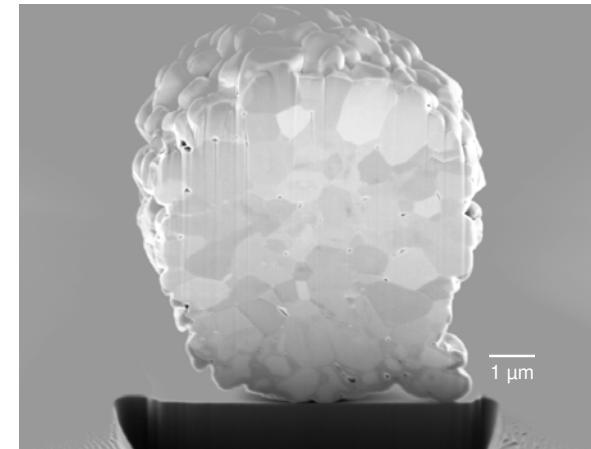
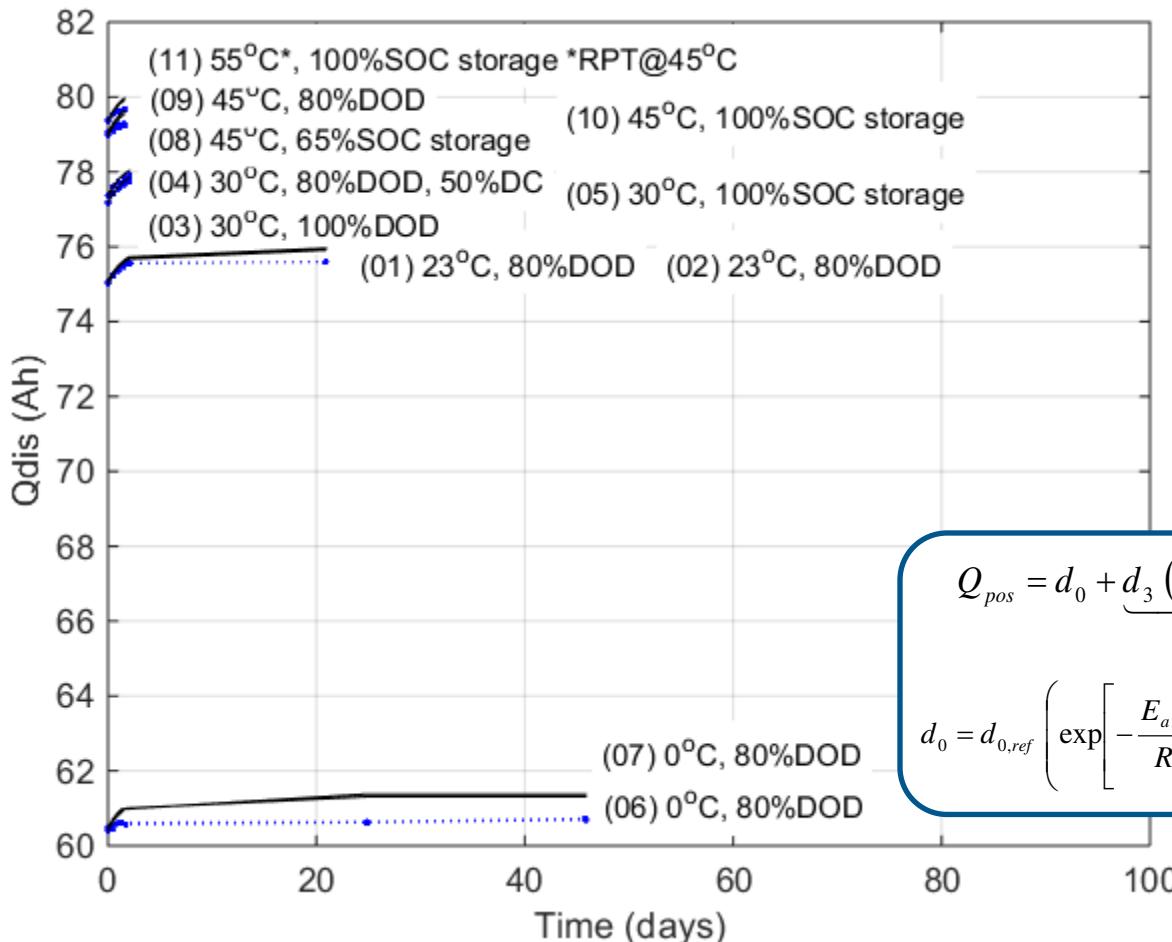


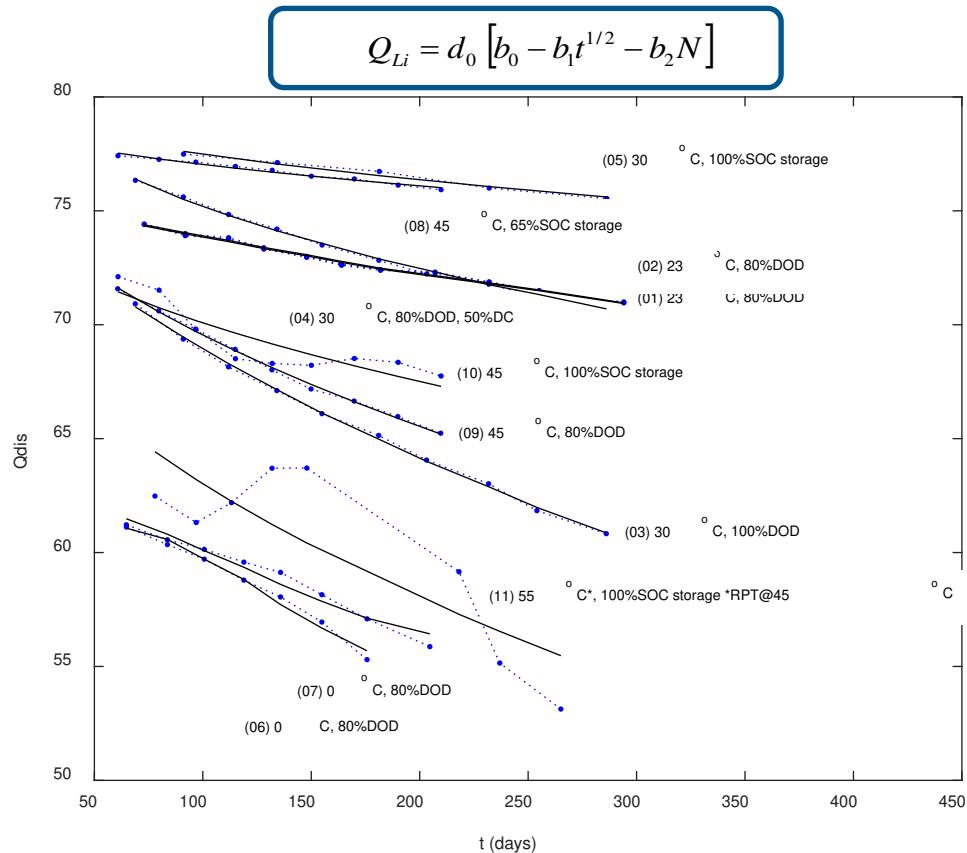
Image: Dean Miller & Daniel Abraham,
Argonne National Laboratory

$$Q_{pos} = d_0 + \underbrace{d_3 (1 - \exp(-Ah_{dis} / 228))}_{\text{Increase in capacity at BOL}}$$

$$d_0 = d_{0,ref} \left[\exp \left[-\frac{E_{a,d_0,1}}{R_{ug}} \left(\frac{1}{T_{RPT}(t)} - \frac{1}{T_{ref}} \right) - \left(\frac{E_{a,d_0,2}}{R_{ug}} \right)^2 \left(\frac{1}{T_{RPT}(t)} - \frac{1}{T_{ref}} \right)^2 \right] \right]$$

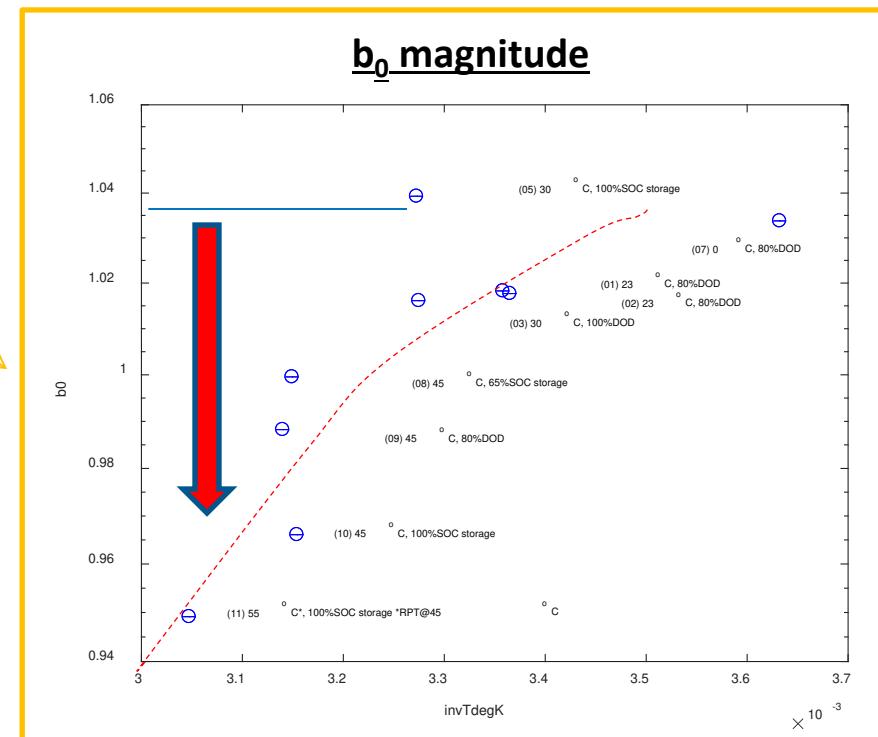
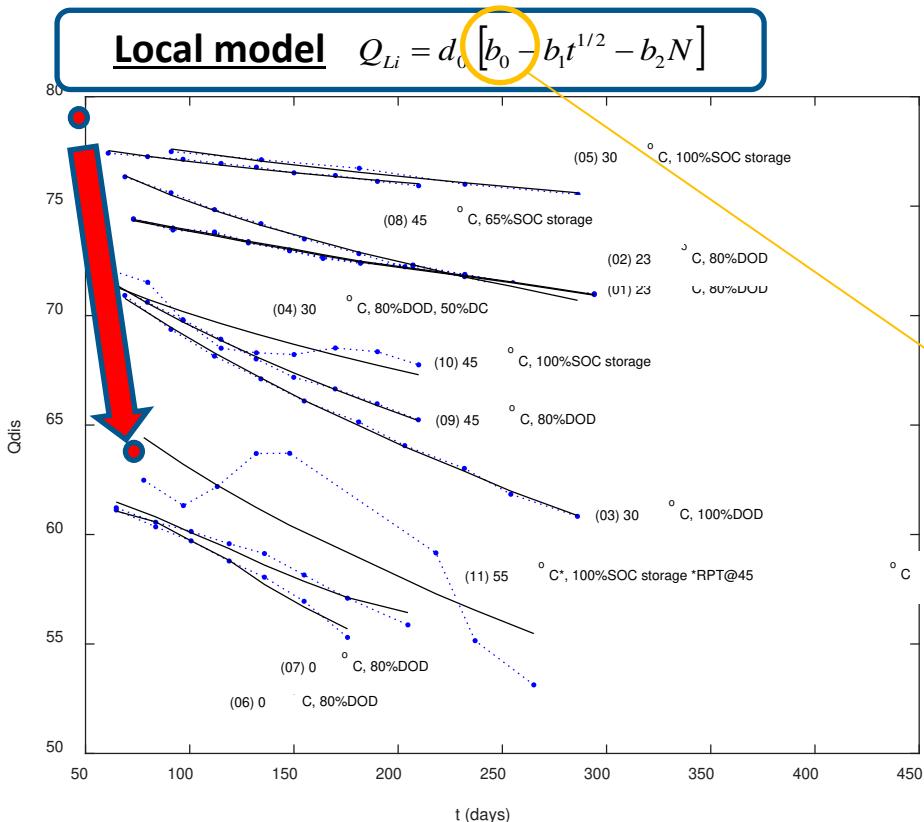
Q_{Li} Local Models

- Local models: Separately fit b_0 , b_1 , b_2 for each data set, excluding
 - First 50 days of data (allows y-intercept to vary with break-in)
 - Knee at 0°C (to be captured later with Q_{neg} model)



- Choice of mechanisms justified by $R^2=0.990$ and flat residuals

Q_{Li} Magnitude of break-in Li-loss



- Least degraded cells show ~3-4% excess Li capacity
- High temperature causes rapid loss in first 50 days
 - Open-circuit voltage and DOD also increase loss
 - Evidence of film layer formation at positive electrode?

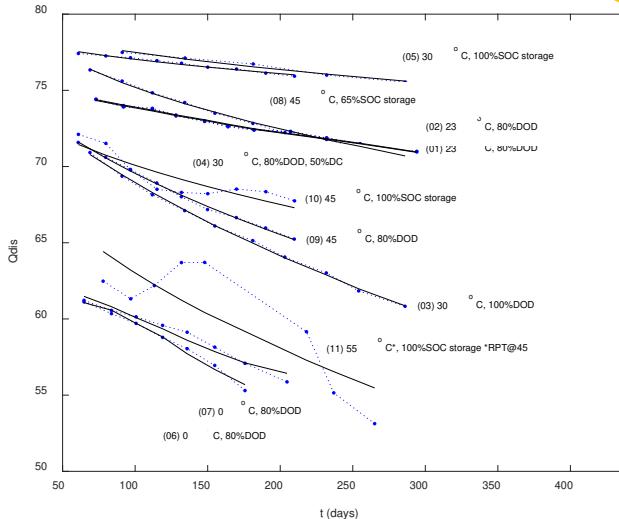
b_0 magnitude model

$$y_0 - b_3(1 - \exp(-t / \tau_{b3}))$$

$$b_3 = b_{3,ref} \exp\left[-\frac{E_{a,b_3}}{R_{ug}}\left(\frac{1}{T(t)} - \frac{1}{T_{ref}}\right)\right] \exp\left[\frac{\alpha_{b_3} F}{R_{ug}}\left(\frac{V_{oc}(t)}{T(t)} - \frac{V_{ref}}{T_{ref}}\right)\right] (1 + \theta DOD_{max})$$

Q_{Li} Calendar fade rate

Local model $Q_{Li} = d_0 [b_0 - b_1 t^{1/2} - b_2 N]$

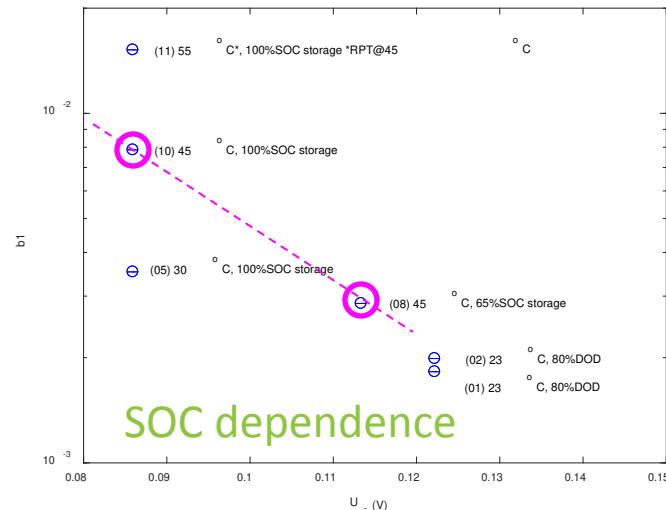
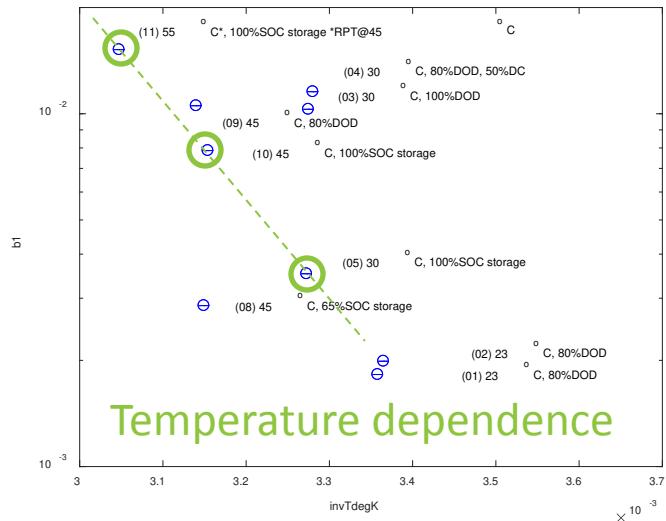


b_1 rate model

$$b_1 = b_{1,ref} \exp\left[-\frac{E_{a,b_1}}{R_{ug}}\left(\frac{1}{T(t)} - \frac{1}{T_{ref}}\right)\right] \exp\left[\frac{\alpha_{b_1} F}{R_{ug}}\left(\frac{U_-(t)}{T(t)} - \frac{U_{ref}}{T_{ref}}\right)\right] \exp\left[\gamma_{b_1} (DOD_{max})^{\beta_{b_1}}\right]$$

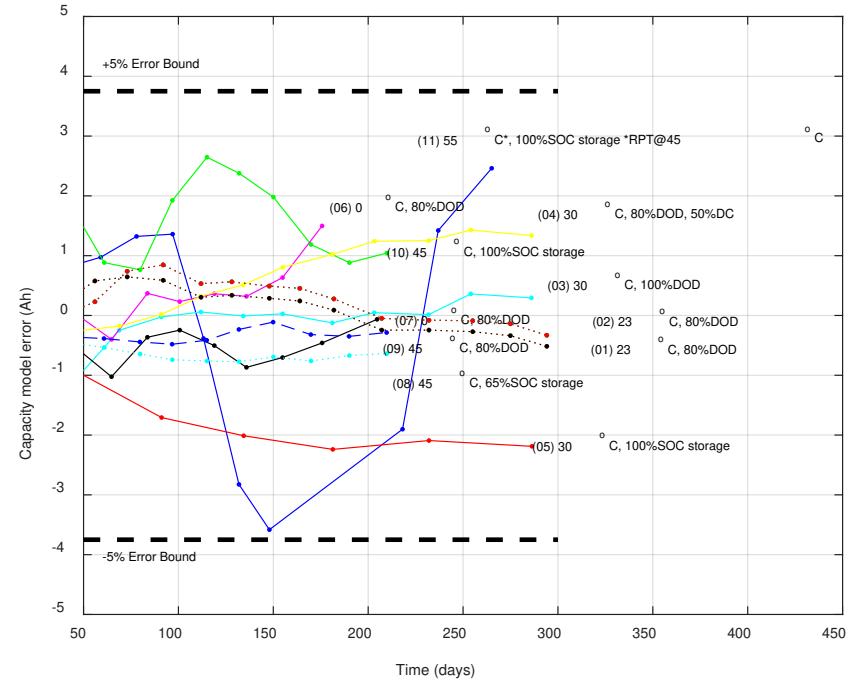
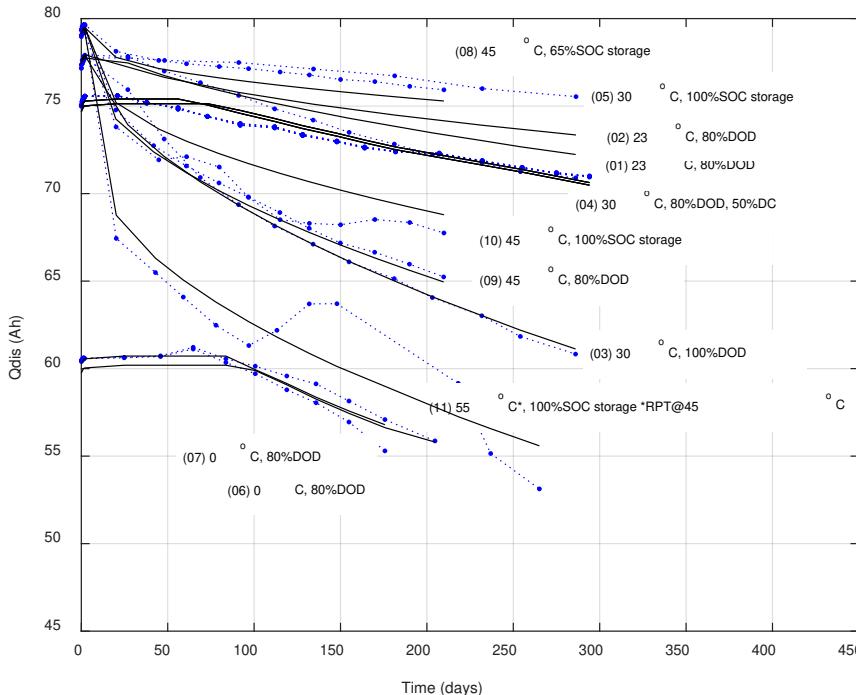
- Visualization of rates suggests rate model equations
- Fitted rate model parameters provide initial guess for global model parameters

b_1 rate



Q_{Li} Global Model

- With equations known, parameters fit to all data simultaneously
- R² = 0.985, RMSE = 1% of capacity, flat residuals



Q_{Li} global model

$$Q_{Li} = d_0 \left[b_0 - \underbrace{b_1 t^{1/2}}_{\text{SEI growth with calendar time}} - \underbrace{b_2 N}_{\text{Loss with cycling}} - \underbrace{b_3 (1 - \exp(-t / \tau_{b3}))}_{\text{Break-in mechanism at BOL}} \right]$$

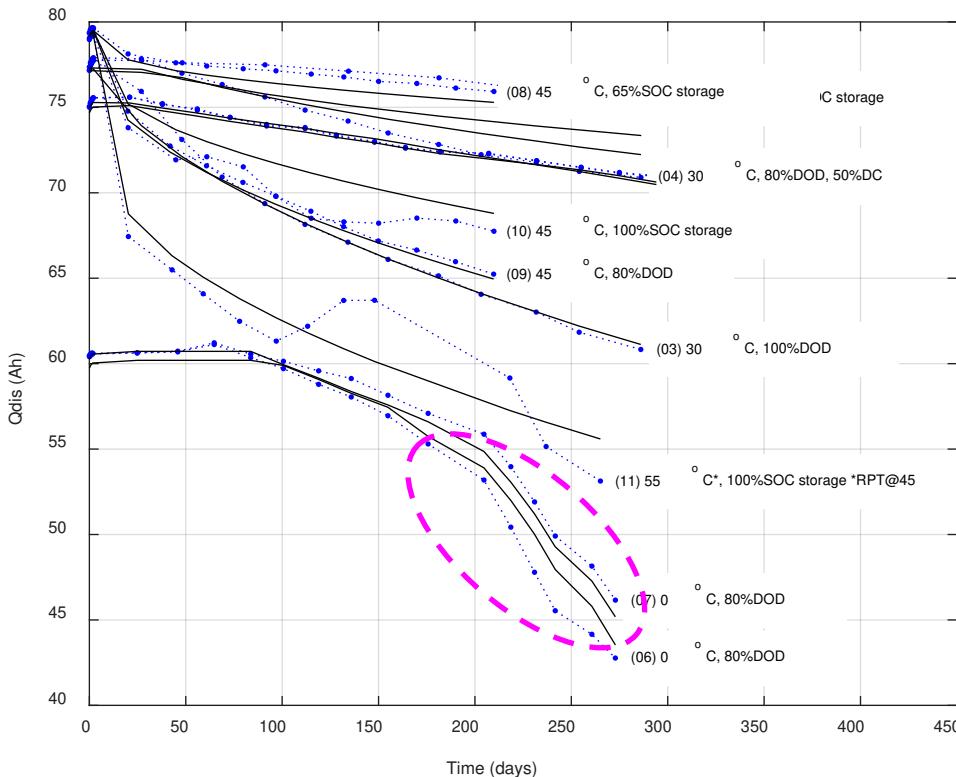
$$b_1 = b_{1,ref} \exp \left[-\frac{E_{a,b_1}}{R_{ug}} \left(\frac{1}{T(t)} - \frac{1}{T_{ref}} \right) \right] \exp \left[\frac{\alpha_{b_1} F}{R_{ug}} \left(\frac{U_-(t)}{T(t)} - \frac{U_{ref}}{T_{ref}} \right) \right] \exp \left[\gamma_{b_1} (DOD_{max})^{\beta_{b1}} \right]$$

$$b_2 = b_{2,ref} \exp \left[-\frac{E_{a,b_2}}{R_{ug}} \left(\frac{1}{T(t)} - \frac{1}{T_{ref}} \right) \right]$$

$$b_3 = b_{3,ref} \exp \left[-\frac{E_{a,b_3}}{R_{ug}} \left(\frac{1}{T(t)} - \frac{1}{T_{ref}} \right) \right] \exp \left[\frac{\alpha_{b_3} F}{R_{ug}} \left(\frac{V_{OC}(t)}{T(t)} - \frac{V_{ref}}{T_{ref}} \right) \right] (1 + \theta DOD_{max})$$

Q_{Neg} Model

- Captures knee with cold temperature cycling
- Minor importance in most real-world scenarios



Q_{Neg} global model

$$\frac{dQ_{\text{neg}}}{dN} = - \left(\frac{c_2}{Q_{\text{neg}}} \right)$$

$$Q_{\text{neg}} = \left[c_0^2 - 2c_2c_0 N \right]^{\frac{1}{2}}$$

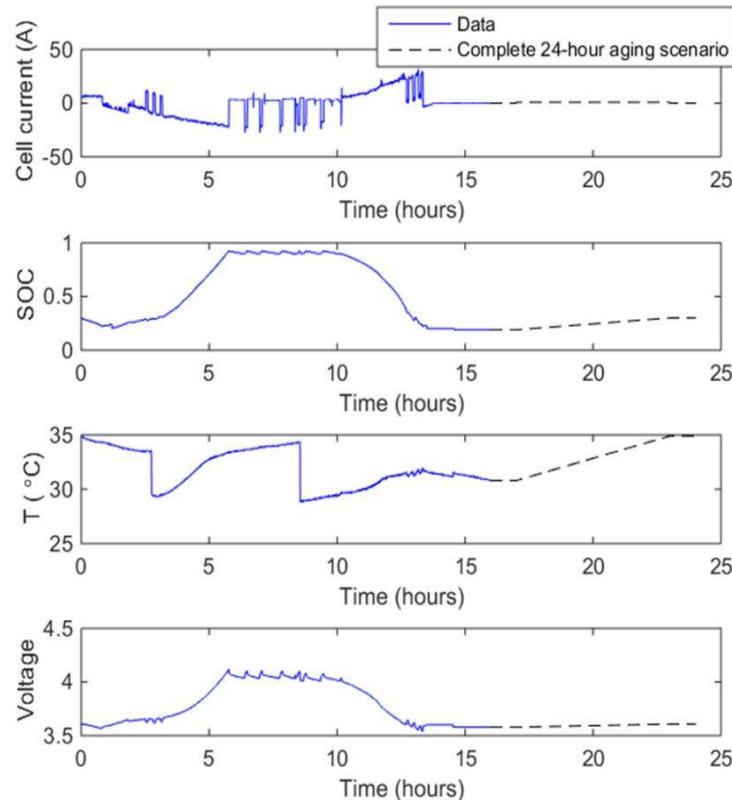
$$c_0 = c_{0,\text{ref}} \exp \left[- \frac{E_{a,c0}}{R_{ug}} \left(\frac{1}{T(t)} - \frac{1}{T_{\text{ref}}} \right) \right]$$

$$c_2 = c_{2,\text{ref}} \exp \left[- \frac{E_{a,c2}}{R_{ug}} \left(\frac{1}{T(t)} - \frac{1}{T_{\text{ref}}} \right) \right] (DOD)^{\beta_{c2}}$$

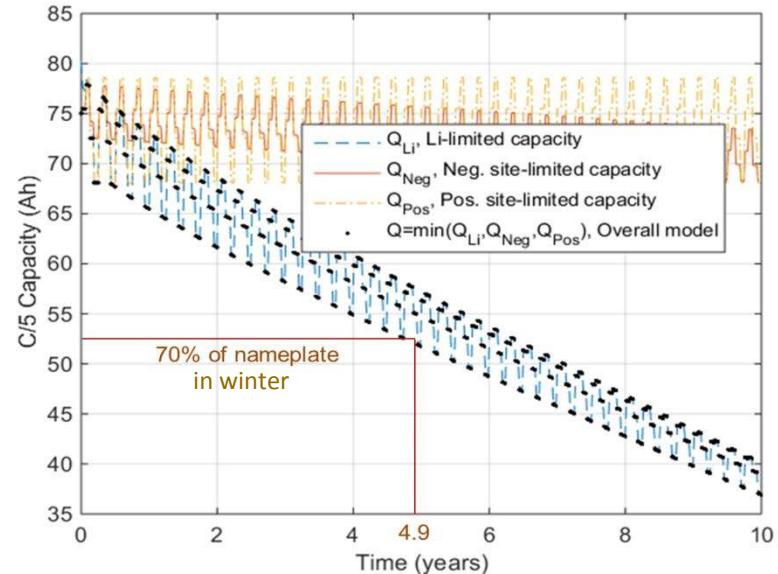
Lifetime analysis – PV self consumption

- Model reformulated in rate-based form
- SOC(t) discretized into microcycles, DOD_i, using Rainflow algorithm

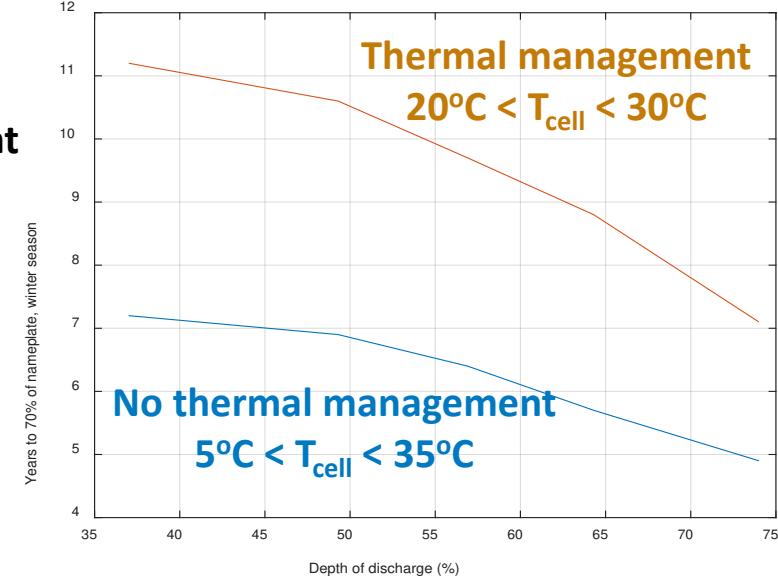
- Application data



- Multi-year, 4-season simulation
- Same cycle each



- Impact of DOD and thermal management



Conclusions

- **Battery energy storage can enable increased integration of renewable power generation on the grid**
- **Battery life modeling methodology formalized, aiding systems design process**
 - Capacity error: $L_2 = 1\%$, $L_\infty = 5\%$
 - For studied Gr/NMC Li-ion ES technology, best to restrict daily cycles < 55% DOD with occasional larger excursions
 - Thermal management extends life from 7 to 10 years
- **Battery aging experiments are time consuming & expensive**
- **Additional model validation needed**
 - Longer duration
 - Variable cycling & temperature
- **Life model accuracy may be enhanced in the future by coupling with electrochemical modeling & diagnostics**

Acknowledgements

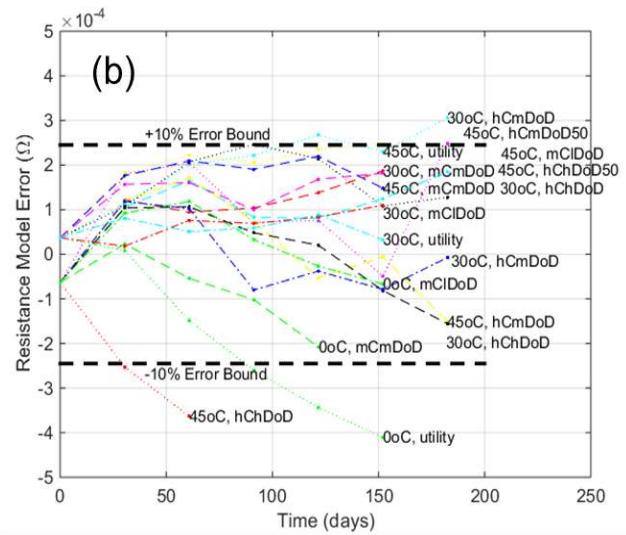
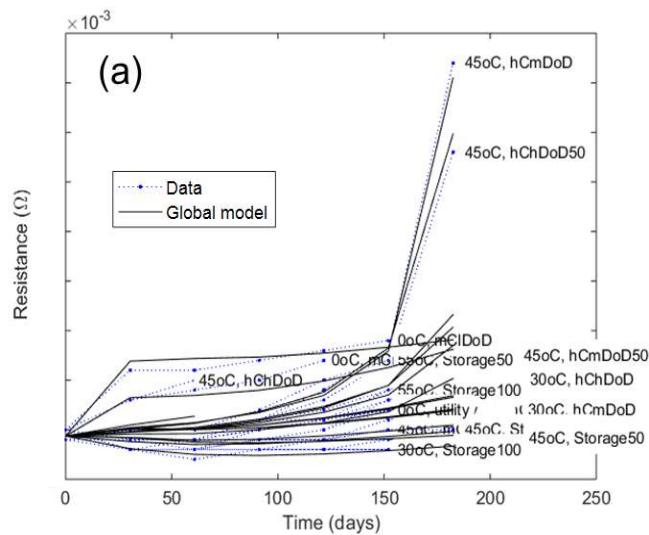
- U.S. DOE Office of Energy Efficiency and Renewable Energy Solar Energy Technologies Program
- SunPower Corporation

Extra Slides

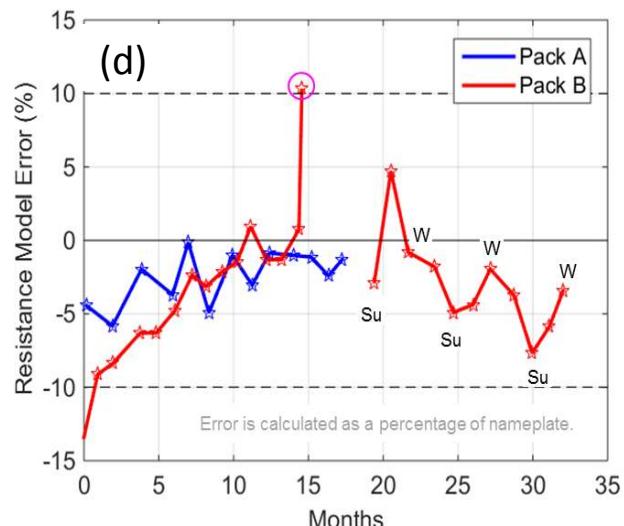
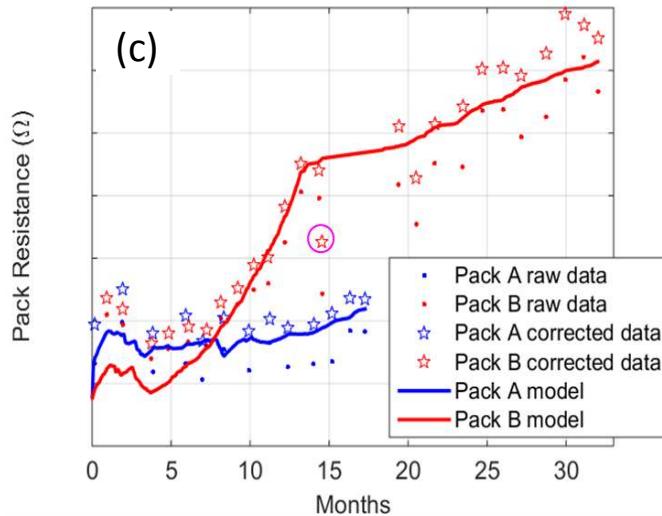
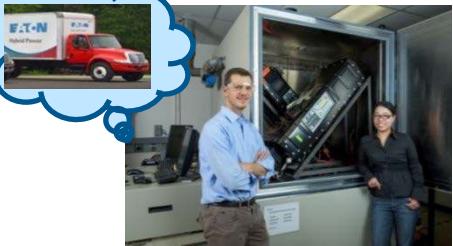
Previous Validation of Life Model

Eaton Corp. ARPA-E AMPED project resulting in 35% smaller HEV battery (PI: Dr. Chinmaya Patil/Eaton)

Cell-level aging tests Prognostic model characterization



Pack-level HIL tests HEV prognostic control algorithm validation



Model tuned to 6 months simple cell aging data matches 33 months 4-season cycling with same accuracy