



# Linking Microdosimetric Measurements to Biological Effectiveness in Ion Beam Therapy: A Review of Theoretical Aspects of MKM and Other Models

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Different qualities of radiation are known to cause different biological effects at the same absorbed dose. Enhancements of the biological effectiveness are a direct consequence of the energy deposition clustering at the scales of DNA molecule and cell nucleus whilst absorbed dose is a macroscopic averaged quantity which does not take into account heterogeneities at the nanometer and micrometer scales. Microdosimetry aims to measure radiation quality at cellular or sub-cellular levels trying to increase the understanding of radiation damage mechanisms and effects. Existing microdosimeters rely on the well-established gas-based detectors or the more recent solid-state devices. They provide specific energy  $z$  spectra and other derived quantities as lineal energy ( $y$ ) spectra assessed at the micrometer level. The interpretation of the radio-biological experimental data in the framework of different models has raised interest and various investigations have been performed to link *in vitro* and *in vivo* radiobiological outcomes with the observed microdosimetric data. A review of the major models based on experimental microdosimetry, with a particular focus on ion beam therapy applications and an emphasis on the microdosimetric kinetic model (MKM), will be presented in this work, enlightening the advantages of each one in terms of accuracy, initial assumptions, and agreement with experimental data. The MKM has been used to predict different kinds of radiobiological quantities such as the relative biological effects for cell inactivation or the oxygen enhancement ratio. Recent developments of the MKM will be also presented, including new non-Poissonian correction approaches for high linear energy transfer radiation, the inclusion of partial repair effects for fractionation studies, and the extension of the model to account for non-targeted effects. We will also explore developments for improving the models by including track structure and the spatial damage correlation information, by using the full fluence spectrum and by better accounting for the energy-deposition fluctuations at the intra- and inter-cellular level.

**Keywords:** microdosimetry, microdosimetric kinetic model, relative biological effectiveness, oxygen enhancement ratio, biophysical modeling, ion beam therapy

## 1 INTRODUCTION

Ion beam therapy is becoming a well-established clinical option for tumor treatment, particularly advantageous for the highly localized dose deposition and for the radiobiological properties [1]. While the first feature is obvious, for the macroscopic energy deposition profile, characterized by the Bragg peak in depth, and also often by a sharper lateral penumbra, due to the small multiple Coulomb scattering of fast and heavy particles, the second one is related to microscopic features of the ionization pattern induced by particle radiation, for different charge and energy, down to the molecular scale of the biological target (DNA). The accurate prediction of relative biological effectiveness (RBE) in different positions of an irradiating field is a fundamental requirement, in order to correctly estimate treatment responses [2]. Moreover, RBE depends on several factors, of different nature, biological, patient, and treatment-specific, because of the complexity of the mechanisms of action underlying tumor and normal tissue responses in radiation therapy. A numbers of models have been presented, historically, to predict RBE, attempting to account for such effects. Among these models, the following four main categories can be identified:

- (1) Purely phenomenological models: NIRS<sup>1</sup> mixed beam approach [3–6], mainly used for carbon ion beams.
- (2) Dose-averaged LET ( $LET_D$ )-based models that exploit a linear relationship between the RBE and the  $LET_D$  [7–10], used exclusively for proton beams.
- (3) Local effect model (LEM)-based models [11–17], mainly used for heavier ions, such as carbon ions;
- (4) More general models based on microdosimetry concepts:
  - a. Models based on the microdosimetric kinetic model (MKM), proposed initially by Hawkins in 1994 [18] and then explored and extended till nowadays [19–23];
  - b. Other models, such as the repair–misrepair–fixation RMF model [24–26] and phenomenological models based on RBE-weighting functions [27–33].

All the different models present different advantages and limitations. While RBE is not measurable with physical methods, the fourth category allows a strong link with physics measurements through different types of microdosimeters. The present paper is focused on reviewing the modeling of biological effect of protons and other ions used in ion beam therapy based on the microdosimetry concepts with particular emphasis to the MKM, a widely used model to predict the cell survival and the RBE by using microdosimetric data. This topical review is organized as follows: the fundamental microdosimetric quantities [34, 35], required for addressing the problem, are defined in **Section 2** together with a focus on relevant experimental quantities. Then, the original formulation of MKM is presented in **Section 3** with its theoretical bases (**Section 3.1**) and followed by the main extensions such as non-Poisson and

saturation corrections [19, 20] (**Section 3.5**), the incorporation of a track model [21], a variable  $\beta$  parameter deriving from the effects of the lesion yield fluctuations in the cell nucleus and domains, [22, 23] in **Section 3.8**, and the generalization of the model in case of a time structured irradiation introduced in **Section 3.7**. The available experimental *in vitro* and *in vivo* validations are also reported for each extensions. **Figure 1** represents a conceptual scheme of the main MKM formulations and extensions presented in this paper. Further, an example of treatment planning systems (TPS) implementation of the MKM [36] will be given in **Section 3.6**. Other applications of the MKM, such as the oxygen enhancement ratio (OER) modeling [37, 38] and the incorporation of non-targeted effects [39] will be described in **Section 3.9**. Finally, other models based on microdosimetry as well, i.e., the distribution function by Loncol et al. [40] and the RMF model [24, 25], will be presented in **Section 4**.

## 2 MICRODOSIMETRIC DISTRIBUTIONS AND THEIR MOMENTS

The main microdosimetric quantities of interest are the *specific energy*  $z$  and *lineal energy*  $y$  [34, 41–43]. The *specific energy*  $z$  is the ratio between energy imparted by ionizing radiation  $\epsilon$  and the mass  $m$  of the matter that has received the radiation, that is,

$$z = \frac{\epsilon}{m}. \quad (1)$$

The energy imparted  $\epsilon$  may be due to one or more energy deposition events, i.e., due to one or more statistically independent particle tracks. The *lineal energy*  $y$  is the ratio between energy imparted to the matter in a volume of interest by a single energy-deposition event,  $\epsilon_1$ , and the mean chord length in that volume,  $\bar{l}$ , that is,

$$y = \frac{\epsilon_1}{\bar{l}}. \quad (2)$$

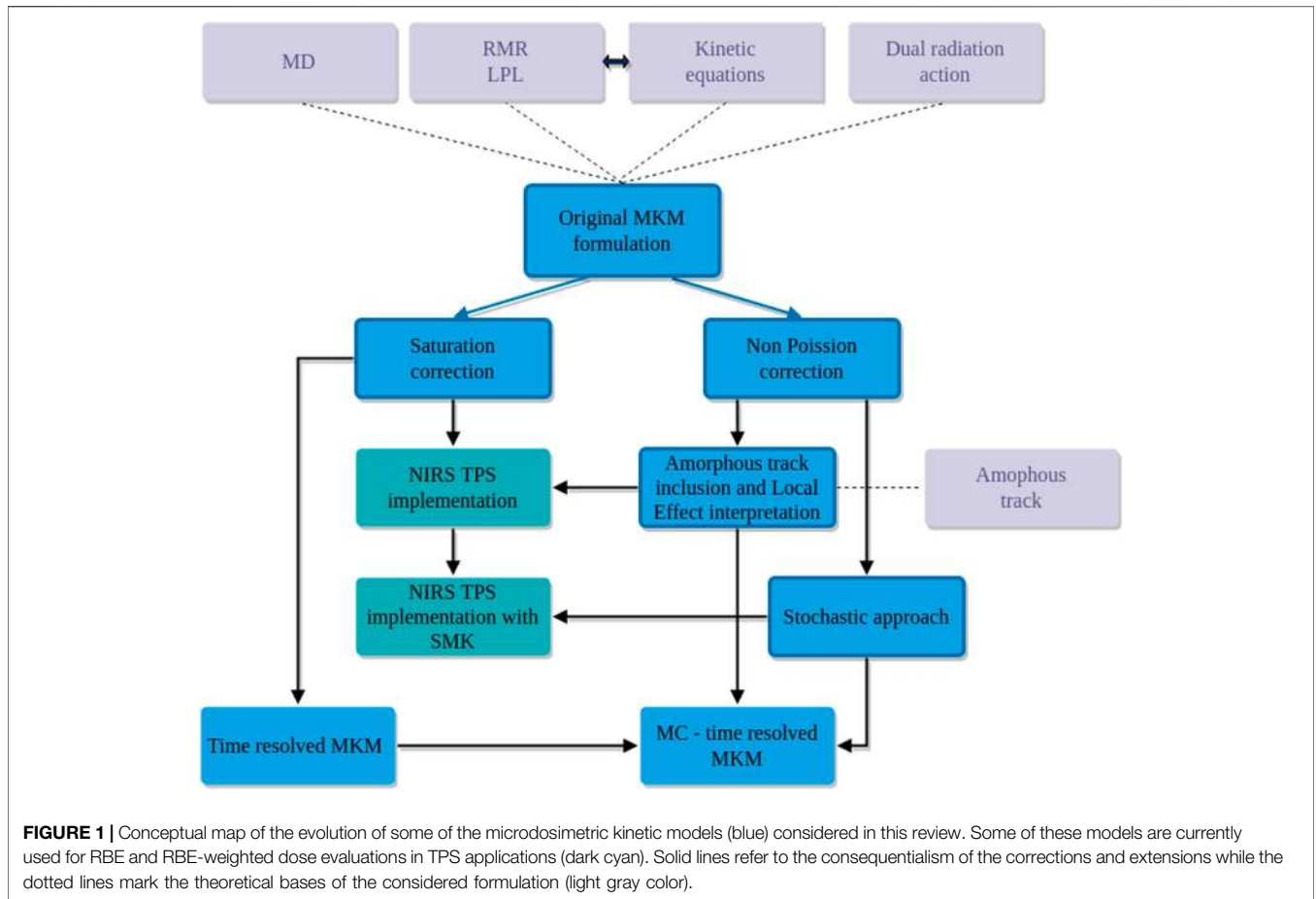
The stochastic nature of  $\epsilon$  and  $\epsilon_1$  implies that also  $z$  and  $y$  are stochastic quantities. In the following, given a probability density distribution  $f(z)$ , we will assume that the probability that a specific energy  $z$  is produced in the interval  $[z_a, z_b]$  is given by

$$\int_{z_a}^{z_b} f(z) dz. \quad (3)$$

When dealing with *specific energy spectra*, it is important to distinguish between the *single-event distribution* and the *multi-event distribution*. It is worth stressing that, although experimental microdosimetry determines single event quantities such as the  $\epsilon_1$  or the *lineal energy*  $y$ , the starting point for models are multi-event quantities such as the *specific energy*  $z$  and its distribution.

The *single-event distribution*, denoted by  $f_1(z)$ , is the probability distribution of  $z$  conditioned to the fact that precisely a single-event happened. The single-event distribution is the building block to define the more-general  $n$ -event distribution  $f_n(z)$  and the *multi-event distribution*  $f(z)$ .

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**FIGURE 1** | Conceptual map of the evolution of some of the microdosimetric kinetic models (blue) considered in this review. Some of these models are currently used for RBE and RBE-weighted dose evaluations in TPS applications (dark cyan). Solid lines refer to the consequentialism of the corrections and extensions while the dotted lines mark the theoretical bases of the considered formulation (light gray color).

The  $n$ -event distribution  $f_n(z)$ , that is, the probability distribution conditioned to the fact that precisely  $n$  events occurred, can be computed as the  $n$ -fold convolution of the single-event distribution  $f_1(d)$ , as follows:

$$\begin{aligned}
 f_2(z) &:= \int_0^\infty f_1(z')f_1(z-z')dz', \\
 &\dots \\
 f_n(z) &:= \int_0^\infty f_1(z')f_{n-1}(z-z')dz',
 \end{aligned}
 \tag{4}$$

see [42] for details.

Using the  $n$ -event distributions defined above, we can define the general *multi-event distribution* as

$$f(z; \lambda_n) := \sum_{n=0}^\infty p(n; \lambda_n)f_n(z),
 \tag{5}$$

with  $p(n; \lambda_n)$  an integer valued probability distribution with average  $\lambda_n$ , meaning that

$$\lambda_n := \sum_{n=0}^\infty np(n; \lambda_n).$$

The *multi-event distribution*  $f(z; \lambda_n)$  plays a crucial role in the development of microdosimetric-based radiobiological models. It is worth noticing that  $f(z; \lambda_n)$  depends on the

number of events  $n$  only through  $p(n; \lambda_n)$ , which is independent of specific energy  $z$ . Also, given  $p(n; \lambda_n)$ , the single-event distribution  $f_1$  completely determines the multi-event distribution  $f(z; \lambda_n)$ .

Typically, since events are statistically independent,  $p(n; \lambda_n)$  is assumed to be a Poisson distribution with mean value  $\lambda_n$ , so that Eq. (5) becomes

$$f(z; \lambda_n) := \sum_{n=0}^\infty e^{-\lambda_n} \frac{\lambda_n^n}{n!} f_n(z).
 \tag{6}$$

Denoting by  $\langle z \rangle$  the first moment of the distribution  $f(z; \lambda_n)$ , formally

$$\langle z \rangle := \int_0^\infty zf(z; \lambda_n)dz,
 \tag{7}$$

it follows that the following relation holds true,

$$\langle z \rangle = \lambda_n z_F,
 \tag{8}$$

being  $z_F$  the *frequency-average* of the single-event specific energy defined as

$$z_F := \int_0^\infty zf_1(z)dz,
 \tag{9}$$

see [42], Chapter II. In microdosimetry,  $\langle z \rangle$  is often identified with the absorbed dose  $D$ ; we shall use this identification in the following of the paper.

Above argument, with particular reference to Eq. (8), yields the form for the average value  $\lambda_n$  of the *multi-event distribution* to be

$$\lambda_n = \frac{D}{z_F}, \quad (10)$$

see [34, 42]. Again, in the following, if not differently specified, we will consider  $\lambda_n$  to be defined as in Eq. (10).

Further computations, see [34, 42], shows that regarding the second moment it holds

$$\int_0^\infty z^2 f(z; \lambda_n) dz = D^2 + z_D D, \quad (11)$$

with  $z_D$  the *dose-average* of the single-event specific energy

$$z_D := \frac{1}{z_F} \int_0^\infty z^2 f_1(z) dz = \frac{\int_0^\infty z^2 f_1(z) dz}{\int_0^\infty f_1(z) dz}. \quad (12)$$

Notation and computations performed in the current section will be extensively used through the work to formally derive analytical solution for some relevant biological endpoints, typically the cell-survival probability, starting from a mathematical model for DNA damage.

In the following, we assume that a cell nucleus is divided into  $N_d$  domains, so that the above microdosimetric distributions will be used both on single-domain and on the whole cell nucleus. In particular, the superscript  $(c, d)$  will denote that the corresponding quantity, such as a microdosimetric distribution or a corresponding average value, is considered on the domain  $d$  of the cell  $c$ . Further, the subscript  $n$  denotes that microdosimetric distributions are on the cell-nucleus, whereas if no subindex is specified, it is assumed that the corresponding distribution is on the domain.

In order to make computations less heavy as possible, whenever we will say that we average a function  $g(z)$  over all domains of a cell nucleus, denoted for short by  $\langle g \rangle_d^{(c)}$ , it formally means

$$\langle g \rangle_d^{(c)} := \frac{1}{N_d} \sum_{d=1}^{N_d} \int_0^\infty g(z) f^{(c,d)}(z; z_n) dz, \quad (13)$$

where  $f^{(c,d)}(z; z_n)$  denotes the probability density of  $z$  in a domain for cell with nucleus specific energy  $z_n$ . Similarly, by averaging over all cell population function  $g_n(z)$  defined over a nucleus, denoted by  $\langle g_n \rangle_c$ , we mean

$$\langle g_n \rangle_c := \frac{1}{N_c} \sum_{c=1}^{N_c} \int_0^\infty g_n(z) f_n^{(c)}(z; D) dz, \quad (14)$$

where  $N_c$  is the total number of the considered cells and  $f_n^{(c)}(z; D)$  denotes the probability density of  $z$  in a nucleus for a population of cells irradiated with macroscopic dose  $D$ . Notice that in practical computations of an irradiated population of cells, such as those described in the immediate next sections, the

probability densities are reasonably considered equals among different cells and domains. In this case, we will drop the indexes  $c$  and  $d$  and the sums in Eqs (13) and (14) can be carried out implicitly:

$$\langle g \rangle_d = \int_0^\infty g(z) f(z; z_n) dz, \quad (15)$$

$$\langle g_n \rangle_c = \int_0^\infty g_n(z) f_n(z; D) dz. \quad (16)$$

## 2.1 Experimental Quantities

In order to account for the different densities and sizes of the sites of radiobiological interests. (e.g., the cell nucleus and the domain), the specific energy  $z$  used in the models as described in the following sections can be obtained experimentally through the *lineal energy*  $y$  defined in Eq. (2).

The lineal energy can be measured through a microdosimeter detector, where the most frequently used are the tissue-equivalent proportional counters (TEPC) [44–47]; analogous information can be achieved also by solid-state detectors [48, 49] and gas electron multiplier (GEM) detectors [50, 51], recently investigated for their use in microdosimetric measurements [52, 53]. The relationship between  $\bar{l}$  of the tissue-equivalent volume of the microdosimeter, from which the lineal energy is calculated, and the physical mean chord of the detector,  $\bar{l}_{det}$ , is given approximately by

$$\bar{l} = \bar{l}_{det} \frac{\rho_{det}}{\rho}, \quad (17)$$

where  $\rho$  and  $\rho_{det}$  are the densities of the tissue and the detector material, respectively. For more general conversion methods of microdosimetric spectra between different materials and shapes see, for example, [54, 55], for an MC-based method.

The theoretical single-event imparted energy,  $z_1$ , can be estimated from the lineal energy  $y$  as

$$z_1 = y \bar{l}_t / m_t, \quad (18)$$

where  $\bar{l}_t$ ,  $m_t$  are the mean chord length and the mass of the biological site of interest, respectively. The subscript  $t$  is used in this context to indicate the tissue in terms of material, mass, and geometry of the biological site. The single-event dose-averaged specific energy  $z_D$  can be obtained from the mean-dose lineal energy  $y_D$  as

$$z_D = \frac{\bar{l}_t}{m_t y_F} \int_0^\infty y^2 f(y) dy = \frac{\bar{l}_t}{m_t} y_D, \quad (19)$$

where  $y_F$  is the frequency-average lineal energy.

In the case of a spherical volume with density  $\rho_t = 1 \text{ g/cm}^3$ , the specific energy  $z_1$  is linked to the lineal energy  $y$  [56] as

$$z_1 \text{ (Gy)} = 0.204 \times \frac{y \text{ (keV}/\mu\text{m})}{[2r_{det} \text{ (}\mu\text{m)}]^2}, \quad (20)$$

where the constant factor is due to the Gy-keV conversion (1 Gy =  $1.6 \times 10^{-16}$  keV) and to the consideration that the mean chord length in the case of a sphere is  $\bar{l} = 4/3 r_{det}$ .

### 3 MICRODOSIMETRIC KINETIC MODEL

The microdosimetric kinetic (KM) model has been developed by Roland B. Hawkins [18] by taking inspiration from the theory of dual radiation action (TDRA) [57, 58], the repair-misrepair model [59, 60], and the lethal-potentially lethal (LPL) model [61, 62]. In the following sections, after a brief description of the historical bases of the model and the details of its original formulation, we compare and contrast the more recent developments of the model.

#### 3.1 Historical Bases

This section presents a brief explanation of the theoretical formulations on which the considered models are based on. In the theory of dual radiation action (TDRA), the concept of *dual radiation action* is introduced as a process in which cellular lesions are produced as a result of the interaction of pairs of sublesions that are molecular alterations produced by ionizing radiation that in turn results in an observable cellular effect such as a chromosome aberration or cell reproductive death. The TDRA in its original formulation developed for neutron irradiation and then further generalized [57] assumes that, after the cell irradiation, the number of lethal lesions  $\epsilon$  in a small volume of the cell nucleus, defined *site*, is proportional to the square of the specific energy  $z$  in that site.

$$\epsilon(z) = kz^2. \quad (21)$$

By evaluating the expectation value of  $z^2$  (Eq. 11), it is possible to derive a linear-quadratic relation between  $\epsilon$  and the dose:

$$\epsilon(D) = k\langle z^2 \rangle = k(z_D D + D^2) = k(z_D + D)D. \quad (22)$$

The interpretation of Eq. (22) is that the number of sublesions is proportional to  $D$  and the mean energy concentration around the individual sublesions is proportional to  $(z_D + D)$ . Within the bracket,  $z_D$  represents the energy concentration produced by the same particle track (*intratrack action*), and  $D$  represents the contribution from other particle tracks (*intertrack action*). A problem in Eq. (22) arise when one has to account the possibility of a non-vanishing linear term in the dose (observable for low doses) even for sparsely ionizing radiation, such as photons, since the term  $z_D$  is expected to be negligible for such radiation. This is obtained by generalizing Eq. (21) by including an additional linear term:

$$\epsilon(z) = k(\lambda_0 z + z^2), \quad (23)$$

from which one obtains the dose dependence:

$$\epsilon(D) = k((z_D + \lambda_0)D + D^2). \quad (24)$$

An important additional assumption that drives the dual action process is that sublesions can be produced throughout the nucleus of the cell but can combine with appreciable probability only over distances smaller than the dimension of the nucleus. This effect of sublesion proximity on the formation of lethal lesions was incorporated in the TDRA by the concept of the *sites* within which such sublesions can combine. In a

generalization of the TDRA [58], the interaction probability of sublesions has been also further refined using an explicit function of their separation.

MKM inherits the concept of damage time evolution for the repair or conversion into a lethal irreparable lesion (chromosome aberration) [18, 63, 64] of the primary potentially lethal radiation induced lesions in DNA from the *repair-misrepair (RMR) model*, developed by Tobias *et al.* to interpret radiobiological experiments with heavy ions [59, 60]. The RMR model considers that the amount of DSBs in the DNA,  $U(t)$ , is linearly proportional to the radiation dose-rate  $\dot{D}(t) = dD(t)/dt$ ; a number of DSBs evolve in lethal lesions,  $L(t)$ , while most breaks are successfully repaired with a first-order process. The model includes also the possibility of a misrepair as a second-order process since it involves two broken DNA strands to form a chromosomal aberration. The idea of misrepair was initially applied by Lea and Catcheside [65] to describe the formation of chromosome aberrations in *Tradescantia*.

These assumptions yield the following kinetic equations:

$$\begin{aligned} \frac{dU}{dt} &= \underbrace{\delta \dot{D}}_{\text{damage}} - \underbrace{\lambda U}_{\text{repair}} - \underbrace{\kappa U^2}_{\text{misrepair}}, \\ \frac{dL}{dt} &= \underbrace{(1-\phi)\lambda U}_{\text{unsuccessful repair}} + \underbrace{\sigma \kappa U^2}_{\text{lethal misrepair}}, \end{aligned} \quad (25)$$

where  $\delta$  is the number of DSBs induced per Gy of radiation,  $\lambda$  is the rate at which DSBs are repaired,  $\kappa$  is the rate constant for second-order DSB interaction, and  $\phi$  is the fraction of simple repairs that are successful. The fraction of misrepairs that result in a lethal lesion is  $\sigma$ .

Like the RMR model, the *lethal-potentially lethal (LPL) model* [61, 62] accounts that the damages caused by ionizing radiation at the molecular level and contributing to cell death can be separated into two broad classes (i) that which has the potential of being lethal,  $P(t)$  (by fixing or binary misrepair) but also can be repaired correctly and (ii) that which is lethal *ab initio* and cannot be repaired correctly,  $L(t)$ . Both lesions are linearly proportional to the radiation dose-rate [66], and after a prescribed time, the remaining potentially lethal lesions become lethal as described in the following equations:

$$\begin{aligned} \frac{dP}{dt} &= \underbrace{\delta \eta \dot{D}}_{\text{reparable damage}} - \underbrace{\lambda P}_{\text{repair}} - \underbrace{\kappa P^2}_{\text{misrepair}}, \\ \frac{dL}{dt} &= \underbrace{\delta(1-\eta)\dot{D}}_{\text{irreparable damage}} + \underbrace{\kappa P^2}_{\text{lethal misrepair}}, \end{aligned} \quad (26)$$

where  $\eta$  is the amount of radiation induced DSBs that are reparable, while all the other parameters correspond in meaning to the ones in Eq. (25).

The solutions of the RMR and the LPL models are similar. However, in contrast to the RMR, the LPL predicts that the probability of the interaction between potentially lethal lesions is strongly dependent to the dose-rate and becomes negligible for low dose-rates, where only the channel of the direct creation of lethal events through  $\delta$  dominate.

### 3.2 Original Formulation and General Considerations

The MKM computes the cell survival in a way that emphasizes subcellular microdosimetry while abstracting the specific description and modeling of the radiation-induced damage to the cell by using the general categories of lethal and potentially lethal lesions as defined in [61]. More specifically, the MKM is based on the following assumptions [18, 67, 68]:

- (1) The cell nucleus is the sensitive target and it is divided into  $N_d$  sub-units, called domains, similar to the sites of TDRA. In general, domains have a variety of shapes that fit together to fill the nucleus. In the case of mammalian cells, the domain diameter is usually considered to be in the range  $0.5 \leq d_d \leq 1.0 \mu\text{m}$  and the number of domains per nucleus is in the order of few hundreds.
- (2) Radiation can create two different types of DNA damages, called of type I and II.
- (3) Type I lesions represent damage that cannot be repaired, for this reason will be also called lethal lesion. On the contrary, type II lesions, also called sub-lethal or potentially-lethal lesions, can be repaired or converted into a lethal lesion either by spontaneous conversion or by binary combination with another sub-lethal lesion.
- (4) Type I and II lesions are confined to the domain in which they are created. This assumption defines a sub-nuclear correlation length among lesions in a way that the interaction of two lesions can happen only if they are in close spatial proximity. Specifically, a pair of type II lesions can combine to form a type I lesion only if they are created in the same domain; a remark on this assumption is needed. The idea behind the division of a cell into subvolumes arises because couples of type II lesions are all likely to happen in a short time period, even for lesions that are far away in the cell-nucleus. In order to overcome such a problem, a possible approach is to divide the nucleus into smaller subdomains so that interactions might happen solely inside a single volume, as it is assumed in the MKM. It is important to stress the key role that the choice of such domains plays. In fact, if too big domains imply that far away lesions can interact, on the contrary, too small domains yield that the overall number of lesions inside a single domain is so small that couple interactions are less likely to happen. Therefore, the choice of the best possible division of the cell nucleus into smaller domains is a key aspect of the model and different choices of domains can in principle lead to different results. A possible solution to reduce the sensitivity of the model from the arbitrary choice of the domains is to assume that interactions are possible also within different domains, allowing therefore lesions to move from one domain to another or pairs of lesions to interact if in adjacent domains.
- (5) The initial number of type I and II lesions in a single domain  $d$  is proportional to the specific energy  $z$  in the domain.

If above assumptions hold, then the following further assumption is made regarding the reproductive survival of the cell:

- (6) If at least one domain contains a lethal lesion, then the whole cell is “dead.”

It has to be noted that, while the MKM assumptions reported in this section are general, in many studies [69, 70], the lethal lesions are intended to represent a specific complex DNA damage (e.g., lethal chromosome aberrations) that cannot be repaired, whereas the creation of sub-lethal lesions are explicitly associated to the induction of double-strand breaks (DSB) that can be repaired.

Following the MKM notation, we denote by  $x_I^{(c,d,z)}(t)$  and  $x_{II}^{(c,d,z)}(t)$  the time-dependent average number of type I and type II lesions for a cell-domain  $(c, d)$  caused by an acute dose  $z^{(c,d)}$  at  $t = 0$  deposited in the cell  $c$  and domain  $d$ . Starting from the concept, introduced in the TDRA, that a cell experiences a randomly varying dose in a microscopic volume [34, 41], the microscopic specific energy  $z^{(c,d)}$  is considered as a random variable with  $\langle \langle z^{(c,d)} \rangle_d \rangle_c = D$ , the macroscopic dose experienced by the cell population.

Type II lesions are assumed that can be repaired with a constant repairing rate  $r$  or can be converted to irreparable lesions through a first order process with constant rate  $a$ , or at the second order, representing pairwise combinations, with constant rate  $b$ . The average number of type I and II lesions at time 0 is proportional to the amount of specific energy  $z^{(c,d)}$  with factors  $\lambda$  and  $\kappa$ . These assumptions formally define the following set of coupled ODE similar in concept to Eq. (25):

$$\begin{cases} \dot{x}_I^{(c,d,z)} = ax_{II}^{(c,d,z)} + b(x_{II}^{(c,d,z)})^2, \\ \dot{x}_{II}^{(c,d,z)} = -(a+r)x_{II}^{(c,d,z)} - 2b(x_{II}^{(c,d,z)})^2, \end{cases} \quad (27)$$

subject to the initial average number of lesions

$$x_I^{(c,d,z)}(0) = \lambda z^{(c,d)}, \quad x_{II}^{(c,d,z)}(0) = \kappa z^{(c,d)}. \quad (28)$$

In the case of ion radiation, typically the rate of pairwise combination between type II lesions is negligible with respect to the first order evaluation of  $x_{II}$  for low dose [67], that is,

$$2b(x_{II}^{(c,d,z)})^2 \ll (a+r)x_{II}^{(c,d,z)}, \quad (29)$$

so that the time-evolution of the average number of type II lesion can be rewritten as

$$\dot{x}_{II}^{(c,d,z)} = -(a+r)x_{II}^{(c,d,z)}. \quad (30)$$

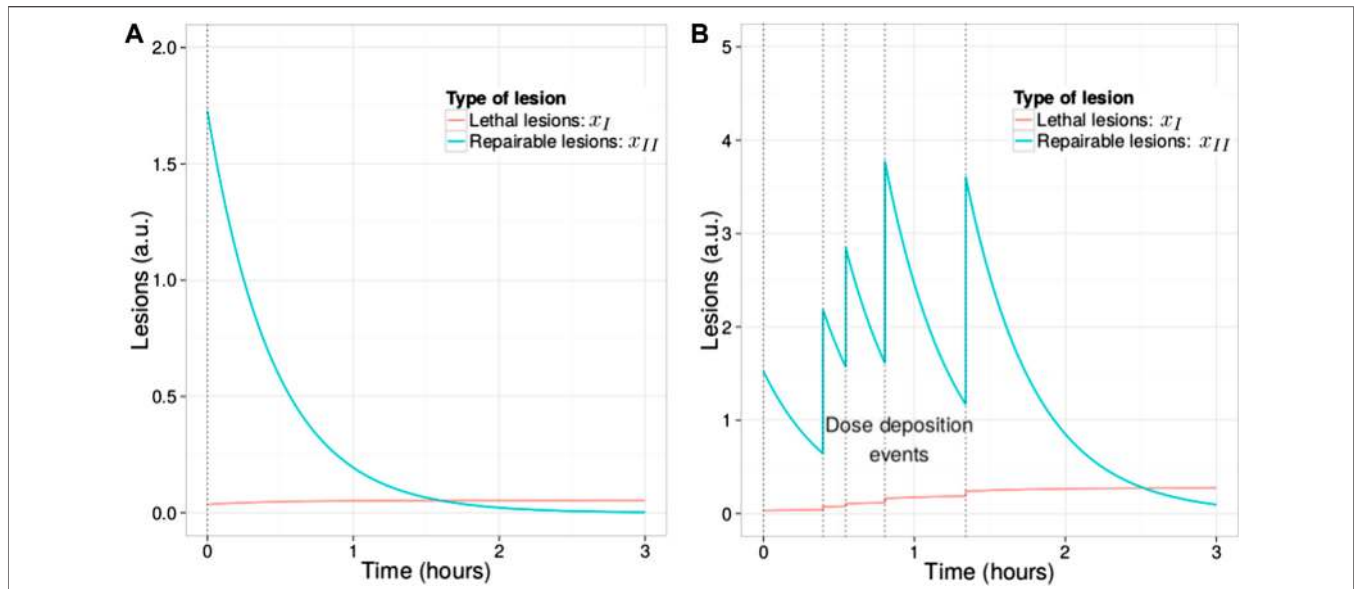
The solution to Eq. (30) can be seen to be

$$x_{II}^{(c,d,z)}(t) = \kappa z^{(c,d)} e^{-(a+r)t}. \quad (31)$$

Substituting Eq. (31) into the kinetic Eq. (27) and integrating  $x_{II}^{(c,d,z)}$  with respect to time, it follows that

$$\begin{aligned} x_I^{(c,d,z)}(t) &= \lambda z^{(c,d)} + a\kappa z^{(c,d)} \left( \frac{1 - e^{-(a+r)t}}{a+r} \right) \\ &+ b\kappa^2 (z^{(c,d)})^2 \left( \frac{1 - e^{-2(a+r)t}}{2(a+r)} \right). \end{aligned} \quad (32)$$

An example of the temporal evolution of lesions in a cell is depicted in Figure 2.



**FIGURE 2 |** Time evolution of  $x_I$  and  $x_{II}$  damages for a single instantaneous irradiation as described by Eqs (31) and (32), respectively (A). Generalization of the temporal evolution for any time structured irradiation as describe in Sections 3.7 and 3.8.1. The dotted vertical lines represent the energy deposition events in the cell nucleus due to the passage of ionizing particles (B). Figure from [71].

It is important to remark that the exponential decay in Eq. (32) derives from the assumption of first order repair kinetics and that it could likely represents an approximation of more complex repair kinetics present in the real cell [72–75]. Postulating that the total number of lesions  $x_I(t) + x_{II}(t) \sim N_{DSB}(t)$  describes specifically the number of double strand breaks (DSBs) in the DNA, the repair kinetics represented in Eq. (32) can be verified through H2AX phosphorylation mapping experiments ( $\gamma$ -H2AX) [76, 77]. In the case of high-LET particle irradiation, such as carbon ions, the presence of a plateau (offset) in the observed  $N_{DSB}(t)$  [75, 78, 79] suggests the presence of irreparable complex clustered damage that can be related directly to the parameter  $\lambda$  of the kinetic equations and hence to the linear parameter  $\alpha_0$  of the macroscopic cell survival LQ formulation that will be introduced in the following (see Eqs 35 and 39).

In order to connect the above explicit solution of Eqs (31) and (32), i.e., the average number of type I and II lesions given a certain energy deposition  $z^{(c,d)}$ , to the survival probability, one more fundamental assumption must be made:

- (7) The lethal lesion distribution given a specific energy  $z$  follows a Poisson distribution.

Under the Poisson distribution assumptions stated above, the probability that the domain  $d$  does not contain a lethal lesion at time  $t \rightarrow \infty$  when exposed to the specific energy  $z^{(c,d)}$ , denoted by  $s^{(c,d)}(z^{(c,d)})$ , can be computed as the probability that the random outcome of a Poisson random variable is null. Therefore,  $s^{(c,d)}$  is given by

$$s^{(c,d)}(z^{(c,d)}) = e^{-\lim_{t \rightarrow \infty} x_I^{(c,d,z)}(t)}. \tag{33}$$

Using Eq. (32), it can be seen that the average number of lethal lesion given  $z^{(c,d)}$  as  $t \rightarrow \infty$  can be computed as

$$\lim_{t \rightarrow \infty} x_I^{(c,d,z)}(t) = \left( \lambda + \frac{a\kappa}{a+r} \right) z^{(c,d)} + \frac{b\kappa^2}{2(a+r)} (z^{(c,d)})^2, \tag{34}$$

so that the log-survival for the domain  $d$  is given by

$$\log s^{(c,d)}(z^{(c,d)}) = -Az^{(c,d)} - B(z^{(c,d)})^2, \tag{35}$$

with  $A$  and  $B$  defined as

$$A = \left( \lambda + \frac{a\kappa}{a+r} \right), \quad B = \frac{b\kappa^2}{2(a+r)}. \tag{36}$$

We remark that these constants are independent of the domain  $d$  and specific energy  $z^{(c,d)}$  in the domain  $d$ .

Indicating with  $S_n^{(c)}(z_n^{(c)})$  the probability of the reproductive survival of the cell  $c$  that has received exactly a specific energy  $z_n^{(c)}$  in the nucleus, the log-survival of this quantity,  $-\log S_n^{(c)}(z_n) = x_{I,n}^{(c)}(z_n)$ , represents the expected number of lethal lesions in the whole cell nucleus and can be therefore evaluated by summing of the single-domain log-survival  $-\log s^{(c,d)}(z) = x_I^{(c,d)}(z)$  over all the domains of the cell or, equivalently, by formally using the average of this quantity over the domains. Assuming that the probability density function of specific energy is the same over all domains and cell, we can drop the index  $c$  and  $d$  and use Eq. (15) to write

$$\begin{aligned} \log S_n(z_n) &:= -x_{I,n}(z_n) \\ &= -N_d \langle x_I(z) \rangle_d = -N_d \langle \log s(z) \rangle_d \\ &= -N_d (A \langle z \rangle_d + B \langle z^2 \rangle_d) \\ &= -N_d A \int_0^\infty z f(z; z_n) dz - N_d B \int_0^\infty z^2 f(z; z_n) dz, \end{aligned} \tag{37}$$

where  $f(z; z_n)$  denotes the probability density of  $z$  in a domain for a cell with a mean specific energy in the nucleus  $z_n$ . In particular, as shown in Section 2, the following holds:

$$z_n = \langle z \rangle_d = \int_0^\infty z f(z; z_n) dz. \tag{38}$$

Using Eqs (11) and (12) derived in Section 2, the log survival in Eq. (37) can be written as

$$\log S_n(z_n) = -(\alpha_0 + z_D \beta_0) z_n - \beta_0 (z_n)^2, \tag{39}$$

with  $\alpha_0 := N_d A$  and  $\beta_0 := N_d B$ . Also,  $z_D$  is the dose-averaged  $z$  per event in a domain, obtained from Eq. (12) applied to the domain (compare for reference Eq. 24 of the TDRA).

Notice that in Eq. (37), we have used the notation  $f(z; z_n)$  to denote the *multi-event distribution*, rather than  $f(z; \lambda_n)$ , as done in Section 2. This is due to the fact that, since the following relation holds true,

$$\lambda_n = \frac{z_n}{z_F}, \tag{40}$$

we have preferred to specify the dependence upon the *multi-event distribution* average.

In order to obtain the cell survival  $S(D)$  for a population of cells irradiated with macroscopic dose  $D$ , the quantity  $S_n(z_n)$  defined in Eq. (37) should be averaged accounting for the distribution of the specific energy  $z_n$  over the cell population. In terms of the logarithm of the cell population survival,  $\log S$ , under again the assumption that all the cells have the same probability distribution of specific energy  $z_n$ , this can be written as

$$\begin{aligned} \log S(D) &:= \log \langle S_n(z_n) \rangle_c \\ &= \log \left( \int_0^\infty S_n(z_n) f_n(z_n; D) dz_n \right), \end{aligned} \tag{41}$$

where similar to above, we have denoted by  $f_n(z_n; D)$  the probability density of  $z_n$  for a macroscopic absorbed dose  $D$  over the cell population, i.e.,

$$D = \langle z_n \rangle_c = \int_0^\infty z_n f_n(z_n; D) dz_n. \tag{42}$$

We remark that Eq. (41) is fundamentally different from Eq. (37) since it considers the average of the argument of the logarithm, whereas in Eq. (37), the average of the logarithm has been taken. This basically indicates that, due to the stochastic nature of  $z_n$ , the distribution of lethal lesions  $\log S_n(z_n)$  over the cell population is in general non-Poisson and hence that the log of the survival cannot be directly related to the average number of lethal lesions per cell,  $\log S(D) \neq -\langle x_{I,n}(z_n) \rangle_c$ . However, provided that the variance of  $z_n$  is small, a Poisson approximation is assumed and the same procedure used to obtain Eq. (37) can be used. In this approximation, Eq. (41) can be written as follows:

$$\begin{aligned} \log S(D) &= \log \langle S_n(z_n) \rangle_c \\ &\approx -\langle x_{I,n}(z_n) \rangle_c = \langle \log S_n(z_n) \rangle_c \\ &= \int_0^\infty \log(S_n(z_n)) f_n(z_n; D) dz_n \\ &= -(\alpha_0 + (z_D + z_{n,D}) \beta_0) D - \beta_0 D^2, \end{aligned} \tag{43}$$

with  $z_{n,D}$  the dose-averaged  $z_n$  in the nucleus per event. All the quantities  $z_{n,D}$ ,  $z_D$ , and  $z_n \approx \langle z_n \rangle_c = D$  are assumed to be the same for each cell or domain. All other notations are used as previously introduced. Since the size of the domain is usually much smaller

than the size of the nucleus, it holds that  $z_{n,D} \ll z_D$  (see [67]) so that we eventually obtain

$$\log S = -\alpha_P D - \beta D^2, \tag{44}$$

with

$$\alpha_P := \alpha_0 + z_D \beta_0, \quad \beta := \beta_0. \tag{45}$$

where the subscript P indicates that the relationships hold when the assumption of Poisson distribution of lethal lesions among the irradiated cell population is reasonable, i.e., for low-LET irradiation, as it is discussed in the following section.

A further refinement of the MKM kinetic equations involves a fourth type of possible interaction that happens at time  $t_r$ . The following is assumed:

- (8) After a time  $t_r > 0$ , all the remaining sub-lethal lesions are automatically transformed into lethal lesions.

The mathematical formulation of the main kinetic equations remain the same as in Eqs (27)–(32) in the time interval  $t \in [0, t_r)$ . As soon as  $t_r$  passes, all type II lesions that have not been either repaired or converted into type I lesion, will immediately be converted into type I lesions, meaning

$$x_{II}(t) = 0, \quad t > t_r. \tag{46}$$

The solution for the average number of type I lesions can be now explicitly found for  $t > t_r$ , adding all type II lesions that persisted after  $t_r$  passes, that is,

$$x_I^{(c,d,z)}(t) = x_I^{(c,d,z)}(t) + x_{II}^{(c,d,z)}(t_r), \tag{47}$$

so that we obtain

$$\begin{aligned} \lim_{t \rightarrow \infty} x_I^{(c,d,z)}(t) &= \lim_{t \rightarrow \infty} x_I^{(c,d,z)}(t) + x_{II}^{(c,d,z)}(t_r) \\ &= \left( \lambda + \frac{a\kappa}{(a+r)} + \frac{\kappa r}{(a+r)} e^{-(a+r)t_r} \right) z^{(c,d)} \\ &\quad + \frac{b\kappa^2}{2(a+r)} (1 - e^{-2(a+r)t_r}) (z^{(c,d)})^2. \end{aligned} \tag{48}$$

Proceeding as above, taking therefore the average over all cell domains and cell population, we obtain the generalization of Eq. (44) to be

$$\log S = -\alpha D - \beta D^2, \tag{49}$$

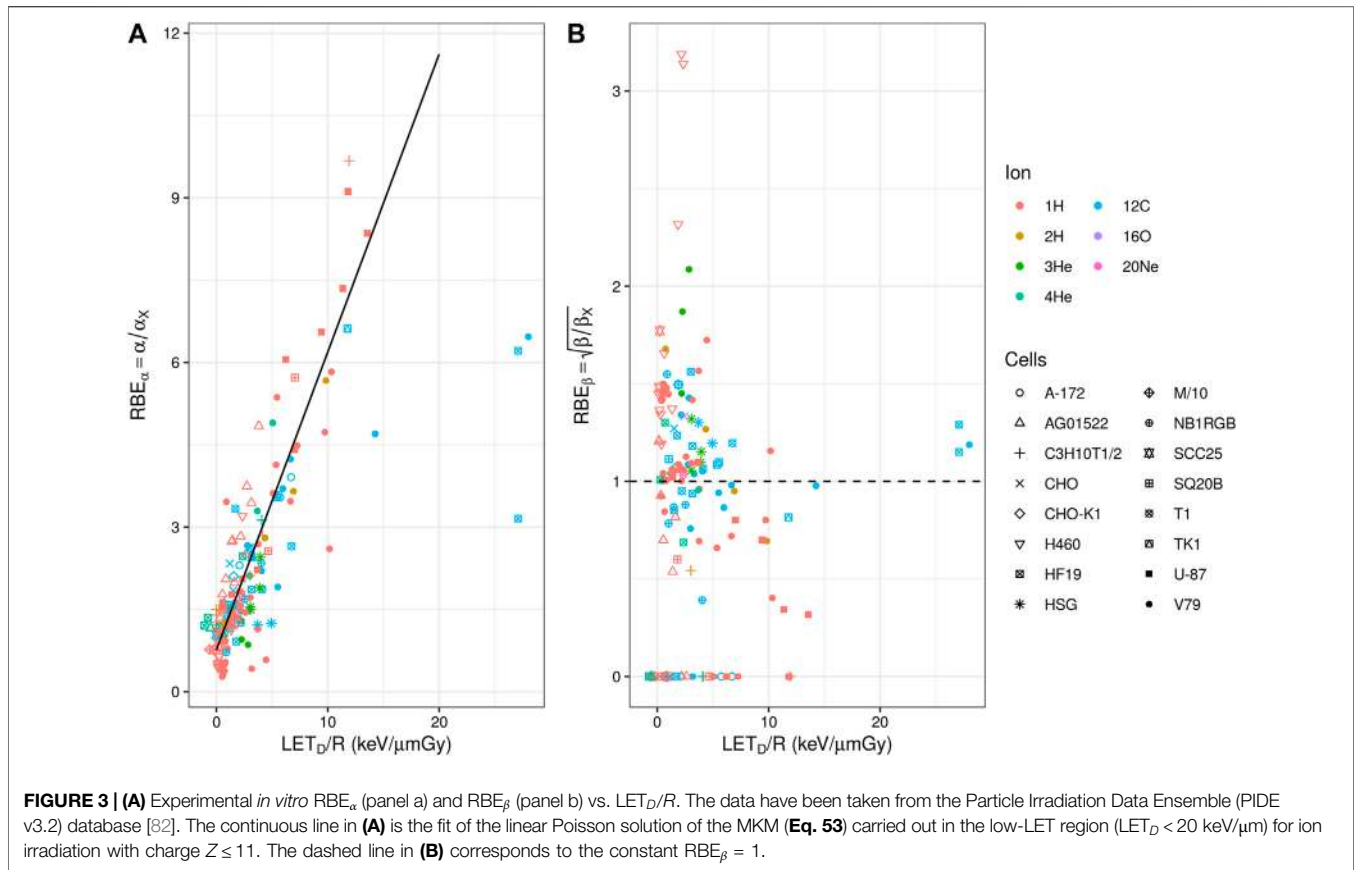
with

$$\left\{ \begin{aligned} \alpha &:= \bar{\alpha}_0 + z_D^{(c,d)} \bar{\beta}_0, \quad \beta := \bar{\beta}_0 \\ \bar{\alpha}_0 &:= N_d \left( \lambda + \frac{a\kappa}{(a+r)} + \frac{\kappa r}{(a+r)} e^{-(a+r)t_r} \right), \\ \bar{\beta}_0 &:= N_d \frac{b\kappa^2}{2(a+r)} (1 - e^{-2(a+r)t_r}). \end{aligned} \right. \tag{50}$$

### 3.3 Link to the Radiobiological Observables

From Eqs (44) and (45), it is possible to obtain the direct link of the model to the phenomenological LQ formulation of the cell





survival. The  $\alpha$  coefficient is therefore explicitly dependent on the radiation quality through a single term, the dose-averaged specific energy per event  $z_D$ , that can be related to microdosimetric measurements (Eq. 19). It has to be noted that, in this formulation of the MKM, there is no explicit dependence to the radiation quality in the quadratic coefficient  $\beta_0$  that is considered constant analogously to the result of the TDRA [57]. The latter is an approximation of the model that is in contrast with experimental observations [80–82] although in many cases, considering in particular the experimental uncertainties associated to the  $\beta_0$  determination (see for example Figure 3), and it is assumed to be reasonable. In an evolution of the model which accounts for the stochastic aspects of the irradiation, as described in Section 3.8, this approximation will be relaxed and the  $\beta$  coefficient will be considered dependent on the quality of the radiation.

From the knowledge of the LQ parameters, it is possible to derive the dose ( $D$ ) and radiation quality ( $z_D$ ) dependent RBE [83, 84]:

$$RBE(D, z_D) = \frac{R}{2D} \left( -1 + \sqrt{1 + \frac{4}{R} \left( RBE_\alpha(z_D)D + \frac{(RBE_\beta D)^2}{R} \right)} \right), \quad (51)$$

where  $R = \alpha_X/\beta_X$ ,  $RBE_\alpha(z_D) = \alpha(z_D)/\alpha_X$ , and  $RBE_\beta = \sqrt{\beta/\beta_X}$ , and  $\alpha_X$  and  $\beta_X$  are the phenomenological LQ coefficient for the photon reference radiation.

Since the parameters  $\alpha_0$  and  $\beta_0$  are assumed to be independent on the radiation quality and  $\beta = \beta_0$ , it is possible to identify  $\alpha_0 = \alpha(LET \rightarrow 0)$  and  $\beta_0 \approx \beta_X$  ( $RBE_\beta \approx 1$ ).

In the case of LET low enough that lethal lesions are Poisson distributed, it is possible to write

$$RBE_\alpha = \frac{\alpha_P}{\alpha_X} = \frac{\alpha_0}{\alpha_X} + \frac{\beta_0 z_D^{(c,d)}}{\alpha_X} \approx \frac{\alpha_0}{\alpha_X} + \frac{1}{R} z_D, \quad (52)$$

where the ratio  $R$  can be derived from a nonlinear regression analysis of measured cell survival data for a low-LET reference radiation. Equation (52) can be generalized as

$$RBE_\alpha = k_1 + \frac{k_2}{R} z_D, \quad (53)$$

where  $k_1$  and  $k_2$  are phenomenological parameters. Since  $z_D$  is proportional to the dose-averaged lineal energy  $y_D$  (Eq. 19), Eq. (53) is analogous to the linear RBE models based on the dose-averaged LET ( $LET_D$ ) used for protons [7–10]. Following the MKM model premises, Eq. (53) could also be generally used for other ions to describe the linear growth of the RBE as a function of the  $y_D$  (or  $LET_D$ ) in the low-LET region (see Figure 3). However, the linear dependence on the LET fails to be adequate in the region of mid- and high-LET as found in experimental studies [82]. In these regions, further corrections to the MKM are used to reproduce the experimental observations. Different corrective approaches

for high-LET irradiation are described in the following sections.

### 3.4 Non-Poisson Correction

In the approximation introduced in Eq. (43), it is assumed that the variance of the specific energy  $z_n$  among cells is sufficiently small. In this assumption, the number of lethal events follows the same Poisson distribution in each cells, with average  $x_{n,I}$ .

However, in general, the specific energy observed in the cell is a stochastic quantity that varies from cell to cell, bringing also a deviation from the Poisson distribution when considering the whole population of irradiated cells. We remark that this deviation is present even if the radiation is perfectly mono-energetic. In this case, the variance of the specific energy  $z_n$  arises from the fluctuation of the number of particles that are hitting the cells. The fluctuations are particularly relevant when the LET of the particle is relatively high since, given a macroscopic dose  $D$ , the average number of high-LET particles interacting with the cell is lower than the number of low-LET particles. To account for the non-Poisson distribution of the lethal events, a correction to the MKM has been introduced by Hawkins in 2003 [19], bringing a deviation from the linear behavior of the RBE vs. LET, described in Eq. (52), in the high-LET region.

The effect of the non-Poisson distribution of lethal lesions is considered by explicitly evaluating the fraction of hit and non-hit cell nuclei. Considering a high-LET irradiation in the limit of very low dose,  $D \rightarrow 0$ , the probability for a cell to interact with more than one particle is negligible. In this case, the population of cells can be subdivided in a fraction  $\Phi$  of cells that suffer a single particle interaction and a fraction  $1 - \Phi$  of cells with zero interactions.

A further approximation is assumed in order to match the request of still having a Poisson distribution in the population of hit cells: only a single well defined value of  $z_n = z_{n,D}$  is observed when the particle hits the cell. Generally, this is not the case and the specific energy can also vary due to energy straggling and the random impact parameter of the particle with respect to cell nucleus. This assumption can be reasonable when low energy particles with high LET (see also Section 3.6) are considered.

We denote with  $x_{I,n}(z_{n,D})$  the average number of type I lethal lesions in the fraction  $\Phi$  of cells whose sensitive nucleus has been hit by a single particle imparting exactly a specific energy  $z_{n,D}$  in the nucleus. Then, recalling Eq. (39), we obtain

$$x_{I,n}(z_{n,D}) = -\log S(z_{n,D}) = (\alpha_0 + z_D \beta_0) z_{n,D} + \beta_0 z_{n,D}^2. \quad (54)$$

It is possible to explicitly write the global surviving fraction of cells (including both hit and non-hit nuclei) as

$$S(D) = (1 - \Phi) + \Phi e^{-x_{I,n}(z_{n,D})}. \quad (55)$$

This corresponds to consider a probability density function  $f_n(z_n; D) = (1 - \Phi)\delta(z_n) + \Phi\delta(z_n - z_{n,D})$  in Eq. (41). Since the number of lethal lesions per cell averaged over the whole cell population (including both hit and non-hit nuclei) exposed to the macroscopic dose  $D$  can be directly evaluated as

$$\langle x_{I,n}(z_n) \rangle_c = \Phi x_{I,n}(z_{n,D}), \quad (56)$$

Equation (55) can be rewritten as

$$\begin{aligned} S(D) &= 1 + \frac{\langle x_{I,n}(z_n) \rangle_c}{x_{I,n}(z_{n,D})} (e^{-x_{I,n}(z_{n,D})} - 1) \\ &= 1 + \left[ \frac{e^{-(\alpha_0 + z_D \beta_0) z_{n,D} - \beta_0 z_{n,D}^2} - 1}{(\alpha_0 + z_D \beta_0) z_{n,D} + \beta_0 z_{n,D}^2} \right] ((\alpha_0 + \beta_0 z_D) D + \beta_0 D^2). \end{aligned} \quad (57)$$

Notice that, in the last passage, we exploited Eq. (43) in order to evaluate the average  $\langle x_{I,n}(z_n) \rangle_c$  as an explicit function of the dose. Taking the log of  $S$ , expanding around  $D = 0$  and dropping terms in  $D^2$  or higher powers, the linear term of  $\log S(D)$  can be written as

$$-\log S(D)|_{D \rightarrow 0} \approx (\alpha_0 + z_D \beta_0) \left( \frac{1 - e^{-(\alpha_0 + z_D \beta_0) z_{n,D} - \beta_0 z_{n,D}^2}}{(\alpha_0 + z_D \beta_0) z_{n,D} + \beta_0 z_{n,D}^2} \right) D. \quad (58)$$

The explicit non-Poisson  $\alpha$  coefficient is then derived from Eq. (58) and can be formulated as a correction to  $\alpha_p$  (defined in Eq. 45) as

$$\begin{aligned} \alpha_{NP} &= \alpha_p \left( \frac{1 - e^{-\alpha_p z_{n,D} - \beta_0 z_{n,D}^2}}{\alpha_p z_{n,D} + \beta_0 z_{n,D}^2} \right) \\ &\approx (1 - \exp(-\alpha_p z_{n,D})) \left( \frac{1}{z_{n,D}} \right), \end{aligned} \quad (59)$$

where following also the original formulation of Hawkins [19], in the last passage, the quadratic terms  $z_{n,D}^2 \ll z_{n,D}$  were also neglected. According to Hawkins, one can also approximate  $z_{n,D} \propto \text{LET}_{\infty}/A$ , where  $\text{LET}_{\infty}$  is the unrestricted linear energy transfer in  $\text{keV}\mu\text{m}^{-1}$  of the incident particle and  $A$  is the area of the cell nucleus in  $\mu\text{m}^2$ , assuming  $\rho = 1 \text{ g cm}^{-3}$  for the density of water. By assuming  $A = \pi R_n^2$ , Eq. (59) becomes

$$\alpha_{NP} \approx \left( 1 - \exp\left(-\alpha_p \frac{\text{LET}_{\infty}}{\rho \pi R_n^2}\right) \right) \left( \frac{\rho \pi R_n^2}{\text{LET}_{\infty}} \right). \quad (60)$$

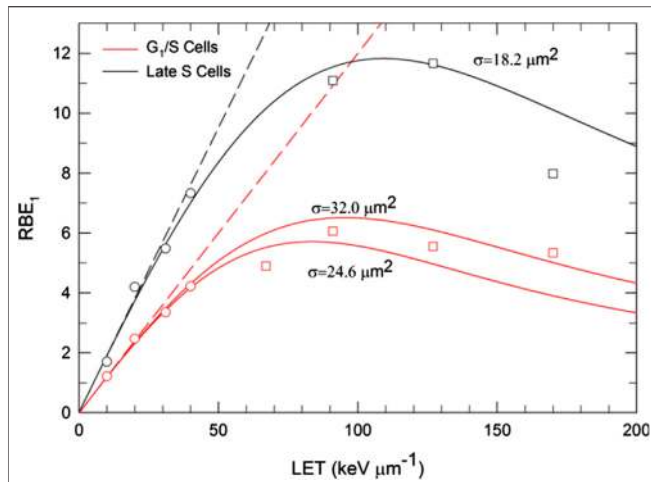
No correction is considered for the  $\beta$  coefficient and it is still assumed to be independent on the energy and particle type.

The non-Poisson correction to the RBE in the limit of zero dose ( $\text{RBE}_{\alpha}$ ) is given by

$$\text{RBE}_{\alpha, NP} = \frac{\alpha_{NP}}{\alpha_X} = \left( \frac{1 - e^{-\alpha_p z_{n,D}}}{\alpha_p z_{n,D}} \right) \text{RBE}_{\alpha, p}, \quad (61)$$

with  $\text{RBE}_{\alpha, p}$  given by Eq. (52). No corrections are applied to the  $\text{RBE}_{\beta}$ , that is still assumed constant ( $\text{RBE}_{\beta} \sim 1$ ) and independent on the quality of the radiation.

The correction causes the  $\text{RBE}_{\alpha}$  to be less than indicated by the extrapolation of the linear relationship (Eq. 53) to higher LET and to pass through a maximum in the range of LET of 50–150  $\text{keV}/\mu\text{m}$ . This behavior is compatible with several experimental studies from the literature [82] and it shows also a sensitivity of the maximum of the RBE to the response of the cell



**FIGURE 4 |** Comparison of MKM estimates of particle  $RBE_{\alpha}$  to experimental values for V79 cells. Red curves show  $RBE_{\alpha}$  for cells synchronized at G1-S transition for cross sections of  $\sigma = 32.0 \mu\text{m}^2$  (reference radiation: 250 kVp X-rays,  $\alpha_R = 0.234 \text{ Gy}^{-1}$ , and  $\beta_R = 0.042 \text{ Gy}^{-2}$ ). Black curve shows  $RBE_{\alpha}$  for cells synchronized in late S phase for cross sections of  $\sigma = 18.2 \mu\text{m}^2$  (reference radiation: 250 kVp X-rays,  $\alpha_R = 0.064 \text{ Gy}^{-1}$ , and  $\beta_R = 0.0165 \text{ Gy}^{-2}$ ). Dashed lines represent  $RBE_{\alpha} = 0.02 + 0.19 \times \text{LET}$  in the Poisson regime. Experimental data are from [86, 87], plot taken from [26].

at low-LET, related to the parameter  $R = \alpha_X/\beta_X$  [85]. An exemplification of the RBE behavior and the prediction of the model is reported in **Figure 4**.

We remark that, while the non-Poisson correction factor associated to the linear parameter  $\alpha$  is derived in the limit  $D \rightarrow 0$  (and, by definition, it is independent on the dose), the non-Poisson concept of Hawkins’s correction is in general inapplicability to a high dose irradiation, since all nuclei and domains will be hit in such irradiation. The quantity  $RBE_{\alpha}$  defined in **Eq. (61)** is hence expected to represent the relevant behavior for low doses, where the linear term is dominant and the RBE is maxed out [83, 84], whereas the correct stochastic evaluation of  $\beta$  could be critical in the study of clinical applications with high doses per fraction (see **Section 3.8**). In **Figure 5**, some qualitative implications of the non-Poisson regime in high-LET and low dose per fraction ion beam therapy are depicted.

### 3.5 The Saturation Correction

Kase et al. [20] introduced a correction factor in the MKM to account for the decrease in RBE due to the overkill effect observed in high-LET radiations (see, for example, **Figure 6**). The correction factor was applied to the dose-averaged specific energy per event,  $z_D$ , for mixed radiation field with wide-ranging spectra.

In terms of lineal energy, the corrected value of  $y_D$  (and hence  $z_D$ ) was obtained by applying a correction for each lineal energy component of the lineal energy spectrum. The correction of the components was obtained by using an empirical *saturation parameter*  $y_0$  based on the saturation correction method introduced by [89] and then used in the TDRA [58]

$$y_D^* = \frac{y_0^2 \int [1 - \exp(-y^2/y_0^2)] f(y) dy}{\int y f(y) dy} \tag{62}$$

The saturation parameter indicates the lineal energy above which the correction due to the overkill effects became important.

The correction to cell survival is then obtained by evaluating the saturation-corrected dose-averaged specific energy per event  $z_D^*$  in the domain, which can be obtained from the saturation-corrected dose-averaged lineal energy (62) using the relationships reported in **Eqs (12)** and **(19)**:

$$z_D^* = \frac{\bar{l}_d}{m_d} y_D^* = \frac{y_D^*}{\rho \pi r_d^2} \tag{63}$$

where  $\rho$ ,  $r_d$ ,  $\bar{l}_d$ , and  $m_d$  are the density, radius, mean cord length, and mass of the domain, respectively. The equation for the cell survival (**Eq. 44**) is then modified as follows:

$$-\ln(S) = (\alpha_0 + \beta_0 z_D^*) D + \beta_0 D^2 \tag{64}$$

Considering the linear term in the macroscopic dose  $D$ , the corrected  $\alpha^*$  coefficient is hence

$$\alpha^* = (\alpha_0 + \beta_0 z_D^*) \tag{65}$$

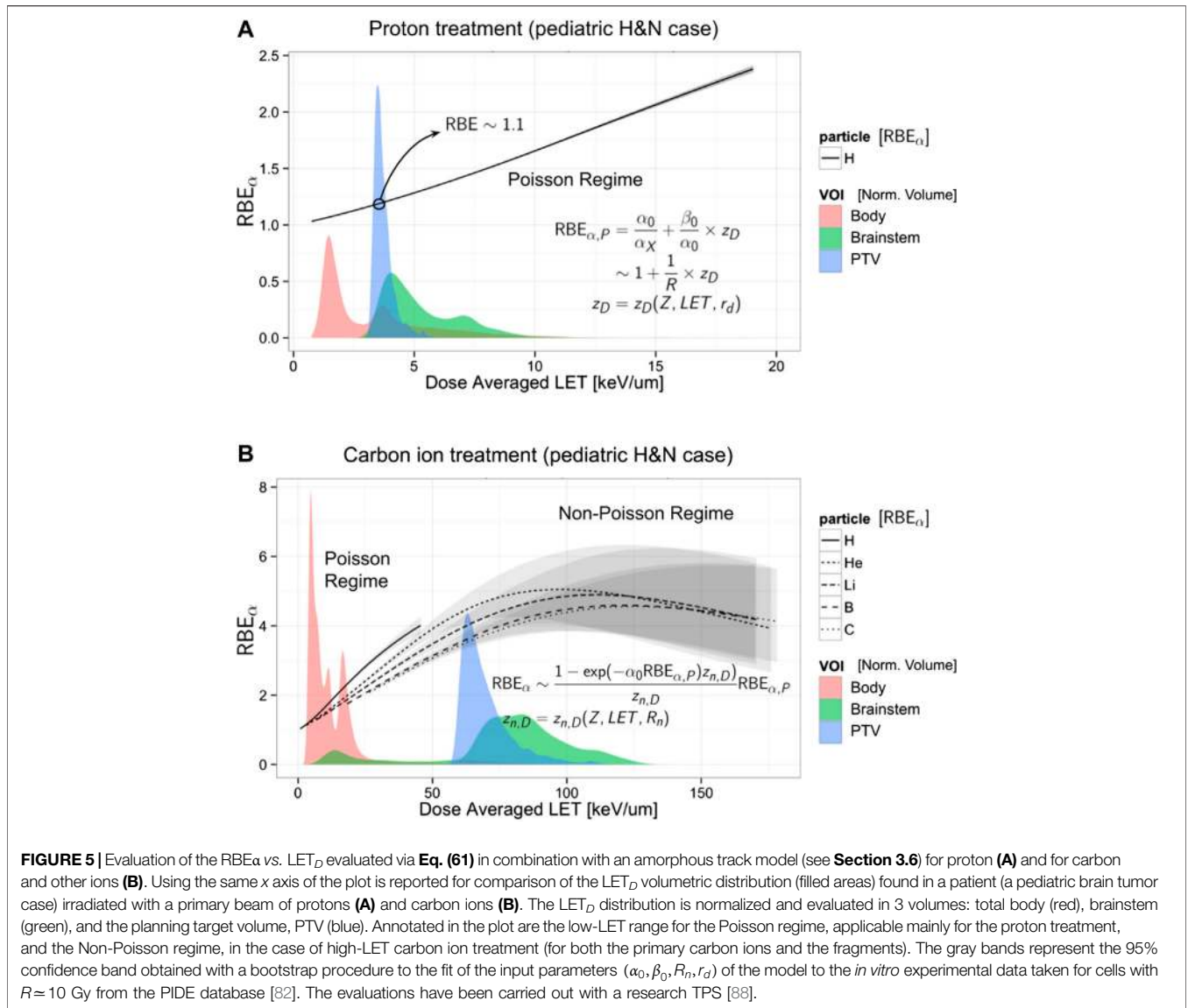
No correction is considered for the  $\beta$  coefficient and it is still assumed to be independent on the energy spectrum.

An example of the prediction by MKM modified with the saturation correction compared with experimental data is reported in **Figure 6**, where the  $\alpha$  vs.  $y_D$  for HSG cells irradiated with carbon ions is shown. It is interesting to note, by comparing **Eqs (59)** and **(65)**, that the saturation correction can be considered an alternative way to describe the non-Poisson correction defined in **Section 3.4**, since both factors modulate the behavior of  $RBE_{\alpha}$  in similar ways (see also **Figure 4**). In particular, it was shown in [20] that in the case of mono-energetic spectra, **Eqs (58)** and **(65)** are functionally equivalent for  $y < 500 \text{ keV}/\mu\text{m}$ . Thus, by matching these equations in the limit of low LET ( $y_D \rightarrow 0$ ), and defining  $z_{n,D} = y_D/\rho\pi R_n$ , with  $R_n$  the radius of the nucleus, analogously to **Eq. (63)** for the domain, it is possible to link the saturation correction parameter  $y_0$  with the other parameters of the model

$$y_0 = \frac{\rho \pi r_d R_n^2}{\sqrt{\beta_0 (r_d^2 + R_n^2)}} \tag{66}$$

A typical used value of the saturation parameter was  $y_0 = 150 \text{ keV}/\mu\text{m}$  [20, 36].

Other quantities that one needs to determine for the RBE evaluations are the lineal energy spectra, obtainable with a microdosimeter detector such as TEPC [43] and the values of  $\alpha_0$ ,  $r_d$ , and  $R_N$  from which the correction to the  $y_D^*$  is calculated. The  $\alpha_0$  and  $r_d$  coefficients can be extrapolated experimentally from the initial slope of the survival curves (**Eq. 65**) for low-LET irradiation (in the limit of  $y_D \rightarrow 0$  and  $D \rightarrow 0$ )



$$r_d = \sqrt{\frac{\beta(y_D - (y_D)_X)}{\rho\pi(\alpha - \alpha_X)}} \tag{67}$$

$$\lim_{y_D \rightarrow 0} \alpha \equiv \alpha_0 = \alpha_X - \left( \frac{\alpha - \alpha_X}{y_D - (y_D)_X} \right) (y_D)_X,$$

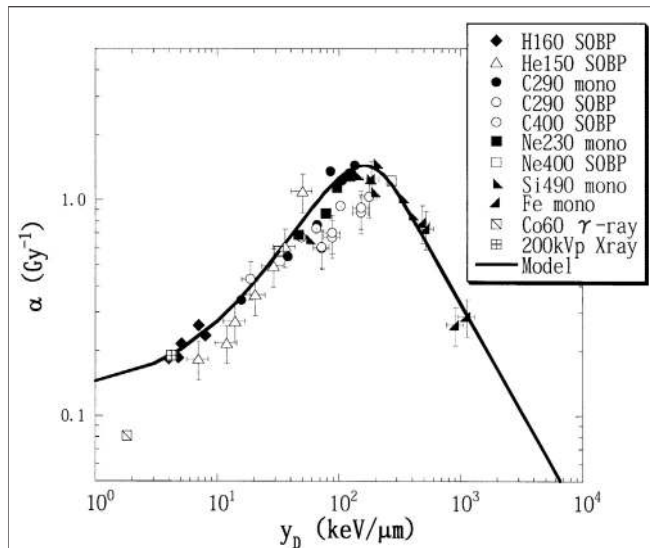
where  $\rho = 1.0 \text{ g/cm}^3$ ,  $\alpha_X$  is the LQ parameter of the X-Ray, and  $(y_D)_X$  is the dose-averaged lineal energy for X-ray irradiation.

The saturation-corrected formulation of the MKM is one of the most widely used approaches to estimate the RBE from microdosimetric measurements. Many studies have been published where the computed RBE is compared with the RBE measured along single Bragg peaks or more complex mixed field irradiations [49, 90–92]. In Figure 7, the RBE vs. depth for a proton spread-out Bragg peak is reported as an example of these assessments [92].

### 3.6 Track Structure Model Incorporation

In 2008, Kase et al. [21] introduced the usage of amorphous track structure models as an alternative numerical approach to evaluate theoretically the dose-averaged per event in the nucleus  $z_{n,D}$  and in the domain  $z_D$  for the MKM calculations. This approach has the advantage of bypassing the necessity to acquire experimental lineal energy spectra to evaluate the RBE; this approach is particularly useful when experimental spectra are not available, such as in TPS calculations. Another interesting aspect is the possibility to evince the dependence of LET-RBE curves on the ion type.

The amorphous track model adopted for the MKM calculation is based on a combination of the Kiefer model for the penumbra region [93] and the Chatterjee model for the core radius [94], introduced for explaining the responses of the diamond detector to heavy-ion beams [95]. Here, the core radius  $R_c$  ( $\mu\text{m}$ ), the penumbra radius  $R_p$  ( $\mu\text{m}$ ), and the dose  $z_{KC}$  as function of track radius  $r$  ( $\mu\text{m}$ ) are evaluated as follows:



**FIGURE 6 |** Experimental  $\alpha$  values, fitted by the linear-quadratic model from the survival curves of HSG cells value with  $\beta_0 = 0.05 \text{ Gy}^{-2}$ , as a function of the dose-averaged linear energy,  $y_D$ . The  $y_D$  were measured by the TEPC with a simulated diameter of  $1.0 \mu\text{m}$ . The solid line indicates the curve calculated using Eq. (65) with the following model parameters:  $r_d = 0.42 \mu\text{m}$ ,  $R_n = 4.1 \mu\text{m}$ ,  $\alpha_0 = 0.13 \text{ Gy}^{-1}$ , and  $\beta_0 = 0.05 \text{ Gy}^{-2}$ . Plot taken from [20].

$$R_c = 0.0116 \times \beta_{\text{ion}}, \quad (68)$$

$$R_p = 0.0616 \times (E_s)^{1.7}, \quad (69)$$

$$z_{\text{KC}}(r \leq R_c) = \frac{1}{R_c^2} \left( \frac{\text{LET}_{\infty}}{r\rho} - 2\pi K_p \ln(R_p/R_c) \right), \quad (70)$$

$$z_{\text{KC}}(r > R_c) = 1.25 \times 10^{-4} (Z^*/\beta_{\text{ion}})^2 r^{-2}, \quad (71)$$

where  $E_s$  is the specific kinetic energy in MeV/u,  $Z^*$  is the effective charge given by the Barkas expression,  $\beta_{\text{ion}}$  is the velocity relative to the speed of light,  $\text{LET}_{\infty}$  is the unrestricted LET, and  $\rho$  is the density of water;  $K_p$  is a parameter that depends only on the effective charge given with the Barkas expression and the  $\beta$  ion is the velocity relative to the light velocity [21]. In order to evaluate the dose-averaged specific energy, the domain and nucleus are assumed to have a cylindrical symmetry with the direction of the incident ion parallel to the cylinder axis. Using this geometry, it is possible to write explicitly the single-track dose-averaged specific energy (Eq. 12) for both domain and nucleus as

$$z_D = \int_0^{b_{\text{max}}} z_{\text{KC}}(b)^2 b db / \int_0^{b_{\text{max}}} z_{\text{KC}}(b) b db, \quad (72)$$

$$z_{n,D} = \int_0^{b_{\text{max}}^{(n)}} z_{\text{KC}}(b)^2 b db / \int_0^{b_{\text{max}}^{(n)}} z_{\text{KC}}(b) b db, \quad (73)$$

where  $b_{\text{max}}$  and  $b_{\text{max}}^{(n)}$  are the maximum impact parameters to have a non-negligible energy deposition in the domain and in the nucleus, respectively. These parameters, or equivalently the radius of the domain  $r_d$  and of the nucleus  $R_n$ , represent two parameters of the model. Examples of these evaluations are

shown in Figure 8. In principle,  $R_n$  can be related to direct observations while  $r_d$  does not represent a measurable quantity, since it cannot be uniquely identified with any structure in the cell or cell nucleus.  $r_d$  can be used as a free parameter to be fixed by fitting the model to the experimental survival and RBE data.

As seen in Section 3.4, in the case of high LET irradiation, the  $z_D$  value is comparably very large with respect to the  $(z_D)_X$  evaluated for photon; consequently, from Eq. (36),  $\alpha_0$  and  $\beta_0$  can be approximated with the experimental  $\alpha_X$  and  $\beta_X$ . An example of the model evaluations compared to the experimental data is reported in Figure 9.

Interestingly, the explicit usage of a track model shows how some aspects of the MKM are conceptually similar to that of the LEM [11–17]. In both MKM and LEM, the principal target is the cell nucleus for any radiation quality, the nucleus is divided into small independent sub-volumes (infinitesimal volumes in the case of LEM and domains in the case of MKM), and a cell survival curve for X-rays is adopted as the local dose-effect curve of each sub-volume. Finally, the summation of the local effect in all sub-volumes over the whole nucleus determines the cell survival probability.

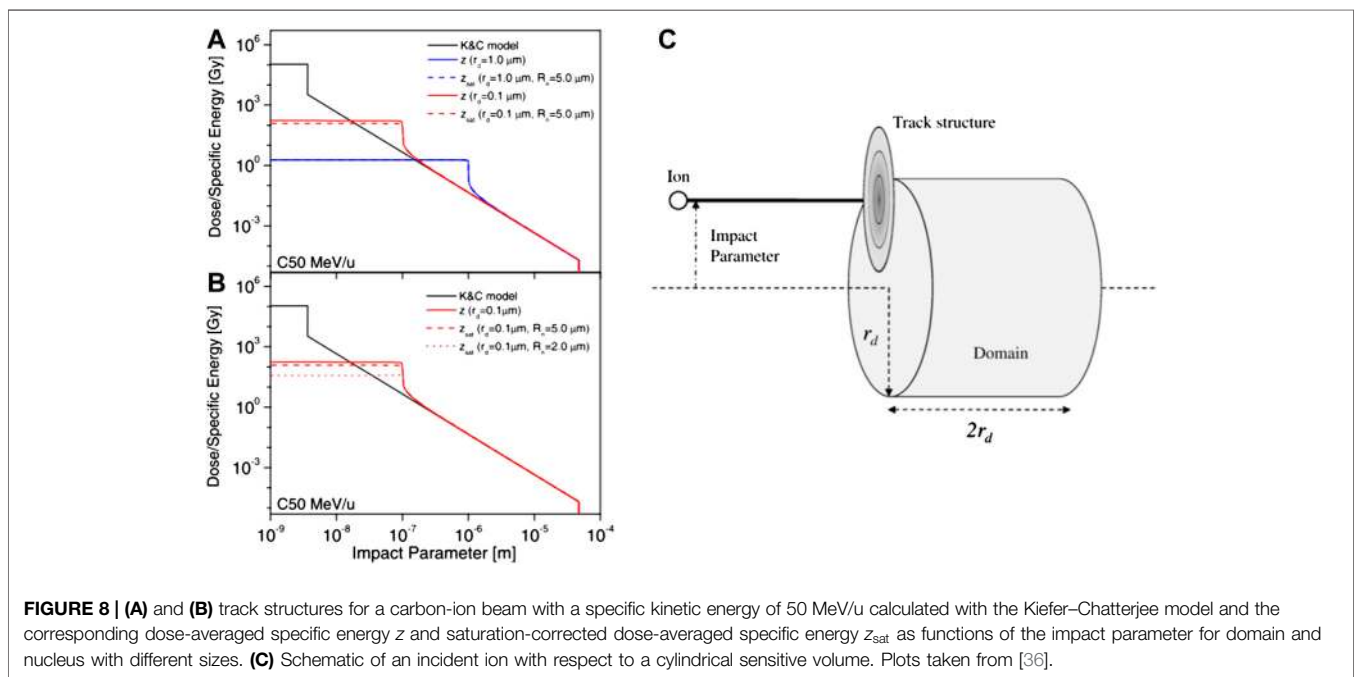
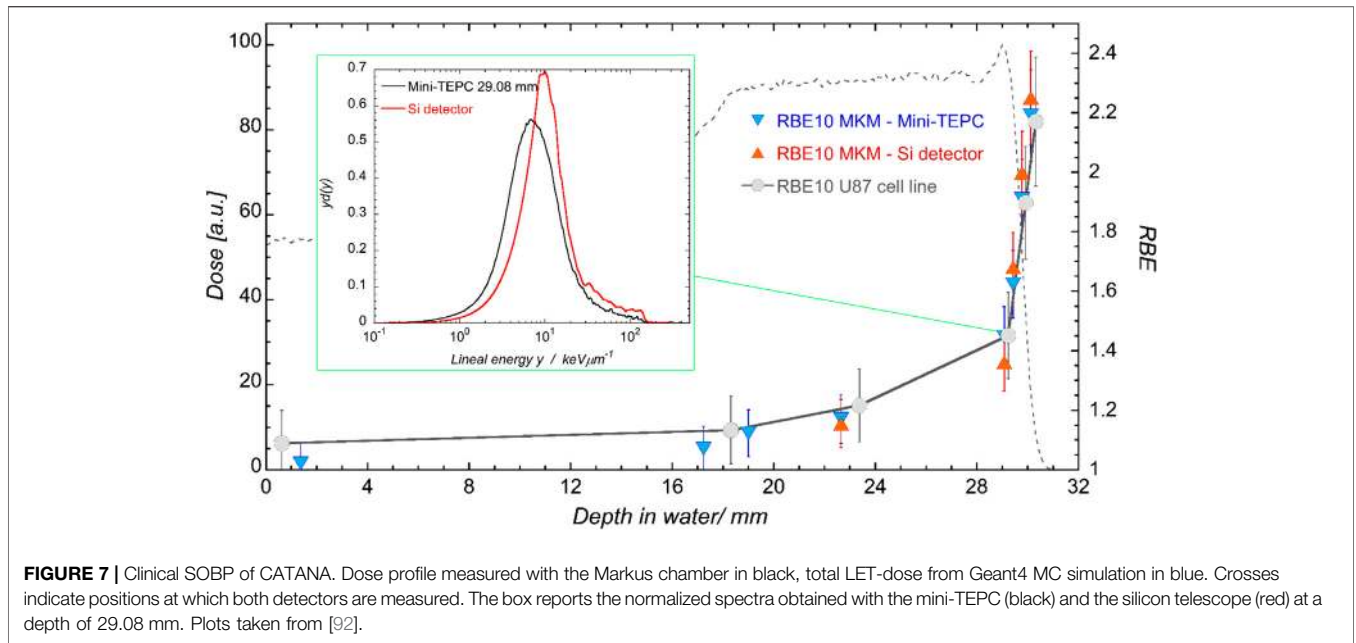
The inclusion of the amorphous track model allows to evaluate directly  $z_D$  and  $z_{n,D}$  without the necessity to obtain these values by extrapolating them from microdosimetric measurements via scaling relationships such as Eq. (19). This aspect can be particularly advantageous for some applications where these spectra are generally not easily or partially available such as in the simulation and optimization of treatments in TPS applications, where the biological effect should be evaluated in the whole irradiated 3-D patient volume.

At present, the MKM is implemented in the proton and carbon ion TPS used clinically at the National Institute of Radiological Sciences (NIRS) in Japan to evaluate the RBE and the RBE-weighted dose optimized for the individual patients. The computation method, developed by Inaniwa et al. [36, 96], takes advantage of the incorporation of the amorphous track model in combination with the saturation-corrected dose-averaged approach developed by Kase et al. [20] described in Section 3.5, for evaluations in case of mixed field irradiation. In the TPS implementation, a set of pre-calculated look-up tables of the saturation corrected specific energies for mono-energetic beams are created using a generalization of Eqs (72), (73) where the saturation effect is explicitly included for the dose-averaged specific energy for the domain

$$z_D^* = \int_0^{b_{\text{max}}} z_{\text{sat}}(b) z_{\text{KC}}(b) b db / \int_0^{b_{\text{max}}} z_{\text{KC}}(b) b db \quad (74)$$

and equivalently for the nucleus, where  $z_{\text{sat}}$  is the saturation-corrected specific energy

$$z_{\text{sat}}(b) = \frac{z_0^2}{z_{\text{KC}}(b)} \left( 1 - \exp\left(-\frac{z_{\text{KC}}(b)^2}{z_0^2}\right) \right), \quad (75)$$



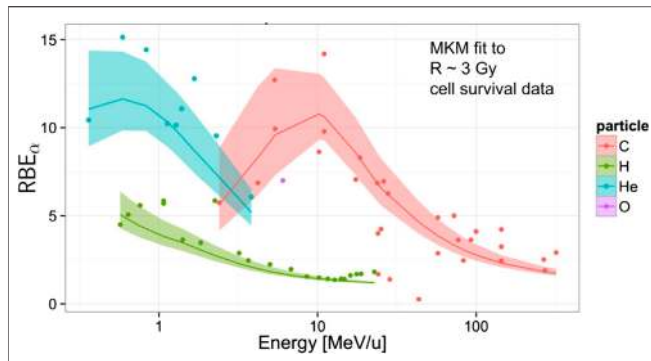
with saturation coefficient  $z_0 = y_0 (\bar{l}_d/m_d)$  (see Eq. 66) evaluated in the cylindrical geometry (see also panel (c) of Figure 8). The effect of the mixed-field of the treatment at a position is hence evaluated through a dose-weighted linear combination

$$(z_{D,mix}^*)_i = \frac{\sum_{j=1}^{N_b} D_{ij} (z_{D,ij}^*)_i}{\sum_{j=1}^{N_b} D_{ij}}, \quad (76)$$

where  $N_b$  is the number of beams of the treatments,  $D_{i,j}$  is the dose released at position  $i$  by the beam  $j$ , and

$$(z_D^*)_{ij} = \frac{\sum_{k=1}^{N_{ij}} e_k (z_{D,k}^*)_{ij}}{\sum_{k=1}^{N_{ij}} e_k} \quad (77)$$

is the saturation-corrected dose-averaged specific energy of the domain of cells at position  $i$  delivered by the  $j$ -th beam, obtained through the sum of mono-energetic evaluations,  $(z_{D,k}^*)_{ij}$ , described in Eq. (74), where  $k$  is an index of the deposition events and the sum is performed from 1 to  $N_{ij}$ , the observed number of the deposition events in cell  $i$  delivered by the  $j$ -th beam.



**FIGURE 9 |** Global fitting of the MKM to experimental  $RBE_n$  data for different ion irradiation subsetted from the PIDE database [82] with  $R = \alpha_x/\beta_x \in [2.8, 3.2]$  Gy. The plotted points indicate the experimental results and the lines represent the MKM results calculated with the Kiefer–Chatterjee track structure model. The bands represent the 90% confidence band obtained from the MKM parameters  $\{\alpha_0, \beta_0, R_n, r_d\}$  probability distribution, evaluated through a bootstrap procedure.

To obtain the energy imparted  $e_k$  and the number  $N_{ij}$ , Monte Carlo (MC) simulations are used, taking advantage of available codes such as, for example, those derived from the Geant4 libraries [97–99] and Fluka [100].

### 3.7 The Dependence of the Biological Effect on the Dose-Rate Time Structure

One of the interesting features of the MKM, in contrast to other radiobiological models used in ion beam radiotherapy such as the LEM, is the possibility to account inherently for arbitrary time dependent dose-rates, such as protracted irradiations and fractionations. This feature derives from the explicit description of the time depending response of the cell to the irradiation through the kinetic equations (Eq. 32).

Different approaches to investigate and to model the dose-rate time effects have been carried out using the MKM as a theoretical base. Some examples of these approaches can be found in [23, 39, 67, 101–104]. In these studies, the kinetic Eq. (27) is slightly generalized to account for an arbitrary time dependent specific energy deposition rate  $\dot{z}^{(c,d)}$  in the domains:

$$\begin{cases} \dot{x}_I^{(c,d)} = \lambda \dot{z}^{(c,d)} + a x_{II}^{(c,d)} + b (x_{II}^{(c,d)})^2, \\ \dot{x}_{II}^{(c,d)} = \kappa \dot{z}^{(c,d)} - (a + r) x_{II}^{(c,d)} - 2b (x_{II}^{(c,d)})^2 \approx \kappa \dot{z}^{(c,d)} - (a + r) x_{II}^{(c,d)}, \end{cases} \quad (78)$$

where in the second equation, as described in Section 3.2, the second order process describing the pairwise combination between type II lesions has been removed since it is considered negligible if compared to the first-order process.

In [101, 104], the effects of dose-delivery time structure on the RBE in a mixed radiation field of therapeutic carbon ion beams are investigated using the modified microdosimetric kinetic model introduced by Kase et al. [20, 21, 36]. These studies evaluate the biological effect of the irradiation in two different

dose-rate conditions: a split-dose irradiation and a protracted continuous irradiation.

In the case of a *split-dose irradiation*, a population of cells is considered exposed to a macroscopic dose  $D_1$  at time  $t = 0$  and a dose  $D_2$  at time  $t = \Delta T$ , where a domain absorbs  $z_1$  and  $z_2$  from the two separate irradiations, respectively. Evaluating  $x_I$  in the limit  $t \rightarrow \infty$  by integrating Eq. (27) and using the saturation-corrected dose-averaged specific energy as given in Eq. (64), we obtain for the cell survival

$$\begin{aligned} \ln S(D, \Delta T) = & -(\alpha_0 + \beta(z_D^*)_1)D_1 - \beta D_1^2 - (\alpha_0 + \beta(z_D^*)_2)D_2 - \beta D_2^2 \\ & - 2\beta D_1 D_2 e^{-(a+c)\Delta T} \frac{1 - e^{-2(a+c)(t_r - \Delta T)}}{1 - e^{-2(a+c)t_r}}, \end{aligned} \quad (79)$$

where  $(z_D^*)_1$  and  $(z_D^*)_2$  are the saturation-corrected dose-averaged specific energy of the first and second irradiation and the total dose  $D = D_1 + D_2$ . The time parameters  $t_r$  indicate the time after which all sub-lethal lesions that are still unrepaired are fixed in lethal lesions, according to assumption (9) introduced in Section 3.2. If the quality of the radiation does not change between the two irradiations, then  $(z_D^*)_1 = (z_D^*)_2 = z_D^*$  and Eq. (79) can be simplified as

$$\begin{aligned} \ln S(D, \Delta T) = & -\alpha_0 (D_1 + D_2) - z_D^* \beta (D_1 + D_2) - \beta (D_1 + D_2)^2 \\ & + 2\beta D_1 D_2 \left[ 1 - e^{-(a+c)\tau} \frac{(1 - e^{-2(a+c)(t_r - \tau)})}{(1 - e^{-2(a+c)t_r})} \right]. \end{aligned} \quad (80)$$

The values of  $(a + c)$  and  $t_r$  can be determined by using the following approximations (see Eqs 35, 40 in [101]):

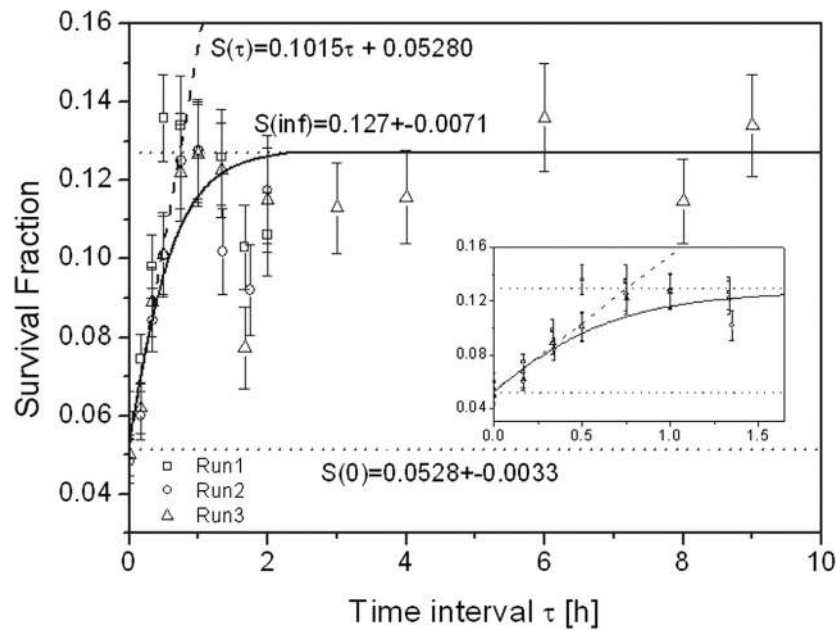
$$(a + c) \cong \frac{1}{2\beta D_1 D_2} \left[ \frac{1}{S} \frac{dS}{d\tau} \right]_{\tau=0}, \quad (81)$$

$$t_r = -\frac{\ln(\alpha/\kappa)}{(a + c)}. \quad (82)$$

In the case of a *continuous protracted irradiation*, a population of cells receive a constant macroscopic dose-rate of  $\dot{D}$  starting at time  $t = 0$  and ending at  $t = T$ . In order to carry out the evaluation, the irradiation is assumed microscopically equivalent to a number  $N$  of instantaneous irradiations with random doses to a domain delivering every infinitesimal interval. The time interval between these irradiations is  $\delta t = T/(N - 1)$ , with  $\delta t \ll 1/(a + c)$ , and each domain absorbs  $z_1, z_2, \dots, z_N$ . The number of lethal lesions per domain  $x_I$  is therefore obtained by integrating and summing the solution of Eq. (27) for each time segment. The final cell survival probability is then obtained by introducing the corresponding saturation-corrected dose-averaged specific energy in a way analogous to the split dose evaluation. In the case in which the quality of the radiation does not change with time, the final log survival is given as

$$\ln S = -(\alpha_0 + \beta_0 z_{d,D}^*)D - \beta' D^2, \quad (83)$$

where



**FIGURE 10** | Survival fraction of HSG tumor cells after exposure to two equal doses of carbon-ion beams with  $D_1 = D_2 = 2.5$  Gy separated by time interval  $\tau$  ( $\Delta T$  in the text) from 0 to 9 h. Three different series of experiments (runs) are shown. The estimated tangent at  $\tau = 0$  h is reported in dashed line, while the solid curve is the predicted survival by **Eq. (80)** with  $\beta = 0.0703 \text{ Gy}^{-2}$ ,  $\beta = 0.237 \text{ Gy}^{-2}$ ,  $(a + c) = 2.187 \text{ h}^{-1}$ , and  $t_r = 2.284$ . Plot taken from [101].

$$\beta' \equiv \beta_0 \left[ 1 - \frac{2}{N^2} \sum_{n=1}^{N-1} \left\{ (N-n) \left( 1 - e^{-\frac{(a+r)n}{N-1} T} \right) \times \frac{(1 - e^{-2(a+r)(t_r - \frac{n}{N-1} T)})}{(1 - e^{-2(a+r)t_r})} \right\} \right] \quad (84)$$

The notation used in **Eqs (83) and (84)** highlights the importance of the quadratic term  $\beta$ , which modulates the impact of the dose-rate time structure, according to the LQ interpretation of the biological effects [105–108].

It is worth remarking that these MKM-based temporal formulations of the cell survival derived from the kinetic **Eq. (78)** do not account for re-population and cell cycle redistribution. **Figure 10** reports the evaluation via **Eq. (80)** of the survival fraction of HSG cell line for various time intervals compared to experimental data. An initial rise in cell survival due to repair is visible until time interval  $\Delta T = 0.75$  h followed by a decrease in survival due to cell cycle redistribution and a rise due to re-population ( $1.4 < \Delta T < 4$  h) and by the saturation region for  $\Delta T > 4$  h. The predicted cell survival reasonably agrees with data in the first and last regions, while it does not account for re-population and redistribution. The temporal formulations described in this section have been also incorporated in the TPS used at NIRS [36] (see also **Section 3.6**) and successfully used to estimate the impact of the beam interruption in single-fractionated treatments with carbon ions for patients with prostate tumor [104].

### 3.8 Stochastic Approaches and Variable $\beta$

As discussed in the previous sections, the MKM accounts for the stochastic aspects of the induction of damage in the cell by exploiting probability theory to develop simple formulas for

the LQ coefficients of the cell survival (**Eqs 44, 45, 58, 64, and 83**). These formulations of the model are obtained introducing approximations [19] or ad-hoc corrections [20] that shows some discrepancies with experiments for high-LET irradiation, in particular in the determination of the  $\beta$  coefficient, since the measured  $\beta$  tends to decrease at very high LET [82, 109–111], while the  $\beta$  derived from the MKM is considered constant.

The disagreements in the  $\beta$  coefficient are ultimately acknowledged to be induced by the partial accounting of the stochastic nature of the specific energies in the MKM calculations that play an important role for high-LET irradiation [22]. Following these considerations, attempts to improve the model, introducing more refined approaches to account a variable  $\beta$ , have been made [22, 23, 70, 112]. In the rest of this section, some of these developments, based on improved stochastic modelings of the specific energy depositions, are described in detail.

#### 3.8.1 Monte Carlo-Based Evaluations

A method to account in a natural and straightforward way the inherent stochastic nature of the irradiation is to implement a Monte Carlo algorithm in the MKM, as recently shown by Manganaro et al. [23, 113] in their formulation of the model named MCt-MKM (Monte Carlo temporal microdosimetric kinetic model). The implemented model accounts also for the stochastic temporal correlations characteristic of the irradiation process and the cellular repair kinetics by solving explicitly in the MC evaluations the kinetic **Eq. (78)** where the time dependent specific energy rate  $\dot{z}^{(c,d)}$  appears explicitly [101, 114].



In the MC approach, the irradiation of a complete population of  $N_c$  cells is simulated, where  $N_c$  is supposed to be large enough in order to achieve statistical convergence. The irradiation is modeled as an ordered temporal sequence of particles (primaries and secondaries) that interact with the cell nucleus at random spatial coordinates and random times  $t_0^{(c)} \leq t_1^{(c)} \leq t_2^{(c)} \leq \dots$ , compatible with the chosen irradiation setting and the definition of the time-dependent macroscopic dose-rate  $\dot{D}(t)$ . The irradiation is hence modeled as a sequence of spikes in  $\dot{z}^{(c,d)}(t)$ , each one of them corresponding to the passage of a particle through or nearby the nucleus, delivering a sequence of random specific energies in the domains

$$z_0^{(c,d)}(t_0), z_1^{(c,d)}(t_1), z_2^{(c,d)}(t_2), \dots \tag{85}$$

depending on the particle spectra and track impact positions with respect to the cell. A depiction of the temporal evolution of the lesions ( $x_I$  and  $x_{II}$ ) due to the effects of the irradiation as described in Eq. (85) is reported in panel (b) of Figure 2. For a macroscopic dose  $D$  and a component  $e$ , indicating a specific particle and bin of the kinetic energy histogram sampled from the particles interacting with the cell nucleus, the total number of particles  $N_e$  interacting with the nucleus follow a Poisson distribution with mean

$$\bar{N}_e = \frac{\rho\sigma Dw_e}{LET_F}, \tag{86}$$

where  $LET_F$  is the frequency-average LET of the radiation computed on the total energy spectrum, considering all the contributing particles,  $\sigma$  is the cross section of the nucleus,  $\rho$  is the density of the tissue, and  $w_e$  is the normalized weight of the  $e$ -th bin of the energy and particle histogram.

In principle, the tracks can be directly sampled from the full measured microdosimetric spectra (i.e., not only the first and second moment) from which the experimental  $w_e$  can be obtained. From a practical point of view, the specific energies deposited randomly in each domain of each nucleus are evaluated by coupling general purpose MC tools (such as Geant4 [97, 115] or Fluka [116]) in combination with an amorphous track structure model as described in [21, 36]. The MC code is used to identify the ions that can interact with a cell located in a certain point of the irradiated macroscopic volume at a certain time. The domains are arranged according to a close packing hexagonal structure inside the nucleus.

Once the time sequence of specific energies in the domains (85) are obtained, the kinetic Eq. (78) can be formally solved for  $t \rightarrow \infty$  to obtain the average number of lethal lesions for each cell-domain  $(c, d)$ :

$$-\log s^{(c,d)} = x_I^{(c,d)}|_{t \rightarrow \infty} = \frac{\alpha_0}{N_d} \sum_{i=0}^{n_c-1} z_i^{(c,d)} + G_{c,d} \frac{\beta_0}{N_d} \left( \sum_{i=0}^{n_c-1} z_i^{(c,d)} \right)^2, \tag{87}$$

where  $n_c$  is a Poisson random variable indicating the number of particles that interacted with the cell  $c$ ,  $\tau = 1/(a+r)$  is the time constant that defines the first order repair kinetics, and  $G$  is the

generalized Lea-Catcheside time factor [57, 65] defined at the nanodosimetric level of the domain:

$$G^{(c,d)} = 1 - \frac{2}{\left(\sum_{i=0}^{n_c-1} z_i^{(c,d)}\right)^2} \sum_{i=0}^{n_c-2} \sum_{j=i+1}^{n_c-1} \left(1 - e^{-\frac{1}{\tau}(t_j^{(c)} - t_i^{(c)})}\right) z_i^{(c,d)} z_j^{(c,d)}. \tag{88}$$

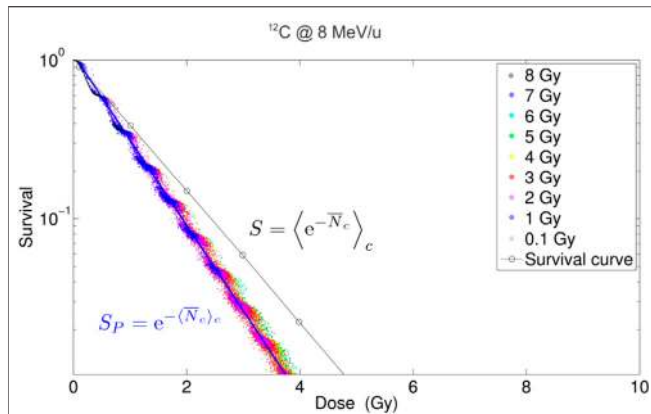
The survival fraction  $S$  is obtained by averaging over the entire cell population the survival probability evaluated for each single cell  $S_n(c)$  (see for comparison Eqs 37, 41)

$$S(D) = \langle S_n^{(c)}; D \rangle_c = \left\langle \exp\left(-\sum_{d=1}^{N_d} x_I^{(c,d)}\right) \right\rangle_c = \left\langle \exp\left(-N_d \langle x_I^{(c,d)} \rangle_d\right) \right\rangle_c. \tag{89}$$

Notice that the Monte Carlo approach does not compute directly the LQ coefficients  $\alpha$  and  $\beta$ , in contrast to the analytical approaches described in the previous sections. However, it is possible to derive the LQ coefficients by simulating a complete survival curve, i.e., by evaluating (89) using different macroscopic doses  $D_1 < D_2 < D_3 < \dots$ , and then fitting the curve with the LQ formula. An example of a complete simulated survival curve is reported in Figure 11. We remark also that, as done in Section 3.7, the cell population generated by the solutions of the kinetic Eq. (78) neglects re-population and cell cycle re-distributions.

One of the benefits of the MCt-MKM approach is that both  $\alpha$  and  $\beta$  coefficients, obtained through the survival fitting, show the expected saturation behavior for high-LET irradiation without adding any corrective factors, like the non-Poisson (Section 3.4) or (Section 3.5) saturation. The disadvantage of the approach, other than the inherent approximations specific to the used MC transport code and the adoption of an amorphous track model, is that it can be particularly computing intensive, although this is mitigated by exploiting the multi-core parallelism of modern CPUs [113].

The MCt-MKM has been validated on *in-vitro* experiments considering acute and *split-dose* irradiation on HSG, T1, and V79 cell lines in aerobic conditions of H, He, C, and Ne ion beams [23]. An example of the behavior of the LQ  $\alpha$  and  $\beta$  coefficients is reported in Figure 12, where also a comparison with the prediction of other models, a non-stochastic MKM evaluation, the LEM, and the repair-misrepair-fixation (RMF) model (see Section 4.2), is shown. The main difference with respect to the original MKM is that the MCt-MKM predicts a non-constant and vanishing  $\beta$  with high LET values. This behavior is ultimately due to the non-Poisson statistics inherently implemented in the model. However, we remark that, although, as previously noted, there is a general consensus for a vanishing  $\beta$  for high LET irradiation, there are still contradictory experimental results and significant uncertainties for  $\beta$  vs. LET behavior (see, for example, also [118]). In particular, in Figure 12, the data show a beta significantly larger than zero for a large number of experimental points for He and C ions also for relatively high LET.



**FIGURE 11** | Simulated survival curves obtained for acute irradiation, ( $t_0 = t_1 = t_2 = \dots$ ), of mono-energetic carbon ion (8 MeV/u) with imposed macroscopic doses ranging from 0.1 to 8 Gy represented in different colors. The dots represent the values of cell survival  $S_n^{(c)}(z_n^{(c)})$  with specific energy  $z_n^{(c)} = N_d \sum_{d=1}^{N_d} \sum_{i=0}^{(n_c-1)} z_i^{(c,d)}$  delivered in the cell  $c$  (a small dot for each simulated cell); the variability of the delivered dose with respect to the imposed dose derives by the fluctuation determined by the MC simulation. The two curves were fitted using the LQ model (solid and dashed lines, respectively) in order to get the LQ parameters. The blue curve is fitted directly to the  $S_n^{(c)}(z_n)$  data and corresponds to the Poisson approximation described in **Eq. (43)**. The black line corresponds to the fit to the population averages  $\langle S_n^{(c)}; D \rangle_c$  defined in **Eq. (89)** for each imposed dose  $D$  (open dots) and corresponds to the non-Poisson formulation of **Eq. (59)**. Plot taken from [117].

The model was also implemented in a TPS [88] to evaluate the effect of the temporal protraction of treatments with different ion beams. The effect of the protraction, described microscopically by **Eq. (88)**, was shown to be compatible with a macroscopic first order effect with temporal constant  $\tau$  [23]. We remark that, in the framework of the LQ formalism, in the studies of high dose irradiation and the dose-rate effect, such as those reported in [23, 101–104], the specific way  $\beta$  is modeled which plays a fundamental role [119, 120]. In particular, the behavior of a vanishing  $\beta$  for high LET is compatible with the experimental observation of a reduction of the sensitivity to the dose-rate (including the fractionation) in healthy tissues for treatments with high-LET ions and, hence, the potential advantage of hypofractionated treatments with these particles.

### 3.8.2 The Stochastic Microdosimetric Kinetic Model

The analytical computation method proposed by Sato and Furusawa [22] introduces a correction to the original formulation of MKM, taking into account the stochastic nature of specific energy in both the domain  $z$  and the cell nucleus  $z_n$ , to improve the adherence of the model to the measured survival fractions for high-LET and high-dose irradiation. The new model is named double-stochastic microdosimetric kinetic (DSMK) model. In the same study [22], a second model, termed stochastic microdosimetric kinetic (SMK) model, is derived to represent the stochastic nature of domain specific energy  $z$  by its approximated mean value and variance in order to reduce the computational time.

Based on radiobiological evidences that state that DNA damage saturates at high-LET regions [121, 122], the original assumption of the MKM, that the initial numbers of lethal and sub-lethal lesions produced in a domain to be proportional to the specific energy in the site, is changed in the DSMKM, assuming that the initial numbers of lethal and sub-lethal lesions produced in a domain are proportional to the *saturation-corrected specific energy*,  $z^*$  in the domain, calculated as

$$z^* = z_0 \sqrt{1 - \exp[-(z/z_0)^2]}, \quad (90)$$

where  $z_0$  can be obtained from  $z_0 = y_0 (\bar{l}_d/m_d)$  with the saturation correction parameter  $y_0$  defined in **Eq. (66)**.

By applying this new parameter, the natural logarithm of survival for a domain and the nucleus, **Eqs (35)** and **(37)**, can be rewritten, respectively, as

$$\begin{aligned} \log(s(z)) &= -Az^* - Bz^{*2}, \\ \log(S_n(z_n)) &= -\alpha_0 \int_0^\infty z^* f(z; z_n) dz - \beta_0 \int_0^\infty z^{*2} f(z; z_n) dz, \end{aligned} \quad (91)$$

with the natural log of the survival fraction of cell irradiated with dose  $D$ ,  $\log S(D) = \langle S_n \rangle_c$ , given by substituting **Eq. (91)** in **Eq. (41)**.

The evaluation of the multi-event probability density  $f(z; z_n)$  is obtained numerically by applying a general  $n$ -fold convolution method such as the one presented in **Section 2 (Eqs 4 and 6)** to the single event probability density  $f_1(z)$ . The evaluation of  $f_1(z)$  is performed exploiting a microdosimetric function implemented in the PHITS Monte Carlo code [123, 124]. The sum in **Eq. (6)** can be truncated for practical purposes, with 100 events being enough to evaluate the density probability function of cells with  $z_n = 100$  Gy.

The same approach is used to calculate the multi-event probability density of the cell nucleus specific energy, for an absorbed macroscopic dose  $D$ ,  $f_n(z_n, D)$ , from the single event function  $f_{n,1}(z_n)$ . However, since the nucleus radius is over the available range of the microdosimetric function implemented in PHITS,  $f_{n,1}(z_n)$  is determined from the frequency distribution of the LET  $L$ ,  $F_L(L)$ :

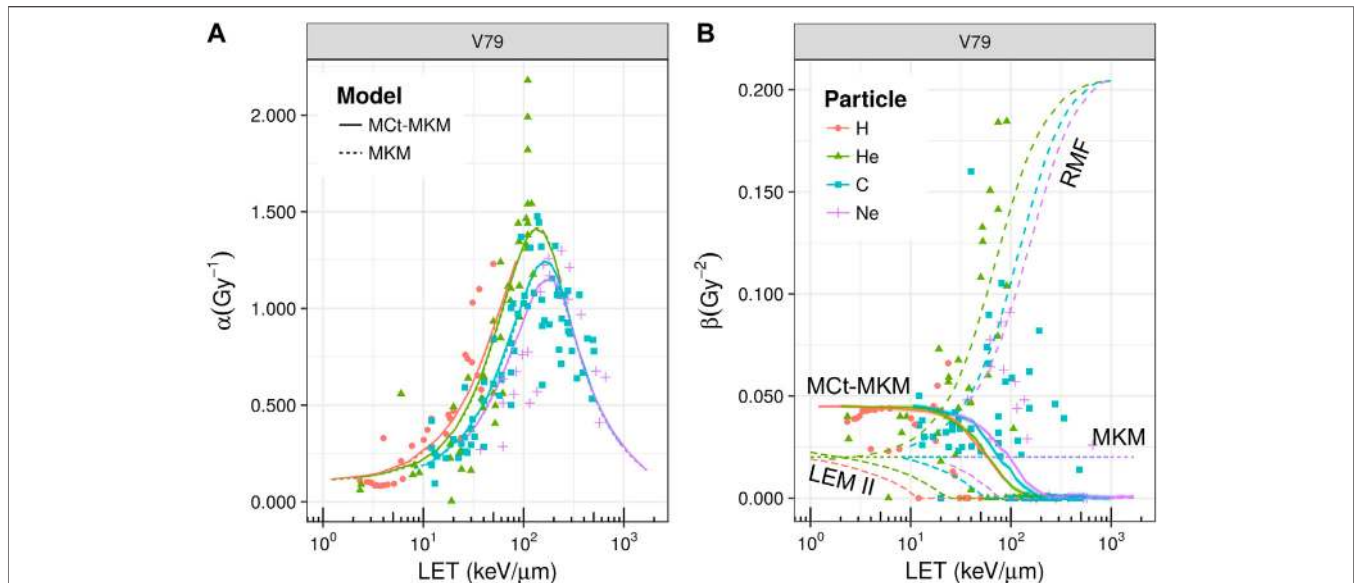
$$f_{n,1}(z_n) = \int_0^\infty F_L(L) f_{n,1}(z_n, L) dL, \quad (92)$$

where  $f_{n,1}(z_n, L)$  represents the probability density of  $z_n$  from a particle with LET =  $L$ . Following the formalism carried out in [125], the expression for  $f_{n,1}(z_n, L)$  is written as a Fermi function:

$$f_{n,1}(z_n, L) = \frac{2C}{(L\eta)^2} \frac{z_n}{\exp[(z_n - L\eta)/\gamma] + 1}, \quad (93)$$

where  $C$  is a normalization constant and  $\eta$  is a units conversion coefficient. The parameter  $\gamma$  tunes the slope of the Fermi function or, equivalently, the magnitude of the fluctuation of  $z_n$  due to the energy straggling.

Once  $f_{n,1}(z_n)$  is determined, the multi-event function  $f_n(z_n; D)$  for the nucleus is obtained with the same  $n$ -fold convolution procedure used in the case of  $f(z; z_n)$ . In this case, however, due to the higher average number of events that can happen in the nucleus



**FIGURE 12 |** Linear quadratic  $\alpha$  (panel A) and  $\beta$  (panel B) parameters as a function of LET for the irradiation of V79 cells with different ions. Points represent experimental data taken from PIDE [82], different colors/gray levels and shapes refer to H, He, C, and Ne ions, respectively (the color/gray level and shape legend refers both to panels A and B). In panel A, solid and dashed lines represent, respectively, the extrapolation with the MCT-MKM and the original MKM, while in panel B, a comparison between different models is reported (namely, MKM, MCT-MKM, LEM-II, and RMF). In the case of the MCT-MKM, overlapped to the  $\alpha$  and  $\beta$  curves, the MC statistical confidence bands (68%) are reported. These bands are small due to the high statistics and they blend with the curves' thickness. A saturation effect is observed for both  $\alpha$  and  $\beta$  parameters. Plot taken from [23].

compared to the domain,  $\lambda_n(D) \gg \lambda(z_n)$ , the computation is significantly more demanding and cannot be practically used for applications inherently complex such as TPS evaluations for ion beam treatments. To overcome this problem, in the case of high-dose irradiations, a pre-evaluated database of probability densities derived from mono-energetic irradiations is used and combined in a central limit approximation.

To overcome the long computational time of the DSMK model in a TPS workflow, a further optimization is performed for the computation of the survival in (91) that bypasses the necessity to compute the  $n$ -fold convolution integral (Eq. 6). In this formulation of the model (SMK), it is assumed that a saturation effect triggered by multiple hits of radiations to a domain is negligibly small so that the magnitude of the effect for the  $n$ -event energy deposition can be derived from the estimate with the single event density probabilities (see also Eqs 9 and 12):

$$\frac{\int_0^\infty z^* f(z, \lambda_n) dz}{\int_0^\infty z f(z, \lambda_n) dz} \approx \frac{\int_0^\infty z^* f_1(z) dz}{\int_0^\infty z f_1(z) dz} = \frac{z_F^*}{z_F} \quad (94)$$

and

$$\frac{\int_0^\infty z^{*2} f(z, \lambda_n) dz}{\int_0^\infty z^2 f(z, \lambda_n) dz} \approx \frac{\int_0^\infty z^{*2} f_1(z) dz}{\int_0^\infty z^2 f_1(z) dz} = \frac{z_D^*}{z_D} \quad (95)$$

Following these approximations, the natural log of the survival fraction of a cell can be calculated by substituting Eqs (94) and (95) in Eq. (91), Obtaining

$$\log(S_n(z_n)) = -\alpha_0 z_n \frac{\bar{z}_F^*}{z_F} - \beta_0 (z_D z_n + z_n^2) \frac{z_D^*}{z_D} \quad (96)$$

In order to reduce further the computational effort for TPS applications, assuming that in standard condition of ion beam radiotherapy the events inducing the saturation of complex DNA damages are rare, and hence  $z_F^*/z_F \approx 1$ , the following approximation of Eq. (41) was derived [112]:

$$\log S(D) = \log \left\{ 1 + D \left[ -\beta_{SMK} + \frac{1}{2} (\alpha_{SMK} + 2\beta_{SMK} D)^2 \right] z_{n,D} \right\} - \alpha_{SMK} D - \beta_{SMK} D^2, \quad (97)$$

with

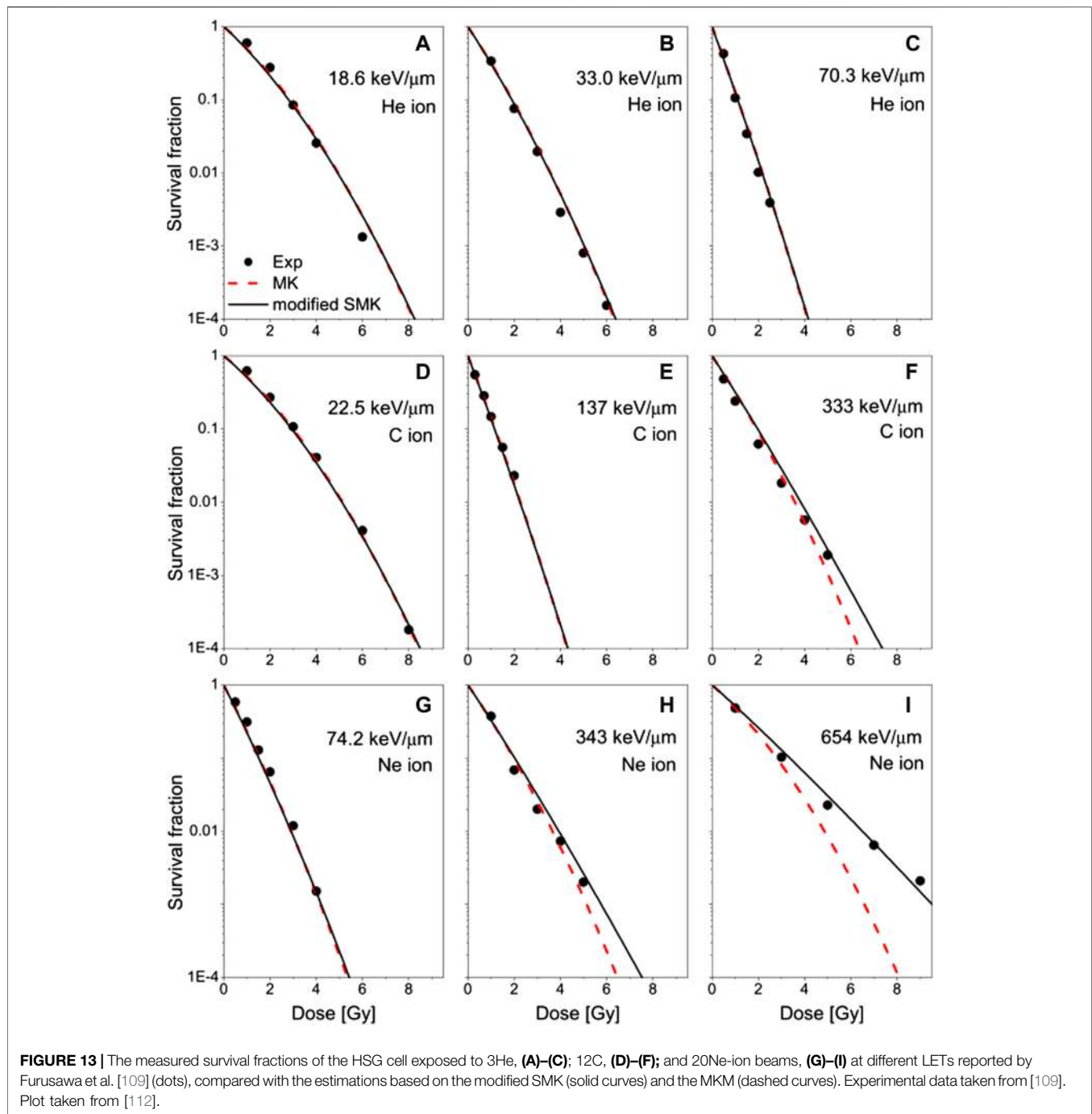
$$\alpha_{SMK} := (\alpha_0 + z_D^* \beta_0), \quad (98)$$

$$\beta_{SMK} := \beta_0 (z_D^*/z_D). \quad (99)$$

Both DSMK and SMK models can reproduce the measured survival fractions, even for high-LET and high-dose irradiations, whereas the simple saturation-based MKM [20] predicts lower values for these irradiations due to the intrinsic ignorance of the stochastic nature of the cell nucleus specific energies (see Figure 13). In particular, the DSMK model can account for the decrease in the  $\beta$  parameter observed in high-dose irradiations over 10 Gy due to the saturation effect triggered by multiple hits of radiations to a domain.

### 3.9 Extensions and Further Improvements

In recent years, a number of studies have been published reporting further refinements and extensions of the MKM. Among these are further improvement accounting of the non-Poissonian statistics [112, 126], the inclusion of an explicit DNA modeling [69, 70], the effect of a heterogeneous cell population



including the cell-cycle variance [39, 114, 127], and the inclusion of non-target effects [128]. Extension of the model has been also proposed to compute quantities beyond the RBE, such as the oxygen enhancement ratio (OER) [37, 38]. In the following of this section, some details about a selection of these developments are described.

### 3.9.1 Oxygen Enhancement Ratio (OER) Modeling

Several experiments show that cellular oxygenation condition strongly affects their response to ionizing radiation. In particular,

a significantly lower cell death rate is observed after exposure to ionizing radiation in the presence of a reduced concentration of oxygen in the cells, i.e., in hypoxic conditions. As clinically observed, solid tumors can contain oxygen-deficient regions, thus increasing their radioresistance and potentially leading to treatment failure [129, 130]. An understanding of why high-LET radiations are so effective at overcoming tumor hypoxia [131, 132] is also particularly relevant for the individualization and optimization of ion beam radiotherapy. For this purpose, attempts to extend the MKM to describe the dependence of

the radiation effects on the oxygen concentration in cells and to model the oxygen enhancement ratio (OER) have been made [37, 38].

It is interesting to note that these MKM-based approaches, although different, do not focus on OER modeling, a relative value, but directly on the prediction of hypoxic cell survival data, being the OER a derived quantity.

In [37], the reduction of lethal ( $x_I$ ) and potentially lethal ( $x_{II}$ ) damage due to the absence of oxygen is linked in the low-LET region to the phenomenological photon OER. This linking is realized through the application of an Alper and Flanders functional formalism [133] to add an explicit dependence to the oxygen concentration to the parameters  $\lambda$  and  $\kappa$  (Eq. 28) and the sizes of the domain and nucleus. In particular, the parameters  $\lambda$  and  $\kappa$  and the domain size are assumed to vary with the inverse of the photon OER while the nucleus size is assumed to be proportional to the photon OER as a function of oxygen concentration.

In [38], the general approach proposed by Wenzl and Wilkens [134] has been adapted to the amorphous track approach to the MKM [21] (the latter described in Section 3.6). The inclusion of track model ultimately brings to the OER an explicit dependence on ion type while the Wenzl and Wilkens formalism brings an explicit dose and oxygen concentration dependence in the  $\alpha$  and  $\beta$  parameters. These characteristics have been exploited, by integrating the model in a TPS, to evaluate the tumor control probability (TCP), to facilitate the identification of the optimal treatment conditions in terms of ion choice and dose fractionation in the presence of hypoxia.

The MKM-based OER models were verified against *in vitro* data from HSG, V79, and CHO cells in aerobic and hypoxic conditions, irradiated with different ion beams [109]. Examples of the model prediction vs. the experimental data are reported in Figure 14.

### 3.9.2. Non-Targeted Effects

In the majority of cell survival modeling approaches, it is assumed that biological effects of radiation are exclusively due to direct DNA damage resulting from the ionization caused by the incident radiation. In recent years, this assumption has been extensively challenged by considering a variety of indirect processes, also referred to as bystander or non-targeted effects (NTE) that significantly impact on the cellular response to the radiation [137]. NTEs have been interpreted as a result of intercellular communication with cell-killing signals between hit and non-hit cells [138, 139], resulting in induced DNA damage in non-hit cells [140].

Attempts to derive kinetic equations to model the intercellular signaling which incorporates signal production and response kinetics have been made [141–143]. In recent studies, such as by Matsuya et al. [128], an integration of these signaling kinetic equations in the MKM has been proposed.

In this formulation, denoted integrated microdosimetric kinetic (IMK) model, the number of signaling activation events,  $N_{NT}$ , in the domain is assumed to be a linear-quadratic function of the specific energy  $z$ . Thus, following the same procedure and the assumption of a Poisson statistics used to

derive Eqs (44), (45), the dose dependent fraction of receiving cells that are activated is written as

$$f_{NT}(D) = 1 - e^{-\langle N_{NT} \rangle_c} = 1 - e^{-(\alpha_{NT} + zD\beta_{NT})D + \beta_{NT}D^2}, \quad (100)$$

where  $\alpha_{NT}$  and  $\beta_{NT}$  are the LQ coefficients of the signal activation process. The propagation of the cell-killing signal is modeled as a diffusion process with diffusion constant  $\theta$  and a simple exponential decay with a rate constant  $\lambda$ . The signal concentration  $\rho_s(\underline{r}, t)$ , where  $\underline{r}$  is a spatial position and  $t$  is time, can hence be obtained by solving the continuity equation:

$$\frac{\partial \rho_s(\underline{r}, t)}{\partial t} = \theta \nabla^2 \rho_s(\underline{r}, t) - \lambda \rho_s(\underline{r}, t). \quad (101)$$

In non-hit cells, the NTE sub-lethal lesions  $[x_{II}]_{NT}$  are assumed to be induced in proportion to the signal concentration  $\rho_s(\underline{r}, t)$  and then converted to lethal lesions  $x_I$  with the same constant rate  $a$  of Eq. (27) so that the number of sub-lethal lesions is written as

$$\begin{aligned} [\dot{x}_{II}(\underline{r}, t)]_{NT} &= (1 - f_{NT}(D)) [x_{II}(\underline{r}, t)]_{NT} \kappa_{NT} R_{NT} \rho_s(\underline{r}, t) \\ &\quad - (a + r_{NT}) [x_{II}(\underline{r}, t)]_{NT}, \end{aligned} \quad (102)$$

where  $R_{NT}$  is the constant rate for cell-killing signals reacting with the nucleus of non-hit cells,  $\kappa_{NT}$  is the number of sub-lethal lesions per domain caused by the signals, and  $r_{NT}$  is a constant rate for repair in non-hit cells (in general,  $r_{NT} \neq r$ , i.e., the repair rates in target and non-target cells are different). In [128], the following functional form for the cell survival fraction by the NTE ( $S_{NT}$ ) has been proposed as an approximate solution of the previous equations

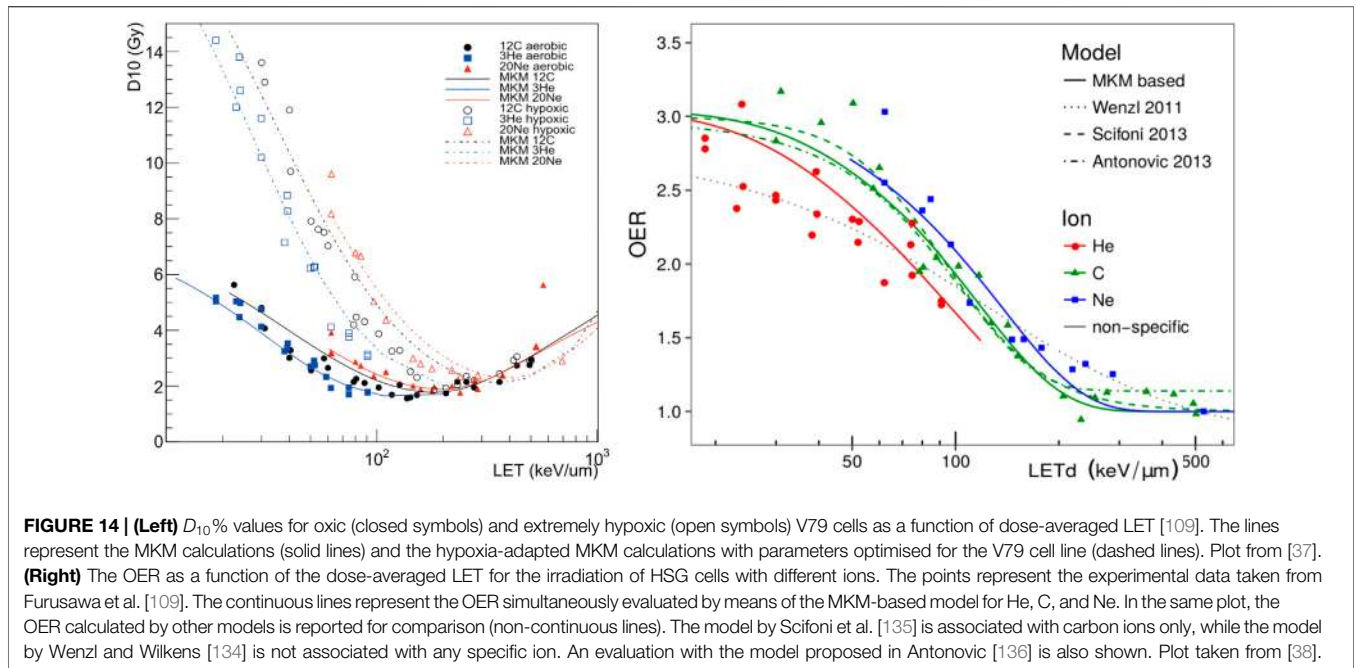
$$\log S_{NT} = -\langle [x_{I,II}]_{NTE} \rangle_c = -\delta \left( 1 - e^{-(\alpha_{NT} + zD\beta_{NT})D + \beta_{NT}D^2} \right) e^{-(\alpha_{NT} + zD\beta_{NT})D + \beta_{NT}D^2}, \quad (103)$$

where  $\delta$  is a function of the other parameters introduced in the former equations that characterize the intercellular signaling process.

In order to compute the cell survival probability  $S$  with the inclusion of both NTEs and targeted effects, an approximation is made in which it is assumed that the probability of interactions between sub-lethal lesions  $x_{II}$  and  $[x_{II}]_{NT}$  in the domain is negligible. This assumption factorizes the two systems of Eqs (27) and (102) and hence considers the total cell survival as the product of  $S = S_T \times S_{NT}$ , where the survival for targeted cells,  $S_T$ , is given by Eq. (43). Figure 15 shows an example of the fitting of the IMK model with experimental clonogenic data. It is interesting to note the possibility of the IMK model to account for deviations from the LQ formalism, reproducing the low-dose hypersensitivity behavior of cell response and evincing its relation with DNA repair mechanisms.

## 4 OTHER MODELS

This section presents alternative models to determine RBE based on microdosimetric approaches.



### 4.1 RBE Weighting Functions

The microdosimetric RBE weighting function approach has been proposed initially by Menzel, Pihet, and Wambersie et al. [27, 33] to compare the beam quality of different neutron [27] and proton [144, 145] therapeutic installations using measured microdosimetric distributions of lineal energy. Based on previous studies on proton beams [146, 147], this approach uses measured microdosimetric distributions of lineal energy,  $y$ , combined with an experimentally derived *biological weighting function*, for specific cell line and endpoints,  $r(y)$ , to evaluate the RBE.

Let  $P(y)$  be the cellular response function for a population suffering the fraction of dose  $d(y)dy$  corresponding to the lineal energy  $y$ .  $d(y)$  is the dose probability density of  $y$  and can be evaluated as  $d(y) = \frac{y}{y_F} f(y)$  [34]. The linear  $\alpha$  parameter, interpreted as the biological effect  $E$  per unit dose, is expressed as

$$\alpha = E/D = \int \frac{P(y)}{y} d(y) dy \equiv \int r(y) d(y) dy, \tag{104}$$

where  $r(y)$  is defined as the response function. Therefore, the model is rigorously valid under the assumption of a low dose approximation where the cellular response function is linear.

$P(y)$  or directly  $r(y)$  is experimentally derived. A formulation for  $r(y)$  is given in the following [148, 149]:

$$r(y) = \sigma_E [1 - \exp(-a_1 y - a_2 y^2 - a_3 y^3)]/y, \tag{105}$$

where the  $\sigma_E$ ,  $a_1$ ,  $a_2$ , and  $a_3$  are parameters specific to the radiobiological end points and are independent on the quality of the radiation. These parameters are determined experimentally by fitting a set of different measurements of  $\alpha_i$  or  $RBE_{\alpha,i} = \alpha_i/\alpha_X$  using different irradiation modalities with different radiation qualities  $i = 1, 2, 3, \dots, N$ .

The set of relations that have to be fitted is hence

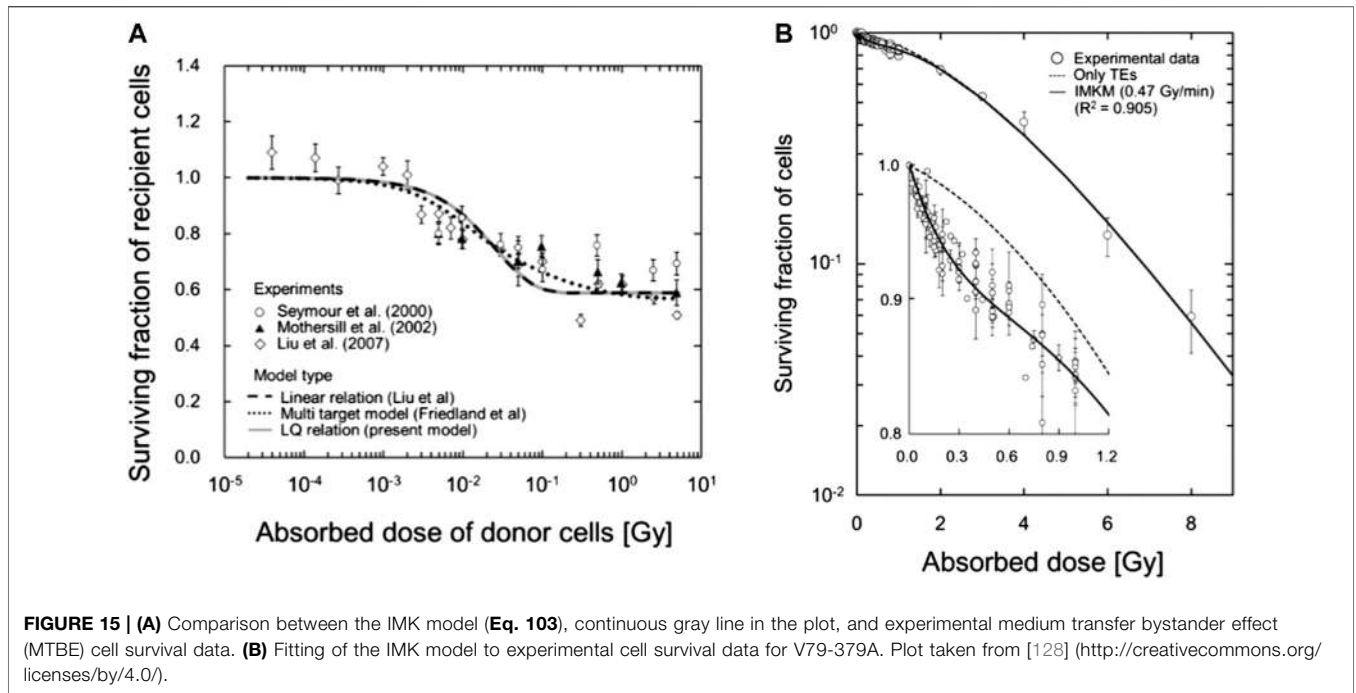
$$RBE_{\alpha,i} = \int r(y) d_i(y) dy; \quad i = 1, \dots, N. \tag{106}$$

The solution of the system of Eq. (106) can be obtained with different methods, such as non-parametric multi-objective optimization methods [150] or iterative procedures [40] through which an initial guess function  $r(y)$  is iteratively updated to best fit Eq. (106).

### 4.2 The Repair–Misrepair–Fixation (RMF) Model

The repair–misrepair–fixation (RMF) model combines the RMR and LPL models, adding the consideration of intra- and inter-track<sup>2</sup> binary misrepair to predict the biological effect of LET [24–26]. The RMF model considers the entire cell nucleus as the volume for pairwise DSB interactions. In the RMF model, a coupled system of nonlinear ordinary differential equations is used to model the time-dependent kinetics of DSB induction, rejoining, and pairwise DSB interaction to form lethal (and nonlethal) chromosome damage. The model treats initial DSB formation as a compound Poisson process and postulates a first-order repair term that gives rise to exponential rejoining kinetics for most DSB (>98%) and a second-order (quadratic) term to

<sup>2</sup>Intratrack binary misrepair occurs when an energy deposition along the track forms two or more DSBs that interact in pairwise mode to form an exchange. Intertrack, instead, is a binary misrepair arising from the pairwise interaction of break ends associated with DSBs that were formed by two separate radiation tracks through a cell.



account for the small subset of the initial DSB (< 2%) that undergo pairwise DSB interactions to form an exchange.

An LQ approximation of the solution of the RMF system of differential equations can be expressed as follows [24, 25]:

$$RBE_{\alpha} = \frac{\Sigma}{\Sigma_X} \left( 1 + \frac{2}{R\Sigma_X} (\Sigma z_{n,F} - \Sigma_X (z_{n,F})_X) \right), \quad (107)$$

$$RBE_{\beta} = \frac{\Sigma}{\Sigma_X}, \quad (108)$$

where  $\Sigma$  is the initial number of DSB per gray per giga base pair ( $Gy^{-1} Gbp^{-1}$ ) and  $z_{n,F}$  is the frequency-average specific energy evaluated in the nucleus (see Eq. 9), for the particle radiation. The suffix  $X$  indicates the same quantities for the reference photon radiation.  $RBE_{\alpha}$ ,  $RBE_{\beta}$ , and  $R$  are defined in Eq. (51), while the ratio  $\Sigma/\Sigma_X = RBE_{DSB}$  can be interpreted as the RBE for DSB induction.

From Eq. (107), it follows that the radiation response of a cell exposed to a low- or high-LET radiation is uniquely determined by one microdosimetric parameter ( $z_{n,F}$ ) and two biological parameters ( $RBE_{DSB}$ ) and  $R$ .  $z_{n,F}$  can be derived from microdosimetric measurements or computed via Monte Carlo simulations. Implicit in the determination of  $z_{n,F}$  is the knowledge of the size of the nucleus. For a spherical water target of diameter  $d$ , the frequency-average specific energy can be approximated by Eq. (20). A complication arises from the fact that, in general,  $RBE_{DSB}$  also strongly depends on particle type and kinetic energy (and thus LET or lineal energy) although it is considered to be the same among all eukaryotes. Consequently,  $R$  is basically left as the main parameter of the RMF is needed to discriminate the radiation response among different cell lines (compare also the MKM formulation, Eq. 53).

From a practical point of view,  $RBE_{DSB}$  is obtained and stored in a look-up table as a function of particle type and kinetic energy by means of Monte Carlo computations. The MCDS Monte Carlo code [151, 152], which is able to simulate also the dependence on the oxygen concentration, is typically used in these computations, so that the RMF has been also used to predict the OER [153] along with the clonogenic data [25] and DSB induction estimates [24] for ion irradiations.

In panel (b) of Figure 12, the RMF prediction of the  $RBE_{\beta}$  compared with experimental data and the evaluations of other models is reported. It is worth noting that the RMF model predicts an increasing  $\beta$  for increasing LET (see Eq. 107). This is in contrast with other models, such as the LEM, which predict a decreasing  $\beta$ , or the MKM, which, depending on the specific formulation, predicts both a constant and a decreasing  $\beta$ .

The RMF has been also implemented in a TPS to evaluate the 3D RBE distribution in irradiated patients [154]. It is interesting to note that one of the appealing aspects of the RMF for TPS studies is that the specific response of the tissue, both healthy and tumoral, is explicitly determined by a single parameter,  $R$ . This is a simplification, but allows to study the effect of the specificity of the tissue response in a direct way, also allowing for a distribution of  $R$  values and hence easily accounting for the variability and the uncertainty associated to this clinical parameter.

## 5 SUMMARY

In clinical treatment planning, the RBE has to be calculated by radiobiological mathematical models, which, in spite of all validation efforts, still involve significant sources of uncertainty.

The aim of this review was to present the theoretical aspects of a selection of radiobiological models that emphasize the link of *in vitro* and *in vivo* radiobiological outcomes, such as the RBE, to microdosimetric experimental data. We approached these models through a conceptual sketch of their assumptions, highlighting the continuity and leaps of their mathematical formulations. For each model, we addressed the limit of applicability and eventual improvements and the link of their input parameters to experimental observables.

A particular emphasis to the microdosimetric kinetic (MKM)-based models has been given. Starting from its first seminal formulation by Hawkins [18], the MKM has represented an effective approach to link the microdosimetric quantities, which describe the quality of the radiation, to the radiobiological effects and, at present, it is one of the most widely used models to evaluate the RBE in both research and clinical applications. The MKM approach for RBE evaluations has gained a particular interest in recent years, with the appearance of different studies aimed to improve the accuracy of the model and to extend its range of applicability in different biological contexts, such as the OER prediction and non-target effects.

Although sharing similar theoretical bases, the MKM-based models make different assumptions and approximations in their implementation. Based on these differences, the models considered in this review (including also the RMF model) make, in particular, different predictions in the dependence of  $\beta$  on particle LET and the RBE for cell survival in the overkill regime, for particles with a  $LET \geq 150$  keV/ $\mu\text{m}$ .

Two main aspects of the considered models, where recent efforts have brought interesting insight, and where further future studies could bring potential improvements, could be identified. One aspect is the ascertainment of a more accurate

link of the theoretical descriptions to specific cellular mechanisms of DNA damage induction and its evolution, exploiting also information from nanodosimetric data. Another aspect is to improve the theoretical statistical description of the involved processes, be them either the stochastic nature of the energy deposition or the stochastic nature of the cell response to the irradiation.

Future comparisons of model predictions with experimental data are hence needed to fully discriminate among competing mechanisms to be incorporated for the improvement of these models to evaluate the RBE.

## AUTHOR CONTRIBUTIONS

VB and AA have provided a critical interpretation of the theoretical aspects of each model and its applications, deciding structure and principal contents of this review. They have cured the links with experimental data underlining limitations and strengths of each approach. The experience and accuracy of AA have led the entire work. FG has principally handled the mathematical aspects of the work, his help has been precious in revising notation and clarifying model formulation. ES has helped particularly in the general parts and introduction and has given also his valuable opinion on the structure and contents. MM and FT have given a contribution to experimental links, CT has supervised.

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**Conflict of Interest:** The authors declare that the research was conducted in the absence of any commercial or financial relationships that could be construed as a potential conflict of interest.

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