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# Low-loss metasurface optics down to the deep ultraviolet region

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## Abstract

Shrinking conventional optical systems to chip-scale dimensions will benefit custom applications in imaging, displaying, sensing, spectroscopy, and metrology. Towards this goal, metasurfaces—planar arrays of subwavelength electromagnetic structures that collectively mimic the functionality of thicker conventional optical elements—have been exploited at frequencies ranging from the microwave range up to the visible range. Here, we demonstrate high-performance metasurface optical components that operate at ultraviolet wavelengths, including wavelengths down to the record-short deep ultraviolet range, and perform representative wavefront shaping functions, namely, high-numerical-aperture lensing, accelerating beam generation, and hologram projection. The constituent nanostructured elements of the metasurfaces are formed of hafnium oxide—a loss-less, high-refractive-index dielectric material deposited using low-temperature atomic layer deposition and patterned using high-aspect-ratio Damascene lithography. This study opens the way towards low-form factor, multifunctional ultraviolet nanophotonic platforms based on flat optical components, enabling diverse applications including lithography, imaging, spectroscopy, and quantum information processing.

## Introduction

An optical metasurface is a planar array of sub-wavelength electromagnetic structures that emulate the operation of a conventional refractive, birefringent, or diffractive optical component, such as a lens, waveplate, or hologram, through individually tailored amplitude, phase, or polarization transformations of the incident light<sup>1–9</sup>. Dielectric materials such as amorphous Si<sup>10,11</sup>, polycrystalline Si<sup>12</sup>, titanium dioxide (TiO<sub>2</sub>)<sup>13,14</sup>, and gallium nitride (GaN)<sup>15,16</sup> have been used to realize metasurfaces operating at infrared and visible frequencies. The scarcity of dielectric materials that are characterized

by low optical loss at higher frequencies and simultaneously amenable to high-aspect-ratio nanopatterning has impeded the development of metasurfaces for applications in the ultraviolet (UV) range, a technologically important spectral regime hosting diverse applications in lithography, imaging, spectroscopy, time keeping, and quantum information processing<sup>17–19</sup>. To date, metasurfaces designed for operation in the near-UV range (UV-A; free-space wavelength range:  $315 \text{ nm} \leq \lambda_0 \leq 380 \text{ nm}$ ; energy range:  $3.26 \text{ eV} \leq E_0 \leq 3.94 \text{ eV}$ ) have been implemented using niobium pentoxide (Nb<sub>2</sub>O<sub>5</sub>), down to an operation free-space wavelength of  $\lambda_0 = 355 \text{ nm}$ <sup>20</sup>. Crystalline Si has been used to realize metasurfaces operating down to  $\lambda_0 = 290 \text{ nm}$ <sup>21</sup>, a wavelength that falls within the mid-UV range (UV-B;  $280 \text{ nm} \leq \lambda_0 \leq 315 \text{ nm}$ ;  $3.94 \text{ eV} \leq E_0 \leq 4.43 \text{ eV}$ ), but the device efficiencies remain limited by the severe absorption loss associated with illumination frequencies above the bandgap of Si ( $E_g \approx 1.1 \text{ eV}$ ). In both studies, the demonstrated functionalities are limited to hologram generation and beam deflection,

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while other important wavefront shaping functionalities that can be empowered by optical metasurfaces, such as high-numerical-aperture focusing and structured beam generation, have not yet been achieved. Meanwhile, metasurfaces that can operate at even higher frequencies, such as within the deep-UV range (longer wavelength portion of UV-C;  $190 \text{ nm} \leq \lambda_0 \leq 280 \text{ nm}$ ;  $4.43 \text{ eV} \leq E_0 \leq 6.53 \text{ eV}$ ), have not been realized due to the challenge of identifying a dielectric material that has a suitably low optical absorption coefficient in that range and can be patterned into high-aspect-ratio nanostructures using the available nanofabrication techniques.

Here, we report high-performance dielectric metasurfaces that operate over a broad UV range, including within the record-short, deep-UV regime, and perform representative wavefront shaping functionalities. The constituent nanostructured elements of the metasurfaces are formed of hafnium oxide ( $\text{HfO}_2$ )—a UV-transparent, high-refractive-index dielectric material. Although  $\text{HfO}_2$  has been commonly exploited as a high-static-dielectric-constant (high- $\kappa$ ) material in integrated circuit fabrication<sup>22,23</sup>, its applications in photonics have largely been limited to optical coatings based on planar thin films, in particular due to the difficulty of patterning the material into high-aspect-ratio nanostructures. In this work, we overcome this limitation and use  $\text{HfO}_2$ , for the first time, to implement meta-devices operating in the UV and deep-UV regimes. We deposit high-quality, UV-transparent  $\text{HfO}_2$  films using low-temperature atomic layer deposition (ALD) and pattern the films using a high-aspect ratio, resist-based Damascene lithography technique<sup>24–26</sup>. We implement metasurfaces designed for operation at three representative UV wavelengths of 364, 325, and 266 nm, which perform a variety of optical functions, namely, high-numerical-aperture lensing, accelerating beam generation, and hologram projection, including under spin control for the last two applications. This achievement opens the way for low-form-factor and multifunctional photonic systems based on UV flat optics, and suggests promising applications in photolithography, high-resolution imaging, UV spectroscopy and quantum information processing.

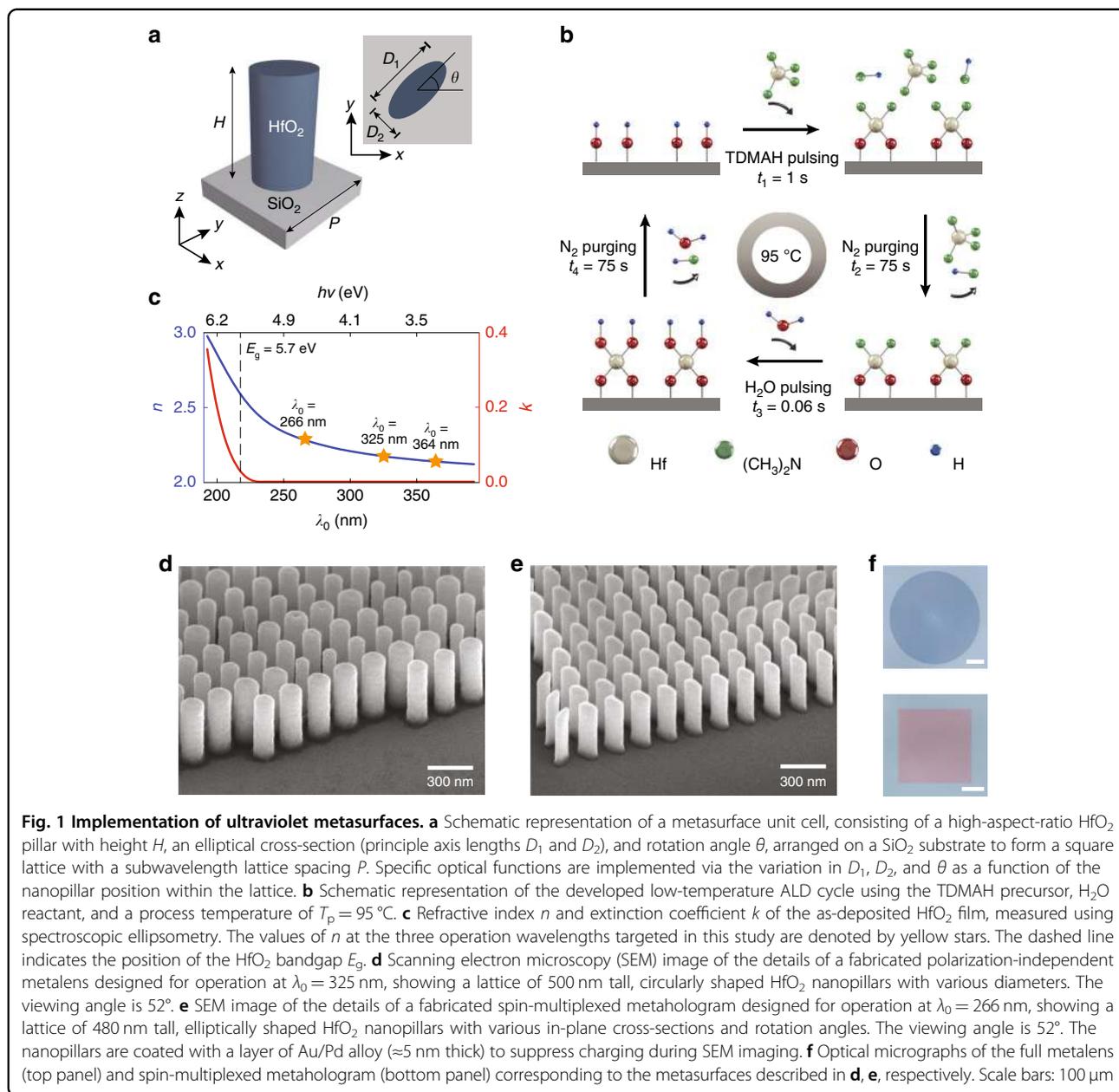
## Results

### Material choice and fabrication approach

The implemented metasurface devices consist of  $\text{HfO}_2$  nanopillars of either circular or elliptical in-plane cross-sections (Fig. 1a), densely arrayed on a transparent UV-grade fused silica substrate with a low refractive index (Supplementary Information, Fig. S1). The choice of  $\text{HfO}_2$ —a material most commonly exploited for its high static dielectric constant as a transistor gate insulator in complementary metal oxide semiconductor (CMOS) integrated circuits—is guided by the promise of both a

large refractive index ( $n > 2.1$  for  $\lambda_0 < 400 \text{ nm}$ ) and a wide bandgap  $E_g = 5.7 \text{ eV}$  ( $\lambda_g = 217 \text{ nm}$ ) located well within the deep-UV range, leading to a negligible extinction coefficient ( $k \approx 0$ ) for  $\lambda_0 \geq \lambda_g$ . Although the requirement of nanopillar dimensions with a wavelength-scale height (several hundred nanometers), a subwavelength-scale in-plane circle diameter or ellipse minor axis (few tens of nanometers), and vertical sidewalls suggest that pattern transfer with a directional dry-etching technique such as reactive ion etching would be optimal, we were unable to identify a suitable high-aspect-ratio, dry-etching chemistry for  $\text{HfO}_2$  (a material commonly patterned by non-directional wet chemical etching<sup>27</sup>). We instead explore the use of Damascene lithography<sup>24–26</sup> for  $\text{HfO}_2$  metasurface fabrication, a process that involves first patterning resist using electron beam (e-beam) lithography, conformally filling the open volumes of the resist template with  $\text{HfO}_2$  using ALD, back-etching the over-coated  $\text{HfO}_2$  layer using argon (Ar) ion milling, and finally removing the remaining resist with solvent to form the required high-aspect-ratio nanopillars (see “Materials and methods”).

The preservation of the physical integrity of the resist template requires the use of a plasma-free thermal ALD process with a process temperature,  $T_p$ , lower than the glass transition temperature (reflow temperature) of the utilized resist,  $T_g$ , along with a process chemistry involving by-products that are not corrosive to the resist. Fulfilling both process tolerance requirements rules out the use of common Hf precursors such as Tetrakis(ethylmethylamino)Hafnium (TEMAH)<sup>28</sup>, for which the minimum  $T_p$  ( $\approx 150^\circ\text{C}$ ) is significantly higher than the  $T_g$  of common e-beam resists, or hafnium chloride ( $\text{HfCl}_4$ )<sup>29</sup>, for which the reaction by-product (HCl) attacks the resist. Instead, we investigate Tetrakis(dimethylamino)Hafnium (TDMAH)<sup>30</sup> as an alternative Hf precursor for thermal ALD of high-optical-quality  $\text{HfO}_2$ , using a  $T_p$  below the  $T_g$  of common e-beam organic resists (such as ZEP, for which  $T_g \approx 105^\circ\text{C}$ ). To avoid the risk of incomplete reaction cycles and the physical condensation of precursors associated with low-temperature ALD (yielding films with defects and voids, and hence, degraded sub-bandgap optical properties, such as a reduced refractive index  $n$  and finite extinction coefficient  $k$ ), an existing ALD process which uses TDMAH and  $\text{H}_2\text{O}$  precursors and operates at  $T_p = 200^\circ\text{C}$  is modified (Fig. 1b) by (1) decreasing the process temperature to  $T_p = 95^\circ\text{C}$ ; (2) increasing the TDMAH pulsing time,  $t_1$ , from 0.25 to 1 s to enable a complete reaction with the OH monolayer resulting from the previous cycle; and (3) increasing the  $\text{N}_2$  purging times,  $t_2$  and  $t_4$ , from 12 to 75 s to ensure full removal of the excessive precursors and reaction by-products (see “Materials and methods”). As revealed by X-ray diffraction characterization (Supplementary Information, Section II) and spectroscopic ellipsometry measurements



(Fig. 1c and Supplementary Information, Section III), HfO<sub>2</sub> films deposited using the modified low-temperature ALD process are amorphous and characterized by a high refractive index ( $n > 2.1$ ) and negligible optical loss ( $k \approx 0$ ) over a UV wavelength interval  $220\text{ nm} \leq \lambda_0 \leq 380\text{ nm}$  spanning the full mid-UV and near-UV ranges and more than half of the deep-UV range. The measured wavelength dependences of  $n$  and  $k$  closely match those of a film grown using the  $200^\circ\text{C}$  reference ALD process (Supplementary Information, Fig. S4), demonstrating that the optical quality of the deposited HfO<sub>2</sub> can be maintained at significantly lower ALD process temperatures with a suitable Hf precursor and a proper adjustment of

the pulsing and purging times. Note that the  $95^\circ\text{C}$ -ALD-deposited HfO<sub>2</sub> films exhibit a high refractive index ( $n > 2.0$ ) and zero optical loss ( $k = 0$ ) in the visible range ( $380\text{ nm} \leq \lambda_0 \leq 800\text{ nm}$ ), making the films suitable for the fabrication of low-loss metasurface devices in this wavelength range as well (Supplementary Information, Fig. S5).

Using ZEP resist for e-beam lithography and the low-temperature TDMAH-based ALD process for the HfO<sub>2</sub> deposition, the proposed Damascene fabrication process is applied to yield defect-free metasurfaces, each consisting of a large array of densely packed HfO<sub>2</sub> nanopillars on a UV-grade fused silica substrate (Fig. 1f). The nanopillars have uniform heights, circular (Fig. 1d), or elliptical (Fig. 1e)

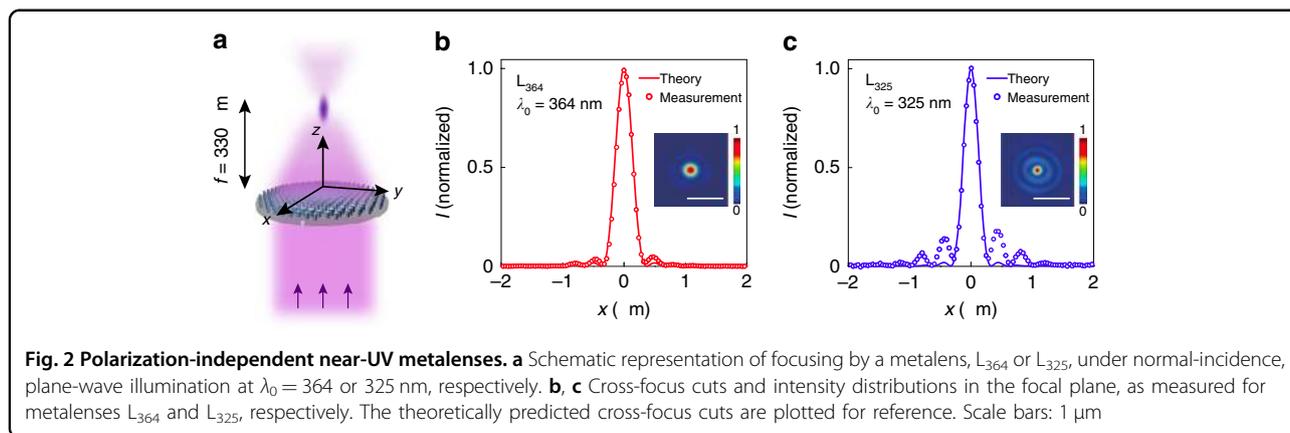
in-plane cross sections, and are characterized by straight, vertical, and smooth sidewalls (Fig. 1d, e, and Supplementary Information, Figs. S7–S11). The nanopillar rotation angle and two principle axis lengths in the plane of the metasurfaces ( $\theta$ ,  $D_1$ , and  $D_2$ , respectively, where  $\theta = 0$  and  $D_1 = D_2 = D$  in the case of a circular cross-section) vary as a function of the nanopillar position (with  $0 \leq \theta < \pi$  and  $50 \text{ nm} \leq (D_1, D_2) \leq 160 \text{ nm}$ ) depending on the optical function implemented by the metasurface. The nanopillar height  $H$  varies depending on the operation wavelength of the metasurface ( $400 \text{ nm} \leq H \leq 550 \text{ nm}$ ).

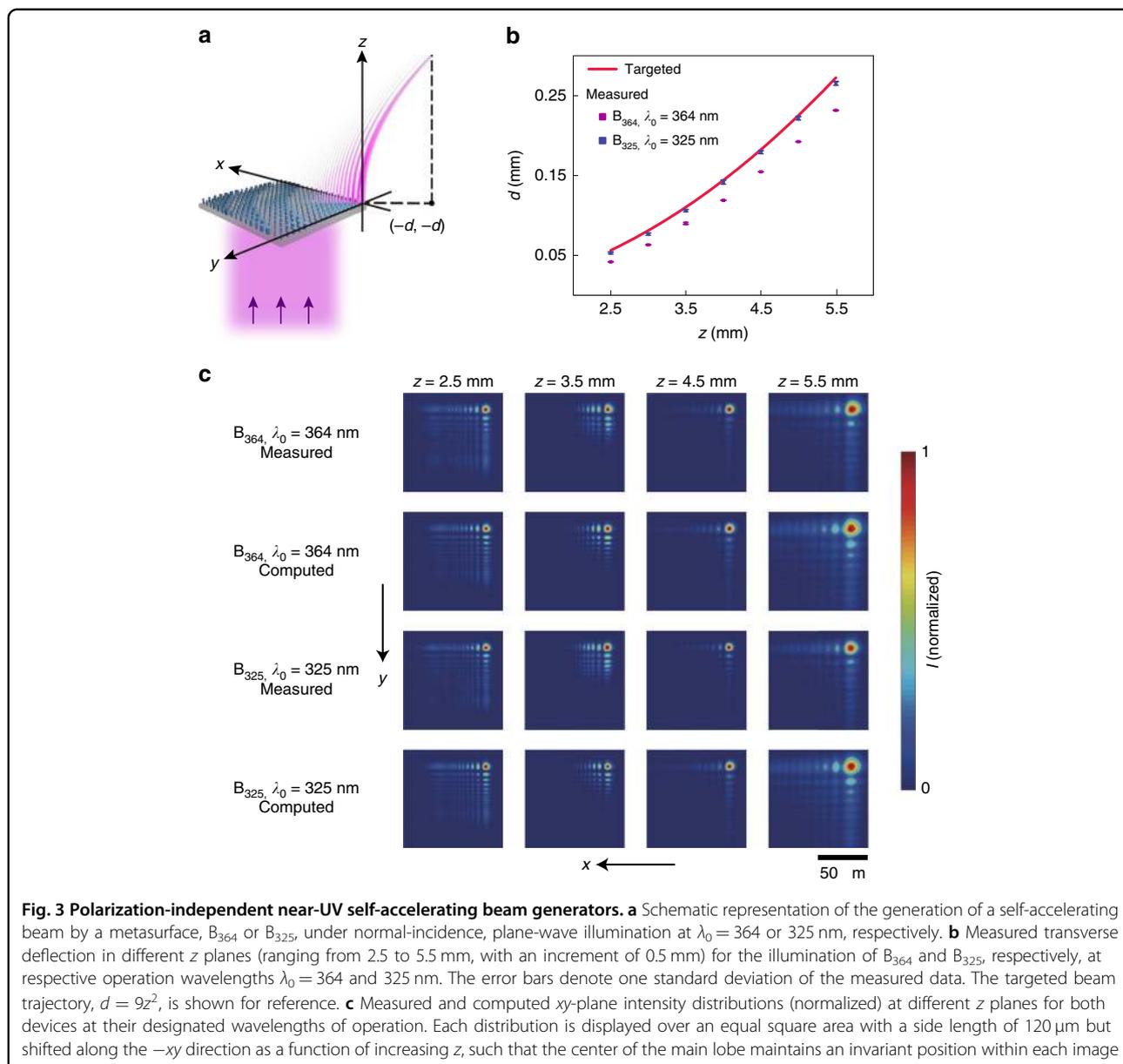
We first demonstrate lenses, self-accelerating beam generators, and holograms based on polarization-independent metasurfaces consisting of nanopillars with in-plane circular cross-sections, that operate at near-UV wavelengths of 364 and 325 nm (corresponding to emission lines of argon-ion and helium–cadmium lasers, respectively) with efficiencies up to 72%. Further exploiting the high patterning fidelity of the Damascene technique and leveraging the negligible optical loss of the as-deposited  $\text{HfO}_2$  dielectric material across most of the UV regime, we scale down the metasurface critical dimensions to realize polarization-independent holograms operating at a deep-UV wavelength of 266 nm (corresponding to the emission line of an optical parametric oscillator pumped by a nanosecond Q-switched Nd:YAG laser), with relatively high efficiencies (>60%). Finally, by opening up the design space with the three degrees of freedom provided by elliptically shaped nanopillars ( $\theta$ ,  $D_1$ , and  $D_2$ ), compared to the single degree of freedom provided by circularly shaped nanopillars ( $D$ ), we realize spin-multiplexed metasurfaces that impart independent phase shift profiles onto light emerging from the device under illumination with left-handed circularly polarized (LCP) or right-handed circularly polarized (RCP) light. The implemented self-accelerating beam generators and spin-multiplexed metaholograms operate at UV wavelengths of 364 and 266 nm, respectively, with efficiencies up to 61%.

### Polarization-independent UV metasurfaces

Each polarization-independent metasurface implemented in this study (lens, self-accelerating beam generator, and hologram) consists of a square lattice of  $\text{HfO}_2$  cylindrical nanopillars, where the diameter of each pillar varies as a function of its position within the lattice. Each nanopillar acts as a truncated dielectric waveguide with top and bottom interfaces of low reflectivity, through which light propagates with a transmittance and phase shift controlled by the pillar height  $H$ , pillar diameter  $D$ , and lattice spacing  $P$ . For each targeted operation wavelength ( $\lambda_0 = 364, 325$ , and  $266 \text{ nm}$ ), a corresponding pillar height ( $H = 550, 500$ , and  $400 \text{ nm}$ , respectively) and subwavelength lattice spacing ( $P = 200, 190$ , and  $150 \text{ nm}$ , respectively) are chosen, along with a range of pillar diameters that yield phase shifts varying over a full range of  $2\pi$ , while maintaining a relatively high and constant transmittance ( $[50, 160 \text{ nm}]$ ,  $[50, 150 \text{ nm}]$ , and  $[50, 110 \text{ nm}]$ , respectively). The detailed design procedure is elaborated in Supplementary Information, Section VIII.

As a first demonstration of polarization-independent UV metasurfaces, two  $500\text{-}\mu\text{m}$ -diameter, polarization-independent metalens designs,  $L_{364}$  and  $L_{325}$ , with an identical numerical aperture of  $\text{NA} = 0.6$  (corresponding to a focal length of  $f = 330 \mu\text{m}$ ), are implemented to focus UV light at respective free-space wavelengths of  $\lambda_0 = 364$  and  $325 \text{ nm}$  (Fig. 2a). Singlet-mode focusing of a plane wave can be achieved by implementing the radially symmetric phase shift function  $\phi^L(x, y, \lambda_0) = \text{mod}((2\pi/\lambda_0)(f - \sqrt{x^2 + y^2 + f^2}), 2\pi)$ , where  $f$  is the focal distance normal to the plane of the lens (along the  $z$  direction),  $x$  and  $y$  are in-plane distances along orthogonal directions from the center of the lens, and normal incidence is assumed. Each measured intensity distribution at the metalens focal plane (Supplementary Information, Section IX) reveals a circularly symmetric focal spot, characterized by a cross-section that closely matches the intensity distribution theoretically predicted for a diffraction-limited lens with a numerical

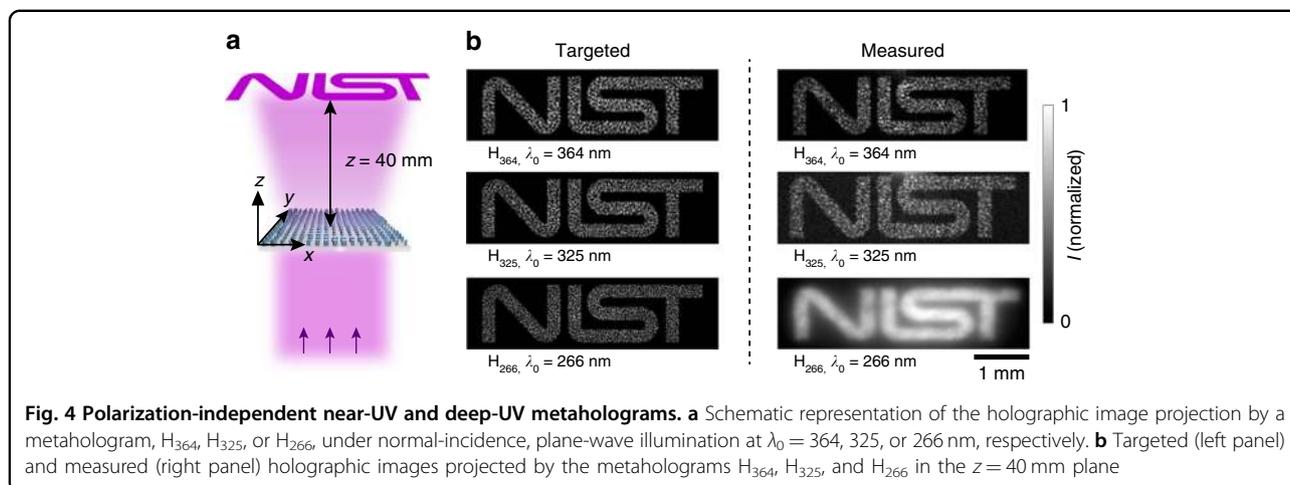




aperture of  $\text{NA} = 0.6$  and given by the Airy disk function  $I(x) = [2J_1(A)/A]^2$ , where  $J_1$  is the Bessel function of the first kind of order one, and  $A = 2\pi\text{NA}x/\lambda_0$  (Fig. 2b, c). Metalens  $L_{325}$  exhibits a less-than-ideal focusing profile with larger side lobes, which could be due to fabrication imperfections and a nonideal realization of the required phase shift profile. The focusing efficiencies, defined as the ratio of the optical power of the focused spot to the total power illuminating the metalens, are  $(55.17 \pm 2.56)\%$  ( $L_{364}$ ) and  $(56.28 \pm 1.37)\%$  ( $L_{325}$ ). The cited uncertainties represent one standard deviation of the measured data.

Next, we demonstrate polarization-independent metasurfaces that can transform a normally incident plane wave into a diffraction-free output beam propagating

along a curved trajectory, i.e., a self-accelerating beam (SAB)<sup>31–33</sup>. Two  $270\text{-}\mu\text{m}$ -square SAB generator designs,  $B_{364}$  and  $B_{325}$ , are implemented for operation at the respective wavelengths of 364 and 325 nm (Fig. 3a). The SAB generator design and operation are conveniently described using a Cartesian coordinate system in which the constituent metasurface is located in the  $z = 0$  plane and the first  $xy$  quadrant, with one corner positioned at the origin. The implemented SAB for each targeted free-space wavelength,  $\lambda_0 = 364$  and  $325$  nm, is characterized by an L-shaped wave-packet of the main lobe centered on the trajectory  $y = x = -az^2$ , where  $a = 9 \text{ m}^{-1}$  (in other words, originating from  $(0, 0, 0)$  and propagating in the  $+z$  direction in a curved trajectory confined to the plane



**Fig. 4 Polarization-independent near-UV and deep-UV metaholograms.** **a** Schematic representation of the holographic image projection by a metahologram,  $H_{364}$ ,  $H_{325}$ , or  $H_{266}$ , under normal-incidence, plane-wave illumination at  $\lambda_0 = 364, 325,$  or  $266$  nm, respectively. **b** Targeted (left panel) and measured (right panel) holographic images projected by the metaholograms  $H_{364}$ ,  $H_{325}$ , and  $H_{266}$  in the  $z = 40$  mm plane

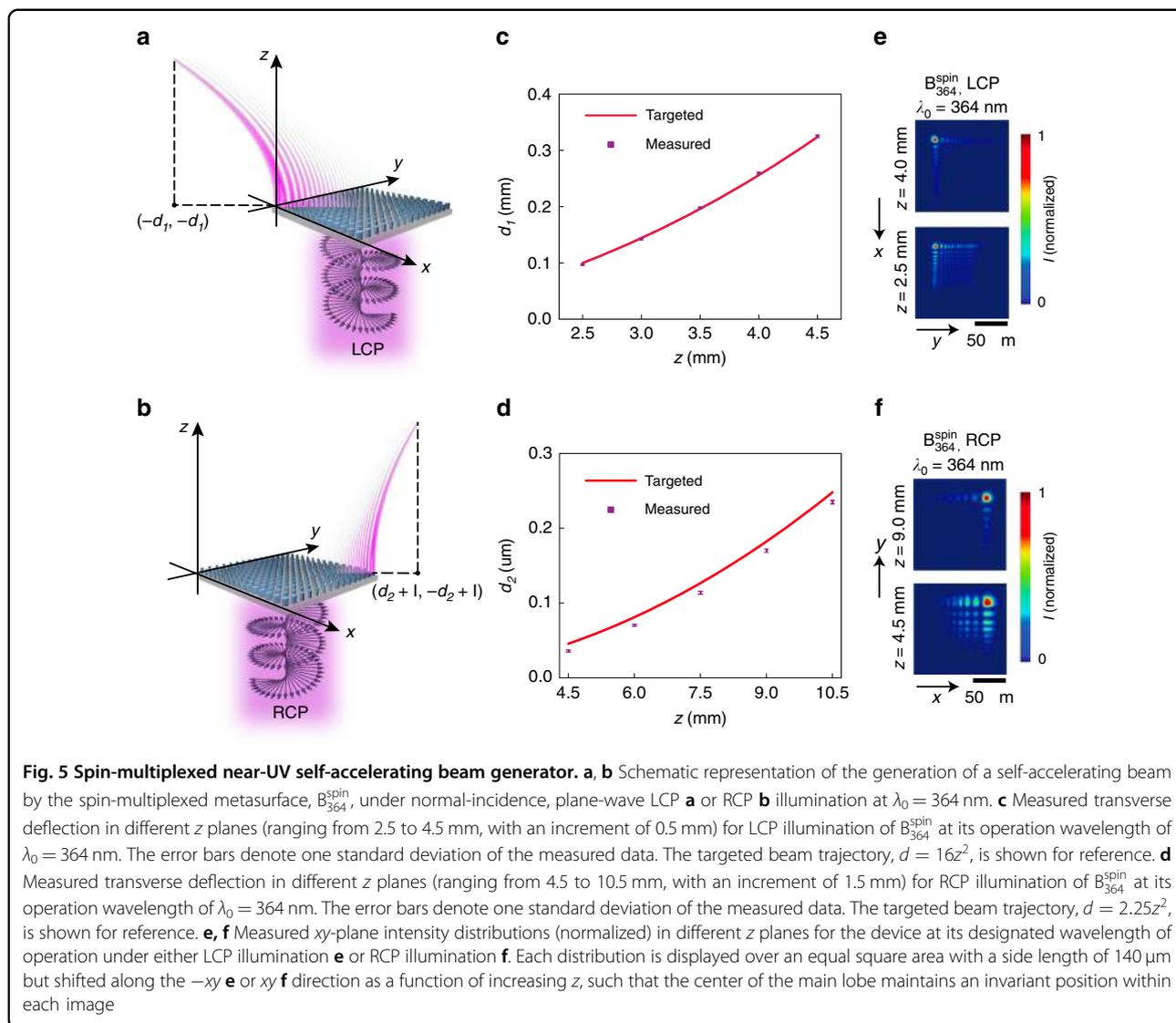
$y = x$  with a height above the surface given by  $z = \sqrt{d/a}$ , where  $d = |x| = |y|$  is the lateral displacement). The targeted SAB can be generated by implementing a phase shift profile  $\phi^B(x, y, \lambda_0) = \text{mod}(-\frac{8\pi}{3\lambda_0} \sqrt{a}(x^2 + y^2), 2\pi)$  in the metasurface<sup>34</sup>. The measured lateral displacement values  $d(z)$  are observed to closely match, in each case, the calculated values based on the targeted trajectory (Fig. 3b and Supplementary Information, Section X). The experimental SAB generated by each device exhibits diffraction-free characteristics with  $xy$ -plane intensity distributions similar to the intensity distributions numerically computed using the angular spectrum representation method<sup>35</sup>, assuming an ideal metasurface realization with both the designed phase shift profile  $\phi^B$  and unity transmittance  $T$  (Fig. 3c). The measured efficiencies, defined as the ratio of the total optical power of the SAB in the  $z = 5$  mm plane to the total power illuminating the metasurface, are  $(46.75 \pm 2.31)\%$  ( $B_{364}$ ) and  $(67.42 \pm 4.43)\%$  ( $B_{325}$ ). The efficiencies compare favorably to that of a recently reported  $\text{TiO}_2$ -based self-accelerating beam generator operating at visible frequencies<sup>36</sup>.

As a final demonstration of polarization-independent UV metasurfaces, we demonstrate three metaholograms, denoted  $H_{364}$ ,  $H_{325}$ , and  $H_{266}$ , operating at three respective UV wavelengths  $\lambda_0 = 364, 325,$  and  $266$  nm (Fig. 4a). Implementing computer-generated holograms with metasurfaces enables high-efficiency and low-noise operation, fine spatial resolution, a compact footprint, and multiplexing capability<sup>37–40</sup>. Each demonstrated metahologram, which occupies a square area with a side length of  $270 \mu\text{m}$ , is mapped to a Cartesian coordinate system in which the constituent metasurface is located in the  $z = 0$  plane and the first  $xy$  quadrant, with one corner positioned at the origin. The Gerchberg–Saxton algorithm<sup>41</sup> is employed to calculate the phase shift profiles,  $\phi_{364}^H(x, y, \lambda_0)$ ,  $\phi_{325}^H(x, y, \lambda_0)$ , and  $\phi_{266}^H(x, y, \lambda_0)$ , required to project a holographic “NIST” image located in the  $z =$

$40$  mm plane, under normal-incidence, plane-wave illumination (Supplementary Information, Section XI). An additional offset of  $y = -3$  mm is added to avoid overlap of the generated holographic image with the residual directly transmitted beam. The images projected by metaholograms  $H_{364}$ ,  $H_{325}$ , and  $H_{266}$  are measured (Supplementary Information, Sections XII and XIII) and displayed in the right panel of Fig. 4b. Each of the experimental holographic images faithfully replicates the shape of the corresponding target image (left panel of Fig. 4b), numerically computed assuming an ideal metahologram realization with both the designed phase shift profile  $\phi^H$  for a given operation wavelength and unity transmittance  $T$ . In addition, the speckle patterns filling the shapes of the measured images projected by metaholograms  $H_{364}$  and  $H_{325}$  exhibit numerous similarities with those of the corresponding target images; the as-measured holographic image projected by metahologram  $H_{366}$  does not offer the possibility of such a comparison due to the employed fluorescence transduction characterization scheme, which washes out the details of the speckle patterns. The measured efficiencies for metaholograms  $H_{364}$  and  $H_{325}$ , defined as the ratio of the total optical power of the holographic image to the total power illuminating the structure, are  $(62.99 \pm 4.14)\%$  and  $(71.78 \pm 2.06)\%$ , respectively. The measured efficiency for metahologram  $H_{266}$ , defined as the ratio of the total fluorescence power of the holographic image to the fluorescence power of the light illuminating the structure (Supplementary Information, Section XIII), is  $(60.67 \pm 2.60)\%$ . These efficiency values are comparable to those of recently reported  $\text{TiO}_2$ -based metaholograms operating in the visible range<sup>26</sup>.

#### Spin-multiplexed UV metasurfaces

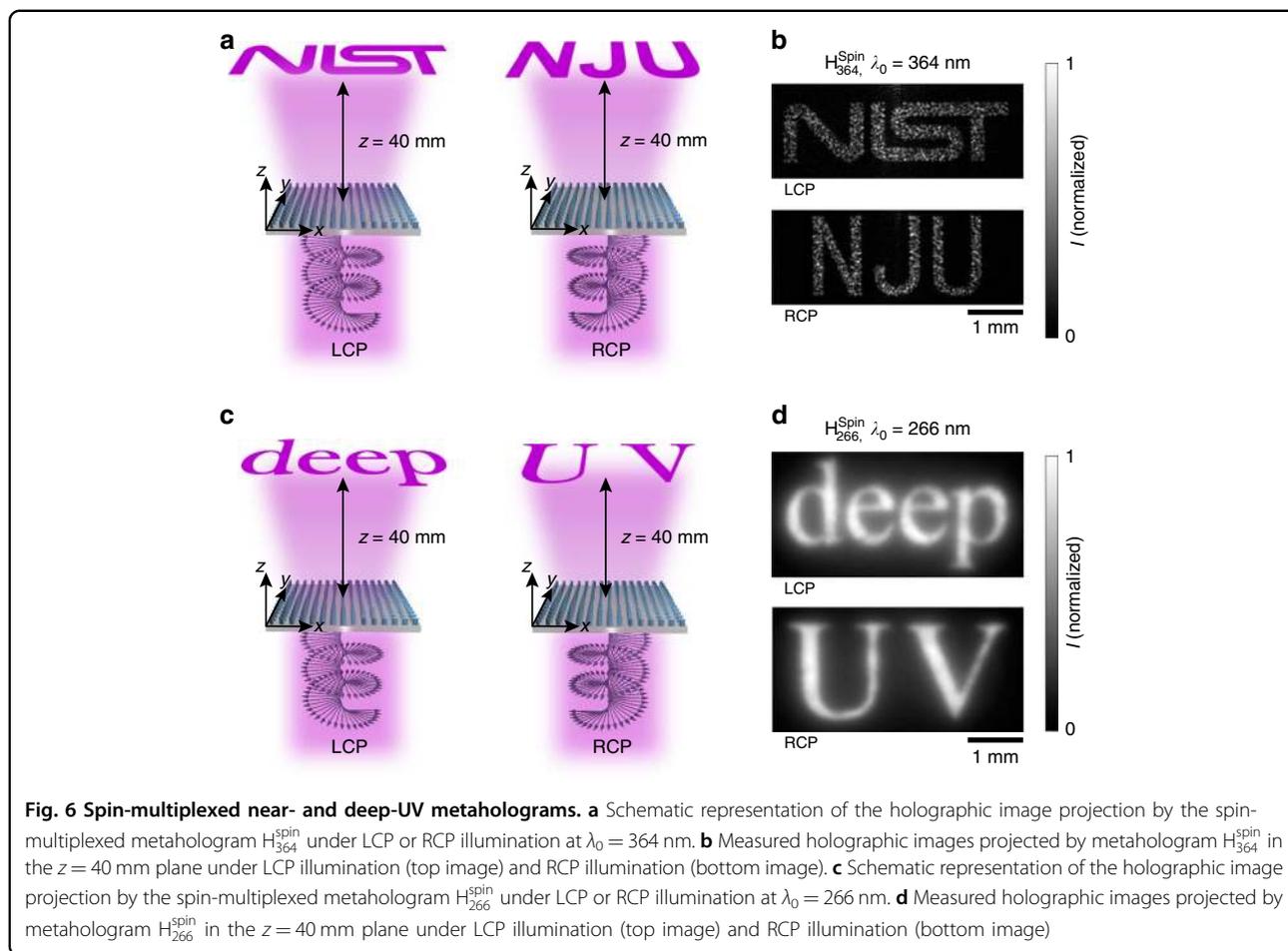
Metasurfaces have been demonstrated to switch between distinct optical outputs, such as different holographic images or differently oriented beams, under the



control of the fundamental optical state of the input beam, e.g., polarization<sup>42,43</sup>, or a spatial feature of the input beam such as the angle of incidence<sup>44</sup>. Here, we demonstrate, for the first time, spin-multiplexed UV metasurfaces that can switch between distinct outputs depending on the handedness of the input light (left-hand circularly polarized, LCP, or right-hand circularly polarized, RCP). The detailed design procedure is elaborated in Supplementary Information, Section XIV.

As a first demonstration of a polarization-dependent, spin-multiplexed UV metasurface, we implement a self-accelerating beam generator operating at  $\lambda_0 = 364$  nm, denoted as  $B_{364}^{\text{spin}}$ , that generates SABs following different trajectories under the control of the handedness of circularly polarized incident light. The spin-multiplexed SAB generator, which occupies a square area with a side length of

$l = 330 \mu\text{m}$ , is referenced to a Cartesian coordinate system in which the constituent metasurface is located in the  $z = 0$  plane and the first  $xy$  quadrant, with one corner positioned at the origin. Two distinct phase shift profiles,  $\phi^{\text{LCP}}(x, y, \lambda_0) = \text{mod}\left(-\frac{8\pi}{3\lambda_0} \sqrt{16}(x^{\frac{3}{2}} + y^{\frac{3}{2}}), 2\pi\right)$  and  $\phi^{\text{RCP}}(x, y, \lambda_0) = \text{mod}\left(-\frac{8\pi}{3\lambda_0} \sqrt{2.25}\left((l-x)^{\frac{3}{2}} + (l-y)^{\frac{3}{2}}\right), 2\pi\right)$ , are targeted for the device operation to yield SABs exiting the metasurface from opposite corners and following different trajectories,  $y = x = -d_1 = -16z^2$  and  $(y-l) = (x-l) = d_2 = 2.25z^2$ , under LCP and RCP illuminations, respectively (Fig. 5a, d). The measured lateral displacement values,  $d_1(z)$  and  $d_2(z)$ , are observed to closely match, in each case, the calculated values based on the targeted trajectory (Fig. 5c, d). The experimental SAB generated by the device exhibits



diffraction-free characteristics with  $xy$ -plane intensity distributions (Fig. 5e, f) similar to the targeted intensity distributions (Supplementary Information, Figs. S14 and S15), numerically computed assuming an ideal metasurface realization with both the designed phase shift profile  $\phi^{\text{LCP}}$  ( $\phi^{\text{RCP}}$ ) and unity transmittance  $T$ . The measured efficiency under LCP illumination (RCP illumination), defined as the ratio of the total optical power of the SAB in the  $z = 4.5$  mm [ $z = 10.5$  mm] plane to the total power illuminating the metasurface, is  $(38.42 \pm 1.95)\%$  [ $(61.90 \pm 2.03)\%$ ]. The reduced efficiency under LCP illumination, compared to the RCP case, can be attributed to challenges associated with implementing a phase shift profile of a higher spatial gradient (Supplementary Information, Section XVI).

Next, we demonstrate a spin-controlled metahologram operating at the same near-UV wavelength of 364 nm. The  $330\text{-}\mu\text{m}$ -square metahologram,  $H_{364}^{\text{spin}}$ , located in the  $z = 0$  plane, is designed to project a holographic “NIST” image (for LCP illuminating light) and “NJU” image (for RCP illuminating light) at  $\lambda_0 = 364$  nm, all located in the  $xy$ -plane at  $z = 40$  mm with an offset of  $y = -3$  mm (Fig. 6a; the corresponding phase shift profiles are plotted in the Supplementary Information, Fig. S17). Both of the

experimentally captured holographic images (Fig. 6b) faithfully replicate the shape of the corresponding targeted image computed from the designed phase profiles, including some fine grain details (Supplementary Information, Fig. S18). The measured efficiencies, defined as the ratio of the total optical power of the holographic image to the total power illuminating the metahologram, are  $(54.02 \pm 2.22)\%$  (under LCP illumination) and  $(53.76 \pm 2.42)\%$  (under RCP illumination), respectively.

Finally, a spin-multiplexed metahologram,  $H_{266}^{\text{spin}}$ , occupying a square area with a side length of  $320\text{ }\mu\text{m}$ , is implemented for operation at the deep-UV wavelength of 266 nm. The device, located in the  $z = 0$  plane, is designed to project, at  $\lambda_0 = 266$  nm, a holographic “deep” image for LCP illumination and a holographic “UV” image for RCP illumination, where both images are located in the  $z = 40$  mm plane with a lateral offset of  $y = -3$  mm (Fig. 6c; the corresponding phase shift profiles are plotted in the Supplementary Information, Fig. S19). Each of the experimental holographic images (Fig. 6d) faithfully replicates the shape of the corresponding target image (Supplementary Information, Fig. S20), including subtle details of the chosen font, such as the linewidth variation

and serif. The measured efficiencies, defined as the ratio of the total fluorescence power of the holographic image to the fluorescence power of light illuminating the structure, are  $(58.95 \pm 1.95)\%$  under LCP illumination and  $(61.23 \pm 1.49)\%$  under RCP illumination.

## Discussion

Given the negligible extinction coefficient of the low-temperature-ALD deposited  $\text{HfO}_2$  down to its bandgap ( $\lambda_0 \approx 217$  nm) and the high patterning fidelity of the Damascene process, it should be straightforward to push the metasurface operation wavelengths to significantly shorter values than those demonstrated here. In addition, an experimental demonstration of a broader range of device functionalities in the deep-UV regime other than hologram projection should be possible by using a continuous-wave light source and an appropriate direct imaging system. Moreover, the efficiency of  $\text{HfO}_2$ -based metasurface devices can be improved by further optimizing the Damascene process or by employing advanced metasurface design strategies, such as topology optimization<sup>45</sup> and the generalized Huygens principle<sup>46,47</sup>.

In conclusion, an assortment of high-performance metasurface components operating in the UV regime, including wavelengths down to the record-short deep-UV range, is demonstrated by using  $\text{HfO}_2$ , a CMOS-compatible, wide-bandgap, and low-loss dielectric material, and an associated fabrication process based on low-temperature ALD and Damascene lithography. This approach paves the way towards further development of “flat” UV optical elements with customized functionalities and their integration into chip-scale nanophotonic systems, enabling applications such as atom trapping, fluorescence imaging, and circular dichroism spectroscopy with a compact form factor.

## Materials and methods

### Metasurface fabrication process

As the first step in the metasurface fabrication process, 500- $\mu\text{m}$ -thick, double-side-polished UV-grade fused silica wafers are vapor-coated (150 °C) with an adhesion-enhancing monolayer of hexamethyldisilazane (HMDS). A layer of ZEP 520A resist is spin-coated onto the substrate, followed by baking on a hot plate at 180 °C for 10 min. The spin speed is adjusted to yield a resist thickness varying between 400 and 550 nm (as characterized by spectroscopic ellipsometry), depending on the specific metasurface design. To suppress charging during electron beam (e-beam) lithography, a 20-nm-thick Al layer is thermally evaporated onto the ZEP layer (deposition rate of 0.1 nm/s). The ZEP-resist template is fabricated using e-beam lithography (accelerating voltage of 100 kV and beam current of 0.2 nA), followed by Al layer removal (AZ 400 K 1:3 developer for 2 min and DI water for 1 min) and resist development (hexyl

acetate for 2 min and isopropyl alcohol for 30 s). The deposition of  $\text{HfO}_2$  (deposition rate: 0.11 nm/cycle) is then performed using the low-temperature ALD described below. For all of the processed structures, the deposition thickness is chosen to be 200 nm, which not only exceeds the largest radius (or the largest semi-minor axis length) of the circular (or elliptical) openings of the exposed resist patterns for all metasurface designs, providing complete filling of the patterns, but also provides a substantial over-coating of the resist, yielding a quasi-planar top surface (Supplementary Information, Section VI). Following the ALD, the  $\text{HfO}_2$  layer is back-etched to the resist top surface using argon (Ar) ion milling ( $\text{HfO}_2$  mill rate of  $\approx 0.4$  nm/s). During the Ar ion milling, a non-patterned, planar  $\text{HfO}_2$  sample of the same initial thickness is also back-etched, and its film thickness is periodically monitored by spectroscopic ellipsometry to ensure that a proper milling time is employed. Finally, the remaining resist is removed by soaking in a solvent, yielding circular or elliptical  $\text{HfO}_2$  posts with smooth and straight sidewall profiles (due to the resist templating process), heights varying from 400 to 550 nm (depending on the specific metasurface), and aspect ratios varying from  $\approx 3$  to  $\approx 11$ .

### Low-temperature TDMAH-based $\text{HfO}_2$ ALD

In step 1 of the ALD cycle, TDMAH vapor ( $\text{Hf}[(\text{CH}_3)_2\text{N}]_4$ ) is pulsed into the ALD chamber for a duration of  $t_1 = 1$  s, reacting with the dangling O–H bonds on the hafnium-coated surface to create a new solid monolayer of  $\text{Hf}[(\text{CH}_3)_2\text{N}]_2\text{O}$  and generate the gas by-product  $(\text{CH}_3)_2\text{NH}$  (dimethylamine). In step 2, high-purity nitrogen ( $\text{N}_2$ ) gas is flowed for a duration of  $t_2 = 75$  s to fully remove any un-reacted TDMAH vapor and dimethylamine by-product from the chamber. In step 3, water vapor is pulsed into the chamber for a duration of  $t_3 = 60$  ms, reacting with the  $\text{Hf}[(\text{CH}_3)_2\text{N}]_2\text{O}$  to create a monolayer of  $\text{HfO}_2$  on the surface. Finally, in step 4, the excessive water vapor and the dimethylamine reaction by-product are completely removed from the chamber by  $\text{N}_2$  purging for a duration of  $t_4 = 75$  s.

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**Author contributions**

The project was initiated by C.Z. The device fabrication and characterization were performed by C.Z., S.D., W.Z., and A.A. The simulations were performed by Q.F., S.D., C.Z. with further analysis by Y.L., T.X., and H.J.L. All authors contributed to the interpretation of results and participated in the manuscript preparation.

**Conflict of interest**

The authors declare that they have no conflict of interest.

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