

Microstructured Tellurite Glass Fibre Laser Development

by Michael Raymond Oermann

A Thesis Submitted to the University of Adelaide for the degree of

DOCTOR OF PHILOSOPHY

in the
Faculty of Science
School of Chemistry & Physics

November 2011

Supervisors:	
Prof. Tanya Monro, Principal Supervisor	
A/Prof. Peter Veitch, Co-supervisor	
A/Prof. Heike Ebendorff-Heidepriem, Co-superv	— visor
Dr. David Ottaway, Co-supervisor	

The University of Adelaide Adelaide, South Australia November, 2011

CONTENTS

Mi	crostr	uctured	Tellurite Glass Fibre Laser Development	i
CC	NTE	NTS		v
ΑF	BSTR A	ACT		ix
DE	ECLAI	RATIO	N	xi
A(CKNO	WLED	GMENTS	xiii
PU	BLIC	ATION	IS DURING CANDIDATURE	xv
LIS	ST OF	TABL	ES	xvii
LIS	ST OF	FIGU	RES	xix
LIS	ST OF	ABBR	REVIATIONS	xxix
GI	LOSSA	ARY		xxx
1.	Intro	duction		1
	1.1	Resear	rch Motivation	1
	1.2	State-	of-the-Art	3
		1.2.1	Tellurite Glass Development	4
		1.2.2	Microstructured Fibre Development	9
		1.2.3	Tellurite Fibre Development	16
		1.2.4	Tellurite Glass Laser Development	20
		1.2.5	Erbium 3µm Fibre Laser Development	23
	1.3	Projec	ts Aims and Thesis Structure	28
2.	Tellu	urite Glass Development		
	2.1	Glass	Fabrication	34
	2.2	Mater	ial Transmission Loss	36
		2.2.1	Bare fibre loss measurements	36
		2.2.2	FTIR measurements looking at the OH absorption and IR tr	
	2.3	Densit	·V	47

	2.4	Glass	Transition Temperature and Crystallisation Stability	49
	2.5	Refrac	etive Index	52
	2.6	Viscos	sity/Temperature Relations	57
	2.7	Glass	Tellurite Glass Development Summary	62
3.	Fibre	Model	ling and Fabrication	65
	3.1	Fibre 1	Fabrication	66
		Extrus	sion	66
		Fibre o	drawing	68
	3.2	Large	Mode Area Microstructured Fibres	70
		3.2.1	Modelling of four-ring LMA fibres	70
		3.2.2	Fabrication of 4-ring LMA fibres	76
	3.3	Core d	loped four-ring LMA fibres	81
		3.3.1	Modelling of core-doped LMA fibres	81
		3.3.2	Fibre fabrication and analysis	83
	3.4	Small	Core Microstructured Fibres	90
		3.4.1	Small core seven-ring fibre	91
		3.4.2	Small core four-ring structure	92
		3.4.3	Wagon Wheel Fibre	96
		3.4.4	6μm core, wagon wheel fibre	. 100
4.	Erbiu	ım III d	oped tellurite glass spectroscopic properties	. 103
	4.1	Absor	ptionption	. 103
	4.2	Energ	y Level Lifetimes	. 107
		4.2.1	Judd-Ofelt analysis, predicting the radiative energy level lifetimes	. 107
		4.2.2	Non-radiative decay	. 113
		4.2.3	Experimental lifetime measurements	. 114
	4.3	Emiss	ion Cross-section	. 122
5	Lase	r Devel	opment and Results	. 129

	5.1	Steady	state laser threshold calculations	130
	5.2	Bulk glass laser modelling and experiments		
		5.2.1	Laser setup modelling and results	134
		5.2.2	Free space laser testing using phosphate glass slab	144
		5.2.3	Bulk tellurite laser experiments	147
		5.2.4	Bulk glass experimental outcomes	148
	5.3	Fibre 1	aser setup, modelling and results	154
		5.3.1	Determining the optimal dopant concentration	155
		5.3.2	Thermal modelling of the wagon wheel fibre	157
		5.3.3	Fibre laser setup	162
		5.3.4	Fibre laser results	163
		5.3.5	Future Outlook	172
6.	Conc	lusions		177
Ap	pendi	x 1		181
1.1	Glass	Fabric	ation	181
1.2	Dens	ity Mea	surements	183
1.3 Refractive Index Measurements				184
1.4	Glass	Stabili	ty Measurements	185
1.5	Redu	cing the	e OH concentration in the glass	185
Appendix 2: Analytical modelling of the three level laser modelling				
Ap	Appendix 3: Publications during candidature			
D _O	ferenc	ec		212

ABSTRACT

This thesis contains a study of the suitability of tellurite glass for use in microstructured fibre lasers. This thesis looks into the possibility for lasing at around 3µm, where tellurite glass is transparent. To test the lasing potential of fabricated tellurite glass microstructured fibres, lasing at 1.5µm was demonstrated.

The research contained within this thesis includes: The development and characterisation of the tellurite glass composition; including modifications made to this composition to match the refractive indices of the doped and undoped glasses, reducing the glass material loss, finding the glass crystallisation stability and density as well as measuring the temperature dependence of the glass melt viscosity, of which an understanding is required for its extrusion (Chapter 2). The fabrication of microstructured tellurite fibres which included large mode area fibres, motivated by the desire to fabricate a double clad fibre and the development of small core fibres which were used in the fibre laser experiments (Chapter 3). A spectroscopic study of the erbium III doped glass including lifetimes, absorption and emission measurements (Chapter 4) and a description of the laser modelling, experiments and results (Chapter 5).

DECLARATION

I confirm that this work contains no material which has been accepted for the award of any other degree or diploma in any university or other tertiary institution to Michael Oermann and, to the best of my knowledge and belief, contains no material previously published or written by another person, except where due reference has been made in the text.

I give consent to this copy of my thesis when deposited in the University Library, being made available for loan and photocopying, subject to the provisions of the Copyright Act 1968.

The author acknowledges that copyright of published works contained within this thesis (listed on page and presented in Appendix 3) resides with the copyright holder(s) of those works.

I also give permission for the digital version of my thesis to be made available on the web, via the University's digital research repository, the Library catalogue, the Australasian Digital Theses Program (ADTP) and also through web search engines, unless permission has been granted by the University to restrict access for a period of time.

Signed:		
Date:		

ACKNOWLEDGMENTS

I would like to acknowledge a number of people for the assistance they have given me throughout my PhD.

My supervisors, Tanya Monro, Peter Veitch, Heike Ebendorff-Heidepriem and David Ottaway, have provided me with an immense amount time and effort on assisting me through every component of this project.

The optics and photonics research group as a whole. The ideas and suggestions that have been provided to me by the group, whether in a group meeting or over lunch have seen the solving of many problems that have arisen throughout this research.

The technical support that I have been given. This includes Roger Moore for a significant amount of the fibre fabrication, Alastair Dowler for some of the fibre drawing and a large amount of assistance in the workshop, Adrian Selby for machining work early in this project and Blair Middlemiss for training me in the use of the workshop machinery and for the organisation of many group social barbeques.

I would like to acknowledge the assistance provided to me to generate the results presented in Chapter 2, particularly in the glass making which was a joint effort by Herbert Foo, Kevin Kuan and Katarina Markulic. Other measurements included the DSC measurements organised by Sean Manning, and FTIR measurements done by Kevin Kuan. A special thank you to Dr Jim Richards who assisted me with the alignment of the free space laser resonator. His experience and patience was much appreciated.

This research began as a collaborative project supported by DSTO. I would therefore like to thank DSTO for their initial funding and direction for this area of work. I would also like to thank Alex Hemming, Bradley Clare, Kerry Mudge and Ken Grant for the useful discussions that occurred during this time.

I would also like to thank DSTO for the use of their equipment including their CARY spectrophotometer, and ANU for the use for their prism coupler for refractive index measurements.

I would like to achnowledge the administrative support provided by Olivia Towers and Sara Boffa who constantly help with ensuring I have completed any required paper work as well as organise any university related travel.

On a personal side, I would like to extend my thanks to my friends and family. My parents, Ray and Heather, for supporting me and providing me with the educational background required to undergo this research. I would like to acknowledge my siblings, Alison, Andrew, Catherine and Elizabeth. I know they will all succeed in everything they pursue. Most importantly, I would like to thank my wife Belinda. She has been a great motivator and has supported me through my ups and downs during my research candidature, she is my world.

PUBLICATIONS DURING CANDIDATURE

Journal publications:

- M.R. Oermann, H. Ebendorff-Heidepriem, Y. Li, T.-C. Foo, T.M. Monro, "Index matching between passive and active tellurite glasses for use in microstructured fiber lasers: Erbium doped lanthanum-tellurite glass", Optics Express 17 (18), 15578-15584, August 2009
- M. Oermann, H. Ebendorff-Heidepriem, D. Ottaway, D. Lancaster, P. Veitch, T.M. Monro, "Extruded microstructured fiber lasers", Submitted to Photonics Technology Letters

First author refereed conference papers (accepted for invited talk):

M. Oermann, D. Ottaway, H. Ebendorff-Heidepriem, P. Veitch, T.M. Monro "Tellurite Glass for use in 2.3μm Thulium Fibre Lasers" IQEC/CLEO Pacific Rim 2011, Sydney, August 2011

First author refereed conference papers (accepted for oral presentation):

- M. Oermann, D. Ottaway, H. Ebendorff-Heidepriem, P. Veitch, T.M. Monro "Microstructured Erbium Doped Tellurite Fibre Laser" 19th Australian Institute of Physics Congress/35th Australian Conference on Optical Fibre Technology (ACOFT/AIP), Melbourne, December 2010
- M.R. Oermann, D. Ottaway, P. Veitch, H. Ebendorff-Heidepriem, T.M. Monro, "Erbium-doped bulk tellurite glass laser at 1.5 μ m", Australian Conference on Optics, Lasers and Spectroscopy (ACOLS), Adelaide, December 2009.
- M.R. Oermann, H. Ebendorff-Heidepriem, Y. Li, T.M. Monro, "Spectroscopy of erbium in La³⁺-doped tellurite glass & fibres", Australian Conference on Optical Fibre Technology (ACOFT), Sydney, July 2008

Co-author refereed conference papers (accepted for oral presentation):

- Y. Li, M. Oermann, H. Ebendorff-Heidepriem, T.M. Monro, "Simultaneous infrared and visible emission in Er³⁺-doped ZBLAN fibre", International Commission for Optics (ICO), Sydney, July 2008
- H. Ebendorff-Heidepriem, T.C. Foo, Y. Li, M. Oermann, T.M. Monro, "New tellurite glasses for erbium fibre lasers", Australian Conference on Optical Fibre Technology (ACOFT), Sydney July 2008

Conference abstracts (accepted for oral presentation):

M.R. Oermann, Y. Li, H. Ebendorff-Heidepriem, T.M. Monro, "Core doped tellurite microstructured optical fibre for erbium fibre laser at $2.7\mu m$ ", AIP Congress 2008 AOS, Adelaide, December 2008

Michael R. Oermann, Heike Ebendorff-Heidepriem, David Ottaway, Peter Veitch, Tanya M. Monro, "Tellurite glass microstructured fibre laser development", PACRIM 2011, Cairns, July 2011

LIST OF TABLES

Table 1: Glass loss at $3.3\mu m$ for the bulk glasses varying the melt time and glass
agitation46
Table 2: Measured glass transition temperatures and crystallization stability for doped
and undoped base tellurite glass and lanthanum tellurite glass
Table 3: Table of the measured refractive indices for both doped and undoped glass
samples for both the base glass and the lanthanum tellurite glass
Table 4: Difference in refractive index for differing cladding air fractions
Table 5: Absorption cross-sections for the ground state absorption transitions in erbium
III doped TZN and TZNL glasses
Table 6: The matrix elements $\boldsymbol{U}(\boldsymbol{t})$ and the magnetic dipole contribution to the oscillator
strength for erbium III given a glass refractive index of 1.983 at 1550nm [179-181].
Table 7: Results for the Judd-Ofelt analysis on the TZN glass including the transition,
the emission wavelength between the barycentres of the transitions, radiative decay
rate, $A_{i,j}$, for the transition from the <i>i</i> th to the <i>j</i> th energy levels, branching ratios, $\beta_{i,j}$,
for the i to j transition, and lifetime, τ_i , for the i th energy level
Table 8: Table of the non-radiative decay rates for various energy gaps in a binary
sodium tellurite glass [83, 84, 175, 183]
Table 9: Temperature coefficients for the optical path length change when the glasses are
heated
Table 10: Temperature at the core-cladding, cladding-jacket and fibre-air interfaces
dissipating its limit of 8W/m (top) and 0.4W/m (bottom) of heat
Table 11: Table of the output powers achieved with different lengths of fibre 168
Table 12: Input parameters used in the modelling of the 2.2m fibre laser



LIST OF FIGURES

Figure 1: Electronic energy level diagram for the free erbium III ion
Figure 2: Electronic energy level diagram for the free erbium III ion illustrating the
pumping at 980nm, excited state absorption (ESA) and the most significant
upconversion (ETU) processes that occur in erbium III
Figure 3: Absorption cross-sections and emission spectra for $R_2O-ZnO-TeO_2$ glasses,
where R ₂ O is the alkali metal oxide: Li ₂ O, Na ₂ O or K ₂ O. [30]
Figure 4: (a) SEM images of the first microstructured-silica fibre reported by Knight et
al. in 1996 [110] and (b) the large mode area fibre cross-section presented by
Knight et al. in 1998 [97]
Figure 5: Fibre cross-section of the effectively single mode six hole fibre (a) and the
fibre's guided mode (b) [105]
Figure 6: Cross-sectional profile of the segmented cladding fibre [134]
Figure 7: Double clad fibre structure
Figure 8: Geometry of the first microstructured structured inner and outer clad fibre used
in a laser [136]
Figure 9: The fibre geometry of a recently fabricated double clad fibre laser [101]
generating 320W at 1064nm
Figure 10: Step index tellurite fibre fabrication technique reproduced from Mori et al.
[81]
Figure 11: Large mode area tellurite fibre cross-section (a) and mode guided by the fibre
(b) (ref)
Figure 12: Photograph of the extrusion die (a), the extruded preform (b), the fibre
fabricated (c) and an image of the fibre guiding light (d) for the fibre presented by
Kumar et al. [52]
Figure 13: The laser output performance, which had a slope efficiency of 0.65%, for the
erbium III doped tellurite fibre laser presented by Mori et al. extracted from Ref.
[34]

Figure 14: The electronic energy level diagram for free Ho ³⁺ , Yb ³⁺ and Tm ³⁺ ions in
tellurite glass and transitions associated with a Ho3+-Yb3+-Tm3+ system. Image
reproduced from Ref. [35].
Figure 15: Laser performance of the Tm ³⁺ doped tellurite fibre laser along with the
laser's spectral output [35]
Figure 16: Energy level diagram from the paper by Pollnau et al. [15] describing the
cascade lasing scheme that was presented
Figure 17: Energy level diagram for erbium III including the energy transfer processes
used to achieve lasing at 2.7µm. Image reproduced from [19]
Figure 18: Photograph of a 300g tellurite glass billet containing shiny gold particles
(left) compared to a 300g billet fabricated using the revised melting procedure
aimed at reducing the scattering loss caused by these particles (right)35
Figure 19: Loss plot for the TZN glass (red) as well as the TZNL glass both doped
(green) and undoped (blue). The glasses were melted using the procedure described
in Appendix 1
Figure 20: Loss spectra for the TZNL glass melted, using the melting procedure
described in Appendix 1, in a platinum crucible compared to the loss of a glass
melted the same way using a gold crucible
Figure 21: Plot of the glass loss for TZNL glass bare fibres melted from differing
purities of raw materials. 4N, 5N and 6N correspond to a 99.99%, 99.999% and
99.999% raw material purity, respectively. When a component's purity was
increased, only that component was changed and the rest of the components
remained at purities of 4N TeO ₂ , 4N La ₂ O ₃ , 4N ZnO and 5N Na ₂ CO ₃ . The sources
of these chemicals are provided in Appendix 1
Figure 22: Plot of the IR absorption of undoped and doped (1×10 ²⁰ ions/cm ³) TZN
glasses of different batch size compared to the IR absorption of the TZNL glass
The theoretical location of the IR absorption for the two glass compositions is also
plotted for comparison. 42
Figure 23: FTIR measurements of the bulk TZNL glass' optical material loss due to OH
absorption when remelted in the glovebox (blue). The loss of an open air melted
sample (red) is plotted for comparison

Figure 24: Plot of the IR loss for the initial glovebox fabricated TZNL bulk glass
samples
Figure 25: Plot of the bulk glass loss as a function of melting time while also varying the
amount of agitation given to the melt during its melting
Figure 26: Plot of the TZNL glass density as a function of erbium III concentration. The
densities of the samples melted in open atmosphere are given in blue and the base
TZN glass given in green for comparison. The controlled atmosphere melted TZNL
glass densities are given in red
Figure 27: Example of a DSC scan for an undoped lanthanum tellurite sample 50
Figure 28: Viscosity-temperature plot of the TZNL glass including the Tg (DSC)
deformation temperature and DSC crystallisation onset temperature. The curve is
fitted from measured viscosity data discussed in section 2.6. The extrusion and fibre
drawing temperature ranges are included to illustrate their location between the
glass transition temperature and crystallization onset temperature
Figure 30: Scan of the reflected intensity from the prism/glass sample interface using a
HeNe laser and a 1×10^{20} ions/cm ³ Er ³⁺ doped TZNL glass sample. The sample
angle has been converted to refractive index and the location of the sudden drop in
intensity has been circled in red. The sampling of the data is every 1×10^{-4} refractive
index units54
Figure 29: Experimental setup for the refractive measurements using the prism coupler
The glass sample and rutile (TiO2) prism is rotated and the intensity of light
reaching the silicon detector is measured as a function of angle
Figure 31: The measured refractive indices for the TZNL glass and a fitted Sellmeier
curve are plotted. Sellmeier curves for the sodium and zinc binary tellurite glasses
[74] along with a prediction of the TZNL glass as a linear combination of these two
binary glass curves are also plotted for comparison
Figure 32: Undoped TZNL glass rod generated from the extrusion of a 100g glass billet
Figure 33: Plot of the temperature dependence of the tellurite glass viscosity. The fitted
viscosity curve along with the measured viscosity data for the doped and undoped
TZNL glass is given in blue and the viscosity data for the base TZN glasses are

given in green (doped) and red (undoped). The red line is the Arrhenius equation
found from [171] (i.e. it is not a fit to the measured data) for the TZN glass
composition61
Figure 34: Extrusion body parts used to extrude 30mm (a) and 50mm (b) billets 67
Figure 35: Photograph of the extrusion machine
Figure 36: Photograph of the fibre drawing tower
Figure 37: Illustration of the preform "neck down" and "drop" that forms at the start of a
fibre pull69
Figure 38: Microstructured optical fibre (MOF) geometry defining the structures air
filling fraction (d/ Λ) and pitch (Λ)
Figure 39: Fundamental space filling mode
Figure 40: The propagating mode through a tellurite glass microstructured fibre with a
pitch of 12.5 μm and d/ Λ of 0.5 (upper). The fundamental mode for the equivalen
step index fibre, with no air holes (lower)
Figure 41: Four-ring stainless steel die output face (top) and a side view (bottom) of ar
extruded four-ring TZN glass preform
Figure 42: Side view (a) and end view (b) of the TZN glass preform used to fabricate the
first LMA tellurite fibre and the cross-section of the fibre fabricated (c)
Figure 43: Side view (top) and end cross-section (bottom) of a LMA preform fabricated
using the TZNL glass and a larger d/Λ in the preform die
Figure 44: SEM images of some of the fabricated fibres using the TZNL glass and larger
diameter preform pins (left) along with the modes guided by these fibres (right) 80
Figure 45: Mode profile for the mode that would propagate through a fibre with the
depressed core refractive index
Figure 46: Die design for the core doped four-ring fibres
Figure 47: Optical microscope image of the first attempt at the core doped fibre. The
cladding used the TZNL glass composition and the core used the same composition
and was doped with 1×10^{20} ions/cm ³ erbium III. The fibre had an outer diameter of
240μm85
Figure 48: Optical microscope image of the core doped fibre using a tighter fitting cane
and a lower fibre drawing temperature to reduce the inflation of the gap between

the doped cane and the cladding. The cladding used the TZNL glass composition
and the core used the same composition and was doped with 1×10^{20} ions/cm
erbium III. The fibre had an outer diameter of 240µm
Figure 49: The resultant fibre geometries following the use of a vacuum to seal the core
cladding interface. The cladding once again used the TZNL glass composition and
the core used the same composition and was doped with 1×10^{20} ions/cm ³ erbium
III. These fibres all had outer diameters of 240µm
Figure 50: Fibre cross-sections with apparent fusion of the core-cladding interface. As
with the previous core doped fibres, the cladding used the TZNL glass composition
and the core used the same composition and was doped with 1×10^{20} ions/cm
erbium III. These fibres also had outer diameters of 240µm
Figure 51: The index difference between the core and cladding of a commercial SMF
silica fibre compared to a SEM of the core region of a core doped MOF 88
Figure 52: SEM image of the fibre pictured in Figure 50 (right) illustrating the nano
scale holes present at the interface between the doped core and the cladding 89
Figure 53: Pin configuration of the 7-ring die design reproduced from Ref [159] 91
Figure 54: Extruded seven-ring preform and a SEM of the seven-ring fibre pulled from
this preform92
Figure 55: Three stage fibre drawing process consisting of the caning of the structured
preform and the use of a jacket to get the desired core diameter
Figure 56: Photograph of the 0.1×10^{20} ions/cm ³ erbium III doped TZNL glass jacket and
structured preform used for both small core four-ring fibre fabrication attempts 94
Figure 57: Optical reflection microscope images of the structure of the self pressurized
small core four-ring fibre fabricated out of 0.1×10^{20} ions/cm ³ erbium III doped
TZNL glass
Figure 58: (a), the 0.1×10^{20} ions/cm ³ erbium III doped TZNL glass billet, (b), die exi
geometry, (c) and (d), the preform cross-sections, (e), a side view of the three stru
preform and (f) and (g), SEM images of the three-hole fibre
Figure 59: Image of the output of the 0.1×10^{20} ions/cm ³ erbium III doped TZNL glass
three hole fibre showing no coupling in the core (a), moderate coupling in the core
(b) and good coupling in the core (c)

Figure 60: Photograph of the die exit (a) and an image of the internal structure of the die
(b) including the feed holes the move glass from the inside of the die to the outer
ring
Figure 61: The large core three strut preform extruded from a 300g billet of 0.5×10^{20}
ions/cm ³ erbium III doped TZNL glass
Figure 62: Side and end view of the extruded TZNL glass preform after increasing the
amount of glass fed to the outside of the preform
Figure 63: Photograph made by Russell Grew of erbium III doped tellurite glass samples
increasing in dopant concentration from left to right
Figure 64: Plot of the absorption cross-sections for erbium III in TZN and TZNL glasses.
The dopant concentration was 1 x 10 ²⁰ ions/cm ³
Figure 65: Absorption cross-section for a range of erbium III concentrations
Figure 66: Experimental setup used in the lifetime measurements of the $^4I_{13/2}$ and $^4I_{11/2}$
erbium III energy levels
Figure 67: Exponential decay of the 1.5 μm fluorescence in the 10 x $10^{20}\ ions/cm^3$
erbium III doped TZN glass after excitation for 6ms and waiting for 1ms before
sampling. The measured data were fit to a single exponential, $I = Ae^{Bt}$ where I is the
intensity and the fitting parameters A and B were calculated to be 1.386 \pm 0.002
and -462.7 \pm 0.9, respectively
Figure 68: Measured lifetimes of the $^4I_{13/2}$ energy level to ground level transition, for a
range of erbium III concentrations in the TZN glass, compared to the theoretical
lifetime. The samples were pumped along their edge to minimize re-absorption
effects. As the most significant source of systematic error in these measurements
was due to re-absorption, the error of these plotted data points was minimized
through pumping the glass samples as close as practical to their edge. Shot to shot
variation was then in the order of 3%
Figure 69: Measured lifetimes for the ${}^4I_{11/2}$ energy level for a range of erbium III
concentrations in the TZN glass compared to the theoretical lifetime (a). As with
the 1.5µm lifetime measurements, the error in these measurements was primarily
due to shot to shot variations in the decay curves and was \approx 5%. The lifetimes on a
linear concentration scale are also plotted in (b) along with the linear fit $\tau = c +$

a[Er ³⁺]. The values for c and a are 0.2157 ± 0.03 and $-2.2 \times 10^{-23} \pm 2 \times 10^{-23}$
respectively
Figure 70: Experimental setup for the lifetime measurements using the pinhole to reduce
re-absorption
Figure 71: Measured lifetimes of the $^4I_{13/2}$ energy level for different erbium III
concentrations in a TZNL glass host. The samples melted in open atmosphere
(blue) are compared to those melted in the dry environment (red). The theoretical
lifetime including radiative and non-radiative decay is also included along with its
uncertainty for comparison. 121
Figure 72: Measured lifetimes of the $^4I_{11/2}$ energy level for different erbium III
concentrations in a TZNL glass host. The samples melted in open atmosphere
(blue) are compared to those melted in the dry environment (red). The theoretical
lifetime including radiative and non-radiative decay is also included along with its
uncertainty for comparison. 121
Figure 73: Fluorescence emission spectra for different erbium III concentrations in a
TZNL glass host with (a) and without (b) the use of a pinhole to reduce re-
absorption. 124
Figure 74: Fluorescence emission spectra for varying pump powers of (a) 0.2×10^{20}
ions/cm 3 and (b) 0.5×10^{20} ions/cm 3 doped samples in the TZNL glass host 126
Figure 75: Pump power dependence of the fluorescence intensity from the 0.5×10^{20}
ions/cm ³ doped TZNL glass
Figure 76: Plot of the emission cross-section and absorption cross-section for the $^4\mathrm{I}_{13/2}$
energy level of the doped TZNL glass
Figure 77: Plots of the threshold dependence on the gain medium length (a), where a
pumped diameter of $250\mu m$ was used and the fibre length was given in terms of the
absorption length making this plot independent of the erbium III concentration, and
the pumped cross-sectional area (b) using a concentration of 1×10^{20} and a length
of 2.5cm, which corresponds to $1/\alpha$ for this concentration. The result where the
diameter equalled 250µm is indicated for comparison
Figure 78: Plots of the predictions for the filling (a) and gain (b) of the $1.5\mu m$ energy
level as a function of time for a range on incident pump powers. The modelling

used a concentration of 5×10^{20} ions/cm ³ and a pumped diameter and length of 0.25
and 2mm, respectively
Figure 79: Ray tracing of the output from the multimode pump source used to determine
the optimum pump configuration and the location of the focus of the pump 139
Figure 80: Plot illustrating the difference in pump beam diameters through the glass
sample when collimating with a 20mm (blue) or 40mm (red) lens 140
Figure 81: Plot of the cavity mode diameter for a flat-curved resonator length of 25mm
(a) and the mode diameter through the glass sample positioned at the waist (b) 142
Figure 82: Plot of the cavity mode waist radius as a function of the cavity length 143
Figure 83: Setup used for the bulk glass laser experiments
Figure 84: Output power vs input power for the free space bulk Kigre QX phosphate
glass laser
Figure 85: Increase in the amount of 1550nm fluorescence with incident pump power for
a TZNL glass sample doped with 2×10 ²⁰ ions/cm ³ . The blue dashed line is linear
and plotted for comparison
Figure 86: Fluorescence emission spectra for varying pump powers of a 0.5×10^{20}
ions/cm ³ doped sample, reproduced from Figure 74 with fewer pump intensities
plotted
Figure 87: Log of the intensity decay when pumped at a 5% (blue) and 95% (red) duty
cycle. In both cases the erbium III was exposed to the pump for 10ms 151
Figure 88: Modelled excited state population (a) and gain (b) for the fabricated wagon
wheel fibre (cross-section provided as the inset) as a function of pump duration for
various fibre lengths. The TZNL glass used was doped with $0.1 \times 10^{20} \; ions/cm^3$
erbium III
Figure 89: Illustration of the wagon wheel fibre defining the regions and surfaces refered
to in the thermal modeling.
Figure 90: Temperature profile of the TZNL glass three strut fibre dissipating 0.4W/m
from its core when omitting any heat transfer across the air in the cladding (a) and
including the heat conduction through the cladding holes (b)
Figure 91: (a) Illustration of the fibre laser setup. (b) Photograph of the erbium III doped
TZNL glass fibre laser

Figure 92: Measured output power from the erbium III doped TZNL glass 1m fibre laser
Figure 93: Spectral output from the erbium III doped TZNL glass 1m fibre laser 165
Figure 94: Plot of the output power as a function of input power with (blue) and without
(red) the inclusion of pump bleaching in the calculation. The measured output
powers are included (green) erbium III doped TZNL glass three strut fibre laser for
comparison to the model
Figure 95: Plot of the output power as a function of the coupled pump power for
increasing fibre length, assuming a TZNL glass host and the 0.1×10^{20} ions/cm ²
Er ₂ O ₃ concentration. The predicted laser efficiency calculated using the two level
rate equation analysis is plotted in brown/red and the three level analysis generated
the output plotted in blue. 10mW of coupled pump power is indicated by the green
dashed line
Figure 96: Erbium III doped TZNL glass microstructured fibre laser output plotted
against the coupled pump power for a fiber length of 2.2 m (blue) the modelled
output including the fibre loss is included in green
Figure 97: Spectral output from a 2.2m length of the erbium III doped TZNL glass three
strut fibre, averaged over a series of scans
Figure 98: Energy level diagram for erbium III and cerium illustration the energy
transfer process used to depopulation the pumped ${}^4I_{11/2}$ energy level
Figure 99: Plot of the predicted improvement in output power with (light blue) and
without (dark blue) the co-doping with cerium
Figure 100: Plot illustrating the potential increase in output power when increasing the
erbium III concentration and core diameter. The three level model (red) is
compared to the two level model (blue) to see the impact of the pump bleaching
Figure 101: Predicted output power from the geometry targeted in the final preforms
fabricated (Section 3.4.4) with (blue) and without (red) the inclusion of pump
bleaching in the calculation. The preforms were doped with 0.5×10^{20} ions/cm ²
erbium III and a target fibre core diameter of 3um

Figu	are 102: Setup used for the density measurements. The weight of the billet and	the
	reduction in this weight when it is submerged in the suspended beaker of water	are
	measured	184

LIST OF ABBREVIATIONS

CoEP Centre of Expertise in Photonics (component of IPAS)

CR Cross Relaxation

CW Continuous Wave

DSC Differential Scanning Calorimetry

EDFA Erbium **D**oped Fibre Amplifier

ESA Excited State Absorption

ET Energy Transfer

ETU Energy Transfer Upconversion

FEM Finite Element Modelling

FSM Fundamental Space Filling Mode

FTIR Fourier Transform Infrared

GSA Ground State Absorption

IPAS Institute for Photonics and Advanced Sensing

IR Infrared

JO Judd Ofelt

LMA Large Mode Area

MOF Microstructured Optical Fibre

NA Numerical Aperture

OSA Optical Spectrum Analyser

PBG (PbO-Bi₂O₃-Ga₂O₃) glass composition

PTFE Polytetrafluoroethylene (Teflon)

QCW Quasi-Continuous Wave

SEM Scanning Electron Microscope

SMF Single Mode Fibre

TZN (TeO2-ZnO-Na₂O) glass composition

TZNL (TeO2-ZnO-Na₂O-La₂O₃) glass composition

UV Ultraviolet

WNT (25WO₃-15Na₂O-60TeO₂) glass composition

ZBLAN (**Z**rF₄-**B**aF₂-**L**aF₃-**A**lF₃-**N**aF) glass composition

GLOSSARY

Glass viscosity – viscosity of the supercooled glass melt.