

Mixed finite element methods: implementation
with one unknown per element, local flux
expressions, positivity, polygonal meshes, and
relations to other methods

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Outline

- 1 Introduction and motivation
- 2 Known equivalences
- 3 Discrete maximum principle
- 4 General polygonal meshes
- 5 One unknown per element: a unified construction principle and a link to the MPFA
 - Local problems definition and a link to the MPFA method
 - Global problems definition
- 6 Numerical experiments
- 7 Conclusions and future work

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- there exist no local flux expressions
- there is no discrete maximum principle
- they cannot work on general polygonal meshes
- they cannot be implemented with one unknown/element
- they are only related to finite difference, finite volume, mimetic finite difference, or MPFA through approximate numerical quadratures

All these beliefs are false!

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Motivations

Motivations of the present work

- recall the rectifications to the five false beliefs
- present a **unified framework** in which MFEs with one unknown/element can be derived/studied/used
- present a comparative **numerical study**
- show **closeness in building principles** of MFE and FD/FV/MFD/MPFA, even on general polygonal meshes

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Model problem and mixed finite elements

A model second-order elliptic problem

$$\begin{aligned} -\nabla \cdot (\mathbf{S}\nabla p) &= g && \text{in } \Omega, \\ p &= 0 && \text{on } \partial\Omega \end{aligned}$$

Mixed finite element method

find $p_h \in \Phi_h$ and $\mathbf{u}_h \in \mathbf{V}_h$ such that

$$\begin{aligned} (\mathbf{S}^{-1}\mathbf{u}_h, \mathbf{v}_h) - (p_h, \nabla \cdot \mathbf{v}_h) &= 0 && \forall \mathbf{v}_h \in \mathbf{V}_h, \\ (\nabla \cdot \mathbf{u}_h, \phi_h) &= (g, \phi_h) && \forall \phi_h \in \Phi_h \end{aligned}$$

- Φ_h, \mathbf{V}_h : Raviart–Thomas–Nédélec MFE space

Matrix form

$$\begin{pmatrix} \mathbb{A} & \mathbb{B}^t \\ \mathbb{B} & \mathbf{0} \end{pmatrix} \begin{pmatrix} U \\ P \end{pmatrix} = \begin{pmatrix} F \\ G \end{pmatrix}$$

- indefinite, saddle point type
- both fluxes U (1/side) and potentials P (1/element) involved

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Equivalence with nonconforming finite elements

Crouzeix–Raviart nonconforming finite element method

- find $\tilde{\lambda}_h \in \tilde{\Psi}_h$ such that

$$(\mathbf{S}\nabla\tilde{\lambda}_h, \nabla\tilde{\psi}_h) = (g, \tilde{\psi}_h) \quad \forall \tilde{\psi}_h \in \tilde{\Psi}_h$$

- degrees of freedom: 1 potential/side (vector Λ)
- matrix form

$$\mathbb{Z}\Lambda = E$$

- \mathbb{Z} is symmetric and positive definite

Equivalence of MFEs with nonconforming finite elements

- MFEs \longrightarrow Lagrange multipliers Λ , mixed-hybrid FEM:

$$\mathbb{Z}\Lambda = E$$

- same matrices and RHS as in the nonconforming finite element method (when \mathbf{S} and g are piecewise constant)
- $\tilde{\lambda}_h$ from MFEs and $\tilde{\lambda}_h$ from NCFEs coincide
- Arnold & Brezzi 1985, Marini 1985, Arbogast & Chen 1995, Chen 1996

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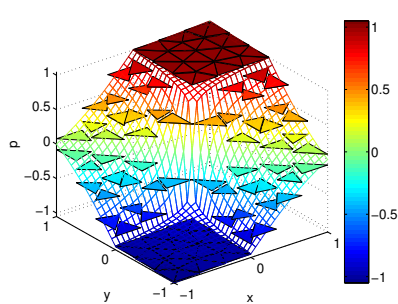
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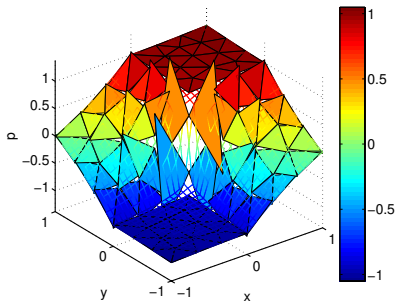
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Different representations of the MFE solution



p_h



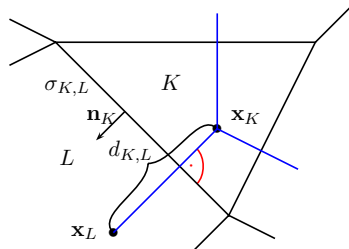
$\tilde{\lambda}_h$

4-point finite volume scheme

4-point finite volume scheme ($\mathbf{S} = \mathbb{I}$)

- find $\bar{p}_h \in \Phi_h$ such that

$$-\sum_{L \in \mathcal{N}(K)} \frac{\bar{p}_h|_L - \bar{p}_h|_K}{d_{K,L}} |\sigma_{K,L}| = (g, \mathbf{1})_K \quad \forall K \in \mathcal{T}_h$$



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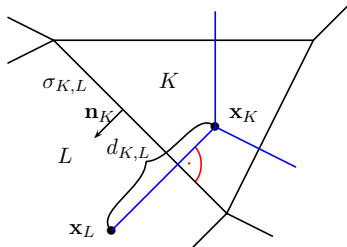
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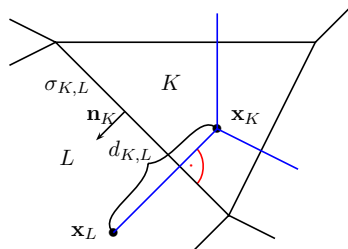
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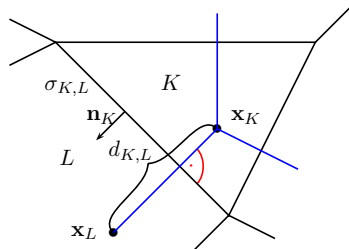
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Equivalence with 4-point finite volumes

Equivalence of MFEs with 4-point finite volumes

- let $g = 0$, $\mathbf{S} = \mathbb{I}$, and \mathcal{T}_h consist of **equilateral simplices**: then p_h from MFEs and \bar{p}_h from FVs **coincide**
- $g \neq 0$, $\mathbf{S} \neq \mathbb{I}$, or \mathcal{T}_h not consisting of equilateral simplices: p_h from MFEs and \bar{p}_h from FVs **do not coincide** anymore
- **conclusion: MFEs and FVs are different**
- this **conclusion is almost completely wrong**

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Equivalence with 4-point finite volumes

- in MFEs (Marini 1985):

$$p_h|_K = \tilde{\lambda}_h(\mathbf{x}_K) + \frac{g_K}{2d|K|} ((\mathbf{x} - \mathbf{x}_K)^t \mathbf{S}_K^{-1} (\mathbf{x} - \mathbf{x}_K), 1)_K$$

- \mathbf{x}_K is the **barycenter**
- p_h represents the **mean value** of the potential
- **influence of the source term g**
- in FVs, if $g = 0$ (Younès, Mose, Ackerer, & Chavent 1999–2004):

$$\bar{p}_h|_K = \tilde{\lambda}_h(\mathbf{z}_K)$$

- \mathbf{z}_K is the **circumcenter**
- \bar{p}_h represents the **point value** of the potential
- **no influence of the source term g**
- **MFEs and FVs are equivalent when g is constant**
 - holds on **arbitrary simplicial meshes** (not necessarily Delaunay)!
 - holds for **full matrix \mathbf{S} !**

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Links to MFDs and MPFAs

Links to the mimetic finite difference and multi-point flux-approximation methods

- using **approximate** numerical integration
 - Klausen & Winther, 2006
 - Wheeler & Yotov, 2006
 - Aavatsmark, Eigestad, Klausen, Wheeler, & Yotov, 2007
 - Drioniou, Eymard, Gallouët, & Herbin, 2010
 - Bause Hoffmann, & Knabner, 2010
 - ... Brezzi, da Veiga, Lipnikov, Manzini, Shashkov ...

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Discrete maximum principle in MFEs

Discrete maximum principle in MFEs ($\mathbf{S} = \mathbb{I}$)

- **DMP** for the Lagrange multipliers λ_σ (values of $\tilde{\lambda}_h$ in side barycenters) whenever \mathcal{T}_h is acute (equivalence with the NCFE method)
- **DMP** in 2D for the values \bar{p}_K (values of $\tilde{\lambda}_h$ in circumcenters) whenever \mathcal{T}_h is Delaunay and the source g is constant (equivalence with the FV method)
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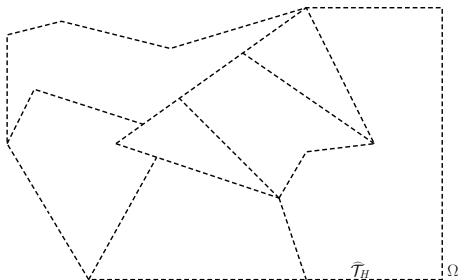
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General polygonal meshes

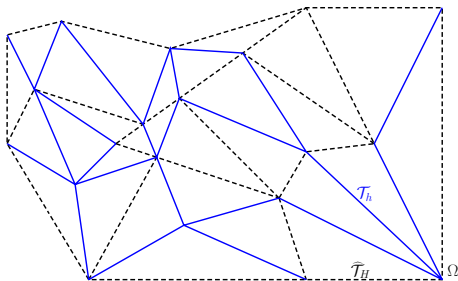
A general polygonal mesh $\widehat{\mathcal{T}}_H$



- nonconvex and non star-shaped elements in $\widehat{\mathcal{T}}_H$
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MFEs on general polygonal meshes

MFEs on \mathcal{T}_h

$$\begin{pmatrix} \mathbb{A} & \mathbb{B}^t \\ \mathbb{B} & \mathbf{0} \end{pmatrix} \begin{pmatrix} U \\ P \end{pmatrix} = \begin{pmatrix} F \\ G \end{pmatrix}$$

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- \hat{U} : flux unknowns related to the sides of $\hat{\mathcal{T}}_H$ only
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Local flux expression from the Lagrange multipliers

Nonconforming finite element method

find $\tilde{\lambda}_h \in \tilde{\Psi}_h$ such that

$$(\mathbf{S}\nabla\tilde{\lambda}_h, \nabla\tilde{\psi}_h) = (g, \tilde{\psi}_h) \quad \forall \tilde{\psi}_h \in \tilde{\Psi}_h$$

Local flux expression from the Lagrange multipliers

there holds (Marini 1985)

$$\mathbf{u}_h|_K = -\mathbf{S}_K\nabla\tilde{\lambda}_h|_K + \frac{g_K}{d}(\mathbf{x} - \mathbf{x}_K) \quad \forall K \in \mathcal{T}_h$$

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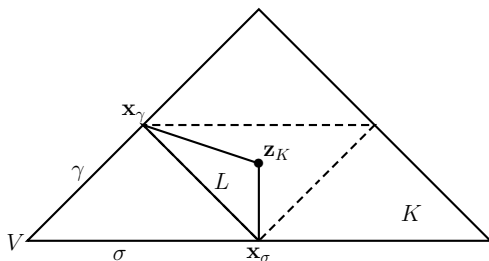
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A new element value

A new element value in $K \in \mathcal{T}_h$

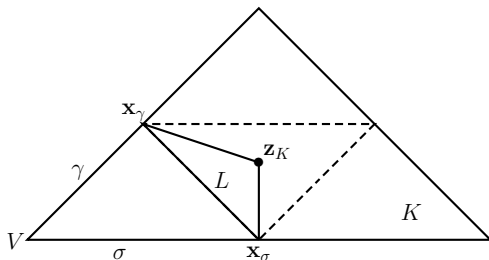
- \mathbf{z}_K : a new point related to K (not necessarily inside K)
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- $\tilde{\lambda}_h$ expressed in the three points \mathbf{x}_σ , \mathbf{x}_γ , and \mathbf{z}_K ($d = 2$)
- Lagrange basis functions $\tilde{\varphi}_\sigma$, $\tilde{\varphi}_\gamma$, and $\tilde{\varphi}_K$



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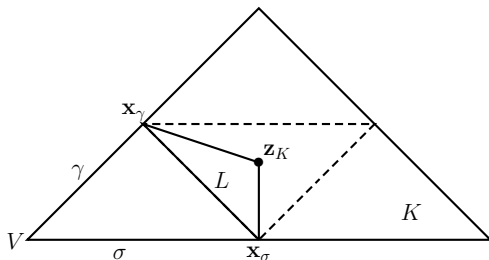
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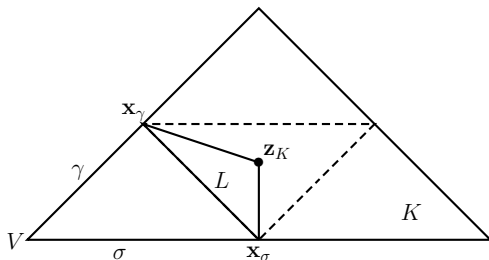
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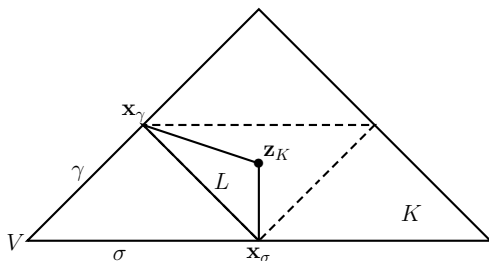
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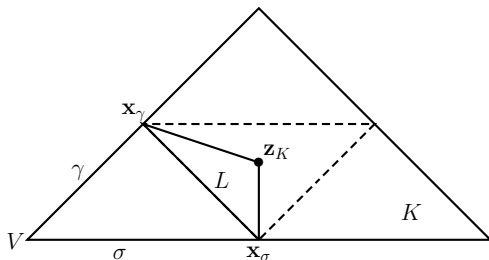
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Definition of a local problem

Definition of a local problem

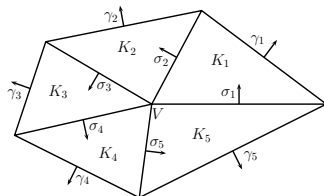
- consider a patch \mathcal{T}_V of the elements around a vertex V
- given the **new element values** \bar{p}_K and λ_σ , $\sigma \in \mathcal{E}_V^{\text{int}}$, in the patch, express the **fluxes \mathbf{u}_h in the patch**
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- the **same building principle** as that of **MPFA methods**



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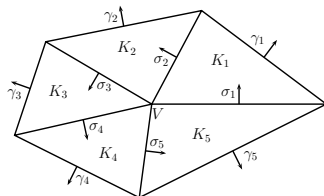
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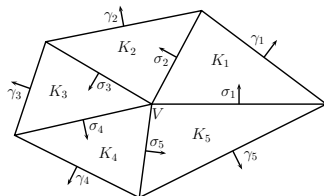
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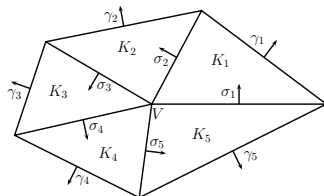
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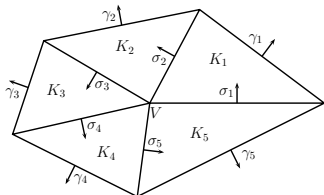
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- local problem:** given $\bar{P}_V = \{\bar{p}_K\}_{K \in \mathcal{T}_V}$, find $\Lambda_V^{\text{int}} = \{\lambda_\gamma\}_{\gamma \in \mathcal{E}_V^{\text{int}}}$ s.t.

$$\mathbb{M}_V \Lambda_V^{\text{int}} = \tilde{G}_V - \mathbb{J}_V \bar{P}_V$$

- the **same building principle** as that of **MPFA methods**

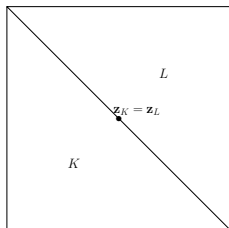


$$\begin{aligned} \mathcal{T}_V &= \{K_i\}_{i=1}^5 \\ \mathcal{E}_V^{\text{int}} &= \{\sigma_i\}_{i=1}^5 \\ \mathcal{E}_V^{\text{ext}} &= \{\gamma_i\}_{i=1}^5 \\ \mathcal{E}_V &= \mathcal{E}_V^{\text{int}} \cup \mathcal{E}_V^{\text{ext}} \end{aligned}$$

S-circumcenter as the evaluation point

S-circumcenter as the point \mathbf{z}_K

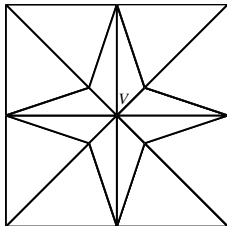
- circumcenter when $\mathbf{S}_K = \mathbb{I}S_K$
- the approach of Younès, Mose, Ackerer, & Chavent, 1999
- \mathbb{M}_V gets **diagonal**
- no local linear system needs to be solved
- **two-point flux expression** (on arbitrary triangular grids and full-matrix piecewise constant \mathbf{S})
- **impossible in 3D** (except particular cases)
- \mathbb{M}_V **can explode** (modifications necessary):



Barycenter as the evaluation point

Barycenter as the point \mathbf{z}_K

- this is the approach of Vohralík, 2004/2006
- \mathbb{M}_V is not diagonal (unless barycenter = circumcenter)
- a local linear system needs to be solved
- multi-point flux expression
- works generally in d space dimensions
- \mathbb{M}_V can get singular (modifications necessary):



Changing adaptively the evaluation point

Changing adaptively the evaluation point

- change \mathbf{z}_K according to the local geometry and diffusion tensor
- ensure the well-posedness of the local problems
- influence the properties of the local matrices \mathbb{M}_V
- influence the properties of the final matrix

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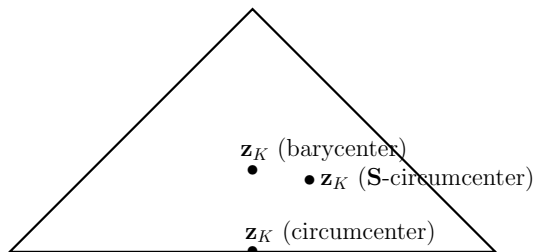
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Examples of the different evaluation points

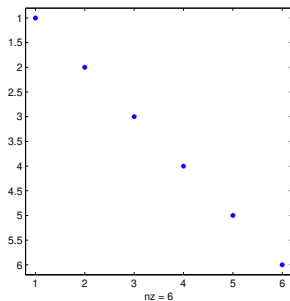
Examples of the different evaluation points \mathbf{z}_K

- $\mathbf{S} = \begin{pmatrix} 0.7236 & 0.3804 \\ 0.3804 & 0.4764 \end{pmatrix}$

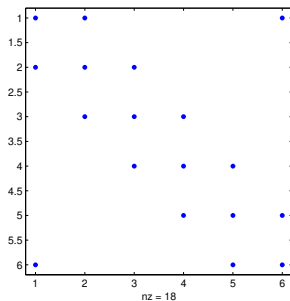


Examples of the local matrices

Examples of the local matrices \mathbb{M}_V



S-circumcenter



barycenter/opt. evaluation point

Outline

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Expressing the Lagrange multipliers Λ or the fluxes U

Expressing the Lagrange multipliers Λ or the fluxes U

- local problems give $\Lambda_V^{\text{int}} = (\mathbb{M}_V)^{-1}(\tilde{G}_V - \mathbb{J}_V \bar{P}_V)$
- for every vertex V , we have one expression for Λ_V^{int}
- run through all vertices and combine the (weighted) inverses of the local condensation matrices
- this gives

$$\Lambda = \tilde{\mathbb{M}}^{\text{inv}} \tilde{G} - \mathbb{M}^{\text{inv}} \bar{P}$$

- similarly

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- recall $U = \tilde{\mathbb{O}}^{\text{inv}} G - \mathbb{O}^{\text{inv}} \bar{P}$
- put this into $\mathbb{B}U = G$
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$$\bar{\mathbb{S}}\bar{P} = \bar{H}$$

with

$$\bar{\mathbb{S}} = -\mathbb{B}\mathbb{O}^{\text{inv}}, \quad \bar{H} = G - \mathbb{B}\tilde{\mathbb{O}}^{\text{inv}} G$$

- $\mathbf{z}_K = \mathbf{S}$ -circumcenter gives the **FV** method (Younès, Mose, Ackerer, & Chavent, 1999)
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- using $\mathbf{z}_K = \mathbf{S}$ -circumcenter, we name it the MFEC method
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Model problem

Model problem

- $\Omega = (0, 1) \times (0, 1)$
- inhomogeneous Dirichlet boundary condition given by $p(x, y) = 0.1y + 0.9$
- $K \in \mathcal{T}_h$:

$$\mathbf{S}|_K = \begin{pmatrix} \cos(\theta_K) & -\sin(\theta_K) \\ \sin(\theta_K) & \cos(\theta_K) \end{pmatrix} \begin{pmatrix} s_K & 0 \\ 0 & \nu s_K \end{pmatrix} \begin{pmatrix} \cos(\theta_K) & \sin(\theta_K) \\ -\sin(\theta_K) & \cos(\theta_K) \end{pmatrix}$$

- homogeneous isotropic case, $s_K = 1$ for all $K \in \mathcal{T}_h$, $\nu = 1$
- anisotropic case, $s_K = 1$ for all $K \in \mathcal{T}_h$, $\theta_K \in \{\frac{\pi}{5}, \frac{3\pi}{4}, \frac{\pi}{2}, \frac{3\pi}{5}, \frac{\pi}{3}\}$, $\nu = 0.2$
- inhomogeneous case, $s_K \in \{10, 1, 0.1, 0.01, 0.001\}$, $\nu = 1$

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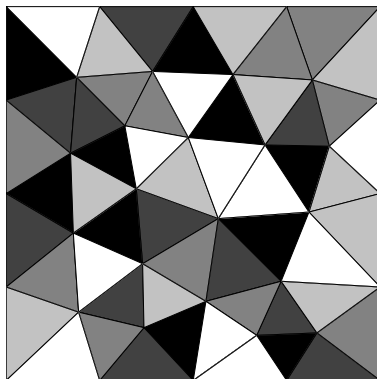
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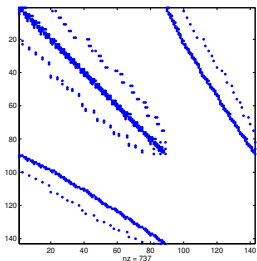
Initial mesh

Initial mesh and the distribution of the inhomogeneities and anisotropies

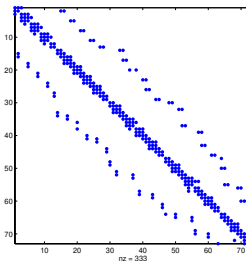


Matrices of the different methods

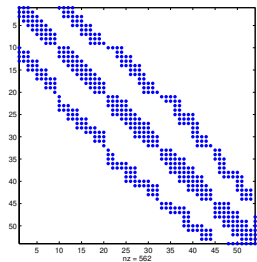
System matrix sparsity patterns



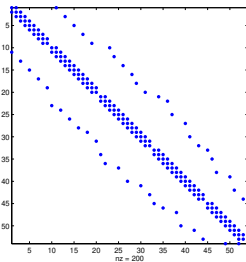
MFE



NCFE



MFEB
MFEO
CMFE



FV
MFEC

Results, homogeneous isotropic case

Meth.	Un.	Mat.	St.	Nonz.	CN	CNS	CPU	CG/		PCG/		
								DS	Bi-CGStab	PBi-CGStab	IC/	ILU
MFEB	13824	NPD	14	177652	7564	7580	0.27	4.86	324.5	0.81	0.36	9.0
MFEC	13824	NNS	4	55040	11256	11056	0.09	2.23	372.0	0.42	0.19	6.5
MFEO	13824	NPD	14	177652	7531	7558	0.28	4.08	270.0	0.80	0.41	7.5
CMFE	13824	NPD	14	177652	7397	7380	0.27	4.70	312.0	0.83	0.39	8.5
FV	13824	SPD	4	55040	65722	8898	0.07	3.09	1098.0	0.42	0.17	17.0
NCFE	20608	SPD	5	102528	14064	9944	0.14	2.92	620.0	1.11	0.56	19.0

Results, anisotropic case

Meth.	Un.	Mat.	St.	Nonz.	CN	CNS	CPU	CG/		PCG/		
								DS	Bi-CGStab	PBi-CGStab	IC/	Iter.
MFEB	13824	NPD	14	177652	14489	11203	0.28	6.61	448.0	0.98	0.59	6.5
MFEC	13824	NID	4	55040	2401279	416769	0.08	—	—	0.45	0.20	7.0
MFEO	13824	NPD	14	177652	13401	10767	0.27	6.51	440.5	0.95	0.41	10.0
CMFE	13824	NPD	14	177652	9276	7758	0.28	5.27	350.5	0.84	0.38	9.0
FV	13824	SID	4	55040	247055	239934	0.09	—	—	0.45	0.20	7.0
NCFE	20608	SPD	5	102528	25393	16969	0.18	4.03	850.0	1.12	0.41	30.0

Results, inhomogeneous case

Meth.	Un.	Mat.	St.	Nonz.	CN	CNS	CPU	DS	CG/ Bi-CGStab	PCG/ PBi-CGStab	IC/ ILU	Iter.
								CPU	CPU	Iter.		
MFEb	13824	NPD	14	177652	819248	740706	0.28	13.33	897.5	1.05	0.62	6.5
MFEc	13824	NNS	4	55040	903789	763849	0.09	5.34	947.5	0.47	0.20	7.5
MFEo	13824	NPD	14	177652	820367	739957	0.28	12.45	790.5	1.05	0.56	8.0
CMFE	13824	NPD	14	177652	2500730	478974	0.28	102.27	6842.5	1.01	0.41	10.5
FV	13824	SPD	4	55040	16387758	497974	0.07	39.41	14101.0	0.44	0.17	16.0
NCFE	20608	SPD	5	102528	4797335	670623	0.18	52.42	11226.0	1.22	0.64	16.0

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- 3 Discrete maximum principle
- 4 General polygonal meshes
- 5 One unknown per element: a unified construction principle and a link to the MPFA
 - Local problems definition and a link to the MPFA method
 - Global problems definition
- 6 Numerical experiments
- 7 Conclusions and future work

Conclusions and future work

Conclusions

- mixed finite elements: **one method** with
 - saddle point / symmetric pos. definite / nonsymmetric pos. definite / symmetric indefinite / nonsymmetric indef. matrix
 - U and P unknowns / Λ unknowns / P unknowns
 - narrow stencil and two-point flux expressions / wider stencil and multi-point flux expressions
 - discrete maximum principle for values in some points but not in some others
- no free parameter to choose, no stabilization, the best method if your criterion is min. complementary energy
- **close relations** in **building principles** between MFE/FD/FV/ MFD/MPFA, even on general polygonal meshes

Work in progress

- a general principle for nonconforming finite elements
- extensions to all order MFE schemes
- multigrid solvers

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Thank you for your attention!