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Model Selection And Initial Application Of CONTRAM Model For Evaluating In-vehicle Information Systems

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CALIFORNIA PATH PROGRAM INSTITUTE OF TRANSPORTATION STUDIES UNIVERSITY OF CALIFORNIA AT BERKELEY

## Model Selection and Initial Application of CONTRAM Model for Evaluating In-Vehicle Information Systems

Yonnel Gardes Bruce Haldors Adolf D. May

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PATH Research Report UCB-ITS-PRR-91-11

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#### **EXECUTIVE SUMMARY**

#### BACKGROUND

The preliminary evaluation of the potential benefits of in-vehicle information systems was conducted by an Institute of Transportation Studies research team in 1988 and 1989 using the computer programs, FREQ and TRANSYT to model the Smart Corridor in Los Angeles, California. Out of that study came recommendations for future research on the need for more realistic simulation of the interaction between the freeway and parallel arterials. A study was conducted in 1990 to assess which models were suitable to evaluate in-vehicle information systems within an integrated freeway/arterial corridor. Twenty-four models were identified as being potentially suitable. Of the 24 models identified, three were recommended for further analysis and application: CONTRAM, SATURN, and INTEGRATION.

#### **OBJECTIVES**

The objectives of this study were to select a traffic assignment and simulation model, apply that model to an integrated freeway/arterial network such as the Smart Corridor in Los Angeles, California, and, using the model, make an initial evaluation of in-vehicle information systems and the applicability of the model.

#### APPROACH

The approach consisted of first evaluating of the **CONTRAM**, SATURN, and INTEGRATION models and then selecting of one of the models for a detailed analysis of the features which would be best suited to this particular application. The next step was an initial application of the selected model to a generic network and then the Smart Corridor. The final steps in the study were to make an assessment of the model, present major findings of the study, and describe the potential for future research.

#### RESULTS

After review of the **CONTRAM**, SATURN, and INTEGRATION models, the **CONTRAM** model was chosen for further evaluation. Since the **CONTRAM** model was primarily developed for use in the design of traffic management schemes for urban signalized arterial networks, further analysis into the models ability to model freeway congestion was necessary. In order to gain a more clear understanding of the freeway modelling characteristics within **CONTRAM**, several test networks were designed and evaluated and as a result problems were discovered regarding the ability of the model to accurately reflect freeway congestion. However, an analysis ensued to evaluate the potential benefits of in-vehicle

information systems. The results of the study should be viewed with some caution due to difficulties with the freeway modelling characteristics of **CONTRAM**, as well as weaknesses within the characteristics of the network and structure of the demand pattern. The results are best considered in a qualitative manner with the findings being, the more vehicles that are equipped with in-vehicle information, the better the system performance. For a severe incident condition on the freeway, as the percentage of vehicles equipped with information increases, the performance of the system improves until the system is at a level of performance that is only slightly less than that before the incident occurred.

## 1.0 INTRODUCTION

This report describes the results of the study team's efforts to:

- 1) select a traffic assignment and simulation model;
- apply that model to an integrated freeway/arterial network such as the Smart Corridor in Los Angeles, California; and,
- 3) using the model, make an initial evaluation of in-vehicle information systems and the applicability of the model.

## 1.1 Background

As **traffic** congestion increases worldwide, attempts are being made at improving the efficiency of the existing systems through the use of information available through computers. Past research has indicated that up to \$45 billion per year is lost due to excess travel time which could be recovered if there was a more efficient transportation system that used navigational systems [1].

Several researchers have attempted to make a quantitative assessment of in-vehicle information systems [2]. Most previous studies have been network specific, i.e., the benefits of in-vehicle information systems were related only to the network in question. This holds true for this particular application as well. For this study, the integrated freeway/arterial network chosen for modelling was the Smart Corridor in Los Angeles, California.

#### 1.2 Purpose

The purpose of this study was to select an appropriate traffic assignment and simulation to evaluate invehicle information systems. After the appropriate model was selected, an initial application to the Smart Corridor was conducted and a second and third application were undertaken to simulate an incident on the freeway. Varied percentages of in-vehicle information systems were then modelled which permitted an initial evaluation of the applicability of the model.

#### **1.3** Scope and Study Approach

Based on previous research (Al-Deek, Martello, Sanders and May [3]), it was determined that an equilibrium model combining traffic simulation, control, and assignment was desirable for evaluating the potential benefits of in-vehicle information systems in an integrated freeway/arterial corridor. Thus, a study was begun to evaluate the models available for the task of evaluating in-vehicle information systems. This project is an extension of the original work by May in 1986 [3].

Chapter 2 of this report outlines the history and background of this and previous studies. Chapter 3 describes the evaluation of the **CONTRAM**, SATURN, and INTEGRATION models. Chapter 4 discusses in more detail the features in **CONTRAM** that were best suited for application in this study. Chapter **5** describes the Smart Corridor and the features that made it particularly attractive to be used in the modelling process. Chapter 6 describes the initial applications of the **CONTRAM** model to both a generic freeway segment, and the freeway segment to be used in the entire corridor. Chapter 7 outlines the design of the experiment and how a reference-base-run assignment was derived. Chapter 8 gives a description of incident modelling within **CONTRAM**. Chapter 9 presents the analysis findings and results, while Chapter 10 summarizes an assessment of the model and the modelling effort and discusses the potential for future research.

#### 2.0 PREVIOUS RESEARCH

Since the early 1980's much research has been conducted in the area of in-vehicle information systems [4 - 9]. One of the primary objectives of much of this research has been to provide a quantitative assessment of in-vehicle information value in a real-world freeway corridor under recurring and non-recurring congestion.

#### 2.1 1987-1989

The history of this study dates back to 1987. PATH Research Report UCB-ITS-PRR-88-2[3] details the initial attempts at understanding *the Potential Benefits of In-Vehicle Information Systems in a Real Life Freeway Corridor under Recurring and Incident-Induced Congestion.* This initial attempt was conducted using the simulation models FREQ and TRANSYT-7F. The Santa Monica freeway corridor was simulated based on data collected by the Los Angeles Department of Transportation and Caltrans from 1984 to 1988.

Since TRANSYT-7F and FREQ do not perform traffic assignment, a network model was developed called **PATHNET. PATHNET** was utilized to determine the travel times for the shortest path between any origin and destination point in the network or for any other path in the network. **PATHNET** is a prototype version of a generalized network analysis package. **PATHNET** prints a report listing the links in the minimum-cost path and the cumulative route cost for each link. Thus, the research team was able to assess the potential benefits by comparing travel times between different origin and destination pairs under different scenarios.

The results of the study were as follows [3,10-11]:

- under the recurring, non-incident congestion scenario, the travel time savings were generally negligible (less than three minutes for a 20-25 minute trip);
- under the non-recurring, incident congestion scenario, travel time savings were found to be significant (greater than three minutes);
- the greatest travel time savings occur during the time slices following the introduction of a freeway incident.

One recognized weakness with the earlier study was the fact that the user equilibrium issue was not addressed. To address this weakness, a traffic assignment model which combines traffic assignment with

simulation was chosen as the tool for evaluation which achieves user equilibrium through each assignment. Thus, the first objective of this study was to find a model that could model an integrated freeway/arterial network and also combine traffic assignment with simulation.

#### 2.2 1989-1990 RESEARCH

The 1989-1990 research focused on the modelling approaches for evaluating advanced traffic control strategies and in-vehicle information systems within an integrated network of traffic signals and freeways. Efforts included a literature review of candidate freeway/arterial models. An assessment of model suitability was carried out in order to determine if any existing model would be potentially suitable, the specific modifications needed to be included in a reasonable level of effort, or the specifications that would be required for developing a new model.

The approach consisted of a literature review and preliminary assessment of candidate models, an in-depth evaluation of the most promising models, and the selection of a few models for further analysis and testing. The literature review resulted in the identification of twenty-four candidate models, classified into four categories:

- 1) Transportation planning models: MINUTP, Tmodel, TRANPLAN, CARS, MICROTRIPS, EMME2, MULATM;
- 2) Freeway operation models: FREQ, INTRAS, MACK-FREFLO-FRECON, KRONOS, FREESIM, ROADRUNNER;
- 3) Signalized network operation models: TRAFFICQ, MICRO-ASSIGNMENT, SATURN, CONTRAM, JAM;
- 4) Freeway/arterial operation models: CORQ1C, SCOT, TRAFLO, DYNEV, CORQ-CORCON, INTEGRATION.

A preliminary screening process (summarized in Table 2.1) indicated that only five of the models chosen were capable of simultaneously performing traffic assignment and traffic simulation under oversaturated conditions, which were considered as two essential features for the purposes of this study. For three of these models (INTEGRATION, SATURN and CONTRAM), an in-depth evaluation was carried out, including tabular summaries of the characteristics of each model, rating of the performance of each model and the corresponding strengths and weaknesses, and a discussion on model suitability with regard to our application. A final report describing the **1989/1990** activities was published in June 1990 [12]. It was

	OPERA	TING ENVIRO	TRAFFIC ASSIGNMENT	QUEUING CONDITIONS	
MODEL	Freeway	Corridor	Arterial	August	
1) CARS	x	Р	Р	x	
2) EMME2	x			x	
3) MICROTRIPS	x			x	
4) MINUTP	x			x	
5) MULATM	Р	Р	Р	x	Р
6) THODEL	x	Р	Р	x	
7) TRANPLAN	x			x	
8) FREESIM	×				
9) FREQ	x	Р		Р	x
10) INTRAS	×	Р	Р		
11) KRONOS	x				x
12) MACK-FREFLO	×				x
FRECON2	. ×	x	Р		x
13) ROADRUNNER	×				
14) CONTRAM	Р	Р	x	X	x
15) JAM	Р	Р	x	×	x
16) MICRO-ASSIGNMENT			x	. ×	Р
17) SATURN	Р	Р	x	x	x
18) TRAFFICQ			x		x
19) CORQÍC	x	x	x	x	Р
20) CORG-CORCON	×	x	x	x	x
21) DYNEV	x	X	x	x	
22) INTEGRATION	x	×	x	x	x
23) SCOT	x	×	x	x	
24) TRAFLO	×	×	x	x	

## TABLE 2.1 PRELIMINARY SCREENING PROCESS

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x: Existing P: Partially Existing

recommended that the three selected models be acquired in order to perform a hands-on experiment and assessment.

## **3.0 MODEL EVALUATION**

The main features of the **CONTRAM**, SATURN and INTEGRATION models are highlighted in this chapter and a demonstration of SATURN and **CONTRAM** is described.

## **3.1 CONTRAM**

**CONTRAM** is a traffic assignment model developed by the Transport and Road Research Laboratory for use in the design of traffic management schemes in urban areas. **CONTRAM5** (Continuous Traffic Assignment model Version 5) is the latest version of the **CONTRAM** program which was originally written in the early 1970s. Given the traffic demands between origins and destinations for a network, it predicts routes of vehicles and flows and queues on links. It is a capacity restrained model which takes account of the interactive effects of traffic between intersections and the variation through time of traffic conditions. In particular, **CONTRAM** models the build up and decay of congestion such as occurs during peak periods.

## **3.1.1 Basic Structure** [13]

The overall structure and suite of programs in **CONTRAM** is outlined in Figure 3.1. The inputs are the network data, the traffic demand data, and the control data. The bases of the program are the assignment process, which calculates and stores vehicle route information, and the calculation through time of the delays on links derived from the flows and queues of vehicles.

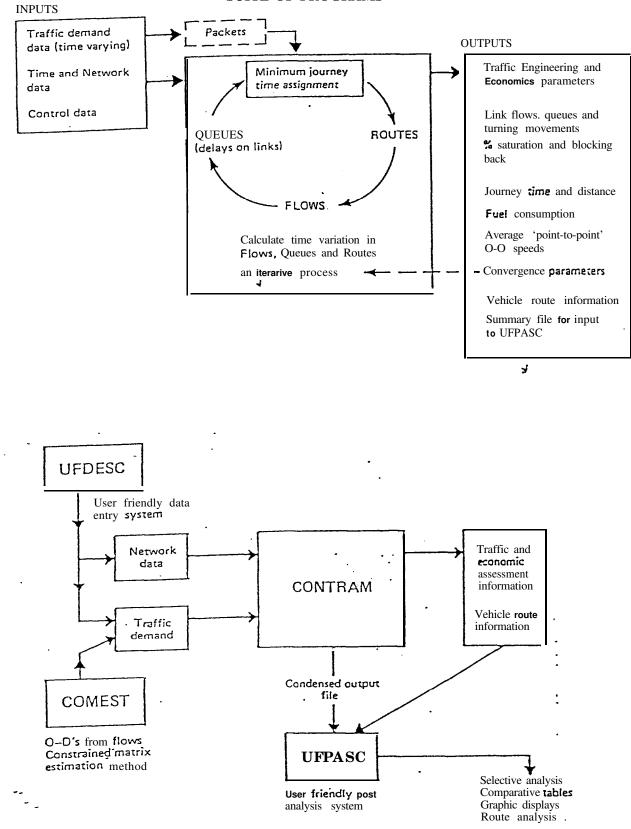
#### 3.1.2 Input Data Requirements [13]

The three major components of input to the model are the network and time data, the demand data, and the control data. The following pages outline the characteristics of these three areas.

#### 3.1.2.1 Network and Time Data

This defines the period to be simulated and the geometric properties of the network. The following provides a description of the basic card types used in the CONTRAM model.

#### FIGURE 3.1 OVERALL STRUCTURE OF CONTRAM & SUITE OF PROGRAMS



Card type 1 is the time card which defines the duration of the simulation period and the time intervals into which the period is divided. The maximum number of time intervals is 13 while the maximum duration of a simulation period is eight hours.

Card type 2 defines the general parameters of the network. It sets the values of certain network parameters used for the estimation of storage capacity on a link, to specify signal lost time for capacity calculations and to select the separate calculation of geometric delay at intersections.

Card type 3 defines the links to which an origin is connected.

Card types 4, 5, and 6 define the type of control used at link junctions. Card type 4 represents an uncontrolled link. It gives detail required for an uncontrolled link: cruise time (or cruise speed, or speed-flow relationship to be used), length, saturation flow, storage capacity. Card type 5 represents give-way links. Card type 6 represents signal-controlled links and has the same basic requirements as card type 4 plus percentage green and delay factors.

Card type 7 defines the speed-flow relationships. Speed/flow relationships have been incorporated to be used on roads where cruise time is a significant proportion of total time, e.g. on urban freeways and other limited-access high speed urban roads. The effect of a speed/flow relationship is in addition to explicit queuing at the downstream end of the link to which it applies. The general form of speed/flow relationships used by **CONTRAM** consists of two linear sections of different slope. The exact form is determined by entering as data three points:

- 1) the free speed, where flow is zero
- 2) the break point, where the slope changes
- 3) the capacity point, which is a point through which the second section passes.

Card type 8 is the change of mind card, which allows the user to vary values of a parameter without changing the original data cards.

Card type 9 defines the vehicle classes used in the simulation. The card specifies passenger car unit equivalents and relative cruise times for each vehicle type. The model distinguishes three classes of vehicle, car, bus, and trucks.

Card type 10 defines the coefficients of the fuel model, which is based on the following formula for fuel consumption per unit distance at steady speed V:

$$F = A + (B / V) + (C * V^2)$$

Card types 11 and 12 allow the saturation flow value on a link to be varied from time interval to time interval, for example to allow the effect of an accident to be simulated.

Card type 13 allows the calculation of a geometric delay due to deceleration and acceleration at an intersection. **CONTRAM 5** provides the option to calculate the geometric delay explicitly for each separate turning movement.

Card types 14, 15 and 16 set the speeds for turning movements out of individual links.

Card type 18 defines the range of allowed destination numbers.

## **3.1.2.2** Traffic Demand Data

The traffic demand data specifies the flow rate during each time interval for each origin-destination movement. The traffic demand for each origin-destination movement in a network is specified as a series of flow rates (veh/h) for each time interval. For a given O-D pair, one data card is used for each classified vehicle demand (C, B or L). The card also contains:

- the packet size, which can be generated automatically;
- the "straight-line" distance between the origin and destination (optional);
- the start-code (time of start of the first packet from the O-D demand to enter the network in the first time interval).

It is possible to model the movements of more than one demand for the same class of vehicle, between the same origin and destination, by using separate cards, or the change of mind card. The change of mind cards can be used to change specified flow rates.

## 3.1.2.3 Control Data

The data in the control data pack has two control functions. The first, describing the running of the program, defines the number of iterations to be carried out and the types of output required. The second provides the additional data required for signalized intersections. The data required for vehicles with fixed routes are also specified in this pack.

• Card type 50: Maximum number of iterations

Selection of outputs:

- Card type 51: Network summary information for assessing convergence
- Card type 52: Change in vehicle arrivals convergence matrix
- Card type 53: Link-by-link data all parameters
- Card type 54: Link-by-link values flows, queues, queue times, average speeds
- Card type 55: Measure of fairness
- Card types 56 and 57: Output of turning movements
- Card type 58: Alternative units of measurement
- Card type 59: Alternative file units for results
- Card type 60: Control of algorithms (used to select variable or constant packet size)
- Card type 154: Selection of tables in output

Cost parameters are specified by the following card types:

- Card type 61: Perceived cost output units
- Card type 62: Perceived cost functions
- Card types 63 and 64: Resource cost functions

The perceived cost is the cost that is perceived by drivers which they seek to minimize by their route choice. The resource cost is assumed to represent the real cost of travel and in CONTRAM, is purely an output quantity which has no effect on route choice. In CONTRAM, the functional form of both perceived and resource cost is  $C = Ad + Bt + Cv^{2*}d$  which expresses cost C in terms of distance d, time t and average speed v.

Additional signal data can be specified by the following card types:

- Card type 70: Common signal coordination factor
- Card type 71: Signal plans fixed cycle/fixed splits
- Card type 72: Signal plans fixed cycle/optimized splits
- Card type 73: Signal plans optimized cycle/optimized splits
- Card type 77: Intersection signal plans schedule

Fixed route data can be specified by the following card types:

- Card type 81: Specification of fixed routes
- Card type 85: O-D movements having fixed routes

## 3.1.3 outputs [13]

There are six forms of output, any selection of which can be called by the appropriate card types 51 to **56.** 

## 3.1.3.1 Summary Information

The data provided for each time-slice are as follows:

- Total Journey-time (veh.h)
- Total Distance Travelled (veh.kms)
- Overall Network Speed (km/h)
- Total Final Queues (veh)
- Fuel Consumption (litres)
- Total Link Counts (veh)

## 3.1.3.2 Convergence Monitor

The purpose of these printouts is to provide data for assessing convergence. The convergence indicators are, for all iterations, the total journey-time, the total distance travelled, and the changes in initial queues plus arrivals on links.

## 3.1.3.3 Link-by-Link Values (All Parameters)

These data contain, for each time slice, the values of the following parameters:

- Link entry flow (veh);
- Mean initial queue (veh): number of vehicles queuing on the link at the start of the time slice;
- Vehicle arrivals (veh): number of vehicles in each class reaching the stopline on the link in the time slice;
- Departures from queue (veh): number of vehicles which leave the link in the time slice;
- Mean final queue (veh): number of vehicle queuing on the link at the end of the time slice;
- Spare throughput capacity (veh): difference between the maximum throughput capacity of the link and the number of vehicles which leave the link in the time slice;
- Mean PCU factor (Passenger Car Units);

- **Rho** = ratio of arrivals to capacity at stop line, to be used in place of degree of saturation;
- Mean total and queue time per vehicle (secs);
- Total delays **by** source (free moving, flow-delay or queuing) (veh.h);
- Percentage of occupancy;
- Measure of the number of stops, as a percentage of arrivals;
- An estimate of the efficiency of signal coordination.

The following information is necessary for signal controlled links:

- Plan type
- Cycle time (secs)
- Green time (secs)

The following network totals for each time interval are printed out:

- Total times by vehicle class (veh.h)
- Total distances travelled (veh.km)
- Total fuel consumption (litres)

## 3.1.3.4 Link-by-Link All Intervals Tables

The following lists the tables that can be output for each time slice:

- Arrivals (veh/h)
- Capacities (veh/h)
- Mean final queues (veh)
- Mean queuing times per vehicle (sec)
- Mean travel times per vehicle (sec)
- Total delay (veh-hr)
- Average speed of a car (km/h)
- Generalized costs

## **3.1.3.5 Point to Point Speeds**

This output indicates the variation with time of the average straight-line speed (km/h) for selected O-D movements.

#### **3.1.3.6** Turning Movements: For Selected Intersections or For All Links

These data provide detailed information for all time slices of turning movements. The first form of this option is intersection-oriented and contains additional information on flows, signal timings, final queues, and mean queue time for the links feeding the intersection. The second form provides turning movements from all links without any additional information.

### 3.1.4 Demonstration [14]

### 3.1.4.1 Test Network

The test network shown on Figure 3.2 has been designed to demonstrate the use of the facilities in CONTRAM [14].

## 3.1.4.2 Input Data Files

TEST.NET (Appendix A): Network and Time Data TEST.DEM (Appendix A): Traffic Demand Data TEST.CON (Appendix A): Control Data

### **3.1.4.3** Running the Program

The main executable program is called **CONTRAM7.EXE**. The command **CONTRAM7** TEST is used to run the program with the TEST data files.

### 3.1.4.4 output

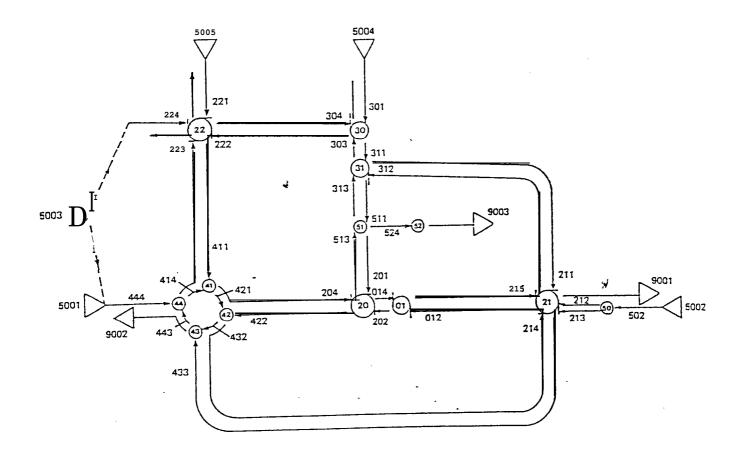
Three output files are created:

- 1) **TEST.RES** (Appendix A): Normal Results file (printer file)
- 2) TEST.RTE (Appendix A): Vehicle Route file (detailed information for each packet path)
- 3) TEST.PAF: Post Analysis Output File

- Demonstration of UFPASC (User Friendly Post Analysis System for Contram)

Input: TEST.PAF Post Analysis file TEST.RTE Vehicle Route file

## FIGURE 3.2 CONTRAM TEST NETWORK



Output: OUTPUT1 (Appendix A)

- Demonstration of UFDESC5 (User Friendly Data Entry System for Contram)

Input: TEST.NET or TEST.DEM or TEST.CON

- Demonstration of COMEST (Constrained O-D Matrix Estimation)

Input: X2.OBS Observed link counts X2.RTE Assigned routes and flows in CONTRAM type packet route format X2.CON Control file

Output: X2.RES Results file

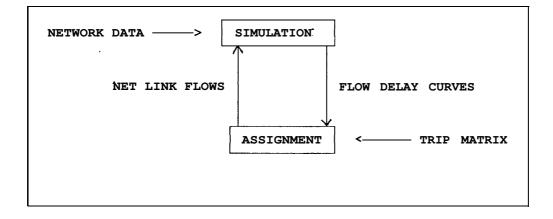
## **3.2 SATURN**

SATURN (Simulation and Assignment of Traffic to Urban Road Networks) is a computer model developed at the Institute for Transportation Studies, University of Leeds, for the analysis and evaluation of traffic management schemes over relatively localized networks (typically of the order of 100 to 150 intersections) [15]. It is primarily intended to be used as a highly sophisticated traffic assignment model. This sophistication is due to a highly detailed simulation of delays at intersections. Unlike conventional assignment models, SATURN places great emphasis on intersections and specific turning movements as opposed to links.

#### 3.2.1 Basic Structure

The basic structure of SATURN incorporates two phases, as shown in Figure 3.3, a simulation and an assignment phase [15].

Figure 3.3 The Simulation and Assignment Phases of SATURN



## **3.2.1.1 The Simulation Model [15]**

The primary objective of the simulation is to determine intersection delays resulting from a given pattern of traffic. Two fundamental assumptions are made to do this:

- 1) A traffic pattern is constant for time periods of 15 or 30 minutes;
- 2) A cyclical behavior is imposed on the flows by traffic signals operating with a common cycle time of typically 60 to 120 seconds.

The first assumption restricts analysis to the average behavior of the system within the given time period. However, a quasi-dynamic analysis of **traffic** patterns may be carried out by modelling a series of successive 15 or 30 minute time periods. By changing the trip matrices for each time period, one can follow, for instance, the growth and decay of traffic over a morning or evening peak period.

The second assumption permits concentration of the simulation effort on one cycle, where traffic is represented as semi-continuous flow profiles, as opposed to individual vehicles or packets of vehicles.

## 3.2.1.2 The Assignment Model [15]

The simulation model is used to model the flow-delay curves by calculating the delays for each turning movement at zero flow, current flow and capacity, with all other flows (i.e. opposing traffic) fixed.

The model assumes that:

- 1) the travel time of each link is fixed independent of flow
- 2) the delay of each turning movement at an intersection is a function of that turning volume.

The flow-delay curves determined by the simulation are fed to the assignment. The objective of the assignment phase is to select minimum time routes through the network for each element in the trip matrix. The model uses an equilibrium technique which optimally combines a succession of all-or-nothing assignments.

#### **3.2.1.3** The Complete Model [15]

As shown in Figure 3.3, the complete model is based on an iterative loop between the assignment and simulation phases. Although described as two separate phases, SATURN appears as a single program for the user. The simulation and assignment stages can be run automatically without user intervention until either convergence has been achieved or a specified number of iterations performed.

#### 3.2.2 Input Data Requirements [15]

Two distinct forms of data input are required. The first is an O/D trip matrix representing the period of interest, or a set of trip matrices. The second is network data.

#### 3.2.2.1 Trip Matrices

The O/D trip matrix is conventional in most respects, but a very fine zoning system is often required in order to perform detailed modelling. The accuracy of the assigned flows will depend critically on the validity of that matrix. The traditional techniques to gather a O/D matrix are direct observations, such as roadside interviews or license plate surveys. However, these techniques are expensive in terms of manpower and data processing, as well as being subject to errors.

To overcome these problems, at least partially, SATURN makes use of a technique which was also developed at the Institute for Transportation Studies, known as ME2. The technique is based on the principles on entropy maximization; in essence, ME2 calculates the most likely trip matrix consistent with all the available information, which may be, in the simplest case, a limited number of traffic counts. Since link counts, as opposed to O/D trips, can be obtained quickly, cheaply and accurately, the method is extremely attractive. ME2 has been an essential component in virtually every application of SATURN to date.

#### 3.2.2.2 Network Data

As usual, the road network is described graphically as a set of nodes and connecting links. SATURN allows networks to be coded at two levels of detail:

 an "inner" or "simulation" network which is coded and simulated in detail, restricted to 100-150 intersections; and 2) an "outer" or "buffer" network coded in much less detail, in a conventional link-based detail.

Since **SATURN** assumes that virtually all delays to traffic occur at intersection, the simulation network coding is primarily intersection-based. The user is required to supply for each intersection:

- 1) A node type (basically signals, priority or roundabout);
- 2) The travel distances and times (or speeds) from the previous intersection for each entry arm;
- 3) The number of lanes on each entry arm;
- 4) For each permitted turn, the lanes used and the saturation flow;
- 5) Information on whether one stream of traffic takes priority over any other;
- 6) The phase structure of all traffic signals (cycle times, offsets, green splits between different turns, etc.).

## 3.2.3 Outputs [15]

#### 3.2.3.1 Assignment Stage

Outputs from **the SATURN** assignment stage are essentially conventional, e.g. flows and travel times for both links and turns plus various aggregate measures such as average speeds, total vehicle-kilometers, interzonal travel times, etc.

### 3.2.3.2 Simulation Stage

Mostly intersection-based, the information provided by the simulation phase is far more detailed. It includes:

- 1) Capacities, average delays, and average queues for each individual turn;
- 2) Cyclical flow profiles, as in TRANSYT;
- 3) The rate of growth of any permanent queues at over-capacity intersections;
- 4) Estimates of the number of vehicle stops at each intersection (these estimates are used in estimates of fuel consumption);
- 5) Separate performance measures for buses.

One of the basic programs which comes with the SATURN suite, **SATLOOK**, allows the user to look directly at delays, queues, etc., at a selected intersection, as opposed to having all possible data output to the line printer following each run.

#### 3.2.4 Demonstration [16]

The basic model has six components:

- -SATNET: Network Build Program
- SATASS: Assignment Program
- SATSIM: Simulation Program
- SATLOOK: Analysis Program
- SATED: Network Editing Program
- P1: Network Plot Program

The demonstration was made in the following way:

 Build the trip matrix Command: MI LIVTRIPS Printer Output: LIVTRIPS.LPM (Appendix B)
 Build the network Command: SATNET LIVNET Printer Output: LIVNET. LPN (Appendix B)
 Run first assignment Command: SATASS LIVNET LIVTRIPS Printer Output: LIVNET.LPA (Appendix B)
 Run first simulation Command: SATSIM LIVNET LIVNET1 Printer Output: LIVNET1.LPS (Appendix B)
 Run second assignment Command: SATASS LIVNET1 LIVTRIPS Printer Output: LIVNET1.LPS (Appendix B)

The process may then be repeated to convergence.

#### 3.2.5 References

The following applications have been reported:

Harrogate, North Yorkshire, England [17]
1980, 45 nodes, 24 zones
Ref: Traffic Engineering & Control, April 1980

Liverpool, England [18]
1982, 818 nodes, 106 zones
Ref: Traffic Engineering & Control, January 1983

#### **3.3 INTEGRATION [19]**

INTEGRATION is a traffic model developed at Queen's University in Kingston, Canada to evaluate the operation of integrated freeway/traffic signal networks during periods of recurring and non-recurring congestion.

The INTEGRATION modelling approach consists of a discrete simulation that traces the path of each vehicle throughout the network. The links that a vehicle uses are selected in accordance with its estimate of the best route, and, along its path, each vehicle's route is further adjusted in view of any changes in the prevailing traffic congestion and traffic controls.

The self-assignment capability circumvents the need to use either an explicit time slice or iterations during the traffic assignment. Consequently, one can consider continuously variable traffic demands and controls, both freeway and signalized networks, as well as any links that join them.

#### 3.3.1 Basic Structure [19]

Figure 3.4 provides an overview of the main steps within the modelling approach and indicates that it basically consists of four stages. The first stage sets up the model by generating the configuration of the network (link-node structure) and specifying the traffic demands (O-D demands). The second stage performs the actual simulation of traffic flows; it enters vehicles into the network; routes them through it; and then remove them upon reaching their destination. This second phase frequently interfaces with the third, which updates the dynamic parameters of the network, and may provide intermediate statistics or graphics. Lastly, the fourth stage generates any final statistics.

Insert Figure 3.4

Figure 3.4 also illustrates that the main simulation consists primarily of a loop, which steps through time in increments of a decisecond. Within this loop, checks are made to see if any vehicles are eligible to enter the network or to be moved forward within it. In addition, checks are made to determine if minimum path trees should be updated or any intermediate statistics provided.

## 3.3.2 Input Data Requirements [19]

The model requires five basic inputs:

Node coordinates file
 Link descriptor file
 Traffic demand file
 Signal timings file
 Incident descriptor file

## 3.3.2.1 Node Coordinates File

This file is used to describe the x-y location of the nodes. The coordinates are utilized primarily for purposes of displaying the network and its attributes during the progress of the simulation, but they can also be used to assist in the computation of approximate link lengths.

## **3.3.2.2** Link Descriptor File

This file provides the attributes of each link that joins the above nodes. The primary data required in this file are:

- link length (meters)
- number of lanes (integer)
- saturation flow per lane (veh/hour/lane)
- saturation flow reduction coefficient for congested conditions (ratio = congested saturation flow/uncongested saturation flow)
- number of traffic signal controlling the link, if any
- signal phase number (phase during which the signal has effective green)
- link descriptor label (character string)

#### **3.3.2.3** Traffic Demand File

The traffic demand to be applied to the network is expressed to the model as a series of origin-destination flow rates for a user-specified time period.

The model internally translates these flow rates into corresponding individual vehicle departures during the specified 'time period.

#### 3.3.2.4 Signal Timings File

This file identifies the signal control logic that is to be used to set or modify the signal timings at any signalized intersections or ramp meters in the network. This file provides the initial timings as well as the signal timing constraints that cannot be violated by the traffic signal optimizer, if utilized:

- initial, minimum and maximum cycle time (sec)
- offset of phase 1 relative to absolute clock (sec)
- number of phases at intersection (integer)
- phase start/end time and associated lost time

#### 3.3.2.5 Incident Descriptor File

This file indicates the number of incidents that are to be modelled, their severity and duration. Multiple consecutive or concurrent incidents can be modelled. The incident severity is specified as an effective reduction in the number of lanes, while the incident duration is specified in terms of the start and end times of the incident with reference to the master simulation clock.

#### 3.3.3 outputs [19]

At the conclusion of the simulation run, the model produces two types of summary outputs. The first provides user-oriented statistics on the trips between each origin-destination (Appendix C). The second provides system-oriented statistics on the operation of each network link (Appendix C). INTEGRATION was not tested as a copy of the program was not available at the time the evaluations were conducted in November 1990. However, the model is now available.

#### 3.4 MODEL SELECTION

Based on an evaluation of the test runs and further evaluation of previous applications of each of the models, it was determined that **CONTRAM** was best suited for this particular application. This is not a negative reflection upon the other two models, as both other models could have been used for this project as well. Chapter 4 describes in greater detail the features of **CONTRAM** that made it most attractive for 'this application.

#### 4.0 FEATURES OF CONTRAM RELEVANT. TO THIS APPLICATION

**CONTRAM 5** is the latest version of the Transport and Road Research Laboratory's traffic assignment program which models time-varying traffic demands on urban and other road networks subject to capacity constraints, and predicts the variation through time of the resulting routes, queues and delays. This chapter summarizes the main features of the model relevant to our specific application.

Two programs, COMEST and RODIN [20], used in our study in relation with CONTRAM are also discussed in this chapter.

### 4.1 CONTRAM 5

#### 4.1.1 Representation of Traffic

The traffic, for each Origin-Destination movement, is handled in groups called packets. Each packet consists of an integral number of vehicles of the same type, typically in the range 1-20, assigned at the same time between the same origin and destination. The grouping of vehicles into packets can be regarded, for assignment purposes, as a process in which the behavior of one vehicle in a packet is taken as typical of the behavior of the other vehicles in that packet.

The default mode of packet generation in **CONTRAM** 5 is variable packet size. This means that packet size can be adjusted up to a certain maximum value, so as to match the demand specified in the O-D data. The maximum packet size for each O-D movement can be specified in the data or calculated automatically (subject to an optional scaling factor **or** an optional upper limit). The optimum choice of packet size is necessarily a compromise:

- Large packet sizes require fewer assignments leading to shorter run time, but produce a grainy loading and possibly an unrealistic assignment;
- Small packet sizes tend to give a better representation of the demand flow profile.

#### 4.1.2 Assignment

The method of assignment in **CONTRAM 5** is a modified form of Dijkstra's algorithm which at any point on a route seeks to minimize the sum of the actual cost from the origin to that point and an estimate of the minimum cost from that point to the destination. Packets are assigned to their minimum cost routes by an iterative procedure shown in Figure 4.1. After the initial loading iteration the sequence of operations for assigning each packet is:

- (i) Remove the increment of flow, due to the packet, from the flows stored for each link (in the appropriate time intervals) for the route taken by the packet in the previous iteration;
- (ii) Recalcula e the queues on links affected by the previous route of the packet;
- (iii) Assign the packet to its new minimum cost route;
- (iv) Add the flow due to the packet to the links on the new route and recalculate the queues affected by the new route;
- (v) Take the next packet and repeat steps (i) through (iv).

The updating of flows and queues on links and the recalculation of delays for the reassignment of each packet is made for the appropriate time intervals during which a packet travels along each link of its journey. The procedure for loading and assigning traffic combines progressive and incremental loading techniques. Although the assignment procedure for an individual packet is all or nothing, it is not all or nothing overall, since different packets for the same O-D movement can be assigned to different routes in response to changes in **traffic** conditions throughout the period modelled.

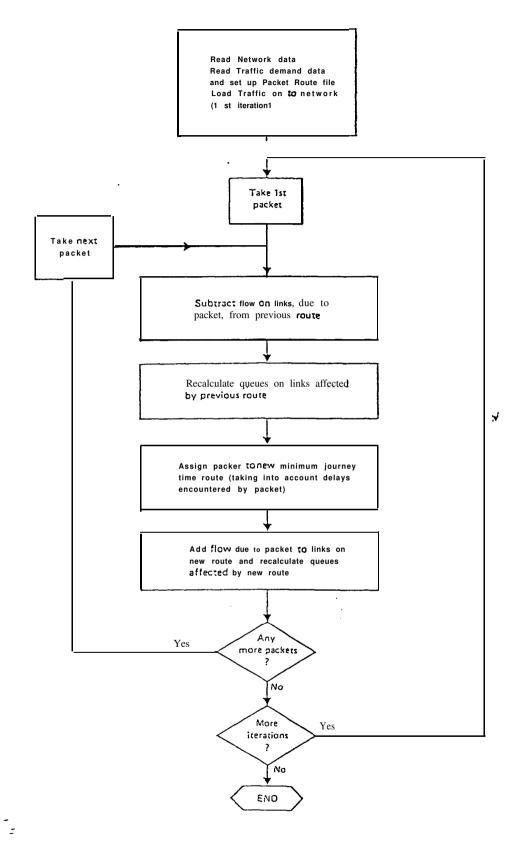
### 4.1.3 Queue and Delay Model

**CONTRAM** 5 calculates the lengths of queues using time-dependent stochastic queuing theory. **Random**and-oversaturation queues are calculated using the queue formulae developed by Kimber and Hollis (1979) and Kimber and Daly **(1986)**, and other formulae are used to calculate queues due to signals. Vertical queuing is assumed, i.e., the queuing process is formally defined as occurring at the stop line.

Queuing models are compatible with those employed by the intersection modelling programs ARCADY2, PICADY2 and **OSCADY2** (Semmens 1985 a,b, Burrow 1987). A queue is calculated either for a particular moment within a time slice, such as the arrival time of a packet, or for the end of a time slice, to provide a size for the initial queue in the next time slice. The size of the queue depends on five variables:

- 1) the initial queue at the start of the time interval;
- 2) the mean vehicle arrival rate;

#### FIGURE 4.1 ITERATIVE PROCEDURE USED BY CONTRAM



- 3) the throughput capacity (average flow rate at which vehicles discharge from a queue on a link);
- 4) the length of time during which the queue develops;
- 5) the intersection type.

#### 4.1.4 Blockirig-Back

Blocking-back occurs when the queue of vehicles on a link extends back to the previous links, thereby blocking free access to the link from the upstream links. The net effect is to reduce the throughput capacity of the upstream links as long as the blocking-back condition persists.

The basis of the blocking-back mechanism is as follows: since the **CONTRAM** model is based on vertical queuing at a stopline, the onset of blocking-back on a link is detected by comparing the equivalent length of the queue with the storage capacity of the link (number of vehicles which can be stored on the link). The comparison is made immediately after each packet has been assigned to its new route, for each of the links along the packet's route working backwards from the destination to the origin. If the queue on a link calculated, using the current arrivals, is found to exceed its storage capacity, then the throughput of the upstream link is reduced to match the sum of the initial queue on the link and the current arrivals at the stop line, for the rest of the time interval for the remainder of the iteration.

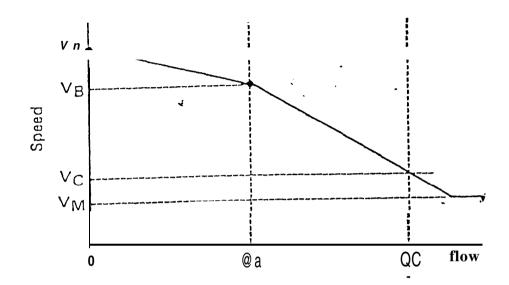
#### 4.1.5 Speed/Flow Relationships

Speed/flow relationships are intended to be used in **CONTRAM** for two main purposes: to represent cruise speeds on high-speed and limited access roads; and to take account of the aggregate effect of delays in buffer networks, i.e., parts of a network which need not be **modelled** in detail but which may affect traffic alignment in the areas of main interest.

The effect of a speed/flow relationship is in addition to any delay due to explicit queuing at the downstream end of the link to which it applies. The relatively simple, time-independent, form assumed for speed/flow relationship, presumes that traffic is free-flowing or well under saturation so that any queuing effects can be subsumed by the relationship. The speed/flow relationships are not intended to model congestion.

**CONTRAM 5** uses COBA-type speed/flow relationships whose general form consists of two linear sections of different slope (see Figure 4.2). The exact form of each relationship is determined by entering as data three points through which it passes:

FIGURE 4.2 SPEED/FLOW RELATIONSHIP IN CONTRAM



 $V_0 - The free speed where flow is Zero$   $V_8 - The break point speed where the slope of the line changes$  $<math>V_c - The capacity point, which is the highest level of traffic flow observed$  $<math>V_M - The speed at which the inter-vehicle headway equals minimum distance headway input by the user$  $<math>Q_B - The break point flow$  $O_C - The capacity flow$ 

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- 1) the free speed (where flow is zero);
- 2) the break point (flow and speed) where the slope changes;
- 3) the capacity point (flow and speed) which is a point through which the second section passes.

This last point need not actually represent capacity but it is convenient to identify it with the highest level of traffic flow that has been observed. A minimum speed cut-off can also be entered.

# 4.2 COMEST

COMEST stands for Constrained O-d **ESTimation**. Its purpose is to fit a time-varying origin-destination matrix to a set of observed link counts and set of routes.

# 4.2.1 Principles

Due to the difficulty of obtaining detailed origin-destination information, a synthetic O-D matrix generation technique must be used. The COMEST program uses a combination of entropy maximization (Van Zuylen and Willumsen, 1980) and Furness-type balancing (Maher, 1987) to achieve its objectives. The latter acts as a constraint on the way individual O-D flows change so avoiding bias due to the number of times each O-D is counted.

# 4.2.2 COMEST/CONTRAM Relationship

COMEST is designed to be used with CONTRAM-type data files in which time-variation is represented by specifying O-D and link counts in up to 13 consecutive time slices. A flow diagram of the operation of COMEST in relation with **CONTRAM** is shown in Figure 4.3.

COMEST loads three sets of data in sequence:

1) a set of control parameters;

# RELATIONSHIP BETWEEN COMEST AND CONTRAM

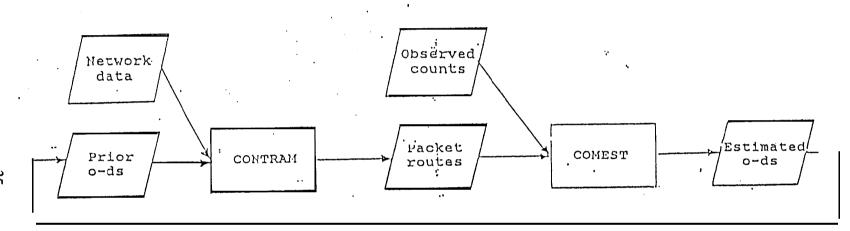
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FIGURE 4.3 COMEST-CONTRAM RELATIONSHIP

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- 2) a set of target link counts, which may be time-dependent and disaggregated by the three CONTRAM vehicle classes;
- 3) a set of prior O-D movements and routes, in the form of a CONTRAM-type route file containing the routes and times of a number of packets.

# 4.3 RODIN [20]

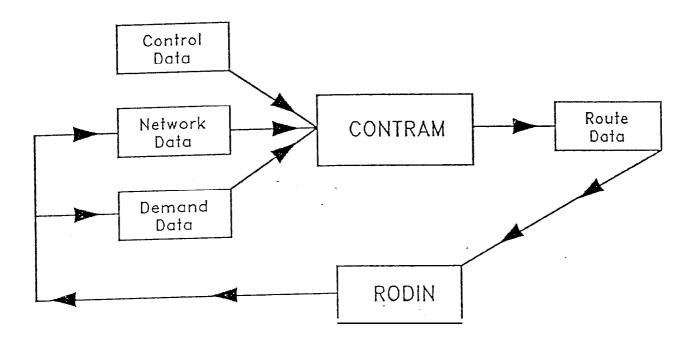
**RODIN** is an external software developed by Nick Taylor (**TRRL**) and intended to be used in relation with **CONTRAM** to simulate route guidance. This program converts a packet route file output by **CONTRAM** into an O-D matrix and a set of routes which it embeds as fixed routes in a copy of the network file. The O-D movements are duplicated and each set is preceded by a percentage multiplying or split factor.

When rerun using the new network and O-D files as data, the first set of 0-Ds is assigned on the fixed routes (i.e. along the original routes), while the second set is assigned to minimum cost routes in the usual way. This provides a framework in which experiments involving two user classes (guided and unguided vehicles) can be performed.

The use of **RODIN** in relation with **CONTRAM** is highlighted in Figure 4.4. **RODIN** is designed to perform the basic operations described above. In addition to these functions, it provides:

- a choice of methods for setting packet sizes;
- alternate vehicle class for the second set of 0-Ds;
- randomization of the output O-D counts.





#### 5.0 SMART CORRIDOR

Five key factors led to the decision whereby the Smart Corridor in Los Angeles, California would be used as the integrated freeway/arterial network in the **CONTRAM** simulation of the potential benefits of in-vehicle information systems.

- 1) The availability of a good database in terms of traffic counts, arterial geometric considerations, average arterial and freeway travel times, and freeway capacity calibrations.
- 2) The size of the corridor and the fact that the corridor is experiencing traffic congestion and incidents occur regularly.
- **3)** The interest and continued assistance of CALTRANS and the City of Los Angeles Department of Transportation.
- 4) The Pathfinder in-vehicle motorist information and road navigation project that is currently underway within the corridor.

#### 5.1 Database

As mentioned previously, this project is a continuance of an earlier project [3]: the database used in the earlier project provided the vast majority of information used in setting up the CONTRAM model. Due to time and resource constraints, and since the earlier project had only evaluated the morning peak period, it was determined that the morning peak period would be used in all analyses. The morning peak period captures mostly work trips; therefore, people are typically more time conscious. Additionally, the morning peak period provides a more defined peak period as well as the fact that the arterials have more available capacity in the morning peak hours. Demand data was provided to the earlier research effort by the City of Los Angeles Department of Transportation and Caltrans.

#### **5.1.1 Supply Parameters**

To properly code the network into the **CONTRAM** model it was important that the supply side of the Smart Corridor be coded properly. These supply parameters consist of the link distance, the cruise speed on each link, and the number of lanes and the ideal saturation flows per link for each intersection approach. The saturation flows used on each link were a result of the earlier research team's effort to calibrate the model. Table 5.1 summarizes the general guidelines established for the saturation flows.

Movement Type	Ideal Saturation Flow (vphgpl)
Exclusive Through	1700
Exclusive Left (Protected)	1600
Exclusive Right	1450
Shared Through-Right	I 1700

Table 5.1 Ideal Saturation Flows

The ideal saturation flow for a shared through-left movement was calculated by reducing the ideal saturation flow for an exclusive left turn movement by applying a left turn factor. This factor was determined from utilization of Chapter 9 of the 1985 Highway Capacity Manual[21]. An absolute minimum of 450 vphgpl was used as a result of the advice from the City of Los Angeles Department of Transportation.

The ideal saturation flows for exclusive left-turn movements with permitted phasing was calculated based upon the relationship of the exclusive left permitted saturation flow rate versus the opposing flow rate. Once again, the saturation flows were determined from Chapter 9 of the 1985 Highway Capacity Manual [21]. As before for shared through-left movements, an absolute minimum of 450 vphgpl was used on advice of the City of Los Angeles Department of Transportation.

#### 5.1.2 Control Parameters

The control parameters required for the **CONTRAM** model consist of the signal timing data. Information such as interval lengths, minimum phase durations, cycle lengths, offsets/yield points, reference intervals, type of signal control, and phase sequencing were all obtained from the City of Los Angeles Department of Transportation.

#### 5.2 Size of the Corridor and Traffic Congestion

The Santa Monica Freeway in Los Angeles is considered to be one of the most congested freeways in the world. As one of eight freeways which provides direct access to the downtown Los Angeles area, the

Santa Monica Freeway is also the only facility which connects the west side of Los Angeles to the central downtown region. The Santa Monica Freeway is the only east-west freeway between the Santa Monica Mountains to the north and the Artesia Freeway to the south, a distance of approximately 13 miles. The five major arterials, Olympic, **Pico**, Venice, Washington and Adams Boulevards are connected to the freeway by approximately 15 major north-south streets. Figure 5.1 displays a map of the entire corridor.

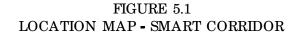
The principal'cause of **traffic** congestion is the peak hour(s) travel demands. Although the Santa Monica Freeway is four to five lanes in each direction, the travel demand during the peak hours still exceeds the amount of available freeway capacity. Daily traffic volumes on the freeway range from a low of approximately 180,000 to a high of nearly 315,000 close to the downtown area. Stop-and-go conditions exist daily during the peak hours on the freeway, where the average speeds throughout the corridor on the freeway are often below 35 miles per hour in both directions.

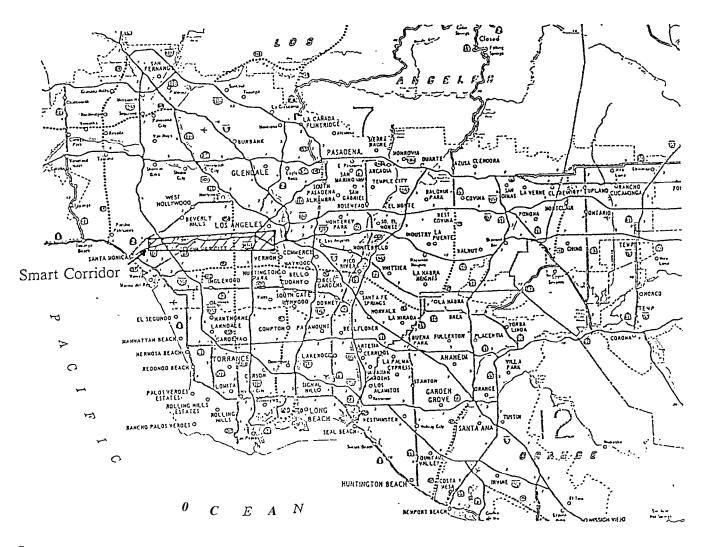
Traffic on the parallel arterials is different from that on the freeway. Olympic Boulevard carries the most traffic of the five parallel arterials with a range of approximately 14,000 vehicles per day to nearly 32,000 vehicles per day near Century City. Adams Boulevard is the least travelled arterial with volumes ranging from 2,600 vehicles per day to nearly 11,000 vehicles per day. Adams, Washington and Venice Boulevards have significant amounts of unused capacity. Therefore, the arterials offer a considerable savings over the freeway in terms of travel time, especially when an incident occurs on the freeway. Thus, diverting freeway traffic to one of the major arterials in an incident scenario is a high priority of **the** Smart Corridor Demonstration Project.

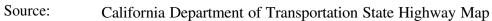
#### 5.4 Pathfinder

Pathfinder is an experimental project designed to test the feasibility of using the latest technological devices to assist motorists in avoiding traffic congestion. The Smart Corridor is the test bed for the project. The project provides drivers of specially equipped General Motors Oldsmobile Eighty-Eights, real-time information about accidents, congestion, highway construction, and alternate routes. The invehicle motorist information and road navigation system demonstration project is being sponsored by Caltrans, the Federal Highway Administration and General Motors.

Since the objective of this research is to determine the potential benefits of in-vehicle information systems using the **CONTRAM** model, meaningful results may be used at some point to compare with those to come out of the Pathfinder demonstration project. Thus, any results found from this research may be compared with "real-world" results to make a more definitive determination as to what the potential benefits may be since each project is using the Smart Corridor as its test bed.







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#### 6.0 INITIAL MODEL APPLICATION

The purpose of this chapter is to describe the initial applications of the **CONTRAM** model to the Smart Corridor with particular emphasis on freeway performance modelling. The freeway performance modelling was found to be more difficult than originally anticipated and required a number of modifications which are described in this chapter. The freeway performance modelling undertaken for a simple directional freeway is presented first, and then the modelling of the I-10 Santa Monica Freeway is discussed.

The **CONTRAM** model was primarily developed for use in the design of traffic management schemes for urban signalized arterial networks. As mentioned in Chapter 4, **CONTRAM** has the ability to represent limited access and buffer network roads. The speed flow relationships represent the relationship between average speed and flow on roads where cruise time is a significant proportion of total time and journey times on links in a buffer network in order to simulate the general effects of capacity restraint. A standard **COBA** type speed/flow relationship is used whereby two linear sections of different slopes, one representing the break point speed/flow and the second representing the capacity point speed/flow are used.

In order to gain a more clear understanding of the freeway modelling characteristics within CONTRAM, a linear test segment of freeway was designed. To evaluate the characteristics of the CONTRAM model, both manual calculations and the FREQ model were chosen as tools for calibration. The FREQ family of freeway simulation models has been in existence since the 1960's [22]. Both manual calculations and the FREQ model were used in the I-10 calibration process. FREQ is a macroscopic deterministic simulation model in which time can be broken into equal discrete time-slices and the directional freeway segment divided into homogeneous subsets with demands and capacities remaining constant during each time slice . Merging and weaving analysis, when selected, follows the 1965 Highway Capacity Manual procedures. A limitation to the FREQ model is that freeway congestion can only begin and end at boundaries between time slices. The queue contour maps in FREQ provide a picture of both bottleneck locations and queue lengths over both time and space.

The criteria for freeway calibration were based on three key considerations. The first consideration was that **CONTRAM** identified the bottlenecks in the same subsections as those determined by manual calculations and shown in FREQ. The second consideration was that of queue length. Once the bottlenecks were identified and located properly, queue lengths were evaluated to see whether **CONTRAM** had the proper queue lengths as shown in the manual calculations and determined by FREQ. The third consideration in the freeway calibration process was that of freeway speeds in terms of free flow speeds, speeds at the bottleneck, and speeds within the congestion.

#### 6.1 Linear Test Freeway Segment

In an attempt to gain a more comprehensive understanding of the operation of the **CONTRAM** model as it relates to freeway operations, a simple linear test freeway segment was created as shown in Figure 6.1. The test freeway segment is 8,100 feet long with five subsections and nine time slices. Figure 6.1 also presents the 'time slice demands as well as the capacities assumed for each subsection. In the test segment, the first subsection through the third subsection is composed of three lanes. The fourth subsection is two lanes with a length of 100 feet. The fifth and last sub-section is composed of three lanes and is 2000 feet long. The capacity of each lane of the freeway is assumed to be 2000 passenger vehicles per hour.

The demands were set to create queuing at the bottleneck in the fourth time slice. All queuing would dissipate by the beginning of the ninth time slice. A manual shock wave analysis was conducted to predict queue lengths and speeds in each subsection during each time slice. The complete results of the analysis are contained in Appendix D. Figure 6.2 displays the shock wave and speed information in **km/hr** by time slice and subsection. In Figure 6.2 the shock wave can be seen beginning in subsection three at the beginning of time slice four. At the end of time slice six and beginning of time slice seven, the queue reaches its longest at approximately 700 meters. The shock wave ends during time slice eight.

Figure 6.3 presents the speeds and shock wave as predicted by **CONTRAM**. As seen in the figure, the speeds predicted by **CONTRAM** do not match those from the manual calculations. The queue pattern does not identically match that of the manual calculations either.

Several key reasons for the differences between the manual analysis and the **CONTRAM** output deserve mention. It should be noted that because the **CONTRAM** model is macroscopic and sends vehicles through the system in packets, not all packets make it through each subsection during each time slice. To identify the bottleneck in the proper subsection, the approach used was to code the saturation flow of a link as the capacity of the downstream link. This technique is theoretically correct since the saturation flow of each link is measured as the throughput capacity of that link. Thus, in this particular application the bottleneck was properly identified in sub-section four.

The key input to calibrate queue lengths is the minimum distance headway. Since the **CONTRAM** model is designed for arterials, an estimated storage capacity is calculated by the program based on a minimum distance headway that is either provided by the program or input by the user. The default provided within the model for the minimum headway distance is 5.75 meters. The minimum distance headway directly determines the densities that are represented on the freeway. Since freeway densities are much lower than those at an intersection, the minimum distance headway in the **CONTRAM** model must be

# FIGURE 6.1 LINEAR TEST FREEWAY INFORMATION

	Subsection 1 Length = 2000° Capacity = 5000 vph	Subsection Z Length = 2000" Capacity = 5000 vph	Subsection 3 Length = 2000' Capacity = 8000 vph	Jubsection 4 Length = 100° Capacity = 4000 vph	Subsection 5 Length = 2000° Capacity = 5000 vph
	<b>}</b> -				
			<b>_</b>		<u>an an a</u>
Time Slice	Demand	Demand	Demand	Bemand	Demand
1	3000	3000	3000	3000	3000
2	3900	3900	3900	3900	3900
3	4000	4000	4000	4000	4000
4	4100	4100	4100	4100	4100
5	4100	4100	4100	4100	4100
6	4100	4100	4100	4100	4100
7	3800	3800	3800	3800	3800
, 8	3800	3800	3800	3800	3800
9	3800	3800	3800	3800	3800

.

Time Slice	SS 1	ss 2	SS <b>3</b>	SS 4	SS 5
1	SPEED	SPEED	SPEED	SPEED	SPEED
	94	94	94	91	· 94
2	SPEED	SPEED	SPEED	SPEED	SPEED
	93	- 93	93	70	93
3	SPEED	SPEED	SPEED	SPEED	S-PEED
	91	91	91	58	91
4	SPEED	SPEED	SPEED	SPEED	SPEED
	91	91	91 127	58	91
5	SPEED 91	SPEED 91	SP52D	SPEED 55	SPEED 91
6	SPEED 91	SPEED 91	SPEED	SPEED . 58	SPEED 91.
7	SPEED	SPEED	SPEED	SPEED	SPEED
	33	93	93 27	58	91
8	SPEED 93	SPEED 93	SPEED 27	SPEED 70	SPEED 93
9	SPEED	SPEED.	SPEED	SPEED	SPEED
	93	93	93	88	93

# FIGURE 6.2 SPEED/SHOCK WAVE INFORMATION - MANUAL CALC.

Time Slice	SS 1	SS 2	SS 3	SS 4	SS 5
1	SPEED	SPEED	SPEED	SPEED	SPEED
	95	45	108	91	·95
2	SPEED	SPEED	SPEED	SPEED	SPEED
	95	495	108	91	95
3	SPEED	speed	SPEED	SPEED	SPEED
	95	95	108	<b>56</b>	<b>95</b>
4	SPEED	SPEED	SPEED	SPEED	SPEED
	95	95	8	89	95
5	SPEED 95	SPEED 92	SPEED	SPEED 5C	SPEED 95
6	${}^{ m SPEED}_{ m 45}$	SPEED 88	SPEED	SPEED 56	SPEED - 95
7	SPEED	SPEED	SPEED	SPEED	SPEED
	95	91	4	90	95
8	SPEED	SPEED	SPEED	SPEED	speed
	95	95	]7	66	<b>95</b>
9	SPEED	SPEED,	SPEED	SPEED	SPEED
	45	95	102	90	95

# FIGURE 63 SPEED/SHOCK WAVE INFORMATION - CONTRAM

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manipulated to create densities that more closely reflect those that are observed on freeway segments. The storage capacity of each link determines the amount of queuing each sub section can handle. Table 6.1 illustrates the conversion of distance headway in meters to densities in vehicles per mile per lane. The minimum distance headway input by the user is universal over all links, thus densities cannot be changed at each link. Through a series of tests for the specific linear freeway segment under investigation in this study, the minimum distance headway of 20 meters was determined to most effectively represent queue lengths as found in the manual calculations.

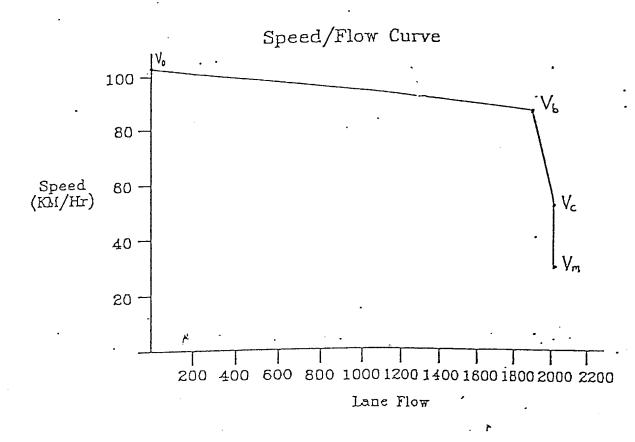
Minimum Distance Headway (m)	Density (Vehicles/Mile/Lane)
5.75	280
7.50	215
10.00	161
12.50	129
15.00	107
16.00	101
17.00	95
18.00	I 89
19.00	85
20.00	80

 Table 6.1

 Relationship Between Minimum Distance Headway and Density

To more realistically represent speeds on the linear test segment as determined in the manual calculations, the speed flow relationship curve as specified in **CONTRAM** was modified in conjunction with the input cruise speeds. The most effective method of replicating speeds determined by the manual calculations was to use the speed-flow relationships only at the bottleneck and one subsection downstream from the bottleneck. As mentioned previously, **CONTRAM** has the ability to model high speed limited access roads through the use of a speed-flow curve. Figures 6.4 and 6.5 present the speed flow curves that were

FIGURE 6.4 SPEED FLOW CURVE - TEST FREEWAY (BOTTLENECK)



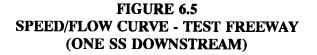
V<sub>0</sub> - The free speed where flow is zero

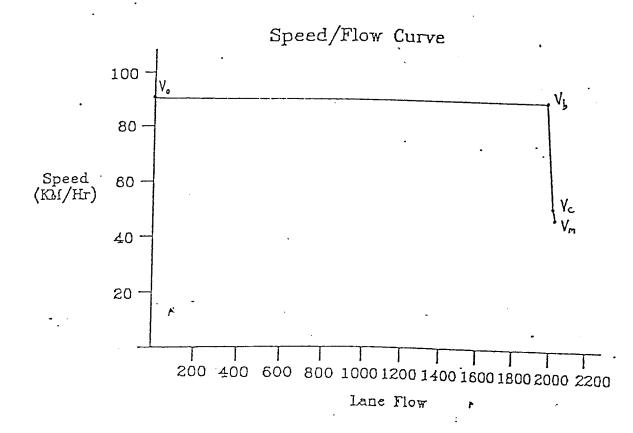
 $V_{g}$  - The break point speed where the slope of the line changes

 $V_c$  - The capacity point, which is the highest level of traffic flow observed

V<sub>M</sub> - The speed at which the inter-vehicle headway equals minimum distance headway input by the user

- $Q_{\rm B}$  The break point flow
- $Q_{c}$  The capacity flow





 $V_0$  - The free speed where flow is zero

 $V_{g}$  - The break point speed where the slope of the line changes

 $V_{C}$  - The capacity point, which is the highest level of traffic flow observed

 $v_{M}$  - The speed at which the inter-vehicle headway equals minimum distance headway input by the user

- $Q_B$  The break point flow
- $Q_c$  The capacity flow

2

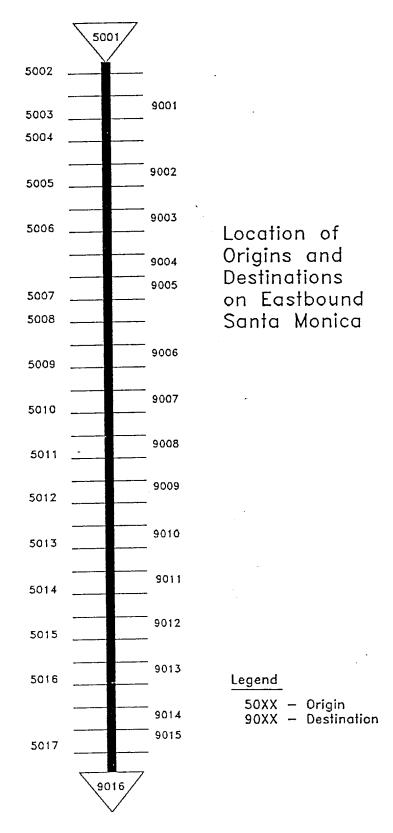
used to best replicate the results as found in the manual analysis for the bottleneck and downstream section. The speed flow curve is a replication of the COBA curve used in the CONTRAM model as described in Chapter 4. As shown in the figures, V<sub>e</sub> represents the point at which the highest level of flow is observed.  $V_{\rm h}$  represents the break point speed and  $V_{\rm m}$  represents the speed at which the speedflow relationship predicts an inter-vehicle headway equal to the minimum distance headway as input from the user. The curves shown in Figures 6.4 and 6.5 are those that provided the best results in terms of matching the 'queue lengths and speeds as derived from the manual calculations. In the subsections without the speed flow relationships the cruise speed of 92 km/hr was used. The free flow speeds on each link do not match because the model truncates the mean time per vehicle in seconds on the link and does not represent a constant free flow speed. The speed flow relationship that CONTRAM uses for modelling high speed limited access roads does not allow for modelling traffic congestion. That is, the speed-flow relationship only obeys the upper limb of the true speed flow relationship on a freeway. Thus, the speeds as output from **CONTRAM** do not obey the speed-flow relationship as input to the program in congestion. The method CONTRAM uses for calculating free flow speeds does not provide for a constant speed across all free flowing links. Additionally, for congested links, the speeds as represented by the model are much **too** high. This has been identified as a problem and is something that needs to be addressed in future research efforts if CONTRAM is to be used to represent a freeway segment.

Although freeway conditions could be represented somewhat realistically through the use of the procedures described in the previous paragraphs, a question regarding the influence of freeway ramps on bottlenecks and other sections of the freeway remained unanswered. To help answer some of the remaining questions regarding the operation of the model another linear test freeway segment was introduced. However, this time a real life freeway corridor was used. The Santa Monica Freeway in Los Angeles, California was modelled in the eastbound direction to reach a better understanding of the operations of the **CONTRAM** model. For comparison purposes, the FREQ model was also applied.

#### 6.2 Smart Corridor Freeway Modelling

The eastbound section of the twelve mile Santa Monica Freeway was the next segment used in the freeway calibration process. The network consists of 32 subsections with 16 on-ramps and 15 off-ramps. The demand data consists of 17 origins and 16 destinations over eight 30 minute time slices. The network and demand information is shown in Figures 6.6 and 6.7. The elements that were given special consideration in this process were; bottleneck location, queue length, and average speeds.

FIGURE 6.6 NETWORK FOR SANTA MONICA EASTBOUND



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# FIGURE 6.7 DEMAND INFORMATION - SANTA MONICA EB

**. .** .

GTOTAL VEHICLE FLOW RATES FROM			RING EAG	CH TIME	SLICE (	VEX/X)			
ORIGINS	FLOWS	•							
5001	1498	2854	3649	3856	4270	4409	3812	3656	٥
5002	2274	3090	3283	2994	2980		3262	3236	0
5003	569	771	1009	1102	899	884	777	757	0
5004	212	357	387	358	374	404	382	336	0
5005	355	377	335	337	327	341	401	403	0
5006	66	280	316	389	382	504	456	508	0
5007	341	384	613	638	515	478	386	347	ů 0
5008	589	1031	976	899	800	768	863	812	0
5009 -	426	479	427	359	324	398	415	450	0
5010	803	833	849	694	627	665	594	500	0
5011	854	940	1007	1027	936	891	798	773	0
5012	715	748	798	1061	763	683	596	434	0
5013	460	606	678	699	542	523	498	433	0
5014	376	409	413	397	378	289	278	231	0
5015	• 276	390	367	422	345	288	277	314	0
5016	357	362	367	359	358	280	263	256	0
5017	600	810	670	707	593	600	560	600	0
TOTAL VEHICLE FLOW RATES DIREC	TED TOWAR	DS EACH	I DESTI	ATION I	OURING F	ACN TH			
						WPU 111	וב סבוננ	E (YEH/H'	
DESTINATIONS	FLOWS				-	F1		t (VEH/H)	)
					-			t (VEN/H)	
		6506	7039	6985	6180	6106	5052		
DESTINATIONS	FLOWS				-			4856	0
DESTINATIONS 9016	FLOWS 4505	6506	7039	6985	- 6180	6106	5052	4856 171	0 0
DESTINATIONS 9016 9003	FLOWS 4505 52	6506 101	7039 130	6985 129	- 6180 128	6106 134	5052 151	4856	0
DESTINATIONS 9016 9003 9006	FLOWS 4505 52 81	6506 101 90	7039 130 104	6985 129 113	- 6180 128 149	6106 134 78	5052 151 111	4856 171 129	0 0 0
DESTINATIONS 9016 9003 9006 9008	FLOWS 4505 52 81 150	6506 101 90 165	7039 130 104 265	6985 129 113 267	6180 128 149 253	6106 134 78 236	5052 151 111 312	4856 171 129 346	0 0 0 0
DESTINATIONS 9016 9003 9006 9008 9009	FLOWS 4505 52 81 150 55	6506 101 90 165 100	7039 130 104 265 193	6985 129 113 267 228	- 6180 128 149 253 284	6106 134 78 236 300	5052 151 111 312 243	4856 171 129 346 203 235	0 0 0 0
DESTINATIONS 9016 9003 9006 - 9008 9009 9010	FLOWS 4505 52 81 150 55 157	6506 101 90 165 100 172	7039 130 104 265 193 185	6985 129 113 267 228 182	6180 128 149 253 284 165	6106 134 78 236 300 148	5052 151 111 312 243 194	4856 171 129 346 203	0 0 0 0 0
DESTINATIONS 9016 9003 9006 - 9008 9009 9010 9011 9012	FLOWS 4505 52 81 150 55 157 123	6506 101 90 165 100 172 194	7039 130 104 265 193 185 321	6985 129 113 267 228 182 344	6180 128 149 253 284 165 344	6106 134 78 236 300 148 375	5052 151 111 312 243 194 311 596	4856 171 129 346 203 235 271 587	0 0 0 0 0 0 0 0
DESTINATIONS 9016 9003 9006 9008 9009 9010 9011	FLOWS 4505 52 81 150 55 157 123 260	6506 101 90 165 100 172 194 356	7039 130 104 265 193 185 321 526	6985 129 113 267 228 182 344 545	6180 128 149 253 284 165 344 604	6106 134 78 236 300 148 375 627	5052 151 111 312 243 194 311	4856 171 129 346 203 235 271 587 561	0 0 0 0 0 0
DESTINATIONS 9016 9003 9006 9008 9009 9010 9011 9012 9013	FLOWS 4505 52 81 150 55 157 123 260 358	6506 101 90 165 100 172 194 356 434	7039 130 104 265 193 185 321 526 591	6985 129 113 267 228 182 344 545 633	6180 128 149 253 284 165 344 604 598	6106 134 78 236 300 148 375 627 656	5052 151 111 312 243 194 311 596 736	4856 171 129 346 203 235 271 587 561 855	0 0 0 0 0 0 0 0
DESTINATIONS 9016 9003 9006 9008 9009 9010 9011 9012 9013 9001 9001	FLOWS 4505 52 81 150 55 157 123 260 358 468	6506 101 90 165 100 172 194 356 434 529	7039 130 104 265 193 185 321 526 591 710	6985 129 113 267 228 182 344 545 633 872	6180 128 149 253 284 165 344 604 598 947	6106 134 78 236 300 148 375 627 656 1016	5052 151 111 312 243 194 311 596 736 993	4856 171 129 346 203 235 271 587 561 855	0 0 0 0 0 0 0 0 0 0
DESTINATIONS 9016 9003 9006 9008 9009 9010 9011 9012 9013 9001 9001 9002	FLOWS 4505 52 81 150 55 157 123 260 358 468 448	6506 101 90 165 100 172 194 356 434 529 530	7039 130 104 265 193 185 321 526 591 710 577	6985 129 113 267 228 182 344 545 633 872 864	6180 128 149 253 284 165 344 604 598 947 926	6106 134 78 236 300 148 375 627 656 1016 1011	5052 151 111 312 243 194 311 596 736 993 1003	4856 171 129 346 203 235 271 587 561 855 911 552	0 0 0 0 0 0 0 0 0 0 0 0
DESTINATIONS 9016 9003 9006 9008 9009 9010 9011 9012 9013 9001 9002 9004	FLOWS 4505 52 81 150 55 157 123 260 358 468 448 141	6506 101 90 165 100 172 194 356 434 529 530 174	7039 130 104 265 193 185 321 526 591 710 577 237	6985 129 113 267 228 182 344 545 633 872 864 412	6180 128 149 253 284 165 344 604 598 947 926 491	6106 134 78 236 300 148 375 627 656 1016 1011 500	5052 151 111 312 243 194 311 596 736 993 1003 530	4856 171 129 346 203 235 271 587 561 855 . 911	0 0 0 0 0 0 0 0 0 0 0 0
DESTINATIONS 9016 9003 9006 9008 9009 9010 9011 9012 9013 9001 9001 9002 9002 9004 9005	FLOWS 4505 52 81 150 55 157 123 260 358 468 448 141 150	6506 101 90 165 100 172 194 356 434 529 530 174 176	7039 130 104 265 193 185 321 526 591 710 577 237 252	6985 129 113 267 228 182 344 545 633 872 864 412 251	6180 128 149 253 284 165 344 604 598 947 926 491 302	6106 134 78 236 300 148 375 627 656 1016 1011 500 321	5052 151 111 312 243 194 311 596 736 993 1003 530 373	4856 171 129 346 203 235 271 587 561 855 911 552 353 429	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
DESTINATIONS 9016 9003 9006 - 9008 9009 9010 9011 9012 9013 9001 9001 9002 9004 9005 9007	FLOWS 4505 52 81 150 55 157 123 260 358 468 468 448 141 150 169	6506 101 90 165 100 172 194 356 434 529 530 174 176 200	7039 130 104 265 193 185 321 526 591 710 577 237 252 242	6985 129 113 267 228 182 344 545 633 872 864 412 251 253	6180 128 149 253 284 165 344 604 598 947 926 491 302 251	6106 134 78 236 300 148 375 627 656 1016 1011 500 321 268	5052 151 111 243 194 311 596 736 993 1003 530 373 364	4856 171 129 346 203 235 271 587 561 855 911 552 353	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0

10771 14721 16144 16298 15413 15497 14618 14046

0

52

#### 6.2.1 Bottleneck Location and Queue Length Pattern

Table 6.2 highlights the main freeway events as predicted by FREQ.

Time	Bottleneck Location	Queue Length (miles)
6:30 - 7:00	SS 29	1.9
7:00 - 7:30	SS 29	3.7
7:00 - 7:30	SS 13	1.4
7:30 - 8:00	<b>SS</b> 29	8.0
8:00 <b>- 8:30</b>	s s 29	3.6
8:00 - <b>8:30</b>	ss 14	1 2.2
8:30 - 9:00	SS 29	1.7
8:30 - 9:00	SS 21	0.8
8:30 - 9:00	SS 14	2.0
9:00 - 9:30	ss 14	0.3

# Table 6.2FREQ Main Freeway Events

As *seen* in the table, the major bottlenecks were identified in subsections 14 and 29. Each freeway subsection was coded as an uncontrolled link in the CONTRAM network while the on-ramps were coded as signalized links with 100 percent green time. The first approach was to code the saturation flow of a link as the capacity of the downstream link. This technique is theoretically correct since the saturation flow of each link is measured as the throughput capacity of that link. The results obtained from this technique did not closely resemble the results provided by FREQ. A possible explanation for the discrepancies could be the ramp merge and diverge points and their influence on capacity.

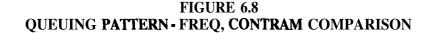
The second approach was to input the capacity of each subsection from FREQ as the saturation flow. This technique led to the results shown in Table 6.3. As shown in the figure, the bottlenecks were usually identified one subsection downstream from those in the FREQ runs.

Time	Bottleneck Location	Queue Length (miles)
7:00 <b>- 7:30</b>	ss 30	1.4
7:00 - 7:30	SS 22	0.6
7:00 - 7:30	SS 14	1.7
7:30 - 8:00	SS 30	8.0
8:00 - 8:30	ss 30	1.6
8:00 <b>- 8:30</b>	s s 22	1.0
8:00 - 8:30	SS 14	2.1
8:30 - 9:00	SS 30	1.4
8:30 - 9:00	SS 22	0.7
8:30 - 9:00	SS 14	2.1
9:00 - 9:30	ss 14	0.2

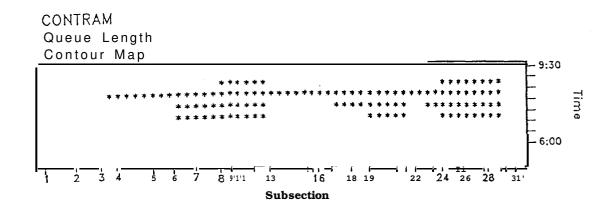
Table 6.3CONTRAM Main Freeway Events

The comparison between Tables 6.2 and 6.3 shows that **CONTRAM** typically identifies bottlenecks one subsection downstream from those of FREQ, and there does not seem to be a way of modifying **CONTRAM** to model it correctly.

The next objective was to obtain the queue patterns as produced by FREQ. Queue length patterns are directly affected by the storage capacities input in the **CONTRAM** network file. As mentioned previously, the minimum distance headway in **CONTRAM** determines the optimum densities that will be replicated on each link. For this particular application, the minimum distance headway which provided the queue pattern which most closely resembled those provided by FREQ was found to be 50 meters or a density of 32 vehicles per mile per lane. Figure 6.8 shows the queuing patterns from both FREQ and **CONTRAM**. While not perfect, this was the closest agreement based on modifying the minimum distance headway.



CONTOUR DIAGRAM CF QUEUS LENGTH BEFGRE OPTIMIZATION • • • SEGIN • 1155 SLICE ..... ΠE . . s . ł, . - 9:30 ÷. 7. \*\*\*\*\*\*\*\*\*\*\*\*\*\*\* 1):11:1 ) fritte frittette 5 63 47 63 **6**4 1 . \*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\* \*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\* \*\*\*\*\*\*\*\*\*\*\*\*\* \*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\* -2:09 Ι. . 22 24 26 E2 ..... 102 : : 93 0= : 01 PLANK DENOTES NOVING TRAFFIC. ASTERISY DENOTES OVEVED VEHICLES AVE TO MAINLINE CONSESTION. N DENOTES DUEVED VEHICLES DUE TO MERGING. 8 DENOTES QUEVED VEHICLES AVE TO MAINLINE CONSESTION AND MERGING. (WHEN POTH QUEVES EXIST, LENGTH OF DISFLAY REPRESENTS MAINLINE CONSESTION.) (HSTITUTE OF TRAMEPORTATION STUDIES WHIVERSITY OF CALIFORNIA, BERKELEY (413)-542-7390



#### 6.2.2 Average Speeds

Figure 6.9 shows the speeds predicted by FREQ. When calibrating the speeds predicted by CONTRAM, two key elements must be considered: free-flow speeds and speed-flow relationships. A uniform freeway free-flow speed of 85 km/h (53 mph) was adopted. Based on the conclusions of Section 6.1 and trial and error, speed-flow relationships were only used in the bottleneck subsections (14, 22 and 30) after the bottleneck locations were identified by a first run. As seen in Figure 6.9, once again CONTRAM predicts speeds within the congestion that are much too high. The speeds one subsection downstream from the bottleneck are too high. It is unclear just how much influence the freeway on-and off-ramps have on the speeds as determined by the model. Further analysis is required to determine the precise amount of influence on-and off-ramps have on average speeds.

#### 6.2.3 Overall Summary Measures

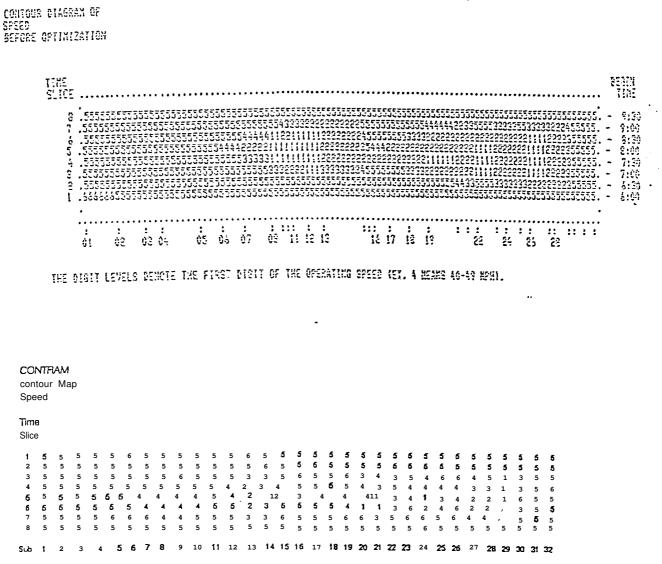
Table 6.4 displays the overall network wide summary results from the FREQ run and the CONTRAM run.

Network Summary Measure	FREQ	CONTRAM
Total Travel Time (veh-hr)	8035	7546
Total Travel Distance (veh-mi)	290975	306388
Overall Network Speed (mi/hr)	36.2	40.6

Table 6.4Overall Network Wide Summary Results Comparison

As seen in the table, from a system-wide perspective, the results are fairly comparable. Once again, the speed is higher in the **CONTRAM** model which is consistent with the previous freeway modelling effort.

FIGURE 6.9 SPEED PATTERN - FREQ, CONTRAM COMPARISON



The digit levels denote the first digit of the operating speed (ex.4 means 4049 mph)

#### 6.2.4 Conclusions

The freeway calibration process focused on three major elements of freeway operations.

- 1) The first element consisted of identifying freeway bottlenecks in the appropriate subsection. It was determined that for a simple network with no on-and off-ramps to identify the bottleneck in the proper subsection, it was necessary to code the saturation flow of a link as the capacity of the downstream link. This technique is theoretically correct since the saturation flow of each link is measured as the throughput capacity of that link. However, for a freeway section with a number of on-and off-ramps this technique did not prove effective and the bottlenecks were identified one subsection downstream.
- 2) Once the bottlenecks were identified and located properly, queue lengths were evaluated to see whether or not CONTRAM had comparable queue lengths to those estimated by the manual calculations and determined by FREQ. The key input to calibrate queue lengths is the minimum distance headway. Since the CONTRAM model is designed for arterials, an estimated storage capacity is calculated by the program based on a minimum distance headway that is either provided by the program or input by the user. The default provided within the model for the minimum headway distance is 5.75 meters. The minimum distance headway directly determines the densities which in turn determine the storage capacity of each link. The storage capacity of each link directly influences the queue lengths found throughout the network. For the first linear test segment a value of 20 meters was used, while in the eastbound Santa Monica Test Segment, a value of 50 meters was used.
- 3) The third consideration in the freeway calibration process was that of freeway speeds. This is the area of most concern. In free flow conditions, the freeway speeds could be approximated through the use of the speed-flow curve and also as input by the cruise speed. However, for congested conditions, the speeds represented by the **CONTRAM** model are not realistic. The speeds within the queues are much too high and the speeds at the bottleneck can only be approximated at best through the use of the speed flow relationship.

# 7.0 DESIGN OF THE EXPERIMENT, REFERENCE BASE ASSIGNMENT, SIMULATION AND VALIDATION

This chapter describes the design of experiment as well as the steps undertaken to develop a reference base assignment. The first section outlines the experiment while the remainder of the chapter is devoted to the development of the base reference assignment.

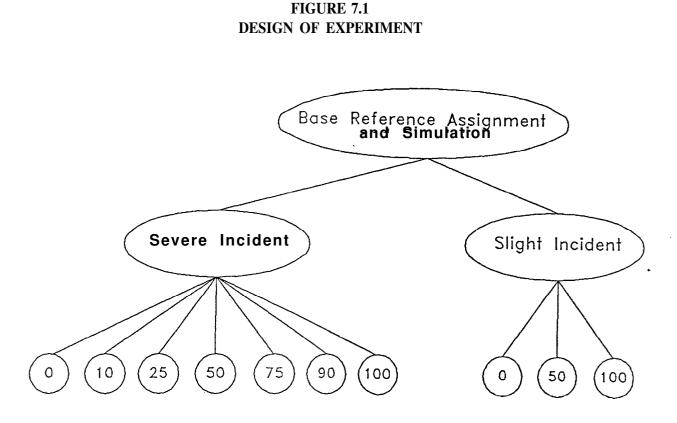
#### 7.1 Design of Experiment

After several months of attempting to model freeway congestion in a realistic fashion, it was decided that despite the limitations of the model with respect to freeway congestion, attention would be given to modelling the Smart Corridor with the **CONTRAM** model. With the goal of determination of the benefits of in-vehicle information systems, the experiment was designed as shown in Figure 7.1. The first step was to develop a reference base assignment and simulation that as closely as possible represented the Santa Monica Smart Corridor. The remainder of this chapter is devoted to discussion of this process. Since, from the previous study **[3]**, the benefits for non-incident conditions were found to be relatively small, the next step was to model a freeway incident. Two incidents were created and are discussed in Chapter 8. Once the incidents were created, tests were begun to evaluate the benefits of in-vehicle information systems. Investigations were made with varying percentages of equipped vehicles from 0 to 100 percent. Chapter 9 describes the results of the experiments with varying percentages of equipped vehicles.

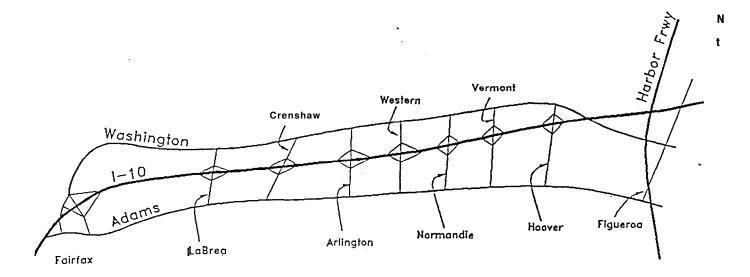
#### 7.2 Network Description and Calibration

Figure 7.2 presents the network **modelled** and used in the analysis. Approximately nine miles of the SMART Corridor with two parallel arterials were coded into the model. The eastern boundary of the network is the Harbor Freeway, while the western boundary is **LaCienega** Boulevard. In addition to the Santa Monica Freeway, the two parallel arterials coded were Washington Boulevard and Adams Boulevard. Ten major north-south streets connecting Washington, Adams, and the Santa Monica Freeway were coded as well.

As previously mentioned, the previous project (PATH-ITS-UCB-PRR-88-2) provided a comprehensive data base for this analysis, in the form of FREQ and TRANSYT input files. All data provided by the previous project represents the year 1987. Some updated information regarding speed-flow relationships provided by Caltrans was used as well.



Percentage of Vehicles Equipped with In-Vehicle Information



# FIGURE 7.2 MAP OF NETWORK MODELLED

. . . The coded network is composed of approximately 200 arterial links. A uniform free-flow speed of 35 miles per hour was adopted for the arterials. The link throughput capacity was determined by the rules described in Section **5.1.1**. The signal timing data were taken from the earlier study as well. Some minor modifications were made in the signal timings, especially at freeway ramp intersections, to improve the simulation of the network.

The freeway part of the corridor is composed of 51 uncontrolled links. The westbound direction is represented by 23 uncontrolled links, while the eastbound direction is made up of 26 uncontrolled links. Two additional links were used to represent the Harbor Freeway at the eastern boundary of the system. A uniform free-flow speed of 60 miles per hour was used on all freeway links. On the basis of the experiments described in Chapter 6, no speed-flow relationships were used and each link throughput capacity was input as the corresponding FREQ capacity. The storage capacity was determined by the standard default formula using the minimum distance headway of 20 meters which was found to be optimum after calibration as described in Chapter 6.

The freeway network includes 24 on-ramps (11 for the westbound direction and 13 for the eastbound direction). These links were coded in **CONTRAM** as signalized links with 100 percent green time. Thus, ramp metering was not **modelled** as a part of this project. A uniform free-flow speed of 30 miles per hour was used on freeway ramps.

### 7.3 Corridor Demand

To achieve a realistic demand level and pattern, a three step process was undertaken. The three steps consisted of the following:

- 1) creation of an origin-destination matrix;
- 2) using the COMEST program, the origin-destination estimator described in Chapter 4;
- 3) manipulation of the COMEST output to create a more realistic demand level

The third step, manipulation of the COMEST output, was necessary because of the crude nature of the original origin-destination matrix which was created in step one. The following paragraphs outline the procedures taken to reach a final origin-destination matrix with demand levels similar to those used in the previous study of the SMART Corridor.

#### 7.3.1 Initial Origin-Destination Matrix Generation

As mentioned in Chapter 4, **CONTRAM** requires the user to input an origin-destination matrix. For this particular application there was not detailed enough origin-destination information available as mentioned in Chapter 5. Although the City of Los Angeles did provide origin-destination information for the vicinity in and around the SMART Corridor, due to the coarse nature of the data and the time and resource considerations, it was decided that the best option was to create a fictitious origin-destination matrix based on traffic counts provided in the previous study and then apply the COMEST program to reach a realistic representation of the demand throughout the corridor.

The first step in creating the fictitious origin-destination matrix was to determine where origins and destinations were to be located. The decision was made to create external origins and destinations as shown in Figure 7.3. This decision was made primarily because information regarding the total number of vehicles entering and exiting each newly created external origin-destination link was readily available for the time period from **7:00** a.m. to 8:00 a.m. No internal origins and destinations were created since the primary sinks and sources within the corridor were not well understood, and they were considered to be less important than the external sinks and sources.

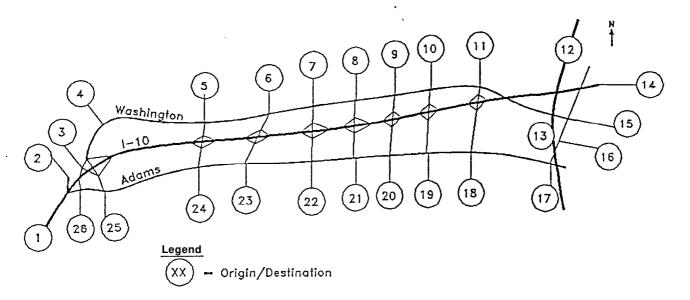
Once the locations of the origins and destinations were decided, the total number of vehicles entering and exiting each link for the time period from 7:00 a.m. to 8:00 a.m. were entered into a spreadsheet as shown in Figure 7.4. Once the row and column sums of the matrix were fixed, the next step was to balance the entries in the matrix. This step was done mostly by trial and error with the assistance of the graph shown in Figure 7.5. The objective of the fictitious origin-destination matrix was to help lead the COMEST program in the proper direction through the use of the observed link counts. A final fictitious matrix was chosen and a **CONTRAM** run was made. The **CONTRAM** run provided the COMEST program with the necessary packet route file and an original origin destination matrix from which to work.

#### 7.3.2 Use of the COMEST Program

The second step in the corridor demand analysis was to create an "observed traffic count" file from the data provided in the Al-Deek, Martello, Sanders and May study [3] on TRANSYT and FREQ runs for the time period from 7:00 a.m. to 8:00 a.m. For the initial application of COMEST every link in the network was input to the observed traffic count file. After many iterations of COMEST and CONTRAM it was discovered that there were too many links for COMEST to balance the traffic counts. The demand

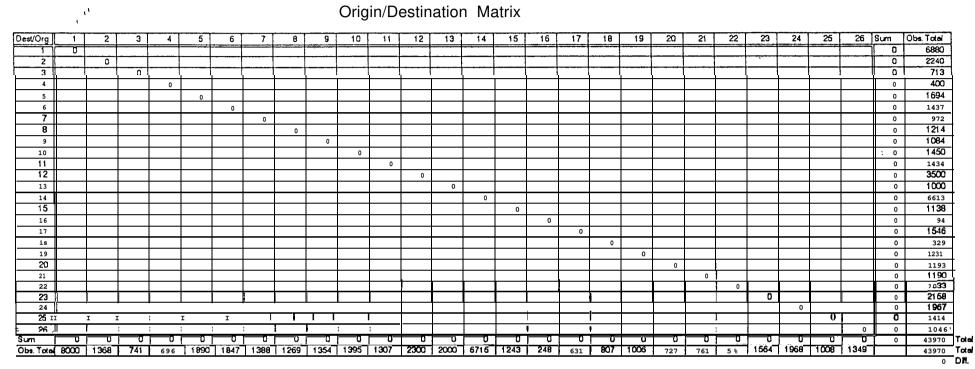
#### FIGURE 7.3

## Location of Origins and Destinations



#### FIGURE 7.4

Origin/Destination Matrix



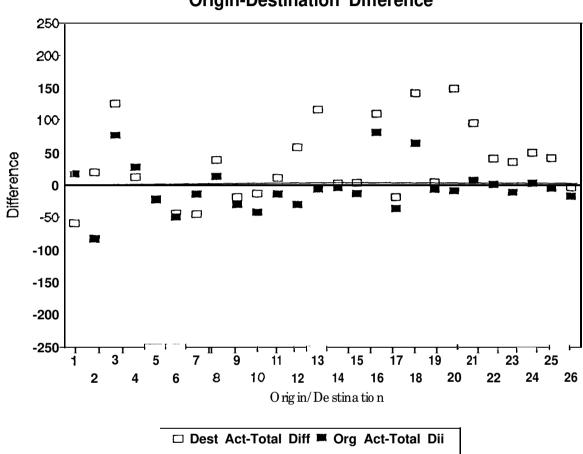


FIGURE 7.5 Origin-Destination Difference

pattern created by COMEST. was not very realistic due to the coarse nature of the original "fictitious" origin-destination information.

To achieve a demand pattern representative of those provided by reference [3], the best results were provided by COMEST when the only observed link counts input were those counts on the eastbound freeway and the corresponding ramp junctions. The relationship between CONTRAM and COMEST as explained in 'Chapter 4 was next used to generate a final origin-destination matrix. Four CONTRAM-COMEST iterations were conducted to obtain the final demand pattern for the 7:00 a.m. to 8:00 a.m. time period.

#### 7.3.3 Final Origin-Destination Matrix

Once the demand pattern provided by the COMEST runs was satisfactory for the 7:00 a.m. to 8:00 a.m. time period, the next step in the process was to develop origin-destination information for the eight **30**-minute time slices from 6:00 a.m. to 10:00 a.m. Based on information provided by the previous study [3] and information regarding the performance of the system, the demand was manipulated to create an origin-destination matrix for the eight time slices. Table 7.1 displays the time slices and corresponding level of demand factors.

Time Slice	Demand Factor
6:00 - 6:30	30 %
6:30 - 7:00	80 %
7:00 - 7:30	100 %
7:30 - 8:00	100 %
8:00 - 8:30	80 %
8:30 - 9:00	60 %
9:00 - 9:30	40 %
9:30 - 10:00	30 %

Table 7.1 Corresponding Time Slice Demands

Once the demand factors were applied, a final origin-destination matrix was completed. The resulting sums from each origin and destination per time slice are shown in Figure 7.6. This matrix was then used as the demand information for the base **CONTRAM** run.

#### 7.4 Base Run Validation

Three key areas were examined **to** validate the model's representation of the Smart Corridor. The first area was that of route choice and travel times/speeds. The second area of concern was that of bottleneck location on the freeway and the corresponding queuing pattern. The final validation process was in the overall network statistics. The following paragraphs describe the three major steps taken in the base run reference assignment validation.

#### 7.4.1 Travel Times/Route Choice

A critical element to the successful modelling of the Smart Corridor is to achieve an equilibrium assignment whereby the travel times via different routes between various sets of origins and destinations are not significantly different. If the travel times differ by a large magnitude then not much diversion will be seen even with a very severe incident. From the work described in Chapter 6, it was recognized that the freeway travel times were slightly lower than real life due to the fact that the speeds within the congested portions of the network are too high. With that in mind, travel time comparisons were made between a route on each parallel arterial only and a route on the freeway only. Figure 7.7 shows the travel time comparisons from Origin 1 to Destination 14, which is a freeway Origin to a freeway Destination. The travel times on the parallel arterials (Adams and Washington) include times on the freeway at the beginning and end of the route as well as the times taken to enter and exit the freeway. Thus, a second comparison was drawn and is shown in Figure 7.8. This comparison is made from freeway link 11 to link 29, which represents the length of Adams and Washington from Fairfax to Hoover. As seen in the figure, travel times on the arterial are much closer to that of the freeway in the heaviest demand time slices. As the demand decreases the difference in travel times increases.

The second key element of travel time/speed is that of route choice. This was done primarily through the use of UFPASC (User Friendly Post Analysis System for CONTRAM) program. The UFPASC is an interactive program for examining the outputs from CONTRAM runs. The UFPASC produces tabular and graphical outputs for selected parameters from the results file produced by CONTRAM. UFPASC uses a menu system to set up the analysis stages for producing the selected outputs. UFPASC allows selective investigations of the results file produced by CONTRAM.

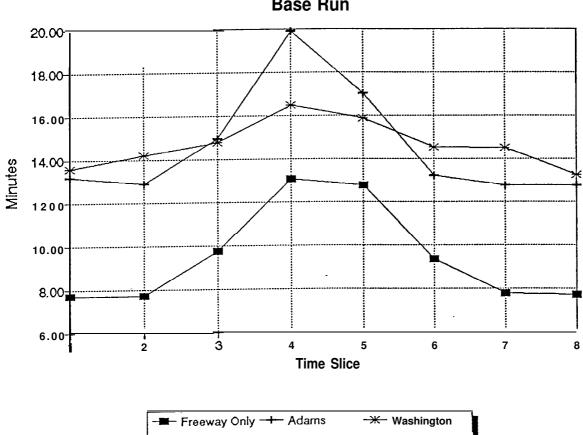
#### FIGURE 7.6 FINAL DEMAND INFORMATION

#### OTOTAL VEHICLE FLOW R A T E S FROM E A C H ORIGIN DURING EACH TIME SLICE (VEH/N)

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	9014 9013 9012 9017 9018 9019 9020 9021 9022 9023 9024 9025 9015 9011 9010 9009 9009 9008 9007 9008 9007 9006 9005 9004 9003 9004	1777 523 1143 132 69 37 46 98 18 206 121 45 148 174 553 251 a2 230 77 314 419 327 401	4715 1387 3038 355 184 108 140 256 51 578 314 130 390 45a 1471 656 223 615 216 824 1112 aao 1068	5 8 7 4 1727 3791 450 224 128 172 321 60 686 394 159 490 575 1830 818 274 772 265 1028 1380 1095 1332	5874 1727 3791 450 224 128 172 321 60 724 39: 159 490 575 1830 818 274 772 265 1028 1380 1095 1332	4715 1387 3038 355 184 108 140 256 51 578 314 130 390 458 1471 656 223 615 216 a24 1112 880 1068	3523 1030 <b>2272</b> 267 138 74 106 1a9 32 <b>406</b> 237 97 293 346 1102 <b>490</b> 161 615 62 161 615 627 659 <b>801</b>	2350 - 693 1522 1777 86 47 64 130 25 291 - 156 59 200 234 738 327 108 310 103 415 550 439 535	1777 523 1143 132 69 37 46 58 18 206 121 45 148 174 553 251 82 230 77 314 418 333 407	0 a 0 0 0 0 0 0 0 0 0 0 0 0 0
OTOTAL VEHICLEFLOWRATESENTERING THE NETWORK DURING EACH TIME SLICE (VEN/N)	9014 9013 9012 9017 9018 9019 9020 9021 9022 9023 9024 9025 9015 9011 9010 9000 9009 9008 9007 9006 9005 9004 9003 9004 9003 9002 _ ~	1777 523 1143 132 69 37 46 98 18 206 121 45 148 174 553 251 a2 230 77 314 419 327 401 43	4715 1387 3038 355 184 108 140 256 51 578 314 130 390 45a 1471 656 223 615 216 824 1112 aao 1068 125	5 8 7 4 1727 3791 450 224 128 172 321 60 686 394 159 490 575 1830 818 274 772 265 1028 1380 1095 1332 154	5874 1727 3791 450 224 128 172 321 60 724 39: 159 490 575 1830 818 274 772 265 1028 1380 1095 1332 154	4715 1387 3038 355 184 108 140 256 51 578 314 130 390 458 1471 656 223 615 216 a24 1112 880 1068 125	3523 1030 <b>2272</b> 267 138 74 106 1a9 32 <b>406</b> 237 97 293 346 1102 <b>490</b> 163 462 161 615 a27 659 <b>801</b> 90	2350 693 1522 177 86 47 64 130 25 291 156 59 200 234 738 327 108 310 103 415 550 439 535 59	1777 523 1143 132 69 37 46 58 18 206 121 45 148 174 553 251 82 230 77 314 418 333 407 43	0 a 0 0 0 0 0 0 0 0 0 0 0 0 0
	9014 9013 9012 9017 9018 9019 9020 9021 9022 9023 9024 9025 9015 9011 9010 9009 9008 9007 9006 9005 9006 9005 9004 9003 9002	1777 523 1143 132 69 37 46 98 18 206 121 45 148 174 553 251 a2 230 77 314 419 327 401 43 33	4715 1387 3038 355 184 108 140 256 51 578 314 130 390 45a 1471 656 223 615 216 824 1112 aao 1068 125 94	5 8 7 4 1727 3791 450 224 128 172 321 60 686 394 159 490 575 1830 818 274 772 265 1028 1380 1095 1332 154 114	5874 1727 3791 450 224 128 172 321 60 724 39: 159 490 575 1830 818 274 772 265 1320 1095 1332 154 114	4715 1387 3038 355 184 108 140 256 51 578 314 130 390 458 1471 656 223 615 216 a24 1112 880 1068 125 94	3523 1030 <b>2272</b> 267 138 74 106 1a9 32 <b>406</b> 237 97 293 346 1102 <b>490</b> 163 462 161 615 a27 659 <b>801</b> 90 <b>65</b>	2350 693 1522 1777 86 47 64 130 25 291 156 59 200 234 738 327 108 310 103 415 550 439 535 59 45	1777 523 1143 132 69 37 46 58 18 206 121 45 148 174 553 251 82 230 77 314 418 333 407 43	0 a 0 0 0 0 0 0 0 0 0 0 0 0 0

 10251	27315	34026	34026	27315	20359	13620	10262	0



### Travel Times from Org. 1 to Dest. 14 Base Run

FIGURE 7.7

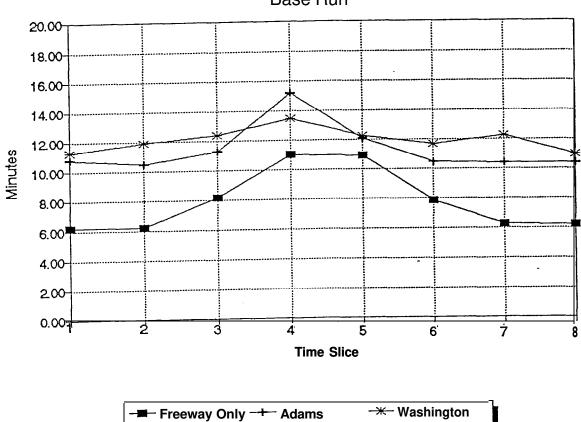


FIGURE 7.8 Equal Distance Travel Times Base Run Thus, by using UFPASC a number of origin destination pairs were chosen and evaluated. An example of such an output is shown in Figure 7.9. As seen in the figure, the route chosen by most is that of the freeway. The average speeds and travel times shown in the figure represent averages over all time slices. The routes chosen from origin to destination were also examined to make sure they were reasonable.

#### 7.4.2 Bottleneck Location/Queuing Pattern

A key validation measure was that of freeway bottleneck location and queue length. Bottlenecks were identified in subsections 14 and 29 which match the work reported in Chapter 6. While the bottlenecks were identified in the same subsections as before, the queuing pattern was not exactly the same. Since the demand pattern is much more complex, it was not possible to achieve the same queuing pattern as before. However, the pattern as shown in Figure 7.10 does closely match that of the work described in Chapter 6. The main difference between the previous freeway-only work and the corridor base simulation run is that the queues do not back up as far from subsection 29 as before. In the freeway-only work, the queues from subsections 14 and 29 collided. In the base reference assignment, the queuing is not as severe as that described in Chapter 6 where the freeway only is modelled. However, because the bottlenecks were properly identified and the demand patterns were reasonable it was felt that existing queuing pattern shown in Figure 7.10 was acceptable to continue with the experiment. Therefore, it was concluded that comparisons made to the base reference assignments would be acceptable for analysis.

#### 7.4.3 Overall Corridor Wide Summary Information

From a system-wide perspective, the amount of free moving delay compared to the amount of flow delay and delay caused by queuing was examined for its reasonableness. The total distance travelled, the overall network speed, and the total final queues were all examined for reasonableness. Table 7.2 presents the overall network summary information for the base reference corridor assignment. As seen in the table, the overall network speed is approximately 30 miles per hour which is in a reasonable range. The total freemoving time as compared to the delay due to queuing is also in a reasonable range. Appendix E contains a condensed input and output of the base reference assignment.

#### FIGURE 7.9 UFPASC EXAMPLE OUTPUT

.

ROUTE INFORMATION \*\*\*\* Origin 5001 and Destination 9015 TABLE OF ROUTES Route Links on Route \*\*\*\*> No. 1 7 **8** 9 10 11 12 13 14 **15 16** --, --> 17 18 19 20 21 22 23 24 25 26 --> --> 27 1205 1001 909 205 10 11 12 13 14 15 **16** --> 2 7 8 9 21 22 23 2205 2101 2009 --> --> 17 18 19 20 205 ···> 1505 905 10 37**8**9 11 12 13 14 15 **16 -->** --> 17 18 20 21 2705 2601 2501 2005 1505 --> 19 --> 905 205 4 7 5305 4905 4801 4701 4603 7605 4105 3505 3005 --> --> .2505 2005 1505 905 -205 --> 5 7 **8** 9 10 4805 4601 7605 4105 3505 3005 --> --> 2505 2005 1505 905 205 -->

TABLE OF FLOWS (Vehicles)

Route	Veh.	Time	Interva	ls											TOTAL	ROUTE	OVERALL (	OVERALL
NO.	Type	1	2	3	4	5	6	7	8	9	10	11	12	13	FLOW	DIST.	AVE. JOU.	AVE.
															(VEH)	(H)	TIME	SPEED
1	с	22	59	74	38	19	44	30	22	0	0	0	0	0	308	10532	646	57.6
2	с	0	0	0	14	15	0	0	0	0	0	0	0	0	29	13390	836	57.6
3	С	0	0	0	8	0		0	0	0	0	0	0	٥	8	12226	846	50.4
4	с	0	0	0	14	0	0	0	0	0	0	0	0	0	14	11951	1010	39.6
5	С	0	0	0	0	15	0	0	0	0	0	0	0	0	15	12169	843	50.4
тоти		22	59	74	74	49	44	30	22	0	0	0	0	0				
0	0	C	) 0															

---

#### FIGURE 7.10 QUEUING PA'ITERN - REFERENCE BASE ASSIGNMENT

LINK-BY-LINK ALL-TIME-SLICES - MEAN FINAL QUEUES (VEH)

SHART CORRIDOR BASE RUN NETWORK and TIME DATA (6/11/91) SHART CORRIDOR BASE DEMAND SHART CORRIDOR COHTROL DATA

	TIME	SLICES	:								ITERATION ROOD	· ·
LINK	1	2	3	4	5	6	7	,	8	9		
NO.&											тот	AL
TYPE											FINAL QUE	UES
	600	630	700	730 8	800 8	330	900	93	30 1000	1300		
7U	.0	.0	.0	.0	.0	.0		0	.0	.0	.0	
au	.0	.0	68.0	334.0	.0	.0	-	0	.0	.0	402.0	
90	.0	.0	87.OF	94.OF	20.0	.0		0	.0	.0	201.0	
100	.0	.0	46.OF	44.0F	74.OF	.0		0	.0	.0	164.0	
110	.0	.0	110.OF	122.OF	126.OF	.0	-	0	.0	.0	358.0	
120	.0	.0	122.OF	137.OF	156.OF	.0		0	.0	.0	415.0	
13u	.0	.0	275.OF	257.OF	251.OF	.0		0	.0	.0	783.0	
14U	.0	.0	37.OF	76.OF	39.OF	.0		0	.0	.0	152.0	
15u	.0	.0	.0	.0	.0	.0	•	0	.0	.0	.0	
160	.0	.0	.0	.0	-0	.0	-	0	.0	.0	.0	
170	.0	.0	.0	.0	.0	.0		0	-0	.0	.0	
180	.0	.0	.0	.0	.0	.0	-	0	.0	.0	.0	
190	.0	.0	.0	.0	.0	.0	-	0	.0	.0	.0	
200	.0	.0	.0	.0	.0	.0	•	0	.0	.0	.0	
210	.0	.0	53.0	.0	52.0	.0		0	.0	.0	105.0	
220	.0	.0	.0	143.0	199.OF	.0		0	_0	.0	342.0	
23U	.0	.0	.0	120.0F	112.OF	.0	•	0	.0	.0	232.0	
240	.0	.0	14.0	121.OF	140.0F	.0		0	.0	.0	275.0	
250	.0	.0	103.OF	144.OF	137.OF	.0		0	.0	.0	384.0	
260	.0	.0	214.OF	201.0F	193.OF	.0		0	.0	-0	608.0	
270	.0	.0	67.OF	66.0F	103.OF	71.0F	•	0	.0	-0	307.0	
280	.0	.0	154.OF	147.OF	126.OF	120.05		0	.0	.0	547.0	
29U	.0	.0	.0	.0	.0	.0		0	.0	.0	.0	
300	.0	.0	.0	.0	.0	.0		0	.0	.0	.0	
31u	.0	.0	.0	.0	.0	.0		0	.0	-0	.0	
32u	.0	.0	.0	.0	-0	.0		0	.0	.0	.0	
500	.0	.0	.0	.0	.0	.0		0	.0	.0	.0	
51u	.0	.0	.0	.0	.0	.0	•	0	-0	.0	.0	

---

1

RUN ON 11/ 6/91

ITERATION NUMBER 3

#### TABLE 7.2 BASE REFERENCE ASSIGNMENT SUMMARY INFORMATION

	SUMMARY INFORMATION	CONTRAM 5.14 (16. 4.91)	RUN ON 11/6/91
SMART CORR'IDOR BASE RUN NETWORK AND TIME DATA	(6/11/91)		
SMART CORRIDOR BASE DEMAND			
SMART CORRIDOR CONTROL DATA			
			ITERATION NUMBER 3
TIME SLICES :			
1 2 3 4	5 6 7 a	9	
600 630 700 730 800	a30 900 930 100	o <b>1300</b>	
			TOTALS
0 JOURNEY-TIME (VEH-H)			
OFREEMOVING 456.8 1222.2 1560.4 1650.4 1 FLOW DELAY .0 .0 .0 .0	.0 .0 .0 .0 .0	43.1 .0	8747.3
	.0 .0 .0 .0	1.2	0.
	639.5 1564.4 765.8 557.5	44.3	3612.9 12360.1
			12360.1
0 DISTANCE TRAVELLED (VEH-KM)			
0 36981.5 98906.8 123665. 127436. 11	5655. 88215.8 56937.3 42310.3	3703.4	693810.9
0 OVERALL NETUORK SPEED (KM/H)			
0 75.4 72.6 58.8 45.0	43.8 56.4 74.4 75.9	83.6	56.1
0 TOTAL FINAL QUEUES (VEH)			
0 69.2 354.4 3425.9 5910.4 4	720.9 832.2 109.3 76.7	.0	15499.0
0			
0 FUEL CONSUMPTION (LITRES)			
OTRAVELLING 3952.4 10530.7 13255.3 13395.8 12:	199.2 9563.2 6140.1 4530.5	408.9	73976.0
QUEUEING 14.3 144.8 702.3 1573.5 1		_0	4627.1
TOTAL 3966.7 10675.5 13957.6 14969.3 13		408.9	78603.1
0 TOTAL LINK COUNTS (VEH)			
OARRIVALS 78446 208733 257975 259595 23	34424 185418 121677 90337	8483	1445088
PCU FACTOR 1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00	1.00	1.00
	66095 36199 <b>10008</b> 6701	247	291152
<b>%</b> STOPPED 7.7 a.3 27.4 29.9	28.2 19.5 8.2 7.4	2.9	20.1
OPACKET SIZE WITHIN EACH O-D MOVEMENT IS VARIA		ROUTE MEMORY:	
TOTAL NUMBER OF PACKETS ENTERING THE NETWORK	12735 MEAN LINKS 88529 WORDS AVAIL		7000/77 .
TOTAL NUMBER OF VEHICLES	88529 WORDS AVAI 88529 USED PER I	••••••	3808437)
TOTAL NUMBER OF PCUS MEAN PCU FACTOR	1.00 CODONS PER		
MARY FOU FROIDE	1.00 COUND PER	10	

#### 8.0 INCIDENT MODELLING

The purpose of this chapter is to describe the techniques applied within the **CONTRAM** model and to report the results of modelling an incident on the freeway. The incidents modelled, the techniques applied within **CONTRAM**, and the results of the efforts are discussed within this chapter. The modelling of an incident on the freeway in conjunction with the modelling of in-vehicle information systems illustrates the benefits to both the equipped vehicles and non-equipped vehicles as well as system-wide results which will be reported in Chapters 9 and 10.

#### 8.1 Incident Scenario

Two likely incident scenarios were created to evaluate the potential benefits of in-vehicle information systems. The key elements which comprise the modelling of an incident are:

- 1) location;
- 2) severity;
- 3) duration.

#### 8.1.1 Location

To determine an appropriate location for an incident, the first consideration used was whether or not the location of the incident caused the freeway congestion to back up out of the initial boundary of the freeway or extend beyond the last time slice. If the congestion were to back out of the **first** subsection on the freeway, the results would be inaccurate as the number of vehicles in the system would not be comparable across different simulation runs.

The second key consideration was to locate an incident in a subsection in such a manner as to cause a congestion pattern quite different from the normal congestion pattern. Thus, the subsections more towards the middle of the freeway section were given consideration as the location of an incident. Two different locations for two separate incident run scenarios were chosen to simulate. The first incident was located in subsection 20. The second run was made with an incident in subsection 22.

#### 8.1.2 Incident Severity and Duration

Many different types of incidents can occur on a freeway section. An incident on the freeway typically reduces the capacity of the subsection where the incident occurred. This capacity reduction can be at various levels and extend over time in different patterns. The following paragraphs describe the two separate incidents modelled.

#### 8.1.2.1 Slight Incident

The first incident (hereafter referred to as the slight incident scenario), was modelled as occurring in subsection 20. The incident began in time slice 4 and reduced the capacity from 10900 vph to 7500 vph for the 30 minutes in time slice 4. The incident was modelled to last into time slice 5. During time slice 5, the capacity was reduced from 10900 vph to 8500 vph. This incident is the equivalent of having approximately one and a half lanes blocked in time slice 4, while in time slice 5, one-half lane is reopened.

#### 8.1.2.2 Severe Incident

The second incident (hereafter referred to as the severe incident), was modelled as occurring in subsection 22. The incident began in time slice 3 and reduced the capacity from 12100 vph to 6900 vph for the one hour in time slices 3 and 4. This incident is the equivalent of having approximately two and a half lanes blocked.

#### 8.2 Incident Modelling Within CONTRAM

The following sections outline the methodology and results of the slight and severe incident simulation runs. Along with results, conclusions are presented at the end of the chapter.

#### 8.2.1 Methodology

The following procedures were used to model an incident within **CONTRAM**. The first step in the process was to make a base run in **CONTRAM** with the capacity reduced in the subsection where the incident has occurred. This was accomplished through the use of Card Type 12. Card Type 12 allows the user to override any capacities calculated by **CONTRAM** except smaller reduced capacities arising

from blocking back. The. link number is entered followed by the capacity of the link in each corresponding time slice.

A three-step process is conducted to model an incident within **CONTRAM**. The first step in the process is to make a base run (described in Chapter 7), whereby all drivers have 100 percent information and are taking their shortest routes. The second step involves the use of **RODIN** as described in Chapter 4. A **RODIN** run is conducted with <u>no</u> vehicles having information systems thereby being set to their fixed routes. The final step in the process is to make another **CONTRAM** run with the new network where the capacity of the subsection is reduced through the use of Card Type 12.

#### 8.2.2 Results

Figure 8.1 presents the output queuing pattern on the eastbound Santa Monica for the slight incident scenario and the base run (described in Chapter 7). Based on a comparison of Figures 7.10 and 8.1 it can be concluded that the slight incident scenario does not change the queuing pattern substantially. It should also be noted that there is little increase in the amount of congestion as a result of the incident. Table 8.1 presents the network wide summary information for the slight incident as well.

Figure 8.2 presents the output queuing pattern on the eastbound Santa Monica for the severe incident and the base run. As a result of the incident, the more queuing occurs and the pattern changes. There is a significant increase in the amount of congestion as a result of the incident. Table 8.2 presents the network-wide summary information for severe incident as well.

As a result of the incident runs, questions began to arise as to both the severity and duration of the congestion as predicted by **CONTRAM** in both incident situations. Therefore, a FREQ analysis was conducted to compare the queuing pattern projected by FREQ to that provided by **CONTRAM**. Figure 8.3 presents the queuing pattern for both the slight and severe incident as predicted by FREQ. As seen in the figure, the congestion predicted by **CONTRAM** is not nearly as severe or as long lasting as that of FREQ.

Due to time constraints, a thorough investigation as to why the discrepancies occurred could not be conducted. Thus, it was concluded that despite the fact that congestion was much less severe in **CONTRAM** than as predicted by FREQ, an analysis would be conducted using the severe incident scenario since, as a result of the incident, there was a change in the queuing pattern and an increase in the amount of congestion on the freeway. This deficiency in **CONTRAM** will be discussed later. Since the slight incident scenario did not result in much change in the queuing pattern on the freeway and not

#### FIGURE 8.1 **QUEUING PATTERN - SLIGHT INCIDENT** (EB SANTA MONICA)

#### LINK-BY-LINK ALL-TIME-SLICES - MEAN FINAL QUEUES (VEH)

SMART CORRIDOR INCIDENT RUN NETWORK and TIME DATA (6/10/91) SMART CORRIDOR BASE D EMAND (0 % guided) SMART CORRIDOR CONTROL DATA

• • •

1

TYPE         600         630         700         730         800         830         900         930         1000         1300           7U         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0         .0	
TYPE       FINAL OF         600       630       700       730       800       830       900       930       1000       1300         7U       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0 <th></th>	
600 $630$ $700$ $730$ $800$ $830$ $900$ $930$ $1000$ $1300$ $7U$ .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0 <th< td=""><td>TAL</td></th<>	TAL
7U.0.0.0.0.0.0.0.0.0 $8U$ .0.0191.0668.094.0.0.0.0.0.0 $9U$ .0.0.55.0F35.0F67.0F.0.0.0.0.0 $10U$ .0.055.0F35.0F67.0F.0.0.0.0.0 $10U$ .0.065.0F42.0F37.0F.0.0.0.0.0 $11U$ .0.0103.0F136.0F131.0F.0.0.0.0.0 $12U$ .0.0151.0F136.0F148.0F.0.0.0.0.0 $13u$ .0.0276.0F260.0F250.0F.0.0.0.0.0 $14u$ .0.0.035.0F47.0F.0.0.0.0.0 $15U$ .0.0.0.0.0.0.0.0.0 $15U$ .0.0.0.0.0.0.0.0.0 $15U$ .0.0.0.0.0.0.0.0.0 $16U$ .0.0.0.0.0.0.0.0.0 $16U$ .0.0.0.0.0.0.0.0.0 $16U$ .0.0.0.0.0.0.0.0.0 $17U$ .0.0	UEUES
8U       .0       .0       191.0       668.0       94.0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0 <td></td>	
9U       .0       .0 $55.0F$ $35.0F$ $67.0F$ .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0 <td< td=""><td>0</td></td<>	0
10U       .0       .0 $65.0F$ $42.0F$ $37.0F$ .0       .0       .0       144 $11U$ .0       .0 $103.0F$ $136.0F$ $131.0F$ .0       .0       .0       .0 $12U$ .0       .0 $151.0F$ $136.0F$ $148.0F$ .0       .0       .0       .0 $12U$ .0       .0 $151.0F$ $136.0F$ $148.0F$ .0       .0       .0       .0 $13u$ .0       .0 $276.0F$ $260.0F$ $250.0F$ .0       .0       .0       .0       .0 $14U$ .0       .0 $276.0F$ $260.0F$ $250.0F$ .0       .0       .0       .0 $15U$ .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0	0
110       .0       .0       103.0F       136.0F       131.0F       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0 </td <td>0</td>	0
12U       .0       .0       151.0F       136.0F       148.0F       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0 </td <td>0</td>	0
13u       .0       .0       276.0F       260.0F       250.0F       .0       .0       .0       .0       786.         14U       .0       .0       .0       .0       .0       .0       .0       .0       136.         15U       .0       .0       .0       .0       .0       .0       .0       136.         15U       .0       .0       .0       .0       .0       .0       .0       136.         15U       .0       .0       .0       .0       .0       .0       .0       .0         16U       .0       .0       1.0       105.0F       105.0F       .0       .0       .0       .0         16U       .0       .0       10       105.0F       105.0F       .0       .0       .0       .0       .0         17U       .0       .0       .0       160.0F       160.0F       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0	0
14U       .0       .0       44.0F       37.0F       55.0F       .0       .0       .0       .0       136.         15U       .0       .0       .0       .0       .0       .0       .0       136.         15U       .0       .0       .0       .0       .0       .0       .0       .0         16U       .0       .0       105.0F       105.0F       .0       .0       .0       .0         17U       .0       .0       .0       160.0F       160.0F       .0       .0       .0       .0         18U       .0       .0       .0       195.0F       168.0F       .0       .0       .0       .0       .0         18U       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0         19U       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0       .	0
15U       .0       .0       .0       35.0F       47.0F       .0       .0       .0       .82.         16U       .0       .0       1.0       105.0F       105.0F       .0       .0       .0       211.         17U       .0       .0       .0       160.0F       160.0F       .0       .0       .0       220.         18U       .0       .0       .0       195.0F       168.0F       .0       .0       .0       363.         19U       .0       .0       .0       .0       .0       .0       .0       .0       .0         19U       .0       .0       .0       .0       .0       .0       .0       .0       .0       .0	0
16U       .0       .0       105.0F       105.0F       .0       .0       .0       211.         17U       .0       .0       .0       160.0F       160.0F       .0       .0       .0       320.         18U       .0       .0       .0       195.0F       168.0F       .0       .0       .0       363.         19U       .0       .0       .0       .0       .0       .0       .0       499.	0
16U       .0       .0       105.0F       105.0F       .0       .0       .0       211.         17U       .0       .0       160.0F       160.0F       .0       .0       .0       320.         18U       .0       .0       195.0F       168.0F       .0       .0       .0       363.         19U       .0       .0       .0       .0       .0       .0       .0       499.	
18U       .0       .0       195.0F       168.0F       .0       .0       .0       363.         19U       .0       .0       .0       .0       .0       .0       .0       .0         18U       .0       .0       .0       .0       .0       .0       .0       .0         19U       .0       .0       .0       .0       .0       .0       .0       .0         19U       .0       .0       .0       .0       .0       .0       .0       .0	
19U .0 .0 255.0F 244.0F .0 .0 .0 .0 499.	0
	0
	0
200 .0 .0 .22.0F 115.0F .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0	0
21U .o .o .0 .o .o .o .o .o	
22u _0 .0 .0 .0 28.0 .0 .0 .0 .0 .0 28.0 .0 .0 28.0	
23U .0 .0 .0 82.0 108.0F .0 .0 .0 .0 .0 190.	
24U .0 .0 5.0 121.0F 145.0F .0 .0 .0 .0 .0 271.	
250 .0 .0 99.0F 109.0F 120.0F .0 .0 .0 .0 .0 328.	
26U .0 .0 184.0F 183.0F 182.0F 111.0 .0 .0 .0 .0 660.	
27-U .0 99.0F 63.0F 107.0F 66.0F .0 .0 .0 335.	
28U .0 .0 120.0F 121.0F 160.0F 122.0F .0 .0 .0 523.	
	0
	0
	0
	ů O
	0
	0

ITERATION NUMBER 3

RUN ON 10/ 6/91

#### FIGURE 8.2 QUEUING **PATTERN - SEVERE INCIDENT** (EB SANTA MONICA)

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#### LINK-BY-LINK ALL-TIME-SLICES - MEAN FINAL QUEUES (VEH)

RUN ON 8/6/91

ITERATION NUMBER 3

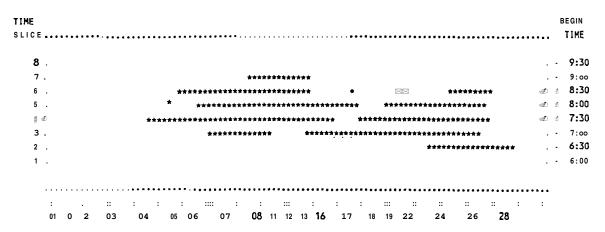
SMART CORRIDOR INCIDENT RUN NETWORK and TIME DATA (6/8/91) SMARI CORRIDOR INCIDENT RUN NETWORK and TIME DATA (6/8/91) SMART CORRIDOR CONTROL DATA

		TIME	SLICES	:								
LINK		1	2	3	4	5	6		7	8	9	
NO.8												TOTAL
TYPE												FINAL QUEUES
	600	6	30	700	730	800	830	900	930	1000	1300	
7u		.0	.0	.0	.0	.0	.0		_0	.0	.0	.0
8U		.0	.0	502.0	1803.0	1308.0	398.0		.0	.0	.0	4011.0
9u		.0	.0	44.OF	61.0F	43.0F	38.OF		.0	.0	.0	186.0
100		.0	.0	42.0F	35.OF	62.0F	37.OF		.0	.0	.0	176.0
110		.0	.0	107.OF	105.OF	103.0F	117.OF		.0	.0	.0	432.0
120		.0	.0	121.OF	125.OF	121.OF	120.OF		_0	.0	.0	487.0
13u		.0	.0	273.OF	250.0F	259.0F	250.0F		.0	.0	.0	1032.0
14u		.0	.0	37.OF	37.OF	64.OF	45.OF		.0	.0	.0	183.0
150		.0	.0	39.0F	51.0F	28.OF	.0		.0	.0	.0	118.0
160		.0	.0	123.OF	97.OF	94.0F	.0		.0	.0	.0	314.0
17U		.0	.0	177.OF	166.OF	43.0	.0		.0	.0	.0	386.0
18U		.0	.0	173.OF	195.OF	176.OF	.0		.0	.0	.0	544.0
19U		.0	.0	286.OF	254.OF	264.0~	148.0		.0	.0	.0	952.0
2ou		.0	.0	96.0F	87.0F	103.0F	94.0F		.0	.0	.0	380.0
210		.0	.0	108.0F	117.OF	91.OF	99.OF		.0	.0	.0	415.0
22u		.0	.0	200.0F	232.0F	_0	36.0		.0	.0	.0	468.0
23U		.0	.0	.0	.0	.0	129.OF		.0	.0	.0	129.0
230 24U		.0	.0	.0	.0	71.0	130.OF		.0	.0	.0	201.0
25U		.0	.0	.0	.0	94.OF	98.OF		.0	.0	.0	192.0
260		.0	.0	.0	.0	186.OF	182.OF		.0	.0	.0	368.0
270		.0	.0	.0	.0	62.0F	66.0F		.0	.0	.0	128.0
280		.0	.0	.0	.0	120.0F	137.OF		.0	.0	.0	257.0
290		.0	.0	.0	.0	.0	.0		.0	.0	.0	.0
3ou		.0	.0	.0	.0	.0	.0		.0	.0	.0	.0
31U		.0	.0	.0	.0	.0	.0		.0	.0	.0	.0
320		.0	.0	.0	.0	.0	.0		.0	.0	.0	.0
50U		.0	.0	.0	.0	-0	.0		.0	.0	.0	
510		.0	.0	.0	.0	.0	.0		.0	.0	.0	.0 •0
210		.0	.0	-0	.0					.0	.0	.0

#### FIGURE 8.3 QUEUING PATTERN - SLIGHT AND SEVERE INC. (FREQ)

CONTOUR DIAGRAM OF QUEUE LENGTH BEFORE ENTRY CONTROL

#### SLIGHT INCIDENT



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BLANK DENOTES MOVING TRAFFIC. ASTERISK DENOTES PUEUEO VEHICLES DUE TO MAINLINE CONGESTION. M DENOTES QUEUED VEHICLES DUE TO MERGING. B DENOTES PUEUEO VEHICLES DUE TO MAINLINE CONGESTION AND MERGING. (WHEN BOTH QUEUES EXIST, LENGTH OF DISPLAY REPRESENTS MAINLINE CONGESTION.)

CONTOUR DIAGRAM OF QUEUE LENGTH BEFORE ENTRY CONTROL

#### SEVERE INCIDENT

TIME		BEGIN
SLICE	*****	TIME
	•	•
8	*	9:30
7	*****	9:00
6	***************************************	8:30
5	***************************************	8:00
4	***************************************	7:30
3	*****	7:00
2	• *	6:30
1	•	6 : 0 0
		: :
	01 02 03 04 05 06 07 08 1 1 1 2 1 3 16 17 <b>18</b> 19 22 24 26 28	

BLANK DENOTES MOVING TRAFFIC. ASTERISK DENOTES QUEUED VEHICLES DUE TOMAINLINE CONGESTION. M DENOTES QUEUED VEHICLES DUE TO MERGING. B DENOTES QUEUED VEHICLES DUE TO MAINLINE CONGESTION AND MERGING. (WHEN BOTH QUEUES EXIST, LENGTH OF DISPLAY REPRESENTS MAINLINE CONGESTION.)

#### TABLE 8.1 SLIGHT INCIDENT ASSIGNMENT SUMMARY INFORMATION

1 SUMMARY INFORMATION CONTRAM 5.14 (16.4.91)	RUN ON 10/6/91
SMART CORRIDOR INCIDENT RUN <b>NETWORK and</b> TIME DATA <b>(6/10/91)</b> Smart corridor base demand <b>(0%</b> guided) SMART CORRIDOR CONTROL DATA	
TIME SLICES :	ITERATION NUMBER 3
1 2 3 4 5 6' <b>7</b> a 9	
600 630 700 730 800 a30 900 930 1000 1300	
	TOTALS
O JOURNEY-TINE (VEH-H)	
OFREEMOVING 456.9 1219.3 1565.1 1584.7 1447.5 1188.9 706.7 520.6 43.0 Flow delay <b>.0</b> .0 .0 .0 <b>.0</b> .0 .0 .0	8732.6
OUEUEING 33.9 153.9 610.1 1222.5 1324.3 562.4 84.9 36.8 1.1	.0 <b>4029 . 9</b>
TOTAL 490.8 1373.2 2175.3 2807.2 2771.0 1751.3 791.5 557.3 44.1	12762.5
0 DISTANCE TRAVELLED (VEH-KM)	
0 <b>36977.0</b> 98592.9 123565. 122527. 112795. 95287.0 57441.4 42351.5 3696.9	693233.3
0 OVERALL NETWORK SPEED (KM/H)	
0 75.3 71.a 56.8 43.6 40.7 54.4 72.6 76.0 83.8	54.3
0 TOTAL FINAL QUEUES(VEH)	
0 68.8 403.1 3301.3 7050.8 6403.4 1334.8 110.5 74.7 <b>.0</b>	18747.4
0	
0 FUEL CONSUMPTION(LITRES)	
OTRAVELLING 3951.3 10183.3 13110.4 12805.8 11975.5 10304.3 6191.4 4535.1 408.0	73764.9
QUEUEING 14.4 161.7 795.0 1624.2 1765.6 723.0 77.0 16.8 .0	5177.7
TOTAL 3965.6 10645.0 13905.4 14430.0 13741.1 11027.3 6268.4 4551.8 408.0	78942.7
0 TOTAL LINK COUNTS(VEH)	
OARRIVALS 78427 207885 257125 250230 230611 198248 122490 90386 8467	1443869
PCU FACTOR 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.0	1.00
STOPS 6052 17427 65667 70937 68376 45214 11000 6668 242	291582
X STOPPED 7.7 6.4 25.5 28.3 29.6 22.8 9.0 7.4 2.9	20.2
OPACKET SIZE WITHIN EACH O-D MOVEMENT IS VARIABLE ROUTES AND ROUTE MEMORY: TOTAL NUMBER OF PACKETS ENTERING THE NETWORK 12735 HEAR LINKS PER ROUTE 16.31	
TOTAL NUMBER OF PACKETS ENTERING THE NETWORK 12735 HEAR LINKS PER ROUTE 16.31 Total Number of Vehicles 88529 WORDS available 3806309 (CUT of	20012427
TOTAL NUMBER OF PCUS 88529 WORDS AVAILABLE 3806309 (COT OF TOTAL NUMBER OF PCUS 88529 USED PER ITERATION 1a.561	380`3437 )
MEAN PCU FACTOR 1.00 COOONS PER WORD 10	

#### TABLE 8.2 SEVERE INCIDENT ASSIGNMENT SUMMARY INFORMATION

• :-

SMART CORRIDOR INCIDENT RUN NETWORK and TIME DATA (6/8/91) SMART CORRIDOR INCIDENT RUN NETWORK and TIME DATA (6/8/91) SMART CORRIDOR CONTROL DATA ITERATION NUM B	
TIME SLICES :	нз
1 2 3 4 5 6 7 <b>8</b> 9	
600 630 700 730 800 830 900 930 1000 1300	
0 JOURNEY-TIME (VEH-H)	
OFREEMOVING 456.9 1219.3 1482.4 1475.7 1475.9 1256.6 001.8 521.1 43.0 0732.6	
FLOW DELAY .0 .0 .0 .0 .0 .0 .0 .0 .0 .0 .0	
QUEUEING 33.9 153.9 691.7 1715.0 2275.9 1342.8 202.5 44.0 1.1 6460.8	
TOTAL         490.8         1373.2         2174.0         3190.6         3751.8         2599.4         1004.3         565.1         44.2         15193.5	
0 DISTANCE TRAVELLED (VEH-KM)	
0 36977.0 98594.2 116480. 113567. 115141. 100840. 65549.4 42385.6 36W.0 693232.6	
000202.0	
0 OVERALL NETWORK SPEED (KM/H)	
0 75.3 71.a 53.6 35.6 30.7 <b>38.8</b> 65.3 75.0 83.7 45.6	
0 TOTAL FINAL QUEUES(VEH)	
0 68.8 403.1 4417.5 8404.4 7776.9 3594.7 174.6 76.1 .0 24916.1 0	
0 FUEL CONSUMPTION (LITRES)	
OTRAVELLING 3951.3 10486.2 12574.1 12003.8 12574.7 11162.2 7177.9 4539.2 408.2 74877.4	
PUEUEING 14.4 161.7 097.3 2281.5 3083.0 1808.7 235.5 26.1 .0 8508.1	
TOTAL         3965.6         10647.9         13471.3         14285.2         15657.7         12970.9         7413.4         4565.3         408.2         03385.5	
0 TOTAL LINK COUNTS (VEH)	
OARRIVALS 70427 207885 241592 230516 235125 210443 140889 90521 8471 1443869	
PCU FACTOR 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.0	
STOPS 6052 17427 57331 60150 84629 66404 15728 <b>6734</b> 243 314700	
X STOPPED 7.7 a.4 23.7 26.1 36.0 31.6 11.2 7.4 2.9 21.8	
OPACKET SIZE WITHIN EACH O-D MOVEMENT IS VARIABLE ROUTES AND ROUTE MEMORY:	
TOTAL NUMBER OF PACKETS ENTERING THE NETWORK 12735 MEAN LINKS PER ROUTE 15.31	
TOTAL NUMBER OF VEHICLES 88529 WORDS AVAILABLE 3806309 (OUT OF 3808437) TOTAL NUMBER OF PCUS 85529 USED PER ITERATION 18710	
MEAN PCU FACTOR 1.00 CODON'S PER WORD 10	
1 CONVERGENCE MONITOR - SUMMARIES OF JOURNEY-TINES. DISTANCES AND CHANGES-FORALLITERATIONS RUN ON 8/ 1	/91

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much increase in congestion, it was determined that the remaining analysis would focus on the results provided by the severe incident.

#### 9.0 SIMULATION RESULTS UNDER SEVERE INCIDENT SCENARIO

The purpose of this chapter is to describe the methodology and analysis results of the investigation into the benefits derived from in-vehicle information systems under the severe incident scenario. The first part of the chapter describes the methodology and techniques used to obtain results from the modelling process. The results are then broken down into both system-wide performance measures and benefits for both guided and unguided vehicles.

#### 9.1 Methodology: Modelling Guidance Systems in CONTRAM

In order to model guidance systems within the CONTRAM model the RODIN program as described in Chapter 4 was used. RODIN is external software program developed by Nick Taylor (TRRL) and is intended to simulate route guidance. This program converts a packet route file output produced by a standard CONTRAM into an origin-destination matrix and a set of routes which it embeds as fixed routes in a copy of the network file. The origin-destination movements are duplicated and each set is preceded by a percentage multiplying or split factor. The network and demand files are then rerun in RODIN. The first set of origins-destinations is assigned on the fixed routes (i.e. along the original routes, which are the minimum time path routes before the incident), while the second set is assigned to minimum cost routes. This provides a framework in which experiments involving two user classes (guided and unguided vehicles) can be performed.

RODIN is also designed to provide:

- a choice of methods for setting packet sizes;
- alternate vehicle class for the second set of 0-Ds;
- randomization of the output O-D counts.

An important point about this procedure is that the fixed and free routed trips are dynamically integrated so that each affects the routes of the others in an expected way.

Once a **RODIN** base run under the severe incident scenario with 0 percent equipped vehicles was complete, a series of **CONTRAM** runs with varying percentages of equipped vehicles was chosen to be evaluated under the severe incident scenario. The percentages of in-vehicle information equipped vehicles chosen for examination was 0, 10, 25, 50, 75, 90 and 100. It was felt that a range of 0 to 100 with five points in-between would identify where the benefits would be the greatest and/or would describe any trends that may develop.

#### 9.2 Analysis Results

An analysis of system-wide benefits and benefits to the users and non-users of the in-vehicle information system was conducted. The first step in the process was to evaluate the system wide results via the system-wide measures output from each **CONTRAM** run for the varying percentages of equipped vehicles under the severe incident scenario. The second phase of the evaluation was through the use of UFPASC as described in Chapter 7.

#### 9.2.1 System-Wide Results

Table 9.1 displays the results from a system-wide perspective. As seen in the table, the results of the simulation under the severe incident situation indicate that 100 percent of the vehicles on the road equipped with in-vehicle information systems provides the greatest benefit to the system in terms of total system travel time, travel time per vehicle, and speed.

Total system travel time is perhaps one of the most important measures of system-wide performance. The total system travel was 12,360 vehicle-hours under the non-incident base run. Under the severe incident scenario but with all unguided vehicles, the total system travel time increased to 15,194 vehicle-hours, a difference of 2,834 vehicle-hours. As the percentage of guided vehicles increased under the incident scenario, the total system travel time decreased from 15,194 to 13,101 vehicle-hours, a reduction of 2,093 vehicle-hours. This would indicate that the adverse effect of the incident was significantly reduced under guided vehicle situations.

In addition to the varying percentages of equipped vehicles under the severe incident scenario, the base run without the incident where all vehicles choose their fastest route is shown. As seen in the table, at 100 percent, equipped vehicles under severe incident conditions, the speeds are only slightly lower and the travel times are only slightly higher than those under the no-incident, 100 percent, guided base run. It also appears as though at either **50** percent equipped vehicles, or 75 percent equipped vehicles, a quirk in the data occurred. For all other percentages between 0 and 50 and 75 to 100 the findings were consistent in that the more equipped vehicles, the more benefit was accrued to the system. However, the data between 50 and 75 percent equipped did not follow that trend. The quirk in the data will be pursued in future research as was not possible in this project.

Percent Vehicles Equipped	0	10	2:		75	<b>'</b> 90	100 …	Base Run
Avg. Travel Time per Veh (min)	10.30	10.00	9.86	9.44	9.52	9.26	8.88	8.38
Avg. Travel Distance per Veh (mi)	12.53	12.48	12.43	12.48	12.45	12.52	12.59	12.54
Average Speed (mph)	28.5	29.2	29.6	31.0	30.7	31.7	33.3	35.1

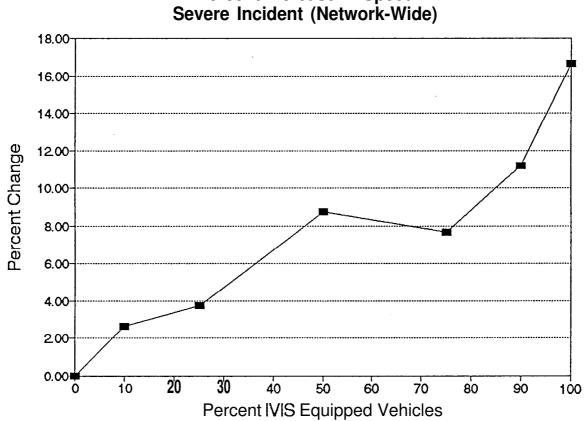
Table 9.1 System-Wide Results

Figure 9.1 displays the increase in average speed, network-wide under the severe incident scenario. As seen in the figure, an increase of approximately 17 percent is obtained for 100 percent information-system-equipped vehicles.

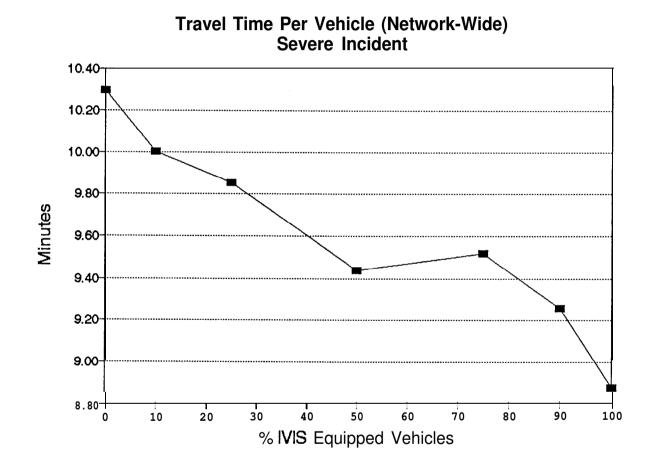
The average travel time per vehicle is displayed in Figure 9.2. The travel time per vehicle on average is network wide from each O-D pair. As seen in the figure, the average travel time per vehicle decreases from slightly more than 10 minutes to less than 9 minutes for 100 percent equipped. This represents a reduction of approximately 14 percent over the nine-mile-long, two-mile-wide corridor for each vehicle on average, as presented in Figure 9.3. It is **difficult** to make conclusive remarks regarding the time saved per vehicle because the average trip length is not very long. An average trip length of over 20 to 25 minutes is more desirable. However, the system-wide results provided by this analysis indicate that the greatest benefits are obtained when all vehicles are equipped with in-vehicle information systems. Assuming optimal data is given to all drivers and that all drivers follow their recommendations.

Figure 9.4 presents the percent decrease in total queues, network-wide under the severe incident scenario. As seen in the figure, a decrease of almost 35 percent is obtained with 100 percent of the vehicles having in-vehicle information. From the figure it can be concluded that the guided vehicles are diverting to avoid the major queues.

Whether or not travellers purchase the IVHS equipment and the various percentages of equipped vehicles occur, depends on two major factors. First, do "IVHS" guided vehicles benefit significantly enough to justify their expenditure of funds for such equipment, and second, will all users and the general public be supported by governmental-supported traffic control centers? In order to begin to address these



# Percent Increase in Speed Severe Incident (Network-Wide)



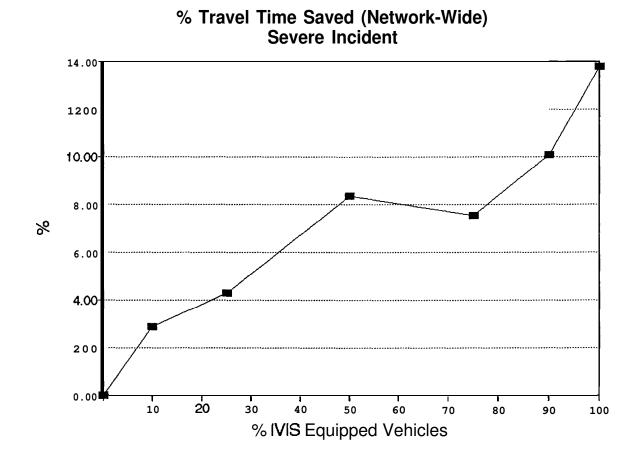
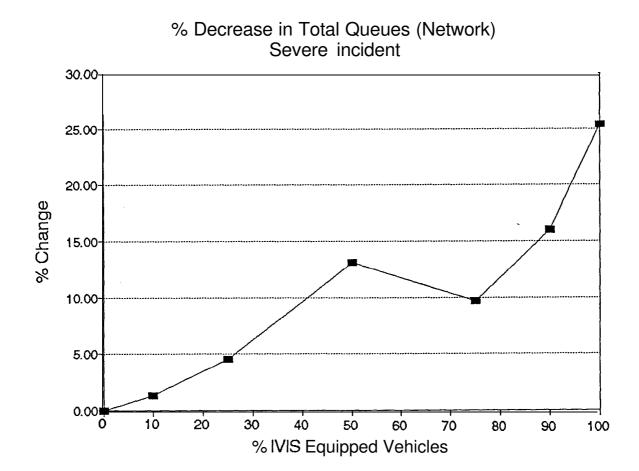


FIGURE 9.3



questions, benefits to **travellers** in guided and unguided vehicles need to be assessed. This initial assessment is discussed in the next section. All benefits are also based on the availability of substantial un-used capacity on the parallel arterials.

#### 9.2.2 Benefits to Guided and Unguided Vehicles

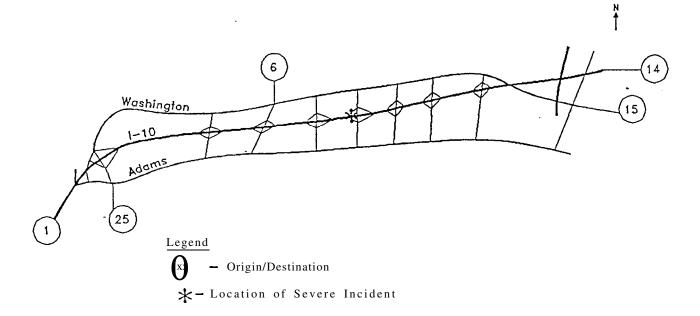
To properly evaluate the benefits to both the guided and non-guided vehicles in the system, a procedure was used whereby two classes of vehicles were set up. The first set of vehicles were those that were considered guided, which were free to be assigned on the fastest routes within CONTRAM. The second class of vehicles were the unguided vehicles, which were the vehicles assigned to the fixed routes that did not change regardless of the incident on the freeway. The primary source of information regarding the benefits that both guided and unguided vehicles obtained with the varying percentages of equipped vehicles under the severe incident scenario on the network came from the UFPASC. The UFPASC (User Friendly Post Analysis System for CONTRAM) is an interactive program for examining the outputs from CONTRAM runs. The UFPASC produces tabular and graphical outputs for selected parameters from the results file produced by CONTRAM. UFPASC uses a menu system to set up the analysis stages for producing the selected outputs. UFPASC allows selective investigations of the .RTE and .PAF files produced by CONTRAM.

Thus, by using the UFPASC, a number of origin-destination pairs were evaluated. The origin-destination pairs were chosen on the basis of three key considerations:

- 1) The O-D pair had to have a reasonably large demand level, at least enough to draw some reasonable conclusions;
- 2) The O-D pair had to have the incident on the freeway between the origin and destination. This is a requirement so that there is the opportunity for some significant diversion to occur;
- 3) Different O-D pairs would be chosen relative to one another so that a cross section of the different areas of the network would be examined and that both Adams Boulevard and Washington Boulevard would have the opportunity to be used.

On this basis three different O-D pairs were chosen. The three different O-D pairs are highlighted in Figure 9.5. The first O-D pair chosen for evaluation was that of origin 6 to destination 14. Origin 6 is off **the** arterial Washington Boulevard while destination 14 is at the end of the Santa Monica eastbound freeway, The second O-D pair chosen was origin 1 on the western boundary of the Santa Monica

## O/D Pairs Chosen For Evaluation



1.14

freeway to destination 15 at the eastern end of Washington Boulevard off Figueroa. The third **origin**destination pair chosen for evaluation was origin 25 off Adams Boulevard to destination 14. Thus, in the three O-D pairs, two originate on the arterial with their final destination being the freeway, while the other pair originates on the freeway and ends on the arterial.

Table 9.2 presents the results for the three origin-destination pairs chosen for evaluation in terms of average speed (mph) and average travel time (min) for both guided and unguided vehicles with the varying percentages of in-vehicle information equipped vehicles. This information is an average over all time slices. Time slice by time slice information is only available for the routes selected, not for the route time, distance, and speed. Figures 9.6 - 11 present the information from Table 9.2 in graphical form.

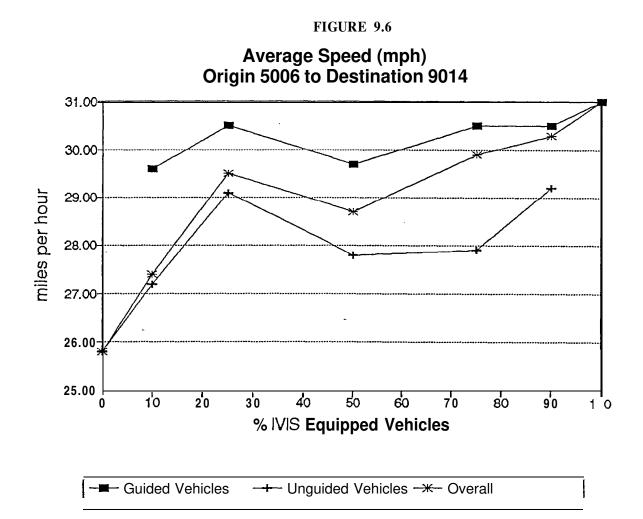
As seen in the figures, the guided vehicles have a higher speed and shorter travel time to the destination than the unguided vehicles. Once again, as in the system-wide results, the highest benefits in terms of speed and travel time were found to occur with 100 percent in-vehicle information equipped vehicles.

The reliability of the total route distance for both types of vehicles was found to be questionable. It appeared that the same route did not have the same distance in different runs; therefore, the total route distance was not used as part of the analysis. However, analysis was conducted to investigate the routes chosen between different origin-destination pairs for varying percentages of equipped vehicles. Figure 9.12 presents the results of such analysis. The figure shows the two most popular routes chosen for the unguided vehicles and guided vehicles between origin 1 which is on the western boundary of the freeway, and destination 15 which is on the eastern boundary of the network at the end of Washington Boulevard. The figure represents the routes chosen when 75 percent of the vehicles are equipped with in-vehicle information systems under the severe incident scenario.

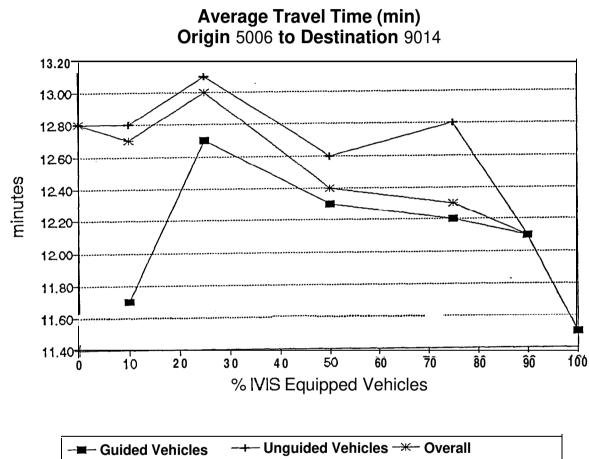
The two most popular routes for the unguided vehicles both travel through the incident on the eastbound Santa Monica Freeway, while for the guided vehicles, the second route of choice was to exit the freeway at the first possible alternative and use Washington to reach destination 15.

#### 9.3 General Evaluation

The following assumptions need be noted again to cautiously view the results of this analysis:

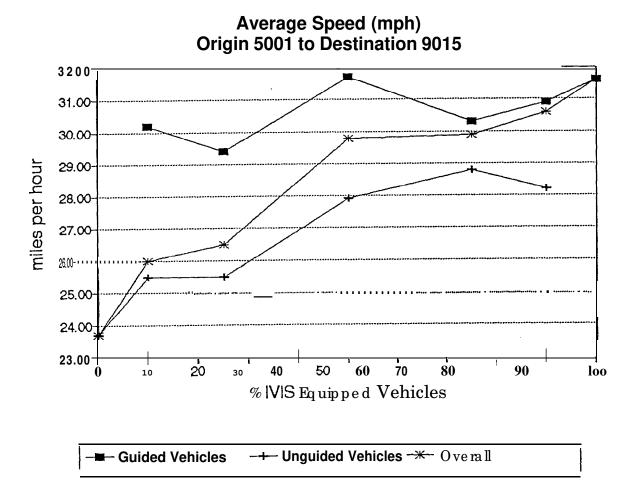


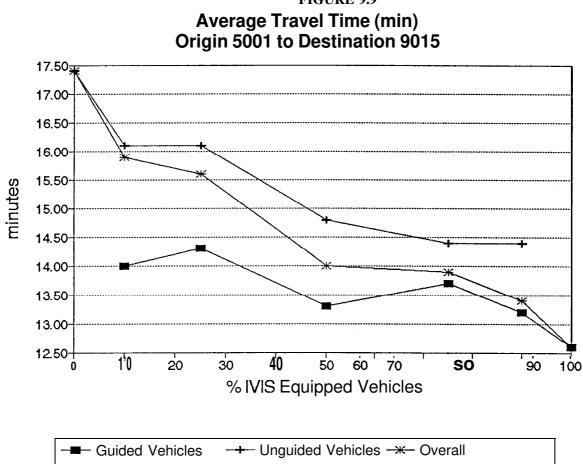
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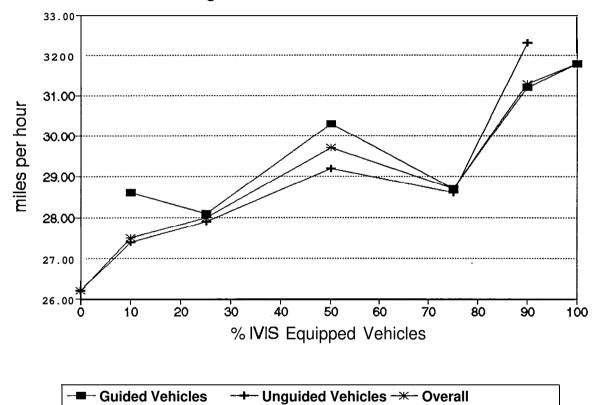




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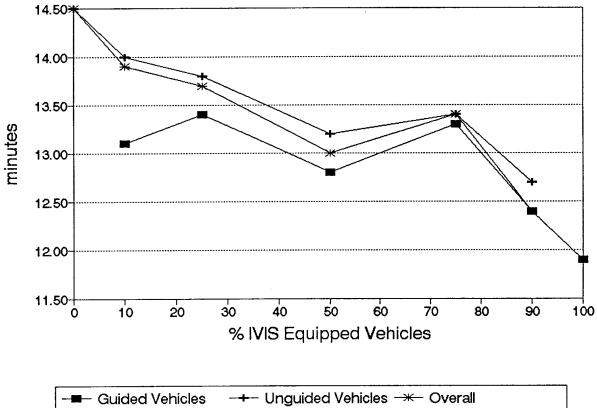
FIGURE 9.10

# Average Speed (mph) Origin 5025 to Destination 9014

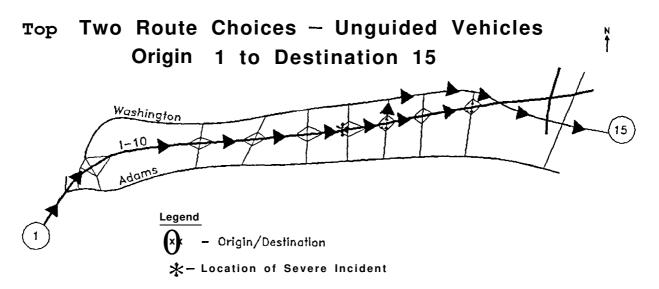


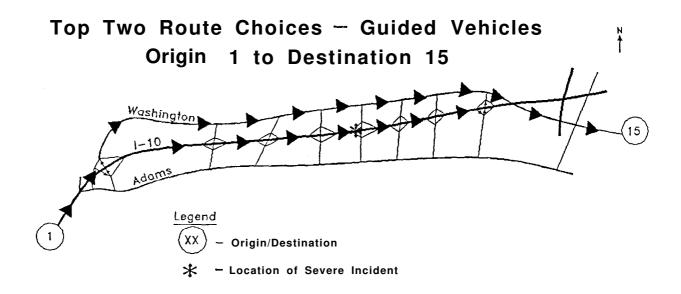












## TABLE 9.2 AVERAGE SPEED AND TRAVEL TIME

Average Speed (mph)

Origin 5006 Destination 9014

	Percent Equipped												
1		10	25	50	75	- 90	100						
Guided		29.6	30.5	29.7	30.5	30.5	31						
Unguide	25.8	27.2	29.1	27.8	27.9	29.2							
Overall	25.8	27.4	29.5	28.7	29.9	30.3	31						

Origin 5006 Destination 9014

.

#### Average Travel Time (minutes)

			P	ercent Equi	pped		
		10	25	50	75	90	100
Guided	<u></u>	11.7	12.7	123	122	121	11.5
Unguide	12.8	12.8	131	126	128	121	
Overall	12.8	12.7	13	124	123	121	11.5

Origin 5001 Destination 9015

#### Average Speed (mph)

		Percent Equipped												
		10	25	50	75	90	100							
Guided	<u></u>	30.2	29.4	31.7	30.3	30.9	31.6							
Unguide	23.7	25.5	25.5	27.9	28.8	28.2								
Overall	23.7	26	26.5	29.8	29.9	30.6	31.6							

## Origin 5001

ſ

#### Average Travel Time (minutes)

100

Destination 9015

#### Percent Equipped 90 10 25 50 75 0

Guided		14	14.3	133	137	13.2	12.6
Unguide	17.4	16.1	16.1	14.8	14.4	14.4	
Overall	17.4	15.9	15.6	14	13.9	13.4	126

Origin 5025 Destination 9014

#### Average Speed (mph)

Destinatio	in 9014		P	ercent Equi	pped		
1		10	25	50	75	90	100
Guided	└────╪┈	28.6	28.1	30.3	28.7	31.2	31.8
Unguide	26.2	27.4	27.9	29.2	28.6	32.3	
Overall	26.2	27.5	28	. 29.7	28.7	31.3	31.8

Origin 5025 Destination 9014

#### Average Travel Time (minutes)

Destinatio	n 9014		Р	ercent Equi	pped		
		10	25	50	75	90	100
Guided	<u></u>	13.1	13.4	12.8	13.3	124	11.9
Unguide	14.5	14	13.8	13.2	13.4	127	
Overall	14.5	13.9	137	13	13.4	12.4	11.9

- Only two of the five parallel arterials within the Smart Corridor were modelled; additionally, three-quarters of the entire length of the Corridor was modelled. Thus, the travel times throughout the corridor are not as large as one would like to evaluate the benefits.
- The structure of the origin-destination pairings was set up so that all origins and destinations were external to the network. The origin and destination data were very coarse and from point to point, each origin and destination could be reached by either the freeway or the arterial, not both. For example, to get to destination 15, a vehicle must exit the freeway and use Washington Boulevard.
- Due to the weaknesses in freeway modelling and incident modelling as described in Chapters 6 and 8, the results presented from this analysis should be viewed with caution. The travel times on the freeway are too low during both incident and non-incident conditions thus, diversion to the arterial is not as attractive as it should be.
- Since this is the first application of **RODIN**, the results should be viewed with some caution as well.
- The simulation results in this analysis apply only to the morning peak period. Additionally, the type of incident modelled is atypical and extreme, since it is unlikely that two-and-a-half lanes would be blocked for longer than one-half hour. All analysis for guided versus unguided vehicles was conducted on the traffic heading eastbound toward downtown Los Angeles.

### **10.0 OVERALL ASSESSMENT AND FUTURE RESEARCH**

This chapter describes the overall assessment of the completed research. First, the suitability of CONTRAM is described followed by a description of weaknesses of the study outside of the model; then the major findings of the study are presented. Finally, potential future directions regarding the application of a modelling process to evaluate the potential benefits of in-vehicle information systems are discussed.

### **10.1 Suitability of CONTRAM**

The **CONTRAM** model has many features that are well suited to an application such as this. However, there still remain questions about some of its capabilities. This section outlines the strengths and weakness of the model for this particular application.

### **10.1.1 Strengths**

- 1) When using the 386 version of **CONTRAM** 5 and DBOS memory management system, there was no problem in terms of network size limitations and running time for this particular application.
- 2) CONTRAM provided evidence of accurate representation of oversaturated conditions on arterials.
- **3)** The use of COMEST in developing O-D matrices was very helpful. The difficulty of setting up a realistic time-sliced O-D matrix is traditionally one of the main problems encountered in an experiment such as this one.
- 4) **RODIN** provided the capability to distinguish between guided and unguided vehicles. The unguided vehicles were always assigned to the same fixed routes determined by the average daily conditions, without incident. These routes were usually no longer optimum under incident conditions. On the other hand, guided vehicles are assigned to their optimum routes, assuming perfect knowledge of current traffic conditions.

#### 10.1.2 Weaknesses - Suggested Improvements

- The weakness of CONTRAM in the area of representation of oversaturated conditions on freeways was identified as the most important problem with regard to this application. Although a lot of time was spent in trying to get acceptable results, as described in Chapter 6, many questions were not answered:
  - What type of link (uncontrolled, give-way or signalized) is the most appropriate to code freeway links and on-ramps? As mentioned in Chapter 6, this decision has an effect on the queuing process.
  - How does the concept of "throughput capacity" used by **CONTRAM** relate to the usual concept of freeway capacity?
  - How can the speed-flow relationships of **CONTRAM** be used in simulating oversaturation conditions?
  - Is it possible to do any weaving analysis?
  - Some parameters, like the jam headway spacing and points on the speedflow curve can be calibrated on a simple freeway section. How can the calibration information be used when applying the model to a complex corridor network?
- 2) The CONTRAM standard assignment assumes that all vehicles take their optimum routes. The base run (no incident) should not be regarded as an accurate representation of average daily conditions. Some drivers do not choose the best route, and this should be accommodated by the model by introducing distortions to the perceived link costs.
- 3) Under incident conditions, it was assumed that unguided vehicles always take the same route that used to be optimum under non-incident conditions. It would be realistic to model the spontaneous diversion of unguided vehicles due to sources of information other than the guidance system, like radio information or the direct view of queues in front of them.
- The use of **RODIN** for varying percentages of guided vehicles led to some discrepancies in the demand structure and the total number of vehicles in the system (in the range of 3%). In order to have some comparable results, the demand should be exactly the same.

- 5) The truncation of link travel times led to some problems in speed calculations. For example, when using a link free-flow speed of 80 km/h in undersaturated conditions, the resulting average **speed** is not necessarily 80 km/h, as expected.
- 6) Output information useful for this type of analysis which is not provided by CONTRAM such as:
  - aggregate statistics per set of links (Freeway-Arterials);
  - aggregate statistics per vehicle type (Guided-Unguided)
- 7) Although the use of UFPASC (described in Chapter 9) for routing analysis was very helpful, some weaknesses were identified:
  - The run time for each O-D pair is a half hour to an hour on a 386 microcomputer;
  - The reliability of the total route distance is questionable, as it appeared that the same route did not have the same distance in different runs;
  - A time slice by time slice analysis would be a useful tool in comparing travel times and travel distances;
  - A network plot showing the two most popular routes for a given O-D pair, vehicle type and time slice would be very useful as well.

### 10.2 Weaknesses of the Study

The improvement of modelling freeway congestion does not alone cure the weaknesses of the study. Weaknesses exist on both the supply and demand side of the modelling process as well. With respect to the supply side, as mentioned in Chapter 5, the Smart Corridor consists of five parallel arterials with approximately 15 cross streets, and is approximately 13 miles long. Due to time and resource limitations, approximately nine miles of the SMART Corridor with two parallel arterials was coded into the model instead of the entire 13 miles and five parallel arterials of the corridor. The eastern boundary of the network is the Harbor Freeway, while the western boundary is LaCienega Boulevard. The two parallel arterials coded were Washington Boulevard and Adams Boulevard. Ten of the 15 major north-south streets connecting Washington, Adams, and the Santa Monica Freeway were coded as well. Thus, with

only two parallel arterials the opportunity for diversion is not as great as it would normally be in the Smart Corridor. Additionally, since approximately nine miles of the 13 mile corridor were modelled, the travel times throughout the corridor were not as high as they would normally be due to the reduced travel distance, and diversion from the freeway to the arterial was not as attractive as it might be with a longer travel time.

From the demand side, problems exist with both the origin-destination matrix and the structure of the demand over time. The problems with the origin destination information and structure are described in Chapter 7. Only external sinks and sources were used; thus, any major internal sinks and sources within the corridor were neglected. Although using the origin-destinationestimator program, COMEST, assisted in creating a somewhat realistic origindestination matrix, it should be pointed out that the inputs to COMEST are the flows instead of the actual demands. Thus, the demand could be underestimated through use of this program. A second weakness in the demand structure is the variation over time. Based on information provided by the previous study [3] and information regarding the performance of the system, the demand was manipulated to create an origin-destination matrix for eight time slices. Information was only available for the time period of 7:00 a.m. to 8:00 a.m., and all information for the previous and remaining time slices was factored based on spot traffic counts. Thus, for the purposes of this study the highest demand was assumed to occur from 7:00 a.m. to 8:00 a.m. while the demand for the other time slices were factored based on information provided from the previous study. Once again, this is likely not the case and leaves the results of the study open to some question.

#### **10.3 Major Findings**

Based on the information provided in the previous two sections, the results of this study should be viewed with some caution. The results should be viewed in a somewhat qualitative manner, the findings being the more vehicles equipped, the better the system performance. As seen in Table 9.1, with a severe incident on the freeway, as the percentage of vehicles equipped with information increases, the performance of the system improves to where the system is at a level of performance that is only slightly less than that before the incident occurred. This degree of improvement is only possible because of the availability of underutilized capacity on the arterials parallel to the freeway. Chapter 9 describes in greater detail the results of the analysis.

### **10.4 Future Research**

1) *The representation of oversaturated conditions on* freeways. As previously mentioned, some difficulties were encountered in the modelling of the freeway portion of the

SMART Corridor. Any further application of **CONTRAM** to this type of network will have to carefully address this question. The authors of the model reported that Southampton University has recently conducted research on modelling congestion on freeways by varying the randomness parameter in the queuing formula [23]. This is similar to the approach suggested some years ago by Davidson [24] and could be repeated using the current version of **CONTRAM**. However, it is not clear how relevant this method is.

- 2) *The* use *of ROGUS*. ROGUS is a program currently under development at TRRL to simulate route guidance based on the CONTRAM model. Because of time constraints it was not possible to use ROGUS in this phase of the study, though it could be used in an extension of the project. ROGUS consists of two main parts: Modified CONTRAM and ROGUS/Ada.
  - a) Modified CONTRAM is responsible for generating the base loading of unguided vehicles, and differs from standard CONTRAM5 only in its ability to distort drivers' perception of link costs to simulate their lack of perfect information, and
  - b) ROGUS/Ada reassigns a certain proportion of the unguided vehicles to simulate guided vehicles. The method of assignment is event-based using simulated beacon information which itself is based on the historical data and simulated real-time data from detectors and vehicle-to-beacon communications.
- 3) *The application and simulation of different traffic management strategies.* It would be interesting to compare the effects of guidance systems with some other corridor management strategies like signal optimization and coordination to determine how the benefits compare and if the benefits are cumulative.
- 4) *The potential re-investigation of the INTEGRATION model. The* model is now available for investigation. It might be worthwhile to reevaluate the application of the INTEGRATION model to the Smart Corridor.

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APPENDIX A

CONTRAM															
1	1	700	730	800	815	<b>83</b> 0	845	900	930	1000	1100				
	5001							<i>,</i> •							
	5002														
		2240	4440												
	5004														
3 5	5005	2210													
4	301	3110	2220	0	0	0	40	500	1500	0	30				
4	303	2220	0	0	0	0	1		1600	2	30				
4	311	2110	5110	0	, O	0	1	10	1600	2	31				
4	313	3030	2110	0	0	0	20	240	1600	0	31				
4	414	2040	4210	0	0	0	4	40	2500	0	41				
4	421	2140	4320	0	0	0	4	40	2500	0	42				
4	4329	0020	4430	0	0	0	4	40	2500	0	43				
4	443	2230	4140	0	0	0	4	40	2500	0	44				
4	502	2130	2120	0	0	0	60	600	4200	0	50				
4	511	5240	2010	0	0	0	20	240	1600	0	51				
4	513	3130	5240	0	0	0	20	200	1600	0	51				
4	5249	0030	0	0	0	0	4	30	1500	40	52				
5	304	3110					75	1000	600	180	303	301	25	30	
5	312	5110	3030	0	0	0	100	1300	600	200	311	313	25	31	
5	411	2040	4210	0	0	0	40	500	2000	0	414	0	70	41	
5	422	2140	4320	0	0	0	80	1000	1500	0	421	0	50	42	
5	4339	0020	4430	0	0	0	300	5000	3000	0	432	0	95	43	
5	444	2230	4140	0	0	0	80	1000	3000	0	443	0	95	44	
6	12	2024	0	0	0	0	75	900	1500	0	1	2	100	100	
6		2154	0	0	0	0	4	50	1500	8	1	2	100	60	
6	201		4220	0	0	0	20	200	1600	0	20	1	100	100	
- 6			5130	0	0	0	4	50	1600	8	20	2	100	100	
6		5130		0	0	0	80	1000		0	20	2	100	100	
6			4330	124	0	0		1300		0	21	1	100	100	
- 6		3120	0	0	0	0	10	100	1500	0	21	2	50	100	
6		4330	-	0	0	0	10		3000	0	21	2	100	100	
6	214		31209		0	0		5000		0	21	1	100	100	
6			90010		0	0	75		1600	0		2	50	70	
6			4110	0	0	0	40		1500			1	100	100	
6		4110	0	0 0	0 0	0		1000		0		2	100	100	
6		3040		0	0 0	0	40		2000			1	100	100	
6			4110	ů 0	0	0		1000				2	100	100	
7	1	25		Ŭ	Ŭ	Ŭ	,,,			•		-			
7	20	10													
7	20	10													
7	21	10													
7 9	10	22		140	120	0	0								
				200	120	107									
-10	1	164			450		1020								
-10	2	492					1020								
-10	4	492	720	600	450	321	1020								

CONTRA	AM TES	T DEN	IAND										
	1	9	105										
5001	9001	10 <b>1</b>	3000	5000	375	750	1125	1500	1350	1050	750	375	0
5001	9001	54	3000	5000	40	80	120	180	160	170	160	100	0
5001	9003	101	2300	5000	150	300	450	600	525	375	300	150	0
	1	9	100										
5002	9002	101	2700	5000	320	560	800	1200	<b>9</b> 50	700	600	300	0
5003	9003	101	2300	5000	50	200	300	350	400	250	150	50	0
5004	9002	104	2000	5000	40	120	200	300	270	240	210	150	0
5005	9001	22	2900	5000	10	20	20	20	20	20	20	20	0
5005	9002	101	1000	5000	100	120	150	200	180	150	120	80	0

CONTR/ 50 53	AM TES 12	ST CON	TROL					<i>,</i> .			
54											
55											
56											
57	1	20	21	22							
71	1	110	50	50							
71	2	110	50	50							
72	6	-110	4	6							
71	3	55	0	30							
71	4	110	40	60							
71	5	110	50	50							
77	1	3	3	3	3	3	3	3	3	3	
77	20	2	2	2	2	2	2	2	2	2	
77	21	5	5	5	5	5	5	5	5	5	
77	22	1	1	1	1	6	6	1	1	1	
81	1	7	221	304	311	511	201	14	215		
85	5005	9001	2	1							

CONTRAM TH CONTRAM TES CONTRAM TES	ST DEMAND			,.								ITERATION	NUMBER
	TIME S	LICES :										1.500	
	1	2	3	4	5	6	7	8	9				
	700 7.	30 8	8 00	15 8	30 8	45 9	00 9	30 100	0 1100				TOTALS
0 JOURNE	Y-TIME (V	נח-חז י											TUTALS
OFREEMOVING	31.9	70.5	55.1	85.8	82.7	65.8	90.1	44.6	3.1				529.4
FLOW DELAY	.0	.0	.0	.0	.0	.0	.0	.0	.0				.0
QUEUEING	7.4	21.5	18.0	27.8	40.9	40.4	30.4	13.3	.6				200.3
TOTAL	39.3	91.9	73.0	113.5	123.6	106.2	120.5	58.0	3.7				729.8
	CE TRAVEL								400.0				25303.0
0	1360.8	3171.8	2634.7	4380.3	4244.0	3287.9	4198.6	1896.0	128.9				2000.0
0 OVERAL	L NETWORK	SPEED (	KM/H)										
0	34.7	34.5	36.1	38.6	34.3	31.0	34.8	32.7	34.6				34.7
•	2.2.	2.12											
0 TOTAL	FINAL QUE	UES (VEH	)										
0	17.3	57.9	77.4	137.1	198.5	156.9	56.4	30.2	.6				732.3
0													
	ONSUMPTIO			(00.0	702.0	705 7		270 7	10 /				2541.8
OTRAVELLING		313.5 35.3	254.2 28.9	402.8 58.2	392.9 88.1	325.3 80.9	460.1 51.8	238.7 24.2	18.4 .2				375.3
QUEUE I NG TOTAL	7.6 143.7		28.9	460.9	481.0	406.2	511.9	262.8	-2 18.6				2917.1
IUTAL	143.7	J40.7	205.1	400.7	401.0	400.2	J 11.7	202.0	10.0				
0 TOTAL	LINK COUN	TS (VEH)	)										
OARRIVALS	2662	5282	3656	4539	4341	3884	6224	3645	304				34537
PCU FACTOR	1.07	1.08	1.09	1.11	1.11	1.12	1.13	1.17	1.26				1.11
STOPS	961	2196	1601	1980	1837	1630	2631	1425	96				14359
% STOPPED	36.1	41.6	43.8	43.6	42.3	42.0	42.3	39.1	31.7				41.6
OPACKET SIZ	E WITHIN	EACH O-D	MOVEMEN	IT IS VA	RIABLE		F	ROUTES AND	O ROUTE MEM				
TOTAL NUMB	ER OF PAC	KETS ENT	TERING TH	E NETWOR		792			S PER ROUTE	4.82			
TOTAL NUMB						158		ORDS AVA			( OUT OF	3985293)	
TOTAL NUMB		S				927			ITERATION	586			
MEAN PCU F	ACTOR				1	.11	C	CODONS PE	R WORD	10			

ITERATION NUMBER

5

CONTRAM TEST NETWORK CONTRAM TEST DEMAND CONTRAM TEST CONTROL OTIME SLICE 3 START 800 FINISH 815 DURATION 15 MINUTES

OCCUP-AV. JUNC .--- SIGNAL---MEAN-TIME TOTAL-TIME-&-DELAY ARR/ ARRIVALS DEPART MEAN THRU-MEAN LINK LINK MEAN ANCY// SPEED NO. GREEN: O LIN PER VEHICLE FREE-FLOW- QUEUE BY CLASS NO. ENTRY INIT. FROM FINAL PUT PCU CAP CYCLE P -IN L QUEUE QUEUE CAP/Y FACTOR (RHO) TOTAL QUEUE MOV/G DELAY - ING STOPS QUEUE С R AND FLOW (SEC) (SEC) (VEH-H) (%//%) (KM/H) (SEC) T (% (VEH) (VEH) (VEH) (VEH) (VEH) TYPE (VEH) 1 30: 55 .99\* .82 9 88 34.6 92 17 3.31 160 152 10.5 162R 125 160 2.0 19.8 30: 55 .09 8 67 1 5 187 1.10 .34 9 5 .07 63 58 .6 14S 63 .8 20 50:110 .08 .03 1 57 19.4 45 17 94 1.93 .05 15 .1 5 5 .1 201S 1.88 F 94 3.9 20 50:110 42 .18 .88 46 157 8.1 182 202S 160 5.0 160 17.9 50:110 99 20 3.94 5.99 17 .97\* 202 122 21.9 171 204S 197 21.6 166 166 36.1 21 50:110 0 63 130 18 .75 .12 25 .5 154 1.33 .16 1.8 10 14 211S 34 21 25:110 85 212S 50:110 79 11.0 21 33 23 .53 1.21 19 .56 188 5.0 341 200 3.3 190 213S 1.34 0 82 54.8 21 50:110 1.05 .60 326 23 16.46 200 .9 188 9 193 5.4 326 214S 25:110 .74 .83 4 95 26.4 21 47 1.39 1.08 124 215s 63 9.0 58 4 67 4.1 84 29.1 22 50:110 68 20 .50 .24 2 5 43 1.0 150 1.14 .29 62 .7 221S 43 38 73 31.9 22 50:110 1 113 23 1.02 .26 114 1.80 .35 40 .7 40 40 1.0 2225 .26 2 69 29.3 22 50:110 .32 60 17 .60 180 1.26 223S 43 1.5 39 19 58 1.3 22 50:110 70 32.4 18 1.43 .33 1 66 1.7 171 .39 108 224S 57 .7 67 30 37.5 1.80 .24 48 .67 50 50 208 301U 50 30 400 303U 6 92 21.9 30 2.33 2.55 .91\* 164 85 130 8.1 77 5 15 97 8.4 107 1.20 304G 31 36.0 5 106 323 1.24 .33 1 .03 24 77 311U 106 31 117 312G 31 400 313U 2 63 30.2 41 .37 1.09 87 1.4 148 1.45 .59 60 15 88 .3 38 50 411G 36.0 41 4 -44 13 397 609 1.03 .65 414U 397 384 36.0 42 532 .52 4 .32 1.17 278 421U 288 215 63 3 87 33.7 42 3.75 1.25 .85 106 26 .7 180 176 4.8 212 422G 160 36.0 43 4 .28 198 248 538 1.16 .46 432U 248 50 43 59.6 1.27 .01 477 433G 30 44 625 443U 1 62 42.8 44 3 10.16 .38 27 439 713 1.05 .62 84 463 .7 413 1.6 444G 50 36.0 60 3.31 .19 200 1050 502U 200 200 40.8 51 .19 21 .40 63 335 1.19 511U 72 48 5 10 .60 36.0 51 20 108 108 108 400 .27 513U 52 27.0 375 .44 4 .18 166 166 524U 156 FLAGS: R = REDUCED CAPACITY L TOTAL OTOTAL TIMES BY VEHICLE CLASS С В = RHO EXCEEDING 90% \*\* = RHO 100% OR GREATER 0.45 55.09 48.86 5.78 (VEH-H) FREEMOVING = FULL LINK 0.00 0.00 0.00 F 0.00 FLOW DELAY 17.95 S = OPTIMISED SPLITS 1.12 16.61 0.23 QUEUEING = OPTIMISED CYCLE & SPLI 6.90 73.04 С TOTAL 65.47 0.67 TOTAL DISTANCES NOTE: FOR FULL DEFINITIONS OF COLUMN HEADINGS SEE USER GU 2634.7 2384.4 14.2 236.2 (VEH-KM) TRAVELLING TOTAL LINK COUNTS (VEH) TOTAL FUEL CONSUMPTION 3656.0 ARRIVALS 184.50 5.45 64.22 254.17 TRAVELL ING (I ITPES)

LINK-BY-LINK ALL-TIME-SLICES - AVERAGE SPEED OF A CAR (KM/H)

CONTRAM TEST NETWORK CONTRAM TEST DEMAND CONTRAM TEST CONTROL

•

										ITERATION NUMBER
		SLICES :								
LINK	1	2	3	4	5	6	7	8	9	
NO.&										OVERALL
TYPE	200 <del>77</del>	0 00		F 07	o <b>o</b> /	F 00	0 07		1100	AVERAGE SPEEL
(	00 73	0 80	0 81	5 83	0 84	5 90	0 93	50 100	00 1100	
12S	39.0	36.9	34.6	36.3	39.8	37.3	35.7	38.6	40.5	36.9
14S	19.9	19.9	19.8	22.2	22.3	20.4	19.8	19.9	25.4	20.3
201S	16.4	16.0	19.4	14.4	15.7	16.5	17.0	17.7	16.4	15.9
202S	7.2	5.0	3.9	6.5	8.1	5.9	4.1	6.5	7.9	5.1
204S	33.0	24.0	17.9	14.6	11.1	10.7	20.1	27.7	36.0	18.7
211S	37.5	36.7	36.1	37.5	34.2	34.4	36.8	35.7	35.9	36.4
212S	.0	.0	.0	.0	8.2	8.2	.0	.0	.0	8.2
213s	12.9	11.7	11.0	7.9	9.6	11.0	11.6	12.9	13.8	10.6
214S	.0	56.9	54.8	51.0	41.3	38.0	51.5	57.0	.0	46.5
215s	25.9	23.5	26.4	27.8	29.5	29.1	23.9	21.6	31.5	24.9
221S	30.3	29.4	29.1	28.8	26.2	26.5	29.4	29.4	.0	28.7
222S	33.6	32.8	31.9	32.7	34.4	34.2	31.8	32.8	34.0	32.8
223S	29.4	28.9	29.3	30.1	26.0	29.0	28.8	29.3	.0	29.1
224S	33.6	34.0	32.4	32.5	33.1	34.0	33.3	34.0	.0	33.3
301U	37.5	37.5	37.5	37.5	37.5	37.5	37.5	37.5	.0	37.5
303U	.0	.0	.0	.0	.0	36.0	.0	.0	.0	36.0
304G	39.0	26.5	21.9	17.8	12.9	11.3	20.2	29.9	23.2	19.9
<b>3</b> 11U	36.0	36.0	36.0	36.0	36.0	36.0	36.0	36.0	36.0	36.0
312G	.0	.0	.0	.0	.0	43.7	.0	.0	.0	43.7
313U	.0	36.0	.0	.0	.0	.0	36.0	36.0	36.0	36.0
411G	40.6	37.8	30.2	10.4	<b>11.</b> i	16.5	33.8	36.7	35.3	22.8
414U	36.0	36.0	36.0	36.0	36.0	36.0	36.0	36.0	36.0	36.0
421U	36.0	36.0	36.0	36.0	36.0	36.0	36.0	36.0	36.0	36.0
422G	43.4	42.8	33.7	22.2	18.1	23.8	39.4	42.7	43.9	33.4
432U	36.0	36.0	36.0	36.0	36.0	36.0	36.0	36.0	36.0	36.0
433G	.0	.0	59.6	59.6	59.6	59.6	.0	.0	.0	59.6
443U	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
444G	43.8	43.3	42.8	40.4	41.6	42.5	42.8	43.1	43.3	42.4
5020	36.0	36.0	36.0	36.0	36.0	36.0	36.0	36.0	.0	36.0
5110	40.5	41.5	40.8	39.9	40.4	41.7	41.2	39.0	30.9	40.7
513U	36.0	35.8	36.0	36.0	36.0	36.0	35.8	34.5	33.1	35.7
5240	27.0	27.0	27.0	27.0	27.0	27.0	27.0	27.0	27.0	27.0
VERALL	34.7	34.5	36.1	38.6	34.3	31.0	34.8	32.7	34.6	34.7

ITERATION NUMBER

CONTRAM TEST CONTRAM TEST D CONTRAM TEST C 0 JU	EMAND	IMREP	20	SIG	NAL CON	נפטו ו בט					ITERATION	5
Ç 30	NUTION N		20	51 Gr							TIENATION	2
0	** 1.47											AVERA
0	1	E SLICES	3	4	5	6	7	8	9			AVERA IN T/
LINK TO LINK	700	730	800	4 815	830	845	900	930	1000	1100		1-
	100		000	015	000	045	,00	,20	1000	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		I
201 - 14	10	16	20	20	16	20	22	20	2			
201 - 422	0	0	0	188	156	40	0	20	0			
202 - 422	280	540	640	280	236	468	598	340	20			4
202 - 513	0	0	0	0	0	0	0	0	0			
204 - 513	138	346	432	552	476	472	344	250	15			3
204 - 14	316	296	232	196	192	200	294	294	20			2
OJUNCTION ENTRY LINK	FLOWS (	VEH/H)										
201	10	16	20	208	172	60	22	40	2			
202	280	540	640	280	236	468	598	340	20			4
204	454	642*	664*	748*	668*	672*	638	544	35			6
OSIGNAL PLAN TY	PES											
	FCFS	FCFS	FCFS	FCFS	FCFS	FCFS	FCFS	FCFS	FCFS			
OCYCLE TIMES (												
	110	110	110	110	110	110	110	110	110			
OGREEN TIMES (	SECS)											
LINK												
201	50	50	50	50	50	50	50	50	50			
202	50	50	50	50	50	50	50	50	50			
204	50	50	50	50	50	50	50	50	50			
OALL-RED TIMES	(SECS)				20			50	20			
	10	10	10	10	10	10	10	10	10			

CONTRAM TE	ST NETW	ORK										
10	5001	46	1	10	9001	444	414	204	14	215		
5	127	131	240	249	369 <sup>.</sup>							
11	5002	57	1	10	9002	502	213	12	202	422	432	
6	117	145	228	253	336	340			547	57/		
10	5001	114	1	10	9003	444	414	204	513	524		
5	195	199	308	328	332	,,,	1.47	20/	14	215		
10	5001	138	1	10	9001	444	414	204	14	215		
5	219	223	332	341	462	502	213	12	202	422	432	
11	5002	169	1 7/0	10 745	9002	502 452	213	12	202	422	452	
6	229	257	340 Z	365 4	448 9001	452 444	223	304	311	211		
10	5001	172 334	3 435	4 436	573	444	225	504	511	2.1		
5	269	554 180	435	438 10	9002	221	411	421	432			
4	5005 2 <b>38</b>	280	284	288	9002	221	411	461	452			
4 10	230 5001	229	204 1	10	9001	444	414	204	14	215		
5	310	314	423	432	554		414	201				
11	5002	282	1	10	9002	502	213	12	202	422	432	
6	342	370	453	478	561	565						
10	5003	288	1	8	9003	224	304	311	511	524		
5	395	481	482	502	506							
10	5001	316	1	9	9001	444	414	204	14	215		
5	397	401	510	519	642							
10	5001	342	1	10	9003	444	414	204	513	524		
5	423	427	536	556	560							
12	5005	360	2	2	9001	221	304	311	511	201	14	215
7	434	550	551	579	623	633	787					
11	5002	394	1	10	9002	502	213	12	202	422	432	
6	454	482	565	590	673	677						
10	5001	403	1	10	9001	444	414	204	14	215		
5	484	488	597	606	729							
10	5004	450	3	10	9002	301	222	411	421	432		
5	498	605	655	659	663							
10	5001	494	1	10	9001	444	414	204	14	215		
5	575	579	688	697	821							
11	5002	507	1	10	9002	502	213	12	202	422	432	
6	567	595	678	703	786	<b>79</b> 0						
10	5001	515	3	4	9001	444	223	304	311	211		
5	612	677	778	779	916				. = =			
9	5005	540	1	10	9002	221	411	421	432			
4	598	640	644	648						50/		
10	5001	570	1	10	9003	444	414	204	513	524		
5	651	655	764	784	788			201	47	245		
10	5001	585	1	10	9001	444	414	204	14	215		
5	666	670	779	788	912	500	247	10	202	(22	172	
11	5002	619	1	10	9002	502	213	12	202	422	432	
6	679	707	790	815	898	902	111	20/	14	215		
10	5001	677	1	10	9001	444	414	204	14	212		
5	758	762	871	880	1004	503	217	12	202	422	432	
11	5002	732	1	10 028	9002	502 1015	213	12	202	466	475	
6	792 5001	820 748	903	928 10	1011 9001	444	414	204	14	215		
10	5001 840	768 853	1 962	971	1096	444	~7 1 *7	204		- 12		
5	849 5001	853 787	962 1	971	9003	444	414	204	513	524		
10 5	5001 868	787 872	י 981	9 1001	1005			204		267		
5 11	868 5002	872 844	901	1001	9002	502	213	12	202	422	432	
	5002 904		י 1015	1040	1123	1127	213	16	202	766	736	
6 10		932 855	1015	1040 9	9001	444	414	204	14	215		
10		940	1049	1058	1183		- 1-7	204	1-7			
<b>ר</b>	חרש	<b>44</b> 0	1047	0101	COL							

Date:21/09/90

MONSTRATION OF UFPASC (USER FRIENDLY POST ANALYSIS) COLUMNED OUTPUT OPTION

LINKS	FLOWS (VEHS /HR)	DEG OF SAT. (%)	FINAL QUEUE (VEH)	INIT. QUEUE (VEH)	AVE. SPEED (KM/ HR)	AVE. TIME DELAY (SEC)	BLOCK -ING BACK
Time Interval	Number 3						
12S	284	23	0	0	39	1	0
14S	92	9	0	0	16	0	0
201S	124	27	1	1	15	20	0
2025	284	40	2	3	5	22	0
204S	552	83	6	4	28	40	0
211S	104	19	1	0	33	18	0
2125	0	0	0	0	0	0	0
2135	804	57	5	3	10	22	0
214S	980	72	8	4	78	27	0
215S	92	44	1	1	24	45	0
221S	172	28	1	1	29	20	0
222S	88	17	0	0	32	14	0
2235	132	22	1	0	25	17	0
224S	180	37	1 1	1	32	21	0
JTALS	3888	478	27	18	366	267	0
AVERAGES	299	36	2	2	28	22	0
MINIMUM	0	0	0	0	0	0	0
MAXIMUM	980	83	8	4	78	45	0

Page: 3

APPENDIX B

# LIVTRIPS. LPM

# 6/12/90

#### THE BATHRA SHITE OF PROBANE

PROGRAM MI HATRIX CONVERSION AND PRINTING

RELIED THE LIVERPOOL TRUE MATRIX ELE NAME

CAFE 18/ 5/190

TIME TRADE C

LIBTING OF THE PARAMETER VALUES EITHER INPUT ON SPADAN OF TAKEN AS COF ALL

ACC.	· :::	-	CHANE			<u>TO</u> V	÷.;	F
THEFT	::	-	114HFG			FACTOR		F
K CRAN			TAF	Ξ	· <u></u> -	FFIT		T
TOTAL A			TRUHE	27	F	FRAFT	:::::	F
1990 card	. ::	- 14	MENEYT		7	L OF HA	<b>.</b>	F
FLAT		F	FART		F	CSRI	:::::	
761 8619 -		1.00 1.00	KFC = ADDR -		1.00 0.00	V <b>F</b> 11 =		a nama Baranta
NROUS IROUS MTYPS		24 0 8	NCOLB JCOL1 MODET		≅4 ○ −1	IFOU: JCOLR MSTACK		0 0 0

HEADER RECORD DATA FOR THE MATRIX WRITTEN TO CHANNEL C.

MATRIX TITLE - INFRADAREA OF (TRAMP CORDOL)

MATRIX SIZE - 24 ROWS 24 COLUMNS Type of elements (htype) = 3 ELEMENT DIMENSIONS - TRIPS ELEMENT INITS - VPH \*:0\*\* C

FUE EVENTS WE UPITTEN AS OWNS

ILF. GINCE LONG = F THE FORMAT ASSUMED IS: TTE.C

## HULLD THE LIVERFOOL TRIP MATRIX

ROW	ID	SUM		C	SMMU IC	-		
		·	1 7 13 19	2 8 14 20	3 9 15 21	4 10 15 紀紀	5 11 17 23	
ţ	1	243.	0.000 0.000 147.000 0.000	2.000 0.000 7.000 17.000	0.000 2.000 0.000 6.000	4.000 0.000 0.000 2.000	0.000 0.000 0.000 2.000	0.0 8.0 81.0 15.0
2	'n	447.	0.000 44.000 192.000 0.000	0.000 0.000 10.000 31.000	0.000 5.000 0.000 4.000	21.000 0.000 0.000 11.000	21.000 0.000 0.000 2.000	0.0 8.0 40.0 56.0
3	3	ο.	0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000	0.0 0.0 0.0 0.0
<i>4</i> 1	٢.	664.	31.000 234.000 38.000 0.000	22.000 0.000 3.000 4.000	0.000 15.000 0.000 24.000	0.000 5.000 0.000 17.000	19.000 0.000 0.000 27.000	0.0 4.0 194.0 23.0
	5	0.	0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000	0.0 0.0 0.0 0.0
6	£	817.	0.000 0.000 4.000 0.000	1.000 0.000 3.000 24.000	0.000 99.000 0.000 91.000	0.000 1.000 0.000 1.000	0.000 0.000 0.000 0.000	0.( 3.( 580.( 10.(
7	7	ο.	0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000	0.( 0.( 0.( 0.(
8	8	335.	18.000 0.000 30.000 0.000	17.000 0.000 12.000 87.000	0.000 0.000 0.000 5.000	13.000 0.000 0.000 10.000	0.000 0.000 0.000 55.000	0.( 17.( 27.( 44.(
· 7	Ģ	0.	0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000	0.( 0.( 0.( 0.(
10	10	1182.	14.000	12.000	0.000	10.000	0.000	.0( ≅(

FAGE

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LIVNET. LPN

THE SATURN SUITE OF PROGRAMS FROSRAM S1 -7.1 BANKARA FROM DATE 13/ 6/90 TIME 10:29:17 LISTING OF THE OPTIONS CHOSEN: HPDATE = F FASSD = F FLOD = FLISTING OF THE PARAMETERS USED A - GENERAL MODEL PARAMETERS: 6 VI.4 MODET = 1MASL = 1 ISTOP = 901 TP = 30B - SATNET SPECIFIC: --- VI.4 LIST = TPRINT = F SPEEDS = F F AUTOZ = F ANTOX = DUTCH = F NGMADS = 1 KNOBS = 0 MAXZM = 500 MINSAT = 500 BCRP = 5.0 MINRF0 = 10 IFCC = 21 RUSPEU = 3.0 KPHMIN = 10 KPHMAX = 100 C - SATSIM SPECIFIC: PRSFD = F NOTUK = O NOPD = 0 3 LCY = 75 NITS = 15 NUC = LRTP = 0 GAP = 5.0 GAPM = 3.0 GAPR = 4.0 TDEL = 3.0 CAPMIN = 30. ALEX = 5.75D - SATASS SPECIFIC: PRINTE =FEXPERT =TCOMPAR =MIFLOW =TSUZIE =FSAVEIT =QUANTA =TAMY=F F SAVEIT = T PPM = 1.0 PPM = 0.0 SUET = 0.20 WAITU = 1.0 GONZO = 1.00NITA = 5

<u>م</u>ر م

NETWORK TITLE: LIVERPOOL MINI NETWORK, WARDROP EQUILIBRIUM, 1 USER CLASS

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	23	E E	5 4)	40 4	0002 88	4 1 25	1400 88	5 5 26			-	.·		
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So	27 28	200 200	2 19 18	54 90	ं ं २८००	0 0 0 1 2	े 4500 0	ं 1 3 0 0						
	31	0 38	12 7	08 S	0 27	0 0 31	C C	00						
31	е С	21 2 4	7 4 1日	2 2 60	89 0 2006	31 0 1 4	0 0	0 0 0						
	92 52	0	24 30	140 110	o o	$\circ$ $\circ$ $\circ$	0 2600	0 0 1 2						
<u>북국</u> 북북	- UAF	RNING - ROUNDAI ROUNDAI	ROUT	NODE	Ē	91, 6	-00 E	EXCEED	S THE	INFU		FE		
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4.7;	31 1 45	0 4	े २० २०	140 0 137	O	O	O	Ó						
45	4 44	э 0	ट ्ट	42 137	40 0	୍ ୁ ୁ	ن م	o o o	0	ୁଁ				
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54. 54. 54. 54		EUT IS RNING -												
	(; <b>1</b> t	HAS BE BUT IS	EN G	IVEN	ZERO	SATU	≎ATIO	V FLOU	4					
****	- UA	RHING - Has Pe							46					
		BUT IS												
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45	4	ALL (G	REEN		GE LE		5 ARE	THER			RED BY	,	0.821	
	45 19	2		200	1700	1 1		12	0 1500X	22				
47	47 51 4	3	18	100	1300		3600		1200G 1500X					
	44	t		45	0	0 0	2000		1400X	11				
***	- UA	RNING -	. <del>.</del> * * f	-×-1 Tt	1K	4.4	47							

# LIVNET. LPA 6/12/90

THE SATURN SUITE OF PROGRAMS

PROGRAM SR-7.1 SATURN ASSIGNENT PROGRAM SATASS

DATE 12/ 6/90 TIME 13:57:18

THE IMPUT SATURN MAG TAPE FILE IS FEAD FROM CHANNEL 1

HEADER DATA FROM THE MAG TAPE FILE READ FROM CHANNEL 1

RUM MAME LIVERPOOL MINI NETWORK, WARDROP EQUILIRRIUM, 1 USER CLASS

CREATED BY PROGRAM 81 DATE AND TIME OF CREATION 12/ 6/90 13/55/55

ke I.4 LISTING OF THE PARAM VALUES TAKEN Ô 5 MPIJA = MODET = MITA = 1 COMPAR = F TITLE = REGO = F F F F EXPERT = Т CCOUNT = FRINTF = F FRFIJA = MTFLOW = Т AMV ...... F F SUZIE = F SAVEIT = T PRTIJA = OUANTA =Т SUET = 0.20 PPM = 1.00 PPK = 0.00  $\mathsf{GONZO} = 1.00$ 

HEADER DATA FROM THE MAG TAPE FILE READ FROM CHANNEL 9

RIN NAME BUILD THE LIVERPOOL TRIP MATRIX

CREATED BY PROGRAM M1 DATE AND TIME OF CREATION 12/ 6/90 13/55/ 0

MATRIX TITLE - LIVERPOOL CENTRAL AREA C-D (TRAMP CORDON)

MATRIX SIZE - 24 ROUS 74 COLUMNS TYPE OF ELEMENTS (MTYPE) = 3 ELEMENT DIMENSIONS - TRIPS ELEMENT UNITS - VPH \*10\*\* 0

FILE ELEMENTS ARE WRITTEN AS REAL

## LISTING OF THE FLOWS ASSIGNED TO THE SELECTED LINKS

## N.B. THE ASSIGNED FLOWS ARE TOTAL FLOWS INCLUDING FIXED FLOWS

				المتعد والمرجوع بالمراجعة التراسية بالمرجوع والمرجوع والمرجوع المرجوع المرجوع المرجوع المرجوع المرجوع المرجوع	والذادي الزرجان والماري ويوبهما كالكارك الزائلا	مى زى الاستاد بارى بىرى بەر بەر بىرى <del>بىرى بىرى بىرى بىرى ب</del> ەر بىرى بىرى بىرى بىرى بىرى بىرى بىرى بى	and the subscription of the second	
LINK NO.	ANDOE	BNODE	CNODE	ASSIGNED FLOU	TARGET COUNT	DIFFERENCE (PCU/HR.)	WDIFF.	
					),			
t	1	58	O	714.0	1252.	578.0	42.97	:
a	58	1	Ô	235.0	779.	544.0	49.8D	1
3	46	47	O	250.7	100.	-150.7	-1E0.7E	1
4	49	48	0	292.1	200.	- 2 ega .1	-45.07	1
<b>E</b>	22	F.1	0	780.6	900.	119.4	13.27	1
6	45	53	52	106.9	826.	719.1	87.06	1
-7	32	33	Ö	1508.3	1500.	-8.3	-0.56	/
8	33	34	O	1392.4	1600.	-92.4	-5.78	/
ç	7	8	<u>о</u>	639.6	800.	110.4	13.80	1
10	tŌ	45	Ō	517.0	400.	-117.0	-29.25	1
11	45	21	0	981.0	1000.	19.0	1.90	1

COMPARISON OF THE ASSIGNED (SET 1) AND TARGET FLOWS (SET 2):

# 

TOTAL NUMBER OF ELEMENTS CONSIDERED 11

STATISTIC	SET 1	SET 2	DIFFERENCE
NUMBER OF ZEROS OR NEGATIVES SUM OF ELEMENTS AVERAGE ELEMENT STAMOARD DEVIATION COEFFICIENT OF VARIATION	0 7768. 706.15 494.82 0.7007	0 9357. 850.64 463.90 0.5454	-1589. -144.49 30.92 0.1554

REGRESSION OF SET 2 ELEMENTS (Y) AGAINST SET 1 (X)

EGUATION	A	B	R-SQUARED
Y = A + BX Standard Errors -	312.201 327.435	0.743 0.380	0.6615
A = HX		1.059	0.5123
Y = X			0.5003

-----

# LIVNETI. LPS 6/12/90

THE SATURN SUITE OF PROBRAMS

PROGRAM S3 -7.1 SATURN SIMULATION PROGRAM SATSIM

DATE 12/ 6/90 TIME 13:58:29

THE IMPUT SATURN FILE IS READ FROM CHANNEL 1

HEADER DATA FROM THE MAG TAPE FILE READ FROM CHANNEL 1

RUN MAME LIVERPOOL MINI NETWORK, WARDROP EQUILIBRIUM, 1 USER (1493

CREATED BY PROGRAM S2 DATE AND TIME OF CREATION 12/ 6/90 13/57/18

LISTING OF THE PARAMETERS USED

TITLE	÷	F	PRSFD		F	NOTUK	=	Ó
MODET	:=:	<u>.</u>	MASL		8	MITS	<b></b> :	1 O
ISTOP		90	LRTP		Ó	NOPD	<b>.</b>	$\odot$
TCEL		З.ОО	CAFMIN	1 =	ЗО.	ALEX		5.75

OUTPUT FROM SATSIM (SATURN SIMULATION) SIMULATION RUN NUMBER 1

ITERATION 1 - AVER. ARS. CHANGE = 131.79614 PCU/HR NO LINKS BLOCKING BACK

ITERATION 2 - AVER. ABS. CHANGE = 28.48292 PRU/HR

BLOCKING BACK CONVERGENCE STATISTICS: 1 LINKS WITH QUEUE GT STACK - TOTAL EXCESS POUS 70.46 0 LINKS WITH QUEUE IT STACK - TOTAL SPARE POUS 0.00 0 LINKS WITH QUEUE EQ STACK (TO +- 0.1 POU) 1 LINKS WITH BLOCKING BACK; SUM OF AMSOLUTE DIFFERENCES BETWEEN QUEUES AND STACKS 70.46 POUS. ITERATION 3 - AVER. ABS. CHANGE = 11.75938 POU/UR

BLOCKING BACK CONVERGENCE STATISTICS: 2 LINKS WITH QUEUE GT STACK - TOTAL EXCESS PCUS 152.96

O LINKS WITH QUEUE LT STACK - TOTAL SPARE POUS 0.00 O LINKS WITH QUEUE EQ STACK (TO +- 0.1 POU) 2 LINKS WITH BLOCKING BACK; SUM OF ABSOLUTE DIFFERENCES BETWEEN QUEUES AND STACKS 152.86 POUS.

يتبوو والارتجار المتروس والبيع وتتع

APPENDIX C

## , 1. User-Oriented Summary Statistics from Integration-1 Model

Drigin Zone	Destination Zone	Number of Arrivals	Average Trip Time (minutes)	iotot Trip Time (minutes)
1	2	150	14.8	2222.3
1	3	150	12.6	1890.7
1	4	150	4.9	738.6
1	5	150	6.4	951.3
1	6	150	9.1	1369.6
1	7	150	11.9	1781.7
2	· 1	150	14.0	2103.4
2	3	150	5.1	764.4
2	4	150	11.4	1/12.0
2	5	150	11.1	1664.9
2	6	150	8.6	1286.4
2	7	150	6.1	· 910.6
3	1	150	11.3	1701.2
3	2	150	4.7	697.9
3	4	675	3.8	5915.d
3	5	150	8.5	1266.3
3	6	150	6.3	944.5
3	7	150	5.2	774.6
4	1	150	4.8	712.1
4	2	150	12.3	1846.3
4	3	1350	9.8	13229.4
5	3	150	3.8	1317.9
5	4	150	4.7	701.7
6	3	150	6.7	998.7
á	4	150	6.2	931.7
7	3	150	5.0	745.2
7	4	150	7.9	1185.
	-			al trip Ilme = 50364. (839.41 hours
			Vehicles ento Vehicles who co	enter network = 577 ered network = 577 ompleted trip = 577 ft on network =

#### Table 2. System-Oriented Summary Statistics from Integration-1 Model

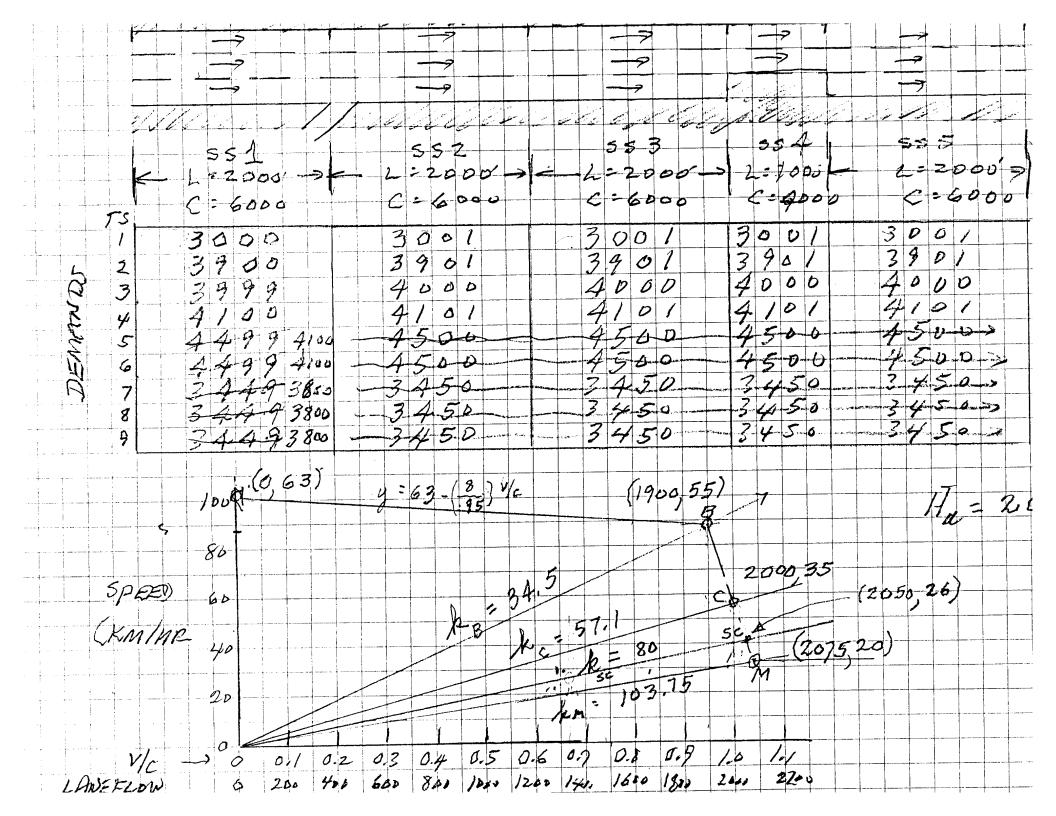
				Link	Summarie	s at Time	e: 10 minu	tes					
			Link					Noc	de	Link	V/C	Total	A
Num	Name	ĩγρ S	P	Speed (kpn)	Satur (vong)	Ln (#)	Lgth (m)	from (#)	to (#)	Fiow (vens)	ratio (#)	Time (min)	Ті (п
1	To-Zone 1	101	1	70.0	2000	2	1414	10	1	17	0.03	27	
2	Ta-Zone 2	101	1	70.0	2000	2	1414	14	2	17	0.03	27	
3	To-Zone 3	101	1	70.0	2000	2	1000	19	3	108	0.16	130	
4	To-Zone 4	101	1	70.0	2000	2	1000	15	4	82	0.12	101	
5	To-Zone S	101	1	70.0	2000	2	1000	11	5	20	0.03	24	
6	To-Zone 6	101	1	70.0	2000	2	1000	12	6	21	0.03	28	
7	To-Zone 7	101	1	70.0	2000	2	1000	13	7	27	0.04	30	
8	Fr-Zone 1	1	1	70.0	2000	2	1414	1	10	144	0.22	253	
9	Kingston Rd WB	1	1	60.0	1600	1	2236	11	10	4	0.01	16	4
10	1st Avenue NB	1	2	50.0	1400	2	1500	15	10	19	0.04	46	:
11	Fr-Zone 5	2	2	70.0	2000	2	1000	5	11	54	0.08	62	
12	Kingston Rd EB	2	1	60.0	1600	1	2236	10	11	45	0.16	163	3
13	Kingston Rd WB	2	1	60.0	1600	1	2000	12	11	0	0.00	0	C
14	2d Avenue NB	2	2	50.0	1400	1	500	16	11	25	0.11	30	1
15	Fr-Zone 6	3	2	70.0	2000	2	1000	6	12	54	0.08	61	1
16	Kingston Rd EB	3	1	60.0	1600	1	2000	11	12	10	0.04	26	2
17	Kingston Rd WB	3	1	60.0	1600	1	2000	13	12	9	0.03	23	2
18	3d Avenue NB	3	2	50.0	1400	1	500	17	12	14	0.06	13	C
19	Fr-Zone 7	4	2	70.0	2000	2	1000	7	13	54	0.08	62	1
20	Kingston Rd EB	4	1	60.0	1600	1	2000	12	13	0	0.00	4	C

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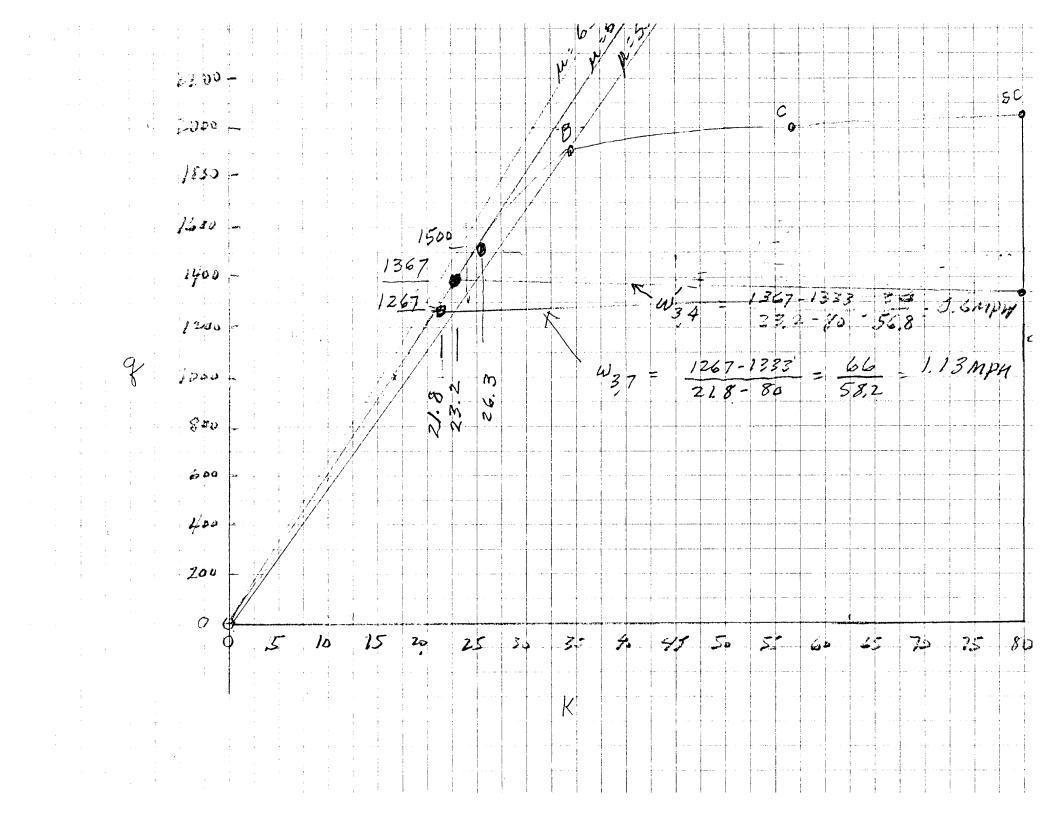
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APPENDIX D



SLOPE OF BC slope = 55-35 1200-2000 - 0.2 MPH/VEH 20 FLOW AT Vy 5/yr = 35-20 \_ - 0.2 2000 - PM  $2000 - P_{14} = 15$ -0.2  $Q_{M} = 2000 + \frac{15}{0.2} = 2000 + 75$ Pm = 2075 DENSITIES AT (B) (AND (A) k = 1900 -34.5 opmal 5% Appropri  $k_{c} = 2000 = 35$ hy = 2075 20 = 103.75 sprayl STORAGE MAL = <u>5280</u> 65,516 5280 A = 5280 3.2808 FTd \_ 80 3.2808×20 Vpm

551 L=2000 C=6000	552 L=2000 C=600	55 3 L=2000 E=6000	S= 4 L= 100 C- 4000	SS 5 2=2000 C-4000
3000 - 0.5 59 6000	3 DN/ 20. 5 (59) 6000	3001 2.5 (59) 6000	2001 3.75 57 4000	300/ D.5 (5) 6000
3900 0.65 58) 6000	3301 - 0.65 (38) 6000	2901 0.65 58 5000	الإيجاب المتعلمين المرابعة المستكنين والمتعادين والمعارين المرابي المرابي المرابي المرابي المرابي المرابي المرا	3401 J. 65 3 6000
3194 0.67 50	4000 0.67 5D	4000 . 5. 57 57 5000	4000 1.00 33 2000	6020 - 0.675
4100 = 0. 18 57 6000	4,01 0.68 57)	5000 - 57 - 4000 6000 - 57 - 4000	4101 = 1.00 33 - 4100 =	6000 6767
4100 0,68 (57)	4701 0.68 (57) 6000	4701 - 167 600 - (7) (50) - 1584 1	401 4201 33	41514201 40 5000 . 67 5
4100 - 0.68 37) 6010	6000 (5)	4100	+2.00+ 4705 4000 1.0 4000 35	+200 <u>+411908</u> 4300, 60
- 800 - 0.63 (58) 6000	5000 58	3800 23767 330 6000 (7) 58)	4000 (35)	380073041000,6 6000 (57
<u>3800</u> - 062 6000 (53)	3800 62 6000 58	380. 67 00,00	3900 U.975 4000 (44)	3850 3900 0 65 6000 58
3860 0,53	3800.63	3800. 63 6000 58	3800 0.95 7001 (55)	3800 D. 63 4000 55



APPENDIX E

1C O N T I N U O U S TR AF F IC AS S I G N M E N T M O D E L V E R S I O N 5 CONTRAM 5.14 (16. 4.91) RUN ON 11/6/91 TRANSPORT AND ROAD RESEARCH LABORATORY (DTP) CROUTHORNE, RG116AU, ENGLAND = TRAFFIC GROUP, 0344-770494 = CROWN COPYRIGHT 1990

#### NETWORK AND TIME DATA

SMART CORRIDOR BASE RUN NETWORK and TIME DATA (6/11/91)

53 \_ 54

SINARI	CORRI	JUR DAS				ATA (0/1	1/91)									
CARD	(ті	ME)	DEFINITI	ON OF TI	ME SLICE	S IN SIM	ULATION	PERIOD (	24 HOUF	R CLOCK	)					
TYPE		NIT)		ICE NUMB				- (								
	<b>\</b> -	,	1	2	3	4	5	6	7	8	9	10	11	12	13	
1		1	600	630	700	730	800	830	900	930 1	000	1300	0	0	0	0
					<b>T</b> O <b>F</b> 1											
CARD TYPE		ORIGIN NUMBER		EEDS UP ETTERS DE												
TTPE		NUMBER	(Ľ		NOTE DAM		EMENTS)									
3		5001	7	0	0	0	0									
3		5002		5304	158	128	0									
3		5003		4804	4603	157	0									
3		5004	4607	4105	4106	0	0									
3		5005	4203	7607	3505	3506	0									
3		5006	3603	3610	4107	3005	3011									
3		5007	3103	3110	3507	3508	2505									
3		5008	2603	2610	3007	2005	2006									
3		5009	2103	2110	2507	2508	1505									
3		5010	1603	2007	2008	905	0									
3		5011	1003	1010	1507	205	211									
3		5012	80	82	83	0	0									
3		5013	81	84	0	0	0									
3		5014	50	0	0	0	0									
3		5015	907	908	303	304	0									
3		5016	202	209	703	704	0									
3		5017	301	309	1307	1308	0									
3		5018	8001	705	1807	1808	0									
3		5019	1701	1305	1306	2307	0									
3		5020	2201	2209	1805	1806	2807									
3		5021	2701	2709	2305	2306	3307									
3		5022	3201	2805	2806	3807	0									
3		5023	3701	3709	3305	3306	4407									
3		5024	4201	3805	3806	4907	0									
3		5025	4405	4406	5307 0	4801 0	4809 0									
3		5026	4905	128	U	U	U									
UNCO	NTROL	LED	FE	EEDS UP	TO 5	LINKS (	OR	CRUISE	LENGTH	SAT/N	STORE	JUNCTION			% DELAY	
	) SET	LINK		ESTINATION				TIME		FLOW		NUMBER				
TYPE		NUMBER		ETTERS DE		INED MOV	EMENTS)		(METRS)	(PCU/H)						
4	1	50	51	0	0	0	0	86V	732	10500	139	136				
4	1	51	52	0	0	0	0	86V	387	10300	100	137				
4	1	52	53	1101	0	0	0	86V	320	12000	96	138				
	-			•	•	•	•	0411	225	11400	05					

86V

86V

86V

86V

86V

86V

86V

335 11400 95

122 10900 33

518 12500

290 11300

488 10300

4	1	60	61	3107	0	0	0	86V	183	9900	45	146
4	1	61	62	0	0	0	0	86V	579	9450	137	147
4	1	62	63	3607	0	0	0	86V	899	11550	260	148
4	1	63	64	0	0	0	0	86V	655	9500	156	149
4	1	64	65	4207	0	0	0	86V	930	8800	205	150
4	1	65	66	0	0	0	0	86V	198	9100	45	151
4	1	66	67	0	0	0	0	86V	101	9600	24	152
4	1	67	68	0	0	0	0	86V	472	9100	107	153
4	1	68	69	4601	0	0	0	86V	899	9150	206	154
4	1	69	70	0	0	0	0	86V	290	9100	66	155
4	1	70	71	0	0	0	0	86V	732	7600	139	156
4	1	71	72	0	0	0	0	86V	533	7550	101	157
4	1	72	9001	0	0	0	0	86V	701	9500	166	158
4	1	7	a	5305	5311	0	0	86V	853	15000	469	107
4	1	8	9	0	0	0	0	86V	335	8700	3500	108
4	1	9	10	5205	0	0	0	86V	122	9200	28	109
4	1	10	11	4805	0	0	0	86V	152	8600	33	110
4	1	11	12	0	0	0	0	86V	457	9000	103	111
4	1	12	13	0	0	0	0	86V	518	9300	120	112
4	1	13	14	4305	0	0	0	86V	1204	8000	241	113
4	1	14	15	0	0	0	0	86V	183	8100	37	114
4	1	15	16	4205	0	0	0	86V	122	9000	27	115
4	1	16	17	0	0	0	0	86V	442	8500	94	116
4	1	17	18	3705	0	0	0	86V	671	9500	159	117
4	1	18	19	0	0	0	0	86V	701	9450	166	118
4	1	19	20	3205	0	0	0	86V	884	10900	241	119
4	1	20	21	0	0	0	0	86V	366	9500	87	120
4	1	21	22	2705	0	0	0	86V	320	10100	81	121
4	1	22	23	0	0	0	0	86V	655	12100	198	122
4	1	23	24	2205	0	0	0	86V	335	12100	101	123
4	1	24	25	0	0	0	0	86V	457	10300	118	124
4	1	25	26	1705	0	0	0	86V	305	11900	91	125
4	1	26	27	0	0	0	0	86V	579	12500	181	126
4	1	27	28	1205	0	0	0	86V	213	11350	60	127
4	1	28	29	0	0	0	0	86V	472	8500	120	128
4	1	29	30	85	0	0	0	86V	213	9850	52	129
4	1	30	31	86	0	0	0	86V	290	9000	65	130
4	1	31	32	0	0	0	0	86V	274	7500	51	131
4	1	32	9014	0	0	0	0	86V	213	9300	50	132
4	1	80	9013	0	0	0	0	86V	700	7600	462E	160
4	1	81	9012	0	0	0	0	86V	700	7600	462E	161

SIGNAL CARD	ISED . SET	 LINK		EDS UP STINATIO		LINKS OR		CRUISE TIME	LENGTH	SAT/N FLOW	STORE CAP.	SIGNAL/ JUNCTION	STAGES UHEN	% GREEN % DELAY
TYPE		NUMBER	(L)	ETTERS D	ENOTE BAN	NNED MOVEME	NTS)	(SECS)	(METRS)	(PCU/H)	(PCUS)	NUMBER	GREEN	
6	2	705	301	309	9017	0	0	55v	837	2778	202E	7	1	
												-	1	
6	2	1305	705	0	0	0	0	55v	732	5100	324E	13	1	
6	2	1306	8001	0	0	0	0	55v	732	900	57E	13	1	
6	2	1307	1807	1808	0	0	0	55v	837	5100	371E	13	1	
6	2	1308	9018	0	0	0	0	55v	837	1000	72E	13	1	
6	2	1805	1305	1306	9019	0	0	55v	804	3400	237E	18	1	
6	2	1806	1701	0	0	0	0	55v	804	900	62E	18	1	
6	2	1807	2307	2308	0	0	0	55v	719	3400	212E	18	1	
6	2	1808	9019	0	0	0	0	55v	719	500	31E	18	1	
6	2	2305	1805	1806	9020	0	0	55v	815	3400	240E	23	1	
6	2	2306	2201	2209	0	0	0	55 <b>v</b>	815	875	62E	23	1	
6	2	2307	2807	2808	0	0	0	55 <b>v</b>	658	3400	194E	23	1	
6	2	2308	9020	0	0	0	0	55 <del>v</del>	658	675	38E	23	1	

6	2	2805	2305	2306	0	0	0	55 <del>v</del>	802	3400	237E	28	2
6	2	2806	2701	2709	0	0	0	55 <del>v</del>	802	700	48E	28	2
6	2	2807	3307	3308	0	0	0	55v	815	3400	240E	28	2
6	2	2808	9021	0	0	0	0	55 <del>v</del>	815	600	42E	28	2
6	2	3305	2805	2806	9022	0	0	55 <del>v</del>	1591	3400	470E	33	1
6	2	3306	3201	0	0	0	0	55 <del>v</del>	1591	955	132E	33	1
6	2	3307	3807	3808	0	0	0	55v	802	3400	237E	33	1
6	2	3308	9022	0	0	0	0	55v	802	1140	79E	33	1
6	2	3805	3305	3306	0	0	0	55v	1478	3400	436E	38	2
6	2	3806	3701	3709	0 0	0	0 0	55v	1478	600	77E	38	2
6	2	3807	4407	4408	0	0	0	55v 55v	1591 1591	3400	470E	38	2
6 6	2 2	3808 4405	9023 3805	0 3806	9024	0	0	55v	1829	825 3400	114E 540E	38 44	2
6	2	4405	4201	0	9024 0	0	0	55v	1829	600	95E	44	2 2
6 6	2	4408	4201	4908	0	0	0	55v	1478	3400	436E	44	2
6	2	4407	4907 9024	4908	0	0	0	55v	1478	975	430L 125E	44	2
6	2	4907	5307	5308	0	ů O	0	55v	1829	3400	540E	49	2
6	2	4908	9025	0	0	0	0	55v	1829	1155	183E	49	2
6	3	205	9015	0	0	0	0	55v	1272	5100	564E	2	1
6	3	206	9015	0	0	0	0	55v	1272	500	55E	2	1
6	3	211	303	304	0	0	0	55v	1272	1450	160E	2	1
6	3	905	206	205	211	0	0	55v	692	5100	306E	9	1
6	3	906	9011	0	0	0	0	55v	692	825	49E	9	1
6	3	907	1507	1508	0	0	0	55 <del>v</del>	1201	5100	532E	9	1
6	3	908	1003	1010	0	0	0	55 <del>v</del>	1201	1600	167E	9	1
6	3	1505	906	905	0	0	0	55v	814	3400	240E	15	2
6	3	1506	9010	0	0	0	0	55v	814	800	56E	15	2
6	3	1507	2007	2008	0	0	0	55v	692	3400	204E	15	2
6	3	1508	1603	0	0	0	0	55 <b>v</b>	692	1600	96E	15	2
6	3	2005	1505	1506	0	0	0	55v	796	3400	235E	20	1
6	3	2006	9009	0	0	0	0	55v	796	800	55E	20	1
6	3	2007	2507	2508	9009	0	0	55v	814	3400	240E	20	1
6	3	2008	2103	2110	0	0	0	55v	814	500	35E	20	1
6	3	2505	2006	2005	0	0	0	55 <b>v</b>	805	3400	238E	25	2
6	3	2506	9008	0	0	0	0	55v	805	650	45E	25	2
6	3	2507	3007	9008	0	0	0	55v	796	3400	235E	25	2
6	3	2508	2603	2610	0	0	0	55 <b>v</b>	796	500	34E	25	2
6	3	3005	2506	2505	0	0	0	55v	1234	3400	364E	30	1
6	3	3006	9007	0	0	0	0	55v	1234	536	57E	30	1
6	3	3007	3507	3508	0	0	0	56V	805	2600	182E	30	1
6	3	3011	3103	3110	0	0	0	55v	1234	1450	155E	30	1
6	3	3505	3005	3006	3011	0	0	55 <b>v</b>	1526	5100	676E	35	2
6	3	3506	9006	0	0	0	0	55v	1526	500	66E	35	2
6	3	3507	4107	4108	9006	0	0	55 <del>v</del>	1164	5100	516E	35	2
6	3	3508	3603	3610	0	0	0	55v	1164	625	63E	35	2
6	3	4105	3506	3505	0	0	0	55v	1280	3400	378E	41	3
6	3	4106	9005	0	0	0 0	0 0	55v	1280	500	55E	41	3
6	3	4107	7612	7607 0	0	0	0	55v 55v	1303 1303	3400	385E	41	3
6 6	3 3	4108 4605	4203 7606	7605	0	0	0	55v	227	875 5100	99E 100E	41 46	3
6	3	4605	4707	000	0	0	0	55v	227	575	11E	46	1 1
6	3	4606	4707	4807	4808	0	0	55v	792	5100	351E	46 46	1
6	3	4807	4903	4807	4808	4601	0	55v	300	3400	2000	46	2
6	3	4807	4701	4702	4510	4001	0	55v	213	3400	62E	48	2
6	3	4808	4903	4904	4910	0	0	55v	213	1600	29E	48	2
6	3	7605	4106	4105	9004	0	0	55v	792	5100	351E	<b>4</b> 0 76	1
6	3	7606	9004	0	0	0	0	55v	792	740	50E	76	1
6	3	7607	4607	0	0	0	0	55v	1280	5100	567E	76	1
6	3	7612	9004	0	0	0	0	55v	1280	1450	161E	76	1
6	4	1501	905	906	9010	0	0	55v	280	3400	82E	15	1

6	4	1502	2007	2008	0	0	0	55V	280	500	12E	15	1
6	4	1601	1501	1502	0	0	0	55V	50	5100	22E	16	
6	4	1602	151	0	0	0	0	55V	50	3200	13E	16	2
6	4	1603	1703	1704	151	0	0	55V	280	5100	124E	16	1
6	4	1607	1501	1502	1703	1704	151	55V	250	3400	2000	16	3
6	4	1701	1601	1602	121	0	0	55V	1330	5100	589E	17	
6	4	1703	1803	1804	0	0	0	55V	165	5100	73E	17	1
6	4	1704	121	0	0	0	0	55V	165	1600	22E	17	2
6	4	1705	1803	1804	1601	1602	121	55V	250	3400	2000	17	3
6	4	1803	2307	2308	9019	0	0	55V	1330	3400	393E	18	2
6	4	1803	1305	1306	0	ů O	ů 0	55V	1330	500	57E	18	2
					0			55V					
6	4	2001	9009	, 0	-	0	0		860	3400	254E	20	2
6	4	2002	2507	2508	0	0	0	55V	860	500	37E	20	2
6	4	2009	1505	1506	0	0	0	55V	860	1450	108E	20	2
6	4	2101	2001	2002	2009	0	0	55V	360	3400	106E	21	2
6	4	2102	152	0	0	0	0	55V	360	1600	50E	21	1
6	4	2103	2203	2204	0	0	0	55V	860	3400	254E	21	2
6	4	2107	2203	2204	2001	2002	2009	55V	240	3400	2000	21	3
6	4	2110	152	0	0	0	0	55V	860	1450	108E	21	2
6	4	2201	2101	2102	0	0	0	55V	1390	3400	410E	22	2
6	4	2203	2303	2304	0	0	0	55V	360	3400	106E	22	2
6	4	2204	122	0	0	0	0	55V	360	1800	56E	22	1
6	4	2205	2303	2304	2101	2102	122	55V	240	3400	2000	22	3
6	4	2209	122	0	0	0	0	55v	1390	1450	175E	22	2
6	4	2303	2807	2808	9020	0	0	55V	1390	3400	410E	23	2
					0	0	0	55V	1390	500			
6	4	2304	1805	1806		0	0	55V	820		60E	23	2
6	4	2501	2005	2006	9008					3400	242E	25	1
6	4	2502	3007	0	0	0	0	55V	820	500	35E	25	
6	4	2601	2501	2502	0	0	0	55V	400	3400	118E	26	_
6	4	2602	153	0	0	0	0	55V	400	1600	55E	26	3
6	4	2603	2703	2704	0	0	0	55V	820	3400	242E	26	1
6	4	2607	2703	2704	2501	2502	153	55V	330	3400	2000	26	2
6	4	2610	153	0	0	0	0	55V.	820	1450	103E	26	1
6	4	2701	2601	2602	0	0	0	55V	1400	5100	620E	27	1
6	4	2703	2803	2804	2810	0	0	55V	400	3400	118E	27	1
6	4	2704	123	0	0	0	0	55V	400	1600	55E	27	3
6	4	2705	2803	2804	2810	2601	2602	55V	330	3400	2000	27	2
6	4	2709	123	0	0	0	0	55V	1400	1450	176E	27	
6	4	2803	9021	0	0	0	0	55V	1400	3400	413E	28	
6	4	2804	2305	2306	0	0	0	55V	1400	500	60E	28	
6	4	2810	3307	3308	0	0	0	55V	427	1450	53E	28	
6	4	3001	2505	2506	3507	3508	9007	55V	1076	3400	318E	30	2
6	4	3101	3001	2500	0	0	0	55V	300	3400	88E	31	2
6	4			0	0	0	0	55V	300	1600	41E		۴.,
		3102	154					55V				31	2
6	4	3103	3203	3204	0	0	0		1076	3400	318E	31	2
6	4	3107	3203	3204	3001	154	0	55V	240	3400	2000	31	3
6	4	3110	154	0	0	0	0	55V	1076	1450	135E	31	2
6	4	3201	3101	3102	124	0	0	55V	1280	3400	378E	32	1
6	4	3203	3303	0	0	0	0	55v	300	3400	88E	32	
6	4	3204	124	0	0	0	0	55V	300	1600	41E	32	1
6	4	3205	3303	3101	3102	124	0	55V	240	3400	2000	32	3
6	4	3303	3807	3808	2805	2806	9022	55V	1280	3215	357E	33	2
6	4	3501	3005	3006	3011	9006	0	55V	1750	5100	776E	35	1
6	4	3502	4107	4108	0	0	0	55V	1750	500	76E	35	
6	4	3601	3501	3502	0	0	0	55V	360	5100	159E	36	1
6	4	3602	155	0	0	0	0	55V	360	1600	50E	36	3
6	4	3603	3703	3704	0	0	0	55V	1750	5100	776E	36	
6	4	3607	3703	3704	3501	3502	155	55V	300	4200	2000	36	2
6	4	3610	155	0	0	0	0	55V	1750	1450	2000 220E	36	1
6	4	3701	3601	3602	0	0	ů	55V	805	6800	476E	30	2
U	-	5701	3301	2002	v	U	v	•	555	5500		51	4

6	4	3703	3803	3804	0	0	0	55V	360	5100	159E	37	2
6	4	3704	125	0	0	0	0	55V	360	1800	56E	37	1
6	4	3705	3601	3602	3803	3804	125	55V	300	3400	2000	37	3
6	4	3709	125	0	0	0	0	55V	805	1600	112E	37	2
6	4	3803	4407	4408	9023	0	0	55v	805	5100	357E	38	1
6	4	3804	3305	3306	0	0	0	55V	805	500	35E	38	1
6	4	4101	3505	3506	9005	0	0	55V	1733	5100	768E	41	1
6	4	4102	7607	7612	0	0	0	55V	1733	1600	241E	41	2
6	4	4201	4101	4102	156	0	0	55V	595	5100	263E	42	1
6	4	4203	4303	156	a7	0	0	55V	1733	5100	768E	42	1
6	4	4205	4101	4102	0	0	0	55V	300	3400	2000	42	3
6	4	4207	4101	4102	4303	156	0	55V	500	3400	2000	42	3
6	4	4303	4403	4404	126	0	0	55V	490	6800	289E	43	1
6	4	4305	4403	4404	126	0	0	55V	300	3400	2000	43	2
6	4	4403	4907	4908	9024	0	0	55V	105	5100	46E	44	1
6	4	4404	3805	3806	0	0	0	55V	105	500	4E	44	1
6	5	901	9011	0	0	0	0	55V	212	3400	62E	9	2
6	5	902	1507	1508	0	0	0	55V	212	500	9E	9	2
6	5	909	205	206	211	0	0	55V	212	1700	31E	9	2
6	5	1001	901	902	909	0	0	55V	169	3400	49E	10	2
6	5	1002	1108	0	0	0	0	55V	169	1600	23E	10	1
6	5	1003	1203	1204	0	0	0	55V	212	3400	62E	10	2
6	5	1005	1203	1204	901	902	909	55V	165	3400	48E	10	3
6	5	1010	1108	0	0	0	0	55V	212	1450	26E	10	2
6	5	1101	1005	150	0	0	0	55V	200	3400	2000	11	2
6	5	1108	150	0	0	0	0	55V	165	1325	19E	11	1
6	5	1201	1001	1002	120	0	0	55V	151	5100	66E	12	2
6	5	1203	7803	0	0	0	0	55V	169	5100	74E	12	1
6	5	1204	120	0	0	0	0	55V	169	1600	23E	12	1
6	5	1205	1001	1002	7803	0	0	55V	220	3200	2000	12	3
6	5	1303	9018	0	0	0	0	55V	298	3400	88E	13	2
6	5	1304	705	0	0	0	0	55V	298	1050	27E	13	2
6	5	1310	1807	1808	0	0	0	55V	298	1450	37E	13	2
6	5	7801	1201	0	0	0	0	55V	97	3400	28E	78	1
6	5	7803	8003	0	0	0	0	55V	151	3400	44E	78	1
6	5	8001	7801	0	0	0	0	55V	298	3400	88E	80	1
6	5	8003	1303	1304	1310	0	0	55V	97	3400	28E	80	1
6	6	4601	4807	4808	4707	7605	0	55V	250	3400	2000	46	3
6	6	4603	7605	7606	4807	4808	0	55V	152	3400	44E	46	3
6	6	4701	4603	9003	0	0	0	55V	140	3400	41E	47	1
6	6	4702	157	0	0	0	0	55V	140	660	8E	47	1
6	6	4707		4804	157	9003	0	55V	152	3400	44E	47	2
6	6	4801	4701	4702	0	0	0	55V	213	3400	62E	48	4
6	6	4803	4903	4904	4910	0	0	55V	140	3400	41E	48	4
6	6	4804	4605	4606	127	0	0	55V	140	1600	19E	48	4
6	6	4809	4605	4606	127	0	0	55V	213	1450	26E	48	4
6	6	4903	9025	0	0	0	0	55V	213	3400	62E	49	1
6	6	4904	4405	4406	0	0	0	55V	213	500	9E	49	1
6	6	4905	4801	4405	4406	9025	0	55V	427	3235	120E	49	2
6	6	4910	5307	5308	0	0	0	55V	213	1450	26E	49	1
6	6	5201	9002	0	0	0	0	55V	210	5100	93E	52	3
6	6	5202	158	0	0	0	0	55V	210	1600	29E	52	3
6	6	5205	9002	0	0	0	0	55V	500	3400	2000	52	3
6	6	5303		9026	0	0	0	55V	210	5100	93E	53	1
6	6	5304	128	0	0	0	0	55V	210	500	95E	53	1
6	6	5307	5201	5202	0	0	0	55V	427	5100	189E	53	3
6	6	5308	9026	0	0	0	0	55V	427	1600	59E	53	3
6	6	5305	5201	5202	4905	128	0	55V	350	3400	2000	53	3
6	6	5311	9026	0	4905 0	0	0	55V	350	1450	2000	53	3
6	7	202	9020	908	0	0	0	55V	457	3400	135E	2	2
5	,	202	307	500	v	v	v		-57	5-00	1005	4	4

6	7	209	9015	0	0	0	0	55v	457	1450	57E	2	2
6	7	301	202	209	0	0	0	55v	334	1450 5100	57E	2 3	2
6	, 7	301	703	209 704	0	0	0	55v	457	5100	202E	3	1
6	, 7	304	9016	,04 0	0	0	0	55v	457	500	19E	3	I
6	7	304	9016 9016	0	0	0	0	55v	334	1450	19E 42E	3	
6	, 7	703	1307	1308	9017	0	0	55v	334	5100	148E	7	2
6	7	704	9017	0	0	0	0	55v	334	500	14E	7	2
4	8	82	51	0	0	0	0	86V	300	9000	234E	136	-
4	8	83	32	0	0	0	0	86V	500	9000	391E	131	
4	8	84	52	0	0	0	0	86V	500	9000	391E	137	
4	8	85	9013	0	0	0	0	86V	300	9000	2000	160	
4	8	86	9012	0	0	0	0	86V	500	9000	2000	161	
4	8	87	15	0	0	0	0	86V	200	9000	156E	114	
6	8	120	29	0	0	0	0	5ov	200	3400	59E	128	
6	8	121	27	0	0	0	0	5ov	250	3400	73E	126	
6	8	122	25	0	0	0	0	50 <b>v</b>	250	3400	73E	124	1
6	8	123	23	0	0	0	0	50 <b>v</b>	300	3400	88E	122	
6	8	124	21	0	0	0	0	5ov	250	3400	73E	120	1
6	8	125	19	0	0	0	0	5ov	300	3400	88E	118	1
6	8	126	17	0	0	0	0	5ov	300	3400	<b>8</b> 8E	116	1
6	8	127	13	0	0	0	0	5ov	400	3400	118E	112	1
6	8	128	9	0	0	0	0	5ov	400	3400	118E	108	
6	8	150	54	0	0	0	0	50V	200	3400	59E	139	
6	8	151	56	0	0	0	0	5ov	250	3400	73E	141	
6	8	152	58	0	0	0	0	5ov	250	3400	73E	143	1
6	8	153	60	0	0	0	0	5ov	300	3400	88E	145	
6	8	154	62	0	0	0	0	5ov	250	3400	73E	147	1
6	8	155	64	0	0	0	0	5ov	300	3400	88E	149	1
6	8	156	68	0	0	0	0	5ov	300	3400	88E	153	
6	8	157	71	0	0	0	0	5ov	350	3400	103E	156	
6	8	158	72	0	0	0	0	5ov	300	3400	88E	157	1
FLAGS:-	V =	SPEED	IN KM/H,	, SF =	LANES*100	0 + SPEE	D/FLOW	NUMBER,	E = ES	STIMATED	STORAGE	CAPACITY,	D = DEPARTURES,

CARD	VEH		F	UEL COEFFICIE	INTS		
TYPE	CLASS		CRUISE	E	WEIGHT	EFFI	CIENCY
		A	В	C	м	EI	E2
		(ML/M)	(ML/S	)(ML/MV**2)	(T)	(ML	/KJ)
D/F	C	0.024	0.361	0.000057	1.080	0.087	0.025
D/F	В	-0.040	2.272	0.000334	8.000	0.074	0.025
D/F	L	-0.040	2.272	0.000334	5.000	0.074	0.025

CARD	PCUS PE	R CLASS		CRUISE 1	IMES (%	CAR VALUE)
TYPE	CAR	В	L	CAR	В	L
D/F	1.0	2.0	1.5	100	100	100

### NETWORK COMPOSITION DEDUCED FROM DATA:

57	UNCONTROLLED LINKS	)	
0	GIVE-WAY LINKS	)	TOTAL OF 275 LINKS OF ALL TYPES
218	SIGNALISED LINKS	)	
41	SIGNAL JUNCTIONS		TOTAL OF 92 JUNCTIONS OF ALL TYPES
NO. OF O	RIGINS	26	NO. OF DESTINATIONS 26

#### OTOTAL VEHICLE FLOW RATES FROM EACH ORIGIN DURING EACH TIME SLICE (VEH/H) FLOWS

ORIGINS

LAST TIME SLICE WITH NON-ZERO O-D DEMAND LENGTH OF "BUSY PERIOD" IN MINUTES ESTIMATED TOTAL DEMAND (VEHICLES)

ONUMBER OF ORIGIN-DESTINATION (O-D) CARDS

OTOTAL VEHICLE FLOW RATES ENTERING THE NETWORK DURING EACH TIME SLICE (VEH/H)

10542 27602 34268 34306 26354 19618 13816 10552

SMART	CORRIDO	R BASE	RUN NETW	опк and т	IME DATA	(6/11/9	21)				
SMART	CORRIDO	R BASE	DEMAND								
SMART	CORRIDO	R C	CONTROL DA	ATA							
											ITERATION NUMBER 3
		TIME S	LICES :								
LINK		1	2	3	4	5	6	7	8	9	
NO.&											MEAN
TYPE											QUEUE TIME
	600	630	700	730	800	830	900	930	1000	1300	
7u		35	35	35	35	35	35	35	35	0	35
80		14	14	15	33	31	14	14	14	0	20
9u		5	5	7	14	8	5	5	5	0	7
IOU		6	6	7	10	8	7	6	6	0	7
110		19	19	24	35	27	21	19	19	0	24
12U		21	21	27	41	32	24	21	21	21	28
13u		50	-50	104	170	163	73	50	50	50	100
14U		7	7	10	23	27	7	7	7	7	13
15U		5	5	5	5	5	5	5	5	5	5
16U		18	18	18	18	18	18	18	18	18	18
17U		28	28	28	28	28	28	28	28	28	28
18U		29	29	29	29	29	29	29	29	29	29
190		37	37	37	37	37	37	37	37	37	37

LINK-BY-LINK ALL-TIME-SLICES - MEAN TRAVEL TIMES PER VEHICLE (SEC)

1

run on 11/6/91

200	15	15	15	15	15	15	15	15	15
210	13	13	27	14	14	13	13	13	13
22u	27	27	27	31	33	29	27	27	27
230	14	14	14	19	18	15	14	14	14
240	19	19	19	25	29	21	19	19	19
25U	12	12	13	23	23	14	12	12	12
260	24	24	31	44	43	27	24	24	24
27U	8	8	10	12	19	11	8	8	8
28U	19	19	44	84	86	75	21	19	19
290	8	8	8	8	8	8	8	8	8
3ou	12	12	12	12	12	12	12	12	12
31u	11	11	11	11	11	11	11	11	11
32U	8	8	8	8	8	8	8	8	8
5ou	30	30	30	30	30	30	30	30	0
51u	16	16	16	16	16	16	16	16	0
52U	13	13	13	13	13	13	13	13	0
53u	14	14	14	14	14	14	14	14	14
54u	5	5	5	5	5	5	5	5	5
55u	21	21	21	21	21	21	21	21	21
56U	12	12	12	12	12	12	12	12	12
57U	20	20	20	22	22	20	20	20	20
58U	7	7	17	25	8	7	7	7	7
590	28	28	28	29	28	28	28	28	28
60U	7	7	15	26	8	7	7	7	7
61U	24	24	29	33	29	24	24	24	24
62U	37	37	37	52	48	40	37	37	37
63U	27	27	32	42	39	30	27	27	27
64U	38	38	80	119	93	49	38	38	38
65U	8	8	8	8	14	8	8	8	8
66U	4	4	4	4	12	4	4	4	4
67U	19	19	19	30	34	21	19	19	19
68U	37	37	38	61	91	59	37	37	37
69U	12	12	14	20	24	12	12	12	12
7ou	30	30	37	62	75	54	32	30	30
70u 71u	22	22	51	90	102	93	27	22	22
72U	29	29	29	29	29	29	29	29	29
80U	29	29	29	29	29	29	29	29	0
81U	29	29	29	29	29	29	29	29	0
82U	12	12	12	12	12	12	12	12	0
820 830	20	20	20	20	20	20	20	20	0
830 84U	20	20	20	20	20	20	20	20	0
85U 84U	12	12	12	12	12	12	12	12	12
86U	20	20	20	20	20	20	20	20	20
87U	8	8	8	8	8	8	8	8	0
120s	14	14	14	14	14	14	14	14	0
121s	18	18	30	88	98	18	18	18	0
122s	18	18	20	59	54	21	18	18	0
123\$	21	21	21	30	34	21	21	21	0
1245	18	18	18	18	18	18	18	18	18
125S	21	21	21	21	21	21	21	21	21
126S	0	21	21	21	21	0	0	0	0
127S	28	28	28	32	37	28	28	28	0
128S	28	28	32	82	55	28	28	28	0
150s	14	14	14	14	14	14	14	14	0
151s	18	18	18	18	18	18	18	18	0
152S	18	18	18	18	18	18	18	18	0
153s	21	21	21	22	21	21	21	21	0
154s	18	18	18	37	20	18	18	18	0
155s	21	21	41	41	41	24	21	21	0
1565	21	21	21	73	95	33	21	21	0
	61			.5					U U

157s	25	25	85	230	292	79	27	25	0
158S	21	21	21	21	21	21	21	21	0
202s	38	38	38	40	40	38	38	38	0
205s	92	92	93	93	92	92	92	92	92
206s	0	0	87	92	90	0	0	0	0
209S	38	38	38	38	38	38	38	38	0
211s	92	93	94	97	97	93	92	92	0
301s	26	26	26	26	26	26	26	26	0
303s	34	34	34	34	34	34	34	34	0
304s	34	35	35	37	37	34	34	34	0
309s	26	26	26	26	26	26	26	26	26
703s	28	28	, 28	28	28	28	28	28	0
704s	0	0	0	21	25	0	0	0	0
705s	66	67	69	77	73	67	66	66	65
901s	22	23	23	23	22	23	22	22	22
902S	22	22	23	24	22	22	22	22	0
905s	54	54	54	55	55	54	54	54	0
906S	54	57	61	77	100	62	55	54	0
907s	87	87	87	87	87	87	87	87	0
908s	87	88	88	95	100	89	87	87	0
909s	23	24	24	24	23	23	23	23	22
1001s	18	19	19	18	18	19	18	18	18
1002s	31	39	42	43	42	39	32	31	0
1003s	20	20	20	21	21	20	20	20	0
1005s	52	123	207	228	117	83	62	52	0
1010s	20	21	21	20	20	20	20	20	0
1101s	35	37	37	36	35	35	35	35	0
1108S	13	14	15	14	15	14	13	13	0
1201s	27	28	30	32	31	28	27	27	0
1203s	24	24	24	24	24	24	24	24	0
1204s	25	26	26	37	83	60	24	25	0
1205s	29	33	37	31	30	33	30	29	27
1303s	28	28	28	28	28	28	28	28	0
1304s	30	34	37	32	30	32	31	30	28
1305s	56		56	57	57	56	56	56	0
1306s	56	57	132	195	211	76	56	56	0
1307s	63	63	63	63	63	63	63	63	0
1308s	63	63	63	64	64	63	63	63	0
1310s	0	28	28	28	28	28	0	0	0
1501s	24	28	29	30	30	28	25	25	23
1502s	23	23	24	24	23	23	23	23	0
1505s	68	68	71	82	79	69	68	68	0
1506s	73	91	214	509	539	296	82	74	0
1507s	59	59	60	60	60	59	59	59	0
1508s	0	59	59	0	0	59	0	0	0
1601s	15	16	17	17	17	16	15	15	14
1602s	16	16	16	16	16	16	16	16	0
1603s	30	32	32	32	31	31	30 40	30	0
1607s	39	116	199	369	307	128	40 97	39	0
1701s	97	98	98 21	98 21	98 21	98 20	20	97 20	0 0
1703s	20	20	21 29		21	20	20	20	0
1704s	25 42	33 98	180	28 300	407	28 146	20 55	25 46	36
1705s		98 92		300 92	407 92	92	92	40 92	
1803s	92		92			92 92	92	92	0
1804s	0	0	95 70	96 95	95 88	92 67	66		0
1805s	66	66	70	85		67 204	66	66	0
1806S	66 61	69 61	98 61	167 61	284 61	204	61	66 61	0
1807S 1808S	61	61	61 67	66		61 62	0	0	
	0	62	67		67				0
2001s	63	63	64	64	63	63	63	63	62

2002s	62	62	63	63	64	62	62	62	0
2005s	64	65	67	68	68	65	64	64	0
2006S	65	70	80	95	105	77	67	65	0
2007s	65	65	66	66	66	65	65	65	0
2008s	0	0	0	0	0	0	0	0	0
2009s	0	0	65	68	65	62	0	0	0
2101s	34	35	35	36	36	35	35	34	34
2102s	45	50	50	53	47	47	45	45	0
2103s	67	68	68	68	68	67	67	67	0
2107s	31	34	50	53	39	33	31	31	0
2110s	68	71	72	70	70	69	69	68	0
2201s	104	104	105	105	104	104	104	104	0
2203s	37	37	37	37	37	37	37	37	0
2204s	41	50	58	59	55	48	41	41	0
22059	31	33	34	37	35	34	31	31	30
2209s	104	106	106	107	115	105	104	104	0
2303s	95	95	95	95	95	95	95	95	0
23046	95	96	104	131	118	96	95	95	0
2305s	67	68	73	94	92	69	67	67	0
2306s	0	0	68	120	103	67	0	0	0
23078	57	57	57	57	57	57	57	57	0
2308s	57	58	58	58	58	57	57	57	0
2501s	58	58	58	58	58	58	58	58	0
25026	58	58	60	74	68	58	58	58	0
2505s	66	68	70	74	74	68	67	66	0
2506s	66	69	70	73	74	69	67	66	0
25076	66	66	67	67	67	66	66	66	0
2508s	0	0	67	68	0	0	0	0	0
2601s	37	37	38	38	38	37	37	37	0
2602S	4s	53	53	56	48	48	46	45	0
2603s	64	65	66	66	65	65	65	64	0
2607s	38	39	41	47	40	38	38	38	0
2610s	66	75	75	74	73	70	67	66	0
2701s	104	104	104	104	104	104	104	104	0
2703s	38	39	40	42	40	39	38	38	0
2704s	42	47	48	45	44	45	43	42	0
2705s	41	42	43	44	45	42	41	41	0
2709s	104	107	115	116	120	107	106	104	0
2803s	100	100	101	101	101	100	100	100	0
28049	0	100	105	116	107	102	0	0	0
2805S	61	61	63	66	66	61	61	61	0
28068	0	62	85	89	114	63	58	0	0
2807s	62	62	62	62	62	62	62	62	0
28088	62	63	64	64	63	63	62	62	0
2810s	36	36	36	41	37	36	36	36	0
3001s	76	77	79	80	79	77	77	76	76
3005s	95	97	101	108	106	97	96	95	0
3006s	97	106	123	189	210	120	100	97	0
3007s	66	67	72	87	77	66	66	66	0
3011s	102	129	253	320	235	117	108	102	0
3101s	31	31	32	32	32	31	31	31	31
31025	36	38	39	37	37	37	36	36	0
3103s	83	84	85	84	85	84	83	83	0
3107s	32	35	39	65	60	34	32	32	0
3110s	82	83	82	82	82	82	82	82	0
3201s	94	96	96	96	96	96	95	95	94
3203s	30	30	30	30	30	30	30	30	0
3204s	34	43	52	43	43	41	36	34	30
3205s	28	28	29	29	30	28	28	28	0
3303s	91	91	91	91	91	91	91	91	0

3305s	115	116	123	158	128	116	115	115	0	
3306s	116	148	164	215	201	147	122	117	0	
3307s	63	63	64	65	64	62	63	63	0	
3308s	63	63	63	63	63	63	63	63	0	
3501s	121	121	121	121	121	121	121	121	0	
3502S	0	0	123	127	134	0	0	0	0	
3505s	111	112	113	115	113	112	111	111	0	
3506s	113	114	119	125	123	116	115	113	0	
3507s	88	88	90	91	92	88	88	88	0	
3508\$	0	0	0	107	0	0	0	0	0	
3601s	33	33	34	34	34	33	33	33	0	
36028	44	57	56	56	45	46	46	44	0	
3603s	124	125	125	126	125	125	124	124	0	
3607s	35	36	39	55	42	36	36	35	0	
3610s	127	135	131	142	143	131	128	127	0	
3701s	60	60	60	61	60	60	60	60	0	
3703s	31	32	32	33	33	32	31	31	0	
3704s	47	81	193	258	214	77	47	47	0	
3705s	36	38	38	38	38	37	37	36	35	
3709s	67	125	162	163	79	95	69	67	60	
3803s	58	58	59	59	59	58	58	58	58	
38035	0	58	61	70	62	0	0	0	0	
38043 3805s	109	113	128	217	123	113	110	109	0	
3805s 3806s	165	113	128	258	249	113	162	180	0	
3807s	117	117	118	119	119	118	117	117	0	
3808s	117	118	118	121	124	118	118	117	0	
4101s	122	123	124	124	124	123	122	122	122	
4102s	0	0	141	147	198	140	0	0	0	
4105s	97	98	101	113	102	98	97	97	0	
4106s	129	114	138	175	265	157	126	126	94	
4107s	99	101	112	155	194	120	100	99	0	
4108s	0	0	100	210	130	114	0	0	0	
4201S	49	49	49	50	62	53	49	49	0	
4203s	125	125	126	127	128	127	125	125	0	
4205s	31	33	33	33	33	32	32	28	0	
42078	45	49	55	69	60	49	46	46	44	
4303s	33	33	34	34	34	34	33	33	0	
4305s	41	42	41	40	42	41	41	41	0	
4403s	14	14	15	14	15	14	14	14	0	
4404s	0	0	0	0	0	0	0	0	0	
4405s	130	130	133	135	134	128	130	130	0	
4406s	0	0	133	247	283	0	0	0	0	
4406s 4407s	107	107	132	109	110	108	107	107	0	
4407s 4408s					110	108	107	107	0	
	0	107	108	110		45		0 31	25	
4601S	29	58	70	94	42		32			
4603S	18	20	24	27	22	19	19	18	0	
4605S	30	0	0	0	30	0	30	30	0	
46063	0	0	0	32	31	0	0	0	0	
4607s	68	69	72	75	77	70	68	68	0	
4701s	18	21	23	29	24	21	19	18	0	
4702s	20	25	64	96	110	63	26	20	0	
4707s	27	35	48	65	99	43	29	28	24	
4801S	27	30	38	67	47	32	28	27	0	
4803s	23	<u>_</u> 25	27	26	26	25	21	23	0	
4804s	36	151	297	322	145	119	86	37	0	
4805s	34	33	34	36	35	34	33	34	0	
4807s	0	28	28	54	42	29	0	0	0	
4808S	32	58	51	54	65	53	43	35	27	
4809s	33	130	192	223	97	48	37	33	0	
4903s	20	20	20	20	20	20	20	20	0	
	20	20	20	20	20	_*	_*	_*	•	

4904s	20	26	54	71	56	25	20	20	0	55	
4905s	39	40	45	52	45	40	39	39	0	45	
4907s	130	131	133	137	136	132	130	130	0	135	
4908S	130	130	130	131	132	130	130	130	0	131	
4910s	23	36	61	36	42	54	27	24	20	42	
5201s	29	32	35	33	33	35	31	30	28	33	
5202s	30	37	176	178	480	75	39	30	0	188	
5205s	47	48	49	49	49	48	47	47	0	48	
5303s	25	25	25	25	25	25	25	25	0	25	
5304s	0	0	0	0	0	0	0	0	0	0	
5305s	34	35	42	103	47	35	35	34	0	65	
5307s	41	43	55	144	267	102	42	41	39	111	
5308s	40	41	41	41	41	41	40	40	39	41	
5311s	34	35	35	35	35	35	34	34	0	35	
7605s	59	60	62	63	61	60	59	59	58	61	
7606S	58	59	61	62	60	59	58	58	0	60	
7607S	90	91	91	92	92	91	90	90	0	91	
7612s	91	92	94	98	100	95	91	91	0	96	
7801s	9	10	10	11	11	10	9	9	0	10	
7803S	13	13	13	13	13	13	13	12	0	13	
8001S	22	22	22	23	23	22	22	22	0	22	
8003s	9	9	9	9	9	9	9	9	9	9	
1		LINK-BY-	LINK AL	L-TIME-SI	LICES	TOTAL I	DELAY (VE	EH-H)		RUN ON 11/6/	91

# SMART CORRIDOR BASE RUN NETWORK and TIME DATA (6/11/91) SMART CORRIDOR BASE DEMAND SMART CORRIDOR CONTROL DATA

.

		TIME	SLI	CES								
LINK		1	2		3	4	5	6	7	8	9	
NO.&												TOTAL
TYPE												DELAY
	600		630	70	0 7	30 8	8 00	30 900	930	1000	1300	
7u		. 00		. 00	.00	.00	.00	.00	.00	.00	. 00	.00
8u		. 00		. 00	.85	9.73	25.97	.00	.00	.00	.00	36.55
<b>9</b> U		.00		. 00	1.63	9.09	3.57	.07	.00	.00	.00	14.35
10U		. 00		.00	1.50	4.56	1.73	1.02	.00	.00	. 00	8.81
110		.00		. 00	3.99	14.81	8.31	2.19	.00	.00	. 00	29.30
12U		.00		. 00	5.80	18.07	12.04	4.06	.00	.00	. 00	39.97
130		.00		.01	61.40	134.69	126.31	20.87	.00	.00	. 00	343.29
14u		. 00		.00	3.52	17.86	22.53	. 00	.00	.00	. 00	43.90
15U		. 00		. 00	.00	.00	.00	.00	.00	.00	. 00	.00
16U		. 00		. 00	.00	.00	.00	.00	.00	.00	. 00	.00
170		.00		. 00	. 00	.00	.00	.00	.00	.00	.DO	.00
18U		.00		. 00	. 00	.00	.00	.00	.00	.00	.00	.00
19U		.00		. 00	.00	.00	.00	. 00	.00	.00	.00	.00
2ou		.00		. 00	. 00	.DO	.00	.00	.00	.00	.00	.00
21u		.00		. 00	19.53	1.10	1.15	.32	.00	.00	.00	22.11
22u		.00		. 00	.00	4.08	6.06	4.97	.00	.00	.00	15.12
23U		.00		. 00	. 00	6.10	5.66	1.59	.00	.00	.00	13.35
24U		.00		.00	.17	6.89	11.53	4.36	.00	.00	.00	22.94
25U		. 00		. 00	1.59	13.38	13.75	4.15	.00	.00	.00	32.86
26U		. 00		.00	5.97	24.02	23.07	6.46	.00	.00	.00	59.51
27U		.00		. 00	2.24	5.36	13.09	4.45	.61	.00	.00	25.75
28U		.00		.00	31.12	76.34	78.63	65.69	2.27	.00	.00	254.04
290		.00		. 00	.00	.00	.00	.00	.00	.00	.00	.00
3ou		.00		. 00	.00	.00	.00	.00	.00	.00	.00	.00
310		.00		.00	.00	. 00	.00	.00	.00	.00	.00	.00

ITERATION NUMBER 3

		00								
320	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
5ou	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
510	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
52U	.00	.00	.00	.00	.00	-00	.00	.00	.00	.00
53u	.00	.00	.00	.00	. 00	.00	.00	. 00	.00	.00
54u	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
55U	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
56U	.00	.00	.00	.00	. 00	.00	.00	.00	.00	.00
57U	.00	.00	.22	2.44	2.30	.00	.00	.00	.00	4.96
58U	.00	.00	13.48	25.00	1.52	.00	.00	.00	.00	39.99
59U	.00	.00	.08	1.25	.81	.00	.00	.00	.00	2.15
60U	.00	.00	10.86	25.98	.89	.00	.00	.00	.00	37.73
61U	.00	.00	6.04	9.38	7.48	.00	.00	.00	.00	22.91
62U	.00	.00	.59	14.01	16.25	3.48	. 00	.00	.00	34.34
63U	.00	.00	3.72	16.34	12.18	4.95	.00	.00	.00	37.19
64U	.00	.00	53.34	99.72	59.50	14.40	.00	.00	.00	226.96
65U	. 00	.00	.00	.00	5.24	.31	.00	.00	.00	5.56
66U	.00	.00	. 00	.00	7.30	.68	.00	.00	.00	7.98
67U	.00	.00	. 00	9.76	13.88	2.79	.00	. 00	.00	26.43
68U	.00	.00	1.12	19.93	55.14	28.13	.00	. 00	.00	104.32
69U	.00	.00	1.08	7.51	10.80	.54	.00	.00	.00	19.93
7ou	.00	.00	4.37	28.51	40.27	22.34	2.99	.00	.00	98.48
710	.00	.00	30.96	72.63	83.10	74.82	3.07	.00	.00	264.57
720	.00 .00	.00	.00	.00	.00	.00	.00	.00	.00	.00
	.00	.00	.00 .00	.00 .00	.00	.00 .00	.00	.00	.00 .00	
80U	.00 ,00				.00 .00		.00			.00
81U		.00	.00	.00		.00 .00		.00	.00	.00
82U	.00	.00	.00	-00	.00		.00	.00	.00	.00
83U	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
84U	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
85U	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
86u	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
87U	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
120s	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
121s	.00	.00	.39	2.27	2.43	.33	.00	.00	.00	5.43
122s	.00	.00	.10	2.05	3.92	1.14	.00	-00	.00	7.21
1235	.00	.00	.00	.47	1.04	.13	.00	.00	.00	1.64
124S	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
125s	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
126S	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
127S	.00	.00	.00	.32	.98	.24	.00	.00	. 00	1.54
128s	.00	. 00	.39	4.12	4.94	.00	. 00	. 00	.00	9.45
150s	.00	. 00	.00	. 00	.00	.00	.00	. 00	.00	.00
151s	.00	.00	. 00	. 00	. 00	.00	.00	. 00	. 00	.00
152S	.00	.00	.00	.00	. 00	.00	. 00	.00	. 00	.00
153s	.00	.00	. 00	.08	.04	.00	. 00	.00	. 00	.12
154s	.00	.00	.00	.36	.17	.00	.00	.00	.00	.52
155s	.00	.00	1.14	3.00	2.30	.69	.00	.00	.00	7.13
1565	.00	.00	.00	2.25	6.69	2.60	.00	.00	.00	11.54
157s	.00	.00	5.08	28.29	39.97	19.09	1.14	.00	.00	93.57
157s	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
202s	.00 .05	.11	.12	.76	.78	.00	.06	.05	.00	2.01
202s 205s	.17	.35	.53	.63	.44	.40	.28	.19	.02	
		.01		.02				.00		3.01
206S	.00 02		.00		.00 1/6	. 00 04	.00 04		.00	.03
2095	.02	.04	.07	.06	.04 57	.04	.04	.02	.00	.31
211s	.04	.15	.24	.63	.53	.14	.07	.06	.00	1.86
301s	.01	.03	.05	.34	.32	.03	.02	.01	.00	.82
303s	.02	.06	.09	.18	.17	.06	.03	.02	.00	.64
304s	.01	.03	.03	.07	.07	.01	.01	.01	.00	.25
309s	.02	.05	.05	.04	.03	.04	.03	.02	.01	.28
703s	.03	.09	.15	.26	.24	.10	.05	.04	.00	.96

704s	.00	.00	.00	.00	.01	.00	.00	.00	.00	
705s	.24 .19	.60 .42	.91 .45	2.52 .38	1.92 .26	.51 .38	.35 .29	.27 .21	.03 .02	
901s <b>902S</b>	.00	.42	.03	.08	.28	.01	.00	.00	.02	
905s	.00	.22	.38	.80	.67	.29	.10	.08	.00	
906S	.03	.18	.42	1.34	2.40	.28	.06	.03	.00	
907s	.01	.03	.04	.05	.06	.02	.01	.01	.00	
908S	.08	. 19	.20	1.07	1.62	.30	.09	.08	.00	
909s	.16	.37	.34	.34	.23	.25	.25	.18	.02	
1001s	.14	.40	.43	.40	.24	.34	.24	.17	.03	
1002s	.24	.88	1.01	.93	1.06	.83	.33	.24	.00	
1003s	.02	.05	.06	.37	.51	.20	.02	.02	.00	
1005s	1.43	5.58	9.42	10.72	4.88	3.08	1.91	1.42	.00	
1010s	.05	.12	.12	.09	.08	.06	.05	.05	.00	
1101s	.76	1.21	1.13	1.18	.98 21	.88 .16	.81	.74	.00 .00	
1108s 1201s	.06 .30	.18 .83	<b>.23</b> 1.69	<b>.18</b> 2.27	<b>.21</b> 2.29	.10 1.17	.07 .39	.06 .30	.00	
1201s 1203s	.14	.20	.18	.25	.24	.18	.18	.14	.00	
1203s 1204s	.14	.20	.25	1.19	5.16	2.31	.05	.13	.00	
1205s	.57	1.71	2.37	1.32	.99	1.76	.89	.61	.05	
1303s	.10	.22	.23	.19	.17	.21	.12	.11	.00	
1304s	.18	.46	.72	.37	.23	.33	.26	.19	.02	
1305s	.04	. 11	.20	.81	.80	.12	.05	.04	.00	
1306s	.03	.08	4.60	8.84	10.00	.92	.03	.03	.00	
1307s	.01	.03	.04	.06	.03	.02	.01	.01	.00	
1308s	.00	.01	.02	.08	.10	.01	.00	.00	.00	
1310s	.00	.00	.05	.03	.04	.01	.00	.00	.00	
1501s	.36	1.61	2.15	2.59	2.30	1.78	.68	.51	.04	
1502S	.00	.01	.02	.03	.01	.01	.00 17	.00	.00 .00	
1505s 1506s	.11 .21	.38 .91	1.16 6.27	3.47 11.66	2.46 17.17	<b>.</b> 60 6.54	.17 .51	.13 .24	.00	
1506s 1507s	.01	.05	•.27 .10	.20	.13	•.54 .04	.02	.01	.00	
1507s	.00	.05	.01	.00	.00	.01	.00	.00	.00	
1601s	.43	1.10	1.55	1.94	1.48	1.33	.68	.59	.06	
1602s	.07	.12	.12	.11	.11	.09	.07	.06	.00	
1603s	.49	1.48	1.70	1.60	1.11	.91	.64	.49	.00	
1607s	.65	8.95	15.36	28.99	25.62	9.49	.97	.68	.00	
1701s	.07	.24	.50	.67	.61	.43	.08	.07	.00	
1703s	.03	.08	. 19	.19	.18	.07	.04	.03	.00	
1704s	.22	1.01	.68	.58	.37	.51	.33	.23	.00	
1705s	.95	6.20	13.62	24.76	29.30	9.00	2.29	1.45	.12	
1803s	.03	.04	.04	.03	.02	.03	.04	.04	.00	
1804S	.00	.00	.08	.11	.09	.01	.00	.00	.00	
1805s 1806S	.07 .01	.31 .16	1.51	4.26	4.85	<b>.</b> 56 4.06	.11 .02	.08 .01	.00 .00	
18005 1807s	.01	. 10	1.23 .13	4.75 .14	9.18 .08	4.06 .04	.02	.01	.00	
1807s 1808s	.02	.02	.12	.09	.13	.04	.02	.02	.00	
2001s	.17	.43	.59	.59	.42	.38	.00	.19	.03	
20015	.00	.01	.02	.03	.03	.00	.00	.00	.00	
20055	.19	.60	1.05	1.50	1.42	.60	.29	.21	.00	
2006s	.07	.27	.69	1.48	1.67	.52	. 15	.07	.00	
2007s	.04	.11	.33	.50	.27	.09	.06	.04	.00	
2008s	.00	.00	.00	.00	.00	.00	.00	.00	.00	
20095	.00	<b></b> 00	.35	.69	.26	.02	.00	.00	.00	
2101s	. 13	.37	.50	.69	.55	.30	.24	.16	.05	
2102s	.15	.47	.46	.56	.32	.30	.20	. 15	.00	
2103s	.09	.26	.30	.32	.23	.18	.12	.09	.00	
2107s	.24	1.19	4.04	4.58	2.21	1.03	.32	-24	.00	
2110s	.13	.43	.50	.36	.30	.25	.18 1/	.13	.00	
2201s	.11	.27	.35	.38	.27	.21	.14	.11	.00	

2x22         .15         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0 <th></th>											
2009         .74         .70         1.05         1.16         1.12         .42         2.9         .06         .72           2009         .07         .00         .20         .20         .48         .10         .00         .07         .00         .20           2006         .00         .03         .25         1.22         .97         .02         .00         .00         .25           2006         .00         .03         .25         1.22         .14         .07         .02         .00         .00         .25           2006         .00         .03         .03         .03         .03         .03         .03         .03         .03         .03         .03         .03         .03         .03         .03         .04         .04         .04         .05         .06         .03         .04         .04         .04         .04         .04         .05         .06         .05         .06         .05         .06         .06         .06         .07         .04         .04         .04         .04         .04         .04         .05         .05         .05         .05         .05         .05         .04         .04         .04 </td <td>22033</td> <td></td> <td>.09</td> <td>.24</td> <td>.27</td> <td>.14</td> <td></td> <td></td> <td></td> <td></td> <td>.91</td>	22033		.09	.24	.27	.14					.91
2293         .07         .20         .22         .48         1.20         .00         .00         .00         .02         .00         .02         .00         .02         .00         .02         .00         .02         .00         .02         .00         .02         .00         .02         .00         .02         .00         .02         .00         .02         .00         .02         .00         .02         .00         .02         .00         .02         .00         .02         .00         .02         .00         .02         .02         .02         .00         .02         .02         .02         .02         .00         .02         .01         .01         .00         .00         .01         .02         .00         .07         .01         .02         .00         .07         .01         .01         .02         .00         .00         .00         .00         .02         .00         .02         .00         .01         .02         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00 </td <td></td> <td>7.42</td>											7.42
2308         .03         .04         .04         .05         .05         .00         .00         .25           2305         .06         .03         .02         .00         .03         .00         .25           2305         .06         .07         .02         .01         .07         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00										.06	
2349         .00         .63         .25         1.3         .97         .02         .00         .00         .00         .00         .00           2366         .06         .43         .15         .53         .56         .70         .00         .70         .20           2367         .06         .11         .21         .22         .16         .07         .06         .00         .01         .11           2368         .03         .03         .03         .03         .02         .01         .00         .00         .01         .11           2369         .00         .07         .11         .01         .03         .02         .00         .00         .01         .01           2369         .00         .00         .01         .02         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00											
2005         .06											
2006 </td <td></td>											
sons </td <td></td>											
sease											
sols <td></td>											
25039                                                                                                       <											
25056         .19         .77         1.47         2.28         2.28         .77         3.56         .22											
2566         .02         .10         .13         .23         .26         .10         .03         .02											
2507s        05        14        46        76        70        05        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>											
sesse											
26018         .06         .13         .22         .37         .25         .08         .08         .00         1.22           26025         .26         .89         .80         1.01         .52         .51         .26         .26         .46         .46           26039         .17         .46         .78         2.22         .71         .50         .50         .51         .22         .77         .50           26039         .26         .16         .78         2.22         .71         .51         .60         .56         .29         .50         .51         .62         .40         .50         .51         .62         .60         .22         .73         .64         .20         .50         .20         .50         .20         .50         .20         .50         .20         .50         .20         .50         .20         .50         .20         .50         .20         .20         .20         .20         .20         .20         .20         .20         .20         .20         .20         .20         .20         .20         .20         .20         .20         .20         .20         .20         .20         .20         .20         .											
2603         .26         .89         .80         1.01         .52         .51         .36         .26											
2603         .15         .42         .44         .69         .35         .31         .21         .15											
$2607_8$ .17       .46       .78       2.22       .71       .31       .22       .77       .26       .00       .5.0 $2101a$ .26       .16       1.13       1.00       .84       .63       .37       .26       .00       .3.00 $2703a$ .20       .50       .51       .62       .43       .15       .10       .08      00       .27 $2703a$ .26       .55       .70       .65       1.15       .43       .34       .22       .00       .34 $2703a$ .26       .55       .70       .65       1.15       .43       .34       .32       .00       .00       .00       .11 $22035$ .12       .26       .34       .37       .38       .24       .13      00       .01       .92 $22035$ .01       .11       .16       .25       .03       .00       .00       .00       .00       .00       .00       .00       .00       .00       .00       .00       .00       .00       .00       .00       .00       .00       .00       .00       .00       .00       .00       .00 <td< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></td<>											
260s         .26         1.16         1.13         1.00         .84         .63         .37         .26         .00         5.6           270s         .20         .50         .51         .62         .43         .31         .25         .20         .00         .30           270s         .20         .66         .82         .49         .34         .44         .28         .20         .00         .34         .44           270s         .20         .66         .82         .49         .34         .44         .28         .20         .00         .34         .44           270s         .20         .66         .82         .49         .34         .44         .28         .20         .00         .44         .46           270s         .21         .44         .13         .00         .00         .00         .00         .51         .19           28048         .02         .19         .85         1.90         1.69         .21         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00         .00 <td></td>											
2703 $.20$ $.50$ $.51$ $.62$ $.43$ $.31$ $.25$ $.20$ $.00$ $3.01$ $2703$ $.08$ $.21$ $.44$ $1.20$ $.50$ $.15$ $.10$ $.08$ $$											
2703s       .08       .21       .44       1.20       .50       .15       .10       .08                                                                                                        <											
27045       .20       .66       .82       .49       .34       .44       .28       .20											
2705a       .26       .55       .70       .85       1.15       .43       .34       .32											
28035       .12       .26       .34       .37       .38       .23       .16       .14       .00       .19         28048      o       .01       .11       .48       .25       .03       .00      o      o      d         28058       .02       .19       .85       1.90       1.6e       .21       .04       .02       .00      d      d         28065       .00       .05       1.14       1.22      d      d      d      d      d      d      d      d      d      d      d      d      d      d      d      d      d      d      d      d      d      d      d      d      d      d      d      d      d      d      d      d      d      d      d      d      d      d      d      d      d      d      d      d      d      d      d      d      d      d      d      d      d      d      d      d      d      d      d      d <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>											
28048        o        0        1        4        2        0        o        o        0           28055        02        9        8         19        2         104        02        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        00        01        02        01        01        01        01        01        01        01        01        01        01        01        01        01        01        01        01        01        01        01        01        01        01        01        01        01        01        01        01        01        01        01        01        01        011        011        011											
2805s $.02$ $.19$ $85$ $1.90$ $1.69$ $21$ $04$ $02$ $00$ $00$ $28066$ $00$ $05$ $16$ $1.26$ $2.50$ $12$ $00$ $00$ $00$ $28076$ $02$ $05$ $14$ $1.2$ $09$ $04$ $02$ $00$ $00$ $00$ $28086$ $02$ $05$ $14$ $1.2$ $09$ $04$ $02$ $02$ $00$ $00$ $28086$ $02$ $05$ $04$ $02$ $02$ $00$ $00$ $05$ $28086$ $02$ $05$ $06$ $02$ $02$ $00$ $06$ $05$ $3001s$ $20$ $56$ $07$ $16$ $16$ $22$ $00$ $00$ $64$ $3005s$ $23$ $95$ $1.85$ $3.25$ $2.83$ $93$ $11$ $26$ $00$ $07$ $3005s$ $23$ $95$ $1.85$ $3.25$ $2.83$ $93$ $11$ $26$ $00$ $07$ $3005s$ $05$ $1.104$ $1.44$ $8.13$ $1.12$ $26$ $00$ $00$ $02$ $3011s$ $44$ $35$ $23$ $1.14$ $16$ $03$ $00$ $133$ $3103s$ $44$ $26$ $21$ $21$ $66$ $00$ $24$ $3103s$ $44$ $26$ $21$ $26$ $21$											
28065.00.051.161.262.50.12.00.005.0028076.02.05.14.12.09.04.02.02.00											
28076.02.05.14.12.09.04.02.02.00.5528086.02.05.07.07.05.04.02.02											
2808s $.02$ $.05$ $.07$ $.07$ $.05$ $.04$ $.02$ $.02$ $00$ $00$ $94$ 2810s $.01$ $.02$ $.09$ $16$ $16$ $02$ $01$ $00$ $99$ 3001s $20$ $54$ $97$ $1.40$ $1.26$ $52$ $56$ $22$ $02$ $02$ $01$ 3005s $23$ $29$ $69$ $2.46$ $239$ $52$ $11$ $05$ $00$ $655$ 3007s $10$ $32$ $1.20$ $353$ $1.81$ $23$ $14$ $10$ $$											
2810s       .01       .02       .09       .61       .16       .02       .02       .01       .00       .94         3001s       .20       .54       .97       1.40       1.26       .52       .36       .22       .02       .5.4       .5.4         3005s       .23       .95       1.85       .325       2.83       .93       .41       .26       .00       .01       .00         3005s       .23       .95       1.85       .325       2.83       .93       .41       .26       .00       .00       .65       .65         3007s       .10       .32       1.20       .353       1.81       .23       .14       .10       .00       .743         3011s       .69       2.65       11.04       14.48       8.73       1.72       1.12       .66       .00       .011       .03         3101s       .14       .35       .03       .47       .26       .21       .18       .03       .00       .04       .04       .04       .04       .04       .04       .04       .00       .00       .00       .00       .00       .00       .00       .01       .01       .00       .											
3001s.20.54.971.401.26.52.36.22.025.433005s.23.951.853.252.83.93.41.26.0010.713006s.05.29.692.462.39.52.11.00.006.533007s.10.321.203.531.81.23.14.10.00.7443011s.692.6511.0414.448.731.721.12.66.00.413101s.14.35.43.39.47.26.21.18.03.24.433102s.03.22.32.18.13.15.07.00.00.60.603107s.391.091.836.344.74.91.51.39.00.60.603107s.04.12.06.07.06.06.05.04.00.6032033.00.02.03.01.00.00.11.123204s.451.512.281.421.64.20.70.48.04.733204s.01.02.03.01.00.00.04.42.443305s.03.342.24.45.13.26.24.00.423305s.03.342.241.64.02.03.01.00.623305s.03											
3005s $.23$ $.95$ $1.85$ $3.25$ $2.83$ $.93$ $.41$ $.26$ $.00$ $10.71$ $3006s$ $.05$ $.29$ $.69$ $2.46$ $2.39$ $.52$ $.11$ $.05$ $.00$ $6.55$ $3007s$ $.10$ $.32$ $1.20$ $3.53$ $1.81$ $.23$ $.14$ $.05$ $.00$ $6.51$ $3011s$ $.69$ $2.65$ $11.04$ $14.44$ $8.73$ $1.72$ $1.12$ $.666$ $.oo$ $41.04$ $3101s$ $.14$ $3.53$ $.43$ $.39$ $.47$ $.26$ $.21$ $.18$ $.03$ $.24$ $3102s$ $.03$ $.22$ $.32$ $.18$ $.13$ $.15$ $.07$ $.03$ $.00$ $1.13$ $3103s$ $.44$ $.83$ $1.05$ $.91$ $1.02$ $.76$ $.54$ $.46$ $.00$ $.60$ $3107s$ $.39$ $1.09$ $1.83$ $6.34$ $4.74$ $.91$ $.51$ $.39$ $.oo$ $.52$ $310as$ $.44$ $.83$ $1.05$ $.91$ $1.02$ $.76$ $.54$ $.46$ $.00$ $.57$ $310as$ $.04$ $.12$ $.06$ $.76$ $.58$ $.31$ $.16$ $.01$ $.40$ $.57$ $3203s$ $.00$ $00$ $00$ $00$ $00$ $00$ $00$ $27$ $3204s$ $.05$ $15$ $28$ $42$ $66$ $03$ $.00$ $67$ $3203s$ $03$ $34$ $20$ <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>											
3006s $.05$ $.29$ $.69$ $2.46$ $2.39$ $.52$ $.11$ $.05$ $.00$ $6.55$ $3007s$ $.10$ $.32$ $1.20$ $3.53$ $1.81$ $.23$ $.14$ $.10$ $.00$ $7.42$ $3011s$ $.69$ $2.65$ $11.04$ $14.44$ $8.73$ $1.72$ $1.12$ $.66$ $.00$ $41.04$ $3101s$ $.14$ $.35$ $.43$ $.39$ $.47$ $.26$ $.21$ $.18$ $.03$ $2.44$ $3102s$ $.03$ $.22$ $.32$ $.18$ $.13$ $.15$ $.07$ $.03$ $.00$ $1.13$ $3103s$ $.44$ $.83$ $1.05$ $.91$ $1.02$ $.76$ $.54$ $.46$ $.00$ $.6.01$ $3107s$ $.39$ $1.09$ $1.83$ $6.34$ $4.74$ $.91$ $.51$ $.39$ $.00$ $.6.23$ $3104s$ $.04$ $.12$ $.06$ $.07$ $.06$ $.06$ $.05$ $.04$ $.00$ $.55$ $3201s$ $.07$ $.70$ $.78$ $.69$ $.76$ $.58$ $.31$ $.16$ $.01$ $.01$ $3203s$ $.00$ $.06$ $.05$ $.04$ $.00$ $.06$ $.05$ $.04$ $.00$ $.06$ $3203s$ $.01$ $.02$ $.03$ $.22$ $.18$ $.42$ $.16$ $.120$ $.70$ $.48$ $.04$ $.97$ $3204s$ $.03$ $.22$ $.03$ $.21$ $.16$ $.05$ $.00$ $.06$ $.06$ $3303$											10.71
3007s.10.321.20 $3.53$ 1.81.23.14.107.42 $3011s$ .692.6511.0414.448.731.721.1241.00 $3101s$ .14						2.39					6.55
3011s.692.6511.0414.448.731.721.12.6641.043101s.14.35.43.39.47.26.21.18.032.443102s.03.22.32.18.13.15.07.03.003103s.44.831.05.911.02.76.54.46.003107s.391.091.836.344.74.91.51.393101s.04.12.06.07.06.05.043201s.07.70.78.69.76.58.31.16.0132033320333203332034	3007s	.10		1.20	3.53	1.81	.23	.14	.10	.00	7.42
3101s.14.35.43.39.47.26.21.18.03.243102s.03.22.32.18.13.15.07.03.001.133103s.44.4831.05.911.02.76.54.46.006.013107s.391.091.836.34 $4.74$ .91.51.393110s.04.12.06.07.06.06.05.043201s.07.70.78.69.76.58.31.16.013203a3204s1.512.281.421.641.203305s3305s<	3011s				14.44	8.73	1.72	1.12	.66	.00	41.04
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		.14	.35	.43	.39	.47	.26	.21	. 18	.03	2.44
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3102s	.03	.22	.32	.18	.13	.15	.07	.03	.00	1.13
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3103s	.44	.83	1.05	.91	1.02	.76	.54	.46	.00	6.01
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3107s	.39	1.09	1.83	6.34	4.74	.91	.51	.39	.00	16.20
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3110s	.04	.12	.06	.07	.06	.06	.05	.04	.00	.50
3204s.45 $1.51$ $2.28$ $1.42$ $1.64$ $1.20$ .70.48.04 $9.73$ $32053$ .20.36.48.68.54.31.26.24.00.00.43 $3303s$ .01.02.03.22.08.02.03.01.00.43 $3305s$ .03.34 $2.34$ $8.00$ $3.57$ .40.06.03.00.43 $3306s$ .07 $2.11$ $2.96$ $5.23$ $4.35$ $1.73$ .34.10.00.63 $3307s$ .05.13.42.75.38.13.06.05.00.22 $33088$ .02.03.03.04.03.02.02.00.26 $3501s$ .01.06.04.06.03.01.00.28 $3502s$ o00.06.15.34ooo $3505s$ .11.671.092.201.39.62.22.12.00o $3506s$ .05.06.23.36.29.11.09.05ooo $3508s$ ooooooooo $3508s$ ooooooooo $3508s$ ooooooooo </td <td>3201s</td> <td>.07</td> <td>.70</td> <td>.78</td> <td>.69</td> <td>.76</td> <td>.58</td> <td>.31</td> <td>.16</td> <td>.01</td> <td>4.07</td>	3201s	.07	.70	.78	.69	.76	.58	.31	.16	.01	4.07
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		.00	. 00	.00	.04	.06	.01	.01	.00	.00	. 12
3303s.01.02.03.22.08.02.03.01.00.43 $3305s$ .03.342.348.003.57.40.06.03.0014.77 $3306s$ .072.112.965.234.351.73.34.10.00.06.03 $3307s$ .05.13.42.75.38.13.06.05.00.02.02 $3308s$ .02.03.03.04.03.02.02.02.00.20 $3501s$ .01.06.04.06.03.01.01.00.28 $3502s$ .00.00.06.15.34.00.00.00.05.00 $3505s$ .11.671.092.201.39.62.22.12.00.643 $3506s$ .05.06.23.36.29.11.09.05.00.00.124 $3508s$ .00.00.54.01.00.00.00.00.55.55.55.54.01.00.00.00.55 $3601s$ .00.07.13.14.14.04.00.00.00.05.00.55 $3601s$ .00.07.13.14.14.04.00.00.00.55 $3601s$ .00.07.13.14.14.04.00.00.00.00<	3204s	.45	1.51	2.28	1.42	1.64	1.20	.70	.48	.04	9.73
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	32053	.20	.36	.48	.68	.54	.31	.26	.24	.00	3.06
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3303s	_01	.02	.03	.22	.08	.02	.03	.01	.00	.43
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3305s	.03	.34	2.34	8.00	3.57	.40			.00	14.77
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3306s	.07								.00	16.88
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3307s										1.96
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	33088	.02			.04					.00	.20
3505s       .11       .67       1.09       2.20       1.39       .62       .22       .12       .00       6.43         3506s       .05       .06       .23       .36       .29       .11       .09       .05       .00       1.24         3507s       .16       .40       1.11       2.25       2.18       .45       .22       .17       .00       6.94         3508s       .00       .00       .00       .54       .01       .00       .00       .00       .55       .50         3601s       .00       .07       .13       .14       .14       .04       .00       .00       .00       .55	3501s	.01	.06				.03	.01	.01	.00	.28
3506s       .05       .06       .23       .36       .29       .11       .09       .05       .00       1.24         3507s       .16       .40       1.11       2.25       2.18       .45       .22       .17       .00       6.94         3508s       .00       .00       .00       .54       .01       .00       .00       .00       .00       .55         3601s       .00       .07       .13       .14       .14       .04       .00       .00       .00       .53	3502s		00	.06	.15	.34					.55
3507s       .16       .40       1.11       2.25       2.18       .45       .22       .17       .00       6.94         3508s       .00       .00       .00       .54       .01       .00       .00       .00       .55         3601s       .00       .07       .13       .14       .14       .04       .00       .00       .00       .53	3505s	.11	.67				.62		.12	.00	6.43
3508s       .oo       .oo       .oo       .oo       .oo       .55         3601s       .00       .07       .13       .14       .14       .04       .oo       .oo       .oo       .55	3506s	.05	.06	.23	.36	.29		.09	.05		1.24
3601s .00 .07 .13 .14 .14 .04 .00 .00 .00 .53	3507s	.16	.40	1.11			.45	.22	.17	.00	6.94
	3508s	.00						.00	.00	.00	.55
36025 .25 1.12 .98 .97 .35 .38 .38 .27 .00 4.70			.07								.53
	36025	.25	1.12	.98	.97	.35	.38	.38	.27	.00	4.70

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3603S	.04	.41	.53	.75	.56	.23	.06	.04	.00	
3607s	. 19	.60	1.96	5.10	2.58	.53	.36	.19	.00	
3610s	.29	1.16	.60	1.77	1.61	.60	-40	.29	.00	
3701s	.10	.28	.31	.38	.22	.13	. 14	.10	.00	
3703s	.10	.37	.77	1.16	-85	.28	.22	.10	.00	
3704s	.04	1.37	5.20	6.39	5.00	.97	.16	.04	.00	
3705s	.24	.68	.72	.58	.71	.56	.35	.27	.02	
3709s	.91	7.76	11.29	10.62	2.30	4.12	1.25	.88	.00	
3803s	.16	.40	.77	.89	.78	.36	.25	.20	.01	
3804s	.00	.01	.08	.41	.09	.00	.00	.00	.00	
3805s	.12	1.27	4.58	18.97	3.78	1.13	.30	.13	.00	
3806S	1.72	1.85	2.00	4.74	4.02	1.65	1.65	1.93	.00	
3807s	.04	.13	.40	.61	.55	.25	.05	.04	.00	
3808s	.03	.04	.06	.19	.28	.03	.05	.03	.00	
4101s	.24	.99	1.34	1.50	1.29	.87	.44	.33	.02	
41015 4102s	.00	.00	.07	.23	.92	.06	.00	.00	.00	
4102s 4105s	.10	.58	1.40	3.79	1.73	.44	.23	.10	.00	
4106S	.72	.35	.97	2.18	2.87	1.25	.59	.65 25	.01	
4107s	.25	.68	3.40	10.49	16.21	2.54	.35	.25	.00	
4108s	.00	.00	.14	4.77	1.63	.03	.00	.00	.00	
4201s	.11	.25	.30	.79	1.30	.32	.13	.12	.00	
42033	.34	.75	1.27	1.43	1.85	1.05	.45	.34	.00	
4205s	.06	.65	.69	.57	.73	.40	.24	.07	.00	
4207s	.39	1.42	2.79	5.43	3.93	1.63	.65	.48	.03	
4303s	.01	.03	.13	.16	.13	.07	.02	.01	.00	
305s	.15	.30	.18	.05	.13	.21	.17	. 15	.00	
403s	.14	.36	.64	.56	.58	.43	.22	. 14	.00	
404s	.00	.00	.00	.00	.00	.00	.00	.00	.00	
405s	.01	.13	1.09	1.56	1.20	.09	.02	.01	.00	
4065	.00	.00	.05	4.08	5.18	.00	.00	.00	.00	
407s	.05	.16	.60	.93	.95	.31	.07	.06	.00	
4407s	.00	.00	.00	.25	.23	.04	.00	.00	.00	
					4.67				.09	
4601S	1.44	8.27	11.13	16.41		5.24	2.30	1.91 <b>.12</b>		
4603S	.10	.75	1.55	2.69	1.11	.38	.20		.00	
4605S	.06	.00	.00	.00	.06	.00	.04	.04	.00	
606S	.00	.00	.00	.05	.04	.00	.00	.00	.00	
607s	.51	1.35	2.45	3.12	3.74	1.43	.65	.51	.00	
1701s	.10	.72	1.49	3.08	2.12	.91	.19	.11	.00	
7025	.05	.19	1.23	2.44	2.91	1.87	.32	.05	.00	
1707s	.95	3.13	4.86	5.93	7.60	5.57	1.35	1.15	.07	
801S	.21	1.08	2.64	5.84	3.09	1.53	.58	.24	.00	
1803s	.12	.76	1.39	.79	1.05	.82	.17	.12	.00	
8048	1.33	11.52	18.00	21.87	8.50	8.13	4.58	1.39	.00	
805s	.44	.23	.69	1.24	.83	.36	.34	.41	.00	
807s	.00	. 19	.42	2.25	3.03	.69	.00	.00	.00	
1808s	.61	2.73	2.52	2.40	3.49	2.44	1.50	.85	.06	
1809s	.62	7.62	10.98	13.38	4.68	1.82	.92	.60	.00	
903s	.03	.06	.15	.10	.06	.05	.04	.03	.00	
1903s	.00	.15	1.31	1.69	1.41	.02	.01	.00	.00	
905s	.20	.75	1.88	3.47	1.85	.55	.31	.21	.00	
905s 907s	.06	.26	1.88	2.22	1.85	.93	.09	.07	.00	
908s	.00	.02	.02	.08	.12	.04	.00	.00	.00	
910s	.36	2.01	4.84	1.87	2.71	4.21	.77	.49	.03	
201s	.72	2.04	2.90	2.31	2.41	2.97	1.43	.93	.08	
202s	.22	.80	9.07	12.33	33.74	3.45	1.23	.22	.00	
205s	.11	.35	.60	.66	.55	.40	.15	.11	.00	
5303s	.01	.04	.05	.07	.05	.03	.02	.01	.00	
5304s	.00	.00	.00	.00	.00	.00	.00	.00	.00	
	.09	.40	2.17	12.71	2.45	.21	.20	.09	.00	
5305s	.07									

53083	.05	.16	.21	.24	.18	.20	.08	.07	.01	1.20
5311s	.02	.06	.08	.08	.06	.05	.03	.02	.00	.40
7605s	.50	1.17	2.11	2.71	1.56	.95	.67	.60	.02	10.29
7606s	.02	.06	.14	.19	.10	.06	.02	.02	.00	.60
7607s	.11	.38	.75	.95	΄1.05	.38	. 14	.11	.00	3.88
76129	.08	.22	.50	1.09	1.15	.59	.12	.09	.00	3.84
7801s	.05	.17	.34	.45	.52	.22	.07	.05	.00	1.87
7803s	.12	.22	.28	.20	.18	.20	.15	.08	.00	1.43
8001s	.05	.13	.25	.42	.38	.17	.07	.05	.00	1.51
80035	.08	.17	.21	.15	.13	. 15	.11	.09	.00	1.09
OTOTALS	33.82	140.33	543.26	1181.42	1144.84	465.16	65.44	37.44	1.15	3612.86
		LINK-B	Y,-LINK	ALL-TIME	-SLICES	- AVERAGE	SPEED	OF A CAR	(KM/H)	RUN ON 11/6/91

**ITERATION NUMBER 3** 

## SMART CORRIDOR BASE RUN NETWORK and TIME DATA (6/11/91) SMART CORRIDOR BASE DEMAND SMART CORRIDOR CONTROL DATA

											TIERATION NO	WIDER
		E SLIC	ES :									
LINK	1	2		3	4	5	6	7	8	9		
NO.&											OVERA	
TYPE											AVERAGE S	SPEED
	600	630	700	730	800	830	900	930	1000	1300		
7U	87.	7 07	.7	87.7	87.7	87.7	87.7	87.7	87.7	.0	87	7
90 8u	86.1		.1	81.7	51.4	28.9	86.1	86.1	86.1	.0	60.	
9U	87.		.8	68.9	33.3	52.9	86.4	87.8	87.8	.0	60	
100	91.		.2	74.7	53.2	71.8	74.4	91.2	91.2	.0	73	
110	86.		. 6	72.5	48.5	60.3	75.1	86.6	86.6	.0	68.	
120	88.			70.4	47.4	56.4	71.3	88.8	88.8	88.8	67.	
120 13u	86.		5.7	42.2	25.4	26.5	59.9	86.7	86.7	86.7	43.	
14U	94.3		.1	65.3	29.0	24.2	94.1	94.1	94.1	94.1	49	
140 15u	87.			87.8	87.8	87.8	87.8	87.8	87.8	87.8	87.	
15U 16U	88.4			88.4	88.4	88.4	88.4	88.4	88.4	88.4	88.	
180 17U	86.3			86.3	86.3	86.3	86.3	86.3	86.3	86.3	86.	
180	87.0			87.0	87.0	87.0	87.0	87.0	87.0	87.0	87.	
190	86.			86.0	86.0	86.0	86.0	86.0	86.0	86.0	86	
20u	87.			87.8	87.8	87.8	87.8	87.8	87.8	87.8	87.	
20u 21u	87.		. 6	42.9	83.4	82.8	86.6	88.6	88.6	88.6	73.	
21u 22u	87.3			87.3	78.3	73.5	74.2	87.3	87.3	87.3	81.	
22U 23U	86.1			86.1	65.1	65.2	78.3	86.1	86.1	86.1	77	
230 24U	86.			86.1	67.1	57.3	78.5	86.6	86.6	86.6	75.	
240 250				83.8	49.4	48.4	71.4	91.5	91.5	91.5		
250 260	91.			73.0	49.4	48.5	70.8	86.9	86.9	91.5 86.9	68.	
	86.			79.1				86.7		95.9		
27U	95.		.9	38.0	62.4 20.3	41.5 19.8	66.4 22.6	76.3	95.9 89.4		68 .	
28U	89.					19.8 95.9	22.0 95.9	95.9	89.4 95.9	89.4 95.9	31.	
29U	95.			95.9	95.9 87.0	95.9 87.0	95.9 87.0				95.	
3ou	87.0			87.0	87.0 89.7	89.7	87.0 89.7	87.0	87.0 89.7	87.0	87.	
31u	89. 95.9			89.7 95.9	89.7 95.9	95.9	89.7 95.9	89.7 95.9	95.8	89.7 95.9	89	
32U				95.9 87.8	95.9 87.8	95.9 87.8		87.8	95.8 87.8	.0	95. 87.	
5ou	87.8 87.1				87.8	87.8	87.8 87.1	87.1	87.1	.0		
51u				87.1 88.6	88.6	88.6	88.6	88.6		.0	87.	
52U	88.0								88.6		88.	
53u	86.1			86.1	86.1	86.1	86.1	86.1	86.1	86.1	86.	
54u	87.8			87.8	87.8	87.8	87.8	87.8	87.8	87.8	87.	
55u	88.8			88.8	88.8	88.8	88.8	88.8	88.8	88.8	88.	
56U	87.0			87.0	87.0	87.0	87.0	87.0	87.0	87.0	87.	
570	87.8			87.1	80.5	79.4	87.8	87.8	87.8	87.8	84.	
58U	94.1			39.2	26.1	79.0	94.1	94.1	94.1	94.1	52.	
59U	86.3	8 86	. 3	86.1	83.4	84.1	86.3	86.3	86.3	86.3	85.	.3

60U	94.1	94.1	44.4	25.4	85.1	94.1	94.1	94.1	94.1	
61U	86.9	86.9	72.9	66.1	67.7	86.9	86.9	86.9	86.9	
620	87.5	87.5	86.4	67.1	62.9	78.5	87.5	87.5	87.5	
63U	87.3	87.3	78.3	56.0	60.7	71.4	87.3	87.3	87.3	
64U	88.1	88.1	41.5	28.1	37.0	62.4	88.1	88.1	88.1	
65U	89.1	89.1	89.1	89.1	52.7	85.2	89.1	89.1	89.1	
66u	90.9	90.9	90.9	90.9	30.7	76.0	90.9	90.9	90.9	
67U	89.4	89.4	89.4	60.5	49.8	76.7	89.4	89.4	89.4	
68U	87.5	87.5	85.3	58.4	35.7	49.4	87.5	87.5	87.5	
69U	87.0	87.0	79.7	51.7	43.2	82.8	87.0	87.0	87.0	
7ou	87.8	87.8	76.4	43.2	35.0	47.5	73.2	87.8	87.8	
710	87.2	87.2	37.9	21.3	18.8	20.6	71.1	87.2	87.2	
720	87.0	87.0	87.0	87.0	87.0	87.0	87.0	87.0	87.0	
80U	86.9	86.9	86.9	86.9	86.9	86.9	86.9	86.9	.0	
810	86.9	86.9	86.9	86.9	86.9	86.9	86.9	86.9	.0	
82U	90.0	90.0	90.0	90.0	90.0	90.0	90.0	90.0	.0	
820 830	90.0 90.0	90.0	90.0 90.0	90.0	90.0 90.0	90.0	90.0	90.0	.0 <b>.0</b>	
830 84U					90.0 90.0	90.0	90.0 90.0	90.0		
	90.0	90.0	90.0	90.0					0.	
85U	90.0	90.0	90.0	90.0	90.0	90.0	90.0	90.0	90.0	
86U	90.0	90.0	90.0	90.0	90.0	90.0	90.0	90.0	90.0	
87U	90.0	90.0	90.0	90.0	90.0	90.0	90.0	90.0	.0	
120s	51.4	51.4	51.4	51.4	51.4	51.4	51.4	51.4	.0	
121s	50.0	50.0	32.7	11.1	9.1	31.7	50.0	50.0	.0	
122s	50.0	50.0	45.9	18.5	16.4	29.4	50.0	50.0	.0	
1235	51.4	51.4	51.4	39.9	30.2	45.7	51.4	51.4	.0	
124S	50.0	50.0	50.0	50.0	50.0	50.0	50.0	50.0	50.0	
125S	51.4	51.4	51.4	51.4	51.4	51.4	51.4	51.4	51.4	
126S	.0	51.4	51.4	51.4	51.4	.0	.0	.0	.0	
127S	51.4	51.4	51.4	47.2	39.2	48.1	51.4	51.4	.0	
128S	51.4	51.4	44.5	21.6	17.6	51.4	51.4	51.4	.0	
150s	51.4	51.4	51.4	51.4	51.4	51.4	51.4	51.4	.0	
151s	50.0	50.0	50.0	50.0	50.0	50.0	50.0	50.0	.0	
152s -	50.0	50.0	50.0	50.0	50.0	50.0	50.0	50.0	.0	
153s	51.4	51.4	51.4	49.1	50.2	51.4	51.4	51.4	.0	
154s	50.0	50.0	50.0	26.9	33.3	50.0	50.0	50.0	.0	
155s	51.4	51.4	30.0	26.6	26.3	33.7	51.4	51.4	.0	
1565	51.4	51.4	51.4	17.0	12.6	15.9	51.4	51.4	.0	
157s	50.4	50.4	20.0	6.7	4.3	7.6	32.5	50.4	.0	
158s	50.4 51.4	51.4	20.0 51.4	51.4	4.3 51.4	7.8 51.4	51.4	51.4	.0	
					51.4 41.2			51.4 43.3		
202s	43.3	43.3	43.3	41.2		43.2	43.3		.0	
205S	49.8	49.8	49.2	49.2	49.8	49.8	49.8	49.8	49.8	
206S	0.	53.0	52.9	49.9	50.9	.0	.0	.0	.0	
209S	43.3	43.3	43.3	43.3	43.3	43.3	43.3	43.3	.0	
211s	49.8	49.2	48.7	47.2	47.3	49.3	49.8	49.8	.0	
301s	46.2	46.2	46.2	46.2	46.2	46.2	46.2	46.2	.0	
303s	48.4	48.4	48.4	48.4	48.4	48.4	48.4	48.4	.0	
304s	48.4	47.0	47.0	44.9	44.7	48.1	48.4	48.4	.0	
309s	46.2	46.2	46.2	46.2	46.2	46.2	46.2	46.2	46.2	
703s	42.9	42.9	42.9	42.9	42.9	42.9	42.9	42.9	.0	
704s	.0	.0	57.3	55.2	47.7	.0	.0	.0	.0	
705s	45.7	45.0	44.0	39.2	41.4	45.0	45.7	45.7	46.4	
901s	34.7	33.2	33.2	33.2	34.7	33.2	34.7	34.7	34.7	
902S	34.7	34.7	33.2	31.7	34.7	34.7	34.7	34.7	.0	
905s	46.1	46.1	46.2	45.3	45.3	46.1	46.1	46.1	.0	
906s	46.1	43.8	40.2		43.3 24.9	40.5	45.3	46.1	.0	
9003 907s	40.1 49.7		40.7 49.7	32.3 49.7	24.9 49.7	40.5 49.7	43.3 49.7	40.1 49.7	.0 .0	
		49.7								
908S	49.7	49.1	49.1	45.5	43.3	48.3	49.7	49.7	.0	
909s	33.2	31.8	31.7	31.8	33.2	33.1	33.2	33.2	34.7	
1001s	33.8	32.1	32.0	33.0	33.8	32.7	33.8	33.8	33.8	
1002s	19.6	15.5	14.5	14.1	14.6	15.7	19.0	19.6	.0	

2502s	50.9	50.9	48.9	39.6	43.7	50.9	50.9	50.9	.0
25058	43.9	42.6	41.4	39.2	39.4	42.6	43.3	43.9	.0
2506s	43.9	42.0	41.4	39.7	39.3	42.0	43.2	43.9	.0
2507S	43.4	43.4	43.0	42.4	42.7	43.4	43.4	43.4	.0
2508S	.0	.0	42.9	42.1	.0	.0	.0	.0	.0
2601s	38.9	38.9	37.9	37.9	37.9	38.9	38.9	38.9	.0
2602s	32.0	27.2	27.1	25.7	29.9	30.0	31.3	32.0	.0
26035	46.1	45.4	44.7	44.7	45.4	45.4	45.4	46.1	.0
2607S	31.3	30.5	29.2	25.3	29.4	30.9	31.3	31.3	.0
2610s	44.7	39.1	39.6	40.1	40.6	42.2	43.8	44.7	.0
2701s	48.5	48.5	48.5	48.5	48.5	48.5	48.5	48.5	.0
							37.9		
2703s	37.9	36.9	36.2	34.4	36.0	36.9		37.9	0. 0
27043	34.3	30.6	29.9	32.0	33.1	32.3	33.5	34.3	.0
2705S	29.0	28.3	27.6	27.3	26.3	28.3	29.0	29.0	.0
2709s	48.5	47.2	43.8	43.5	42.1	46.8	47.5	48.5	.0
2803s	50.4	50.4	49.9	50.0	49.9	50.4	50.4	50.4	.0
2804s	.0	50.4	48.2	43.6	47.4	49.4	.0	.0	.0
2805s	47.3	47.4	45.9	43.6	43.8	47.3	47.3	47.3	.0
2806S	.0	46.9	34.2	32.5	25.4	46.7	49.8	.0	.0
28075	47.3	47.3	47.3	47.3	47.3	47.3	47.3	47.3	.0
2808S	47.3	46.6	45.8	45.8	46.6	46.6	47.3	47.3	.0
2810s	42.7	42.7	42.4	37.4	41.5	42.7	42.7	42.7	.0
2010s 3001s	51.0	50.3	49.1	48.7	48.8	50.3	50.3	51.0	.0 51.0
						45.7	46.3	46.8	
3005s	46.8	45.8	44.0	41.3	42.0				0. 0
3006S	45.8	41.8	36.0	23.3	21.1	37.0	44.4	45.8	.0
3007s	43.9	43.3	40.5	33.2	37.7	44.0	43.9	43.9	.0
3011s	43.6	34.4	17.9	13.9	18.5	37.9	41.2	43.6	.0
3101s	35.3	34.3	33.8	33.8	33.8	34.8	34.8	34.8	34.8
3102s	30.0	28.8	27.7	29.2	29.2	29.2	30.0	30.0	.0
3103s	46.7	46.1	45.6	46.0	45.7	46.1	46.7	46.7	46.7
3107s	27.0	24.7	22.0	13.3	14.4	25.4	27.0	27.0	.0
3110s	47.2	46.7	47.2	47.2	47.2	47.2	47.2	47.2	.0
3110s 3201s	49.2	48.0	47.8	48.0	48.0	48.1	48.5	48.6	48.8
3203s	36.0	36.0	36.0	36.0	36.0	36.0	36.0	36.0	.0
32043	31.8	25.0	20.7	25.0	24.9	26.4	30.2	31.8	36.0
32053	30.9	30.9	29.8	29.8	29.2	30.9	30.9	30.9	.0
3303s	50.6	50.8	50.8	50.6	50.6	50.6	50.6	50.6	.0
3305s	49.8	49.4	46.6	36.6	44.7	49.3	49.8	49.8	.0
3306S	48.6	38.4	34.4	26.3	28.5	39.2	47.1	49.0	.0
3307s	45.8	45.8	45.3	44.5	45.6	45.9	45.8	45.8	.0
3308S	45.8	45.8	45.8	45.8	45.8	45.8	45.8	45.8	.0
3501s	43.0 52.1	43.0 52.1	52.1	52.1	52.1	52.1	52.1	52.1	.0
3502s	.0	.0	51.3	49.4	47.0	.0	.0	.0	.0
3505s	49.5	49.1	48.7	48.0	48.7	49.1	49.5	49.5	.0
3506S	48.6	48.2	46.0	43.9	44.7	47.4	47.8	48.6	.0
3507s	47.6	47.8	46.7	45.8	45.5	47.6	47.6	47.6	.0
3508s	.0	.0	.0	39.3	39.2	.0	.0	.0	.0
3601S	39.3	39.3	38.1	38.4	38.1	39.3	39.3	39.3	.0
3602S	29.5	22.7	23.0	23.0	28.5	28.2	28.2	29.5	.0
36036	50.8	50.4	50.5	50.0	50.2	50.4	50.8	50.8	.0
3607S	30.9	30.0	27.5	19.6	25.4	30.0	30.1	30.9	.0
3610s				44.5		48.1	49.2	49.6	.0
	49.6	46.7	48.1		44.3				
3701s	48.3	48.3	48.3	47.5	48.3	48.3	48.3	48.3	.0
3703s	41.8	40.5	40.2	39.3	39.3	40.5	41.8	41.8	.0
3704s	27.6	16.0	6.7	5.0	6.0	16.4	27.6	27.6	.0
3705s	30.0	28.4	28.4	28.5	28.4	29.2	29.2	30.0	30.9
3709s	43.3	23.1	18.0	17.7	36.4	30.6	41.6	43.3	48.3
38033	50.0	50.0	49.1	49.1	49.1	50.0	50.0	50.0	50.0
3804s	.0	50.0	47.3	41.6	46.7	.0	.0	.0	.0
3805s	48.8	47.1	41.5	24.5	40.9	47.2	48.4	48.8	.0
30038	40.0	<b>=</b> /.⊥	41.3	44.3	-0.7	-1.4		-0.0	.0

3806s	32.2	30.0	31.1	20.4	22.9	29.3	32.9	29.6	.0	27.4
3807s	49.0	49.0	48.5	48.2	48.1	48.5	49.0	49.0	.0	48.4
3808S	49.0	48.5	48.6	47.4	46.2	48.5	48.5	49.0	.0	47.5
4101s	51.1	50.7	50.3	50.2	50.3	50.7	51.1	51.1	51.1	50.5
4102s	.0	.0	44.2	42.5	31.5	44.7	.0	.0	.0	36.7
4105s	47.5	47.0	45.6	40.9	45.1	47.0	47.5	47.5	.0	44.2
4106s	35.7	40.3	33.4	25.9	17.1	29.4	36.7	37.4	49.0	29.5
4107s	47.4	46.5	41.8	30.0	24.3	37.7	46.9	47.4	.0	32.8
4108s	.0	.0	45.9	22.0	34.9	39.6	.0	.0	.0	27.9
42015	43.7	43.7	43.9	42.5	35.0	38.3	43.7	43.7	.0	40.4
42015 4203s	49.9			49.2	48.8		49.9		.0 .0	
		50.0	49.5			48.9		49.9 25.5		49.3
4205s	34.8	32.7	32.5	32.7	32.7	33.7	35.0	35.5	.0	33.1
4207s	40.0	36.8	32.7	25.9	30.2	36.5	39.2	39.1	40.9	32.2
4303s	53.5	53.5	51.9	51.9	51.9	52.5	53.5	53.5	.0	52.3
4305s	26.3	25.7	26.3	27.0	25.7	26.3	26.3	26.3	.0	26.2
4403s	27.0	27.0	25.3	26.3	25.2	27.0	27.0	27.0	.0	26.2
4404s	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
4405s	50.6	50.6	49.5	48.7	49.5	50.7	50.6	50.6	.0	49.3
44068	.0	.0	49.9	26.7	23.3	.0	.0	.0	.0	25.7
4407s	49.7	49.8	49.2	48.6	48.4	49.3	49.7	49.7	.0	48.9
44088	.0	49.7	49.9	47.9	48.0	49.3	.0	.0	.0	48.4
4601s	30.7	15.6	12.9	9.6	21.2	20.1	28.0	29.0	36.0	16.7
4603s	30.4	27.4	23.2	20.6	25.4	28.8	28.8	30.4	.0	23.9
								27.2		
4605s	27.2	.0	.0	.0	27.2	.0	27.2		.0	27.2
46068	.0	.0	.0	25.5	26.3	.0	.0	.0	0.	25.9
4607S	41.9	41.2	39.8	38.3	37.0	40.8	41.9	41.9	.0	39.4
4701s	28.0	24.3	21.8	17.4	21.0	24.1	26.5	28.0	.0	21.0
4702s	25.2	20.5	8.8	5.4	4.7	6.8	19.4	25.2	.0	7.4
4707s	20.3	15.6	11.6	9.1	6.4	8.5	18.8	19.5	22.6	11.0
4801s	28.4	25.6	20.2	12.3	15.3	20.4	27.2	28.4	.0	17.8
4803s	21.9	20.2	18.4	19.6	19.5	20.1	23.2	21.9	.0	19.7
4804s	14.0	3.3	1.7	1.6	3.4	4.3	5.6	13.6	.0	3.2
4805s	31.8	32.7	31.6	30.2	31.1	31.8	32.4	31.8	.0	31.3
4807s	.0	27.8	27.3	16.9	16.0	23.6	.0	.0	.0	18.5
4808\$	24.0	13.3	15.0	14.1	11.9	14.4	18.0	21.9	28.4	15.1
4809s	23.2	5.9	4.0	3.5	6.8	15.8	20.7	23.2	.0	6.5
4903s	38.3	38.8	38.5	38.3	38.3	38.3	38.3	38.3	38.3	38.4
4903s	38.3	29.1	14.2	10.7	13.8	30.7	38.3	38.3	.0	13.9
4905s	39.4	38.4	34.5	29.8	34.4	38.4	39.4	39.4	.0	34.2
4907s	50.6	50.6	49.3	48.0	48.4	49.7	50.6	50.6	.0	48.9
4908s	50.6	50.6	50.6	50.3	49.9	50.6	50.6	50.6	.0	50.2
4910s	33.3	21.2	12.6	21.0	18.3	14.2	28.6	32.0	37.9	18.4
5201s	26.1	23.7	21.8	22.9	22.9	21.6	24.5	25.2	27.0	23.1
5202s	25.2	20.7	4.6	4.1	1.6	8.6	16.9	25.2	.0	4.0
5205s	38.3	37.5	36.7	36.7	36.7	37.5	38.3	38.3	.0	37.1
5303s	30.2	30.2	30.2	30.2	30.2	30.2	30.2	30.2	.0	30.2
5304s	.0	.0	.0	.0	.0	.0	.0	.0	.0	.0
5305s	37.1	36.0	30.2	12.5	23.1	36.0	36.0	37.1	.0	19.3
5307s	37.5	35.8	29.0	13.6	6.4	8.8	36.6	37.5	39.4	13.8
5308s	38.4	37.9	37.6	37.6	37.5	37.7	38.4	38.4	39.4	37.8
5311s	37.1	36.0	36.0	36.0	36.0	36.0	37.1	37.1	.0	36.2
7605s	48.4	47.6	46.0	45.3	46.8	47.5	48.3	48.3	.0 49.1	46.8
7605s 7606s			46.7		47.5	48.3		40.3		
	49.2	48.3		46.0			49.2		.0 0	47.3
7607s	51.2	50.7	50.7	50.1	50.1	50.6	51.2	51.2	.0	50.5
7612s	50.6	50.1	49.0	46.8	46.1	48.5	50.6	50.6	.0	48.0
7801s	38.8	34.9	34.9	32.7	32.2	34.9	38.8	38.8	.0	34.1
7803s	41.8	41.8	41.8	41.8	41.8	41.8	41.8	45.3	.0	42.1
8001s	48.8	48.8	48.8	46.9	46.7	48.8	48.8	48.8	.0	47.8
8003s	38.9	38.9	38.8	38.8	38.8	38.8	38.8	38.8	38.8	38.8
OOVERALL	75.4	72.6	58.8	45.0	43.8	56.4	74.4	75.9	83.6	56.1