# THE JOURNAL OF PHYSICAL CHEMISTRY

Subscriber access provided by King Abdullah University of Science and Technology Library

## **Feature Article**

# Modeling Plasma-based CO2 and CH4 Conversion in Mixtures with N2, O2 and H2O: the Bigger Plasma Chemistry Picture

Weizong Wang, Ramses Snoeckx, Xuming Zhang, MinSuk Cha, and Annemie Bogaerts

J. Phys. Chem. C, Just Accepted Manuscript • DOI: 10.1021/acs.jpcc.7b10619 • Publication Date (Web): 18 Jan 2018 Downloaded from http://pubs.acs.org on January 23, 2018

## **Just Accepted**

"Just Accepted" manuscripts have been peer-reviewed and accepted for publication. They are posted online prior to technical editing, formatting for publication and author proofing. The American Chemical Society provides "Just Accepted" as a free service to the research community to expedite the dissemination of scientific material as soon as possible after acceptance. "Just Accepted" manuscripts appear in full in PDF format accompanied by an HTML abstract. "Just Accepted" manuscripts have been fully peer reviewed, but should not be considered the official version of record. They are accessible to all readers and citable by the Digital Object Identifier (DOI®). "Just Accepted" is an optional service offered to authors. Therefore, the "Just Accepted" Web site may not include all articles that will be published in the journal. After a manuscript is technically edited and formatted, it will be removed from the "Just Accepted" Web site and published as an ASAP article. Note that technical editing may introduce minor changes to the manuscript text and/or graphics which could affect content, and all legal disclaimers and ethical guidelines that apply to the journal pertain. ACS cannot be held responsible for errors or consequences arising from the use of information contained in these "Just Accepted" manuscripts.



The Journal of Physical Chemistry C is published by the American Chemical Society. 1155 Sixteenth Street N.W., Washington, DC 20036 Published by American Chemical Society. Copyright © American Chemical Society. However, no copyright claim is made to original U.S. Government works, or works produced by employees of any Commonwealth realm Crown government in the course of their duties.

## Modeling Plasma-based CO<sub>2</sub> and CH<sub>4</sub> Conversion in Mixtures with N<sub>2</sub>, O<sub>2</sub> and

## H<sub>2</sub>O: the Bigger Plasma Chemistry Picture

Weizong Wang<sup>\*, 1, (a)</sup>, Ramses Snoeckx<sup>\*, 1, 2, (a)</sup>, Xuming Zhang<sup>2, 3</sup>, Min Suk Cha<sup>2</sup> and Annemie Bogaerts<sup>\*</sup>,<sup>1</sup>

1. Research group PLASMANT, Department of Chemistry, University of Antwerp, Universiteitsplein

1, B-2610 Wilrijk-Antwerp, Belgium

2. King Abdullah University of Science and Technology (KAUST), Clean Combustion Research Center (CCRC), Thuwal 23955, Saudi Arabia

3. College of Environmental Science and Engineering, Zhejiang Gongshang University, Xiasha High Education District, Hangzhou, Zhejiang Province, China

Corresponding Author

\*E-mail: wangweizong@gmail.com, ramses.snoeckx@uantwerpen.be,

annemie.bogaerts@uantwerpen.be

(a) These authors contributed equally to this work

**ABSTRACT:** Due to the unique properties of plasma technology, its use in gas conversion applications is gaining significant interest around the globe. Plasma-based CO<sub>2</sub> and CH<sub>4</sub> conversion have become major research areas. Many investigations have already been performed regarding the single component gases, i.e. CO<sub>2</sub> splitting and CH<sub>4</sub> reforming, as well as for two component mixtures, i.e. dry reforming of methane (CO<sub>2</sub>/CH<sub>4</sub>), partial oxidation of methane (CH<sub>4</sub>/O<sub>2</sub>), artificial photosynthesis (CO<sub>2</sub>/H<sub>2</sub>O), CO<sub>2</sub> hydrogenation (CO<sub>2</sub>/H<sub>2</sub>), and even first steps towards the influence of N<sub>2</sub> impurities have been taken, i.e. CO<sub>2</sub>/N<sub>2</sub> and CH<sub>4</sub>/N<sub>2</sub>. In this feature article we briefly discuss the advances made in literature for these different steps from a plasma chemistry modeling point of view. Subsequently, we present a comprehensive plasma chemistry set, combining the knowledge gathered in this field so far, and supported with extensive experimental data. This set can be used for chemical kinetics plasma modeling for all possible combinations of CO<sub>2</sub>, CH<sub>4</sub>, N<sub>2</sub>, O<sub>2</sub> and H<sub>2</sub>O, to investigate the bigger picture of the underlying plasmachemical pathways for these mixtures in a dielectric barrier discharge plasma. This is extremely valuable for the optimization of existing plasmabased CO<sub>2</sub> conversion and CH<sub>4</sub> reforming processes, as well as for investigating the influence of N<sub>2</sub>, O<sub>2</sub> and H<sub>2</sub>O on these processes, and even to support plasma-based multi-reforming processes.

## 1. INTRODUCTION: PLASMA TECHNOLOGY

Today—more than ever—plasma technology lies at the base of modern technology, as the entire microelectronics industry relies on plasma-surface interactions. <sup>1-2</sup> These interactions make it possible for scientists to extend Moore's law by providing the current nanometer resolution of microprocessors.

In general, plasma consists of various types of ions (both positive and negative), electrons and a large variety of neutral species, i.e. different types of atoms, molecules, radicals and excited species. This makes plasma a highly reactive—but complex—chemical cocktail, which is of interest to many potential applications.<sup>1,3-4</sup>

Plasma is often referred to as the 'fourth state of matter'. Indeed, upon increasing energy input, matter transforms in the sequence: solid, liquid, (neutral) gas and finally ionized gas or plasma. Although plasma might not be so widely known as the other three states of matter, 99 % of the visible universe is actually in plasma state, mainly as stars (including our Sun) and interstellar matter. Furthermore, natural plasmas also occur on Earth, in the form of most natural occurring weather phenomena which emit light, e.g. lightning, auroras (Borealis and Australis), Saint Elmo's fire, and red sprites.

Beside natural plasmas, two main groups of man-made plasmas are distinguished, i.e. high temperature or fusion plasmas and low temperature plasmas or gas discharges. The latter group can be further subdivided based on whether or not the plasma is in thermal equilibrium. Due to the multitude in different types of species, which can all have different temperatures and degrees of freedom, plasma can exhibit—and is defined by—multiple temperatures, e.g., gas temperature, electron temperature, ion temperature, vibrational temperature, rotational temperature. When—in a localized area—these temperatures are the same, the plasma is said to be in 'local thermodynamic equilibrium' (LTE), and mostly called a 'thermal plasma'. In the other case, the plasma is said to be in 'non-local thermodynamic equilibrium' (non-LTE), and mostly called a 'non-thermal plasma'.

One of the main reasons why low temperature (non-LTE) plasmas have such a large potential for a wide variety of applications, is their capability of producing a reactive chemical environment while staying at room temperature. This is possible due to most of the energy being directed into the electrons, leading to a much higher electron temperature ( $T_e$ ), compared to the gas temperature ( $T_g$ ). Subsequently, these highly energetic electrons can activate the gas and initiate reactions by electron impact collisions, rather than the classical form of energy used in industry, i.e. heat.

Applications range from materials science (e.g., coating deposition, surface modification, nanotechnology, and chip manufacturing, as mentioned above) over lighting, lasers, plasma displays (as plasma emits light due to the presence of many excited species), to analytical chemistry, thrusters, as well as environmental, energy and medical applications (e.g., sterilization, wound healing and even cancer treatment). <sup>1,3-4</sup> Environmental and energy applications include, among others, air pollution control, <sup>5</sup> nitrogen fixation from the air to form ammonia and nitric oxides, <sup>6-7</sup> hydrocarbon reforming <sup>8-10</sup> and CO<sub>2</sub> conversion into value-added chemicals and fuels. <sup>11</sup> These applications often use a combination of plasma with catalysts, yielding plasma catalysis.<sup>11-14</sup>

To improve these applications, a good knowledge of the underlying plasma processes is indispensable. The

latter can be obtained by experiments and computer modeling. As detailed measurements inside the plasma are not always straightforward, modeling can indeed be of great value. This feature article will focus on the continuous research efforts in modeling the plasma chemistry for the growing application of low temperature (non-LTE) plasmas used for  $CO_2$  conversion and  $CH_4$  reforming, as well as combinations with other gases, and highlight the contributions of the PLASMANT research group in this field.<sup>15-16</sup> Based on the gained knowledge so far, and an extensive set of experiments carried out for various gas mixtures and mixing ratios, a new comprehensive plasma chemistry model is presented that can be used to describe the underlying mechanisms of  $CO_2$  and  $CH_4$  conversion, also in the presence of  $N_2$ ,  $O_2$  and  $H_2O$ .

## 2. PLASMA CHEMISTRY MODELING FOR CO<sub>2</sub> CONVERSION AND CH<sub>4</sub> REFORMING

Interest in the application of plasma technology for  $CO_2$  conversion and  $CH_4$  reforming has been growing rapidly. <sup>9,11,17-20</sup> Due to the adverse effects of climate change on our society, the conversion of these gases into value-added chemicals and fuels is considered as one of the great challenges of the 21<sup>st</sup> century.<sup>21</sup> Successfully converting the greenhouse gas  $CO_2$  would be interesting from both an economic and ecological perspective. This would lead to the successful generation of an artificial closed carbon loop, which fits into the 'cradle-tocradle' concept,<sup>22</sup> i.e., upcycling waste material into new feedstock. Additionally, with the increase of biogas, landfill gas and hydrogenation of  $CO_2$  to  $CH_4$ , the straightforward reforming of  $CH_4$  into liquid products would be beneficial, because the energy density of liquid fuel is much higher and it is easier to transport.<sup>23-24</sup>

As outlined in an extensive recent review on the use of plasma technology for CO<sub>2</sub> conversion: <sup>11</sup> "Plasmas possess some important advantages over other (novel) technologies for the conversion of CO<sub>2</sub> and CH<sub>4</sub>: (i) they can operate at room temperature using any source of (renewable) electricity, (ii) they have a large flexibility in terms of the feeds that need to be processed, (iii) they provide an extremely flexible 'turnkey' process, which allows for the efficient storage of energy, peak shaving and grid stabilization, (iv) the reactors have low investment and operating costs, (v) they have a simple scalability both in size and applicability, and (vi) last but not least, the technology does not rely on rare earth materials—making it rather unique at this point. This unprecedented combination of features gives plasmachemical conversion a very high overall flexibility, making it an extremely useful and valuable technology for CCU."

To improve this application, several research groups developed models for chemical kinetics simulations, to better understand the underlying mechanisms, and a brief literature overview will be given below. This development can be subdivided in three main stages: (1) modeling single component molecular gases, i.e. plasma-based CO<sub>2</sub> splitting and CH<sub>4</sub> reforming; (2) investigating common two component mixtures, i.e. dry reforming of methane (CO<sub>2</sub>/CH<sub>4</sub>), partial oxidation of methane (CH<sub>4</sub>/O<sub>2</sub>), artificial photosynthesis (CO<sub>2</sub>/H<sub>2</sub>O) and CO<sub>2</sub> hydrogenation (CO<sub>2</sub>/H<sub>2</sub>); (3) moving towards more realistic gas mixtures by investigating the effect of N<sub>2</sub> both as admixture and impurity, i.e. CO<sub>2</sub>/N<sub>2</sub> and CH<sub>4</sub>/N<sub>2</sub>. The following subsections will be divided according to these three stages.

The knowledge obtained during these different stages is now combined into one comprehensive chemical kinetics plasma model for use in low temperature (non-LTE) plasmas, presented for the first time in this feature

article. Therefore, in the following subsections, we will each time compare the  $CO_2$  and/or  $CH_4$  conversion, calculated with this new model, with our previous (published) experimental data, in order to step-by-step validate the individual chemistry sets. This validation will be performed for a dielectric barrier discharge (DBD) plasma, as the chemistry model presented in this feature article is specifically developed for this type of plasma. A DBD plasma is created by applying a potential difference between two electrodes, of which at least one is covered by a dielectric barrier. For  $CO_2$  and  $CH_4$  conversion applications, a tubular DBD reactor is most often used,<sup>11</sup> consisting of an inner electrode surrounded by a dielectric tube, covered by an outer electrode (see Figure 1).



Figure 1. Schematic diagram of a dielectric barrier discharge (DBD).

Subsequently, in section 3 we will present this new comprehensive chemical kinetics plasma model for use in low temperature (non-LTE) plasmas. The applications of this extensive model are broad. They can range from very specific investigations, like the effect of  $CH_4$  on  $NO_x$  mitigation for  $CO_2/N_2$  plasmas, to realistic industrial gas mixtures for dry reforming of methane by inclusion of  $N_2$ , as well as unravelling the possibilities for plasmabased multi-reforming processes. Furthermore, this chemistry set can also be used as a foundation to build a comprehensive computational data set in the field of plasma-assisted combustion. <sup>25-26</sup> Finally, certain data from this set could even be used for exotic models, like planetary atmosphere and spacecraft re-entry modeling. <sup>27-28</sup>

#### 2.1 Single Component Molecular Gases

With the breakthrough of sufficient—and continuously increasing—computational power available to researchers, plasmachemical modeling efforts could expand from simple noble gases towards reactive molecular gases.

In the past 10 years many different plasmachemical kinetic models have been developed for pure  $CO_2$  splitting in various kinds of plasmas.<sup>9,29-49</sup> Several of these models have been developed in the research group

PLASMANT.<sup>29-39</sup> Furthermore, there is also interest in pure CH<sub>4</sub> reforming, also known as 'the pyrolysis of methane', used to synthesize higher hydrocarbons.<sup>9</sup> Few models exist in literature,<sup>50-53</sup> of which one has been developed in the research group PLASMANT.<sup>52</sup>

Figure 2 illustrates a comparison of the calculated CO<sub>2</sub> conversion, using our new comprehensive model (see section 3), with measured values for a pure CO<sub>2</sub> DBD plasma, <sup>29</sup> at a fixed plasma power of 40 W and varying the gas flow rate to yield different values of the specific energy input (SEI). The CO<sub>2</sub> conversion is mainly caused by electron impact dissociation at these conditions (see below and ref. (29)). The conversion gradually increases with rising SEI, both in the experiments and calculation results, which is logical as more energy is put into the system. Above 25 eV/molecule, the model does not show saturation yet, although it is observed in the experimental data. However, as described in the review of Snoeckx and Bogaerts,<sup>11</sup> these higher SEI values are not attractive, because of very low energy efficiency. The recommended SEI range is in the order of 0.1 to 5 eV/molecule. Therefore, we may conclude that the agreement between model and experiments is good, especially in the SEI region of most practical interest.



**Figure 2.** Comparison of the calculated  $CO_2$  conversion, as obtained from our new comprehensive plasma chemistry model, with measured data adopted from ref. 29, as a function of SEI, at a fixed plasma power of 40 W and varying gas flow rate.

#### 2.2 Two Component Mixtures

With even more computing power and the successful development of models for simulating single component molecular gases, as described above, the combination of these models into two component reactive mixtures was the logical—albeit not always easy—next step.

## 2.2.1 Dry Reforming and Partial Oxidation Of Methane

The combined conversion of CO<sub>2</sub> and CH<sub>4</sub>, also known as 'dry reforming of methane' (DRM) has been extensively studied, <sup>9,11</sup> and a variety of models have been developed in literature. <sup>54-66</sup> Again, several of these models have been developed within the research group PLASMANT.<sup>63-66</sup> Besides CO<sub>2</sub>, another—stronger—oxidant used to reform CH<sub>4</sub> is O<sub>2</sub>, and this combination is known as 'partial oxidation of methane' (POX). <sup>9</sup>

Several modeling investigations exist in literature, <sup>66-72</sup> including one from our group PLASMANT. <sup>66</sup> Although this process leads to higher CH<sub>4</sub> conversions than DRM, its strong oxidative character causes a total oxidation of CH<sub>4</sub>, producing CO<sub>2</sub>, and is therefore of less interest.

Figure 3 illustrates the calculated absolute conversions of  $CH_4$  and  $CO_2$  in plasma-based DRM as a function of discharge power using our new comprehensive model (see section 3), in comparison with experimental values obtained from Ref. (63), for a DBD in a 1:1  $CO_2/CH_4$  mixture at a total flow rate of 50 sccm. The  $CH_4$  and  $CO_2$  conversions both increase with discharge power, which is again logical, and the  $CH_4$  conversion is about a factor 1.5 higher than the  $CO_2$  conversion. Very good agreement is reached between calculated and experimental conversions.



**Figure 3.** Comparison of the calculated absolute conversion of  $CO_2$  and  $CH_4$ , as obtained from our new comprehensive plasma chemistry model, with measured data adopted from ref. (63), in a 1:1  $CO_2/CH_4$  mixture at a total flow rate of 50 sccm, as a function of discharge power.

## 2.2.2 Artificial Photosynthesis and CO<sub>2</sub> Hydrogenation

Research towards  $CO_2$  conversion in the presence of  $H_2O$  (artificial photosynthesis) and  $H_2$  ( $CO_2$  hydrogenation) is quite limited and to our knowledge the only models available are developed within the research group PLASMANT.<sup>73-74</sup>

In figure 4, the calculated absolute  $CO_2$  and  $H_2O$  conversions, as obtained from our new plasma chemistry model, are compared with experimental data for a DBD, as a function of water vapor content for a total gas flow rate of 600 mL/min at 323 K for a SEI value of 1.1 eV/molecule. Both the experimental and calculated absolute  $H_2O$  conversions show a slightly decreasing trend with increasing water vapor content, although the drop is more pronounced in the simulation results. This is probably due to some more complex processes taking place in the experiments as a result of water vapor, which could not be easily accounted for in the 0D plasma chemistry model. Indeed, the model does not take into account some physical effects, such as condensation and nebulization.<sup>73</sup> Furthermore, water cluster ions and surface processes, which might be important in a water discharge,<sup>75</sup> are not yet taken into account in our current model.

#### The Journal of Physical Chemistry

The experiments also show a slight drop in  $CO_2$  conversion with increasing water content. As explained in Ref. (73), this may result from destabilization of the discharge induced by the presence of water. This trend is also not captured by the simulation, but the agreement is still reasonable, because both simulations and experiments show that the addition of water vapor into  $CO_2$  only exerts a weak influence on the  $CO_2$  conversion.



**Figure 4.** Comparison of the calculated absolute conversion of  $CO_2$  and  $H_2O$ , as obtained from our new comprehensive plasma chemistry model, with measured data adopted from ref. (73), in a  $CO_2/H_2O$  mixture, as a function of water vapor content, for a SEI of 1.1 eV/molecule and a total flow rate of 600 mL/min at 323 K.

#### 2.3 Effect of N<sub>2</sub> as Impurity and Admixture

The modeling studies in the above two sections—and their experimental counterparts—are limited to high purity gases, hence without the presence of impurities. However, in the real world—for which we are trying to design industrial applications—this will never be the case.  $N_2$  will always be an important impurity or even admixture. This must be taken into account in modeling, since it is known that  $N_2$  can influence the plasma physics, and moreover,  $N_2$  has metastable states, which could influence the plasma chemistry. As a result, the next step in plasma chemistry modeling must be the inclusion of these real world impurities into existing models.

#### 2.3.1 Effect of N<sub>2</sub> on CH<sub>4</sub> Reforming

Few modeling studies exist in literature regarding the addition of  $N_2$  to the CH<sub>4</sub> reforming process,<sup>76-81</sup> but to our knowledge, the research group PLASMANT was the only one focusing on both the impurity and admixture level.<sup>81</sup>

The values for the absolute conversion of CH<sub>4</sub>, calculated with our new plasma chemistry model, are plotted versus N<sub>2</sub> content in figure 5, showing a good agreement with measured results, obtained in a DBD, for a residence time of 2.2 s and a SEI of 1.5 eV/molecule.<sup>81</sup> Upon addition of N<sub>2</sub>, the absolute CH<sub>4</sub> conversion first remains more or less constant or even slightly decreases, and subsequently it increases. This trend results from the interplay of several effects, i.e. the decreasing electron density with increasing N<sub>2</sub> content and the lower reaction rate constants for several three-body reactions with N<sub>2</sub> compared to CH<sub>4</sub> as third body cause a drop in absolute CH<sub>4</sub> conversion, but on the other hand N<sub>2</sub> can also enhance the absolute CH<sub>4</sub> conversion, due

to the dissociation of  $CH_4$  upon collision with  $N_2$  metastable molecules.



**Figure 5.** Comparison of the calculated absolute  $CH_4$  conversion, as obtained from our new comprehensive plasma chemistry model, with measured data adopted from ref. (81), in a  $CH_4/N_2$  mixture as a function of  $N_2$  content, for a residence time of 2.2 s and a SEI of 1.5 eV/molecule.

## 2.3.2 Effect of N<sub>2</sub> on CO<sub>2</sub> Splitting

Investigating the influence of  $N_2$  present during the conversion of  $CO_2$  is of vital importance, since most  $CO_2$  effluent gases contain large fractions of  $N_2$ , and the combined presence of N- and O-species is bound to lead to the formation of unwanted  $NO_x$  byproducts. The only modeling studies performed here are from the research group PLASMANT. <sup>82-83</sup>



**Figure 6.** Comparison of the calculated absolute  $CO_2$  conversion, as obtained from our new comprehensive plasma chemistry model, with measured data adopted from ref. (83), in a  $CO_2/N_2$  mixture as a function of  $N_2$  content, for a residence time of 0.73 s and a SEI of 3.0 eV/molecule.

Figure 6 illustrates the absolute  $CO_2$  conversion, calculated with the new plasma chemistry model, in comparison with our previous experimental data, <sup>83</sup> in a  $CO_2/N_2$  mixture as a function of the N<sub>2</sub> content, for a

residence time of 0.73 s and a SEI of 3.0 eV/molecule, showing again a very good agreement. The absolute  $CO_2$  conversion increases more or less exponentially with rising  $N_2$  fraction, both in the experiments and the calculations. This indicates that  $N_2$  has a beneficial effect on  $CO_2$  splitting, due to the dissociation of  $CO_2$  upon collision with  $N_2$  metastable molecules (mainly  $N_2(A^3\Sigma_u^+)$ ).

## 3. COMPREHENSIVE CHEMICAL KINETICS PLASMA MODEL

It is clear from the previous section that the new plasma chemistry model provides good agreement with our previous (published) experimental data for pure CO<sub>2</sub>, as well as binary mixtures (CO<sub>2</sub>/CH<sub>4</sub>, CO<sub>2</sub>/H<sub>2</sub>O,  $CH_4/N_2$  and  $CO_2/N_2$ ), which serves as an important first validation. In this section we will present for the first time the combination of all these chemistry models, and validate it against new experimental data in multicomponent mixtures. The temperature-controlled coaxial DBD reactor used for these new experiments has been introduced in previous work. 84-85 This new comprehensive chemistry model can be used to investigate any desired multi-component mixture, containing CO<sub>2</sub>, CH<sub>4</sub>, N<sub>2</sub>, O<sub>2</sub> and H<sub>2</sub>O in its feed. We will start by giving a brief explanation of the model, as well as an overview of the included plasma chemistry and how it was developed. Subsequently we will look into the results of some multi-component mixtures, i.e.  $CO_2/CH_4/N_2$ ; CO<sub>2</sub>/CH<sub>4</sub>/N<sub>2</sub>/O<sub>2</sub>; and CO<sub>2</sub>/CH<sub>4</sub>/N<sub>2</sub>/H<sub>2</sub>O. For these mixtures we will compare the calculated and measured conversions of  $CO_2$  and  $CH_4$ , and the product selectivities, at various gas mixing ratios, for the purpose of validation. Indeed, the present (experimental) results were not optimized; they were only obtained at a fixed condition of flow rate and power, so not focusing on the highest conversion or product selectivities, but they only serve to validate the new chemical kinetics model. Finally, we will discuss in detail the underlying chemistry as predicted by the model, in order to explain the observed trends in conversion and product selectivities.

## 3.1 Plasma Chemistry Model

There exist different types of models for non-LTE plasmas, <sup>86-88</sup> but the most straightforward approach to model a detailed plasma chemistry is a OD chemical kinetics model, also called global model. It is based on solving balance equations for the densities of the various plasma species (i.e., various types of molecules, radicals, atoms, ions, excited species, and the electrons), based on production and loss terms, as defined by chemical reactions. <sup>15-16</sup> Details of the model that is used here to describe the plasma chemistry of CO<sub>2</sub> and CH<sub>4</sub> conversion in the multi-component mixtures are presented in the Supporting Information.

As indicated in section 2, within the PLASMANT group several different plasma chemistry models have been developed in the past 5 to 10 years, not only for gas conversion applications, but also for other reactive gas mixtures. The most important chemistries used here for developing our new comprehensive plasma chemistry model for a DBD plasma, are (i) the pure CO<sub>2</sub> chemistry model of Aerts et al.<sup>29,33</sup>; (ii) a model containing the H<sub>2</sub>O/O<sub>2</sub> chemistry by van Gaens et al.<sup>89</sup>; (iii) the interaction of CO<sub>2</sub> and CH<sub>4</sub> in the DRM process developed by De Bie et al.<sup>65</sup> and Snoeckx et al.<sup>63</sup>; (iv) a chemistry set describing the interaction between CO<sub>2</sub> and H<sub>2</sub>O in the work of Snoeckx et al.<sup>73</sup>; (v) a model containing the CH<sub>4</sub>/N<sub>2</sub> chemistry by Snoeckx et al.<sup>81</sup>; and finally (vi) chemistry models describing the interaction in CO<sub>2</sub>/N<sub>2</sub> plasmas by Heijkers et al.<sup>82</sup> and Snoeckx et al.<sup>83</sup>. All these different chemistry models were developed and used to investigate specific problems in combination with experiments for pure CO<sub>2</sub> splitting, in humid air, for dry reforming of methane, artificial photosynthesis, and the influence of N<sub>2</sub> on CH<sub>4</sub> reforming and on pure CO<sub>2</sub> splitting, respectively. In this section we combine all this knowledge from previous research on the different single component, two component and impurity mixtures, to arrive at a new comprehensive chemistry model, which can be used to investigate any desired multi-component mixture containing CO<sub>2</sub>, CH<sub>4</sub>, N<sub>2</sub>, O<sub>2</sub> and H<sub>2</sub>O in its feed. To achieve this, the chemistry from the above mentioned models was adopted, adapted and expanded with additional reactions. This led to a model containing 137 species as listed in Table 1. Note that the model does not include vibrationally excited molecules, in contrast to other models developed within PLASMANT. <sup>30-38,82</sup> Indeed, the plasma chemistry model presented here is applied to a DBD plasma (see Section 2 and Figure 1), where vibrationally excited species are very important, <sup>30-32,34-38,82</sup> and thus, the model would have to be extended to these species, to account for their role in the conversion mechanisms (see Conclusions and Outlook).

These 137 species react with each other through 355 electron impact reactions, 631 ion reactions, and 743 neutral reactions. The full list of all these reactions can be found in the Supporting Information, together with their corresponding rate coefficients and the references where these data were adopted from. The model itself is based on solving balance equations for all species densities, with production and loss terms defined by chemical reactions, as explained in the Supporting Information. In addition, a Boltzmann equation is used to calculate the rate coefficients of all the electron impact reactions. The processes included in this Boltzmann equation are elastic collisions, electron impact vibrational excitation/de-excitation, electronic excitation/de-excitation (both dissociative and non-dissociative), electron attachment, as well as electron impact ionization of various important species (see table S1 in the Supporting Information).

As validation of this newly developed chemistry set, we compared the calculated conversions with measured values for different gas mixtures obtained from our earlier work; see figures 2-6 above. These simulations were performed for exactly the same operating conditions as in the experiments. Furthermore, additional experiments were performed for the new multi-component mixture containing  $CO_2$ ,  $CH_4$ ,  $N_2$ ,  $O_2$  and  $H_2O$ , for extra validation of the new model, which will be presented below. For more details of the model and the additional experiments, as well as the definitions of gas conversion and product selectivities, we refer to the Supporting Information.

Molecules	Charged species	Radicals	Excited species
$C_{3}H_{8}, C_{3}H_{6}, C_{2}H_{6}, C_{2}H_{4}, C_{2}H_{2}, CH_{4}$	$\begin{array}{c} C_2H_6^+,\ C_2H_5^+,C_2H_4^+,\ C_2H_3^+,\\ C_2H_2^+,\ C_2H^+,\ CH_5^+,\ CH_4^+\\ ,\ CH_3^+,\ CH_2^+,\ CH^+ \end{array}$	C <sub>4</sub> H <sub>2</sub> , C <sub>3</sub> H <sub>7</sub> , C <sub>3</sub> H <sub>5</sub> , C <sub>2</sub> H <sub>5</sub> , C <sub>2</sub> H <sub>3</sub> , C <sub>2</sub> H, CH <sub>3</sub> , CH <sub>2</sub> , CH	
CO <sub>2</sub> , CO	$\begin{array}{c} \text{CO}_2^+, \ \text{CO}^+, \text{CO}_3^-, \ \text{CO}_4^-, \\ \text{CO}_4^+, \text{C}_2\text{O}_4^+, \ \text{C}_2\text{O}_3^+, \ \text{C}_2\text{O}_2^+ \end{array}$	C <sub>2</sub> 0	CO <sub>2</sub> (E1), CO <sub>2</sub> (E2)
$C_2N_2$		CN, NCN	
$H_20, H_20_2$	$H_20^+, H_30^+, 0H^+, 0H^-$	HO <sub>2</sub> , OH	
$N_2H_4$ , $NH_3$ , $N_2H_2$	$\mathrm{NH}_4^+, \mathrm{NH}_3^+, \mathrm{NH}_2^+, \mathrm{NH}^+$	NH <sub>2</sub> , NH, N <sub>2</sub> H,	

Table 1. Overview of the species included in the model

		N <sub>2</sub> H <sub>3</sub>	
$N_20, N_20_3, N_20_4, N_20_5$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	NO, NO <sub>2</sub> , NO <sub>3</sub>	
СH <sub>2</sub> CO, CH <sub>3</sub> OH, CH <sub>3</sub> CHO , CH <sub>3</sub> OOH, C <sub>2</sub> H <sub>5</sub> OH, C <sub>2</sub> H <sub>5</sub> OOH, CH <sub>2</sub> O		CHO, $CH_2OH$ , $CH_3O$ , $CH_3O_2$ , $C_2HO$ , $CH_3CO$ , $CH_2CHO$ , $C_2H_5O$ , $C_2H_5O_2$	
HCN		H <sub>2</sub> CN	
	C <sub>2</sub> <sup>+</sup> , C <sup>+</sup>	ONCN,NCO C, C <sub>2</sub>	
N <sub>2</sub>	N <sub>2</sub> <sup>+</sup> , N <sup>+</sup> , N <sub>3</sub> <sup>+</sup> , N <sub>4</sub> <sup>+</sup>	N	$\begin{array}{c} N_{2}(a'\Sigma_{u}^{-}), \ N_{2}(C^{3}\Pi_{u}), \\ N_{2}(V), \ N_{2}(A^{3}\Sigma_{u}^{+}), \\ N_{2}(B^{3}\Pi_{g}) \ N(2P), \\ N(2D) \end{array}$
H <sub>2</sub>	$H_2^+, H^+, H^-, H_3^+,$	Н	H(2P), H <sub>2</sub> (V), H <sub>2</sub> (E)
0 <sub>3</sub> , 0 <sub>2</sub>	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0	0(1D), 0(1S), 0 <sub>2</sub> (a1),0 <sub>2</sub> (b1)
	e-		

#### 3.2 Plasma Conversion and Product Selectivity

## 3.2.1 CO<sub>2</sub>/CH<sub>4</sub>/N<sub>2</sub> Mixture: Varying CO<sub>2</sub> and N<sub>2</sub> Content

Effluent gas flows from industrial and Carbon Capture Sequestration/Utilization/Recycling (CCS/U/R) often contain impurities, of which in most cases  $N_2$  is the main component. Therefore, it is of interest to study the CO<sub>2</sub> and CH<sub>4</sub> conversion in the presence of N<sub>2</sub>. Figure 7 shows the measured and calculated absolute CO<sub>2</sub> and CH<sub>4</sub> conversions (a) and the product selectivities (b) plotted as a function of the CO<sub>2</sub> (and N<sub>2</sub>) content in a CO<sub>2</sub>/CH<sub>4</sub>/N<sub>2</sub> mixture, keeping the CH<sub>4</sub> content fixed at 10 %.

At all the gas mixing ratios investigated, the  $CH_4$  conversion is much higher than the  $CO_2$  conversion. This can be explained because the rate of electron impact dissociation of  $CH_4$  is higher than that of  $CO_2$ , due to the lower C-H bond dissociation energy. Although there is some small deviation in the exact trend with increasing  $CO_2$  content, in general the calculated values show reasonable agreement with the experiments.



**Figure 7.** Comparison of the calculated and measured conversion of  $CH_4$  and  $CO_2$  (a), and selectivities of the most important products (b), in a  $CO_2/CH_4/N_2$  mixture, as a function of the  $CO_2$  (and  $N_2$ ) content, for a fixed total flow rate of 200 ml/min and plasma power of 10 W, corresponding to an SEI of 0.76 eV/molecule. The  $CH_4$  content was fixed at 10 %, with the remainder being  $CO_2$  and  $N_2$ .

The CO<sub>2</sub>/CH<sub>4</sub> ratio has an important influence on the product selectivities, as is clear from figure 7(b). At low CO<sub>2</sub>/CH<sub>4</sub> ratio (CO<sub>2</sub> content of 5%), the selectivities of the hydrocarbons (mainly C<sub>2</sub>H<sub>6</sub>) are comparable or even slightly higher than that of CO. With increasing CO<sub>2</sub>/CH<sub>4</sub> ratio, the selectivities of the hydrocarbons and H<sub>2</sub> steadily decrease, while the CO selectivity increases, which is logical as CO is the major product of CO<sub>2</sub> splitting, while the hydrocarbons and H<sub>2</sub> originate from CH<sub>4</sub> dissociation. Increasing the CO<sub>2</sub>/CH<sub>4</sub> ratio from 0.5 to 4 yields a drop in the H<sub>2</sub>/CO ratio from 2.45 to 0.42. These results show that the H<sub>2</sub>/CO ratio can be varied in a wide range, simply controlled by the inlet gas mixing ratio. This is an advantage compared to classical processes, including steam reforming, partial oxidation, and CO<sub>2</sub> reforming, which typically produce syngas with H<sub>2</sub>/CO molar ratios of >3, <2, and <1, respectively. <sup>90-91</sup> Finally, we conclude from figure 7(b) that the calculated selectivities are in good agreement with the experiments.

## 3.2.2 CO<sub>2</sub>/CH<sub>4</sub>/N<sub>2</sub> Mixture: Varying N<sub>2</sub> Content



**Figure 8.** Comparison of the calculated and measured conversion of  $CH_4$  and  $CO_2$  (a), and selectivities of the most important products (b), in a  $CO_2/CH_4/N_2$  mixture, as a function of the  $N_2$  content, for a fixed 1:1  $CO_2/CH_4$  ratio, a fixed total flow rate of 200 ml/min and a corresponding SEI of 0.76 eV/molecule.

Figure 8 illustrate the effect of  $N_2$  content on the experimental and calculated absolute  $CO_2$  and  $CH_4$  conversions (a) as well as on the product selectivities (b) keeping the  $CO_2/CH_4$  ratio fixed at 1. Again good agreement is reached between calculated and measured results, especially for the conversions. Figure 8(a) shows that increasing the  $N_2$  content leads to a higher absolute conversion for both  $CO_2$  and  $CH_4$ , both in the experimental and simulation results. This is mainly caused by the increasing role of the  $N_2$  metastable states in the dissociation of both  $CO_2$  and  $CH_4$ , as will be discussed in more detail in section 3.3.

In our previous work, we investigated the effect of  $N_2$  for both pure CH<sub>4</sub> <sup>81</sup> and pure CO<sub>2</sub> splitting <sup>83</sup> and in both cases the presence of  $N_2$  led to unwanted effects, i.e. soot deposition and NO<sub>x</sub> production, respectively. However, when combining both gases into the current CO<sub>2</sub>/CH<sub>4</sub>/N<sub>2</sub> mixture, no excessive soot deposition or NO<sub>x</sub> production is observed. This can be explained by the chemical kinetics model. Indeed, the O-species, which react with N-species to form NO<sub>x</sub> in the CO<sub>2</sub>/N<sub>2</sub> mixture, form H<sub>2</sub>O in the presence of a hydrogen source due to the faster rates of the latter reactions. Vice versa, the O-species prevent the occurrence of soot deposition by oxidation of the carbon containing species.

The major products in this  $CO_{2/}CH_4/N_2$  mixture are again CO,  $H_2$ ,  $C_2H_6$  and  $C_3H_8$ . The measured and calculated selectivities show only a weak dependence on the  $N_2$  content within the investigated range, except

for the calculated  $H_2$  selectivity, which clearly rises upon rising  $N_2$  content, while the measured values show only a very weak increase. The calculated CO,  $H_2$  and  $C_2H_6$  selectivities are somewhat higher than the experimental data, which might be attributed to the limitation of the 0D model, neglecting transport and surface reactions. The latter may become important in some conditions. In contrast, excellent agreement between calculations and experiments is reached for the  $C_3H_8$  selectivity. In general, we consider the agreement between calculated and measured selectivities as fairly good, in view of the complex chemistry and the limitations of the 0D model.

It is worth to mention that, although the  $CO_2/CH_4$  ratio is kept constant, the experimental and calculated syngas (H<sub>2</sub>/CO) ratio slightly rises upon increasing N<sub>2</sub> content, i.e. from 1.16 to 1.40 in the experiments and from 0.97 to 1.96 in the calculated values, as can be deduced from the rising H<sub>2</sub> selectivities and the decreasing CO selectivities in figure 8 (b). The reason for the latter will be explained in section 3.3 below.

#### 3.2.3 CO<sub>2</sub>/CH<sub>4</sub>/N<sub>2</sub>/O<sub>2</sub> Mixture: Varying O<sub>2</sub> (and N<sub>2</sub>) Content

In literature, POX is widely used because  $O_2$  is very effective for low-temperature plasma activation of methane. However, a possible drawback of POX is an excessive oxidation, resulting in the formation of  $CO_2$ . The use of  $CO_2$  as a milder oxidant with a little addition of  $O_2$  may combine the advantages of DRM and POX and have a positive influence on the products formed. Therefore, we also investigate the influence of  $O_2$  addition on the  $CO_2$  and  $CH_4$  conversions, as well as on the product selectivities, as presented in figures 9 (a) and 9 (b), respectively.

The addition of  $O_2$  leads to a higher CH<sub>4</sub> conversion while the CO<sub>2</sub> conversion decreases. Indeed, POX becomes the dominant process over DRM. As a result, part of the converted CH<sub>4</sub> is oxidized towards CO and CO<sub>2</sub>, which explains the lower CO<sub>2</sub> conversion. The calculated CH<sub>4</sub> conversion is in good agreement with experiments, but there is some discrepancy for the CO<sub>2</sub> and O<sub>2</sub> conversion. This might be attributed to the occurrence of carbon deposition on the surface of the DBD reactor, which will be oxidized to CO and CO<sub>2</sub> by O-species. Since the model does not take surface reactions into account, this process is neglected, which could explain the somewhat higher CO<sub>2</sub> conversion in the model than in the experiments. Furthermore, this may also explain the deviation in the calculated and measured O<sub>2</sub> conversion and the underestimated CO selectivity (see figure 9 (b). However, we consider the agreement still as satisfactory, in view of the complex chemistry and limitations of the model.





**Figure 9.** Comparison of the calculated and measured conversions of  $CH_4$ ,  $CO_2$  and  $O_2$  (a), and selectivities of the most important products (b), in a  $CO_2/CH_4/N_2/O_2$  mixture, as a function of the  $O_2$  (and  $N_2$ ) content, for a 1:1  $CO_2/CH_4$  ratio, a fixed total flow rate of 200 ml/min and a corresponding SEI of 0.76 eV/molecule. The  $CO_2$  and  $CH_4$  content were both 10 %, with the remainder being  $O_2$  and  $N_2$ .

Both the experiments and calculations show that the addition of  $O_2$  rapidly decreases the selectivities of the hydrocarbons (mainly  $C_2H_6$  and  $C_3H_8$ ) and  $H_2$ , because of their oxidation into CO and  $H_2O$ . Indeed, the CO selectivity rises dramatically for the same reason. This also leads to a significant drop in the syngas ratio upon increasing  $O_2$  content from 0 to 8 %, i.e. from 1.23 to 0.17 in the experiments, and from 1.34 to 0.25 in the calculations. Again, with some exceptions as explained above, quite good agreement is reached between the calculations and experiments.

## 3.2.4 CO<sub>2</sub>/CH<sub>4</sub>/N<sub>2</sub>/H<sub>2</sub>O Mixture: Varying H<sub>2</sub>O (and N<sub>2</sub>) Content

An interesting co-reactant and hydrogen source for the conversion of  $CO_2$  is  $H_2O$ . It is the most ubiquitous and cheapest hydrogen source available, especially compared to  $CH_4$  and  $H_2$ . In addition, the combined conversion of  $CO_2$  and  $H_2O$  to produce value-added products using renewable energy would successfully mimic the natural photosynthesis process. Our previous study, however, revealed that this process is not an interesting one to pursue by means of plasma technology, due to a severe drop in  $CO_2$  conversion and energy efficiency when adding  $H_2O$ .<sup>73</sup> This was mainly attributed to the recombination of CO with OH into  $CO_2$ , as well as the recombination of H atoms with O atoms into OH and subsequently  $H_2O$ .<sup>73,92</sup> However, from figure 10 (a), it becomes clear that the combined conversion of  $CH_4$  and  $CO_2$  remains almost unchanged upon addition of  $H_2O$ . Hence, the presence of  $CH_4$  seems to counteract the negative effect of  $H_2O$  addition, because the H atoms originating from  $CH_4$  dissociation can recombine with the OH radicals, and thus suppress their negative effect, as there will be less OH available for the back reaction from CO to  $CO_2$ . Furthermore, the syngas ratio increases (from 1.35 to 1.65 in the experiments, and from 1.34 to 1.50 in the model) upon increasing  $H_2O$  content from 0 to 8 %, which means that the added  $H_2O$  is successfully converted into  $H_2$  as well, and the formation of  $H_2O$  from O and H atoms is limited due to Le Chatelier's principle. <sup>93</sup> Figure 10 (b) shows that the selectivities of both  $H_2$  and CO slightly increase with rising  $H_2O$  content, indicating that  $H_2O$  addition is beneficial for the production of syngas. Again, in general good agreement is obtained between the experimental and calculated selectivities of the most important products as a function of the  $H_2O$ content.



**Figure 10.** Comparison of the calculated and measured conversion of  $CH_4$  and  $CO_2$  (a), and selectivities of the most important products (b), in a  $CO_2/CH_4/N_2/H_2O$  mixture, as a function of the  $H_2O$  (and  $N_2$ ) content, for a 1:1  $CO_2/CH_4$  ratio, a fixed total flow rate of 200 ml/min and a corresponding SEI of 0.76 eV/molecule. The  $CO_2$  and  $CH_4$  content were both 10 %, with the remainder being  $H_2O$  and  $N_2$ .

## 3.3 Underlying Mechanisms of Plasma-based CO<sub>2</sub> and CH<sub>4</sub> Conversion

As the agreement between calculated and measured conversions and product selectivities is quite good, in a wide range of gas mixtures and mixing ratios, we can conclude that our chemical kinetics model can provide

a realistic picture of the plasma chemistry of the DBD reactor for the multi-component mixtures containing  $CO_2$ ,  $CH_4$ ,  $N_2$ ,  $O_2$  and  $H_2O$  in its feed. Thus, we can now discuss in more detail the underlying plasma chemistry, as predicted by the model, for both the  $CO_2$  and  $CH_4$  conversion, as well as for the formation of CO,  $H_2$ ,  $C_2H_6$  and  $C_3H_8$  in the presence of  $N_2$ . Similar results, but for the effect of  $O_2$  and  $H_2O$  addition, are presented in the SI. This is the most powerful aspect of plasma chemistry modeling. Indeed, a detailed analysis of the reaction pathways allows us to gain a better insight in the underlying chemical reactions and in the overall process. This in turn can help to optimize existing processes, overcome ongoing problems, find new research areas and advance the steps towards a future industrial application of plasma-based gas conversion processes.

## 3.3.1 CO<sub>2</sub> Conversion

Process	Loss reaction	Process	Formation reaction
L1	$CO_2 + e \rightarrow e + CO + O$	F1	$CO + C_2O_3^+ + M \rightarrow CO_2 + C_2O_2^+ + M$
L2	$\mathrm{CO}_2 + \mathrm{N}_2(\mathrm{A}^3\Sigma^+_\mathrm{u}) \to \mathrm{N}_2 + \mathrm{CO} + \mathrm{O}$	F2	$CO + C_2O_4^+ + M \rightarrow CO_2 + C_2O_3^+ + M$
L3	$\mathrm{CO}_2 + \mathrm{N}_2 (\mathrm{B}^3 \Pi_\mathrm{g}) \rightarrow \mathrm{N}_2 + \mathrm{CO} + \mathrm{O}$	F3	$0 + CH_3CO \rightarrow CO_2 + CH_3$
		F4	$CO + OH \rightarrow CO_2 + H$
		F5	$CO_3^- + C_2O_2^+ \to CO_2 + 0 + CO + CO$
		F6	$\mathrm{CH}_4 + \mathrm{CO}_2^+ \to \mathrm{CO}_2 + \mathrm{CH}_4^+$
		F7	$CO_3^- + H_3O^+ \to CO_2 + H_2O + H + O$
		F8	$e + CO_4^+ \rightarrow CO_2 + O_2$
		F9	$CH_2 + O_2 \rightarrow CO_2 + H + H$

Table 2. Dominant	CO <sub>2</sub> loss	and formation	reactions.
-------------------	----------------------	---------------	------------



**Figure 11.** Relative contributions of the main processes leading to  $CO_2$  loss (a) and formation (b) for a  $CO_2/CH_4/N_2$  mixture, as a function of the  $CO_2$  (and  $N_2$ ) content. The total flow rate is fixed at 200 ml/min and the plasma power is 10 W, corresponding to an SEI of 0.76 eV/molecule. The CH<sub>4</sub> content was fixed at 10 %, with the remainder being  $CO_2$  and  $N_2$ .

Table 2 lists the most important loss (L1-L3) and formation (F1-F9) processes for CO<sub>2</sub>, and figure 11 shows their relative contributions for a CO<sub>2</sub>/CH<sub>4</sub>/N<sub>2</sub> mixture. The CH<sub>4</sub> content was fixed at 10 %, with the remainder being CO<sub>2</sub> and N<sub>2</sub>. In the SI, we present similar results for a CO<sub>2</sub>/CH<sub>4</sub>/N<sub>2</sub> mixture at fixed CO<sub>2</sub>/CH<sub>4</sub> ratio, as well as upon addition of O<sub>2</sub> or H<sub>2</sub>O.

In the absence of  $O_2$  and  $H_2O$  (figure 11) and at high  $CO_2$  content (and thus low  $N_2$  content), the most important dissociation reaction of  $CO_2$ , at the present DBD conditions, is electron impact dissociation (L1) into CO and O, while at low  $CO_2$  content (and high  $N_2$  content), the dissociation reaction with metastable  $N_2(A^3\Sigma_u^+)$ molecules (L2) is dominant, yielding the same splitting products (CO and O). The reaction with metastable  $N_2(B^3\Pi_g)$  molecules (L3) also has a non-negligible contribution to the dissociation of  $CO_2$ . Upon higher  $N_2$ contents (lower  $CO_2$  contents), the electron energy is gradually being used for  $N_2$  excitation instead of  $CO_2$ dissociation, explaining the drop in the relative contribution of electron impact dissociation and the corresponding increase in the relative contribution of dissociation by  $N_2$  metastable molecules, which provides an alternative dissociation mechanism for  $CO_2$ . The same behavior can be seen in the  $CO_2/CH_4/N_2$  mixture with fixed (1:1)  $CO_2/CH_4$  ratio (see figure S1 (a) in the SI) and in the presence of  $O_2$  (figure S2 (a)) as well as in the presence of  $H_2O$  (figure S3 (a) in the SI). Thus, at high  $N_2$  content, the major loss process of  $CO_2$  is due to  $N_2$  metastable states (reactions L2 and L3) and this explains why the presence of  $N_2$  enhances the CO<sub>2</sub> conversion (See figure 8 in section 3.2.2).

If we take a look at the CO<sub>2</sub> formation in the CO<sub>2</sub>/CH<sub>4</sub>/N<sub>2</sub> mixture, the most significant processes are the ones between CO and the positive ions  $C_2O_3^+$  and  $C_2O_4^+$ , through three-body reactions (F1, F2) as well as the neutral reactions between O atoms and CH<sub>3</sub>CO molecules (F3); see figure 11 (b) as well as figure S1 (b) in the SI. A similar conclusion can be obtained for the addition of H<sub>2</sub>O (figure S3 (b) in the SI).

With the addition of  $O_2$ , the behavior is a bit different. Indeed, the  $CO_2/CH_4/O_2$  mixture gives rise to a high concentration of OH radicals. As a result, the reaction between CO and OH, leading to  $CO_2$  and H atoms, becomes the dominant  $CO_2$  formation process at  $O_2$  contents above 5 % (see figure S2 (b): F4). This explains why the addition of  $O_2$  leads to a decrease in  $CO_2$  conversion as indicated in figure 9 in section 3.2.3. This was also the case in our previous study for a  $CO_2/H_2O$  mixture, and resulted in a drop in  $CO_2$  conversion upon  $H_2O$  addition. <sup>73</sup> In the  $CO_2/CH_4/N_2/H_2O$  mixture, however, the addition of  $H_2O$  does not cause a drop in absolute  $CO_2$  conversion, as presented in figure 10 above, because the presence of  $CH_4$ , and thus H atoms, counteracts the negative effect of the OH radicals, as explained in section 3.2.4 above.

Besides the recombination between CO and OH (F4), electron recombination with  $CO_4^+$  (F8) and the reaction between O<sub>2</sub> and CH<sub>2</sub> (F9), which are quasi negligible for CO<sub>2</sub> production in the other gas mixtures, also become important upon addition of O<sub>2</sub> (figure S2 (b)). Other reactions involving ions (F5, F6, and F7) can also contribute to the CO<sub>2</sub> formation, but with a relative contribution no more than 10%.

Finally, it is important to realize that the total formation rate of  $CO_2$  is much smaller (no more than 10%) than the total  $CO_2$  loss rate for a  $CO_2/CH_4/N_2$  mixture, as well as a  $CO_2/CH_4/N_2/H_2O$  mixture, so the formation processes only have a minor contribution to the net  $CO_2$  conversion at these conditions. However, the addition of  $O_2$  enhances the formation of  $CO_2$ . With the addition of 8%  $O_2$ , the total  $CO_2$  formation rate reaches 41% of the total  $CO_2$  loss rate.

#### 3.3.2 CH<sub>4</sub> Conversion

Table 3. Dominant CH<sub>4</sub> loss and formation reactions.

Process	Loss reaction	Process	Formation reaction
L1	$CH_4 + e \rightarrow e + CH_3 + H$	F1	$CH_3 + H + M \rightarrow CH_4 + M$
L2	$CH_4 + CH \rightarrow C_2H_4 + H$	F2	$e + C_3H_8 \rightarrow CH_4 + e + C_2H_4$
L3	$CH_4 + N_2(a'\Sigma_u^-) \rightarrow N_2 + C + 2H_2$	F3	$\mathrm{CH}_5^+ + \mathrm{H}_2\mathrm{O} \to \mathrm{CH}_4 + \mathrm{H}_3\mathrm{O}^+$
L4	$CH_4 + N_2(A^3\Sigma_u^+) \rightarrow N_2 + CH_3 + H$		
L5	$CH_4 + N_2(a'\Sigma_u^-) \rightarrow N_2 + CH_3 + H$		
L6	$CH_4 + N_2(a'\Sigma_u^-) \rightarrow N_2 + CH_2 + H_2$		
L7	$CH_4 + 0 \rightarrow CH_3 + 0H$		

L8  $CH_4 + OH \rightarrow CH_3 + H_2O$ 



Figure 12. Relative contributions of the main processes leading to  $CH_4$  loss (a) and formation (b) for a  $CO_2/CH_4/N_2$  mixture, as a function of the  $CO_2$  (and  $N_2$ ) content. The total flow rate is fixed at 200 ml/min and the plasma power is 10 W, corresponding to an SEI of 0.76 eV/molecule. The  $CH_4$  content was fixed at 10 %, with the remainder being  $CO_2$  and  $N_2$ .

Table 3 lists the most important loss (L1-L8) and formation (F1-F3) processes for CH<sub>4</sub> and in figure 12 the relative contributions of these processes are plotted as a function of CO<sub>2</sub> (and N<sub>2</sub>) content in the CO<sub>2</sub>/CH<sub>4</sub>/N<sub>2</sub> mixture, at fixed CH<sub>4</sub> content of 10 %, with the remainder being CO<sub>2</sub> and N<sub>2</sub>. The results in the CO<sub>2</sub>/CH<sub>4</sub>/N<sub>2</sub> mixture with fixed CO<sub>2</sub>/CH<sub>4</sub> ratio, as well as upon addition of O<sub>2</sub> or H<sub>2</sub>O, are presented in figures S4-S6 of the SI.

It is clear from figure 12 that the dominant loss reactions change with increasing CO<sub>2</sub> content (N<sub>2</sub> content). Electron impact dissociation of CH<sub>4</sub> (L1) is always an important loss process at the present DBD conditions. It shows little dependence on the CO<sub>2</sub> content in figure 12. The reaction between CH and CH<sub>4</sub> leading to C<sub>2</sub>H<sub>4</sub> and H (L2) is also relatively important for CH<sub>4</sub> dissociation at low CO<sub>2</sub> content. The same applies for the reactions with N<sub>2</sub> metastable singlet and triplet states (reactions L3-L6, and especially L4).

Figure 12 shows that the dissociation process of CH<sub>4</sub> by metastable nitrogen molecules (L3+L4+L5+L6)

could be more important than the direct electron impact processes (L1). The rate coefficients of these processes are subject to some uncertainties, and this will affect the exact values of the relative contributions of these processes, predicted by the model. Nevertheless, we expect the general trends to be valid. Indeed, similar conclusions were made in literature, <sup>81</sup> using the same reaction rate coefficients as in our work for the reactions with  $N_2$  metastable singlet and triplet states (reactions L3-L6), and good agreement was reached with experiments, regardless of the conditions.

With increasing CO<sub>2</sub> content, the reactions between CH<sub>4</sub> and O atoms or OH radicals (L7 and L8) become increasingly important, and their relative contribution towards CH<sub>4</sub> loss even exceeds the contribution of electron impact dissociation (L1) at the highest CO<sub>2</sub> contents (and lowest N<sub>2</sub> contents) investigated. It should be noted that electron impact vibrational excitation of CH<sub>4</sub> is also important as loss process for the CH<sub>4</sub> ground state molecules, but this process is only taken into account in our model as energy loss for the electrons, and not as a chemical loss process for CH<sub>4</sub>, because the vibrationally excited species are not considered separately in our model. Indeed, electron impact vibrational excitation mainly takes place in the lower electron energy range, and thus it is of lower importance when the reduced electric field (i.e., ratio of electric field over gas density) is quite high, such as in a DBD plasma.<sup>33</sup>

In the  $CO_2/CH_4/N_2$  mixture with fixed 1:1  $CO_2/CH_4$  ratio, a similar behavior is observed (see figure S4 (a) in the SI), except that the relative contribution of electron impact dissociation clearly drops upon increasing  $N_2$  content, because of the drop in CH<sub>4</sub> content. With high  $N_2$  content, the dissociation of CH<sub>4</sub> due to collisions with  $N_2$  metastable states (reactions L3–L6) becomes most important, explaining why the presence of  $N_2$  enhances the CH<sub>4</sub> conversion (see figure 8 in section 3.2.2).

Upon addition of  $O_2$  to the mixture, the loss reaction of  $CH_4$  with OH radicals (L8) is dominant (figure S5 (a) in SI). Its relative contribution gradually increases with higher  $O_2$  contents, because the concentration of produced OH radicals rises during both the microdischarge filaments and afterglow stages of the DBD. The same applies, to a lower extent, for the loss reaction upon collision with O atoms (L7). This explains why the  $CH_4$  conversion rises drastically upon increasing  $O_2$  content (see figure 9 in section 3.2.3).

H<sub>2</sub>O addition has no significant effect on the relative contributions of the various loss processes, except that the reaction with N<sub>2</sub> metastable triplet states N<sub>2</sub>( $A^{3}\Sigma_{u}^{+}$ ) (L4) drops and the reaction with OH radicals (L8) rises (see figure S6 (a) in the SI), due to a decreasing concentration of N<sub>2</sub>( $A^{3}\Sigma_{u}^{+}$ ) and increasing concentration of OH radicals, respectively.

If we take a look at the formation processes, the three-body recombination of  $CH_3$  radicals with H atoms (F1) is the dominant formation process at all the investigated conditions (see figure 12 (b), as well as figures S4 (b), S5 (b) and S6 (b) in the SI). Other reactions, such as electron impact dissociation of  $C_3H_8$  into  $CH_4$  (F2) and charge transfer between  $H_2O$  and  $CH_5^+$  (F3), have relative contributions of less than 5% to the  $CH_4$  formation.

If we compare the total formation rate with the total loss rate of  $CH_4$ , we can conclude that the total formation rate is relatively large (up to 40%) compared to the total  $CH_4$  loss rate, at least without  $O_2$  addition.

Hence, this behavior is different from the  $CO_2$  loss and formation rates, as mentioned above. The reason is that the three-body recombination of  $CH_3$  radicals with H atoms is very important outside the microdischarge filaments in the DBD reactor (see SI for more details on how the microdischarge filaments in the DBD are treated: they are treated as afterglow in between discharge pulses). A similar behavior was reported by Snoeckx et al.<sup>63</sup> However, upon  $O_2$  addition, the formation processes have a decreasing contribution to the net  $CH_4$ conversion (formation rate no more than 10% of the total  $CH_4$  loss rate with 8%  $O_2$  addition), explaining again why the  $CH_4$  conversion drastically rises upon  $O_2$  addition (see figure 9).

## 3.3.3 CO Production

Process	Formation reaction	Process	Loss reaction
F1	$e + CO_2 \rightarrow CO + e + O$	L1	$CO + C_2O_3^+ + M \rightarrow C_2O_2^+ + CO_2 + M$
F2	$N_2(A^3\Sigma_u^+) + CO_2 \rightarrow CO + N_2 + O$	L2	$CO + C_2O_4^+ + M \rightarrow C_2O_3^+ + CO_2 + M$
F3	$CH_2O + O \rightarrow CO + OH + H$	L3	$CO + N \rightarrow CN + O$
F4	$N_2(B^3\Pi_g) + CO_2 \rightarrow CO + N_2 + O$	L4	$CO + CH + N_2 \rightarrow C_2HO + N_2$
F5	$H + CHO \rightarrow CO + H_2$	L5	$CO + H + M \rightarrow CHO + M$
		L6	$CO + OH \rightarrow CO_2 + H$
		L7	$CO + O(1D) \rightarrow CO_2$

 Table 4. Dominant CO formation and loss reactions.

N<sub>2</sub> content (%)

F5

(b)

(a)

Relative contribution (%)

Relative contribution (%)



Figure 13. Relative contributions of the main processes leading to CO formation (a) and loss (b) for a  $CO_2/CH_4/N_2$  mixture, as a function of the  $CO_2$  (and  $N_2$ ) content. The total flow rate is fixed at 200 ml/min and the plasma power is 10 W, corresponding to an SEI of 0.76 eV/molecule. The CH<sub>4</sub> content was fixed at 10 %, with the remainder being  $CO_2$  and  $N_2$ .

L7

CO, content (%)

As CO is the major product of the CO<sub>2</sub> conversion, with a selectivity of about 30–100 % (see figures 7-10 above), we present here the dominant reaction pathways for the formation and loss of CO, to obtain a better understanding of the influence of the CO<sub>2</sub>/CH<sub>4</sub> ratio, the N<sub>2</sub> content, and the addition of O<sub>2</sub> or H<sub>2</sub>O on the CO yield. Table 4 lists the most important formation (F1-F5) and loss (L1-L7) processes for CO. Their relative contributions in the CO<sub>2</sub>/CH<sub>4</sub>/N<sub>2</sub> mixture are plotted in figure 13, as a function of the CO<sub>2</sub> (and N<sub>2</sub>) content. The corresponding results at fixed CO<sub>2</sub>/CH<sub>4</sub> ratio, as well as upon addition of O<sub>2</sub> or H<sub>2</sub>O, are presented in figures S7-S9 of the SI.

Electron impact dissociation of CO<sub>2</sub> (F1), as well as dissociation of CO<sub>2</sub> upon collision with N<sub>2</sub> metastable singlet and triplet states (F2 and F4), are the dominant formation processes of CO, at all conditions investigated (see figure 13 (a), and figures S7 (a) and S9 (a) in the SI), except upon addition of O<sub>2</sub>. Furthermore, the reaction between CH<sub>2</sub>O and O, leading to CO, OH and H (F3), also plays a quite important role, and this process even becomes the prime source of CO when O<sub>2</sub> is added (see figure S8 (a) in the SI). This additional channel for CO production explains why the addition of O<sub>2</sub> leads to a drastic increase in CO selectivity (see figure 9).

As far as the loss of CO is concerned, the three-body reactions between CO and the positive ions  $C_2O_3^+$ 

and  $C_2O_4^+$  (L1, L2) are dominant at all conditions (see figure 13 (b), and figures S7 (b) and S9 (b) in the SI), except upon addition of O<sub>2</sub>. These two reactions are also the most important for CO<sub>2</sub> formation (see section 3.3.1 above). Upon addition of O<sub>2</sub>, however, the reaction of CO with OH becomes the most important route towards CO loss (L6, in figure S8 (b)), which is also the dominant process of CO<sub>2</sub> formation under these conditions.

Besides the CO loss reactions towards  $CO_2$  formation (L1, L2, L6, L7), other loss channels include the reaction of CO with N, leading to CN and O (L3), the reaction with CH, leading to C<sub>2</sub>HO (L4), and the reaction with H, producing CHO (L5), which have relative contributions up to 20 % at the conditions investigated.

Finally, it is important to realize that the total loss rate of CO is much smaller (no more than 6 %) than the total CO formation rate for all gas mixtures and mixing ratios investigated, so the loss processes only have a minor contribution to the net CO formation at these conditions.

#### 3.3.4 H<sub>2</sub> Production

Process	Formation reaction	Process	Loss reaction
F1	$N_2(a'\Sigma_u^-) + CH_4 \rightarrow 2H_2 + N_2 + C$	L1	$H_2 + C \rightarrow CH + H$
F2	$H_2CN + H \rightarrow H_2 + HCN$	L2	$H_2 + OH \rightarrow H_2O + H$
F3	$N_2(a'\Sigma_u^-) + CH_4 \rightarrow H_2 + N_2 + CH_2$	L3	$H_2 + e \rightarrow e + H + H$
F4	$e + C_2H_6 \rightarrow H_2 + e + C_2H_4$	L4	$H_2 + 0 \rightarrow 0H + H$
F5	$CH_2 + H \rightarrow H_2 + CH$	L5	$H_2 + N(2P) \rightarrow NH + H$
F6	$CH_3OH + H \rightarrow H_2 + CH_2OH$		
F7	$CHO + H \rightarrow H_2 + CO$		
F8	$CH_3OH + H \rightarrow H_2 + CH_3O$		
F9	$CH_3 + 0 \rightarrow H_2 + CO + H$		

Table 5. Dominant H<sub>2</sub> formation and loss reactions.



Figure 14. Relative contributions of the main processes leading to  $H_2$  formation (a) and loss (b) for a  $CO_2/CH_4/N_2$  mixture, as a function of the  $CO_2$  (and  $N_2$ ) content. The total flow rate is fixed at 200 ml/min and the plasma power is 10 W, corresponding to an SEI of 0.76 eV/molecule. The CH<sub>4</sub> content was fixed at 10 %, with the remainder being  $CO_2$  and  $N_2$ .

 $H_2$  is also a significant product, due to the CH<sub>4</sub> conversion, with a selectivity of about 10–50 % (see figures 7-10 above). Table 5 lists the most important formation (F1-F9) and loss (L1-L5) processes for  $H_2$  and figure 14 illustrates the relative contributions of these processes for the CO<sub>2</sub>/CH<sub>4</sub>/N<sub>2</sub> mixture at constant CH<sub>4</sub> content. The results for the other conditions can be found in figures S10 - S12 in the SI.

The most important production process at all conditions investigated is the reaction of CH<sub>4</sub> with N<sub>2</sub>(a' $\Sigma_u^-$ ) metastable singlet states, producing C atoms and two H<sub>2</sub> molecules (F1). This reaction of course becomes increasingly important with increasing N<sub>2</sub> content. Furthermore, electron impact dissociation of C<sub>2</sub>H<sub>6</sub> (F4) is an important formation process at lower N<sub>2</sub> content (see especially figure S10 (a)). The reaction of CH<sub>4</sub> with N<sub>2</sub>(a' $\Sigma_u^-$ ) towards the production of CH<sub>2</sub> radicals and one H<sub>2</sub> molecule (F3) also contributes to the H<sub>2</sub> production to some extent, as well as the reaction of H<sub>2</sub>CN, CH<sub>2</sub> radicals, CHO and CH<sub>3</sub>OH with H (reactions F2, F5-F8) and the reaction of CH<sub>3</sub> with O atoms (F9), depending on the conditions.

The dominant loss process is the reaction of  $H_2$  with a C atom producing a CH radical and a H atom (L1) at all gas mixing ratios (see figure 14 (b), and figures S10 (b) and S12 (b) of the SI), except upon addition of  $O_2$  (see figure S11 (b) in the SI). The relative contribution of this reaction, however, rapidly drops with increasing

 $CO_2$  content, because the C atom density decreases due to reaction with O-containing species, such as OH and  $O_2$ , which are directly or indirectly formed from  $CO_2$ . This also explains why the loss reaction with OH radicals (L2) becomes gradually more important upon rising  $CO_2$  content (see figure 14 (b)). The latter reaction is also dominant upon addition of  $O_2$  (see figure S11 (b) of the SI), for the same reason. The increasing role of reaction L2 in the loss of H<sub>2</sub> also explains why the selectivity of H<sub>2</sub> decreases upon addition of  $H_2$  (L3), oxidization of H<sub>2</sub> by O atoms generating OH and H (L4), and the reaction of H<sub>2</sub> with excited N atoms towards NH (L5), can also contribute to H<sub>2</sub> loss, but their relative contributions do not exceed 20% at the conditions investigated.

Finally, the total loss rate of  $H_2$  ranges from 13 % to 24 % of the total  $H_2$  formation rate for all gas mixtures and mixing ratios investigated, so the loss processes have a non-negligible contribution to the net  $H_2$  formation at these conditions. Especially  $O_2$  addition enhances the total loss rate of  $H_2$  via reaction L2, as mentioned above.

## 3.3.5 C<sub>2</sub>H<sub>6</sub> Production

Loss reaction Process Formation reaction Process  $C_2H_6 + e \rightarrow e + C_2H_4 + H_2$ F1  $CH_3 + CH_3 + M \rightarrow C_2H_6 + M$ L1  $C_2H_5 + H + M \rightarrow C_2H_6 + M$  $C_2H_6 + OH \rightarrow C_2H_5 + H_2O$ F2 L2 F3  $C_2H_5 + CH_3O \rightarrow C_2H_6 + CH_2O$ L3  $C_2H_6 + O \rightarrow C_2H_5 + OH$  $C_2H_5 + CHO \rightarrow C_2H_6 + CO$  $C_2H_6 + N_2(a'\Sigma_u^-) \rightarrow N_2 + C_2H_4 + H_2$ F4 L4  $C_2H_5 + C_2H_5 \rightarrow C_2H_6 + C_2H_4$  $C_2H_6 + N_2(A^3\Sigma_u^+) \rightarrow N_2 + C_2H_4 + H_2$ L5 F5 L6  $C_2H_6 + e \rightarrow e + C_2H_5 + H$ L7  $C_2H_6 + CH_2 \rightarrow C_3H_8$ 

**Table 6.** Dominant  $C_2H_6$  formation and loss reactions.





Figure 15. Relative contributions of the main processes leading to  $C_2H_6$  formation (a) and loss (b) for a  $CO_2/CH_4/N_2$  mixture, as a function of the  $CO_2$  (and  $N_2$ ) content. The total flow rate is fixed at 200 ml/min and the plasma power is 10 W, corresponding to an SEI of 0.76 eV/molecule. The CH<sub>4</sub> content was fixed at 10 %, with the remainder being  $CO_2$  and  $N_2$ .

Table 6 lists the most important formation (F1-F5) and loss (L1-L7) processes for  $C_2H_6$ . In figure 15, the relative contributions of these processes are plotted for a  $CO_2/CH_4/N_2$  mixture at fixed  $CH_4$  content. The results at the other conditions are given in figures S13-S15 of the SI.

The dominant formation channel for  $C_2H_6$  in all gas mixtures is three-body recombination of two  $CH_3$  radicals (F1), contributing for more than 60 % to the  $C_2H_6$  formation, and even up to 95 % upon addition of  $O_2$ . Upon addition of  $CO_2$  and  $O_2$ , the  $CH_3$  radicals are consumed by other competitive channels involving oxygen containing species, and this explains why the  $C_2H_6$  selectivity gradually decreases with the addition of  $CO_2$  and  $O_2$  (see figures 7 and 9). The second most important reaction is three-body recombination of  $C_2H_5$  with H (F2), while the other recombination reactions of  $C_2H_5$  with  $CH_3O$ , CHO and  $C_2H_5$  (F3-F5) are of minor importance.

The dominant loss reaction for  $C_2H_6$  at nearly all conditions investigated is electron impact dissociation into  $C_2H_4$  and  $H_2$  (L1). The reaction of  $C_2H_6$  with OH or O towards the production of  $C_2H_5$  (L2-L3) is also relatively important; see especially figure S13 (b) and figure S14 (b). Indeed, upon addition of  $O_2$ , L2 even becomes dominant (see figure S14 (b)). Finally, the dissociation of  $C_2H_6$  upon collision with  $N_2$  metastable molecules (both  $N_2(a'\Sigma_u^-)$  and  $(N_2A^3\Sigma_u^+)$ ) (L4 and L5) becomes gradually more important upon rising  $N_2$  content, as expected. This explains why the  $C_2H_6$  selectivity slightly decreases upon increasing  $N_2$  content in figure 8.

Finally, the total loss rate of  $C_2H_6$  is 42 to 60 % of the total  $C_2H_6$  formation rate for all gas mixtures and mixing ratios investigated, so the loss processes have a quite large contribution to the net  $C_2H_6$  formation at these conditions. Like for  $H_2$ , increasing the  $O_2$  content enhances the total loss rate of  $C_2H_6$ .

#### 3.3.6 C<sub>3</sub>H<sub>8</sub> Production

Process	Formation reaction	Process	Loss reaction
F1	$CH_3 + C_2H_5 + M \rightarrow C_3H_8 + M$	L1	$C_3H_8 + e \rightarrow e + C_3H_6 + H_2$
F2	$C_2H_6 + CH_2 \rightarrow C_3H_8$	L2	$C_3H_8 + e \rightarrow e + C_2H_4 + CH_4$
F3	$C_3H_7 + H \rightarrow C_3H_8$	L3	$C_3H_8 + e \rightarrow e + C_3H_7 + H$

Table 7. Dominant C<sub>3</sub>H<sub>8</sub> formation and loss reactions.



**Figure 16.** Relative contributions of the main processes leading to  $C_3H_8$  formation (a) and loss (b) as a function of the CO<sub>2</sub> (and N<sub>2</sub>) content, for a fixed total flow rate of 200 ml/min and plasma power of 10 W, corresponding to an SEI of 0.76 eV/molecule. The CH<sub>4</sub> content was fixed at 10 %, with the remainder being CO<sub>2</sub> and N<sub>2</sub>.

Table 7 lists the most important formation (F1-F3) and loss (L1-L3) processes for  $C_3H_8$ , while the relative

contributions of these processes for a  $CO_2/CH_4/N_2$  mixture at constant  $CH_4$  content are plotted in figure 16. The results for the other gas mixtures are again presented in the SI (figures S16-S18)

Three-body recombination of  $C_2H_5$  and  $CH_3$  radicals (F1) is the most important formation process. It contributes above 70 % at all conditions investigated, and even up to 90 % upon addition of  $O_2$  (figure S17 (a)). Finally, the loss of  $C_3H_8$  occurs almost entirely through electron impact dissociation (L1-L3 in decreasing order of importance) at all conditions investigated.

Finally, our calculations reveal that the loss of  $C_3H_8$  is quite significant compared to their production, because the total loss rate takes up around 38 to 46% of the total formation rate.

3.3.7 General Overview of the Reaction Pathways



**Figure 17.** Schematic overview of the dominant reaction pathways for the conversion of  $CH_4$  and  $CO_2$ , as well as  $N_2$ , in a 1:1:8  $CO_2/CH_4/N_2$  mixture, for a fixed total flow rate of 200 ml/min and plasma power of 10 W, corresponding to an SEI of 0.76 eV/molecule. The thickness of the arrow lines is linearly proportional to the rate of the net reactions. The most important molecules are indicated with a solid line frame, the molecules formed with lower densities are written in a frame with dashed lines, while the radicals are not written in a frame.

From the above detailed analysis of the dominant loss and formation reactions for  $CH_4$ ,  $CO_2$  and the major products, we can compose a general picture of the dominant reaction pathways in the plasma. This is summarized in figure 17 for a 1:1:8  $CO_2/CH_4/N_2$  mixture, at a fixed total flow rate of 200 ml/min and plasma power of 10 W, corresponding to an SEI of 0.76 eV/molecule.

The conversion process, at the present DBD conditions, starts with electron impact dissociation of CH4,

forming CH<sub>3</sub> radicals. Meanwhile, electron impact excitation of N<sub>2</sub> produces metastable singlet and triplet states, which also promote the dissociation of CH<sub>4</sub> towards CH<sub>3</sub>, CH<sub>2</sub>, CH radicals and C atoms. The CH<sub>3</sub> radicals will recombine toward higher hydrocarbons, i.e., mainly C<sub>2</sub>H<sub>6</sub> and C<sub>3</sub>H<sub>8</sub>. Moreover, the recombination between CH<sub>4</sub> and CH produces unsaturated hydrocarbons, i.e. mainly C<sub>2</sub>H<sub>4</sub>. The latter can recombine with H atoms into C<sub>2</sub>H<sub>5</sub> radicals, which further produce other hydrocarbons, such as C<sub>2</sub>H<sub>6</sub> and C<sub>3</sub>H<sub>8</sub>, as well as CH<sub>3</sub> radicals. Furthermore, dissociation of CH<sub>4</sub> and the higher hydrocarbons by electron impact and by collisions with N<sub>2</sub> metastable states yields the formation of H<sub>2</sub>.

At the same time, electron impact collisions with  $N_2$  also yield splitting of  $N_2$  into N atoms, which can react with  $CH_3$  radicals to generate  $H_2CN$ . The latter are not stable and quickly transform into hydrogen cyanide (HCN) upon impact with N or H atoms. At 80 %  $N_2$  content, our simulation shows that HCN is the most abundant N-containing end product (around 1600 ppm). This indicates that the presence—even in high concentrations—of  $N_2$  does not result in a significant production of N-containing species. This is in qualitative agreement with our experiments, since no N-containing species were detected.

Electron impact dissociation and dissociation upon impact with  $N_2$  metastable states also contribute to the conversion of  $CO_2$  into CO and O. Moreover, the CH<sub>3</sub> radicals, formed by CH<sub>4</sub> dissociation, react with O atoms, to form CH<sub>2</sub>O (formaldehyde) and CH<sub>3</sub>O radicals. The latter can subsequently be converted into CH<sub>2</sub>O as well. Furthermore, the O atoms can react with CH<sub>2</sub>O or CH<sub>4</sub> to produce OH radicals, which can further react with CH<sub>3</sub> radicals into CH<sub>3</sub>OH (methanol), albeit to a lower extent. The OH radicals also react further into H<sub>2</sub>O. Finally, the O atoms, created from CO<sub>2</sub> conversion, initiate the formation of other oxygenates, like acetaldehyde (CH<sub>3</sub>CHO). However, this reaction path is not so important, because of the limited formation of O radicals.

In order of decreasing importance, H<sub>2</sub>, CO, C<sub>2</sub>H<sub>6</sub>, H<sub>2</sub>O, as well as the hydrogen cyanide (HCN) are the main end products (with molar fractions of 0.80 %, 0.60 %, 0.20 %, 0.19 % and 0.16 %, respectively) in a 1:1:8  $CO_2/CH_4/N_2$  mixture. The fraction of other oxygenates (CH<sub>2</sub>O, CH<sub>3</sub>OH, etc.) as well as C<sub>3</sub>H<sub>8</sub> in the end products is lower than 0.1 %, hence their yields are of minor importance. Note that HCN was not detected in our experiments, although the calculations predict a higher concentration than for C<sub>3</sub>H<sub>8</sub>. This is because thermal conductivity detectors (TCD) and a flame-ionization detector (FID) were used to detect the products. These detectors are more sensitive and hence have a much lower detection limit for C<sub>3</sub>H<sub>8</sub> compared to HCN. Moreover, the yield of water (H<sub>2</sub>O) was not calculated in the experiments, since GC measurements are not suitable to deliver quantitative data about H<sub>2</sub>O.

Our earlier study showed that the presence of  $N_2$  during CO<sub>2</sub> splitting leads to the formation of  $N_2O$  and several NO<sub>x</sub> compounds, with concentrations in the range of several 100 ppm.<sup>81</sup> These concentrations are too low to be considered useful for nitrogen fixation <sup>6-7</sup> but will give rise to several environmental problems. N<sub>2</sub>O is an even more potent greenhouse gas than CO<sub>2</sub>, with a global warming potential (GWP) of 298 CO<sub>2</sub>equivalent, while NO and NO<sub>2</sub> are responsible for acid rain and the formation of ozone and a wide variety of toxic products. However, our calculations predict that with the addition of CH<sub>4</sub>, the production of NO<sub>x</sub> compounds upon reaction between N- and O-species is prohibited, because of the faster reaction between Oand H-species, as explained in section 3.2 above. Therefore, no NO<sub>x</sub> compounds are plotted in figure 17. This result is very important, as it indicates that DRM in a real gas effluent, containing significant amounts of  $N_2$ , would not cause problems of  $NO_x$  formation, that are present in  $CO_2$  splitting upon addition of  $N_2$ .



**Figure 18.** Schematic overview of the dominant reaction pathways for the conversion of  $CH_4$ ,  $CO_2$ ,  $O_2$  and  $N_2$  in a 10:10:78:2  $CO_2/CH_4/N_2/O_2$  mixture, for a fixed total flow rate of 200 ml/min and plasma power of 10 W, corresponding to an SEI of 0.76 eV/molecule. The thickness of the arrow lines is linearly proportional to the rate of the net reactions. The most important molecules are indicated with a solid line frame, the molecules formed with lower densities are written in a frame with dashed lines, while the radicals are not written in a frame.

From the analysis of the dominant loss and formation processes in sections 3.3.1-3.3.6 above, it became clear that the addition of water does not change the plasma chemistry to a large extent, because of its limited influence on the CH<sub>4</sub> and CO<sub>2</sub> conversion (see also figure 10 above). Hence, the dominant reaction pathways in a CO<sub>2</sub>/CH<sub>4</sub>/N<sub>2</sub>/H<sub>2</sub>O mixture are also well represented by figure 17.

For the  $CO_2/CH_4/N_2/O_2$  mixture, on the other hand, the situation is different, because  $O_2$  addition affects the dominant loss and formation reactions, as was clear from sections 3.3.1-3.3.6 above. Therefore, we plot in figure 18 the dominant reaction pathways for the conversion of CH<sub>4</sub>, CO<sub>2</sub>, O<sub>2</sub> and N<sub>2</sub> in a 10:10:78:2  $CO_2/CH_4/N_2/O_2$  mixture. Again, electron impact dissociation of CH<sub>4</sub> and dissociation upon impact with N<sub>2</sub> metastable singlet and triplet states results in the formation of CH<sub>3</sub> radicals. The latter can again recombine into hydrocarbons, such as ethane (C<sub>2</sub>H<sub>6</sub>), but the production of higher hydrocarbons through CH<sub>3</sub> recombination is reduced due to the increased recombination rate between CH<sub>3</sub> and O<sub>2</sub> or OH radicals, which are more abundant in case of O<sub>2</sub> addition, yielding methanol (CH<sub>3</sub>OH) formation. Moreover, the recombination of CH<sub>3</sub> radicals and  $O_2$  molecules into  $CH_3O_2$  radicals, which further form  $CH_3O$ , also becomes important. The  $CH_3O$  radicals also yield the formation of formaldehyde ( $CH_2O$ ) and methanol ( $CH_3OH$ ). However, methanol ( $CH_3OH$ ) can quickly react back into  $CH_3O$  radicals through the reverse reactions with O, H or OH radicals at a somewhat larger rate, so our model reveals a net conversion from methanol ( $CH_3OH$ ) to formaldehyde ( $CH_2O$ ).

In addition, methanol (CH<sub>3</sub>OH) can react further into formaldehyde (CH<sub>2</sub>O) through the CH<sub>2</sub>OH radicals, and formaldehyde (CH<sub>2</sub>O) can further be converted into CO, either directly upon reaction with O atoms or indirectly through the CHO radicals. Furthermore, the reaction of formaldehyde (CH<sub>2</sub>O) with O atoms also produces OH radicals. The O<sub>2</sub> molecules are converted into HO<sub>2</sub> radicals, O atoms and CO, as well as formaldehyde (CH<sub>2</sub>O). It is worth to mention that most of the O<sub>2</sub> conversion proceeds through collisions between neutral species. For instance, O<sub>2</sub> dissociation upon impact with N<sub>2</sub> metastable states contributes for about 15%, showing the important role of N<sub>2</sub>, while electron impact dissociation contributes for only 3-4%.

CO can be further oxidized into  $CO_2$  upon reaction with OH radicals. Furthermore, also the  $CH_2$  radicals can be oxidized into  $CO_2$ . These reactions are obviously undesired. The O atoms are also converted into  $CH_3O$  and OH radicals, which can again form water. The production of  $H_2CN$  upon impact between N and  $CH_3$  radicals is prohibited, due to competition with other reactions that consume  $CH_3$  radicals upon addition of  $O_2$ . As a result, the concentration of HCN in the mixture is greatly reduced.

The most important products in a 10:10:78:2  $CO_2/CH_4/N_2/O_2$  mixture, as predicted by our model, are (in order of decreasing importance) H<sub>2</sub>O, CO, H<sub>2</sub>, ethane (C<sub>2</sub>H<sub>6</sub>), methanol (CH<sub>3</sub>OH) and hydrogen cyanide (HCN), with molar fractions of 1.60 %, 1.30 %, 0.78 %, 0.13 %, 0.10 %, and 0.094 %, respectively. Note that methanol (CH<sub>3</sub>OH) was not detected in our experiments, because its concentration approaches the detection limit. In contrast, C<sub>3</sub>H<sub>8</sub> species were detected in spite of their lower concentration because of a much lower detection limit.

The comparison of figures 17 and 18 clearly shows that  $O_2$  addition has a dramatic effect on the plasma chemistry of  $CO_2$  and  $CH_4$  conversion, as was also clear from section 3.2 and sections 3.3.1-3.3.6 above (cf. figure 9 and figures S2, S5, S8, S11, S14 and S17 of the SI). A similar behavior was reported by De Bie et al., when comparing the plasma chemistry of DRM ( $CH_4/CO_2$ ) and POX ( $CH_4/O_2$ ). Indeed, both investigations indicate that mixtures with  $CO_2$  favor the formation of  $H_2$ , while the production of  $H_2O$  is greatly promoted upon addition of  $O_2$ . CO is formed at high density in both gas mixtures. Note that adding  $O_2$  can effectively promote the conversion of  $CH_4$  (see figure 9). However, also a significant amount of undesired  $CO_2$  is formed and thus the net conversion of  $CO_2$  is greatly reduced. Our pathway analysis shows how plasma chemistry modeling can help to obtain better insight, and this is very valuable to optimize the process. For example, the different pathways revealed by our model can help to determine the most suitable feed gas ratio to obtain the highest yield and/or selectivity of desired products.

#### 4. CONCLUSIONS AND OUTLOOK

Chemical kinetics modeling has proven to be very useful to study the plasma-based conversion of  $CO_2$  and  $CH_4$ . In recent years, plasma chemistry models have been developed in a stepwise manner. First models consisted of single component molecular gases, i.e. to study  $CO_2$  splitting and  $CH_4$  reforming. In a next step,

#### The Journal of Physical Chemistry

multi-component mixtures were studied, i.e. DRM, POX, artificial photosynthesis, and  $CO_2$  hydrogenation. Subsequently, the effect of  $N_2$  as impurity and admixture on the  $CO_2$  splitting and  $CH_4$  reforming process was investigated, to better approach real effluent gases.

Combining the knowledge gathered in this field so far, we presented here a new comprehensive plasma chemistry set, that can be used for zero-dimensional modeling of the chemical kinetics in low temperature plasmas, for all possible combinations of  $CO_2$ ,  $CH_4$ ,  $N_2$ ,  $O_2$  and  $H_2O$ , for a wide variety of applications. It will be useful, for instance, for  $CO_2$  conversion studies in the presence of both  $CH_4$  and  $N_2$ , as well as for unravelling the possibilities of plasma-based multi-reforming processes. Furthermore, also in other fields, such as (plasma-assisted) combustion and even more exotic applications, like planetary atmosphere and spacecraft re-entry modeling, this chemistry set could also be used as a foundation to build a comprehensive computational data set.

This comprehensive model was first validated by comparing the calculated  $CO_2$  (and  $CH_4$ ) conversion for pure  $CO_2$ , as well as  $CO_2/CH_4$ ,  $CO_2/N_2$ ,  $CH_4/N_2$  and  $CO_2/H_2O$  gas mixtures, with experimental data from our earlier work. Subsequently, a more extensive validation was performed by a combined calculation and experimental study, investigating the conversion of  $CH_4$  and  $CO_2$ , as well as the selectivity of the major products, in a  $CO_2/CH_4/N_2$  mixture, for varying  $CO_2/CH_4$  ratios and  $N_2$  contents, as well as upon  $O_2$  and  $H_2O$  addition. Good agreement was reached with the experimental data, indicating that the chemical kinetics model sufficiently captures the underlying plasma chemistry for these processes.

The presence of N<sub>2</sub> in a CO<sub>2</sub>/CH<sub>4</sub> gas mixture clearly enhances the absolute CO<sub>2</sub> and CH<sub>4</sub> conversion, due to dissociation of CO<sub>2</sub> and CH<sub>4</sub> upon collision with nitrogen metastable molecules (mainly N<sub>2</sub>(a' $\Sigma_u^-$ ) and N<sub>2</sub>(a' $\Sigma_u^-$ )), and it also yields a slight increase in the syngas (H<sub>2</sub>/CO) ratio. This is because the N<sub>2</sub> metastable molecules contribute more to the dissociation of CH<sub>4</sub>, yielding H<sub>2</sub>, due to the higher dissociation rate than that of CO<sub>2</sub>. Moreover, at a fixed CH<sub>4</sub> content of 10 %, increasing the CO<sub>2</sub>/CH<sub>4</sub> mixing ratio from 0.5 to 4, by modifying the N<sub>2</sub> content, yields a drop in the H<sub>2</sub>/CO ratio from 2.45 to 0.42. These results show that we can exert great control over the H<sub>2</sub>/CO ratio by changing the mixing ratio.

Although the addition of  $O_2$  is also beneficial for the  $CH_4$  conversion, due to a shift towards POX over DRM, it is accompanied by a severe drop in  $CO_2$  conversion and syngas ratio. Furthermore, a large fraction of the converted  $CH_4$  is transformed into  $H_2O$  rather than value-added products.

The addition of  $H_2O$  had virtually no effect on the  $CH_4$  and  $CO_2$  conversion. This is interesting, because in a pure  $CO_2/H_2O$  mixture,  $H_2O$  addition leads to a drop in  $CO_2$  conversion. <sup>73</sup> The reason is that the H atoms, originating from  $CH_4$  dissociation, react with the OH radicals, so that the latter do not recombine with CO into  $CO_2$ , which is the limiting process in the  $CO_2/H_2O$  mixture. <sup>73</sup> Additionally, the syngas ratio increases due to the effective conversion of  $H_2O$  into  $H_2$ .

Although this new chemical kinetics model already yields good agreement with experimental data for various gas mixtures and a wide range of mixing ratios, we should remain cautious when using its results—this is true for any model. The chemistry set contains 1729 reactions, each with its corresponding cross section or rate coefficient, which are subject to certain uncertainties. <sup>94</sup> The latter will of course be reflected in the results.

A crucial next step in the field of plasma chemistry modeling should consist of performing a detailed uncertainty analysis and sensitivity studies. By doing so, the impact of these uncertainties on the model predictions can be revealed, and the accuracy of the model can be determined. Such an analysis was presented already for less complicated mixtures, i.e. by Turner for a He/O<sub>2</sub> mixture,  $^{95-97}$  and in our group for a CO<sub>2</sub> plasma. <sup>38</sup> Although this will be a huge amount of work, we will continue along these lines, since it is indispensable to fully explore the predictive character of such a model.

Additionally, the model presented here mainly applies to a DBD plasma reactor, which has been mostly used for gas conversion studies up to now. However, other types of plasmas are also gaining increasing interest, like microwave plasmas and gliding arc discharges.<sup>11</sup> They operate at somewhat different conditions, such as lower reduced electric field (i.e., ratio of electric field over gas density) around 50 - 100 Td. At these conditions, the electron temperature is in the order of 1 eV, which is most suitable for vibrational excitation. The low vibrational levels will gradually populate higher vibrational levels by vibration-vibration collisions (so-called VV relaxation), and the highest vibrational levels will easily dissociate. Hence, this process of vibrational ladder climbing leading to dissociation is the most energy-efficient process for CO<sub>2</sub> dissociation. This explains why CO<sub>2</sub> dissociation is quite energy efficient in microwave and gliding arc discharges.<sup>4,11</sup> These processes are not considered in detail in the model presented here, as they are of minor importance in a DBD. However, a detailed model for the CO<sub>2</sub> vibrational kinetics has already been developed within the group PLASMANT, <sup>34-35</sup> as well as models for  $CO_2/N_2$  and  $N_2/O_2$  mixtures, accounting in detail for the vibrational kinetics of  $CO_2$ ,  $N_2$  and  $O_2$ .<sup>6,82</sup> In the future, it would be useful to extend this newly developed model for the  $CO_2/CH_4/N_2/O_2/H_2O_2$ mixture with the vibrational kinetics of the various molecules, so that this model becomes applicable to other plasma types as well. This is not only true for the  $CO_2$  vibrational levels, but the  $N_2$  vibrational levels can also be important for CO<sub>2</sub> (and maybe CH<sub>4</sub>) dissociation.<sup>82</sup> Furthermore, when the CO<sub>2</sub> conversion is significant, the CO vibrational kinetics should be considered as well, in relation with the formation of C and O atoms.<sup>98</sup> Again, adding the vibrational levels of all these molecules will require major efforts, in view of the possible coupling between all these vibrational levels, and keeping in mind uncertainties in all rate coefficients, 95-97 and the approximations that need to be made. <sup>15-16</sup>

This combined computational and experimental study reveals that the major products formed by mixtures of  $CO_2$ ,  $CH_4$ ,  $N_2$ ,  $O_2$  and  $H_2O$  are syngas and some higher hydrocarbons (mainly  $C_2H_6$  and  $C_3H_8$ ), as well as  $H_2O$ , while the concentrations of oxygenates like methanol, formic acid, formaldehyde, as well as hydrogen cyanide, are almost negligible. Hence, to increase the product selectivity of future plasma-based reforming processes, preferably to these oxygenates, combinations with a catalyst or membranes will be necessary. This brings us to another future necessity in the field of plasma chemistry modeling, i.e., the need to extend these models with surface reactions, as recently done for  $NH_3$  synthesis by Hong et al. <sup>99</sup> This step would make it possible for 0D plasma chemistry models to account for plasma catalysis, and thus to make it possible to predict the requirements of the underlying plasmachemical pathways to selectively produce the desired value-added compounds. This stresses the power that lies within this type of modeling studies, i.e. to unravel the underlying chemical pathways to obtain a better understanding of the chemistry taking place, which in turn allows to predict whether new conditions could be more promising, and help to point experiments in the right direction.

## ASSOCIATED CONTENT

\*S Supporting Information

The Supporting Information is available free of charge on the ACS Publications website at DOI: xx.xxx/acs.jpcc.xxxxxx. An overview of the reactions included in the model (PDF)

## ACKNOWLEDGMENTS

The authors acknowledge financial support from the European Marie Skłodowska-Curie Individual Fellowship "GlidArc" within Horizon2020 (Grant No. 657304), the Fund for Scientific Research Flanders (FWO) (grant nos G.0217.14N, G.0254.14N and G.0383.16N), Competitive Research Funding from King Abdullah University of Science and Technology (KAUST), the IAP/7 (Inter-university Attraction Pole) program 'PSI-Physical Chemistry of Plasma-Surface Interactions', financially supported by the Belgian Federal Office for Science Policy (BELSPO), as well as the Fund for Scientific Research Flanders (FWO). This work was carried out in part using the Turing HPC infrastructure at the CalcUA core facility of the Universiteit Antwerpen, a division of the Flemish Supercomputer Center VSC, funded by the Hercules Foundation, the Flemish Government (department EWI) and the University of Antwerp.

## REFERENCE

(1) Adamovich, I.; Baalrud, S. D.; Bogaerts, A.; Bruggeman, P. J.; Cappelli, M.; Colombo, V.; Czarnetzki, U.; Ebert, U.; Eden, J. G.; Favia, P.; et al. The 2017 Plasma Roadmap: Low Temperature Plasma Science and Technology. *J. Phys. D. Appl. Phys.* **2017**, *50*, 323001.

(2) Lee, C. G. N.; Kanarik, K. J.; Gottscho, R. A. The Grand Challenges of Plasma Etching: A Manufacturing Perspective. *J. Phys. D. Appl. Phys.* **2014**, *47*, 273001.

(3) Bogaerts, A.; Neyts, E.; Gijbels, R.; van der Mullen, J. Gas Discharge Plasmas and Their Applications, *Spectrochim. Acta, Part B* **2002**, *57*, 609–658.

(4) Fridman, A. Plasma Chemistry; Cambridge University Press: New York, 2008.

(5) Chang, J. S. Recent Development of Plasma Pollution Control Technology: A Critical Review. *Sci. & Tech. of Adv. Materials* **2001**, *2*, 571-576.

(6) Wang, W. Z.; Patil, B.; Heijkers, S.; Hessel, V.; Bogaerts, A. Nitrogen Fixation by Gliding Arc Plasma: Better Insight by Chemical Kinetics Modelling. ChemSusChem **2017**, *10*, 2145–2157

(7) Patil, B. S.; Cherkasov, N.; Lang, J.; Ibhadon, A. O.; Hessel, V., Wang, Q. Low Temperature Plasma-Catalytic NOx Synthesis in a Packed DBD Reactor: Effect of Support Materials and Supported Active Metal Oxides. *Appl. Catal. B- Environ.* **2016**, *194*, 123-133.

(8) Chen, H. L.; Lee, H. M.; Chen, S. H.; Chao, Y.; Chang, M. B. Review of Plasma Catalysis on Hydrocarbon Reforming for Hydrogen Production—Interaction, Integration, and Prospects. *Appl. Catal. B: Environ.* 2008, 85, 1-9.

(9) Snoeckx, R; Rabinovich, A; Dobrynin, D; Bogaerts, A; Fridman, A. Plasma Based Liquefaction of Methane: the Road from Hydrogen Production to Direct Methane Liquefaction. *Plasma Processes and Polymers* 2017, *14*, 1600115.

(10) Tu, X.; Whitehead, J. C. Plasma-Catalytic Dry Reforming of Methane in an Atmospheric Dielectric Barrier Discharge: Understanding the Synergistic Effect at Low Temperature. *Appl. Catal. B: Environ.* **2002**, *125*, 439–448.

(11) Snoeckx, R.; Bogaerts, A. Plasma Technology – a Novel Solution for CO<sub>2</sub> Conversion? *Chem. Soc. Rev.* **2017**, *46*, 5805–5863.

(12) Neyts, E. C.; Bogaerts, A. Understanding Plasma Catalysis Through Modelling and Simulation—A Review.*J. Phys. D: Appl. Phys.* 2014, *47*, 224010.

(13) Neyts, E. C.; Ostrikov, K.; Sunkara, M. K.; Bogaerts, A. Plasma Catalysis: Synergistic Effects at the Nanoscale. *Chem. Rev.* **2015**, *115*, 13408-13446.

(14) Whitehead J. C., Plasma-catalysis: The Known Knowns, the Known Unknowns and the Unknown Unknowns. J. Phys. D: Appl. Phys. 2016, 49, 243001.

(15) Bogaerts, A.; De Bie, C.; Snoeckx, R.; Kozák, T. Plasma Based CO<sub>2</sub> and CH<sub>4</sub> Conversion: A Modeling Perspective. *Plasma Process. Polym.* **2017**, *14*, 1600070.

(16) Bogaerts, A.; Berthelot, A.; Heijkers, S.; Kolev, S.; Snoeckx, R.; Sun, S. R.; Trenchev, G.; Van Laer, K.;
Wang, W. CO<sub>2</sub> Conversion by Plasma Technology: Insights from Modeling the Plasma Chemistry and Plasma Reactor Design. *Plasma Sources Sci. Technol.* 2017, *26*, 63001.

(17) Zou, J. J.; Zhang, Y. P.; Liu, C. J.; Li, Y.; Eliasson, B. Starch-enhanced Synthesis of Oxygenates from Methane and Carbon Dioxide Using Dielectric-Barrier Discharges. *Plasma Chem. Plasma Process.* 2003, *23*, 69–82.

(18) Krauss, M.; Eliasson, B.; Kogelschatz, U.; Wokaun, A. CO<sub>2</sub> Reforming of Methane by the Combination of Dielectric-Barrier Discharges and Catalysis. *Phys. Chem. Chem. Phys.* **2001**, *3*, 294–300.

(19) Mei, D. H.; Zhu, X. B.; He, Y. L.; Yan, J. D.; Tu, X. Plasma-assisted Conversion of CO<sub>2</sub> in A Dielectric Barrier Discharge Reactor: Understanding the Effect of Packing Materials. *Plasma Sources Sci. Technol.* 2015, 24, 015011.

(20) Tu, X.; Gallon, H. J.; Twigg, M. V.; Gorry, P. A.; Whitehead, J. C. Dry Reforming of Methane Over a NI/AL<sub>2</sub>O<sub>3</sub> Catalyst in a Coaxial Dielectric Barrier Discharge Reactor. *J. Phys. D: Appl. Phys.* **2011**, *44*, 274007.

(21) IPCC. Summary for Policymakers; 2014.

 (22) McDonough, W.; Braungart, M.; Anastas, P. T.; Zimmerman, J. B. Peer Reviewed: Applying the Principles of Green Engineering to Cradle-to-Cradle Design. *Environ. Sci. Technol.* **2003**, *37*, 434A–441A.

(23) Jiang, Z.; Xiao, T.; Kuznetsov, V. L.; Edwards, P. P. Turning Carbon Dioxide into Fuel. *Philos. Trans. R. Soc. A Math. Phys. Eng. Sci.* **2010**, *368*, 3343–3364.

(24) Mikkelsen, M.; Jørgensen, M.; Krebs, F. C. The Teraton Challenge. A Review of Fixation and Transformation of Carbon Dioxide. *Energy Environ. Sci.* **2010**, *3*, 43–81.

(25) Ju, Y.; Sun, W. T. Plasma Assisted Combustion: Dynamics and Chemistry. *Prog. Energy Combust. Sci.* **2015**, *48*, 21–83.

Page 37 of 44

1	
2 3 4 5	(26) Starikovskaia, S. M. Plasma-assisted Ignition and Combustion: Nanosecond Discharges and Development of Kinetic Mechanisms. <i>J. Phys. D: Appl. Phys.</i> <b>2004</b> , <i>47</i> , 353001.
6 7 8	(27) Gokcen, T. N <sub>2</sub> -CH <sub>4</sub> -Ar Chemical Kinetic Model for Simulations of Atmospheric Entry to Titan. <i>J. Thermophys Heat Transfer</i> <b>2017</b> , <i>21</i> , 9-18
9 10 11 12	(28) Bultel, A.; Annaloro J. Elaboration of Collisional–Radiative Models for Flows Related to Planetary Entries into the Earth and Mars Atmospheres. <i>Plasma Sources Sci. Technol.</i> <b>2013</b> , <i>22</i> , 025008.
12 13 14 15	(29) Aerts, R.; Somers, W.; Bogaerts, A. Carbon Dioxide Splitting in a Dielectric Barrier Discharge Plasma: A Combined Experimental and Computational Study. <i>ChemSusChem</i> <b>2015</b> , <i>8</i> , 702–716.
16 17 18	(30) Wang, W.; Berthelot, A.; Kolev, S.; Tu, X.; Bogaerts, A. CO <sub>2</sub> Conversion in a Gliding Arc Plasma: 1D Cylindrical Discharge Model. <i>Plasma Sources Sci. Technol.</i> <b>2016</b> , <i>25</i> , 65012.
19 20 21	(31) Wang, W.; Mei, D.; Tu, X.; Bogaerts, A. Gliding Arc Plasma for CO <sub>2</sub> Conversion: Better Insights by a Combined Experimental and Modelling Approach. <i>Chem. Eng. J.</i> <b>2017</b> , <i>330</i> , 11-25.
22 23 24	(32) Sun, S. R.; Wang, H. X.; Mei, D. H.; Tu, X.; Bogaerts, A. CO <sub>2</sub> Conversion in a Gliding Arc Plasma: Performance Improvement Based on Chemical Reaction Modeling. <i>J. CO</i> <sub>2</sub> <i>Util.</i> <b>2017</b> , <i>17</i> , 220–234.
25 26 27	(33) Aerts, R.; Martens, T.; Bogaerts, A. Influence of Vibrational States on CO <sub>2</sub> Splitting by Dielectric Barrier Discharges. <i>J. Phys. Chem. C</i> <b>2012</b> , <i>116</i> , 23257–23273.
28 29 30 31	<ul> <li>(34) Kozák, T.; Bogaerts, A. Evaluation of the Energy Efficiency of CO<sub>2</sub> Conversion in Microwave Discharges Using a Reaction Kinetics Model. <i>Plasma Sources Sci. Technol.</i> 2015, 24, 15024.</li> </ul>
32 33 34	(35) Kozák, T.; Bogaerts, A. Splitting of CO <sub>2</sub> by Vibrational Excitation in Non-Equilibrium Plasmas: A Reaction Kinetics Model. <i>Plasma Sources Sci. Technol.</i> <b>2014</b> , <i>23</i> , 45004.
35 36 37	(36) Berthelot, A.; Bogaerts, A. Modeling of Plasma-Based CO <sub>2</sub> Conversion: Lumping of the Vibrational Levels. <i>Plasma Sources Sci. Technol.</i> <b>2016</b> , <i>25</i> , 45022.
38 39 40	(37) Berthelot, A.; Bogaerts, A. Modeling of CO <sub>2</sub> Splitting in a Microwave Plasma: How to Improve the Conversion and Energy Efficiency. <i>J. Phys. Chem. C</i> <b>2017</b> , <i>121</i> , 8236–8251.
41 42 43 44	(38) Berthelot, A.; Bogaerts, A. Modeling of CO <sub>2</sub> Plasma: Effect of Uncertainties in the Plasma Chemistry. <i>Plasma Sources Sci. Technol.</i> <b>2017</b> , <i>26</i> , 115002.
45 46 47 48	(39) Koelman, P.; Heijkers, S.; Tadayon Mousavi, S.; Graef, W.; Mihailova, D.; Kozak, T.; Bogaerts, A.; van Dijk, J. A Comprehensive Chemical Model for the Splitting of CO <sub>2</sub> in Non-Equilibrium Plasmas. <i>Plasma Process. Polym.</i> <b>2017</b> , <i>14</i> , 1–20.
50 51 52	(40) Ponduri, S.; Becker, M. M.; Welzel, S.; Van De Sanden, M. C. M.; Loffhagen, D.; Engeln, R. Fluid Modelling of CO <sub>2</sub> Dissociation in a Dielectric Barrier Discharge. <i>J. Appl. Phys.</i> <b>2016</b> , <i>119</i> .
53 54 55	(41) Pietanza, L. D.; Colonna, G.; D'Ammando, G.; Laricchiuta, A.; Capitelli, M. Non Equilibrium Vibrational Assisted Dissociation and Ionization Mechanisms in Cold CO <sub>2</sub> Plasmas. <i>Chem. Phys.</i> <b>2016</b> , <i>468</i> , 44–52.
56 57 58 59 60	(42) Pietanza, L. D.; Colonna, G.; D'Ammando, G.; Laricchiuta, A.; Capitelli, M. Electron Energy Distribution Functions and Fractional Power Transfer In "cold" and Excited CO <sub>2</sub> Discharge and Post Discharge Conditions. <i>Phys. Plasmas</i> <b>2016</b> , <i>23</i> .

(43) Pietanza, L. D.; Colonna, G.; Laporta, V.; Celiberto, R.; D'Ammando, G.; Laricchiuta, A.; Capitelli, M. Influence of Electron Molecule Resonant Vibrational Collisions over the Symmetric Mode and Direct Excitation-Dissociation Cross Sections of CO<sub>2</sub> on the Electron Energy Distribution Function and Dissociation Mechanisms in Cold Pure CO<sub>2</sub> Plasmas. *J. Phys. Chem. A* 2016, *120*, 2614–2628.

 (44) Pietanza, L. D.; Colonna, G.; D'Ammando, G.; Capitelli, M. Time-Dependent Coupling of Electron Energy Distribution Function, Vibrational Kinetics of the Asymmetric Mode of CO<sub>2</sub> and Dissociation, Ionization and Electronic Excitation Kinetics under Discharge and Post-Discharge Conditions. *Plasma Phys. Control. Fusion* **2017**, *59*, 14035.

(45) Pietanza, L. D.; Colonna, G.; D'Ammando, G.; Laricchiuta, a; Capitelli, M. Vibrational Excitation and Dissociation Mechanisms of CO<sub>2</sub> under Non-Equilibrium Discharge and Post-Discharge Conditions. *Plasma Sources Sci. Technol.* **2015**, *24*, 42002.

(46) Capitelli, M.; Colonna, G.; D'Ammando, G.; Hassouni, K.; Laricchiuta, A.; Pietanza, L. D. Coupling of Plasma Chemistry, Vibrational Kinetics, Collisional-Radiative Models and Electron Energy Distribution Function Under Non-Equilibrium Conditions. *Plasma Process. Polym.* **2017**, *14*, 1600109.

(47) Moss, M. S.; Yanallah, K.; Allen, R. W. K.; Pontiga, F. An Investigation of CO<sub>2</sub> Splitting Using Nanosecond Pulsed Corona Discharge: Effect of Argon Addition on CO<sub>2</sub> Conversion and Energy Efficiency. *Plasma Sources Sci. Technol.* **2017**, *26*, 35009.

(48) Cheng, J.-L.; Wang, H.-X.; Sun, S.-R. Analysis of Dissociation Mechanism of CO<sub>2</sub> in a Micro-Hollow Cathode Discharge. *Chinese Phys. Lett.* **2016**, *33*, 108201.

(49) de la Fuente, J. F.; Moreno, S. H.; Stankiewicz, A. I.; Stefanidis, G. D. A New Methodology for the Reduction of Vibrational Kinetics in Non-Equilibrium Microwave Plasma: Application to CO<sub>2</sub> Dissociation. *React. Chem. Eng.* **2016**, *1*, 540–554.

(50) Indarto, A.; Choi, J.; Lee, H.; Song, H. K. Kinetic Modeling of Plasma Methane Conversion Using Gliding Arc. *J. Nat. Gas Chem.* **2005**, *14*, 13–21.

(51) Indarto, A.; Coowanitwong, N.; Choi, J. W.; Lee, H.; Song, H. K. Kinetic Modeling of Plasma Methane Conversion in a Dielectric Barrier Discharge. *Fuel Process. Technol.* **2008**, *89*, 214–219.

(52) De Bie, C.; Verheyde, B.; Martens, T.; van Dijk, J.; Paulussen, S.; Bogaerts, A. Fluid Modeling of the Conversion of Methane into Higher Hydrocarbons in an Atmospheric Pressure Dielectric Barrier Discharge. *Plasma Process. Polym.* **2011**, *8*, 1033–1058.

(53) Yang, Y. Direct Non-Oxidative Methane Conversion by Non-Thermal Plasma: Modeling Study. *Plasma Chem. Plasma Process.* **2003**, *23*, 327–346.

(54) Luche, J.; Aubry, O.; Khacef, A.; Cormier, J.-M. Syngas Production from Methane Oxidation Using a Non-Thermal Plasma: Experiments and Kinetic Modeling. *Chem. Eng. J.* **2009**, *149*, 35–41.

(55) Zhou, L. M.; Xue, B.; Kogelschatz, U.; Eliasson, B. Nonequilibrium Plasma Reforming of Greenhouse Gases to Synthesis Gas. *Energy & Fuels* **1998**, *12*, 1191–1199.

(56) Machrafi, H.; Cavadias, S.; Amouroux, J. Valorization by Means of Dielectric Barrier Discharge. *J. Phys. Conf. Ser.* **2011**, *275*, 12016.

(57) Goujard, V.; Tatibouët, J. M.; Batiot-Dupeyrat, C. Carbon Dioxide Reforming of Methane Using a Dielectric Barrier Discharge Reactor: Effect of Helium Dilution and Kinetic Model. *Plasma Chem. Plasma Process.* **2011**, *31*, 315–325.

(58) Wang, J. G.; Liu, C. J.; Eliassion, B. Density Functional Theory Study of Synthesis of Oxygenates and Higher Hydrocarbons from Methane and Carbon Dioxide Using Cold Plasmas. *Energy & Fuels* **2004**, *18*, 148–153.

(59) Istadi, I.; Amin, N. A. S. Modelling and Optimization of Catalytic-Dielectric Barrier Discharge Plasma Reactor for Methane and Carbon Dioxide Conversion Using Hybrid Artificial Neural Network-Genetic Algorithm Technique. *Chem. Eng. Sci.* **2007**, *62*, 6568–6581.

(60) Kraus, M.; Egli, W.; Haffner, K.; Eliasson, B.; Kogelschatz, U.; Wokaun, A. Investigation of Mechanistic Aspects of the Catalytic CO<sub>2</sub> Reforming of Methane in a Dielectric-Barrier Discharge Using Optical Emission Spectroscopy and Kinetic Modeling. *Phys. Chem. Chem. Phys.* 2002, *4*, 668–675.

(61) Liu, C.-J.; Li, Y.; Zhang, Y.-P.; Wang, Y.; Zou, J.; Eliasson, B.; Xue, B. Production of Acetic Acid Directly from Methane and Carbon Dioxide Using Dielectric-Barrier Discharges. *Chem. Lett.* **2001**, *30*, 1304–1305.

(62) Janeco, A.; Pinha, N. R.; Guerra, V. Electron Kinetics in He / CH<sub>4</sub> / CO<sub>2</sub> Mixtures Used for Methane Conversion. *J. Phys. Chem. C* **2015**, *119*, 109.

(63) Snoeckx, R.; Aerts, R.; Tu, X.; Bogaerts, A. Plasma-Based Dry Reforming: A Computational Study Ranging from the Nanoseconds to Seconds Time Scale. *J. Phys. Chem. C* **2013**, *117*, 4957–4970.

(64) Snoeckx, R.; Zeng, Y. X.; Tu, X.; Bogaerts, A. Plasma-Based Dry Reforming: Improving the Conversion and Energy Efficiency in a Dielectric Barrier Discharge. *RSC Adv.* **2015**, *5*, 29799–29808.

(65) De Bie, C.; Martens, T.; van Dijk, J.; Paulussen, S.; Verheyde, B.; Corthals, S.; Bogaerts, A. Dielectric Barrier Discharges Used for the Conversion of Greenhouse Gases: Modeling the Plasma Chemistry by Fluid Simulations. *Plasma Sources Sci. Technol.* **2011**, *20*, 24008.

(66) De Bie, C.; Van Dijk, J.; Bogaerts, A. The Dominant Pathways for the Conversion of Methane into Oxygenates and Syngas in an Atmospheric Pressure Dielectric Barrier Discharge. *J. Phys. Chem. C* 2015, *119*, 22331–22350.

(67) Zhou, L. M.; Xue, B.; Kogelschatz, U.; Eliasson, B. Partial Oxidation of Methane to Methanol with Oxygen or Air in a Nonequilibrium Discharge Plasma. *Plasma Chem. Plasma Process.* **1998**, *18*, 375–393.

(68) Nair, S. A.; Nozaki, T.; Okazaki, K. Methane Oxidative Conversion Pathways in a Dielectric Barrier Discharge Reactor-Investigation of Gas Phase Mechanism. *Chem. Eng. J.* **2007**, *132*, 85–95.

(69) Goujard, V.; Nozaki, T.; Yuzawa, S.; Ağiral, A.; Okazaki, K. Plasma-Assisted Partial Oxidation of Methane at Low Temperatures: Numerical Analysis of Gas-Phase Chemical Mechanism. *J. Phys. D. Appl. Phys.* 2011, 44, 274011.

(70) Nozaki, T.; Aĝiral, A.; Yuzawa, S.; Han Gardeniers, J. G. E.; Okazaki, K. A Single Step Methane Conversion Into Synthetic Fuels Using Microplasma Reactor. *Chem. Eng. J.* **2011**, *166*, 288–293.

(71) Zhou, J.; Xu, Y.; Zhou, X.; Gong, J.; Yin, Y.; Zheng, H.; Guo, H. Direct Oxidation of Methane to Hydrogen Peroxide and Organic Oxygenates in a Double Dielectric Plasma Reactor. *ChemSusChem* **2011**, *4*, 1095–1098.

(72) Matin, N. S.; Whitehead, J. C. A Chemical Model for the Atmospheric Pressure Plasma Reforming of Methane with Oxygen. In *28th ICPIG*; 2007; pp 983–986.

(73) Snoeckx, R.; Ozkan, A.; Reniers, F.; Bogaerts, A. The Quest for Value-Added Products from Carbon Dioxide and Water in a Dielectric Barrier Discharge: A Chemical Kinetics Study. *ChemSusChem* 2017, *10*, 409–424.

(74) De Bie, C.; Van Dijk, J.; Bogaerts, A. CO<sub>2</sub> Hydrogenation in a Dielectric Barrier Discharge Plasma Revealed. *J. Phys. Chem. C* **2016**, *120*, 25210–25224.

(75) Ding, K.; Lieberman, Reaction Pathways for Bio-Active Species in a He/H<sub>2</sub>O Atmospheric Pressure Capacitive Discharge. *J. Phys. D: Appl. Phys.* **2015**, *48*, 035401.

(76) Legrand, J. C.; Diamy, A. M.; Hrach, R.; Hrachova, V. Kinetics of Reactions in CH<sub>4</sub>/N<sub>2</sub> Afterglow Plasma. *Vacuum* **1997**, *48*, 671–675.

(77) Majumdar, A.; Behnke, J. F.; Hippler, R.; Matyash, K.; Schneider, R. Chemical Reaction Studies in CH<sub>4</sub>/Ar and CH<sub>4</sub>/N<sub>2</sub> Gas Mixtures of a Dielectric Barrier Discharge. *J. Phys. Chem. A* **2005**, *109*, 9371–9377.

(78) Pintassilgo, C. D.; Jaoul, C.; Loureiro, J.; Belmonte, T.; Czerwiec, T. Kinetic Modelling of a N<sub>2</sub> Flowing Microwave Discharge with CH <sub>4</sub> Addition in the Post-Discharge for Nitrocarburizing Treatments. *J. Phys. D. Appl. Phys.* **2007**, *40*, 3620–3632.

(79) Jauberteau, J. L.; Jauberteau, I.; Cinelli, M. J.; Aubreton, J. Reactivity of Methane in a Nitrogen Discharge Afterglow. *New J. Phys.* **2002**, *4*, 39.

(80) Savinov, S. Y.; Lee, H.; Song, H. K.; Na, B. K. The Effect of Vibrational Excitation of Molecules on Plasmachemical Reactions Involving Methane and Nitrogen. *Plasma Chem. Plasma Process.* **2003**, *23*, 159–173.

(81) Snoeckx, R.; Setareh, M.; Aerts, R.; Simon, P.; Maghari, A.; Bogaerts, A. Influence of N<sub>2</sub> Concentration in a CH<sub>4</sub>/N<sub>2</sub> Dielectric Barrier Discharge Used for CH<sub>4</sub> Conversion into H<sub>2</sub>. *Int. J. Hydrogen Energy* **2013**, *38*, 16098–16120.

(82) Heijkers, S.; Snoeckx, R.; Kozák, T.; Silva, T.; Godfroid, T.; Britun, N.; Snyders, R.; Bogaerts, A. CO<sub>2</sub>
Conversion in a Microwave Plasma Reactor in the Presence of N<sub>2</sub> : Elucidating the Role of Vibrational Levels. *J. Phys. Chem. C* 2015, *119*, 12815–12828.

(83) Snoeckx, R.; Heijkers, S.; Van Wesenbeeck, K.; Lenaerts, S.; Bogaerts, A. CO<sub>2</sub> Conversion in a Dielectric Barrier Discharge Plasma: N<sub>2</sub> in the Mix as a Helping Hand or Problematic Impurity? *Energy Environ. Sci.* 2016, *9*, 999–1011.

(84) Zhang, X.; Cha, M. S. Electron-Induced Dry Reforming of Methane in a Temperature-Controlled Dielectric Barrier Discharge Reactor. *J. Phys. D. Appl. Phys.* **2013**, *46*, 415205.

(85) Zhang, X.; Cha, M. S. Partial Oxidation of Methane in a Temperature-Controlled Dielectric Barrier Discharge Reactor. *Proc. Combust. Inst.* **2015**, *35*, 3447–3454.

(86) van Dijk, J.; Kroesen, G.M.W.; and Bogaerts A., Plasma Modeling and Numerical Simulation. *J. Phys. D: Appl. Phys.* **2009**, *42*, 190301.

4
5
6
7
, 0
0
9
10
11
12
13
14
15
16
17
18
19
20
20
21
22
23
24
25
26
27
28
29
30
21
21
32
33
34
35
36
37
38
39
40
41
<u>4</u> 2
12
د <del>ب</del> ۸۸
44
45
46
47
48
49
50
51
52
53
54
55
55
50
5/
58

- 59
- 60

(87) Bogaerts, A.; Alves, L.L. Special Issue on Numerical Modeling of Low-Temperature Plasmas for Various Applications – Part I: Review and Tutorial Papers on Numerical Modeling Approaches. *Plasma Process. Polym.* 2017, *14*, 169011.

(88) Alves, L.L.; Bogaerts, A.; Guerra, V.; Turner, M. M. Foundations of Modelling of Low-Temperature Plasmas. *Plasma Sources Sci. Technol.*, 2017, in press.

(89) Van Gaens, W.; Bogaerts, A. Kinetic Modelling for an Atmospheric Pressure Argon Plasma Jet in Humid Air. *J. Phys. D. Appl. Phys.* **2013**, *46*, 275201.

(90) Zhou, L. M.; Xue, B.; Kogelschatz, U.; Eliasson, B. Nonequilibrium Plasma Reforming of Greenhouse Gases to Synthesis Gas. *Energ. Fuel.* **1998**, *12*, 1191-1199.

(91) Zhang, K.; Kogelschatz, U.; Eliasson, B. Conversion of Greenhouse Gases to Synthesis Gas and Higher Hydrocarbons. *Energ. Fuel.* **2001**, *15*, 395-402.

(92) Aerts, R.; Snoeckx, R.; Bogaerts, A. In-Situ Chemical Trapping of Oxygen in the Splitting of Carbon Dioxide by Plasma. *Plasma Process. Polym.* **2014**, *11*, 985–994.

(93) Atkins, P.W. (1993). The Elements of Physical Chemistry (3rd ed.). Oxford University Press.

(94) Bogaerts, A.; Wang, W. Z.; Berthelot A.; Guerra, V. Modeling Plasma-based CO<sub>2</sub> Conversion: Crucial Role of the Dissociation Cross Section. *Plasma Sources Sci. Technol.* **2016**, *25*, 055016.

(95) Turner, M. M. Uncertainty and Error in Complex Plasma Chemistry Models. *Plasma Sources Sci. Technol.* **2015**, *24*, 035027.

(96) Turner, M. M. Uncertainty and Sensitivity Analysis in Complex Plasma Chemistry Models. *Plasma Sources Sci. Technol.* **2016**, *25*, 015003.

(97) Turner, M. M. Computer Simulation in Low-Temperature Plasma Physics: Future Challenges. *Plasma Process. Polym.* **2017**, *14*, 1600121.

(98) Pietanza, L. D.; Colonna G. and Capitelli M. Non-equilibrium Plasma Kinetics of Reacting CO: An Improved State to State Approach. *Plasma Sources Sci. Technol.* **2017**, *26*, 125007.

(99) Hong, J.; Pancheshnyi, S.; Tam, E.; Lowke, J. J.; Prawer, S.; Murphy, A. B. Kinetic Modelling of NH<sub>3</sub> Production in N<sub>2</sub>–H<sub>2</sub> Non-Equilibrium Atmospheric-Pressure Plasma Catalysis. *J. Phys. D: Appl. Phys.* **2017**, *50*, 154005.

# **TOC GRAPHIC**



#### 

## BIOGRAPHIES

Weizong Wang was born in Shandong, China, in 1984. He received double Ph.D. degrees in electrical



engineering from Xi'an Jiaotong University, China and University of Liverpool, United Kingdome, in 2013. Since that, he worked at Qian Xuesen Laboratory of Space Technology in China up to 2015, focusing on plasma propulsion. Currently, he is working in the PLASMANT research group at the University of Antwerp in Belgium supported by the Marie Skłodowska-Curie Individual Fellowship towards a better understanding of plasma-based gases conversion into value added products. His main interests concern the fundamental physics, chemistry and applications of low temperature plasmas.

Ramses Snoeckx, born in 1988, obtained master's degrees in both environmental science and chemistry.



Combining these specializations, he successfully obtained a PhD in chemistry (2017, University of Antwerp) for his research on plasma-based conversion of greenhouse gases into value-added chemicals and fuels. Currently he's working as postdoctoral fellow at the King Abdullah University of Science and Technology (KAUST). The underlying chemical reactions taking place in plasmas are his prime focus. By relying on a combination of modelling and experimental techniques, he aims to gain the necessary insights in the plasmachemical pathways to improve existing—as well as to find new—

applications for plasma-based environmental and energy solutions.

Xuming Zhang was born in Hangzhou, China, in 1981. He received Ph.D. degree from Zhejiang University,



China, in 2011. He served in King Abdullah University of Science and Technology (KAUST), as a post-doctoral research fellow from 2011 to 2015. He has been with Zhejiang Gongshang University as an assistant professor since 2016. Dr. Zhang has authored over 30 publications in peer-reviewed journals. His current research interests include non-thermal plasma generation and plasma-induced fuel reforming and environmental remediation.

Min Suk Cha was born in Seoul, Korea, in 1970. He received Ph. D. degrees in Mechanical Engineering from



Seoul National University in 1999, specialized in Combustion Science. He worked in Korea Institute of Machinery & Materials (KIMM), where he obtained a plasma background, as a Principal Research Scientist from 2000 to 2010. Currently he is Associate Professor in King Abdullah University of Science and Technology (KAUST). His current research interests include plasma (and electrically) assisted combustion, plasma fuel reforming, and in-liquid plasma generations.

Annemie Bogaerts, born in 1971, obtained her PhD in chemistry in 1996, from the University of Antwerp in



Belgium. She became professor of physical chemistry in 2003, at this university, and is full professor since 2012. She is head of the interdisciplinary research group PLASMANT. The research activities of her group include modelling of plasma chemistry, plasma reactor design and plasma-surface interactions, as well as plasma experiments, for various applications, including environmental and medical applications (mainly cancer treatment), as well as nanotechnology and analytical chemistry. In recent years, special attention is given to  $CO_2$  conversion by plasma and plasma catalysis.