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Additional Information

Modern Diagnostics Techniques for Electrical Machines, Power Electronics, and Drives

I. INTRODUCTION

FOR THE last ten years, at least three different Special Sections dealing with diagnostics in power electrical engineering have been published in the IEEE TRANSACTIONS ON INDUSTRIAL ELECTRONICS [1]–[5]. All of them had their specificities, but the last ones, starting in 2011, were more connected to relevant events organized on the topic. In fact, these events have been clearly the only international forums fully dedicated to diagnostics techniques in power electrical engineering. For this particular issue, it has been decided to separate the different submissions into six parts:

- state of the art;
- general methods;
- induction machines (IMs);
- synchronous machines;
- electrical drives;
- power components and power converters.

The second section includes only one state-of-the-art paper, which is dedicated to actual techniques implemented in both industry and research laboratories. The third section includes three papers on diagnostic techniques not specifically aimed at a particular type of machine. The fourth section includes three papers devoted to diagnostics of rotor faults, two dedicated to stator insulation issues, and four papers dealing with mechanical faults diagnosis in IMs. The fifth section includes papers focusing on different types of synchronous machines. The first two papers deal with wound-rotor synchronous machines, the following three papers are dedicated to permanent-magnet radial flux machines, and the last one deals with permanent-magnet axial flux machines. Regarding the types of faults analyzed, there are three papers devoted to the diagnosis of interturn short circuits in the stator windings, i.e., one dedicated to the detection and location of field-winding-to-ground faults and a paper devoted to the diagnosis of static eccentricities. In the sixth section, two papers investigate issues related to faults in drive sensors, and one is devoted to fault detections in the coupling inductors. The last section includes two papers devoted to diagnosis of faults and losses analysis in switching components of power converters.

II. STATE OF THE ART

In [6], the authors have screened the most recent papers published on the topic to draw the real “state of the art” on condition monitoring and fault detection of rotating electrical

machines, drives, and power electronics. As expected, since it is the most investigated electrical machine from the very beginning, a large part of the development has been dedicated to IMs. It is well known that most of the methods developed for IMs can be simply used directly or adapted for other types of rotating electrical machines or even for linear actuators or generators.

A large part of this paper is dedicated to IM fault detection since it has been the historical field of investigation for the last 30 years or so. In this way, rotor faults have been under focus mainly for squirrel-cage IMs with convenient signal processing techniques to tackle the fact that many faults cannot be detected easily when the machine load is light. The second largest part dealing with the IM fault detection is related to stator winding, including the insulation degradation and further early stage short circuits. It has been shown that the insulation degradation detection is the best way to prevent short circuits, but it is the most difficult to be implemented online. Moreover, early stage short circuits are easier to detect particularly by the use of a stray flux sensor, which is simple, cheap, and noninvasive for large-power IMs. Other methods to detect early stage short circuits are based on the impedance asymmetry on the stator side. In this last case, the sensors are based on both stator voltages and stator currents measurements. Then, the decision process for early stage short-circuit detection can be based on advanced artificial intelligence techniques, which are well known in this specific area. Finally, in the case of IMs, methods for mechanical failures detection have been investigated. Faults such as eccentricities, bearings, and gearboxes have been under focus. On the other hand, a brief analysis of the ongoing research in the field of multiphase IMs has been pointed out.

The same approach has been presented for permanent-magnet synchronous machines (PMSMs) or even synchronous generators (SGs) but with a shorter description since the main features of the IMs fault detection can be applied in the same way for PMSMs. However, the detection of demagnetization has been added as an important point specific to these machines. As in the case of IMs, a brief analysis of the ongoing research in the field of multiphase PMSMs has also been developed.

The last part of this paper has been dedicated to fault detection in power converters and power components as a part of diagnostic techniques associated with power electronics. For the power converters, specific techniques have been developed in order to speed up the detection process in order to avoid components breakage. These techniques have been successfully applied to inverters, matrix converters, and even to dc–dc converters. The problem of fault detection in dc link capacitors has also been analyzed. For the power components, things are much more difficult since they have fast switching capabilities and the

95 fault detection has to be as fast as possible. Therefore, the fault
 96 detection techniques have been applied to both insulated-gate
 97 bipolar transistors (IGBTs) and MOSFETs in order to protect
 98 them from irreversible failures. In the same way, the very last
 99 part of this paper is dedicated to fault-tolerant drives for which
 100 multilevel and multiphase topologies have been developed in
 101 the last ten years.

102

III. GENERAL METHODS

103 In [7], a robust electric motor fault decision-making algo-
 104 rithm, particularly suited for harsh industrial environments, is
 105 presented. The proposed technique is based on the simultaneous
 106 utilization of multiple fault signature patterns, noise signal fre-
 107 quency patterns, and fundamental harmonics current frequency
 108 patterns in a whole motor current signal for diagnosis purposes.
 109 As the authors pointed out, the identified pattern is proven to be
 110 robust to the signal distortion and inherent monitor noise during
 111 motor dynamic operation. In this paper, it is mathematically and
 112 experimentally proven that the proposed diagnosis algorithm
 113 provides highly accurate monitoring performance while mini-
 114 mizing both false detection and missing detection rates under
 115 high noise and nonlinear machine operating conditions. The
 116 experimental results are obtained with a DSP-based IM drive
 117 system, where motor control and fault diagnosis are performed
 118 in real time. The faulty conditions considered in the work are
 119 broken rotor bars and eccentricities. The authors include some
 120 comments regarding its possible constraints related to industrial
 121 applicability of the proposed technique, stating that since the
 122 proposed method assumes prior knowledge of harmonics in
 123 a motor current spectrum, small additional memory might be
 124 required to implement the proposed method. In addition, a suf-
 125 ficient frequency bandwidth of data acquisition and motor con-
 126 trol is required, particularly for high-frequency signal detection.
 127 In [8], a new online diagnosis of three-phase IM stator
 128 faults using a signal-based method is proposed. The proposed
 129 technique starts with a data preprocessing stage, in which prin-
 130 cipal component analysis (PCA) is applied to current signals.
 131 PCA enables the reduction of the three-phase currents space
 132 to a two-dimensional space. Afterward, features are extracted
 133 from PCA-transformed data using the kernel density estimation
 134 (KDE) improved by fast Gaussian transform along with a point
 135 reduction method. The automatic fault identification is achieved
 136 by means of Kullback–Leibler divergence (KLD), which is used
 137 as an index to identify the dissimilarity between two probability
 138 distributions. The final goal is to ensure that the developed
 139 technique can be used for online monitoring; this is possible due
 140 to the remarkable computational cost reduction obtained with
 141 the aforementioned enhancement techniques, in comparison
 142 with the standard KDE. In this regard, before presenting their
 143 developed algorithm, the authors perform a thorough descrip-
 144 tion and analysis of the considered techniques, namely, PCA,
 145 KDE, improved KDE by fast Gaussian transform, and point
 146 reduction and KLD. This paper also includes experimental
 147 results obtained with two different IMs and under three different
 148 fault conditions: cracked rotor, out-of-tolerance geometry rotor,
 149 and backlash. The tests are carried out at different load and
 150 voltage levels to prove the proposed method effectiveness. The

authors emphasize that it is totally signal based since no IM 151
 parameters are required. 152

In [9], a stochastic modeling-based prognosis approach 153
 [extended Kalman filter (EKF)] is proposed for tracking the 154
 remaining useful life (RUL) of bearings under different oper- 155
 ating conditions. The proposed data-driven methodology relies 156
 on both time and time–frequency domain features of vibration 157
 signals obtained from the PROGNOSTIA platform. In this 158
 regard, the authors reach original conclusions on the better suit- 159
 ability of different features for different operating conditions 160
 depending on the length of the test data set. For instance, the 161
 authors show that the entropy feature is successful at detecting 162
 the early stages of degradation, whereas the variance feature 163
 is not very informative until the final failure stage. As the 164
 authors point out, shorter test data sets provide less information 165
 for RUL estimation yielding higher error rates, which is in 166
 concordance with the conclusions of other works based on the 167
 same data set. Once features have been extracted, an analytical 168
 function, which best approximates the evolution of the fault, 169
 is determined and used to learn the parameters of the EKF. In 170
 this regard, the work gives a detailed description of the RUL 171
 estimation based on EKF, and unlike other investigations, also 172
 provides a procedure to estimate the confidence interval along 173
 with the RUL estimates. The algorithm is finally applied to 174
 bearing vibration data obtained from the mentioned platform, 175
 illustrating the convergence of the algorithm, as well as its be- 176
 havior under different conditions. The work includes a compar- 177
 ison of EKF versus the regular KF showing better performance 178
 of the proposed approach for all operating conditions. 179

IV. IMs

180

In [10], a detailed comparison between the two main groups 181
 of transforms that are employed for IMs rotor assessment based 182
 on transient analysis (continuous versus discrete transforms) 183
 is presented. In this paper, the discrete wavelet transform and 184
 the short-time Fourier transform are taken as representatives 185
 of each respective group. The work begins with an overall 186
 revision of the diagnosis based on transient analysis and the 187
 inherent benefits that such methodology brings in comparison 188
 to the conventional motor current signature analysis (MCSA) 189
 approach. The authors remark on its usefulness in cases where 190
 the MCSA may lead to incorrect diagnostic conclusions. A 191
 detailed description of the operation of each group of trans- 192
 forms is presented making special emphasis on aspects as 193
 fault severity quantification or computational burden. In this 194
 regard, the authors emphasize the following advantages of 195
 the continuous tools versus their discrete counterparts: clearer 196
 extraction of the low-frequency fault components evolutions, 197
 possibility of tracking the high-order harmonics evolutions, 198
 and easier fault discrimination. Afterward, the authors show 199
 the results of applying each transform to data obtained with 200
 real IMs. These results do not only consider trivial fault sit- 201
 uations, where the conventional MCSA also works well, but 202
 also some of the controversial cases, where the application 203
 of the conventional methods often leads to false diagnostics, 204
 namely, outer bar breakages in double cage IMs, IMs with rotor 205
 axial duct influence, as well as combined faults. The authors 206

AQ1

AQ2

207 present a detailed discussion of the performance of each group
208 of transforms based on their results concerning aspects such as
209 quantification or computational time. In their conclusions, they
210 ratify the aforementioned advantages of the continuous tools,
211 and they also tear down the false myth concerning the higher
212 computational burden of continuous transforms.

213 In [11], the authors analyze a diagnostic problem related to
214 IMs with special magnetic structures. More specifically, this
215 paper deals with the false broken rotor bar alarms that have been
216 reported in cage IMs with a number of rotor axial ducts equal to
217 the number of poles. In such cases, even in healthy conditions,
218 two sidebands appear around the fundamental component; their
219 frequencies are equal to those produced by a broken bar. This
220 problem is documented through the analysis of three high-
221 voltage IMs working in actual industrial applications that were
222 misdiagnosed. The authors analyze the theoretical origin of this
223 issue and conclude that the confusing sidebands are produced
224 by the periodical variations of reluctance that the fundamen-
225 tal flux wave undergoes during its relative rotation along the
226 cross section of the rotor. Once the physical phenomenon is
227 explained, the authors propose a diagnosis method based on the
228 current sidebands originated by the fifth and seventh space har-
229 monics of the flux wave. The authors state that these high-order
230 harmonics hardly penetrate the rotor core and, consequently,
231 are not affected by the rotor axial air ducts. This hypothesis is
232 experimentally verified using specifically built prototypes.

233 In [12], the results of a fatigue test that is intended to
234 reproduce, in the most natural way possible, the exposed rotor
235 bar breakage process in an IM. For this purpose, a 1.5-kW
236 two-pole squirrel-cage IM is monitored along 82 265 identical
237 working cycles, each one comprising a heavy start-up, a pe-
238 riod of stationary operation at rated load and, finally, a plug
239 stopping. To accelerate the breakage process, one of the rotor
240 rings was mechanized in order to weaken the junction between
241 the end-ring and the bars. In addition, an incipient breakage
242 was forced in one of the rotor bars. Afterward, the working
243 cycle was repeated until the bar naturally cracked. Taking as
244 bases the results of these tests, the authors carry out three
245 different analyses. First, they compare the performances of sev-
246 eral fault indicators described in the literature for tracking the
247 fault components evolutions; transient and steady-state-based
248 parameters are considered in this study. Second, an explanation
249 of the breakage mechanism is given, based on a series of
250 pictures of the breakage region, which were taken during the
251 breakage development. Third, a physical model of the failure
252 is introduced and, based on this model, the authors propose
253 an algorithm for state estimation and prognosis analysis of the
254 bars health.

255 In [13], a diagnostic method based on parameter estimation,
256 which is applied to the detection of interturn short circuits in
257 IMs, is proposed. The detection algorithm is based on three
258 blocks that are cyclically executed: The first block is a coupled
259 circuits model of the IM, able to simulate faults in the stator
260 windings; in this model, the faults are characterized by three
261 parameters (μf : fault location; μs : severity of the fault; LL:
262 load level). The second block is an objective function whose
263 value depends on the errors between the measured currents
264 and the currents calculated by the model. The third block is a

global optimization algorithm, called hyperbolic cross points 265
algorithm. It efficiently seeks the combination of parameter 266
values, which minimize the objective function under the tested 267
operation conditions. The authors claim that the proposed al- 268
gorithm reliably locates, with a reduced number of iterations, 269
the global minimum of the objective function, avoiding errors 270
due to local minima. The state of the IM, i.e., the severity and 271
location of the fault, is characterized by the set of parameters 272
that lead to the global minimum of the objective function. The 273
authors validate the method by simulations and laboratory tests, 274
showing that it can detect a fault affecting 8% of the turns of a 275
phase with a processing time of 106 s. 276

In [14], a method for monitoring the insulation health of 277
IMs is proposed. As the authors highlight, the objective of 278
this work is not to detect sudden insulation faults but to ob- 279
serve a trend of the insulation state indicator over time. The 280
method is applicable to IMs fed by voltage-source inverters. It 281
relies on an offline test, which consists of applying a voltage 282
step, obtained by switching the inverter, to the tested phase. 283
The subsequent reaction current is recorded and employed to 284
evaluate the winding condition. This current is based on high- 285
frequency oscillations, which vanish after a few microseconds. 286
It is shown that the current evolution depends on the parasitic 287
turn-to-turn and winding-to-ground capacitances that change 288
during the aging process of the insulation. The authors propose 289
two insulation state indicators, which are intended for phase 290
evaluation (ISI) and global winding evaluation (SISI). These 291
parameters are computed comparing the current spectra and 292
reference spectra, obtained in healthy condition. The method 293
is validated on two quite different IMs, rated 280 V, 5.5 kW and 294
1428 kW, 2183 V, respectively. 295

In [15], a new technique based on stray flux measurement is 296
proposed for bearing fault detection in IMs. The method relies 297
on the statistical processing of the measurements of this quan- 298
tity in different positions around the IM. The usefulness of the 299
proposed method is mainly justified based on the simplicity and 300
the flexibility of the custom flux probe with its amplification 301
and filtering stage. The authors first present a detailed literature 302
survey about the use of stray flux measurement in the IMs fault 303
diagnosis area, emphasizing the advantages of such approach 304
in comparison with other techniques. Afterward, their proposed 305
method is described; it requires at least ten data acquisitions of 306
the stray flux, performed under identical conditions, both for 307
the healthy machine (considered as reference) and the same 308
machine having diverse bearing faults. The authors prove the 309
validity of the method in a real IM, considering three different 310
types of bearing failure (crack in the outer race, hole in the 311
outer race, and deformation of the seal) under different load 312
conditions. In addition, different positions for the flux mea- 313
surement with their custom probe are considered, as well as a 314
comparison with a commercial probe, leading to a total number 315
of 32 analyzed cases. Their subsequent discussions lead to 316
interesting conclusions as to the suitability of the method even 317
to detect damages in the bearing seal, the good performance 318
of their probe for higher loads or the general higher effectivity 319
of the custom probe versus the commercial one for stray flux 320
measurements, among others. The only requisite of the method 321
is that it needs an initial data set as “healthy reference” for 322

323 comparisons to the successive measurements during the IM
324 lifetime.

325 In [16], a methodology for diagnosing localized defects in
326 the outer race of IM bearings is introduced. The method relies
327 on the spectral analysis of the squared envelope of the stator
328 current in an optimized frequency band, characterized by a
329 central frequency f_c and a bandwidth Bw , which contains the
330 nonstationary components with frequencies related to fault. The
331 optimum frequency interval is selected using the kurtogram of
332 the current as a decision tool: it simply consists of selecting the
333 central frequency/bandwidth combination that maximizes the
334 spectral Kurtosis in the kurtogram. Advanced algorithms such
335 as the fast kurtogram or the wavelet kurtogram are used in this
336 work to compute the kurtogram in a computationally efficient
337 way. The method is validated by means of laboratory tests,
338 using two bearings with forced faults, consisting of holes with
339 different diameters. Under these strong defect conditions, this
340 technique enables a clear detection of the fault components,
341 although as the authors state, the method needs to be validated
342 with small and real defects.

343 In [17], the authors have presented the gear tooth damage
344 fault detection using the IM as a sensor but measuring its stator
345 currents. The basic principle is to use the torque oscillations
346 as a means to bring to the IM currents the image of what is
347 happening in the mechanical part related to the machine shaft.
348 Therefore, the electromagnetic torque has been developed as
349 a mean part plus an oscillation part for both healthy and faulty
350 cases and characteristic frequencies of the oscillating parts
351 have been identified. A simplified model of the mechanical part
352 has been developed to compute these characteristic frequencies
353 from a theoretical point of view and to relate them to the IM
354 currents. In order to detect the different frequencies related to
355 the mechanical failure, a fault profile reconstruction has been
356 defined and a fault index has been proposed. The proposed
357 methodology has been applied to a simple test rig with a
358 three-phase IM connected by its shaft to a pinion and a wheel
359 with very small surface wear damage on one tooth for each
360 part. Both simulation and experimental results have confirmed
361 the validity of this new technique of mechanical fault detection.

362 In [18], a method called spectral kurtosis with reference is
363 employed to design a system's healthy reference. This approach
364 is afterward evaluated for mechanical unbalance detection in
365 IMs using the stator currents instantaneous frequency. As the
366 authors explain, the definition of a healthy reference enables
367 the computation of normalized fault indicators whose values
368 are independent of the system characteristics. This means a
369 significant advantage when diagnosing systems with different
370 power, coupling, inertia, and load. In this paper, the authors re-
371 view the concept of kurtosis and demonstrate its ability to detect
372 outliers within a reference distribution. They introduce a new
373 kurtosis-based indicator, SK_R , which includes a new reference
374 set, and they prove its ability to generate a system's healthy
375 reference and to detect any drift from it. The authors evaluate
376 this indicator using synthetic signals and also experimentally
377 verify its efficiency when applied to the current instantaneous
378 frequency for the detection of low levels of mechanical unbal-
379 ance. Their results prove the SK_R detection capacity with a
380 single fault threshold for a wide range of load conditions and

ratify the usefulness of creating a system's healthy reference for 381
the robust detection of weak mechanical unbalances, avoiding 382
false alarms for different operating conditions and showing a 383
great robustness against load variations. 384

V. SYNCHRONOUS MACHINES 385

In [19], an SG model that enables the simulation of stator 386
interturn short circuits is presented. The novelty of this work is 387
that it develops a hybrid model, in which the Winding Function 388
Approach (WFA) is combined with the $dq0$ transform. As the 389
authors remark, the proposed model takes advantage of the 390
suitability of WFA for detailed and simple representation of 391
the faults and, at the same time, enables the calculation simplic- 392
ity that is provided by the $dq0$ representation. Consequently, a 393
very precise model that is suitable to run online is achieved. In 394
addition, this model accounts for the effect of local saturation of 395
the magnetic circuit due to the fault currents. Local saturation 396
and saliency are taken into consideration through a modified 397
airgap function, which facilitates the accurate computation of 398
the inductance of the shorted turns. The model is extensively 399
validated by laboratory tests and compared with a model based 400
on the $dq0$ transform. The authors conclude that the proposed 401
model provides more accurate results than the $dq0$ model 402
although its performance with incipient faults needs to be 403
improved. 404

The work presented in [20] deals with the accurate local- 405
ization of field-winding to ground faults in SGs. First, the 406
authors analyze in detail a previously developed method for 407
the online detection of excitation-system faults to ground that 408
is valid for generators with static excitation. The method allows 409
discriminating if the fault takes place in the ac side or in the dc 410
side of the excitation system. In the event of faults in the dc side, 411
the method approximately forecasts the location of the fault in 412
the excitation winding. However, this procedure depends on the 413
value of the fault resistance R_f , which has to be estimated; this 414
fact leading to a wide margin of indetermination. The main 415
contribution of this work is a new algorithm that, from the 416
measured quantities, accurately calculates the value of the fault 417
resistance R_f . The method is validated through laboratory tests 418
and also on a 106-MW SG operating under real conditions in 419
a hydroelectric power plant. From the test results, the authors 420
claim that the proposed method for the computation of R_f 421
significantly reduces the errors in the fault location; this fact is 422
relevant in hydrogenerators with high number of poles, since it 423
reliably enables the location of the pole where the fault occurs. 424
This way, the extraction of the whole rotor can be avoided, thus 425
substantially reducing repair costs. 426

In [21], the authors introduce an approach for interturn short- 427
circuit diagnosis in five-phase PMSMs. The approach relies on 428
the spectral analysis of the modulus of a space vector \vec{D} . This 429
vector is obtained as a combination of two space vectors that 430
are calculated from the measured phase voltages but using two 431
different reference frames, named $\alpha\beta$ and $\alpha2\beta2$. It is justified 432
that an interturn fault in one of the stator phases produces an 433
increase in the DC and $2fs$ components in the spectrum of 434
the modulus of the space vector \vec{D} (fs : supply frequency 435
fundamental harmonic). It is shown from simulations and tests 436

437 that this signature is very sensible, reaching amplitude incre-
438 ments in the fault-related harmonics higher than 15 dB for
439 a fault affecting up to 3% of the turns of a phase; and it is
440 also clearly different from the signatures produced by other
441 kind of faults (as static or dynamic eccentricity and partial
442 demagnetization), thus enabling a robust and reliable diagnosis
443 of interturn short-circuit faults.

444 The work presented in [22], as in the previous paper, deals
445 with interturn short-circuit detection in PMSMs. In this case,
446 the work is focused on three-phase PMSMs working under
447 high variable load and speed conditions, as it happens in
448 aircraft applications. This work proposes an approach based on
449 parameter identification. The authors introduce a PMSM model
450 based on the dq reference frame, where the short-circuited turns
451 ratios of each phase ($n_{s/cA}, n_{s/cB}, n_{s/cC}$) are the parameters
452 to be identified. The estimation of these parameters is carried
453 out using the EKF, which is justified to be a suitable tool that
454 enables to perform accurate estimations in real time, even under
455 continuous and substantial changes in the operation conditions.
456 Finally, the fault indicators are defined as the average value
457 of the estimated short-circuited turns ratios calculated over a
458 sliding window with a length equal to half period of the main
459 component. The approach is extensively validated by simula-
460 tion and laboratory tests; it is demonstrated to be robust against
461 frequency variations, load variations, power factor variations,
462 load unbalances, and harmonic content variations.

463 Reference [23] is the only paper in this Special Section
464 dealing with axial flux PMSMs. In this paper, the authors
465 introduce a method for diagnosing static eccentricities in axial
466 flux PMSMs. The method requires the installation of three
467 search coils, mounted on three stator teeth shifted 120° . First,
468 a parameter named static eccentricity factor (SEF) is defined
469 in order to characterize the fault severity in such type of
470 machines; then, a simple algorithm is theoretically justified
471 that enables calculation of the SEF, and also the position of
472 minimum airgap in a faulty machine, using the measured back
473 electromotive forces in the search coils. It is interesting that
474 the computed SEF depends neither on the rotor speed nor on
475 the load. The approach is extensively validated via simulations,
476 using a 3-D finite-element software, as well as thorough labo-
477 ratory tests.

478

VI. ELECTRICAL DRIVES

479 In [24], a new fault detection and isolation technique is pre-
480 sented with the aim of making the traditional vector-controlled
481 IM drive fault tolerant against current and speed sensor failure.
482 The underlying idea is that the controller keeps estimating
483 the different currents and the speed and, in case of a fault, it
484 switches to the correct estimated value. On the one hand, the
485 proposed technique extracts eight estimates of currents in the
486 $\alpha - \beta$ reference frame (the authors obtain four estimates using
487 the reverse transformation from $d-q$ to $\alpha - \beta$ and the other
488 four using the forward transformation from $a-b-c$ to $\alpha - \beta$).
489 In this context, the concept of vector rotation is introduced to
490 decide the correct estimated value of current corresponding to a
491 fault. On the other hand, the speed is estimated by modifying
492 one of the available model reference adaptive system-based

formulations (X-based MRAS). Both simulations, as well as 493
494 experiments carried out with a laboratory prototype, demon- 494
495 strate that the system is capable of detecting a fault and recon- 495
496 figure itself in a seamless manner. In this regard, the authors 496
497 thoroughly evaluate the performance of the proposed algorithm 497
498 under different faulty conditions of the considered sensors. 498
499 The results prove that proposed technique works well even in 499
500 the case of multiple sensor failures and does not require any 500
501 additional sensor. The developed fault-tolerant controller can 501
502 be particularly useful for applications such as electric vehicles 502
503 to avoid complete shutdown of the system, in case of sensor 503
504 failure. 504

In [25], the detection of incipient faults in coupling inductors 505
506 used in three-phase adjustable-speed drives with direct power 506
507 control-based active front-end rectifiers is considered. More 507
508 specifically, the authors develop a new strategy for early fault 508
509 detection in coupling inductors, which enables a fast identi- 509
510 fication of the defective phase while providing an accurate 510
511 estimation of the inductance value of the coupling inductors that 511
512 enhances the performance of the direct power control method. 512
513 The underlying idea is that coupling inductor faults (e.g., an 513
514 interturn short circuit) lead to a variation in the value of the 514
515 coupling inductance. Hence, the goal is to detect the fault by 515
516 tracking estimations of the coupling inductances associated 516
517 with a fault in each phase. A detailed description of the full 517
518 estimation procedure is given in this paper. Both simulation 518
519 and experimental tests demonstrate the validity of the proposed 519
520 method. As stated in this paper, the detection of the fault 520
521 enables the suspension of the service if this is required to 521
522 avoid a major breakdown. In addition, the identification of the 522
523 affected phase enables the replacement of only the defective 523
524 inductor if three single-phase chokes are used or helps with 524
525 the repair of the nonhealthy winding if a three-phase reactor is 525
526 used. Among the claimed advantages of the proposed method 526
527 are the simplicity, speed, and effectiveness. On the other hand, 527
528 the main constraint relies on the manufacturing tolerance of 528
529 the inductors, which makes their actual values differ from 529
530 each other including when there are not any faults. This latter 530
531 issue, however, does not affect the robustness of the presented 531
532 strategy. 532

In [26], an observer-based fault detection method is designed 533
534 for the rotor position sensor of PMSM drives in an elec- 534
535 tromechanical brake (EMB). To this end, the authors develop 535
536 a position estimation algorithm with a full-order Luenberger 536
537 observer for the rotor flux linkage. However, there are some 537
538 deviations between the observer and the real process caused by 538
539 model uncertainties and parameter variations. To overcome this 539
540 drawback, the authors add a crucial feature in their detection 540
541 method that relies on an adaptive threshold; this is determined 541
542 by analyzing position estimation errors of the observer. The 542
543 adaptive threshold enables, among other things, avoidance of 543
544 missing or false alarms. The experimental results using the 544
545 EMB test bench prove the effectiveness and robustness of the 545
546 designed method that can even detect a small amount of phase 546
547 shift fault within a wide operation range, not only at steady state 547
548 but also under transient operation. Moreover, the fault-tolerance 548
549 capability of the proposed method is achieved by introducing a 549
550 compensation algorithm for the phase shift. The experimental 550

551 results show that this compensation algorithm is useful for
 552 tolerating the phase shift fault. For other types of rotor position
 553 sensor faults, the authors propose potential solutions that can
 554 overcome low-speed limitation issues, such as the incorporation
 555 with a high-frequency injection-based method. This latter ap-
 556 proach can be somehow complementary to that proposed in the
 557 work, since each of them shows special suitability for different
 558 speed ranges.

559 VII. POWER COMPONENTS AND POWER CONVERTERS

560 In [27], an adaptive threshold-based approach is also pre-
 561 sented, but in this case it is to design an electronic failure detec-
 562 tion system applied to the IGBT. More specifically, the method
 563 proposed by the authors relies on the direct measurement of
 564 behavior of the gate signal during the IGBT turn-on transient
 565 via continuous processing using analog and digital electronics.
 566 The main goal pursued with an early fault detection design in
 567 the IGBT is to obtain a corrective action to prevent propagation
 568 of the fault to the complementary device in the same affected
 569 leg in the inverter-motor system, when a short circuit or an
 570 overcurrent occurs. Two different faults are considered in the
 571 work: open-circuit and short-circuit failures. The considered
 572 stages of the developed diagnosis scheme are improved resid-
 573 ual generation stage, ramp rate, and a symmetrical adaptable
 574 thresholds stage. The final scheme is intended to decrease the
 575 false alarm rate by the aforementioned failures. To achieve the
 576 early fault detection, the proposed circuit is implemented in
 577 the gate driver using analog electronics. As the authors point
 578 out, the main advantage of adding detection process with adap-
 579 tive threshold is that the false alarm rate decreases because the
 580 system is not so vulnerable to variations in the power supply
 581 of the IGBT gate driver circuit. On the other hand, the main
 582 limitation is that the proposed design is not suitable for power
 583 applications, where the switching frequency is above 20 kHz
 584 since the introduction of an external resistance limits the IGBT
 585 switching speed.

586 In [28], a methodology to analyze the losses in the converters
 587 of fault-tolerant drives is presented. This work aims to evaluate
 588 the losses in the power components of the converter (IGBT,
 589 diodes, capacitors) during the time the fault takes place, during
 590 the subsequent reconfiguration process and, finally, during the
 591 operation in faulty mode; the objective is to assess whether the
 592 drive components are able to withstand the thermal stresses that
 593 produce transient currents during the fault and reconfiguration
 594 period; and also assess the possible reduction in the rated power
 595 of the converter when operating in faulty mode. The authors
 596 perform the analysis on a single but actual topology of a fault-
 597 tolerant inverter and develop a simple model to assess the
 598 losses in all the components after an IGBT open-circuit fault
 599 event, both during the fault, reconfiguration process, and faulty
 600 operation. The model was validated experimentally by compar-
 601 ing the sum of computed losses and the total losses measured
 602 in the experimental rig. From the analysis, conclusions about
 603 the maximum allowable time in faulty and reconfiguration
 604 conditions or the maximum power after the reconfiguration are
 605 discussed.

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AUTHOR PLEASE ANSWER ALL QUERIES

AQ1 = Please check if provided definition for DSP is correct. Otherwise, please make the necessary corrections.

AQ2 = Please check if provided definition for MCSA is correct. Otherwise, please make the necessary corrections.

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Modern Diagnostics Techniques for Electrical Machines, Power Electronics, and Drives

I. INTRODUCTION

FOR THE last ten years, at least three different Special Sections dealing with diagnostics in power electrical engineering have been published in the IEEE TRANSACTIONS ON INDUSTRIAL ELECTRONICS [1]–[5]. All of them had their specificities, but the last ones, starting in 2011, were more connected to relevant events organized on the topic. In fact, these events have been clearly the only international forums fully dedicated to diagnostics techniques in power electrical engineering. For this particular issue, it has been decided to separate the different submissions into six parts:

- state of the art;
- general methods;
- induction machines (IMs);
- synchronous machines;
- electrical drives;
- power components and power converters.

The second section includes only one state-of-the-art paper, which is dedicated to actual techniques implemented in both industry and research laboratories. The third section includes three papers on diagnostic techniques not specifically aimed at a particular type of machine. The fourth section includes three papers devoted to diagnostics of rotor faults, two dedicated to stator insulation issues, and four papers dealing with mechanical faults diagnosis in IMs. The fifth section includes papers focusing on different types of synchronous machines. The first two papers deal with wound-rotor synchronous machines, the following three papers are dedicated to permanent-magnet radial flux machines, and the last one deals with permanent-magnet axial flux machines. Regarding the types of faults analyzed, there are three papers devoted to the diagnosis of interturn short circuits in the stator windings, i.e., one dedicated to the detection and location of field-winding-to-ground faults and a paper devoted to the diagnosis of static eccentricities. In the sixth section, two papers investigate issues related to faults in drive sensors, and one is devoted to fault detections in the coupling inductors. The last section includes two papers devoted to diagnosis of faults and losses analysis in switching components of power converters.

II. STATE OF THE ART

In [6], the authors have screened the most recent papers published on the topic to draw the real “state of the art” on condition monitoring and fault detection of rotating electrical

machines, drives, and power electronics. As expected, since it is the most investigated electrical machine from the very beginning, a large part of the development has been dedicated to IMs. It is well known that most of the methods developed for IMs can be simply used directly or adapted for other types of rotating electrical machines or even for linear actuators or generators.

A large part of this paper is dedicated to IM fault detection since it has been the historical field of investigation for the last 30 years or so. In this way, rotor faults have been under focus mainly for squirrel-cage IMs with convenient signal processing techniques to tackle the fact that many faults cannot be detected easily when the machine load is light. The second largest part dealing with the IM fault detection is related to stator winding, including the insulation degradation and further early stage short circuits. It has been shown that the insulation degradation detection is the best way to prevent short circuits, but it is the most difficult to be implemented online. Moreover, early stage short circuits are easier to detect particularly by the use of a stray flux sensor, which is simple, cheap, and noninvasive for large-power IMs. Other methods to detect early stage short circuits are based on the impedance asymmetry on the stator side. In this last case, the sensors are based on both stator voltages and stator currents measurements. Then, the decision process for early stage short-circuit detection can be based on advanced artificial intelligence techniques, which are well known in this specific area. Finally, in the case of IMs, methods for mechanical failures detection have been investigated. Faults such as eccentricities, bearings, and gearboxes have been under focus. On the other hand, a brief analysis of the ongoing research in the field of multiphase IMs has been pointed out.

The same approach has been presented for permanent-magnet synchronous machines (PMSMs) or even synchronous generators (SGs) but with a shorter description since the main features of the IMs fault detection can be applied in the same way for PMSMs. However, the detection of demagnetization has been added as an important point specific to these machines. As in the case of IMs, a brief analysis of the ongoing research in the field of multiphase PMSMs has also been developed.

The last part of this paper has been dedicated to fault detection in power converters and power components as a part of diagnostic techniques associated with power electronics. For the power converters, specific techniques have been developed in order to speed up the detection process in order to avoid components breakage. These techniques have been successfully applied to inverters, matrix converters, and even to dc–dc converters. The problem of fault detection in dc link capacitors has also been analyzed. For the power components, things are much more difficult since they have fast switching capabilities and the

95 fault detection has to be as fast as possible. Therefore, the fault
 96 detection techniques have been applied to both insulated-gate
 97 bipolar transistors (IGBTs) and MOSFETs in order to protect
 98 them from irreversible failures. In the same way, the very last
 99 part of this paper is dedicated to fault-tolerant drives for which
 100 multilevel and multiphase topologies have been developed in
 101 the last ten years.

102

III. GENERAL METHODS

103 In [7], a robust electric motor fault decision-making algo-
 104 rithm, particularly suited for harsh industrial environments, is
 105 presented. The proposed technique is based on the simultaneous
 106 utilization of multiple fault signature patterns, noise signal fre-
 107 quency patterns, and fundamental harmonics current frequency
 108 patterns in a whole motor current signal for diagnosis purposes.
 109 As the authors pointed out, the identified pattern is proven to be
 110 robust to the signal distortion and inherent monitor noise during
 111 motor dynamic operation. In this paper, it is mathematically and
 112 experimentally proven that the proposed diagnosis algorithm
 113 provides highly accurate monitoring performance while mini-
 114 mizing both false detection and missing detection rates under
 115 high noise and nonlinear machine operating conditions. The
 116 experimental results are obtained with a DSP-based IM drive
 117 system, where motor control and fault diagnosis are performed
 118 in real time. The faulty conditions considered in the work are
 119 broken rotor bars and eccentricities. The authors include some
 120 comments regarding its possible constraints related to industrial
 121 applicability of the proposed technique, stating that since the
 122 proposed method assumes prior knowledge of harmonics in
 123 a motor current spectrum, small additional memory might be
 124 required to implement the proposed method. In addition, a suf-
 125 ficient frequency bandwidth of data acquisition and motor con-
 126 trol is required, particularly for high-frequency signal detection.
 127 In [8], a new online diagnosis of three-phase IM stator
 128 faults using a signal-based method is proposed. The proposed
 129 technique starts with a data preprocessing stage, in which prin-
 130 cipal component analysis (PCA) is applied to current signals.
 131 PCA enables the reduction of the three-phase currents space
 132 to a two-dimensional space. Afterward, features are extracted
 133 from PCA-transformed data using the kernel density estimation
 134 (KDE) improved by fast Gaussian transform along with a point
 135 reduction method. The automatic fault identification is achieved
 136 by means of Kullback–Leibler divergence (KLD), which is used
 137 as an index to identify the dissimilarity between two probability
 138 distributions. The final goal is to ensure that the developed
 139 technique can be used for online monitoring; this is possible due
 140 to the remarkable computational cost reduction obtained with
 141 the aforementioned enhancement techniques, in comparison
 142 with the standard KDE. In this regard, before presenting their
 143 developed algorithm, the authors perform a thorough descrip-
 144 tion and analysis of the considered techniques, namely, PCA,
 145 KDE, improved KDE by fast Gaussian transform, and point
 146 reduction and KLD. This paper also includes experimental
 147 results obtained with two different IMs and under three different
 148 fault conditions: cracked rotor, out-of-tolerance geometry rotor,
 149 and backlash. The tests are carried out at different load and
 150 voltage levels to prove the proposed method effectiveness. The

authors emphasize that it is totally signal based since no IM 151
 parameters are required. 152

In [9], a stochastic modeling-based prognosis approach 153
 [extended Kalman filter (EKF)] is proposed for tracking the 154
 remaining useful life (RUL) of bearings under different oper- 155
 ating conditions. The proposed data-driven methodology relies 156
 on both time and time–frequency domain features of vibration 157
 signals obtained from the PROGNOSTIA platform. In this 158
 regard, the authors reach original conclusions on the better suit- 159
 ability of different features for different operating conditions 160
 depending on the length of the test data set. For instance, the 161
 authors show that the entropy feature is successful at detecting 162
 the early stages of degradation, whereas the variance feature 163
 is not very informative until the final failure stage. As the 164
 authors point out, shorter test data sets provide less information 165
 for RUL estimation yielding higher error rates, which is in 166
 concordance with the conclusions of other works based on the 167
 same data set. Once features have been extracted, an analytical 168
 function, which best approximates the evolution of the fault, 169
 is determined and used to learn the parameters of the EKF. In 170
 this regard, the work gives a detailed description of the RUL 171
 estimation based on EKF, and unlike other investigations, also 172
 provides a procedure to estimate the confidence interval along 173
 with the RUL estimates. The algorithm is finally applied to 174
 bearing vibration data obtained from the mentioned platform, 175
 illustrating the convergence of the algorithm, as well as its be- 176
 havior under different conditions. The work includes a compar- 177
 ison of EKF versus the regular KF showing better performance 178
 of the proposed approach for all operating conditions. 179

IV. IMs

180

In [10], a detailed comparison between the two main groups 181
 of transforms that are employed for IMs rotor assessment based 182
 on transient analysis (continuous versus discrete transforms) 183
 is presented. In this paper, the discrete wavelet transform and 184
 the short-time Fourier transform are taken as representatives 185
 of each respective group. The work begins with an overall 186
 revision of the diagnosis based on transient analysis and the 187
 inherent benefits that such methodology brings in comparison 188
 to the conventional motor current signature analysis (MCSA) 189
 approach. The authors remark on its usefulness in cases where 190
 the MCSA may lead to incorrect diagnostic conclusions. A 191
 detailed description of the operation of each group of trans- 192
 forms is presented making special emphasis on aspects as 193
 fault severity quantification or computational burden. In this 194
 regard, the authors emphasize the following advantages of 195
 the continuous tools versus their discrete counterparts: clearer 196
 extraction of the low-frequency fault components evolutions, 197
 possibility of tracking the high-order harmonics evolutions, 198
 and easier fault discrimination. Afterward, the authors show 199
 the results of applying each transform to data obtained with 200
 real IMs. These results do not only consider trivial fault sit- 201
 uations, where the conventional MCSA also works well, but 202
 also some of the controversial cases, where the application 203
 of the conventional methods often leads to false diagnostics, 204
 namely, outer bar breakages in double cage IMs, IMs with rotor 205
 axial duct influence, as well as combined faults. The authors 206

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207 present a detailed discussion of the performance of each group
208 of transforms based on their results concerning aspects such as
209 quantification or computational time. In their conclusions, they
210 ratify the aforementioned advantages of the continuous tools,
211 and they also tear down the false myth concerning the higher
212 computational burden of continuous transforms.

213 In [11], the authors analyze a diagnostic problem related to
214 IMs with special magnetic structures. More specifically, this
215 paper deals with the false broken rotor bar alarms that have been
216 reported in cage IMs with a number of rotor axial ducts equal to
217 the number of poles. In such cases, even in healthy conditions,
218 two sidebands appear around the fundamental component; their
219 frequencies are equal to those produced by a broken bar. This
220 problem is documented through the analysis of three high-
221 voltage IMs working in actual industrial applications that were
222 misdiagnosed. The authors analyze the theoretical origin of this
223 issue and conclude that the confusing sidebands are produced
224 by the periodical variations of reluctance that the fundamen-
225 tal flux wave undergoes during its relative rotation along the
226 cross section of the rotor. Once the physical phenomenon is
227 explained, the authors propose a diagnosis method based on the
228 current sidebands originated by the fifth and seventh space har-
229 monics of the flux wave. The authors state that these high-order
230 harmonics hardly penetrate the rotor core and, consequently,
231 are not affected by the rotor axial air ducts. This hypothesis is
232 experimentally verified using specifically built prototypes.

233 In [12], the results of a fatigue test that is intended to
234 reproduce, in the most natural way possible, the exposed rotor
235 bar breakage process in an IM. For this purpose, a 1.5-kW
236 two-pole squirrel-cage IM is monitored along 82 265 identical
237 working cycles, each one comprising a heavy start-up, a pe-
238 riod of stationary operation at rated load and, finally, a plug
239 stopping. To accelerate the breakage process, one of the rotor
240 rings was mechanized in order to weaken the junction between
241 the end-ring and the bars. In addition, an incipient breakage
242 was forced in one of the rotor bars. Afterward, the working
243 cycle was repeated until the bar naturally cracked. Taking as
244 bases the results of these tests, the authors carry out three
245 different analyses. First, they compare the performances of sev-
246 eral fault indicators described in the literature for tracking the
247 fault components evolutions; transient and steady-state-based
248 parameters are considered in this study. Second, an explanation
249 of the breakage mechanism is given, based on a series of
250 pictures of the breakage region, which were taken during the
251 breakage development. Third, a physical model of the failure
252 is introduced and, based on this model, the authors propose
253 an algorithm for state estimation and prognosis analysis of the
254 bars health.

255 In [13], a diagnostic method based on parameter estimation,
256 which is applied to the detection of interturn short circuits in
257 IMs, is proposed. The detection algorithm is based on three
258 blocks that are cyclically executed: The first block is a coupled
259 circuits model of the IM, able to simulate faults in the stator
260 windings; in this model, the faults are characterized by three
261 parameters (μf : fault location; μs : severity of the fault; LL:
262 load level). The second block is an objective function whose
263 value depends on the errors between the measured currents
264 and the currents calculated by the model. The third block is a

global optimization algorithm, called hyperbolic cross points
algorithm. It efficiently seeks the combination of parameter
values, which minimize the objective function under the tested
operation conditions. The authors claim that the proposed al-
gorithm reliably locates, with a reduced number of iterations,
the global minimum of the objective function, avoiding errors
due to local minima. The state of the IM, i.e., the severity and
location of the fault, is characterized by the set of parameters
that lead to the global minimum of the objective function. The
authors validate the method by simulations and laboratory tests,
showing that it can detect a fault affecting 8% of the turns of a
phase with a processing time of 106 s.

276
277 In [14], a method for monitoring the insulation health of
IMs is proposed. As the authors highlight, the objective of
this work is not to detect sudden insulation faults but to ob-
serve a trend of the insulation state indicator over time. The
method is applicable to IMs fed by voltage-source inverters. It
relies on an offline test, which consists of applying a voltage
step, obtained by switching the inverter, to the tested phase.
The subsequent reaction current is recorded and employed to
evaluate the winding condition. This current is based on high-
frequency oscillations, which vanish after a few microseconds.
It is shown that the current evolution depends on the parasitic
turn-to-turn and winding-to-ground capacitances that change
during the aging process of the insulation. The authors propose
two insulation state indicators, which are intended for phase
evaluation (ISI) and global winding evaluation (SISI). These
parameters are computed comparing the current spectra and
reference spectra, obtained in healthy condition. The method
is validated on two quite different IMs, rated 280 V, 5.5 kW and
1428 kW, 2183 V, respectively.

295
296 In [15], a new technique based on stray flux measurement is
proposed for bearing fault detection in IMs. The method relies
on the statistical processing of the measurements of this quan-
tity in different positions around the IM. The usefulness of the
proposed method is mainly justified based on the simplicity and
the flexibility of the custom flux probe with its amplification
and filtering stage. The authors first present a detailed literature
survey about the use of stray flux measurement in the IMs fault
diagnosis area, emphasizing the advantages of such approach
in comparison with other techniques. Afterward, their proposed
method is described; it requires at least ten data acquisitions of
the stray flux, performed under identical conditions, both for
the healthy machine (considered as reference) and the same
machine having diverse bearing faults. The authors prove the
validity of the method in a real IM, considering three different
types of bearing failure (crack in the outer race, hole in the
outer race, and deformation of the seal) under different load
conditions. In addition, different positions for the flux mea-
surement with their custom probe are considered, as well as a
comparison with a commercial probe, leading to a total number
of 32 analyzed cases. Their subsequent discussions lead to
interesting conclusions as to the suitability of the method even
to detect damages in the bearing seal, the good performance
of their probe for higher loads or the general higher effectivity
of the custom probe versus the commercial one for stray flux
measurements, among others. The only requisite of the method
is that it needs an initial data set as "healthy reference" for

323 comparisons to the successive measurements during the IM
324 lifetime.

325 In [16], a methodology for diagnosing localized defects in
326 the outer race of IM bearings is introduced. The method relies
327 on the spectral analysis of the squared envelope of the stator
328 current in an optimized frequency band, characterized by a
329 central frequency f_c and a bandwidth Bw , which contains the
330 nonstationary components with frequencies related to fault. The
331 optimum frequency interval is selected using the kurtogram of
332 the current as a decision tool: it simply consists of selecting the
333 central frequency/bandwidth combination that maximizes the
334 spectral Kurtosis in the kurtogram. Advanced algorithms such
335 as the fast kurtogram or the wavelet kurtogram are used in this
336 work to compute the kurtogram in a computationally efficient
337 way. The method is validated by means of laboratory tests,
338 using two bearings with forced faults, consisting of holes with
339 different diameters. Under these strong defect conditions, this
340 technique enables a clear detection of the fault components,
341 although as the authors state, the method needs to be validated
342 with small and real defects.

343 In [17], the authors have presented the gear tooth damage
344 fault detection using the IM as a sensor but measuring its stator
345 currents. The basic principle is to use the torque oscillations
346 as a means to bring to the IM currents the image of what is
347 happening in the mechanical part related to the machine shaft.
348 Therefore, the electromagnetic torque has been developed as
349 a mean part plus an oscillation part for both healthy and faulty
350 cases and characteristic frequencies of the oscillating parts
351 have been identified. A simplified model of the mechanical part
352 has been developed to compute these characteristic frequencies
353 from a theoretical point of view and to relate them to the IM
354 currents. In order to detect the different frequencies related to
355 the mechanical failure, a fault profile reconstruction has been
356 defined and a fault index has been proposed. The proposed
357 methodology has been applied to a simple test rig with a
358 three-phase IM connected by its shaft to a pinion and a wheel
359 with very small surface wear damage on one tooth for each
360 part. Both simulation and experimental results have confirmed
361 the validity of this new technique of mechanical fault detection.

362 In [18], a method called spectral kurtosis with reference is
363 employed to design a system's healthy reference. This approach
364 is afterward evaluated for mechanical unbalance detection in
365 IMs using the stator currents instantaneous frequency. As the
366 authors explain, the definition of a healthy reference enables
367 the computation of normalized fault indicators whose values
368 are independent of the system characteristics. This means a
369 significant advantage when diagnosing systems with different
370 power, coupling, inertia, and load. In this paper, the authors re-
371 view the concept of kurtosis and demonstrate its ability to detect
372 outliers within a reference distribution. They introduce a new
373 kurtosis-based indicator, SK_R , which includes a new reference
374 set, and they prove its ability to generate a system's healthy
375 reference and to detect any drift from it. The authors evaluate
376 this indicator using synthetic signals and also experimentally
377 verify its efficiency when applied to the current instantaneous
378 frequency for the detection of low levels of mechanical unbal-
379 ance. Their results prove the SK_R detection capacity with a
380 single fault threshold for a wide range of load conditions and

ratify the usefulness of creating a system's healthy reference for 381
the robust detection of weak mechanical unbalances, avoiding 382
false alarms for different operating conditions and showing a 383
great robustness against load variations. 384

V. SYNCHRONOUS MACHINES 385

In [19], an SG model that enables the simulation of stator 386
interturn short circuits is presented. The novelty of this work is 387
that it develops a hybrid model, in which the Winding Function 388
Approach (WFA) is combined with the $dq0$ transform. As the 389
authors remark, the proposed model takes advantage of the 390
suitability of WFA for detailed and simple representation of 391
the faults and, at the same time, enables the calculation simplic- 392
ity that is provided by the $dq0$ representation. Consequently, a 393
very precise model that is suitable to run online is achieved. In 394
addition, this model accounts for the effect of local saturation of 395
the magnetic circuit due to the fault currents. Local saturation 396
and saliency are taken into consideration through a modified 397
airgap function, which facilitates the accurate computation of 398
the inductance of the shorted turns. The model is extensively 399
validated by laboratory tests and compared with a model based 400
on the $dq0$ transform. The authors conclude that the proposed 401
model provides more accurate results than the $dq0$ model 402
although its performance with incipient faults needs to be 403
improved. 404

The work presented in [20] deals with the accurate local- 405
ization of field-winding to ground faults in SGs. First, the 406
authors analyze in detail a previously developed method for 407
the online detection of excitation-system faults to ground that 408
is valid for generators with static excitation. The method allows 409
discriminating if the fault takes place in the ac side or in the dc 410
side of the excitation system. In the event of faults in the dc 411
the method approximately forecasts the location of the fault in 412
the excitation winding. However, this procedure depends on the 413
value of the fault resistance R_f , which has to be estimated; this 414
fact leading to a wide margin of indetermination. The main 415
contribution of this work is a new algorithm that, from the 416
measured quantities, accurately calculates the value of the fault 417
resistance R_f . The method is validated through laboratory tests 418
and also on a 106-MW SG operating under real conditions in 419
a hydroelectric power plant. From the test results, the authors 420
claim that the proposed method for the computation of R_f 421
significantly reduces the errors in the fault location; this fact is 422
relevant in hydrogenerators with high number of poles, since it 423
reliably enables the location of the pole where the fault occurs. 424
This way, the extraction of the whole rotor can be avoided, thus 425
substantially reducing repair costs. 426

In [21], the authors introduce an approach for interturn short- 427
circuit diagnosis in five-phase PMSMs. The approach relies on 428
the spectral analysis of the modulus of a space vector \vec{D} . This 429
vector is obtained as a combination of two space vectors that 430
are calculated from the measured phase voltages but using two 431
different reference frames, named $\alpha\beta$ and $\alpha2\beta2$. It is justified 432
that an interturn fault in one of the stator phases produces an 433
increase in the DC and $2fs$ components in the spectrum of 434
the modulus of the space vector \vec{D} (fs : supply frequency 435
fundamental harmonic). It is shown from simulations and tests 436

437 that this signature is very sensible, reaching amplitude incre-
438 ments in the fault-related harmonics higher than 15 dB for
439 a fault affecting up to 3% of the turns of a phase; and it is
440 also clearly different from the signatures produced by other
441 kind of faults (as static or dynamic eccentricity and partial
442 demagnetization), thus enabling a robust and reliable diagnosis
443 of interturn short-circuit faults.

444 The work presented in [22], as in the previous paper, deals
445 with interturn short-circuit detection in PMSMs. In this case,
446 the work is focused on three-phase PMSMs working under
447 high variable load and speed conditions, as it happens in
448 aircraft applications. This work proposes an approach based on
449 parameter identification. The authors introduce a PMSM model
450 based on the dq reference frame, where the short-circuited turns
451 ratios of each phase ($n_{s/cA}, n_{s/cB}, n_{s/cC}$) are the parameters
452 to be identified. The estimation of these parameters is carried
453 out using the EKF, which is justified to be a suitable tool that
454 enables to perform accurate estimations in real time, even under
455 continuous and substantial changes in the operation conditions.
456 Finally, the fault indicators are defined as the average value
457 of the estimated short-circuited turns ratios calculated over a
458 sliding window with a length equal to half period of the main
459 component. The approach is extensively validated by simula-
460 tion and laboratory tests; it is demonstrated to be robust against
461 frequency variations, load variations, power factor variations,
462 load unbalances, and harmonic content variations.

463 Reference [23] is the only paper in this Special Section
464 dealing with axial flux PMSMs. In this paper, the authors
465 introduce a method for diagnosing static eccentricities in axial
466 flux PMSMs. The method requires the installation of three
467 search coils, mounted on three stator teeth shifted 120° . First,
468 a parameter named static eccentricity factor (SEF) is defined
469 in order to characterize the fault severity in such type of
470 machines; then, a simple algorithm is theoretically justified
471 that enables calculation of the SEF, and also the position of
472 minimum airgap in a faulty machine, using the measured back
473 electromotive forces in the search coils. It is interesting that
474 the computed SEF depends neither on the rotor speed nor on
475 the load. The approach is extensively validated via simulations,
476 using a 3-D finite-element software, as well as thorough labo-
477 ratory tests.

478 VI. ELECTRICAL DRIVES

479 In [24], a new fault detection and isolation technique is pre-
480 sented with the aim of making the traditional vector-controlled
481 IM drive fault tolerant against current and speed sensor failure.
482 The underlying idea is that the controller keeps estimating
483 the different currents and the speed and, in case of a fault, it
484 switches to the correct estimated value. On the one hand, the
485 proposed technique extracts eight estimates of currents in the
486 $\alpha - \beta$ reference frame (the authors obtain four estimates using
487 the reverse transformation from $d-q$ to $\alpha - \beta$ and the other
488 four using the forward transformation from $a-b-c$ to $\alpha - \beta$).
489 In this context, the concept of vector rotation is introduced to
490 decide the correct estimated value of current corresponding to a
491 fault. On the other hand, the speed is estimated by modifying
492 one of the available model reference adaptive system-based

formulations (X-based MRAS). Both simulations, as well as 493
494 experiments carried out with a laboratory prototype, demon- 494
495 strate that the system is capable of detecting a fault and recon- 495
496 figure itself in a seamless manner. In this regard, the authors 496
497 thoroughly evaluate the performance of the proposed algorithm 497
498 under different faulty conditions of the considered sensors. 498
499 The results prove that proposed technique works well even in 499
500 the case of multiple sensor failures and does not require any 500
501 additional sensor. The developed fault-tolerant controller can 501
502 be particularly useful for applications such as electric vehicles 502
503 to avoid complete shutdown of the system, in case of sensor 503
504 failure. 504

In [25], the detection of incipient faults in coupling inductors 505
506 used in three-phase adjustable-speed drives with direct power 506
507 control-based active front-end rectifiers is considered. More 507
508 specifically, the authors develop a new strategy for early fault 508
509 detection in coupling inductors, which enables a fast identi- 509
510 fication of the defective phase while providing an accurate 510
511 estimation of the inductance value of the coupling inductors that 511
512 enhances the performance of the direct power control method. 512
513 The underlying idea is that coupling inductor faults (e.g., an 513
514 interturn short circuit) lead to a variation in the value of the 514
515 coupling inductance. Hence, the goal is to detect the fault by 515
516 tracking estimations of the coupling inductances associated 516
517 with a fault in each phase. A detailed description of the full 517
518 estimation procedure is given in this paper. Both simulation 518
519 and experimental tests demonstrate the validity of the proposed 519
520 method. As stated in this paper, the detection of the fault 520
521 enables the suspension of the service if this is required to 521
522 avoid a major breakdown. In addition, the identification of the 522
523 affected phase enables the replacement of only the defective 523
524 inductor if three single-phase chokes are used or helps with 524
525 the repair of the nonhealthy winding if a three-phase reactor is 525
526 used. Among the claimed advantages of the proposed method 526
527 are the simplicity, speed, and effectiveness. On the other hand, 527
528 the main constraint relies on the manufacturing tolerance of 528
529 the inductors, which makes their actual values differ from 529
530 each other including when there are not any faults. This latter 530
531 issue, however, does not affect the robustness of the presented 531
532 strategy. 532

In [26], an observer-based fault detection method is designed 533
534 for the rotor position sensor of PMSM drives in an elec- 534
535 tromechanical brake (EMB). To this end, the authors develop 535
536 a position estimation algorithm with a full-order Luenberger 536
537 observer for the rotor flux linkage. However, there are some 537
538 deviations between the observer and the real process caused by 538
539 model uncertainties and parameter variations. To overcome this 539
540 drawback, the authors add a crucial feature in their detection 540
541 method that relies on an adaptive threshold; this is determined 541
542 by analyzing position estimation errors of the observer. The 542
543 adaptive threshold enables, among other things, avoidance of 543
544 missing or false alarms. The experimental results using the 544
545 EMB test bench prove the effectiveness and robustness of the 545
546 designed method that can even detect a small amount of phase 546
547 shift fault within a wide operation range, not only at steady state 547
548 but also under transient operation. Moreover, the fault-tolerance 548
549 capability of the proposed method is achieved by introducing a 549
550 compensation algorithm for the phase shift. The experimental 550

551 results show that this compensation algorithm is useful for
 552 tolerating the phase shift fault. For other types of rotor position
 553 sensor faults, the authors propose potential solutions that can
 554 overcome low-speed limitation issues, such as the incorporation
 555 with a high-frequency injection-based method. This latter ap-
 556 proach can be somehow complementary to that proposed in the
 557 work, since each of them shows special suitability for different
 558 speed ranges.

559 VII. POWER COMPONENTS AND POWER CONVERTERS

560 In [27], an adaptive threshold-based approach is also pre-
 561 sented, but in this case it is to design an electronic failure detec-
 562 tion system applied to the IGBT. More specifically, the method
 563 proposed by the authors relies on the direct measurement of
 564 behavior of the gate signal during the IGBT turn-on transient
 565 via continuous processing using analog and digital electronics.
 566 The main goal pursued with an early fault detection design in
 567 the IGBT is to obtain a corrective action to prevent propagation
 568 of the fault to the complementary device in the same affected
 569 leg in the inverter-motor system, when a short circuit or an
 570 overcurrent occurs. Two different faults are considered in the
 571 work: open-circuit and short-circuit failures. The considered
 572 stages of the developed diagnosis scheme are improved resid-
 573 ual generation stage, ramp rate, and a symmetrical adaptable
 574 thresholds stage. The final scheme is intended to decrease the
 575 false alarm rate by the aforementioned failures. To achieve the
 576 early fault detection, the proposed circuit is implemented in
 577 the gate driver using analog electronics. As the authors point
 578 out, the main advantage of adding detection process with adap-
 579 tive threshold is that the false alarm rate decreases because the
 580 system is not so vulnerable to variations in the power supply
 581 of the IGBT gate driver circuit. On the other hand, the main
 582 limitation is that the proposed design is not suitable for power
 583 applications, where the switching frequency is above 20 kHz
 584 since the introduction of an external resistance limits the IGBT
 585 switching speed.

586 In [28], a methodology to analyze the losses in the converters
 587 of fault-tolerant drives is presented. This work aims to evaluate
 588 the losses in the power components of the converter (IGBT,
 589 diodes, capacitors) during the time the fault takes place, during
 590 the subsequent reconfiguration process and, finally, during the
 591 operation in faulty mode; the objective is to assess whether the
 592 drive components are able to withstand the thermal stresses that
 593 produce transient currents during the fault and reconfiguration
 594 period; and also assess the possible reduction in the rated power
 595 of the converter when operating in faulty mode. The authors
 596 perform the analysis on a single but actual topology of a fault-
 597 tolerant inverter and develop a simple model to assess the
 598 losses in all the components after an IGBT open-circuit fault
 599 event, both during the fault, reconfiguration process, and faulty
 600 operation. The model was validated experimentally by compar-
 601 ing the sum of computed losses and the total losses measured
 602 in the experimental rig. From the analysis, conclusions about
 603 the maximum allowable time in faulty and reconfiguration
 604 conditions or the maximum power after the reconfiguration are
 605 discussed.

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