

REVIEW

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# Modern improvement techniques of direct torque control for induction motor drives - a review

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## Abstract

Conventional direct torque control (DTC) is one of the excellent control strategies available to control the torque of the induction machine (IM). However, the low switching frequency of the DTC causes high ripples in the flux and torque that leads to an acoustic noise which degrades the control performances, especially at low speeds. Many direct torque control techniques were appeared to remedy these problems by focusing specifically on the torque and flux. In this paper, a state of the art review of various modern techniques for improving the performance of DTC control is presented. The objective is to make a critical analysis of these methods in terms of ripples reduction, tracking speed, switching loss, algorithm complexity and parameter sensitivity. Further, it is envisaged that the information presented in this review paper will be a valuable gathering of information for academic and industrial researchers.

**Keywords:** Induction machine, Direct torque Control (DTC), Fuzzy logic (FL), Neural network (NN), Sliding mode (SG), Genetic algorithm (GA)

## 1 Introduction

In industry, more than half of the total electrical energy produced is consumed by electric motors [1]. Among several types of electric motors, three-phase induction machines (IMs) occupy a prominent place. Indeed, at least 80% of industrial control systems use induction motors [2], which have gradually taken the place of DC machines because of their good performance: reliability, simple construction, low cost and simple maintenance [3, 4]. However, these numerous advantages are not without inconvenience, the dynamic behavior of the machine is often very complex [5, 6], since its modeling results in a system of nonlinear equations, strongly coupled and multivariable. In addition, some of its state variables, such as flux, are not measurable [7]. These constraints require more advanced control algorithms to control the torque and flux of these machines in real time [8]. For several

years, academic and industrial research has been carried out to remedy the control problem of the IM and to develop robust and efficient controls [9].

In this context, scalar control is the first technique that has been developed to control electrical machines, this control strategy consists of keeping the  $V/f$  constant to keep the flux in the machine constant [10, 11]. It is characterized by its simplicity of implementation, its simple structure, which is based on the stator flux control [12]. However, on a start-up or for change the rotation direction of the machine, the flux oscillates strongly with large amplitudes and its modulus is variable during the transient states [13, 14]. These oscillations will impact the quality of the torque and the speed, thus degrading the performances in transient state of the machine. This type of control is therefore used only for applications where the speed variation is not great, such as in pumping or ventilation [15, 16].

Subsequently, the Field Oriented Control (FOC) method was developed to control transient torque [5]. This control provides a behavior of the IM similar to that of the DC machine with a decoupling between the

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torque and the flux of the machine [17–19], this decoupling provides a very fast torque response, a large speed control range and high efficiency for a wide load range. However, this control also has a high sensitivity to the parametric variations of the machine especially that of the resistors whose value changes substantially with temperature [20–22]. Any difference between the parameters used by the FOC algorithm and the actual parameters of the machine is translated by errors in the output values of the flux and the torque, which leads to increased losses in the machine and reduced performance of the system to be controlled [23].

In the middle of 1980s, Direct Torque Control (DTC) was introduced to compete with conventional controls. This technique was introduced by TAKAHASHI [24] and DEPENDBROCK [25]. It has remarkable dynamic performance as well as good robustness with respect to the variations of the parameters of the machine. Its principle is based on a direct determination of the control pulses applied to the switches of the voltage inverter [26–28]. However, two major drawbacks arise: (i) the switching frequency is highly variable and (ii) the undulations amplitude of the torque and the stator flux remain poorly controlled throughout the speed range of the envisaged operation [29–31]. It should be mentioned that the ripples in the torque generate additional noise and vibrations and therefore cause disturbances in the rotating shaft [32].

Currently, a lot of research has tried to solve these problems. The Artificial Intelligence (AI) control is a vocabulary that has emerged in recent years and occupies a large place in modern research fields. Fuzzy logic, neural networks and genetic algorithms are the major families that constitute AI. In [29, 33], the authors propose AI techniques to improve the dynamic performance of the DTC control, these control methods can provide performance optimization under different operating conditions aiming ripples reduction of the torque and flux, THD reduction, efficiency improvement, energy savings and etc.

From published literature, different works considering DTC schemes for induction motor drives, but these schemes are not reviewed critically. Our contribution of this work is to review different modern techniques for improving the performance of direct torque control; the aim is to give an idea to researchers who are interested in the current state of the art of DTC strategy and work on new lines of research.

This review paper is organized as follows: Section 2 presents the three-phase mathematical model of the IM and its transformation in the two-phase system. A representation in the form of a state is developed from the physical laws that govern its operation by supplying the machine with voltage. Section 3 discusses the classical DTC technique based on the switch table and hysteresis

controllers and the main problems encountered during this control strategy. Section 4 discusses some techniques for improving conventional DTC, briefly recalling some typical techniques and dealing with modern techniques based on artificial intelligence. Section 5 presents a comparative study between the improvement methods presented, a table summarizing the comparison is presented at the end of this article which aims to help in the choice of the appropriate command for the specific application given, and Section 6 summarizes the conclusions of the paper.

## 2 Dynamic model of induction machine

The most appropriate model to study the dynamic behavior and control algorithms design of the three-phase IM is the two-phase model expressed by the reference  $(\alpha, \beta)$  [34, 35]. This model reduces the complexity of the three-phase representation (a, b, c) of the machine.

The electromagnetic equations of the induction machine in the reference frame  $(\alpha, \beta)$  are given by [36, 37]:

$$\frac{d}{dt} \begin{bmatrix} i_{s\alpha} \\ i_{s\beta} \\ \psi_{s\alpha} \\ \psi_{s\beta} \end{bmatrix} = \begin{bmatrix} -\frac{1}{\sigma} \left( \frac{1}{\tau_s} + \frac{1}{\tau_r} \right) & -\frac{\omega_r}{\sigma} \left( \frac{1}{\tau_s} + \frac{1}{\tau_r} \right) & \frac{1}{\sigma L_s \tau_r} & \frac{\omega_r}{\sigma L_s} \\ \frac{\omega_r}{\sigma} \left( \frac{1}{\tau_s} + \frac{1}{\tau_r} \right) & -\frac{1}{\sigma} \left( \frac{1}{\tau_s} + \frac{1}{\tau_r} \right) & -\frac{\omega_r}{\sigma L_s} & \frac{1}{\sigma L_s \tau_r} \\ 0 & -R_s & 0 & 0 \\ 0 & R_s & 0 & 0 \end{bmatrix} \begin{bmatrix} i_{s\alpha} \\ i_{s\beta} \\ \psi_{s\alpha} \\ \psi_{s\beta} \end{bmatrix} + \begin{bmatrix} \frac{1}{\sigma L_s} & 0 \\ 0 & \frac{1}{\sigma L_s} \\ 1 & 0 \\ 0 & 1 \end{bmatrix} \cdot \begin{bmatrix} V_{s\alpha} \\ V_{s\beta} \end{bmatrix} \quad (1)$$

With  $\sigma$ ,  $\tau_s$  and  $\tau_r$  are positive constants defined as:

$$\sigma = 1 - \frac{M^2}{L_s L_r} \quad \tau_s = \frac{R_s}{L_s} \quad \tau_r = \frac{R_r}{L_r}$$

The equations of electromagnetic torque and the movement are given by the following expressions:

$$T_{em} = p \left( \psi_{s\alpha} i_{s\beta} - \psi_{s\beta} i_{s\alpha} \right) \quad (2)$$

$$J \cdot \frac{d\Omega}{dt} + f \cdot \Omega = T_{em} - T_r \quad (3)$$

The passage of a three-phase reference (a, b, c) towards a two-phase reference  $(\alpha, \beta)$  can be achieved by the transformation called Concordia [38], this transformation is given by:

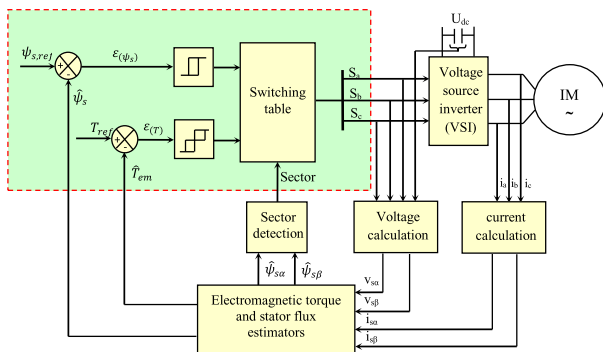
$$\begin{bmatrix} X_\alpha \\ X_\beta \end{bmatrix} = \sqrt{\frac{2}{3}} \cdot \begin{bmatrix} 1 & -\frac{1}{2} & -\frac{1}{2} \\ 0 & \frac{\sqrt{3}}{2} & -\frac{\sqrt{3}}{2} \end{bmatrix} \cdot \begin{bmatrix} X_a \\ X_b \\ X_c \end{bmatrix} \quad (4)$$

With: X can be a current, voltage or the flux of the machine.

### 3 Direct torque control

The direct torque control (DTC) for induction machines was proposed in the middle of 1980s by Takahashi [24] and Depenbrock [25]. Comparing to the vector control, it is less sensitive to parametric variations of the machine [18, 39], its control algorithm is simple because of the absence of pulse width modulation (PWM), of Current Controllers and Park Transformations [40, 41]. It does not use PI regulation loops, which should improve its dynamic skills a priori and eliminate the problems related to the saturation of PI regulators. DTC control ensures high efficiency operation and provides accurate and fast torque dynamics. The principle of DTC is based on the direct application of a control sequence to the switches of the voltage inverter (switching states) placed upstream of the machine [42–45]. The choice of this sequence is made by the use of a switching table and two hysteresis regulators whose role is to control and regulate the electromagnetic torque and the flux of the machine in a decoupled manner. Fig. 1 shows a simple structure of the DTC control. The electromagnetic torque is controlled using a three level hysteresis comparator. While the stator flux is controlled using a two level hysteresis comparator. The outputs of these comparators, as well as the flux vector information, are used to determine the switching table.

In DTC, the accuracy of electromagnetic torque and stator flux estimation is very important to ensure satisfactory performance [34, 46]. So, several parameters must be determined, the stator current is measured while the stator voltage depends on the switching state ( $S_a$ ,  $S_b$  and  $S_c$ ) produced by the switching table and the DC link voltage  $U_{dc}$  [47]. These parameters are transformed into coordinates  $(\alpha, \beta)$ , by the Concordia transformation Eq. (4), which are suitably adapted to the DTC algorithm.



**Fig. 1** Synoptic schema of DTC control of the induction machine

The stator flux  $\psi_s$  and the electromagnetic torque  $T_{em}$  are estimated from the following equations:

$$\hat{\psi}_s = \sqrt{\hat{\psi}_{s\alpha}^2 + \hat{\psi}_{s\beta}^2} \tag{5}$$

$$T_{em} = p \cdot (\hat{\psi}_{s\alpha} \cdot i_{s\beta} - \hat{\psi}_{s\beta} \cdot i_{s\alpha}) \tag{6}$$

The angle  $\theta_s$  is calculated from:

$$\theta_s = \arctg\left(\frac{\hat{\psi}_{s\beta}}{\hat{\psi}_{s\alpha}}\right) \tag{7}$$

With the stator flux components in the reference ( $\alpha, \beta$ ) are:

$$\begin{cases} \hat{\psi}_{s\alpha} = \int_0^t (v_{s\alpha} - R_s \cdot i_{s\alpha}) \cdot dt \\ \hat{\psi}_{s\beta} = \int_0^t (v_{s\beta} - R_s \cdot i_{s\beta}) \cdot dt \end{cases} \tag{8}$$

Then, the estimated values of the electromagnetic torque  $T_{est}$  and the stator flux  $\psi_{est}$  are compared respectively to their reference values  $T_{em}^*$  and  $\psi_{s}^*$ , the results of the comparison form the inputs of the hysteresis comparators [48]. The selection of the appropriate voltage vector is based on the control table [10] (Table 1). The inputs of this table are the flux sector number and the outputs of the two hysteresis comparators.

Despite its simplicity, robustness and speed, the DTC control has major disadvantages. The use of hysteresis controllers causes high ripples in the flux and electromagnetic torque that generate mechanical vibrations and undesirable acoustic noise, and therefore, a deterioration of the machine performances [34, 49], thus a variable switching frequency and current distortions that can degrade the quality of the output power [50, 51]. The negligence of stator resistance causes problems at low speed. In addition, the practical implementation of non-linear elements of the hysteresis type requires a rather low sampling period, and therefore a high calculation frequency leading to constraining architectures [52].

In recent years, many direct control strategies have emerged to overcome the problems of conventional DTC. These strategies are based on the same principle of instantaneous torque and stator flux regulation and the direct determination of the inverter control signals from a switching table. Generally, these control methods can be divided into two categories: typical and modern techniques. These include: Vector Spatial Modulation (SVM) [53], sliding mode based DTC, model predictive DTC and artificial intelligence (fuzzy logic, neural network and genetic algorithm) [54, 55]. Fig. 2 illustrates a

**Table 1** Switching table

Sector		1	2	3	4	5	6
1	$H_s$	1	2	3	4	5	6
	$H_{rem}$	1	2	3	4	5	6
	Voltage vector	$v_2$	$v_3$	$v_4$	$v_5$	$v_6$	$v_1$
0	$H_s$	1	2	3	4	5	6
	$H_{rem}$	0	0	0	0	0	0
	Voltage vector	$v_7$	$v_0$	$v_7$	$v_0$	$v_7$	$v_0$
-1	$H_s$	1	2	3	4	5	6
	$H_{rem}$	-1	-1	-1	-1	-1	-1
	Voltage vector	$v_6$	$v_1$	$v_2$	$v_3$	$v_4$	$v_5$
0	$H_s$	1	2	3	4	5	6
	$H_{rem}$	0	0	0	0	0	0
	Voltage vector	$v_3$	$v_4$	$v_5$	$v_6$	$v_1$	$v_2$
-1	$H_s$	1	2	3	4	5	6
	$H_{rem}$	-1	-1	-1	-1	-1	-1
	Voltage vector	$v_0$	$v_7$	$v_0$	$v_7$	$v_0$	$v_7$
-1	$H_s$	1	2	3	4	5	6
	$H_{rem}$	-1	-1	-1	-1	-1	-1
	Voltage vector	$v_5$	$v_6$	$v_1$	$v_2$	$v_3$	$v_4$

classification of the methods used to improve the DTC control of an induction machine.

**4 Improvement techniques of direct torque control**

**4.1 Typical improvement techniques of direct torque control**

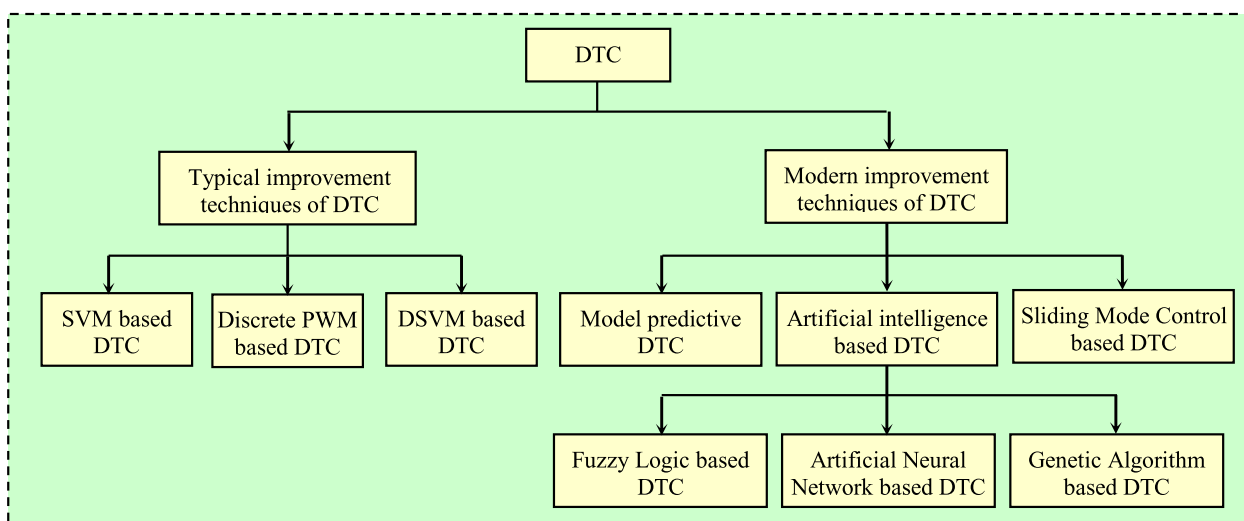
Several authors have used the Space Vector Modulation (SVM) technique in controlling the voltage inverter to improve DTC [56–58]. The principle of this technique consists in imposing the appropriate vector of tension via a vector modulation of space, in order to proceed to a predictive regulation of the torque and the flux. The control algorithm for this method is more complex, but flux and torque oscillations are reduced and the average switching frequency of the inverter became constant [59]. Like any predictive method, the DTC-SVM has some static torque error for control without a speed loop during a practical implementation. Indeed, this error is due to the computation time necessary for the prediction of the control voltage.

The authors of [56] have developed a method that makes it possible to obtain a constant switching

frequency. This strategy is characterized by the elimination of the Takahashi selection table and the hysteresis comparators. In this context, the PWM technique is used to generate the output vector of the control. The objective of this strategy is to realize a direct control of the stator flux vector in a frame  $(\alpha, \beta)$  linked to the stator. The projection components of the desired stator voltage vector on the two adjacent voltage vectors of the frame  $(\alpha, \beta)$  allow the calculation of the desired switching times.

In [60, 61], a method of direct torque control of the IM based on pulse width modulation (PWM) has been proposed to have a constant switching frequency. The proposed control technique is developed in discrete time to allow the implementation on microcontrollers or DSP boards. The authors use simulations and experimental tests to validate the proposed method. In [62, 63], the authors showed that the conventional DTC has a low number of voltage vectors applied to the machine, which causes undesirable oscillations of the torque, flux and current. This work shows that improved performance can be achieved by using a new DTC algorithm, based on the application of SVM for fixed time intervals. In this way, a Discrete Space Vector Modulation (DSVM) using a five-levels torque comparator to produce a higher voltage vector number. Numerical simulations and experimental tests show improved torque and flux response with fixed switching frequency.

Some authors adapted the DTC to the control of machines powered by inverters of multilevel voltage types [64], indeed, the higher number of control vectors promotes a minimization of the resulting ripple in steady state. In [64, 65] a three-level inverter is applied to the DTC, for the reduction of the torque ripples, but the disadvantage of this arrangement is the



**Fig. 2** Classification of improvement techniques of direct torque control

high cost. They are very useful, especially in high power controls.

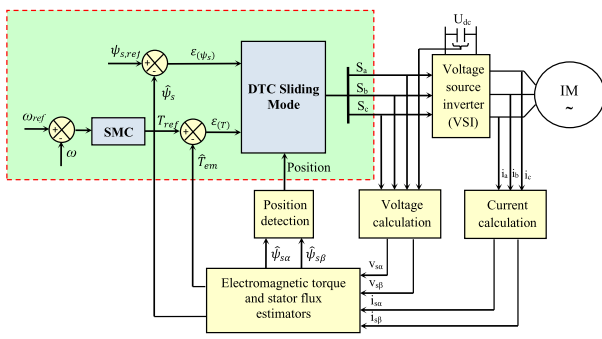
**4.2 Modern improvement techniques of direct torque control**

**4.2.1 Sliding mode based DTC**

Sliding Mode Control (SMC) is a class of the Variable Structure Control (VSC) introduced by Utkin [66], it is mostly known for its robustness towards internal uncertainties (variations of machine parameters), external uncertainties (perturbation due to the load), and phenomena that have been omitted in the modeling [67, 68]. The main characteristic of SMC is manifested in the modified control law in a discontinuous manner [69]. However, it has certain drawbacks: the appearance of the chattering phenomenon caused by the discontinuous part of the control which can have a detrimental effect on the machines [70], at every moment, the system is subject to high control in order to ensure its convergence to the desired and this is not desirable.

The SMC technique was studied to improve DTC for IMs [68, 71, 72]. These techniques improve the steady-state performance and keep advantages of transient state [73]. In [68, 73] the authors begin to use a discrete time sliding mode control strategy so that the torque and flux are robust against the variation of the machine parameters. The controllers supply the reference voltages ( $V_{sa}, V_{sb}$ ) for application to the IM and no controller current is used. However, unlike most sliding mode techniques, the reference voltage vector is calculated by a PWM vector system and a fixed switching frequency is used. Simulations and experimental results are presented to show the effectiveness of the proposed strategy.

Fig. 3 illustrates the general scheme of the direct torque control structure and the flux based on the sliding mode of an induction machine (DTC-SMC) controlled in speed. It is a cascade command for the control of the electromagnetic torque, the square norm of the flux and the speed. So there are sliding regimes control algorithms to implement in the control structure for adjusting the



**Fig. 3** Synoptic schema of DTC-SMC control of the induction machine

torque, flux and speed. The “estimator” block consists of the flux and torque estimator which only uses the measurement of voltages and stator currents in the reference ( $\alpha, \beta$ ). This control scheme is fast and robust. However the controlled magnitude presents undesirable chattering.

Other works used the robust sliding mode observer [74] to make the flux estimation less sensitive to the measurement noise.

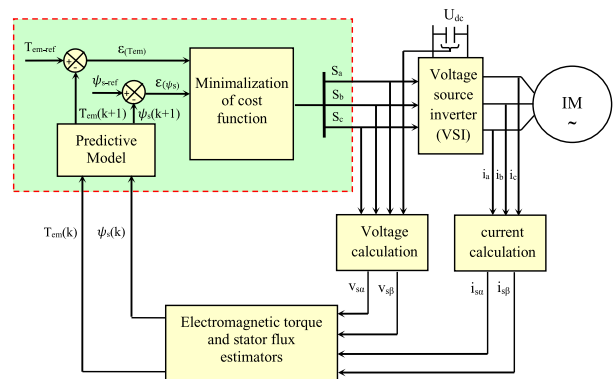
**4.2.2 Model predictive DTC**

Predictive control is an advanced control technique of the automatic. Its objective is to control complex industrial systems. The principle of this technique is based on the calculation of the future behavior of the system based on the dynamic model of the process inside the real-time controller, in order to be able to use this information to calculate the optimal values of the adjustment parameters [75]. The application of the model predictive control (MPC) in the field of digital controls has yielded good results in terms of speed and accuracy [76].

Recently, the predictive control strategy for DTC has received considerable attention, particularly because of its ability to minimize the switching frequency of the voltage inverter that supplies the machine and to reduce torque and flux ripples. In DTC-MPC, the traditional DTC switching table is replaced by an online optimization algorithm [77–79]. The principle of vector selection in predictive control is based on the evaluation of a defined cost function [80, 81]. The predictive model with stator flux, torque and angular velocity is used to predict the future behavior of the controlled variables. The simplified diagram of DTC-MPC is illustrated in Fig. 4.

The execution of the predictive algorithm can be performed in three main steps:

- The estimation of non-measurable variables.
- The prediction of the future behavior of the system.
- The optimization of the control outputs, according to a cost function already defined before.



**Fig. 4** Block diagram of the DTC-MPC

These steps are repeated at each sampling time step, taking into account the new measurements. Closed-loop control is obtained by feedback from measurements used to predict and decide on measures taken to reduce the value of the cost function  $F$ . Fig. 5 shows the flowchart of the DTC-MPC.

Predictive control has many advantages, the MPC concept is very simple and intuitive, easy to achieve, the constraints and nonlinearities of the systems to be controlled can be included in the control and the case of multi-variable systems can be taken into consideration [34]. However, this type of control requires a lot of on-line calculation compared to conventional DTC.

In [82, 83], a predictive control strategy based on the optimization of a cost function defined on a horizon has been presented, to guarantee the rejection of disturbances and improve robustness to parameter variations and make

the system more efficient. Also, in [45, 77–81, 84] the authors propose a technique to improve the dynamic performance of the DTC using predictive control, they have been shown that DTC-MPC provides better performance in terms of dynamics judged fast, reduction of torque and flux ripples and improvement of current shape.

#### 4.2.3 Artificial intelligence based direct torque control

Recently, another category of control based on artificial intelligence is presented in the literature. These methods improve the dynamic performance of the DTC control, either by adapting the hysteresis band [85, 86], or by replacing the Takahashi switching table as well as the hysteresis by intelligent regulators [87–92]. Artificial intelligence such as fuzzy logic, the neural network and the genetic algorithm knew a big success not only in modeling but also in the control of electrical systems, in particular the control of IM. This success is due to the fact that artificial intelligence can easily get close to the control behavior of the human expert who works in often poorly defined environments. Therefore, in this section we will deal with the different artificial intelligence approaches introduced to the DTC control.

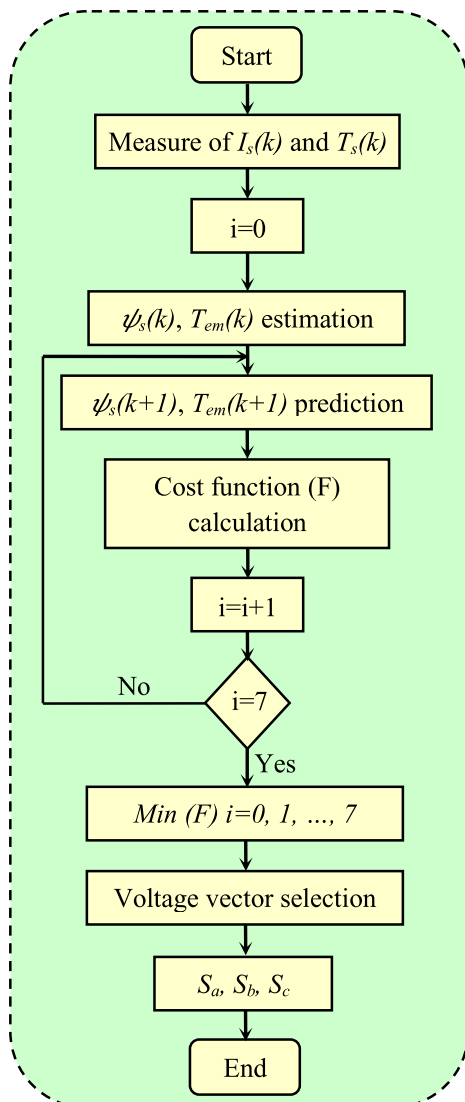
##### 4.2.3.1 Fuzzy logic based DTC

Fuzzy logic, or more generally the treatment of uncertainties, is one of the classes of artificial intelligence [93], it is introduced to improve the performances of the different classical control strategies applied to variable speed drives.

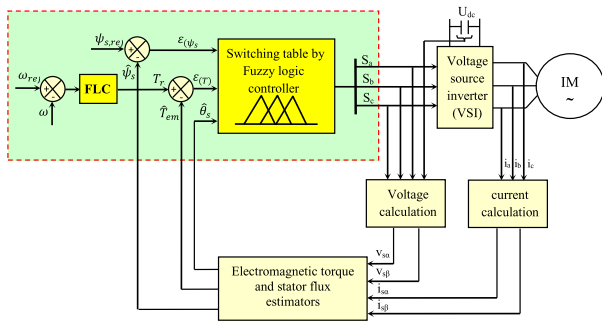
In [94, 95], the authors propose the Fuzzy Direct Torque Control (FDTC) method to improve the dynamic performance of conventional DTC control. They develop a new selection table based on a fuzzy logic controller (FLC) to replace the switching table and the hysteresis comparators, in order to generate the vector voltage that drives the flux and torque to their references in an optimal way. Fig. 6 shows a general structure of the FDTC command applied to the induction machine.

The inputs of the fuzzy switching table are the stator flux error, the electromagnetic torque error and the stator flux vector position, while the outputs are the switching states of the inverter arms ( $S_a$ ,  $S_b$ ,  $S_c$ ) [96–98]. Each input and output is divided into a determined number of fuzzy sets so as to have better control using the minimum of rules.

The inference rules are written in such a way that the differences between the flux and torque set-points and their estimated values can be corrected. Six linguistic variables are used to represent the domain of the angle of the stator flux vector. Three linguistic variables (N: negative, Z: zero and P: positive) are used to fuzzify the speech universe of  $\varepsilon_{T_{em}}$ . And two linguistic variables (N: negative and P: positive) are used to fuzzify the speech universe of  $\varepsilon_{\psi}$ . The discourse universe of each output is



**Fig. 5** Flowchart of the DTC-MPC

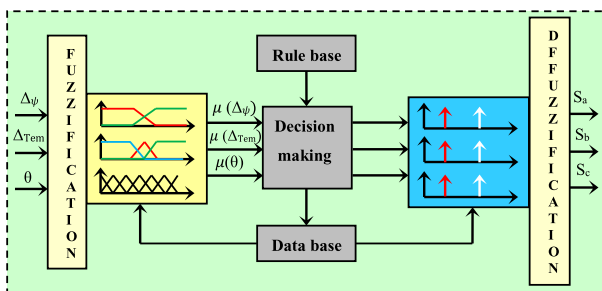


**Fig. 6** Synoptic schema of DTC-Fuzzy control of the induction machine

divided into two fuzzy sets (zero and one). The membership functions adopted for making the fuzzy table and the inference rules are shown in Fig. 7.

In [87], the authors proposed a DTC strategy based on fuzzy logic. The objective of the work is to improve the performance of the DTC control while minimizing the torque at low speeds. They have integrated a fuzzy speed regulator which makes it possible to dynamically adjust the integration coefficient  $k_i$  and the coefficient of proportionality  $k_p$  as a function of the error and of the variations of the speed. In addition, the flux and torque hysteresis are replaced by a fuzzy controller to optimize the selection of the voltage vector. The experimental results show that the proposed fuzzy control system can provide a fast response and a high precision of the steady state speed, as well as the remarkable reduction of torque ripples even at low speeds.

Besides, fuzzy logic is used to control the limits of the electromagnetic torque hysteresis band [99], what entails a minimization of the torque undulations as well as an improvement of the dynamic performances. In the same context, Uddin Nasir et al. [86] proposed a fuzzy controller to adjust the hysteresis band in real time. This adjustment is based on the slopes of the variation of the estimated torque and the stator current, where the fuzzy controller selects the optimum bandwidth of the torque hysteresis. The simulation results from a model developed under Matlab/Simulink, as well as the experimental



**Fig. 7** Structure of the fuzzy switching table

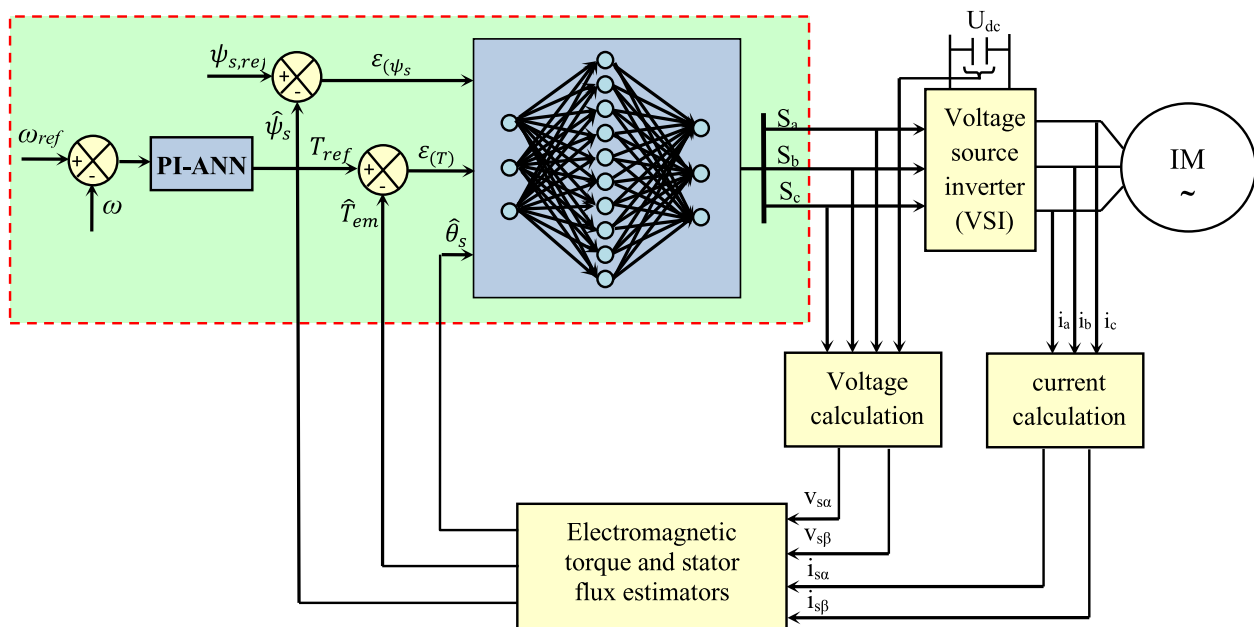
results realized with a DSP board prove the performances obtained by this fuzzy controller. A comparative study between the DTC based on the proposed fuzzy controller and the conventional DTC shows that the torque ripple of the proposed control was considerably reduced.

In [100], fuzzy logic strategy is used to study the effect of parametric variation on DTC performance through the use of control tables developed by fuzzy logic reasoning. The validity of the proposed method has been proven by the simulation results. Fuzzy logic can cope with parameter uncertainties. However, the main problems of this technique are the difficult tuning of fuzzy logic parameters and the complexity of implementation; because fuzzy controller uses many rules base do the extensive experiments.

#### 4.2.3.2 Neural network based DTC

The Artificial Neural Network (ANN) is widely used in many fields of technology application and scientific research. This technique can be used in cases of difficult problems that cannot be described by precise mathematical approaches where they are very complicated to manipulate [101]. The fields of application of these neural networks are very broad: classification, image and speech processing, estimation, process identification [102, 103] and control of electrical systems [104, 105]. In [106], the authors integrated artificial neural networks into the control of an induction machine; they mentioned that in some cases, where the dynamics of the system change over time and/ or with operating conditions, the efficiency of the PI regulator deteriorates and the quality of the adjustment deteriorates. To overcome these problems and to ensure a good performance of the command, the authors have integrated artificial neural networks in the speed control. Several tests have been simulated to assess the contribution of ANN. The results obtained make it possible to affirm an improvement of the performances and robustness in the control of the IM.

Several studies have suggested the application of the ANN technique to select the states of the voltage inverter switches used to power the DTC-controlled IM [107–112]. The idea is always to replace the conventional switching table that determine the inverter states by neural selector capable of managing control signals in the same way. Fig. 8 shows the block diagram of Direct Torque Neural Control (DTNC). The architecture includes a multilayer neural network allowing replacing both hysteresis comparators and the selection table. This neural network is composed of an input layer, two hidden layers and an output layer. The input layer is composed of three neurons, designated respectively by the torque error, the flux error and the angular position ( $\theta$ ) of the stator flux vector. The two hidden layers each consist of ten neurons. The output layer consists of three neurons that



**Fig. 8** Synoptic schema of DTC-ANN control of the induction machine

produce the reference voltage to be applied across the IM through the voltage inverter.

The application of neural networks to DTC ensures a good dynamic response of torque and flux with fixed switching frequency, which leads to a considerable reduction in torque ripples and the harmonic rate of the currents compared to other conventional techniques [107]. Moreover, it is very robust against the various uncertainties of the motor parameters [111]. However, this proposed technique has the disadvantage of the internal structure that is more complicated.

#### 4.2.3.3 Genetic algorithm based DTC

Genetic Algorithms (GAs) represent a fairly rich and interesting family of stochastic optimization algorithms that are based on techniques derived from natural evolution and genetics [113]. The principle of these algorithms is to proceed by a stochastic search on a large space and through a population of pseudo-solutions [114]. The robustness against parametric variations is one of the main features of genetic algorithms; they allow to supply one or several good quality solutions to problems highly varied, by requesting a rather low investment (time and computing power) [115]. However, it has the disadvantage of parameters selection, because the choice of these parameters depends strongly on the studied problematic and the knowledge of the user regarding this problem.

Recently, the genetic algorithm is used to improve the dynamic performance of the DTC control; it is well adapted to optimize the gain values of the speed controller [116, 117].

In [116], the optimization technique (GA) has been applied to DTC, the authors use a PI regulator optimized by the genetic algorithm (PI-GA), This method showed better performance compared to conventional DTC in both transient and stable states, of which many advantages have been confirmed, related to torque and flux ripples, reduction of overshoot and response time.

In [118], the authors proposed a new DTC strategy, using a genetic algorithm to optimize the PI-fuzzy regulator. In this strategy, as a function of the speed error and its derivative with respect to time, the adjustment of the integral coefficient  $k_i$  and proportional  $k_p$  is realized in real time by an adaptive regulator PI-fuzzy of speed. The fuzzy parameters are refined by the genetic algorithm to improve the self-adaptation of the speed. In addition, the hysteresis regulators have been replaced by another fuzzy regulator to improve the choice of the voltage vector. Finally, the author presented a comparative study between Takahashi's conventional DTC, PI-fuzzy regulator and the proposed strategy. This study proved the significant decrease of the ripples at the torque level, flux, and current. As well as improving accuracy and speed tracking.

## 5 Critical analysis

Table 2 presents a critical analysis of the proposed methods for improving the performance of direct torque control in an induction machine. This analysis aims to highlight an idea for researchers who are interested in the DTC technique. The evaluation of these methods is



**Table 2** Critical analysis of the improvement techniques of direct torque control [29, 34, 53–55, 73, 116, 118–121]

	Conventional DTC	SVM based DTC	SMC based DTC	DTC-MPC	Fuzzy based DTC	ANN based DTC	GA based DTC
Torque dynamic response	Fast	Fast	Fast	Fast	Very fast	Very fast	Very fast
Torque and flux ripple	High	Low	Medium	Low	Very low	Very low	Medium
Current THD	More distortions	Less distortion	Less distortion	Less distortion	Less distortion	Less distortion	Less distortion
Switching frequency	Variable	Constant	Almost constant	Constant	Constant	Constant	Almost constant
Parameter sensitivity	Insensitive	Sensitive	Insensitive	Insensitive	Insensitive	Insensitive	Insensitive
Switching loss	High	Low	Medium	Low	Low	Low	Medium
Dynamic at low speed	Poor	Good	Good	Good	Very good	Very good	Very good
Algorithm complexity	Simple	Simple	Complex	Simple	More complex	More complex	Complex
Computation time	Low	Medium	High	Medium	High	High	Medium
Precession	Low	Medium	Medium	Medium	High	High	Medium
Regulation	Hysteresis	PI conventional	SMC controller	Hysteresis	FLC	ANN	GA-PI

carried out in terms torque and flux ripple, switching frequency, parameter sensitivity, steady-state and dynamic response and algorithm complexity. It should be mentioned that evaluation does not have a totally absolute meaning, because it is very difficult to find several works made under the same conditions and on the same type of machine, but the basic disadvantages and advantages must be the same for each control technique.

From this study, it can be said that conventional DTC presents the simplest structure among the other control strategies with a low switching frequency which is the major problem of DTC. In order to overcome these problems and obtain a sufficiently low torque ripple, the sampling frequency must necessarily be high. Artificial intelligence techniques and the predictive model of DTC can achieve lower torque ripple and switching frequency than that of the direct torque control under the same sampling frequency, but the complexity of AI methods is substantially elevated. Therefore, it can be employed for high precision control in high power applications. Moreover, SVM and SMC methods can be solutions to improve DTC, but they have limitations such as sensitivity and chattering phenomenon.

The preferred approach to solve the complexity problem is to simplify the control algorithm without increasing the calculation capacity of the microprocessor. On the other hand, it is possible to improve the performance of the DTC drive and to obtain a low-cost system, by developing a hybrid control strategy by combining two or more modern techniques.

## 6 Conclusion

In this paper, several modern improvement techniques of direct torque control for an induction motor are reviewed. The objective of this improvement is to minimize the ripples of the couple and the flux of the IM on the one hand and the decrease of the switching

frequency of the inverter on the other hand. A classification and comparison of these strategies in terms of ripples reduction, tracking speed, switching loss, algorithm complexity and parameter sensitivity are presented. It is very difficult to conclude which is the best solution to improve the DTC performance. The choice of method depends on the application, cost, hardware availability, reliability and accuracy of the system. This review is expected to provide a very beneficial tool to all the industries and researchers working on electrical machine controls.

## 7 Nomenclatures

$v_{s(\alpha,\beta)}, v_{r(\alpha,\beta)}$ :  $\alpha\beta$  components of the stator and rotor voltages

$i_{s(\alpha,\beta)}, i_{r(\alpha,\beta)}$ :  $\alpha\beta$  components of the stator and rotor currents

$\psi_{s(\alpha,\beta)}, \psi_{r(\alpha,\beta)}$ :  $\alpha\beta$  components of the stator and rotor flux

$S_1, S_2, S_3$ : Switching states

$R_s, R_r$ : Stator and rotor resistances

$L_s, L_r$ : Stator and rotor Inductances

$M$ : Mutual inductance

$\tau_s, \tau_r$ : Stator and rotor time constant

$P$ : Pole pair number

$\sigma$ : Dispersion coefficient

$\omega_s, \omega_r$ : Stator and rotor pulsations

$\Omega$ : Mechanical pulsation

$T_r$ : Load torque

$T_{em}$ : Electromagnetic torque

$\Omega$ : Rotation speed of the machine

$J$ : Moment of inertia

$f$ : Coefficient of viscous friction

$U_c$ : DC bus voltage

$\theta_s$ : Position of stator flux

$H_{T_{em}}$ : Hysteresis band of torque electromagnetic

$H_{\psi_s}$ : Hysteresis band of stator flux

$K_i, K_p$ : Integral and proportional gains

$\varepsilon_{Ai}$ : Error of the magnitude  $A_i$

### Abbreviations

ANN: Artificial neural networks; DSVM: Discrete space vector modulation; DTC: Direct torque control; DTNC : Direct torque neural control; FLC: Fuzzy logic controller; FOC: Field oriented control; GA: Genetic algorithm; IM: Induction machine; MPC: Model predictive control; PI: Proportional integral; PWM: Pulse width modulation; SMC: Sliding mode control; SVM: Space vector modulation; THD: Total harmonics distortion; VSC: Variable structure control

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### Availability of data and materials

Data sharing not applicable to this article as no datasets were generated or analyzed during the current study.

### Authors' contributions

NE, SM and AD performed the study of improvement techniques of Direct Torque Control, AE and AC corresponding, engaged in modifying the paper and submitted it to the PCMP. SM, MT and YM checked the grammar and writing of the paper. All authors read and approved the final manuscript.

### Competing interests

The authors declare that they have no competing interests.

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