

1 **Multivariate analysis of flood characteristics in a climate change context of the**
2 **watershed of the Baskatong reservoir, Province of Québec, Canada**

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23

Abstract

24 The analysis of the impact of climate change (CC) on flood peaks has been the subject
25 of several studies. However, a flood is characterized not only by its peak, but also by
26 other characteristics such as its volume and duration. Little effort has been directed
27 towards the study of the impact of CC on these characteristics. The aim of the present
28 study is to evaluate and compare flood characteristics in a CC context, in the
29 watershed of the Baskatong reservoir (Province of Québec, Canada). Comparisons are
30 based on observed flow data and simulated flow series obtained from hydrological
31 models using meteorological data from a regional climate model for a reference
32 period (1971-2000) and a future period (2041-2070). To this end, two hydrological
33 models HSAMI and HYDROTEL are considered. Correlations, stationarity,
34 change-points and the multivariate behavior of flood series were studied. The results
35 show that, at various levels, all flood characteristics could be affected by CC.

36 **1. Introduction and literature review**

37 Governments and populations are increasingly interested in the impacts of global
38 warming. According to the World Meteorological Organization (WMO), the
39 frequency of extreme events has doubled in last years (Pachauri, 2002). Among these
40 phenomena we mention the strong growth of hurricanes in Europe (category 5) in
41 2005 as well as the prolonged heat waves in Europe during the summer of 2003 (see
42 e.g. Beniston, 2004 and Wilkinson and Souter, 2008).

43 Climate Change (CC), caused by increased concentrations of greenhouse gases,
44 has effects on the hydrological cycle. Impacts on the frequencies and intensities of
45 rainfall are expected. Water quality is also supposed to be degraded as it is directly
46 related to the available water quantity (Arnell, 1999; Warren, 2004). In the province
47 of Québec, Canada, many environmental and industrial sectors may suffer from CC,
48 such as: forest harvesting, hydropower generation, coastal erosion control, aquatic
49 ecosystems protection, water management, agriculture, transportation, human health
50 and tourism (see e.g., Bergeron et al., 1997).

51 In order to identify and study the effects of CC on the hydrologic regime in the
52 province of Québec and other northern countries, a number of hydrological variables
53 were the subject of several studies (e.g., Ouarda et al., 1999; Seidou and Ouarda, 2007;
54 Khaliq et al., 2008 and Saint-Laurent et al., 2009). These studies showed the existence
55 of breaking points, trends of average and/or variance and cyclical evolution in various
56 hydrological variables.

57 Other studies focused on the comparison of the outputs of global climate models

58 coupled with hydrological models, reanalysis results or historical data (e.g., Singh,
59 1987; Mortsch and Quinn, 1996 and Guay et al., 2004). These studies showed an
60 increase in annual average temperatures that promotes evaporation and increases the
61 contribution of precipitations. On the other hand, studies of CC effects on solid
62 precipitations showed that there could be a decrease in the fraction of solid
63 precipitations (e.g., Bruce et al., 2000; Dibike and Coulibaly, 2005; and EEA., 2008).
64 For the mean annual flow, various studies provided that it might be affected (increase
65 or decrease) in the future (e.g., D’Arcy et al., 2005; Graham et al., 2007 and Mareuil
66 et al., 2007). Studies of the effects of CC on the low water level showed that it could
67 be reduced in the future (e.g., Guay et al., 2004; Minville et al., 2008 and Vescovi et
68 al., 2008). Mortsch and Quinn (1996), Lorrain (2007) and Vescovi et al. (2008)
69 studied the effects of CC on winter and spring flows. Contrary to low water level,
70 these studies concluded that winter and spring flows would be sustained over the
71 coming decades.

72 Frequencies and magnitudes of extreme events are of great importance in studies
73 of climate change effects on hydrology in the province of Québec and other northern
74 regions (e.g., Mareuil et al., 2007). These studies pointed out potential increases in the
75 flow volume and flow peak. The effects of CC on the spring flood could be expressed
76 by an advance of its starting date (e.g., Mareuil et al., 2007; Fortin et al., 2007 and
77 Vescovi et al., 2008) and a decrease in its peak (e.g., Doré et al., 2006 and Minville et
78 al., 2008).

79 The impact of CC on flood peak has been the subject of several studies. However,

80 floods are characterized not only by their peak (Q_p), but also by the following
81 characteristics: starting date (ds), ending date (de), peak date (dp), duration (D),
82 volume (V), climb-rate (T_m) and shape of the hydrograph (F_h). Little efforts have been
83 directed towards the study of the impact of CC simultaneously on all these
84 characteristics.

85 The aim of the present study is to assess and compare the aforementioned flood
86 characteristics in a CC context. To this end, we considered the watershed of the
87 Baskatong reservoir (Province of Québec, Canada). Observed and simulated flow data
88 of this basin are employed to obtain all the above flood characteristics on reference
89 and future periods. Furthermore, two hydrological models, HSAMI and HYDROTEL,
90 are considered in order to evaluate sensitivity of the estimation of the flood
91 characteristics regarding the choice of hydrological model. In addition, the followed
92 methodology is composed by several parts including descriptive statistical analysis,
93 correlation study, stationarity testing, detection of break-points of all series and
94 multivariate analysis of the main characteristic.

95 The paper is organized as follows. The study area, the available data as well as the
96 different employed methods are presented in section 2. Section 3 presents the study
97 results. The conclusions are presented in Section 4.

98 **2. Data series and methodology**

99 In the present section, we introduce the study area and we describe the different
100 methods to evaluate and to analyze the considered flood characteristics.

101 The study area is the watershed of the Baskatong reservoir located in the province of
102 Québec in Canada (see Figure 1). The watershed has an area of 13 040 km². The
103 hydrological regime is dominated by snowmelt runoff, which occurs generally from
104 April to June. The Mercier dam, at the outlet of the Baskatong reservoir, is the largest
105 structure in the watershed. The regularization of Mercier dam is controlled by
106 Hydro-Quebec, a public utility in Québec responsible for electricity generation and
107 supply.

108 The flood characteristics are evaluated and compared using three categories of
109 datasets from Baskatong watershed. The first category consists in the observed flow
110 series from January 1st 1969 to December 31st 2000. In the second category, there are
111 two simulated flow data sets obtained by the hydrological models HSAMI (Bisson
112 and Roberge, 1983) and HYDROTEL (Fortin et al., 1995). The inputs of these models
113 are meteorological data. These data are simulated by the Canadian Regional Climate
114 Model (CRCM) using the atmospheric fields from ERA-40 reanalysis as boundary
115 conditions on the period from January 1st 1969 to December 31st 2000. In the third
116 category, there are two simulated flow data sets obtained by HSAMI and
117 HYDROTEL using the direct method on the period from January 1st 1961 to
118 December 31st 2070. For these series, we used the results of the CRCM (e.g., Brochu
119 and Laprise, 2007 and Music and Caya, 2007) driven by the atmospheric fields from
120 Coupled Global Climate Model (CGCM3), run #4 on the assumption of an increase in
121 greenhouse gases for the A2 scenario.

122 For comparison of flood characteristics in CC context, we used two periods of

123 thirty years:

- 124 - Reference period: from January 1st 1971 to December 31st 2000;
- 125 - Future period: from January 1st 2041 to December 31st 2070.

126 The choice of the last thirty years is explained by the fact that, over thirty years,
127 the extended average of long-term climatic cycles such as the El Niño-Southern
128 Oscillation (ENSO) is taken into account in the series. It follows that for the three
129 categories of data we have seven sets of thirty years. The description of these seven
130 sets and the corresponding notations are summarized in Table 1.

131 **2.1 Determination of flood characteristics**

132 As indicated in the introduction, a flood is described by several characteristics
133 throughout a hydrograph. Figure 2 illustrates a typical hydrograph and the different
134 characteristics. In the present study, analyses are focused on spring flood
135 characteristics, resulting mainly from snowmelt, whereas for fall flood only the peak
136 flow is considered. In the following, we give the definition of each flood
137 characteristic as well as the corresponding determination methods from flow series.

138 *Starting and ending dates:*

139 Starting date « *ds* » and ending date « *de* » of flood are the most important
140 characteristics since they affect the determination of the remaining characteristics. To
141 calculate these two characteristics, we use the method proposed by Pacher (2006). It
142 is based on the analysis of cumulative annual hydrographs by adjusting the slopes
143 with a linear approximation.

144

145 *Flood duration:*

146 Once the starting and ending dates are obtained, the duration « D » is defined by
147 the number of days between the starting date and ending date, i.e., $D = de - ds$.

148 *Flood peak:*

149 For the determination of flood peak « Q_p », we use the idea of the
150 Flood-Duration-Frequency (QdF) approach (Cunderlik and Ouarda, 2006) to reduce
151 the 1-day flood peak uncertainty. The method consists in determining the flood peak
152 of the day « i » as the maximum of the « n » flood peaks averages around « i ». From
153 a practical point of view, it is more reasonable to take small values of « n ». Indeed,
154 with a large value of n , we will be more close to the volume concept. In the present
155 study we considered $n = 3$. The corresponding flood peak is then:

$$156 \quad Q_p = \max\{q_{i3}, i = d_s, \dots, d_e\} \quad (1)$$

157 where q_{i3} is the flow of the day « d_i » associated to 3 days given by
158 $q_{i3} = \text{mean}\{q_{i-1}, q_i, q_{i+1}\}$ with q_i is the flow of the day « d_i ».

159 *Peak of fall flood:*

160 For the fall flood, the flood peak « Q_{pa} » is the maximum flow between July 1st
161 and December 31st. It is determined by:

$$162 \quad Q_{pa} = \max\{q_{i3}, i = d_1, \dots, d_n\} \quad (2)$$

163 where d_1 and d_n represent July 1st and December 31st respectively.

164 *Peak date:*

165 The peak date « d_p » is the date that corresponds to flood peak « Q_p ».

166

167 *Flood volume:*

168 The volume « V » is determined by the following equation:

$$169 \quad V = \sum_{i=d_s}^{d_c} q_i \quad (3)$$

170 where q_i is the flow of the day « d_i ».

171 *Hydrograph shape « F_h »:*

172 The shape of the hydrograph can be obtained on the basis of the date of flood
173 peak « d_p » and the date of mid-duration « d_c » (Figure 3). There are three types of
174 hydrograph shapes: positive asymmetric if $d_p < d_c$, symmetric if $d_p = d_c$ and negative
175 asymmetric if $d_p > d_c$.

176 A hydrograph can be modeled by several methods such as the traditional unit
177 hydrograph method, (Pilgrim and Cordery, 1993), the synthetic unit hydrograph
178 method, (US-SCS, 1985), the typical hydrograph method, (Nezhikhovsky, 1971) and
179 the statistical method, (Ciepielowski, 1987; Haktanir and Sezen, 1990).

180 The statistical method is considered in present study where both Gamma and Beta
181 distributions were tested and it was concluded that, for the Baskatong watershed, Beta
182 distribution (with two parameters a and b) better reconstructs the shape of
183 hydrographs. The modeling methodology of the Beta distribution is explained in Yue
184 et al. (2002). The shape of the hydrograph is determined according to the ratio a/b :
185 positive asymmetry if $a/b < 1$, symmetry if $a/b = 1$ and negative asymmetry if
186 $a/b > 1$.

187 *Climb-rate:*

188 The climb-rate may be determined by the following equation (Young et al. 1999).

$$189 \quad T_m = \text{mean}(t_i, i = d_s, \dots, d_p) \quad (4)$$

190 where t_i is the elementary climb-rate, d_s is the starting date and d_p is the peak date
191 (Figure 2).

192 **2.2 Statistical methods to analyze flood characteristics**

193 In this section, we present the different statistical methods employed to analyze
194 and compare flood characteristics. This section is composed of descriptive statistics,
195 several correlations, stationarity, break-point detection and multivariate modeling.

196 *Descriptive statistics:*

197 In the descriptive part, we considered the mean and the variance of each
198 characteristic and we plotted the corresponding box-plots. We used the
199 Mann–Whitney test (Corder and Foreman, 2009) to check the significance of the
200 difference between the compared mean series. To better explain the results, we
201 superimposed the simulated and observed flood hydrographs. These hydrographs are
202 presented for each year in Appendix D in Ben Aissia et al. (2009).

203 *Correlations:*

204 To investigate further the flood characteristics, three types of correlations are
205 studied. The first is the correlation between different flood characteristics for the same
206 series, the second is the correlation between different series of the same flood
207 characteristic and the last one is the correlation between meteorological data and flood
208 characteristics.

209 For space limitations, we considered the main flood characteristics: starting date
210 « d_s », duration « D », peak « Qp » and volume « V ». For each value of the evaluated
211 correlations, a statistical t -test (Kanji, 1993) was applied to check its significance.

212 *Stationarity:*

213 In order to study the stationarity of each one of the considered series, we applied
214 the Mann-Kendall test (Mann, 1945 and Kendall, 1975). The Mann-Kendall test
215 determines the existence of a trend in a series. The test statistic is given by:

$$216 \quad Z = \begin{cases} \frac{S-1}{[\text{var}(S)]^{1/2}} & \text{if } S > 0 \\ 0 & \text{if } S = 0 \\ \frac{S+1}{[\text{var}(S)]^{1/2}} & \text{if } S < 0 \end{cases} \quad (5)$$

217 where

$$218 \quad S = \sum_{k=1}^{n-1} \sum_{j=k+1}^n \text{sgn}(x_j - x_k) \quad (6)$$

219 and

$$220 \quad \text{sgn}(x) = \begin{cases} +1 & \text{if } x > 0 \\ 0 & \text{if } x = 0 \\ -1 & \text{if } x < 0 \end{cases} \quad (7)$$

221 If a series is detected as non-stationary by the Mann-Kendall test, then we apply
222 to that series the modified Mann-Kendall test (Yue and Wang, 2002). This test
223 completes the Mann-Kendall test by taking into account the autocorrelation in the
224 series. Indeed, the presence of an autocorrelation affects the variance of the statistic Z .
225 The modified test statistic Z^* is given by:

$$226 \quad Z^* = \frac{Z}{\sqrt{\eta^*}} \quad (8)$$

227 where Z is the statistic of Mann-Kendall test given in (5) and η^* is a correction
228 factor (see Yue and Wang, 2002).

229 *Break-point:*

230 To examine the existence of break-points in the series, we used the Bayesian
 231 method of multiple break-point detection in multiple linear regressions (Seidou and
 232 Ouarda, 2007). This method determines the number of break-points and their
 233 locations as well as the trends in each segment of the series. The Bayesian procedure
 234 assumes an improper noninformative prior as a distribution for the parameters
 235 representing the break-points. In the present study, the regression model is formulated
 236 as:

$$237 \quad \begin{cases} y = \theta_1 x + \theta_2 + \varepsilon & \text{if } x \leq \tau \\ y = \theta'_1 x + \theta'_2 + \varepsilon' & \text{if } x > \tau \end{cases} \quad (9)$$

238 where y represents the flood characteristic (e.g. peak), x is the time as
 239 years, $\theta_1, \theta_2, \theta'_1$ and θ'_2 are the parameters to be estimated and τ is the break-point time.

240 *Multivariate modeling*

241 Copulas have received increasing attention in various fields of science. Copulas
 242 are used to describe the dependence structure between random variables. They are
 243 independent of marginal distributions. Therefore, the marginal distributions do not
 244 need to be the same. Three main flood characteristics (peak, volume and duration) are
 245 studied in a multivariate analysis. A copula is a p dimensional distribution function C
 246 ($p \geq 2$) with uniform margins on $[0, 1]$. Given such a copula, we can construct a
 247 multivariate distribution F with margins F_{x_1}, \dots, F_{x_p} through Sklar's (1959) theorem
 248 by:

$$249 \quad F(x_1, \dots, x_p) = C(F_{x_1}(x_1), \dots, F_{x_p}(x_p)) \quad x_1, \dots, x_p \in R \quad (10)$$

250 Hence, fitting a multivariate distribution is divided into two parts: fitting a
 251 marginal distribution to each variable and fitting the dependence structure between

252 variables through copulas. On the other hand, copulas are employed to model the
 253 dependence structure. In the literature, there are several copula families to model the
 254 dependence structure between variables. The class of Archimedean copulas is widely
 255 used in hydrology (Wong et al. 2008). For a convex decreasing function φ with $\varphi(1) =$
 256 0, a copulas C_φ is said to be Archimedean with generator φ if C_φ can be expressed
 257 in the form:

$$258 \quad C_\varphi(u_1, \dots, u_p) = \varphi^{-1}(\varphi(u_1) + \dots + \varphi(u_p)) ; \quad 0 < u_1, u_2, \dots, u_p < 1 \quad (11)$$

259 where φ^{-1} represents the inverse of φ .

260 The most common Archimedean copulas are the copula of Gumbel, Frank and
 261 Clayton. The goodness-of-fit test used is the graphical test proposed by Genest and
 262 Rivest (1993) based on the K function given by:

$$263 \quad K_\varphi(u) = u - \frac{\phi(u)}{\phi'(u)} ; \quad 0 < u < 1 \quad (12)$$

264 **3. Results and discussion**

265 All the considered flood characteristics are obtained for the different flow series.
 266 Then, the results of the studied characteristics are analyzed at various levels, namely:
 267 descriptive analysis, correlation study, stationarity study, break-point detection and a
 268 multivariate analysis.

269 **3.1. Descriptive analysis of the results**

270 In this section, we analyze the results of each characteristic in a descriptive
 271 manner. To examine the ability of the used models to reproduce the observed
 272 phenomena, we compare (RHS & RHY) and (SHS & SHY) to observed data. We then
 273 compare SHSF and SHYF to SHS and SHY respectively in order to identify CC

274 effects. The descriptive statistics of the series of flood characteristics are gathered in
275 Table 2 and the corresponding the box-plots are in Figure 4.

276 For all considered flood characteristics, we check the significance of the difference
277 between compared series means by the Mann–Whitney test (Corder and Foreman,
278 2009).

279 *Starting date d_s :*

280 Figure 4a and Table 2 show that the starting dates of the simulated series RHS and
281 RHY are similar in the mean to those observed, but with larger variances. The starting
282 dates of the simulated series SHS and SHY occur later than those observed. However,
283 for the future series SHSF and SHYF, the starting dates could be earlier with more
284 variability.

285 *Ending date d_e :*

286 From Figure 4b and Table 2 we notice that for the HSAMI model, the ending
287 dates of the simulated series SHS and RHS are slightly later than those observed.
288 However, those simulated on the future period (SHSF and SHYF) have larger
289 variances.

290 *Duration D :*

291 The results presented in Figure 4c and Table 2 show that, except for the series
292 SHS, all other flood series simulated in the reference period have longer durations
293 than those observed. Comparisons between SHS and SHSF and between SHY and
294 SHYF show that future floods can be longer than those simulated in the reference
295 period. The series simulated by HYDROTEL have variances larger than those

296 simulated by HSAMI. The difference of variance can be explained by the fact that
297 HYDROTEL is a distributed model where simulated hydrographs can have a slightly
298 different shape than those simulated with HSAMI, a global model (Bisson and
299 Roberge, 1983).

300 *Flood peak Q_p :*

301 Figure 4d and Table 2 show that the flood peak could be lower and with less
302 variability in the future. Flood peaks simulated by HSAMI are higher than those
303 simulated by HYDROTEL. Neither hydrological model is able to simulate high flood
304 peaks as those observed in the historical data series.

305 *Peak date d_p :*

306 From Figure 4e and Table 2 we see that, with the exception of the series SHY,
307 peak date series are similar on average. For the future period, hydrological models
308 expect that the peak date would be earlier and more variable.

309 *Flood volume V :*

310 The results related to flood volume are presented in Figure 4f and Table 2. We can
311 observe that the flood volume series from the reanalysis data RHS is the only one to
312 provide a volume greater than that observed. In the future, flood volume can be bigger
313 and more variable. Flood volumes simulated by HSAMI are greater than those
314 simulated by HYDROTEL.

315 *Shape of the hydrograph F_h :*

316 Figure 4g and Table 2 show that the mean values of asymmetry coefficients
317 obtained are close to 1 for all series. Asymmetry coefficients obtained by

318 HYDROTEL are higher and more variable than those obtained by HSAMI. In
319 addition, we observe that the HSAMI model is not able to simulate the variation in the
320 shape of the hydrograph. The reason could be that, during the computation of water
321 discharge at the outlet, HSAMI uses only the Gamma distribution to model the shape
322 of the hydrograph (Bisson and Roberge, 1983).

323 *Climb-rate T_m :*

324 The results presented in Figure 4h and Table 2 related to the climb-rate of the
325 spring flood hydrograph show a possible increase of climb-rate and its variation in the
326 future. An opposition in the behavior of hydrological models HSAMI and
327 HYDROTEL between the reanalysis results (RHS, RHY) and simulations results
328 (SHS, SHY and SHSF, SHYF) is observed. Indeed, reanalysis results show that the
329 climb-rates simulated by HYDROTEL (RHY) are greater than those simulated by
330 HSAMI (RHS). The opposite is observed from the results of CGCM3.

331 *Peak of fall flood Q_{pa} :*

332 From Figure 4i and Table 2 we note that, except for the series SHYF, the
333 simulated series Q_{pa} by HSAMI are lower than those observed. However, the
334 simulated Q_{pa} series by HSAMI are lower than those simulated by HYDROTEL.
335 Comparisons between SHS and SHSF and between SHY and SHYF show that future
336 fall flood can be more important and with more variability.

337 Based on the results presented in this section, we concluded that the simulated
338 floods from RHS and RHY have later ending dates and longer duration than those
339 observed. Furthermore, the climb-rates of simulated floods from the reanalysis are

340 lower than those observed. For the simulated floods from SHS and SHY, we note that
341 floods begin and end later than those observed and with fall peak, spring peak,
342 volume and climb-rate lower than their observed counterparts. However, simulated
343 floods from SHSF and SHYF could begin earlier than those simulated in the reference
344 period and may have earlier peak. For HSAMI future flood could have longer
345 duration and for HYDROTEL future flood could have larger climb-rate.

346 Comparison of the results of both hydrological models shows that the outputs
347 from HYDROTEL have a variance greater than that of HSAMI. The volumes of the
348 simulated flood by HSAMI are greater than those simulated by HYDROTEL whereas,
349 the fall flood peaks simulated by HYDROTEL are greater than those simulated by
350 HSAMI. On the other hand, from the reanalysis, simulated floods by HYDROTEL
351 have climb-rate greater than those simulated by HSAMI. The opposite is observed
352 from the results of CGCM3 on both periods. That is to say, for reference and future
353 periods, the results of CGCM3 simulated floods by HSAMI have climb-rate greater
354 than those simulated by HYDROTEL.

355 From Figures 4c and 4f we observe that generally the durations of simulated floods by
356 HYDROTEL are longer than those simulated by HSAMI whereas the opposite holds
357 for the volume. This result is not expected due to the usual positive correlation
358 between V and D . This point will be studied in the next session.

359 **3.2. Study of correlations**

360 In this section, we analyze the correlations between the characteristics of the same
361 series, between series of the same characteristic and between meteorological data and

362 different flood characteristics.

363 *Correlations between the characteristics of the same series*

364 Table 4 presents the correlations between the main flood characteristics for each
365 one of the seven considered series (DH, RHS, RHY, SHS, SHY, SHSF and SHYF).
366 We note that there is a strong negative correlation between the starting date and the
367 duration (between -0.47 and -0.72) and a strong positive correlation between the
368 volume and peak (between 0.44 and 0.70). The correlations between the ds and the
369 Qp and those between the V and D are less strong (about 0.3 to 0.4). Between the V
370 and the ds the correlations are low, generally below 0.2, and are considered not
371 significant. For correlations between D and Qp , three of the seven series have
372 moderate correlations (between -0.38 and -0.51) whereas the others have non
373 significant correlations (less than 0.30). These results are in agreement with those
374 generally obtained in the literature (e.g. Yue et al., 1999; Kim, 2003). Namely, there is
375 a correlation between both V and Qp and between V and D and not significant
376 correlation between Qp and D .

377 The moderate correlation between V and D can explain why in Figures 4c and 4f
378 the duration of HYDROTEL simulated floods are longer than those simulated by
379 HSAMI whereas the volume of HYDROTEL simulated floods are smaller than those
380 simulated by HSAMI.

381 *Correlations between series of the same characteristic*

382 For each of the four main characteristics considered, the correlations between the
383 seven series (DH, RHS, RHY, SHS, SHY, SHSF, and SHYF) are evaluated. The

384 corresponding results are presented in Table 5. The correlations are not significant for
385 almost all series. Nevertheless the characteristic series from the reanalysis are
386 correlated with the corresponding observed characteristics and the characteristic series
387 simulated by HSAMI are correlated with those simulated by HYDROTEL.

388 *Correlation between meteorological data and different flood characteristics*

389 The hydrological models (HSAMI and HYDROTEL) have meteorological inputs
390 series such as minimum temperature, maximum temperature and precipitation. Hence,
391 these meteorological series and the characteristics of the simulated floods could be
392 correlated. Moreover, in Québec spring flood is caused mainly by snow melting
393 resulting from the increase in temperature during the spring. Therefore starting dates
394 and maximum temperatures prior starting date could be correlated. Likewise, volume
395 and precipitations could be correlated. First, we examine the correlation between the
396 starting date and the average maximum temperatures of 7, 10 or 14 days prior the
397 starting date. Then we evaluate the correlations between the starting date and the date
398 when the maximum temperatures are always greater than zero. Finally, we calculated
399 the correlation between volume and cumulative rainfall between December 15th and
400 March 15th.

401 The results of correlations between the starting date and the average maximum
402 temperature (Table 6) show that for five of the six series (except RHY) the correlation
403 increases when the duration range increases. The opposite is observed in the series
404 simulated by HYDROTEL (RHY). The starting date is moderately correlated with the
405 date when the maximum temperature is always greater than zero (Table 7).

406 The correlation between the volume and the cumulative precipitation between
407 December 15th and March 15th (Table 8) is between 0.3 and 0.5 for the majority of the
408 series. The only exception is the series SHYF which gives a low correlation value.

409 **3.3. Stationarity**

410 The stationarity of all the considered series (63 series: 9 characteristic x 7 series)
411 is studied in this section using Mann-Kendall and modified Mann-Kendall tests. Table
412 9 shows the detected non-stationary series on the basis of the Mann-Kendall test. It
413 follows that among these series; two are actually slightly non-stationary using the
414 modified Mann-Kendall test: RHS and SHSF for the fall flood peak . These series are
415 both obtained from HSAMI. From Section 3.2, the two series RHS and RHY are
416 correlated (0.78) but only RHS is non-stationary. Similarly, the two series SHSF and
417 SHYF are correlated (0.83) but only SHSF is non-stationary. For a better comparison
418 of the two hydrological models (HSAMI and HYDROTEL), we represent the trends
419 associated with each of these four series of fall flood peak (RHS & RHY and SHSF &
420 SHYF) in Figure 5. We note that the slopes associated to the four identified trends are
421 positive. Series simulated by HYDROTEL have peaks higher than those simulated by
422 HSAMI and have a higher variability. In addition, the slopes of the series simulated
423 by HSAMI are larger than those simulated by HYDROTEL which explains the
424 non-stationarity detected in those simulated by HSAMI. Nevertheless, this
425 non-stationarity is weak given the large values of p-value (Table 9).

426 **3.4. Bayesian analysis for break-points detection**

427 The results of Bayesian analysis of break-points detection show that eight of the

428 considered series are identified with one break-point (Figure 6). These series are: the
429 *D* of SHSF and SHYF, the *V* of RHY, the *Fh* of SHY and SHS, the *Qpa* of DH and the
430 *Tm* of SHY and DH.

431 We note that on the reference period, the detected break-points are around the year
432 1985. Analysis of superimposed hydrographs shows that the period following 1985 is
433 a period characterized by low spring flow. Furthermore, in the future period two series
434 of duration (SHSF and SHYF) have a break-point in 2056. From Figure 6 we
435 conclude that the break amplitude is very slight. This break is caused, in the case of
436 the SHYF by an exceptional value simulated in 2055 (Figure 6) and, in the case of
437 SHSF, by a change of variation before and after the year 2055. The detection of this
438 break-point, with very slight amplitude, is related to the sensitivity of the employed
439 method (e.g. Beaulieu et al. 2009).

440 **3.5. Multivariate analysis**

441 To extend the study of flood characteristics, three main characteristics (peak,
442 volume and duration) are studied in a multivariate analysis. Fitting a multivariate
443 distribution is divided into two parts: fitting a marginal distribution to each variable
444 and fitting the dependence structure between variables through copulas.

445 *Adjustment of marginal distributions*

446 To determine the most appropriate marginal distribution to peak, volume and
447 duration, we used the HYFRAN software (Chaire en hydrologie statistique, 2002).
448 The choice of the appropriate distribution is based on the AIC criterion. The results of
449 marginal distribution are presented in Table 10. It can be seen that several

450 distributions adjust the series and we cannot draw a general conclusion on the
451 marginal fittings.

452 *Bivariate copulas*

453 The fitting results are presented in Table 9 of the considered bivariate series. We
454 observe that generally the Gumbel copula is more appropriate for peak-volume while
455 that of Clayton is convenient for volume-duration.

456 **4. Conclusions**

457 The aim of this study is to evaluate and compare flood characteristics in a CC
458 context. We used the historical flow data, the reanalysis data and the simulated data
459 toward 2050. Both reanalysis and simulated data are obtained from two hydrological
460 models HSAMI and HYDROTEL that used meteorological data from a CRCM. After
461 evaluating and presenting the different flood characteristics associated to the
462 considered series, a statistical study was conducted. This study involves a descriptive
463 analysis of each characteristic, a study of different kinds of correlations, a stationarity
464 analysis, detection of break-points and multivariate analysis.

465 The analysis of future flood characteristics shows that floods could begin earlier
466 than those observed and could have earlier peaks. For HSAMI future floods could
467 have longer durations and for HYDROTEL future floods could have larger
468 climb-rates. The characteristic of the series simulated by HYDROTEL have larger
469 variance than those simulated by HSAMI.

470 The correlations observed between the historical series are kept for both
471 characteristics from reanalysis than for those from CGCM3 in the reference period.

472 We showed that most of the studied series are stationary except the two series RHS
473 and SHSF for the peak of fall flood are very slightly non-stationary. The Bayesian
474 method of break-point detection showed that eight of the 63 studied series have one
475 break-point with slight magnitudes. For all the studied series, multivariate analysis of
476 peak, volume and duration showed that the Gumbel copula is generally more
477 appropriate for peak-volume whereas for volume-duration the Clayton copula
478 represents generally a satisfactory fitting.

479 Although, in this study, most of the flood characteristics were considered and the
480 study was conducted at various levels, some elements are not studied and should be
481 considered. Indeed, the use of alternative future climate scenarios and more
482 hydrological models could clarify the impacts of CC on flood characteristics. In the
483 present study, we focused on comparing the reference and the future periods, the use
484 of a moving average would allow for a complete comparison of the whole period. The
485 use of other types of correlation such as Kendall's tau and Spearman's rho could give
486 a better characterization of the relationship between the various flood characteristics.
487 Furthermore, the use of other tests of break-point could improve our series analysis. It
488 is also interesting to further study the multivariate frequency analysis including the
489 concept of multivariate return period in order to quantify and compare the associated
490 risks.

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497

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670

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671

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672

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673

Figure 5 : Non-stationary in fall flood peak and associated trends: a) RHS, b) SHSF, c)

674

RHY and d) SHYF. The dashed line represents the corresponding trend of

675

each series.

676

Figure 6: Detected break-points in the considered series

677

678

Tables

679 **Table 1 : Data series**

	Hydrological model	CRCM	Period	Notation
Observed	-	-	1971-2000	DH
Simulated	HSAMI	ERA-40	1971-2000	RHS
		CGCM3	1971-2000	SHS
			2040-2070	SHSF
	HYDROTEL	ERA-40	1971-2000	RHY
		CGCM3	1971-2000	SHY
			2040-2070	SHYF

680

681

682 **Table 2: Descriptive statistics of flood series characteristics**

<i>Series</i>		<i>DH</i>	<i>RHS</i>	<i>RHY</i>	<i>SHS</i>	<i>SHY</i>	<i>SHSF</i>	<i>SHYF</i>
<i>d_s (d)</i>	Mean	99	100	98	106	108	93	97
	Variance	91	123	146	151	86	167	220
	Minimum	80	76	71	81	91	66	57
	Maximum	115	118	120	130	125	117	128
<i>d_e (d)</i>	Mean	143	150	146	149	160	143	159
	Variance	99	64	112	83	114	170	254
	Minimum	116	130	123	128	146	114	113
	Maximum	161	163	166	168	187	163	195
<i>D (d)</i>	Mean	44	50	47	43	53	50	62
	Variance	133	55	180	148	232	155	314
	Minimum	22	36	25	27	28	25	38
	Maximum	66	65	85	81	79	81	125
<i>Q_p (m³s⁻¹)</i>	Mean	1282	1169	1094	991	774	979	740
	Variance	124820	45565	92538	77512	118980	83552	74343
	Minimum	672	761	567	459	230	326	268
	Maximum	2211	1576	1680	1678	1765	1641	1599
<i>d_p (d)</i>	Mean	117	119	117	119	134	108	118
	Variance	172	137	237	189	211	190	439
	Minimum	91	91	75	90	99	76	76
	Maximum	138	141	142	146	166	130	169
<i>V (Mm³)</i>	Mean	3101	3389	2535	2400	2016	2522	2216
	Variance	585050	477310	487110	288440	485740	605370	663650
	Minimum	1565	2415	1472	1053	953	1226	881
	Maximum	5147	5105	3888	3175	4081	4321	3963
<i>a/b</i>	Mean	1.04	0.97	1.07	0.99	1.09	0.93	0.99
	Variance	0.01	0.01	0.02	0.01	0.02	0.01	0.04
	Minimum	0.86	0.72	0.85	0.85	0.75	0.65	0.53
	Maximum	1.24	1.15	1.60	1.21	1.46	1.11	1.33
<i>T_m (m³s⁻¹d⁻¹)</i>	Mean	25	21	28	23	10	28	14
	Variance	74	47	97	22	14	58	13
	Minimum	7	9	9	12	3	15	8
	Maximum	39	32	45	31	18	44	21
<i>Q_{pa} (m³s⁻¹)</i>	Mean	550	397	540	329	480	440	595
	Variance	68406	14801	32707	12892	16090	33967	79649
	Minimum	204	182	275	172	301	196	262
	Maximum	1402	655	1046	636	855	916	1453

683

684

685 **Table 3 : p-value of the Mann-Whitney test**

	DH&RHS	DH&RHY	DH&SHS	DH&SHY	RHS&SHS	RHY&SHY	SHS&SHSY	SHY&SHYF
d_s	0.66	0.75	0.02	0.00	0.06	0.00	0.00	0.00
d_e	0.01	0.59	0.03	0.00	0.75	0.00	0.11	0.58
D	0.04	0.36	0.59	0.04	0.00	0.20	0.02	0.06
Q_p	0.37	0.07	0.00	0.00	0.01	0.00	0.98	0.80
d_p	0.55	0.97	0.66	0.00	0.86	0.00	0.01	0.00
V	0.14	0.01	0.00	0.00	0.00	0.00	0.70	0.33
F_h	0.01	0.84	0.03	0.20	0.38	0.30	0.02	0.02
T_m	0.06	0.16	0.16	0.00	0.32	0.00	0.09	0.00
Q_{pa}	0.01	0.74	0.00	0.46	0.01	0.19	0.01	0.19

686 The gray color indicates that the corresponding mean difference is significant.

687

688 **Table 4 : Correlations between main flood characteristics**

	<i>D</i>		<i>Q_p</i>		<i>V</i>		
<i>d_s</i>		-0.57		0.30		-0.03	
		-0.69	-0.66	0.33	0.22	0.06	-0.16
		-0.72	-0.72	0.58	0.39	0.14	-0.11
		-0.47	-0.53	0.11	-0.18	-0.13	-0.45
<i>D</i>	1			-0.28		0.46	
			-0.14	-0.38	0.32	0.46	
			-0.46	-0.51	0.17	0.27	
<i>Q_p</i>	DH			-0.28	-0.15	0.36	0.60
	RHS	RHY	1			0.61	
	SHS	SHY		0.68	0.44		
	SHSF	SHYF		0.70	0.57		
			0.68	0.55			

689 Example: -0.57 is the correlation between the duration and starting date which are determined from the series of
 690 historical data.

691 The gray color indicates that the corresponding correlation is significant.

692

693 **Table 5: Correlations between simulated and historical series**

	<i>RHS</i>		<i>RHY</i>		<i>SHS</i>		<i>SHY</i>		<i>SHSF</i>		<i>SHYF</i>		
<i>DH</i>	0.84	0.59	0.79	0.37	0.21	-0.07	0.12	-0.03	0.00	-0.13	-0.02	-0.17	
	0.47	0.59	0.36	0.49	-0.02	-0.12	0.00	-0.03	0.10	-0.01	0.20	-0.21	
<i>RHS</i>	1		0.95	0.85	0.13	0.15	0.04	-0.04	-0.03	-0.17	-0.18	-0.31	
			0.69	0.88	0.23	0.21	0.38	0.08	0.26	-0.05	0.14	-0.04	
<i>RHY</i>			1		0.10	0.15	-0.02	-0.09	-0.01	-0.13	-0.16	-0.20	
					0.12	0.18	0.29	-0.05	0.31	-0.04	0.24	-0.02	
<i>SHS</i>					1		0.91	0.53	-0.05	-0.23	0.05	-0.11	
							0.86	0.56	0.24	0.17	0.19	0.13	
<i>SHY</i>			d_s	D				1		-0.23	-0.13	-0.04	-0.17
			Q_p	V						0.21	-0.12	0.18	0.00
<i>SHSF</i>									1		0.73	0.31	
											0.80	0.70	

694 Example: 0.85 is the correlation between the duration series determined from RHY and RHS

695 The gray color indicates that the corresponding correlation is significant.

696

697

698 **Table 6 : Correlation between starting date and average maximum temperature.**

Series	Average maximum temperature		
	7 days	10 days	14 days
RHS	0.26	0.37	0.54
SHS	0.44	0.59	0.69
SHSF	0.33	0.41	0.53
RHY	0.38	0.36	0.18
SHY	0.28	0.39	0.44
SHYF	0.33	0.39	0.44

699 The gray color indicates that the corresponding correlation is significant.

700

701

702 **Table 7 : Correlations between the starting date and the date of the maximum**
 703 **temperature are always greater than zero**

Starting date series	Date from which the maximum temperature are always greater than zero
RHS	0.45
SHS	0.64
SHSF	0.49
RHY	0.33
SHY	0.57
SHYF	0.55

704 The gray color indicates that the corresponding correlation is significant.

705

706 **Table 8 : Correlation between the flood volume and the cumulative of rainfall**
707 **between December 15th and March 15th**

Series	Correlation
RHS	0.42
SHS	0.31
SHSF	0.51
RHY	0.37
SHY	0.41
SHYF	0.17

708 The gray color indicates that the corresponding correlation is significant.

709

710

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Table 9 : Stationarity tests of the characteristics

Characteristics	Series	Mann-Kendall			Modified Mann-Kendall		
		K	p-value	Significant Trend	K	p-value	Significant Trend
Climb-rate	DH	2.29	0.02	yes	1.07	0.28	no
	RHS	2.56	0.01	yes	1.50	0.13	no
	RHY	2.65	0.01	yes	0.46	0.64	no
	SHSF	3.11	0.00	yes	1.54	0.12	no
Fall flood	RHS	2.51	0.01	yes	2.45	0.01	yes
	SHSF	2.85	0.00	yes	2.00	0.05	yes

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Table 10 : Parameters of marginal distribution series of peak, volume and duration

Characteristic	Series	Marginal distribution	Parameter		
			α	β	σ
Q_p	HD	Gumbel	1123.0	275.5	
	RHS	Gamma	30.7	38.0	
	RHY	Weibull	4.1	1206.6	
	SHS	Fuites	38.0	26.1	
	SHY	Fuites	73.4	12.6	
	SHSF	Fuites	42.6	23.0	
	SHYF	Gamma	8.0	96.0	
V	HD	Gamma	17.0	182.6	
	RHS	Gumbel	3077.6	538.7	
	RHY	Log-Normal (two parameters)	606.1	0.7	
	SHS	Generalized extreme value	2314.1	7.8	0.3
	SHY	Gumbel	1701.3	543.4	
	SHSF	Fuites	116.6	21.6	
	SHYF	Gamma	7.4	298,0	
D	HD	Fuites	1.5	30.1	
	RHS	Halphen type B	49.4	2.0	14.71
	RHY	Gamma	12.7	3.7	
	SHS	Gumbel	37.9	8.8	
	SHY	Gamma	11.9	4.4	
	SHSF	Gamma	16.5	3.0	
	SHYF	Gumbel	54.0	11.6	

715 Where α is the parameter position for the distributions: Gumbel, Weibull, Fuites, GEV and Log-Normale (two
716 parameters) and the shape parameter for the distributions: Gamma and Halphen type B. While β represents the
717 scale parameter for the distributions: Gumbel, Gamma, Weibull, GEV, Log-Normale (two parameters) and
718 Halphen type B and the shape parameter for the fuites distributions. Finally, σ is the shape parameter for the
719 distributions GEV and Halphen type B

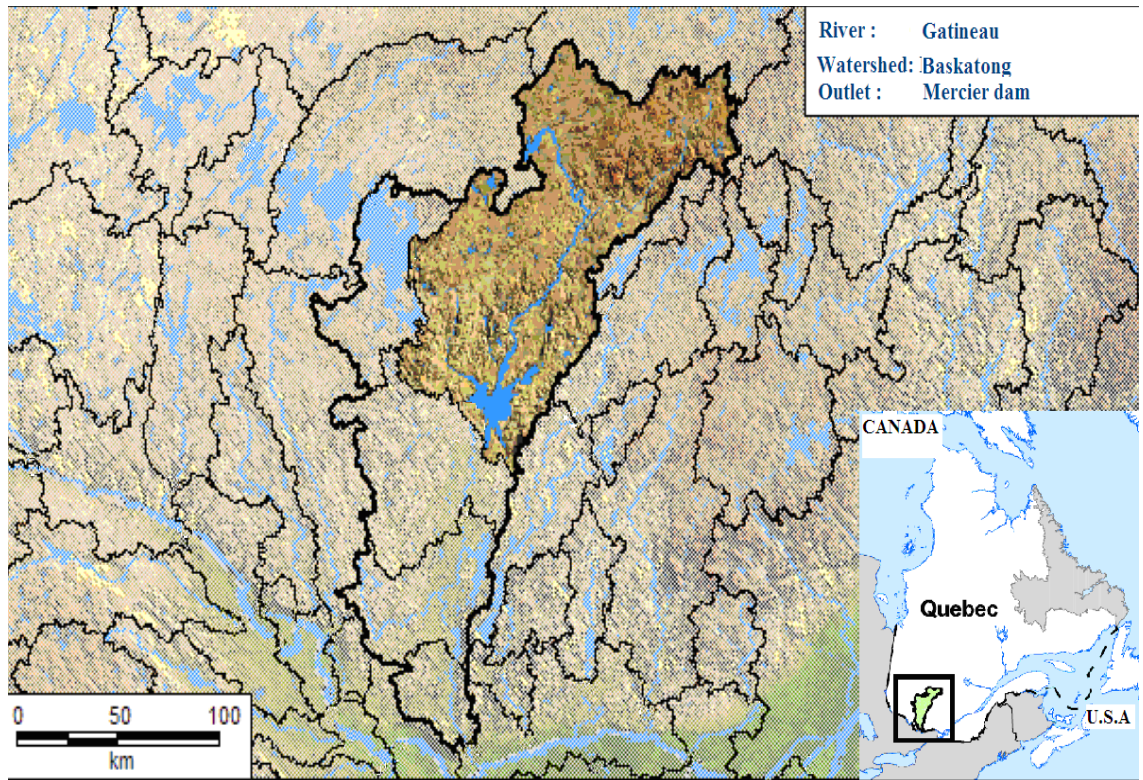
720 **Table 11 : Bivariate copulas fitted to peak-volume and volume-duration**

	DH	RHS	RHY	SHS	SHY	SHSF	SHYF
Peak-Volume	Gumbel	Gumbel	Fank	Gumbel	Gumbel	Gumbel	Clayton
Volume-Duration	Clayton	Clayton	Fank	Clayton	Clayton	Gumbel	Gumbel

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723 **Figures**

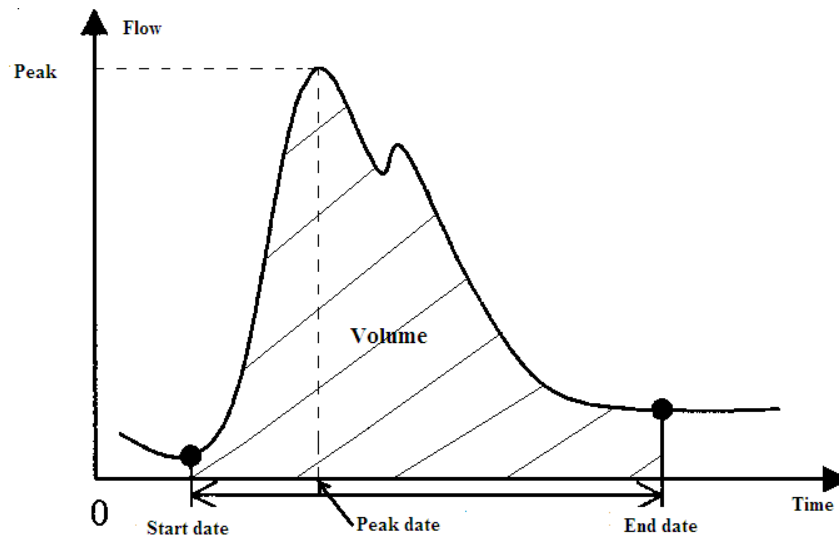


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725 **Figure 1 : Watershed of the Baskatong reservoir map location**

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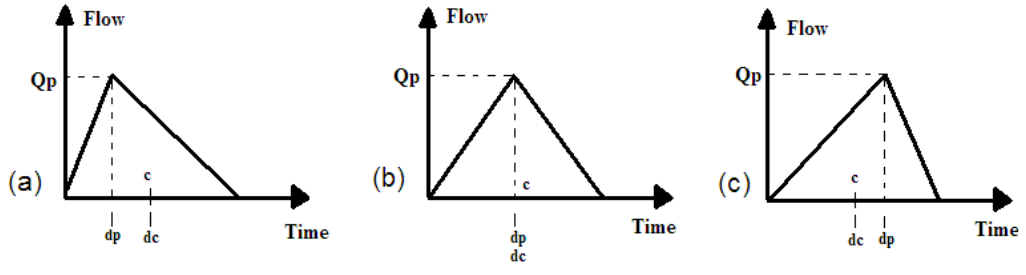
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Figure 2 : Different characteristics of a hydrograph.

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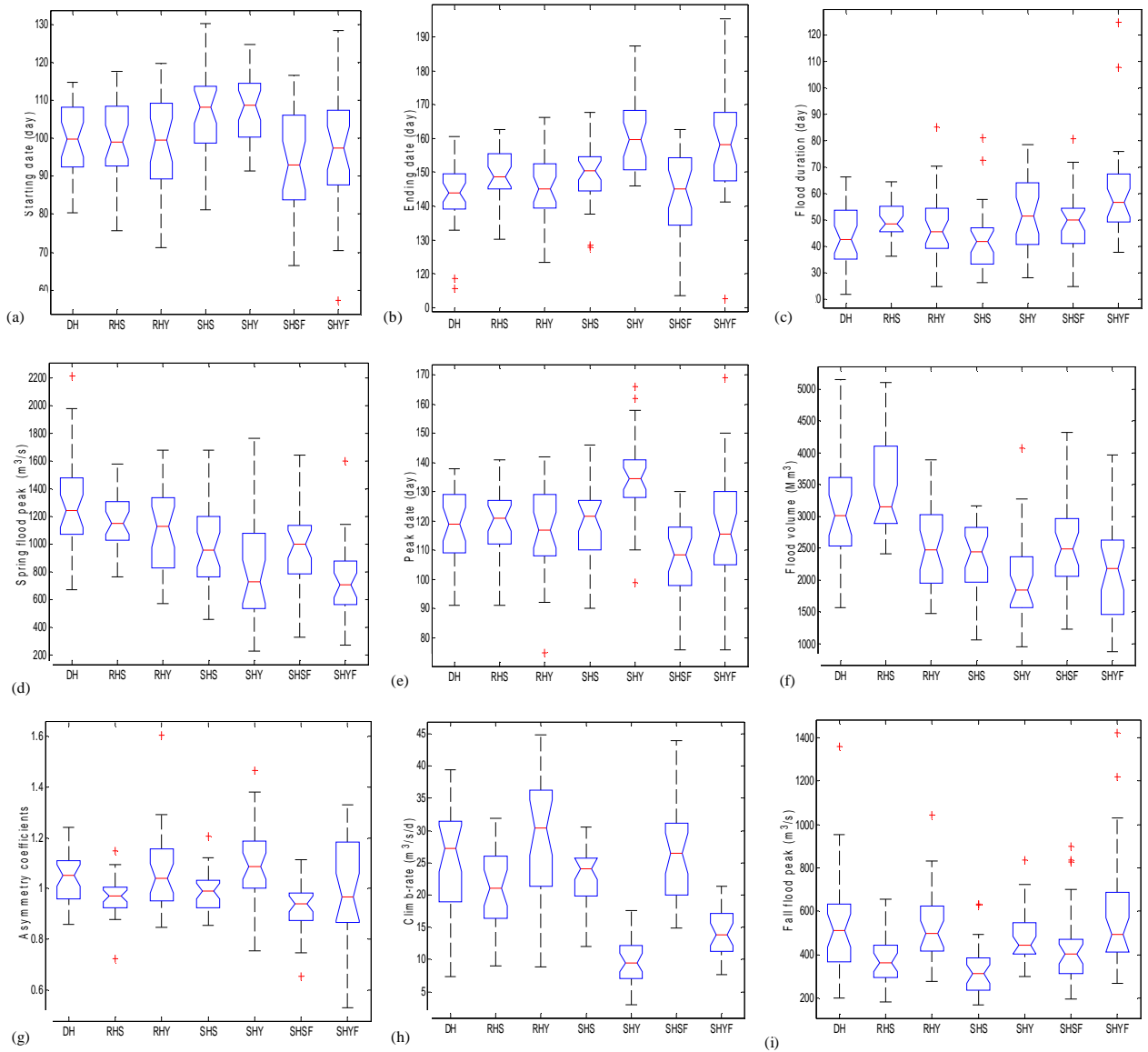
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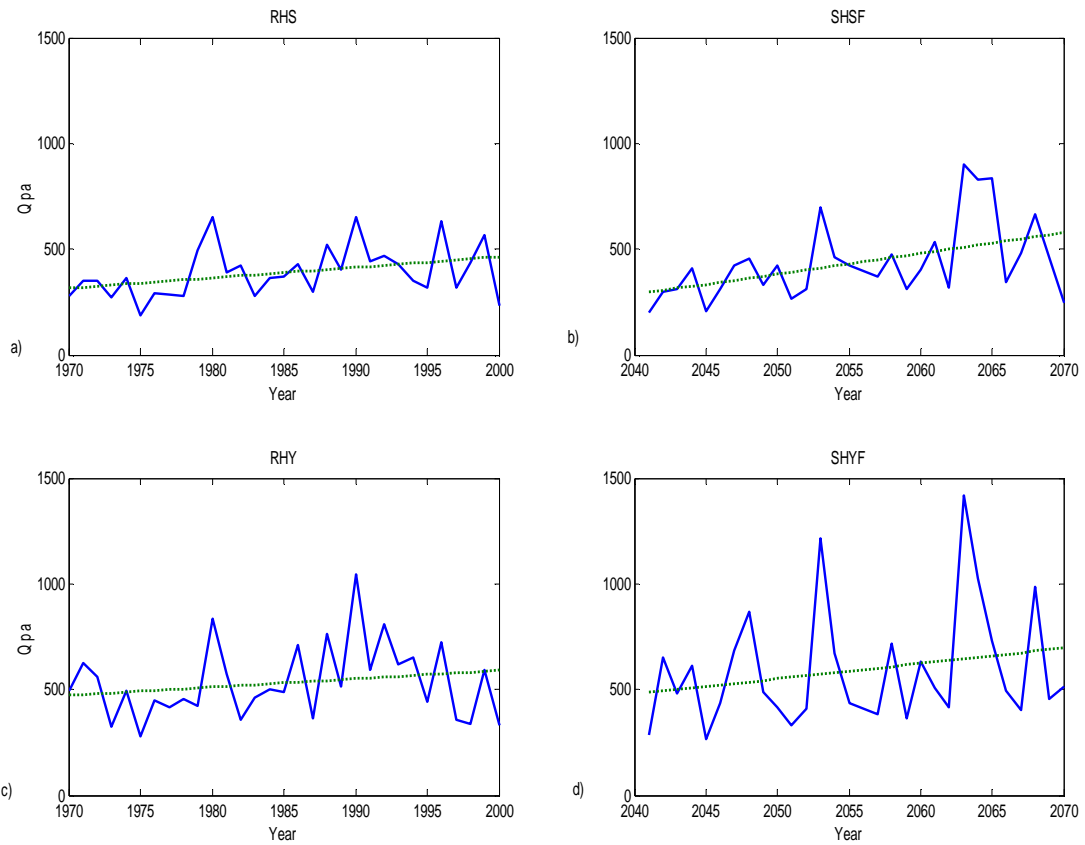
733 **Figure 3 : Diagram illustrating the three types of shape of hydrograph: (a)**
734 **positive asymmetry (b) symmetry (c) negative asymmetry.**

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737 **Figure 4: Box-plot flood characteristics series: a) starting date, b) ending date, c) duration,**

738 **d) peak, e) peak date, f) volume, g) asymmetry coefficient, h) climb-rate and i) fall flood peak**



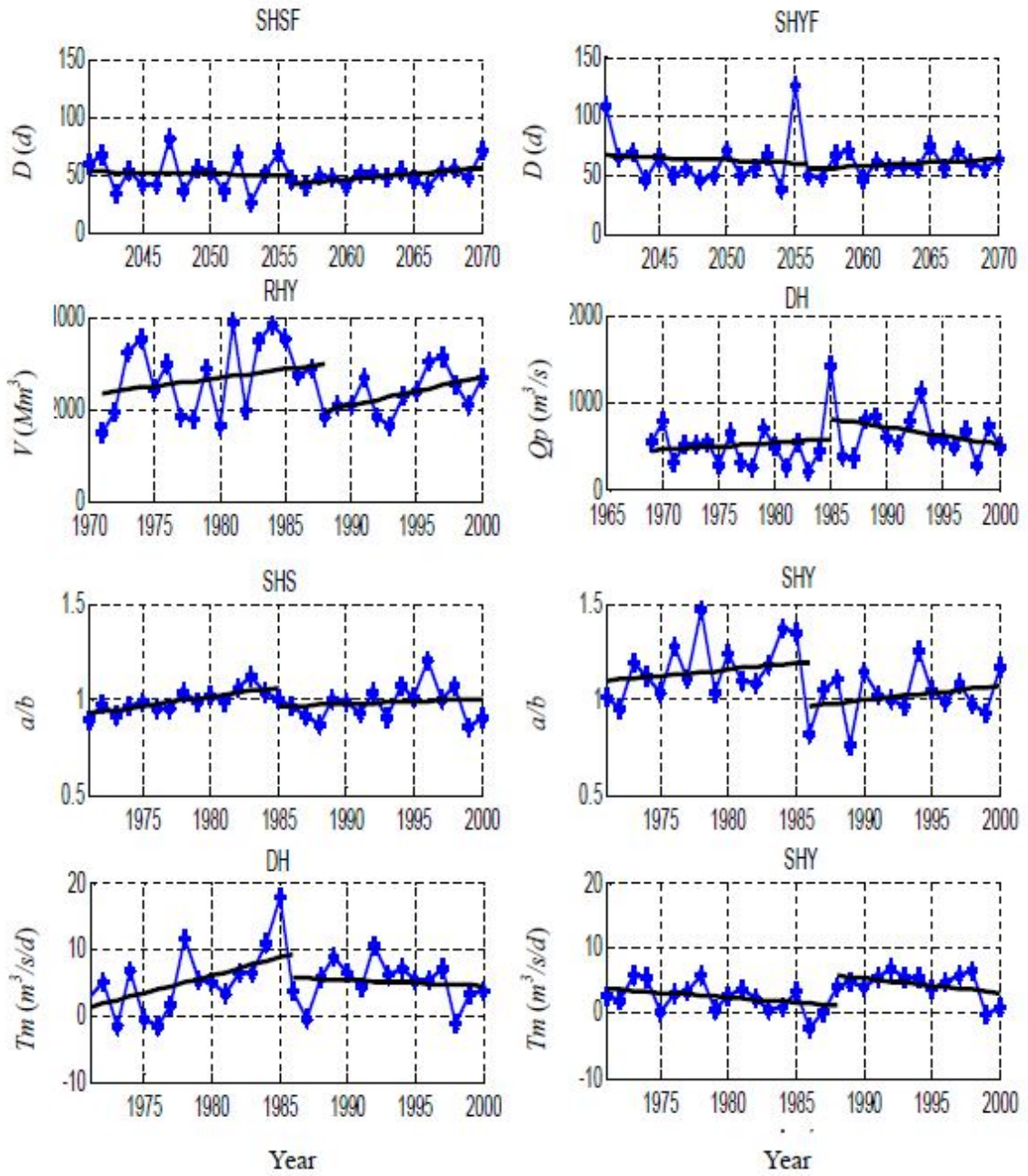
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Figure 5 : Non-stationary in fall flood peak and associated trends: a) RHS, b) SHSF, c) RHY and d) SHYF. The dashed line represents the corresponding trend of each series.



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Figure 6: Detected break-points in the considered series