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# Nanomechanics of flexoelectric switching

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We examine the phenomenon of flexoelectric switching of polarization in ultrathin films of barium titanate induced by a tip of an atomic force microscope (AFM). The spatial distribution of the tip-induced flexoelectricity is computationally modeled both for perpendicular mechanical load (point measurements) and for sliding load (scanning measurements), and compared with experiments. We find that (i) perpendicular load does not lead to stable ferroelectric switching in contrast to the load applied in the sliding contact load regime, due to nontrivial differences between the strain distributions in both regimes: ferroelectric switching for the perpendicular load mode is impaired by a strain gradient inversion layer immediately underneath the AFM tip; while for the sliding load regime, domain inversion is unimpaired within a greater material volume subjected to larger values of the mechanically induced electric field that includes the region behind the sliding tip; (ii) beyond a relatively small value of an applied force, increasing mechanical pressure does *not* increase the flexoelectric field inside the film, but results instead in a growing volume of the region subjected to such field that aids domain nucleation processes; and (iii) the flexoelectric coefficients of the films are of the order of few nC/m, which is much smaller than for bulk BaTiO<sub>3</sub> ceramics, indicating that there is a “flexoelectric size effect” that mirrors the ferroelectric one.

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**I. INTRODUCTION**

Ferroelectric materials are characterized by the presence of a spontaneous polarization that can be switched by application of an external electric field. Recently, a mechanical switching of polarization was also demonstrated [1]. The driving mechanism of the mechanically induced polarization switching is thought to be the flexoelectric effect [2]—a linear coupling between polarization and a strain gradient, which allows control of not only the polarization magnitude but also its orientation. In bulk materials, flexoelectric effects are generally small because large strain gradients are difficult to achieve without fracture or permanent deformation. Conversely, at the nanoscale, strain gradients can acquire extremely large magnitudes leading to giant flexoelectric effects [3–5]. The importance of flexoelectricity for nanodevices has largely contributed to the current surge of interest in this effect that had been known for nearly half a century [2,6].

Despite considerable research in the last decade (see several monographic reviews for Refs. [7–10]) the true magnitude and nature of the flexoelectric coefficients of most materials is only now beginning to be understood [11–14]. Crucially, it is not known whether the large flexoelectric coefficients of archetypal ceramics such as BaTiO<sub>3</sub> (BTO) remain equally large at the nanoscale. This is a critical question because it is at the nanoscale where gradient-induced effects are most important and likely to be useful, so, if we are to exploit them, we need to know the flexoelectric coefficients at the nanoscale. These may not necessarily be the same as in bulk: note, for example, that the dielectric constant of ferroelectric thin films is much smaller than that of bulk, and flexoelectricity is linearly proportional to permittivity [2]. Our work seeks to answer this question, namely, can we quantify the value of

the flexoelectric coefficients in ferroelectric thin films? We demonstrate that reasonable fitting of the experimental results in BaTiO<sub>3</sub> thin films can be achieved only for flexoelectric coefficients of the order of 1 nC/m. This is in contrast to bulk BaTiO<sub>3</sub>, where the flexoelectric coefficients are of the order of 1  $\mu$ C/m, confirming that there is indeed a “flexoelectric size effect” that mirrors the ferroelectric one.

Of equal importance for understanding the mechanically induced ferroelectric switching is the analysis of the actual distribution of the strain gradient. Strain and stress fields produced by a tip of an atomic force microscope (AFM) are much more complex than those associated with pure bending or twisting, and can lead to nontrivial physical effects. In this work, we have established that (i) the mechanical switching process is controlled by critical domain size rather than by critical field; and that (ii) there is a fundamental difference in the strain gradient distributions generated in the normal and sliding load modes so that the former leads to small and unstable domains, while the latter results in more stable domains.

**II. EXPERIMENTS**

We have quantified the flexoelectric behavior in ultrathin BTO films by establishing a correlation between the mechanical load and equivalent electric bias. The samples studied were single-crystalline epitaxial ultrathin BTO films, grown on atomically smooth TiO<sub>2</sub>-terminated (001)-SrTiO<sub>3</sub> substrate with a 30-nm-thick La<sub>0.67</sub>Sr<sub>0.33</sub>MnO<sub>3</sub> layer acting as bottom electrode. Both layers were grown using pulsed laser deposition with *in situ* monitoring using high pressure reflection high energy electron diffraction for thickness control; details of sample preparation can be found elsewhere [1]. The

switching experiments were performed on 12-unit-cell (u.c.)-thick films ( $\sim 5$  nm). The compressively strained BTO thin films were fully coherent with the substrate and possessed only out-of-plane polarization [15]. The flexoelectric switching was studied using a commercial AFM system (MFP-3D, Asylum Research).

Flexoelectric measurements have been performed using two modes of mechanical pressure induced by the AFM tip. In one mode—the sliding contact load mode—the BTO film surface has been scanned with the tip under an incrementally increasing loading force from 100 to 1000 nN, while applying a dc voltage to the tip (this bias ranging from  $-0.4$  to  $1.2$  V was fixed during scanning). Note that for all measurements the external dc bias was below the coercive bias estimated from the piezoresponse force microscopy (PFM) hysteresis loop ( $1.2$  V for 12-u.c.-thick film [1]) and by itself could not cause polarization reversal. Scanning under mechanical load was followed by visualization of the resulting domain patterns using conventional PFM with a low load force of 25 nN. In the normal load mode, we have used an AFM tip at a fixed position on the BTO film surface to measure the local PFM hysteresis loops for different values of the loading forces.

In Fig. 1(a), it can be seen that application of an increasing force in the sliding contact load mode eventually leads to the reversal of the initial upward (away from the electrode) polarization state to the downward state. The threshold force, at which the PFM phase contrast in Fig. 1(a) is inverted (which also corresponds to the minimum in the PFM amplitude), varies with the applied dc bias, i.e., the force required for switching the polarization from “up” to “down” decreases or increases, respectively, depending on whether the voltage applied to the tip is positive or negative.

We interpret these results in terms of cooperation or competition between the external electric bias and the mechanically induced voltage. This mechanical voltage is an effective measure of the complex electric field produced by pressure-induced piezoelectricity plus the strain-*gradient*

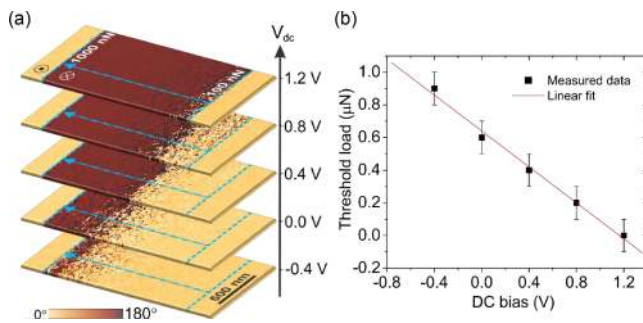


FIG. 1. (Color online) (a) PFM phase images of 12-u.c.-thick BaTiO<sub>3</sub> film after mechanical writing in the area marked by the lines with at a fixed dc voltage  $V_{\text{ex}}$  applied to the tip. Mechanical load was increasing during scanning from 100 to 1000 nN in the direction marked by a dashed arrow. Polarization switches downward as mechanical load increases. Positive dc bias assists polarization switching to the downward direction and negative dc bias opposes it. The threshold load is defined as a load at which phase contrast is inverted. (b) A plot of the threshold load  $F_{\text{th}}$  as a function of the tip voltage obtained using data in (a).

induced flexoelectricity, which varies depending on film thickness, loading mode (sliding vs perpendicular contacts), and tip conductivity. Notice, however, that the piezoelectric contribution always reduces the coercive voltage due to the vertical pressure-induced reduction of tetragonality [16], whereas the flexoelectric contribution can either increase or decrease the required external coercive voltage depending on whether the flexoelectric polarization is parallel or antiparallel to the ferroelectric polarity. Note also that, since the piezoelectric effect can only reduce preexisting polarity, it cannot cause ferroelectric switching, meaning that mechanical switching of polarization is controlled by the flexoelectric contribution. The condition for mechanically induced switching can be expressed as  $V_{\text{fl}}(F) \geq V_c$ , where  $V_{\text{fl}}(F)$  is the flexoelectric voltage for a given value of the tip-applied mechanical force  $F$  and  $V_c$  is the coercive voltage of the film. At the threshold load  $F_{\text{th}}$  the flexoelectric voltage is equal to the coercive bias:  $V_{\text{fl}}(F_{\text{th}}) = V_c$ . When a small (below  $V_c$ ) external dc voltage  $V_{\text{ex}}$  is applied during mechanical writing, the general condition for polarization reversal can be expressed as  $V_{\text{fl}}(F) + V_{\text{ex}} \geq V_c$  so that the flexoelectric voltage corresponding to the threshold load can be found from  $V_{\text{fl}}(F_{\text{th}}) + V_{\text{ex}} = V_c$ . By measuring the threshold load  $F_{\text{th}}$  as a function of the external voltage  $V_{\text{ex}}$ , we establish a relationship between the applied load  $F$  and the flexoelectrically generated voltage  $V_{\text{fl}}$ . A plot in Fig. 1(b) shows a linear relationship between the external dc bias  $V_{\text{ex}}$  and the threshold load  $F_{\text{th}}$  with a proportionality coefficient of  $1.8$  V/ $\mu\text{N}$ .

An alternative and somewhat more direct way to calibrate the flexoelectric voltage is based on scanning the film surface with incrementally increasing a dc bias applied to the tip while maintaining a constant mechanical load. In this case switching to the upward polarization state will occur at the threshold dc bias  $V_{\text{th}}$ , which is measured experimentally, and the flexoelectric voltage can be found from  $V_{\text{fl}}(F) + V_{\text{th}} = V_c$ . At the mechanical load close to zero,  $V_{\text{fl}} = V_c$  (in reality, we take the value of  $V_{\text{th}}$  at the mechanical load of 30 nN as being equal to  $V_c$ ). A series of the domain patterns generated using this approach are shown in Fig. 2(a), while Fig. 2(b) shows the threshold voltage  $V_{\text{th}}$  and the calculated flexoelectric voltage

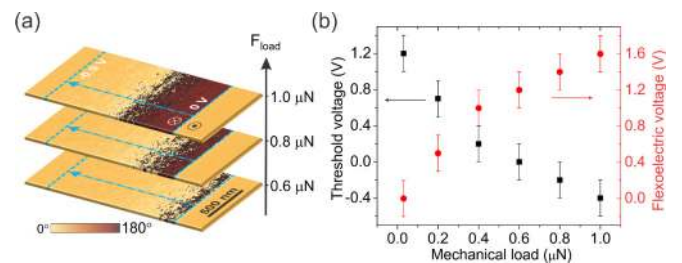


FIG. 2. (Color online) (a) PFM phase images of 12-u.c.-thick BaTiO<sub>3</sub> film after electrical writing at a fixed mechanical load in the area marked by the dashed lines. Electrical bias was changing during scanning in the direction marked by a dashed arrow. Polarization switching is stopped as negative dc bias increases. (b) Plots of the experimentally measured threshold voltage bias and calculated flexoelectric voltage as a function of the mechanical load. For mechanical load below 600 nN, an increasing positive bias is applied to induce polarization switching.

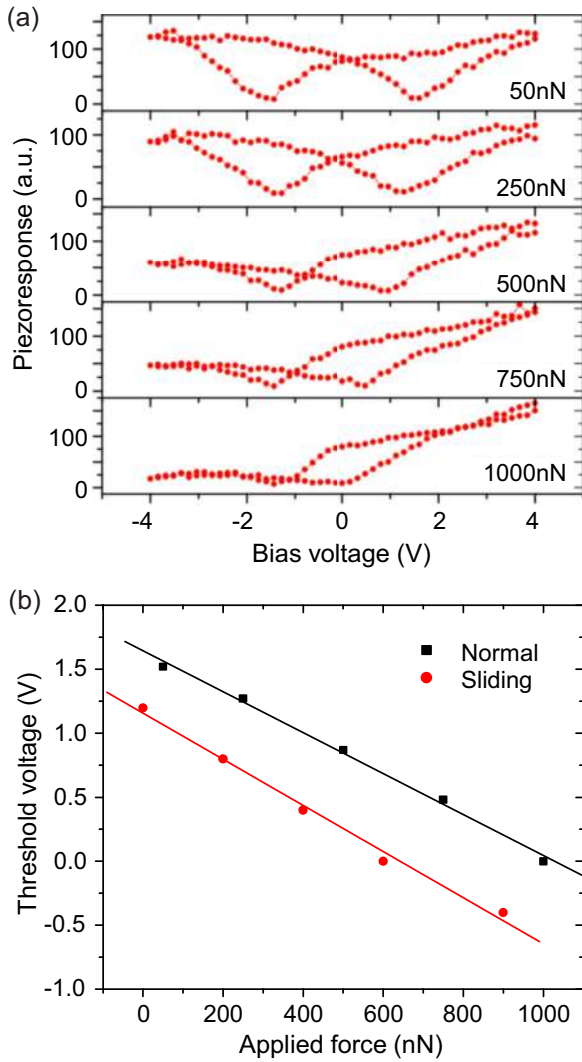


FIG. 3. (Color online) (a) PFM hysteresis loops acquired under different normal loading forces. Note that for the highest force, one of the coercive voltages is zero, indicating that the mechanically induced bias is sufficient to switch to the downward state. (b) Comparison between the threshold voltages required for switching polarization from the upward to the downward state for sliding (scanning) and normal load modes.

$V_{th}$  as a function of mechanical load  $F$ . It can be seen that  $V_{th}$  decreases monotonically as the mechanical load increases, and even becomes negative at a sufficiently high load, indicating that the tip-generated flexoelectric voltage becomes larger than  $V_c$ . A slight nonlinearity of the slope in this case is likely caused by tip wear. Note that at the load of 600 nN, the external voltage required to switch the polarization is exactly  $V_{ex} = 0$ : this implies that, at this mechanical load, the flexoelectric voltage equals the coercive voltage of the film.

The above measurements have been performed in the scanning mode, where in addition to the normal force, friction between the tip and the film generates tangential forces. It is useful to compare these results with those of measurements done in the other mode—normal loading mode, where the load is applied through a tip fixed at a certain point on the surface. In this case, the tangential forces are absent. Experimentally,

however, we found that perpendicular indentation leads to small and unstable domains, so graphic analysis of polarization maps such as those of Fig. 1 was not possible. Instead, we have analyzed the point measurements of the PFM hysteresis loops obtained at different loading forces. In Fig. 3(a), it can be seen that with increase in the loading force the PFM loops become more asymmetric and shift along the horizontal axis (bias) toward the negative voltages. Both the shift and the asymmetry are necessarily associated with the strain gradients. The off-centering of the loop, just like in the scanning mode, is a direct measure of the flexoelectrically induced voltage, while the asymmetry of the PFM loop wings reflects the fact that the PFM signal is amplified when ferroelectric and strain-induced (flexoelectric) polarizations are parallel (i.e., when the total polarization of the film is high) and reduced when they are antiparallel.

In Fig. 3(b) we plot the applied force dependence of the threshold voltage for two different loading regimes. In the normal load regime, the threshold voltage is always higher, indicating that sliding contacts are more efficient in generating flexoelectric voltage and inducing ferroelectric switching. The conversion factor from force into voltage is about  $1.8 \text{ V}/\mu\text{N}$  for both regimes. The reasons for this difference will be discussed in the next section.

### III. SIMULATIONS

In order to explain the experimental observations, it is necessary to calculate the tip-induced strain gradients, associated flexoelectric polarizations, and electrostatic field distributions. For this, we turn to finite element (FE) simulations performed for a spherical elastic contact between a rigid AFM tip with radius of 30 nm (consistent with the value measured with high-resolution field-emission scanning electron microscopy for the tips used in the experiments) and a 12-u.c.-thick BTO film on a  $\text{La}_{0.67}\text{Sr}_{0.33}\text{MnO}_3$  substrate. We used elastic stiffness moduli  $C_{11} = 166 \text{ GPa}$ ,  $C_{12} = 76 \text{ GPa}$ , and  $C_{44} = 42 \text{ GPa}$  for BTO [17] and  $C_{11} = 180 \text{ GPa}$ ,  $C_{12} = 100 \text{ GPa}$ , and  $C_{44} = 56 \text{ GPa}$  for  $\text{La}_{0.67}\text{Sr}_{0.33}\text{MnO}_3$  [18]. For simplicity, the  $\text{La}_{0.67}\text{Sr}_{0.33}\text{MnO}_3$  interlayer used as electrode is assumed to be infinitely thick, which approximates sufficiently well to the elastic boundary condition of the experiments. Complementary simulations were performed for the case of the 12-u.c.-thick BTO film placed on top of a much stiffer  $\text{SrTiO}_3$  (STO) substrate with  $C_{11} = 421 \text{ GPa}$ ,  $C_{12} = 122.1 \text{ GPa}$ , and  $C_{44} = 133.2 \text{ GPa}$ . The purpose of these simulations was to assess the role of an increased elastic contrast between the film and the substrate in flexoelectric nanocontacts. Normal as well as sliding loading modes were modeled under increasing applied loads up to a maximum of 1000 nN. Coulombian friction coefficients  $\mu = 0, 0.2, \text{ and } 0.3$  were considered in the modeling of sliding contacts [19–21].

The following scheme was employed. The strain gradients were first computed from the nodal values in the FE mesh, while the strain gradients were computed by recourse to the shape functions of the quadrilateral elements. Linear flexoelectricity was then invoked, providing all strain gradients in the film, such that

$$P_i = \mu_{ijkl} e_{jk,l}, \quad (1)$$



where  $P_i$  is the polarization vector along the  $i$  axis,  $e_{j,k,l}$  is the derivative along the  $x_l$  direction of the Lagrangian strain tensor,  $\mu_{ijkl}$  is the fourth-rank tensor of flexoelectric coefficients, and subindices  $i, j, k, l$  vary from 1 to 3. In all tensor coefficients in this article,  $x_1$  and  $x_2$  are the in-plane directions, and  $x_3$  is the out-of-plane (indentation) direction. Following the analysis outlined in the Appendix, the components of the polarization vector along the three material axes become

$$P_1 = \mu_{1111} \frac{\partial e_{11}}{\partial x_1} + \mu_{1122} \left( \frac{\partial e_{22}}{\partial x_1} + \frac{\partial e_{33}}{\partial x_1} \right) + 2\mu_{1212} \left( \frac{\partial e_{12}}{\partial x_2} + \frac{\partial e_{13}}{\partial x_3} \right), \quad (2a)$$

$$P_2 = \mu_{1111} \frac{\partial e_{22}}{\partial x_2} + \mu_{1122} \left( \frac{\partial e_{11}}{\partial x_2} + \frac{\partial e_{33}}{\partial x_2} \right) + 2\mu_{1212} \left( \frac{\partial e_{12}}{\partial x_1} + \frac{\partial e_{23}}{\partial x_3} \right), \quad (2b)$$

$$P_3 = \mu_{1111} \frac{\partial e_{33}}{\partial x_3} + \mu_{1122} \left( \frac{\partial e_{11}}{\partial x_3} + \frac{\partial e_{22}}{\partial x_3} \right) + 2\mu_{1212} \left( \frac{\partial e_{13}}{\partial x_1} + \frac{\partial e_{23}}{\partial x_2} \right). \quad (2c)$$

The flexoelectric coefficients  $\mu_{ijkl}$  are not known with certainty, and even for bulk single crystals there are orders of magnitude discrepancies between experiment and theory. Here, we use the more conservative theoretical results from the first-principles calculations:  $\mu_{1111} = 0.37$  nC/m [22],  $\mu_{1122} = 5.5$  nC/m [23], and  $\mu_{1212} = 1.9$  nC/m [23]; this choice is validated by comparison with our experimental results. The small value of the flexoelectric coefficients for thin films is precisely one of the central results of this work.

Since the entire strain gradient field is known from the above simulations, the charge density at all nodal points of the FE mesh representing the BTO film are subsequently computed through

$$q = -\nabla \cdot P_i. \quad (3)$$

Such charge density distribution is then introduced in a final finite element analysis where Maxwell's equations are solved for the electrical boundary conditions imposed by the spherical tip, thus providing the total three-dimensional electric field inside the thin film. In doing so, we assume that the relative permittivity of the film,  $\epsilon_r = 30$  (see Sec. IV C). In the latter computations, the substrate is grounded and the indenter is taken to exhibit either conductive or insulating properties. In the case of conductive tips, Maxwell's equations are solved for imposed boundary voltage values ranging from  $-1.0$  to  $+1.0$  V (in steps of 0.1 V). Boundary voltage conditions at the contact surface are not imposed when modeling the response of insulating tips.

Figure 4 shows the flexoelectric field distribution under the tip, for insulating and conductive tips. In both cases, the peak value of the negative (downward oriented) electric field,  $E_p$ , in the vertical  $x_3$  direction is found at  $0.6r$  underneath the center of contact, where  $r$  is the contact radius. Immediately underneath the tip apex, however, a strong positive (upward) field is induced, which opposes domain inversion (note the region colored in red in Fig. 4). This region of inversion

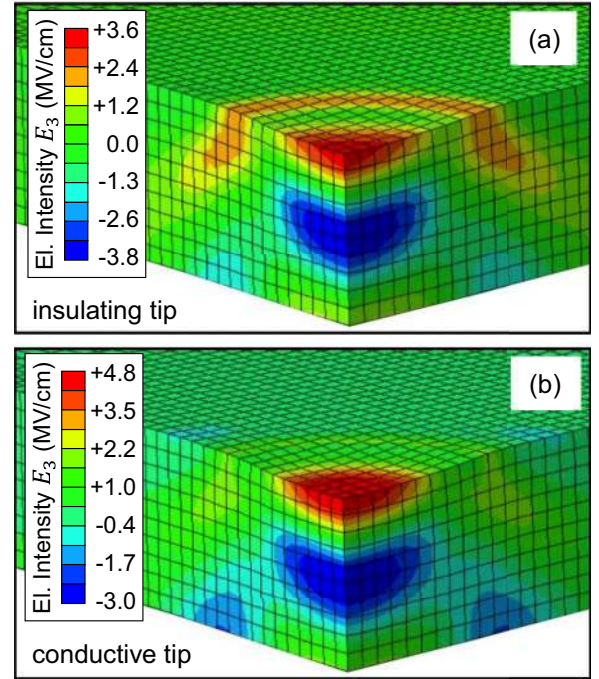


FIG. 4. (Color online) Isocontours of the total field in the vertical direction ( $E_3$ ) for an applied contact load of 500 nN (normal mode). (a) Insulating (nonscreening) tip and (b) conductive tip at 0 V of imposed bias. Regions colored in red indicate the presence of strain gradients opposing domain switching, whereas the maximum flexoelectric field value  $E_p$  is located at the central region colored in blue. The size of one quadrilateral element matches that of 1 u.c. in BaTiO<sub>3</sub>. The same color code is used in (a) and (b).

probably explains the observed instability of domains written by pure normal indentation. The maximum downward field value,  $E_p$ , is 20% smaller for conductive than that for insulating tips under the same applied indentation load, demonstrating the sensitivity of the flexoelectric field to the electrical boundary condition, and suggesting that insulating tips may in fact be better for purely mechanical switching.

The field distribution along the vertical direction directly under the tip apex, plotted in Fig. 5, also shows that, for any given normal mechanical load, the contact area is under a positive (upward oriented) field while a negative field is concentrated a couple of nanometers below. A key finding [Fig. 5(a)] is that increasing mechanical load does not result in a stronger negative field, but in a larger volume fraction of the film being subjected to such negative field, thus indicating that the switching is controlled by critical nucleus size rather than by intensity of local field. By contrast, if we increase the external voltage while maintaining a fixed amount of pressure [Fig. 5(b)], both the nucleus size and the intensity of the negative field do increase. Mechanical load and applied voltage thus generate very different field distributions.

Meanwhile, the field distribution for the sliding contact load regime (Fig. 6) shows a qualitatively new and very important feature: the negative flexoelectric field exists both underneath the tip-sample contact point (as described above) *and* in the material volume trailing behind the sliding tip (Fig. 6). Importantly, while the region of negative field vertically under

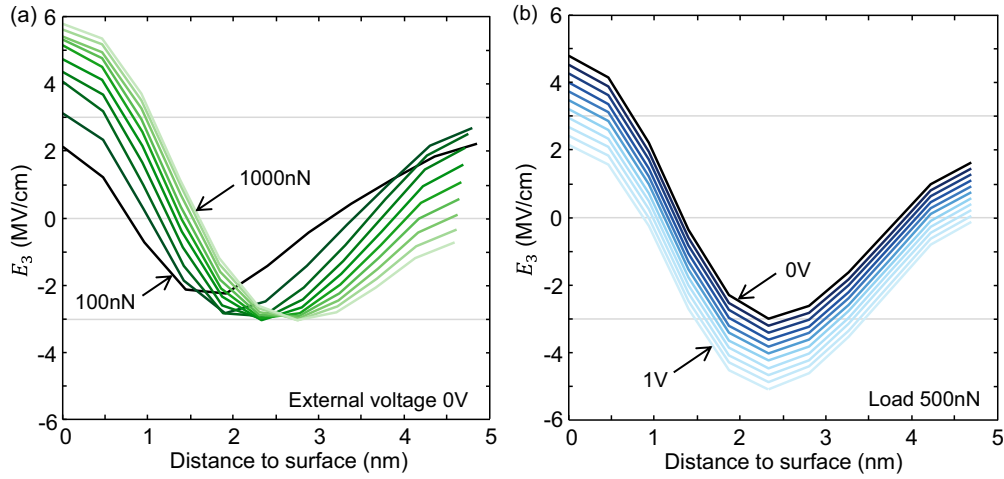


FIG. 5. (Color online) Distributions of the electric field  $E_3$  along a vertical path underneath the contact center for the normal load regime using a conductive tip. Part (a) shows that, in the absence of external voltage, the peak negative field  $E_p$  is almost the same ( $\sim 3$  MV/cm) for any value of mechanical load. (b) Influence of the external voltage upon the distributions of total field for the mechanical load of 500 nN. Consecutive curves are 100 nN apart in (a) and 0.1 V apart in (b).

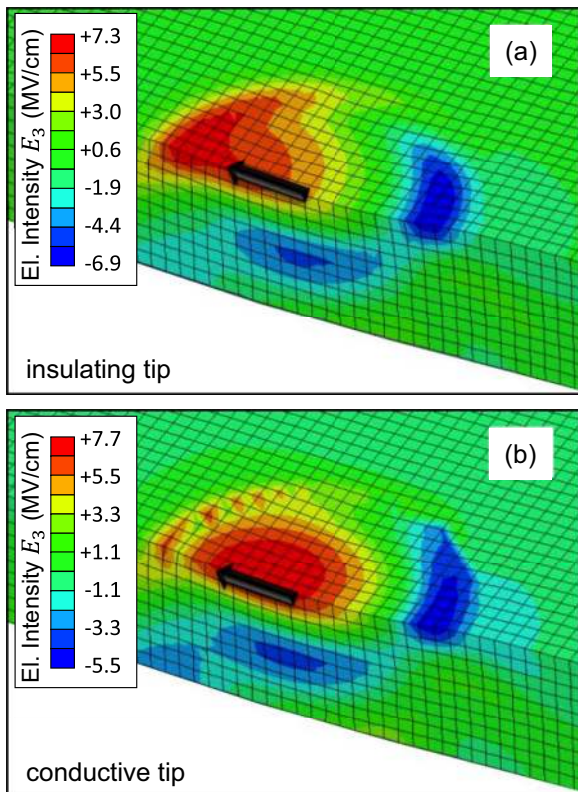


FIG. 6. (Color online) Isocontours of total electric field  $E_3$  for a sliding contact load regime for (a) isolating tip and (b) conductive tip at 0 V of applied voltage. Simulations are made for the Coulombian friction coefficient  $\mu = 0.3$  and vertical load of 500 nN. Black arrow denotes the sliding direction. The strain gradients in the regions colored in red produce positive (upward) electric field, which opposes flexoelectric switching, while domain nucleation occurs under the negative field (blue regions). The size of one quadrilateral element matches that of 1 u.c. in BaTiO<sub>3</sub>. The same color code is used in (a) and (b).

the tip is still partially offset by the positive field in the contact region, the trailing negative field induced under sliding conditions is not offset by any positive field and should thus prevail. Moreover, for sliding contacts with Coulomb's friction coefficient of  $\mu = 0.3$ , the  $E_p$  value underneath the tip increased by  $\sim 50\%$  as compared to that developing for perpendicular contacts, and in addition the material volume subjected to the peak  $E_p$  level is three times greater for the sliding mode. These results thus explain the greater ease with which stable domains can be written in sliding mode compared to perpendicular indentation.

#### IV. DISCUSSION

The principal features of the experiment (magnitude of the effect, greater writing ability for sliding as compared to normal indentation) are well reproduced and explained by the computations. There are, however, a few aspects that require further discussion, namely, (i) flexoelectric switching appears to occur due to the expansion of the downwardly polarized region beyond a certain critical volume rather than due to the increase in the strength of the downward oriented flexoelectric field; (ii) the maximum applied loads are high enough to induce a localized transition to the paraelectric phase; and (iii) though the order of magnitude of the flexoelectric coefficients is known, the accuracy and relative weight of the different flexoelectric components needs to be examined. We discuss these issues in this section.

##### A. Domain nucleation and critical volume for polarization reversal

Switching in ferroelectrics proceeds through domain nucleation and growth [24–27]: nucleation of a critical domain size with downward polarization precedes overall switching across the film thickness so that the free energy of the film is reduced as the nucleated domain expands. Our simulations show that an increase in applied mechanical load results

in a greater material volume subjected to the peak value of the flexoelectric field  $E_p$ . Experimentally, we know that the coercive voltage in the (relative) absence of pressure is approximately 1.5 V (corresponding to 3 MV/cm of electrical field). In our simulations (Fig. 4), this field value defines an isocontour of  $0.9 \times E_p$ , circumscribing a material volume of  $\sim 4 \text{ nm}^3$ . For spherical nuclei, this volume translates to a critical radius  $r_c \sim 1.0 \text{ nm}$  that encompasses  $\sim 32$  unit cells.

Following the analysis in Ref. [26], the thermodynamics of domain nucleation processes is described by

$$U = -2PEv + \gamma_s s + U_d, \quad (4)$$

where  $U$  is the total free energy of the film; the first term in the right-hand side is the energy decrease driving domain nucleation, which contains the magnitudes of the electric field  $E$  and polarization  $P$  within a nucleated domain with volume  $v$ ;  $\gamma_s$  is the surface energy of the domain walls for nuclei with surface area  $s$ ; and  $U_d$  is the depolarization energy imposed by the surrounding material. The saddle point in the energy landscape therefore describes the critical radius of the nucleated domain in accordance with  $(dU/dr) = 0$ . For nuclei with spherical shape, the critical domain radius becomes

$$r_c = \gamma_s / PE. \quad (5)$$

Using the computed peak values of  $E_p$ , associated  $P$  and  $\gamma_s = 17 \text{ mJ/m}^2$  for domain walls in  $\text{BaTiO}_3$  [26,28], Eq. (5) yields  $r_c \sim 0.4 \text{ nm}$  so that the critical volume  $v_c$  encompasses  $\sim 8$  u.c. This estimate is of the same order as the radius circumscribed by the aforementioned assessment using the peak flexoelectric field isocontours from the FE simulations, thus reinforcing the assumption that the flexoelectric coefficients in the nanoscale are of the order of nC/m rather than of the order of  $\mu\text{C/m}$ . Flexoelectric coefficients of several orders of magnitude greater would have rendered markedly larger values for  $E_p$  and associated  $P$  in the FE simulations, sharply decreasing inferred  $r_c$  through Eq. (5). As a matter of fact, the calculated critical nucleus size would be an unrealistic and unphysical subatomic length.

Meanwhile, the simulations for sliding contact mode indicate that domain switching is simultaneously induced behind and underneath the AFM tip where the isocontour of maximum  $E_p$  is reached (Fig. 6). Regions of the film located in front and immediately underneath the sliding tip are, however, subjected to a strain gradient opposing domain expansion. As the material is placed behind the tip during sliding, the aforementioned strain gradients opposing domain switching are removed and hence a critical nucleated domain is allowed to expand. This produces overall switching across the film thickness. The role of the Coulombian friction coefficient  $\mu$  is crucial in the proposed mechanism: a decrease in  $\mu$  gradually reduces the strain gradients that build in front and behind the tip, where the isocontours of flexoelectric field for normal and sliding modes converge at  $\mu = 0$ .

### B. Tip-induced transition through the paraelectric phase

Under sufficient uniaxial compression, the tetragonality is so suppressed that a localized transition to the paraelectric phase is, in principle, possible. At the maximum applied load of 1000 nN, the top surface layer in contact with the

AFM tip is subjected to an extreme triaxial stress field where the vertical compressive stress reaches  $\sigma_{33} \sim -16 \text{ GPa}$  and the transverse (radial) confining stress approximates to  $\sigma_{11} (= \sigma_{22}) \sim -11 \text{ GPa}$ . The tetragonal structure is preserved in the top surface layer in contact with the AFM tip up to 900 nN because of the confinement provided by the aforementioned extreme radial compressive stresses. In contrast, in the central region of the film where the maximum value of  $E_p$  is located, we find  $\sigma_{33} \sim -16 \text{ GPa}$  and  $\sigma_{11} \sim -2 \text{ GPa}$  for the maximum applied load of 1000 nN. Superposition of the substrate-induced elastic misfit strain of  $-2.5 \times 10^{-2}$  to such mechanical solicitations [16,29] results in vanishing tetragonality and transition toward the paraelectric phase in the central region of the film for applied loads in excess of  $\sim 400 \text{ nN}$ . The results suggest that the inversion of polarization at the highest loads may be indirect and mediated through a biased paraelectric phase.

### C. Influence of flexoelectric anisotropy and scaling issues

Another question concerns the relative weight of  $\mu_{1111}$ ,  $\mu_{1122}$ , and  $\mu_{1212}$  when coupled to the specific strain gradients. We can rewrite Eq. (3) with the components of the polarization vector in Eq. (2), where

$$q = \mu_{1111} M_I + \mu_{1122} M_{II} + \mu_{1212} M_{III} \quad (6)$$

and

$$M_I = e_{11,11} + e_{22,22} + e_{33,33}, \quad (7a)$$

$$M_{II} = e_{11,22} + e_{11,33} + e_{22,11} + e_{22,33} + e_{33,11} + e_{33,22}, \quad (7b)$$

$$M_{III} = 4(e_{12,12} + e_{13,13} + e_{23,23}). \quad (7c)$$

Therefore, the coefficient  $\mu_{1111}$  weights the derivative of normal strain gradients along the normal directions ( $e_{ii,ii}$ );  $\mu_{1122}$  weights the derivative of normal strain gradients along transverse directions (the specific above values of  $e_{ii,jj}$ ); and  $\mu_{1212}$  weights the derivative of the shearing strain gradients (the specific above values  $e_{ij,ij}$ ). The results in Fig. 7 show that flexoelectric switching is fundamentally driven by the latter derivative of shear strain gradients (coupled to  $\mu_{1212}$  through  $M_{III}$ ). Only if coefficients  $\mu_{1122}$  and  $\mu_{1111}$  are about

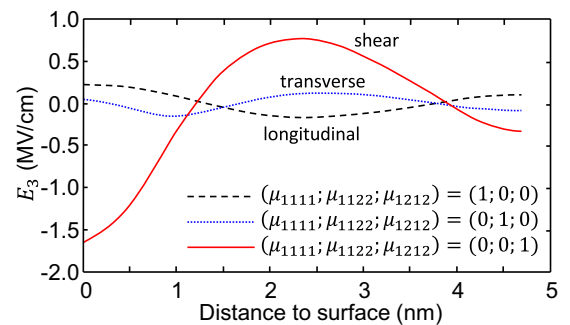


FIG. 7. (Color online) (a) Distributions of the total electric field  $E_3$  along the vertical path underneath the contact center described in Fig. 5. The results are for 500 nN, while the flexoelectric coefficients are systematically varied as shown in the legend. The results illustrate that flexoelectric nanocontacts are only sensitive to  $\mu_{1212}$ .



an order of magnitude greater than  $\mu_{1212}$  will their influence in domain switching be comparable.

An uncertainty in our modeling scheme concerns the role of surface piezoelectricity, which has been shown to be functionally equivalent to flexoelectricity [10]. This means that the employed flexoelectric coefficients are, in practice, the effective values that include both bulk flexoelectricity and surface piezoelectricity. From a quantitative point of view, of greater consequence is the fact that the model used here is not self-consistent: the strain gradient is calculated as a purely elastic problem without accounting for the fact that the elastic results would themselves be affected by the electric field. Strictly speaking, these values are mutually interdependent and should be calculated simultaneously as a coupled problem. The present model, however, still manages to transparently capture all the important features of the problem, and good quantitative agreement with the experiment is obtained using realistic parameters.

The agreement between experiments and simulations is achieved for the flexoelectric coefficients in the order of 1–10 nC/m. Yet, in bulk BaTiO<sub>3</sub> ceramics, the reported experimental flexoelectric coefficients are of the order of 1–10  $\mu$ C/m [30]. So, why is the flexoelectric coefficient of thin films so small? There is a concern that the flexoelectric coefficient of bulk ceramics is in fact anomalously large, and recent works suggest contribution of several extrinsic mechanisms to the total value [11–13]. Once these contributions are factored out, the intrinsic flexoelectric coefficient is a number of the order of 1–10 V multiplied by the permittivity of the material, i.e.,  $1-10 \times \epsilon_r \epsilon_0$  [10,30]. For BTO ceramics, the relative permittivity is of the order of  $\epsilon_r = 1000-30\,000$  depending on the proximity to the ferroelectric phase transition, and thus the flexoelectric coefficient that one should expect in bulk is of the order of  $\sim 0.1 \mu$ C/m, which is still about 100 times greater than we observe in our films.

These results, however, can be readily reconciled by observing that the relative permittivity along the  $c$  axis for BTO thin films epitaxially clamped on STO substrates is much smaller than for bulk: according to Landau theory calculations it is of the order of 30–50 [16]. Also, note that the value  $\epsilon_r = 30$  used in the present simulations yielded a good agreement with the experiment. Hence, the riddle is solved: while the flexoelectric coefficient of our films seems anomalously small in comparison with bulk, the *flexocoupling* coefficient (flexoelectric coefficient divided by permittivity, which is the property that fundamentally relates the strain gradients to the electric field) is still the same, namely, a number between 1 and 10 V. This means that since the permittivity of thin films is much smaller than that of the bulk materials [31–33], the flexoelectric response is preserved in the nanoscale. Maximizing flexoelectricity at the nanoscale thus requires maximizing the dielectric susceptibility.

## V. CONCLUSIONS

The present comprehensive study of the experimental and theoretical aspects of flexoelectric switching yields several nontrivial and important conclusions. Below we summarize them:

(1) In perpendicular load experiments, a ferroelectric domain is nucleated when a critical strain gradient is achieved in a sufficiently large volume fraction of the material. However, the produced domain is unstable due to the existence of a surface layer where the strain gradient has the opposite sign of that at the region below.

(2) In the sliding contact load regime, due to the presence of the tangential strain gradient, the region in the wake of the tip has a net downward flexoelectric field that is not canceled by any inversion layer. Hence, the switching can be realized at lower applied mechanical loads in the sliding regime, where domain growth proceeds unimpeded and stable domains can be formed.

(3) At sufficiently large loading forces ( $\geq 400$  nN), the switching from the upward to the downward polarization may proceed through an intermediate transition to the paraelectric phase, caused by the large vertical compression exerted by the tip.

(4) The obtained results are consistent with flexoelectric coefficients being of the order of a few nC/m, in contrast to the  $\mu$ C/m in bulk BTO ceramics. Yet, when dividing these coefficients by the permittivity, the flexocoupling coefficients of the films are of the order of 1–10 V, which is the same as in bulk.

Though strain gradients can effectively replace voltage in order to switch ferroelectric polarization, the mechanically induced field distribution is very different from that, which would arise from just electrostatic voltage, and has to be exploited differently. In particular, while electrostatic domain switching with a static contact is possible, mechanical switching requires the larger shear stresses associated with sliding contacts—in other words, mechanical writing of lines or dashes is easier than writing of dots. Similarly, the scaling of flexoelectricity and permittivity means that one cannot automatically assume bulk values. Making efficient nanoscale flexoelectric devices requires not just careful strain gradient engineering, but also careful materials science in order to ensure the material properties are optimally translated to the nanoscale.

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## APPENDIX

Using the symmetry considerations by Shu [34] for cubic crystals, Eq. (1) can be strictly simplified as

$$P_i = \mu_{in} e_n,$$

where

$$\mu_{in}^{(3 \times 18)} = \begin{pmatrix} \mu_{1111} & 0 & 0 & \mu_{1122} & 0 & 0 & \mu_{1122} & 0 & 0 & 0 & 2\mu_{1212} & 0 & 0 & 0 & 2\mu_{1212} & 0 & 0 & 0 \\ 0 & \mu_{1122} & 0 & 0 & \mu_{1111} & 0 & 0 & \mu_{1122} & 0 & 2\mu_{1212} & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 2\mu_{1212} \\ 0 & 0 & \mu_{1122} & 0 & 0 & \mu_{1122} & 0 & 0 & \mu_{1111} & 0 & 0 & 0 & 2\mu_{1212} & 0 & 0 & 0 & 2\mu_{1212} & 0 \end{pmatrix}$$

and

$$e_n^{(18 \times 1)} = (e_{11,1} e_{11,2} e_{11,3} e_{22,1} e_{22,2} e_{22,3} e_{33,1} e_{33,2} e_{33,3} e_{12,1} e_{12,2} e_{12,3} e_{13,1} e_{13,2} e_{13,3} e_{23,1} e_{23,2} e_{23,3}).$$

This directly yields Eqs. 2(a), 2(b), and 2(c) from the main text.

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