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2 **Full Paper**

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5 **Negligible-Pb-Waste and Upscalable Perovskite Deposition Technology for High**
6 **Operational-Stability Perovskite Solar Modules**

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28 Abstract:

29 We report an upscalable perovskite film deposition method combining raster ultrasonic spray
30 (RUS) coating and chemical vapor deposition (CVD). Our method overcomes the coating size
31 limitation of the existing stationary spray, single-pass spray and spin-coating methods. In
32 contrast with the spin-coating method (>90% Pb waste), negligible Pb waste during PbI₂
33 deposition makes this method more environmentally friendly. Outstanding film uniformity
34 across the entire area of 5 cm × 5 cm is confirmed by both large area compatible characterization
35 methods (electroluminescence and scattered light imaging) and local characterization methods
36 (AFM, SEM, photoluminescence mapping, UV-vis and XRD measurements on multiple sample
37 locations), resulting in low solar cell performance decrease upon increasing device area. With
38 the FAPb(I_{0.85}Br_{0.15})₃ perovskite layer deposited by this method, champion solar modules show
39 a power conversion efficiency of 14.7% on an active area of 12.0 cm² and an outstanding shelf

1 stability (only 3.6% relative PCE decay after 3600 h aging). Under continuous operation (1 Sun
2 light illumination, maximum power point condition, dry N₂ atmosphere with <5% relative
3 humidity, no encapsulation) our devices show high light-soaking stability corresponding to an
4 average T₈₀ lifetime of 535 h on the small area solar cells and 388 h on the solar module.

5 6 **Introduction**

7 Over the past few years, there have been unprecedented advances in solar cells using metal
8 halide perovskite materials as light absorbers.¹⁻³ A record power conversion efficiency (PCE)
9 of 23.3% has been certified, already surpassing the well-established commercial photovoltaic
10 technologies e.g., multi-crystalline silicon (22.3%), thin film CIGS (22.6%) and CdTe
11 (22.1%).⁴ Substantial efforts have also been made to solve other potential issues that may limit
12 the commercialization of this new technology. Less toxic elements (e.g., Sn²⁺, Bi³⁺, Ag¹⁺, Sb³⁺)
13 are being tested to replace Pb²⁺, and PCE has reached 9%.⁵⁻¹² Device stability is significantly
14 improved by optimizing the device structure,¹³⁻¹⁷ perovskite composition¹⁸ and deposition
15 technologies¹⁹⁻²¹. Research focus is now shifting to development of reliable perovskite
16 deposition technologies that would allow mass production in industry. To manufacture products
17 with commercially viable module size and yield, the factors that are often ignored in making
18 small-size cells in research labs can have a strong impact on levelized cost of electricity (LCOE)
19 and must be considered.²²⁻²⁵ These factors include (i) solar cell PCE should be maintained or
20 only decrease slightly upon increasing the active area from the small solar cell scale (active area
21 ~ 0.1 cm²) towards the solar module scale (> active area ~ 10 cm²); (ii) Pb waste should be
22 minimized during the deposition process; (iii) the perovskite film deposition methods should
23 be transferable to industry.

24 Considering these factors, the methods developed in research labs may not be all suitable for
25 mass production. For example, most high-performing perovskite solar cells (PCE >20%) are
26 prepared by the anti-solvent based spin-coating method on small active areas (~ 0.1 cm²).

1 However film uniformity becomes significantly poorer upon increasing the active area to a
2 module scale due to the short precursor-processing window, leading to decreased device
3 performance and reproducibility.²⁶⁻²⁸ The inherently high Pb waste (> 90%) during the spin-
4 coating process,²⁹ the associated cost of waste disposal, and the environmental impact also
5 make this method unsuitable. On the basis of these considerations, a series of scalable
6 perovskite deposition technologies are being developed including blade coating,^{26, 30-31} slot die
7 coating,³² spray coating,³³⁻⁴¹ ink-jet printing,⁴² screen printing,⁴³ chemical vapor deposition,⁴⁴⁻
8 ⁴⁵ pressure-processed coating⁴⁶ etc. However, devices based on these technologies typically
9 show much lower PCEs than those achieved in research labs on small size cells. Perovskite
10 films coated using these technologies are formed either by a one-step or a sequential conversion
11 process. Remeika *et al.* reported that the sequential conversion shows clear advantages over
12 one step deposition in the scalable technologies because functional film formation is separated
13 from film coating, allowing separate optimization of the two processes.²⁹

14 In this work we develop an upscalable perovskite deposition technology combining raster
15 ultrasonic spray coating and chemical vapor deposition (RUS-CVD). FAPb_xBr_{3-x} (FA =
16 formamidinium) perovskite films are deposited on FTO/ c-TiO₂ substrates via a sequential
17 deposition method (**Figure 1A**). First, PbI₂ films are prepared by raster ultrasonic spray-coating
18 (RUS) using a precursor solution containing a solvent mixture of DMF and DMSO (Figure 1B
19 and movie S1). PbI₂ films are converted to FAPb_xBr_{3-x} by CVD in the vapor of formamidinium
20 iodide (FAI), formamidinium bromide (FABr) and methylammonium chloride (MACl) (Figure
21 1C). The RUS-CVD method can address the aforementioned issues.

22 No limitation with respect to the substrate size. The spray coating methods can be divided
23 to three categories based on the operation modes: (a) Stationary spray with the spray head
24 completely fixed; (b) single-pass spray with the spray head only movable in one direction and
25 (c) raster spray with the spray head movable in both x and y directions. Almost all the reported
26 spray coating methods for perovskite deposition use either stationary spray^{38, 40} or single-pass

1 spray^{33, 34, 36}. Attempting to coat two adjacent areas by stationary or single pass coating would
2 create an overlapped area dense with defects (see Supplementary Information for details of
3 raster coating vs. stationary or single-pass coating). Therefore although spray-coating is a
4 scalable deposition method, most of the reports are on the small cells (active area $\leq 1 \text{ cm}^2$).
5 Uličná et al. reported a scalable perovskite deposition method using the raster spray-coating,³⁵
6 but the active area of their devices was only 0.06 cm^2 . Hilt et al. reported a rapid spray plasma
7 processing method,³⁹ but the authors only demonstrated the fabrication of small-area solar cells,
8 not solar modules. By controlling the precursor film drying process, we report a uniform PbI_2
9 film deposition method based on a raster ultrasonic spray process on substrates with a size of
10 $10 \text{ cm} \times 10 \text{ cm}$, which to our best knowledge, is the first report in the perovskite research
11 community to demonstrate continuously scalable spray coating with a pattern width not limited
12 by the size of the spray head. The subsequent conversion from PbI_2 to perovskite via CVD has
13 also been shown to be scalable⁴⁷⁻⁴⁹ and with weak substrate size dependence⁴⁴. The reaction
14 speed during the CVD step is slower than other open air processing methods, such as blade
15 coating. However, considering that a large number of large area substrates can be processed
16 simultaneously in a large CVD setup⁴⁵, the deposition time per substrate is expected to be
17 substantially shorter.

18 Solar cell performance shows much lower substrate-size dependence than the mostly used
19 spin-coating method, owing to the high film uniformity and quality at large scale. (Figure 1D)

20 Low lead waste. PbI_2 precursor utilization efficiency increases to almost 100% upon
21 increasing substrate size (78% for $1.5 \text{ cm} \times 1.5 \text{ cm}$, 92% for $5 \text{ cm} \times 5 \text{ cm}$, 96% for $10 \text{ cm} \times 10$
22 cm , 99% for $30 \text{ cm} \times 30 \text{ cm}$, see the experimental section), significantly higher than the mostly
23 used spin-coating method (less than 10% Pb utilization at different substrate sizes). (Figure 1E)

24 Transferable to industry. Ultrasonic spray coating is widely used in industry for display and
25 lens coating, active layer and anti-reflection coating for solar cells, etc.⁵⁰ CVD is also a mature
26 coating technology widely utilized in the thin film solar cell industry.⁴⁷⁻⁴⁹

1 It is important to note that widely employed single point local characterization methods that are
2 suitable for small solar cells (e.g., active area $\sim 0.1 \text{ cm}^2$) are no longer sufficient for
3 characterizing mini-modules ($> 10 \text{ cm}^2$ active area).³⁹ To study thin film properties across large
4 area, UV-Vis spectroscopy, X-ray diffraction (XRD), atomic force microscopy (AFM), cross-
5 section scanning electron microscopy (SEM) and photoluminescence mapping are used to
6 characterize multiple locations on the 5 cm x 5 cm photoactive layers, to ensure the absorbance,
7 crystallinity and surface roughness are representative of the large area device. In addition, we
8 study film properties using large-area compatible characterization methods such as scattered
9 light intensity (SLI) imaging and electroluminescence (EL) imaging, which allow rapid
10 characterization of the entire 5 cm x 5 cm mini-modules and are also compatible with in-line
11 characterization in a production environment. With $\text{FAPb}(\text{I}_{0.85}\text{Br}_{0.15})_3$ perovskite layer
12 deposited by our method, perovskite mini-modules using the standard device architecture (i.e.,
13 with a TiO_2 electron transporting layer, a spiro-MeOTAD hole transporting layer, and a gold
14 electrode) show a champion module performance of 14.7% on an active area of 12.0 cm^2 . Under
15 continuous operation (constant 1 Sun light illumination, maximum power point, MPP, N_2
16 atmosphere, $<5\%$ relative humidity, no encapsulation) devices show high stability
17 corresponding to an average T_{80} lifetime of 535 h on the small cells (based on the statistical
18 data of 4 small cells) and 388 h on the module.

19 **Results and discussion**

20 **PbI_2 deposition by RUS.**

21 Several groups have reported using a co-solvent of DMF and DMSO mixture for the perovskite
22 precursor in the spin-coating process and the ratios are between 10:1 to 4:1 (V:V) to achieve
23 uniform perovskite deposition.^{18, 51} However, our initial results based on single-pass ultrasonic
24 spray (SUS)-coated PbI_2 suggest that this optimized ratio for perovskite is not directly
25 applicable to spray-coating PbI_2 due to the different crystallization dynamics.³⁴ Generally, a
26 higher DMSO concentration leads to a longer evaporation time because of its higher boiling

1 point and higher solubility for PbI_2 stemming from its higher coordination number, but a lower
2 viscosity.⁵²⁻⁵⁴ Uniformity of the PbI_2 layer changes substantially as we vary the ratio between
3 DMF and DMSO in the RUS process. The optimal PbI_2 deposition by SUS is not suitable for
4 the RUS process. Therefore we optimize the DMF:DMSO ratio for PbI_2 deposition via RUS
5 starting from 14:1 (volume ratio) according to our reported SUS method.³⁴ Four types of solvent
6 mixtures with the DMF:DMSO ratio varying from 14:0.5 to 14:1 are employed to dissolve PbI_2 .
7 SLI mapping measurements are performed on the entire 5 cm \times 5 cm sprayed PbI_2 precursor
8 and annealed films. Different SLI is either caused by different surface roughness or different
9 amount of micro cracks in the film bulk (see Supplemental Information for details on the SLI
10 mapping measurement). We observe that low DMSO concentration in the co-solvent, i.e.,
11 (DMF : DMSO = 14 : 0.5) results in a PbI_2 precursor film with high SLI that resembles the film
12 coated using pure DMF solvent (**Figure 2A**).³² The high SLI remains after the film is annealed
13 (Figure 2E). Medium DMSO concentration (DMF : DMSO = 14 : 0.65) results in translucent
14 PbI_2 precursor films with low SLI (Figure 2B), which remains after annealing (Figure 2F). High
15 DMSO concentrations (DMF : DMSO = 14 : 0.85 and DMF : DMSO = 14 : 1) result in slightly
16 increased SLI again for the PbI_2 precursor films (Figure 2C and 2D). The SLI increased strongly
17 after annealing (Figure 2G and 2H), due to formation of the internal cracks and voids caused
18 by evaporation of DMSO.⁵⁵ AFM measurements are carried out on 6 different locations of each
19 5 cm \times 5 cm PbI_2 film to study the surface roughness. RMS roughness decreases drastically
20 with DMSO concentration increasing from low (DMF : DMSO = 14 : 0.5) to medium (DMF :
21 DMSO = 14 : 0.65) and decreases slightly with further increasing the DMSO concentration
22 (DMF : DMSO = 14 : 0.85 and DMF : DMSO = 14 : 1) (Figure 2I and **Figure S1**). We interpret
23 the SLI and AFM data as follows. A low DMSO concentration (DMF : DMSO = 14 : 0.5) in
24 the solvent mixture results in a dense PbI_2 film with rough surface. While high DMSO
25 concentrations (DMF : DMSO = 14 : 0.85 and DMF : DMSO = 14 : 1) result in a smooth film
26 surface but with a large amount of internal cracks and voids (Figure 2J-M). A medium DMSO

1 concentration results in a smooth PbI_2 film with negligible internal cracks and voids. A rough
2 PbI_2 film will convert to a rough perovskite film, which is detrimental for the solar cell
3 performance.³⁴ Therefore low DMSO concentration (DMF : DMSO = 14 : 0.5) is not preferred.
4 To compare performance between the perovskite films formed from compact PbI_2 and the films
5 containing internal cracks and voids, we select two DMSO ratios (DMF :DMSO = 14 :0.65 and
6 DMF :DMSO = 14 :1) for the perovskite conversion.

7 **FAPb(I_xBr_{1-x})₃ formation by RUS-D and RUS-CVD.**

8 The two type of RUS-coated PbI_2 films are then reacted with FAI, FABr and MACl to form
9 FAPb(I_xBr_{1-x})₃ perovskite via two approaches, i.e., a CVD (designated as RUS-CVD) and an
10 optimized dipping approach reported by our group (designated as RUS-D).³⁴ Perovskite films
11 converted from the compact PbI_2 (DMF : DMSO = 14 : 0.65 for RUS) show high uniformity
12 with low SLI over the entire 5×5 cm substrate area (**Figure 3A and 3B**) and low surface
13 roughness (RMS roughness 25.2 ± 0.5 nm for RUS-CVD and 33 ± 5 nm for RUS-D) (Figure 3E,
14 3F, 3I, 3J, 3K; see Supplementary Information for statistical AFM results, **Figure S2**). We also
15 performed cross-section SEM measurements on multiple sample locations. All the SEM images
16 consistently show that the films converted from the compact PbI_2 (DMF : DMSO = 14 : 0.65
17 for RUS) have a high degree of uniformity (**Figure S3 and Figure S4**). On the other hand, films
18 converted from the PbI_2 layers with internal cracks (DMF : DMSO = 14 : 1 for RUS) show poor
19 macroscopic uniformity with lots of spots (Figure 3C and 3D), and high surface roughness with
20 many microscopic pin-holes (RMS roughness 75 ± 6 nm for RUS-CVD and 55 ± 6 nm for RUS-
21 D) (Figure 3G, H, L, M and Figure S3). In addition, CVD converted perovskite shows larger
22 grain size than dipping converted perovskite (Figure 3E, 3F and Figure S4). Because pinholes
23 in the perovskite films are detrimental to the device performance⁵⁶, we select the compact PbI_2
24 films deposition process (DMF : DMSO = 14 : 0.65) to study the effect of conversion process
25 on the film composition and optical property.

1 FAPb(I_xBr_{1-x})₃ with x equal to 85% is employed as the target perovskite material owing to its
2 superior thermal stability as reported by previous studies.⁵⁷⁻⁵⁹ For the films prepared by the
3 RUS-D method, the Br⁻ to (I⁻ + Br⁻) molar ratio is around 15% according to their ratio in the
4 dipping solution. To make the two conversion methods comparable, we optimize the RUS-CVD
5 process so as to prepare the perovskite with the similar composition. XRD and UV-Vis
6 measurements are performed on 6 different locations of each 5 cm × 5 cm substrate to study the
7 composition of the perovskite films (**Figure 4A**). Perovskite films converted by RUS-CVD and
8 RUS-D show very similar XRD peak positions at 14.1°, 24.5°, 28.3°, 31.8°, 33.7°, assigned to
9 (-111), (021), (222), (231), (030) perovskite crystal planes, respectively, suggesting that the
10 perovskite films are of a similar composition (Figure 4B). Peak positions agree well with those
11 of FAPb(I_{0.85}Br_{0.15})₃.⁵⁸ The peaks at 26.4°, 37.7° belong to the FTO substrate. RUS-CVD
12 processed perovskite film shows much higher intensity of the (-111), (222) and (231) diffraction
13 peaks but lower XRD intensity at (021) than the RUS-D processed perovskite film. These
14 results suggest that the perovskite films prepared by different methods show different
15 crystalline alignment and RUS-CVD processed perovskite film shows a higher overall degree
16 of crystallinity. Moreover, perovskite films prepared by RUS-D show clear PbI₂ peaks (12.7°,
17 38.6°), similar to our previous study.³⁴ XRD patterns on the same sample but different positions
18 are similar, suggesting the data are representative for large area (Figure 4C). To quantify the
19 PbI₂ crystalline phase fraction in the films, we perform the Rietveld refinement based on the
20 XRD results. A negligible PbI₂ phase fraction is determined for the films prepared by RUS-
21 CVD, while 10±1% (wt) PbI₂ is determined for the films prepared by RUS-D (**Table S1**).
22 Although a small amount of PbI₂ existing at the perovskite grain boundary is reported to be
23 beneficial for the defect passivation,⁶⁰ such a large amount of PbI₂ is expected to be detrimental
24 to the solar cell performance, due to the absorbance loss. To verify this point, we conduct UV-
25 Vis spectroscopy measurements on these films. Indeed, absorbance is lower for the films
26 prepared by RUS-D (Figure 4D). Furthermore, variation of the absorbance at same sample but

1 different positions is 6-8 times smaller for the RUS-CVD method at wavelength between 600
2 – 700 nm, suggesting the RUS-CVD prepared perovskite film is more uniform at the
3 macroscopic scale (detection area is 0.3 cm × 0.5 cm for each measurement) (Figure 4D inset).
4 Absorbance edges for the two perovskite films are both at ~790 nm, agreeing well with that for
5 the $\text{FAPb}(\text{I}_{0.85}\text{Br}_{0.15})_3$ perovskite.⁵⁸

6 **Effect of MACl during the perovskite formation.**

7 MACl is added for both dipping and CVD conversion processes. In the dipping process, MACl
8 strongly affects the perovskite crystallization process and leaves the films after thermal
9 annealing.⁶¹ We find that creation of MACl atmosphere during the perovskite formation via the
10 CVD process also influences the perovskite crystallization, resulting in increase of the
11 perovskite (-111) and (222) peak intensity (**Figure S5A and S5B**) and reduced perovskite film
12 surface roughness (Figure S5C and S5D). Perovskite converted via CVD with or without MACl
13 atmosphere shows negligible change in the XRD peak position, suggesting that the Cl^- amount
14 incorporated into the perovskite lattice is not significant (Figure S5B).⁶² To study whether FA^+
15 is partially substituted by the MA^+ cation, we conduct high resolution X-ray photoelectron
16 spectroscopy (HRXPS) measurements on the two $\text{FAPb}(\text{I}_{0.85}\text{Br}_{0.15})_3$ perovskite prepared by
17 RUS-CVD and RUS-D and also on the RUS-CVD prepared MAPbI_3 and FAPbI_3 perovskite as
18 control. Little peak position change appears for the Pb 4f and I 3d regions comparing the four
19 samples (**Figure S6A and S6B**). Br 3d signals appear in the two $\text{FAPb}(\text{I}_{0.85}\text{Br}_{0.15})_3$ perovskite
20 films (Figure 4E). Two peaks at 288.5 and 284.8 eV assigned to FA^+ related C 1s peaks appear
21 for the two $\text{FAPb}(\text{I}_{0.85}\text{Br}_{0.15})_3$ perovskite films and no typical MA^+ peak (286.5 eV) appears,
22 indicating that no or only a very small amount of MA^+ substitutes the FA^+ position (Figure
23 4F).^{19, 44} The statement is further confirmed by the N 1s peak position. The two
24 $\text{FAPb}(\text{I}_{0.85}\text{Br}_{0.15})_3$ perovskite films show the N 1s peak at 400.7 eV similar to FAPbI_3 , where
25 the N 1s peak associated with MA^+ appears at 402.5 eV (Figure 4G).^{19, 44} PL mapping is a
26 spatially resolved technique that can characterize uniformity and quality of the photoactive

1 layer. We carry out the PL mapping measurements on 4 different positions of each perovskite
2 film (detection area is $80\ \mu\text{m} \times 80\ \mu\text{m}$) and quantitatively compare the PL emission results. The
3 CVD-converted perovskite films show not only a $\sim 10\%$ higher PL intensity, but also ~ 5 times
4 narrower PL intensity distribution than dipping-converted perovskite (Figure 4H, 4I, 4J, **Figure**
5 **S7A-H**). Based on the results, we conclude that perovskite films prepared by RUS-CVD
6 method reveal higher uniformity across large area and higher quality than RUS-D from the
7 purity, crystallinity and optical property point of view.

8 **Perovskite solar cell/module performance and reproducibility.**

9 To study the device performance, we prepare perovskite modules by RUS-CVD and RUS-D on
10 $5\ \text{cm} \times 5\ \text{cm}$ substrates, where each contains 6 cells connected in series with a total active area
11 of $12.0\ \text{cm}^2$ (**Figure 5A**). A patterned TiO_2 layer was deposited by a scalable vacuum sputtering
12 method as the electron transporting layer.⁶³⁻⁶⁴ No mesoporous TiO_2 layer is used because of
13 the patterning difficulty. We are not aiming at demonstrating deposition methods for the
14 complete perovskite solar module. Therefore the deposition process for other layers (e.g., hole
15 transport layer) may not be scalable. The modules are patterned by 3 shadow masks. Details of
16 the module geometry are shown in **Figure S8** and discussed in the supporting information.⁴⁴ J-
17 V measurements are conducted on the modules with 1 to 6 cells connected in series to determine
18 the performance on different device active area. The champion module prepared by the RUS-
19 CVD shows a V_{oc} of 6.29 V, I_{sc} of 42.6 mA, FF of 66.5%, and PCE of 14.7% for the 6 sub-cells
20 connected in series from forward to backward scan (Figure 5B) and a PCE of 13.5% from
21 backward to forward scan (**Figure S9A**). As far as we know, this is among the highest
22 performing perovskite solar module prepared by spray-coating method to date.^{34, 42, 65} In
23 addition, performance of the champion RUS-CVD modules slowly decreases from 16.1% on 2
24 cm^2 to 14.7% on $12\ \text{cm}^2$ (Figure 5D and **Table S2**), corresponding to a very low PCE loss/area
25 (defined as $(\text{PCE}_{\text{single cell}} - \text{PCE}_{\text{module}})/(\text{area}_{\text{module}} - \text{area}_{\text{single cell}})$) of $0.14\ \%/ \text{cm}^2$.⁴⁴ On the other
26 hand, the champion module prepared by RUS-D shows a much lower PCE of 8.6% from

1 forward to backward scan and a PCE of 6.8% from backward to forward scan (Figure 5C and
2 Figure S9B). Performance of the champion RUS-D modules decreases much faster from 13.3%
3 on 2 cm² to 8.6% on 12 cm² (Figure 5D and Table S2), corresponding to a high PCE loss/area
4 (defined as $(PCE_{\text{single cell}} - PCE_{\text{module}})/(area_{\text{module}} - area_{\text{single cell}})$) of 0.47 %/cm². Such a big PCE
5 loss/area gap between the two perovskite processing methods indicates that the RUS-CVD
6 perovskite shows higher uniformity and lower series resistance at the perovskite absorber and
7 related interfaces (see Supplementary Information for details of the reasons causing the module
8 performance decrease upon increase of the active area).

9 To study the reproducibility of the two perovskite fabrication approaches, 16 modules (8
10 modules prepared by RUS-CVD and 8 modules prepared by RUS-D) are prepared for statistical
11 analysis. Averaged PCEs are 14.2±0.3% (12 cm² active area) for RUS-CVD prepared modules,
12 significantly higher than RUS-D prepared modules (6±1%) (Figure 5E). It is worth mentioning
13 that even for the modules prepared by RUS-D, the PCE has already exceeded that for the solar
14 module based on the perovskite film prepared by the combination of SUS-coated PbI₂ and
15 dipping conversion (~8% champion module PCE on 10 cm² active area).³⁴ This result indicates
16 the advantage of the RUS process over our previously reported SUS process in PbI₂ deposition
17 across large area. With perovskite film converted by CVD, the module performance is further
18 increased by 136.6% (PCE increase = $(\text{average } PCE_{\text{RUS-CVD}} - \text{average } PCE_{\text{RUS-D}}) / \text{average}$
19 $PCE_{\text{RUS-D}}$) than those converted by our reported dipping process. RUS-CVD prepared modules
20 shows only marginally higher average J_{sc} than RUS-D prepared modules, suggesting that J_{sc} is
21 not the main factor causing the performance variation. This is confirmed by external quantum
22 efficiency (EQE) measurements. The integrated currents are both 20.3 mA/cm² for champion
23 modules prepared by RUS-D and RUS-CVD, agreeing well with the current values from J–V
24 measurement with variations of less than 5% (Figure S9C). Module performance differences
25 are mainly caused by differences in V_{oc} and FF according to the statistical results (Figure 5F-
26 H), which can be related to the different perovskite film quality and uniformity.⁴⁴

1 **Perovskite solar module quality and uniformity.**

2 To evaluate device quality and uniformity over the entire module area we performed spatially
3 resolved electroluminescence (EL) measurements.⁶⁶ While PCE depends linearly on V_{oc} , I_{sc} ,
4 and FF, EL intensity (LED efficiency) at a given current is exponentially dependent on quasi-
5 Fermi level separation (V_{oc}).⁶⁷ Exponential dependence on V_{oc} leads to a much weaker
6 dependence on FF, and EL intensity probes the quality (non-radiative recombination rate) in
7 the absorber without sensitivity to resistive losses that would reduce measured FF in a PCE
8 measurement. Comparison of EL measurements between RUS-CVD and RUS-D modules
9 shows that RUS-D modules have a lower EL intensity in most locations whereas RUS-CVD
10 modules have dramatically higher EL intensity at the same applied current (Figure 5I and 5J).
11 We plot the EL intensity histogram figure to evaluate the EL intensity as a function of frequency.
12 RUS-D module shows a wide EL intensity distribution between 0-30% relative to the saturated
13 EL intensity, while RUS-CVD module shows over 90% distribution at the saturated EL
14 intensity (Figure 5K and 5K inset). Such dramatic differences in EL intensity suggest that the
15 RUS-CVD prepared perovskite has much less non-radiative recombination centers induced by
16 defects, which contributes to a higher module V_{oc} and PCE.

17 **Perovskite solar cell/module operational stability.**

18 Instability is one of the main challenges for perovskite solar cells. Because perovskite solar cell
19 lifetime varies substantially for different perovskite deposition methods, it is necessary to report
20 the device lifetime for newly developed methods. Conditions for the device stability test such
21 as atmosphere, temperature, illumination (continuous light soaking or storage under dark) and
22 load applied (open circuit, short circuit or MPP) significantly affect the device lifetime.⁶⁸
23 Device stability evaluation based on statistical results is also recommended.⁶⁹ Considering these
24 reasons, we prepare 8 $FAPb(I_{0.85}Br_{0.15})_3$ perovskite solar cells (0.1 cm^2 active area) in two
25 different batches (4 cells prepared by RUS-CVD and 4 cells prepared by RUS-D) and conduct
26 the first operational stability measurements on these devices. The devices are kept at continuous

1 1 sun illumination near their MPP, in the N₂ atmosphere (<5% relative humidity), without
2 encapsulation at room temperature (25.0 °C) and measured by step J-V scans every 30 min
3 (**Figure S10A and S10B**). Similar to other reports, RUS-CVD prepared devices show the initial
4 transient PCE decay (i.e., the exponential regime), which is followed by the linearly decay (i.e.,
5 the linear regime) (**Figure 6A**).⁶⁸ Transient decay is generally recoverable if the device is stored
6 in dark for an extended time.⁶⁸ Therefore the T₈₀ parameter, which represents the time when
7 PCE decays to 80%, can be calculated based on the linear decay regime.⁶⁸ RUS-CVD prepared
8 devices show an average T₈₀ value of 535 h (Figure 6A brown line to green line), closing to the
9 highest reported lifetime for planar structured perovskite solar cells.¹³ Such a high T₈₀ lifetime
10 suggests that RSU-CVD prepared devices are very stable under the operational condition. In a
11 previous study, we report the poor device stability for the CVD converted FAPbI₃ perovskite
12 solar modules due to formation of the yellow non-perovskite phase.⁴⁴ Here we demonstrate that
13 by adding 15% Br in the perovskite, stability of the perovskite solar cells is significantly
14 improved. We find all of the J_{sc}, V_{oc} and FF decay with time and the majority of PCE decay
15 comes from the FF (Figure 6B-D). In comparison, RUS-D prepared devices decay linearly at a
16 much higher rate, corresponding to an average T₈₀ value of 8 h (Figure 6A). Different from
17 RUS-CVD prepared device, J_{sc} of RUS-D prepared devices increase by 20% until reaching the
18 maximum value and then decrease constantly (Figure 6C inset). The majority factor causing the
19 PCE decay is J_{sc}, not the FF (Figure 6B-D). The nearly 70 times larger T₈₀ value for the RUS-
20 CVD prepared device than the RUS-D case suggests the excellent long-term stability of the
21 cells based on our RUS-CVD method.

22 So far, most of the operational stability tests are conducted on small-sized solar cells (e.g.,
23 active area ~ 0.1 cm²), not large-sized perovskite solar modules. The non-uniformity issue of
24 the perovskite film is more pronounced on the enlarged substrate, which has more changes to
25 cause the device failure under operation. On the other hand, temperature of the module increases
26 greatly under continuous illumination, which may also affect their performance and lifetime.⁴⁵

1 Thus, it is important to study the operational stability of the perovskite modules at elevated
2 temperature. Here, we conduct the operation stability measurements at the similar condition as
3 for small cells on the $\text{FAPb}(\text{I}_{0.85}\text{Br}_{0.15})_3$ perovskite solar modules (active area 12 cm^2). We
4 monitor the temperature during the operational stability measurements and find that the
5 temperature rapidly increases from $25.0 \text{ }^\circ\text{C}$ to $> 46.0 \text{ }^\circ\text{C}$ during the first 1000 s (Figure 6E) and
6 stabilizes in the following period (Figure 6F). RUS-CVD prepared module follows the PCE
7 decay behavior of RUS-CVD prepared small cells, including an initial exponential decay
8 regime and a linear decay regime (Figure 6E and 6F). After 1200 min operation, the module
9 still shows a PCE of 13.3%, with only 0.2% PCE decay comparing to the module PCE after an
10 initial transient decay. This result suggests that the RUS-CVD prepared device is quite stable
11 at temperature of up to $46.0 \text{ }^\circ\text{C}$. We measured the operation stability of another RUS-CVD
12 prepared perovskite module under the same condition until the device decayed to less than 80%
13 of its initial PCE. The RUS-CVD prepared device shows a long T_{80} lifetime of 388 h (Figure
14 6G brown line to green line). Comparing with the very few operational stability reports on the
15 perovskite solar modules^{46, 70}, our RUS-CVD prepared module is very stable under such
16 measurement conditions. In comparison, RUS-D prepared perovskite module shows 65% PCE
17 decay from 8.1% to 2.8% after 1200 min operation. In addition, we also study the module
18 storage stability. One RUS-CVD prepared module and one RUS-D prepared module are stored
19 in dark N_2 atmosphere (15% relative humidity) and measured in ambient air ($\sim 50\%$ relative
20 humidity). After 3600 h, RUS-CVD prepared module still shows a PCE of 13.4%, with a
21 relative PCE decay of 3.6% (Figure 6H). In comparison, RUS-D prepared module shows a PCE
22 of 3.3% and a relative PCE decay of 47.4%. Based on all the stability results, we think the RUS-
23 CVD method is not only a scalable perovskite deposition method but also present promising
24 device stability on the solar module size.

25 **Perovskite decomposition and ion migration under operation condition**

1 Furthermore, we study the reason causing the different device operational stability. Perovskite
2 solar cells fail under operation or storage for several reasons, such as light-, thermal- oxygen-
3 and humidity-induced perovskite degradation⁷¹⁻⁷⁵, charge transporting layer decomposition⁷⁶⁻⁷⁷,
4 ion migration⁷⁸⁻⁷⁹ etc. Because the only difference in the two conditions comes from the
5 perovskite film, the perovskite degradation and ion migration can be considered as the main
6 factors that affect the device stability. We prepare perovskite solar cells by the two methods
7 and perform XRD and UV-vis measurements on these samples. Each method includes a fresh
8 device, the same device after 40 h storage in dark and N₂ atmosphere and one operated device
9 under MPP condition for 40 h. Gold electrodes are removed before measurements. Devices
10 prepared by RUS-CVD show negligible change in XRD pattern after storage in dark N₂
11 atmosphere or operation (**Figure 7A**). On the other hand, the XRD peaks assigned to the
12 perovskite significantly decreased after 40 h operation for the RUS-D prepared devices (Figure
13 7B). The RUS-D prepared perovskite stored in dark N₂ atmosphere does not decompose,
14 indicating that decomposition of perovskite is caused by the operation (light, bias). The
15 statement is further confirmed by the UV-vis absorbance spectroscopy results. There is little
16 change in the absorbance for the devices prepared by RUS-CVD (Figure 7C), but there has been
17 an obvious reduction in the absorbance between the wavelength of 500 and 790 nm, which can
18 be assigned to decomposition of perovskite material, for the operated device prepared by RUS-
19 D (Figure 7D). Instability of the perovskite material in turn affects the operation instability of
20 the device. Such a different perovskite material stability might be caused by the different
21 perovskite grain size (Figure 3E and 3F).⁸⁰ To better understand the composition changes and
22 ion migration that relate to the device failure, we perform the second ion mass spectrometry
23 (SIMS) measurements on fresh and operated devices (40 h under MPP condition) prepared by
24 RUS-CVD and RUS-D. Operated devices are stored in the dark N₂ atmosphere for 1-3 days
25 before the SIMS measurements, so the changes observed are irreversible ones.⁸¹ Signals of Au⁺,
26 Pb⁺, FA⁺, I⁺, Br⁺, Ti⁺, Sn⁺ appear sequentially in all of the 4 samples (**Figure S11**). We observe

1 no significant difference of the element distribution (FA^+ , Au^+ , Pb^+ , I^+ , Br^+ , Ti^+ , Sn^+) between
2 fresh and operated devices that are prepared by RUS-CVD (Figure 7E and Figure S11).
3 However, we identify a redistribution and an intensity decrease of FA^+ on RUS-D prepared
4 device after operation (Figure 7F). It has been reported that the FA^+ redistribution can cause the
5 failure of the device after operation.⁸¹ Similar to the report, we do not see obvious I^+ and Br^+
6 migration.⁸¹ The FA^+ migration is likely to be another key factor causing the failure of the RUS-
7 D prepared device after operation at such a time scale. Taken together, the high operational
8 stability of RUS-CVD prepared devices could be explained by the robust perovskite film with
9 negligible decomposition and FA^+ ion migration at such a time scale. These results confirm the
10 excellent stability of perovskite solar cells and modules based on our RUS-CVD method.
11 Comparing with the perovskite films processed by solution based methods when the perovskite
12 is usually formed by annealing for 20 min, the growth rate of CVD-processed perovskite is
13 much slower. The constant supply of organic halide vapors helps the perovskite recrystallize
14 through in situ annealing, leading to formation of high quality perovskite films.⁵⁵

15 **Conclusions**

16 In summary, we develop a scalable perovskite deposition technology with combination of raster
17 ultrasonic spray coating and chemical vapor deposition. Our technology overcomes the coating
18 size limitation of the existing stationary spray and single-pass spray. Negligible lead waste
19 during the PbI_2 deposition process makes this technology environmental friendly and
20 transferable to industry. $\text{FAPb}(\text{I}_{0.85}\text{Br}_{0.15})_3$ perovskite films prepared using this technology show
21 high quality and uniformity. Planar structured perovskite module fabricated basing on this
22 method shows a high module PCE of 14.7% on an active area of 12.0 cm^2 , closing to the highest
23 reported module performance with perovskite film deposited by ultrasonic spray-coating. The
24 device also shows high operational stability, corresponding to an average T_{80} lifetime of 535 h
25 on the small cells (0.1 cm^2) and 388 h on the module (12 cm^2).

26

1 Supporting Information

2 Supporting Information is available from the Wiley Online Library or from the author.

3

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9

10 Conflict of interest

11 The authors declare no conflict of interest.

12

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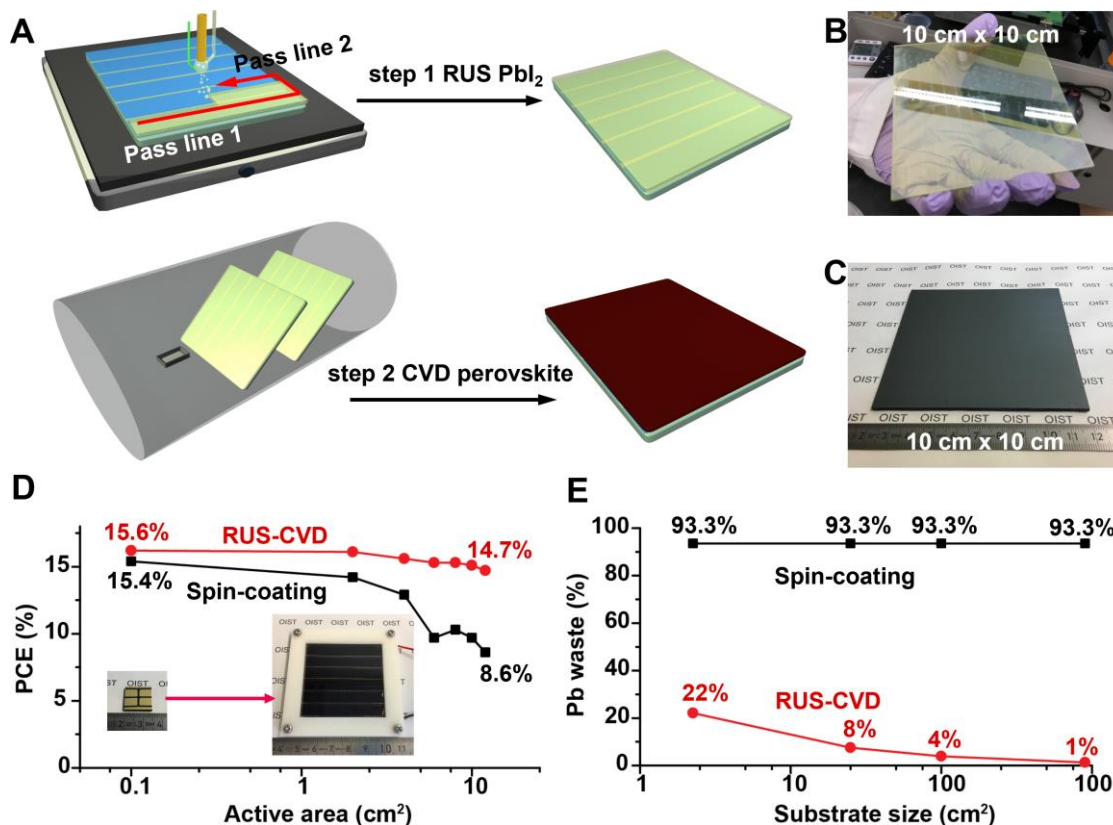
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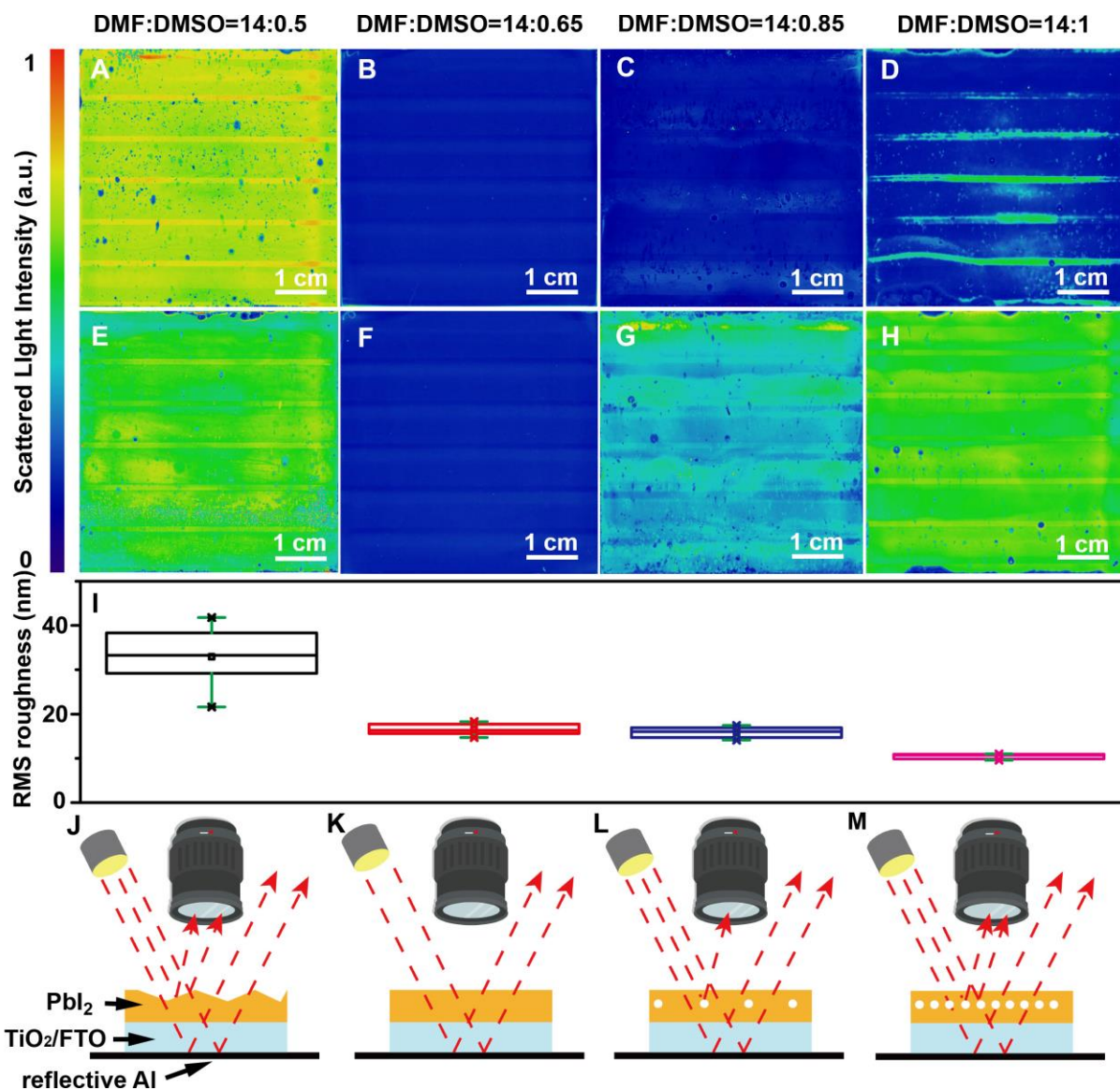
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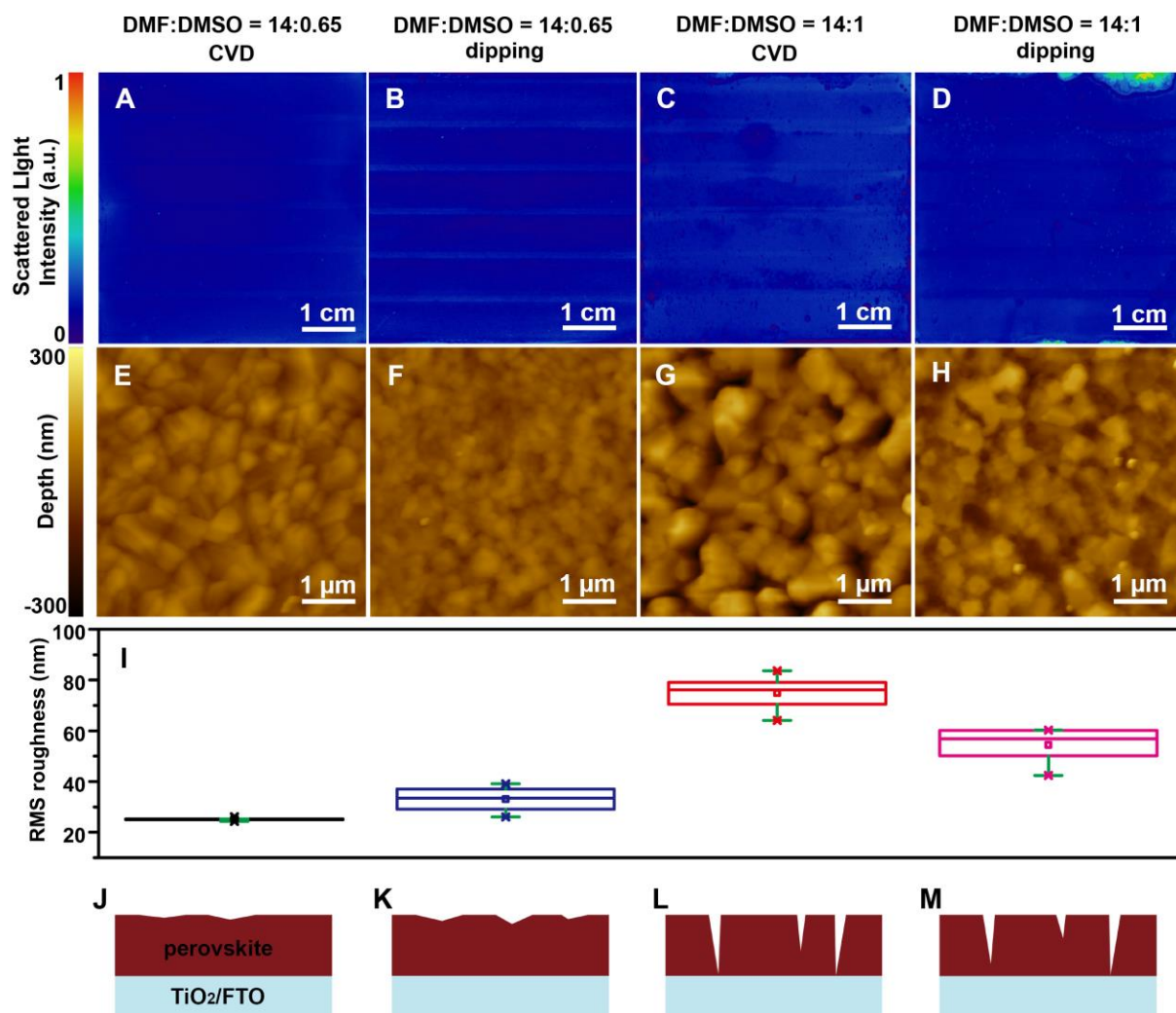
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3 **Figure 1.** Perovskite film deposition. (A) Schematic drawing of the RUS-CVD perovskite film
 4 deposition technology. PbI_2 films are raster ultrasonic spray (RUS)-coated on the FTO/ compact
 5 TiO_2 (c- TiO_2) substrates, and converted to $\text{FAPbI}_x\text{Br}_{3-x}$ via a CVD process. Photograph of (B)
 6 a RUS-coated PbI_2 film before annealing and (C) a CVD converted $\text{FAPbI}_x\text{Br}_{3-x}$ film deposited
 7 on a 10 cm \times 10 cm patterned FTO substrate. (D) Solar cell and module performance as a
 8 function of active area. Spin-coating data are extracted from our previous work.⁴⁴ The RUS-
 9 CVD method shows much lower substrate size dependence than the spin-coating method. (E)
 10 Lead waste during the perovskite deposition process as a function of substrate size. Lead waste
 11 during the RUS-CVD process continuously decreases until negligible, much less than that
 12 generated during the spin-coating process.

13

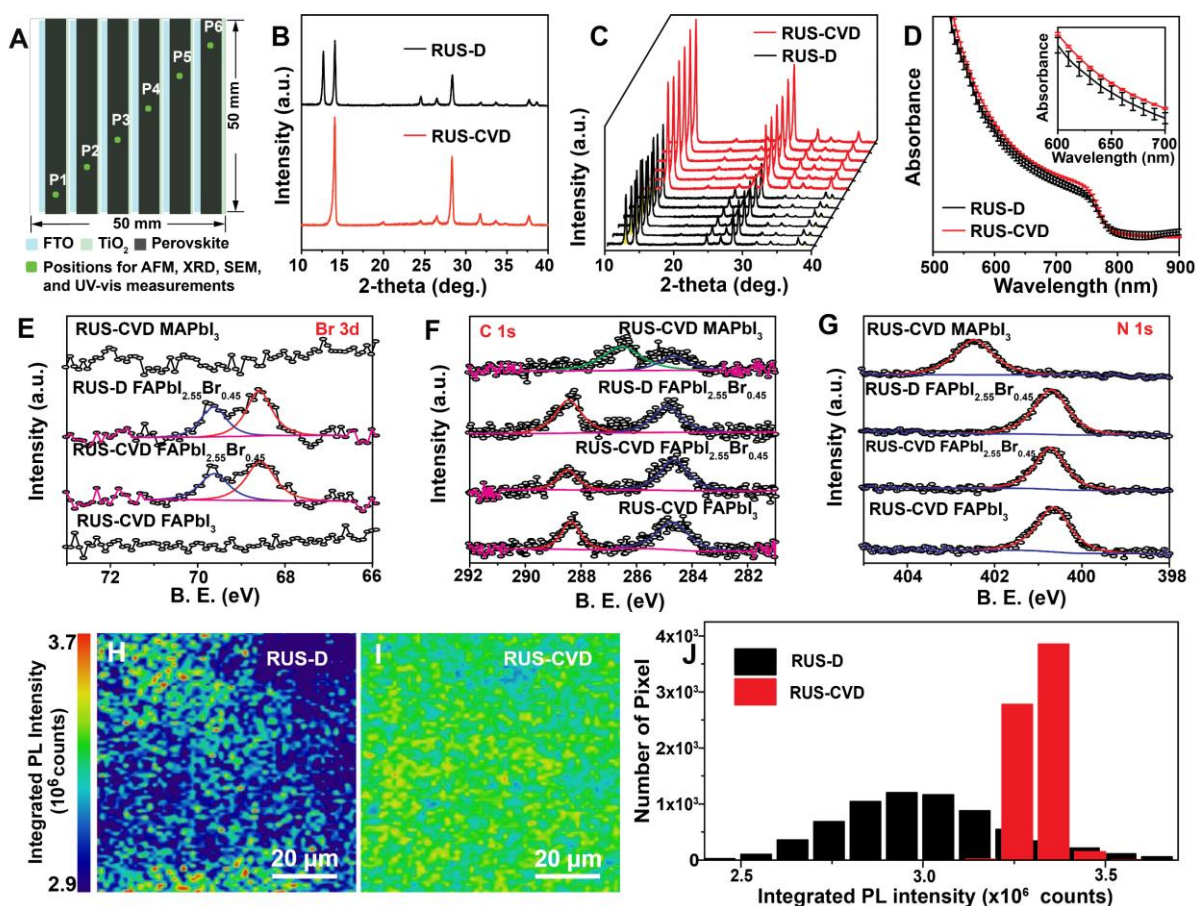


1
 2 **Figure 2.** Effect of solvent mixture on the PbI_2 film texture. False-color monochrome scattered
 3 light optical images of (A-D) PbI_2 precursor films after spray-coating (solvent allowed to
 4 evaporate at process temperature) (E-H) PbI_2 precursor films after annealing to remove the
 5 coordinated DMSO. Optical images show the entire 5 cm \times 5 cm substrates. (I) Root mean
 6 square (RMS) roughness of spray-coated PbI_2 films. AFM measurements are performed on 6
 7 positions of each 5 cm \times 5 cm substrate for statistical analysis. The DMF : DMSO ratios are
 8 14:0.5 for 2A, 2E; 14:0.65 for 2B, 2F; 14:0.85 for 2C, 2G and 14:1 for 2D, 2H, respectively.
 9 (J-M) Schematic drawing showing the SLI mapping measurements on the different PbI_2 films.
 10 Increasing the DMSO ratio results in reduced film surface roughness but increased internal
 11 cracks and voids.
 12



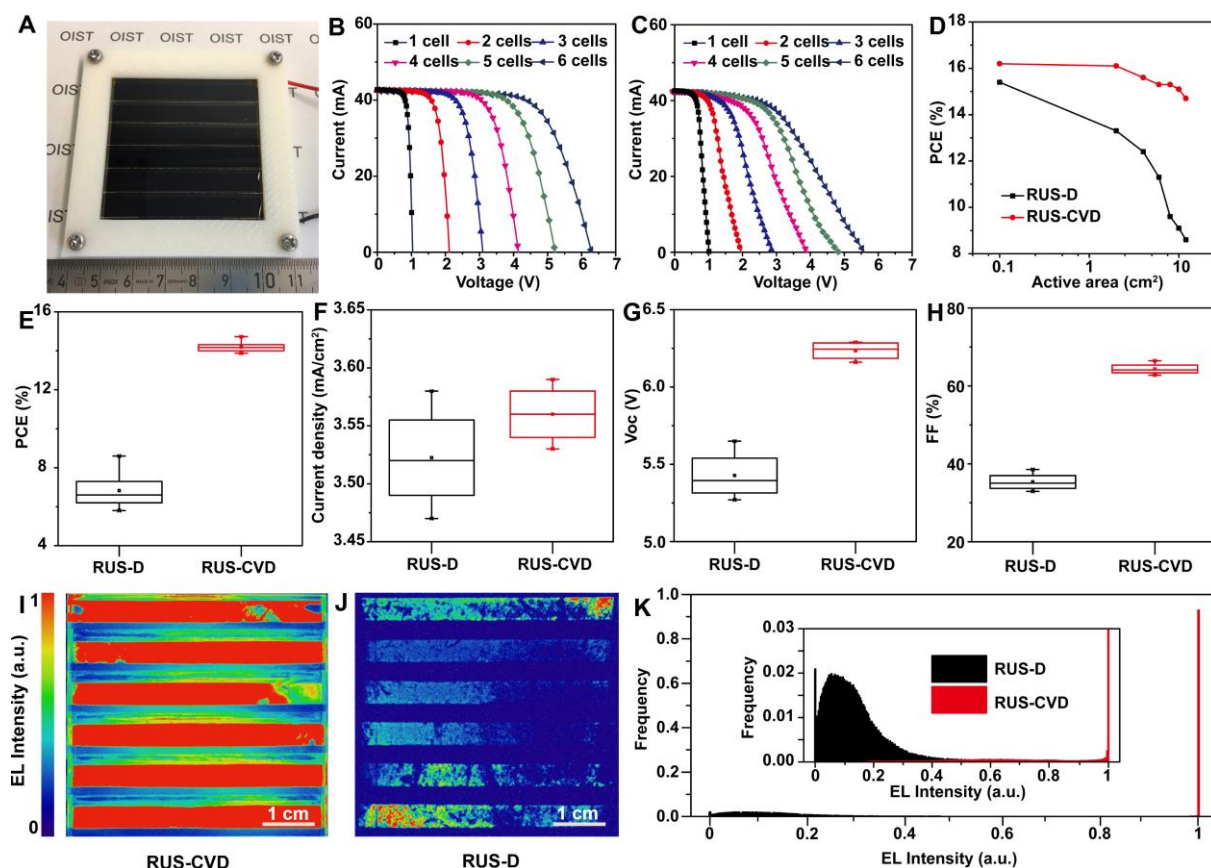
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2 **Figure 3.** Perovskite film morphology. (A-D) False-color monochrome scattered light optical
3 images of perovskite films. (E-H) AFM morphology of perovskite films. (I) Root mean square
4 (RMS) roughness of the FAPb(I_xBr_{1-x})₃ films. AFM measurements are performed on 6 positions
5 of each 5 cm × 5 cm substrate for statistical analysis. (J-M) Schematic drawing showing the
6 characteristics of the FAPb(I_xBr_{1-x})₃ films converted by CVD and the dipping (D) process. The
7 perovskite films are prepared by (A, E) RUS (DMF : DMSO = 14 : 0.65)-CVD, (B, F) RUS
8 (DMF : DMSO = 14 : 1)-CVD, (C, G) RUS (DMF : DMSO = 14 : 0.65)-D, (D, H) RUS (DMF :
9 DMSO = 14 : 1)-D, respectively. Perovskite films converted using RUS (DMF : DMSO = 14 :
10 0.65) PbI₂ show high uniformity without pin-holes.

11



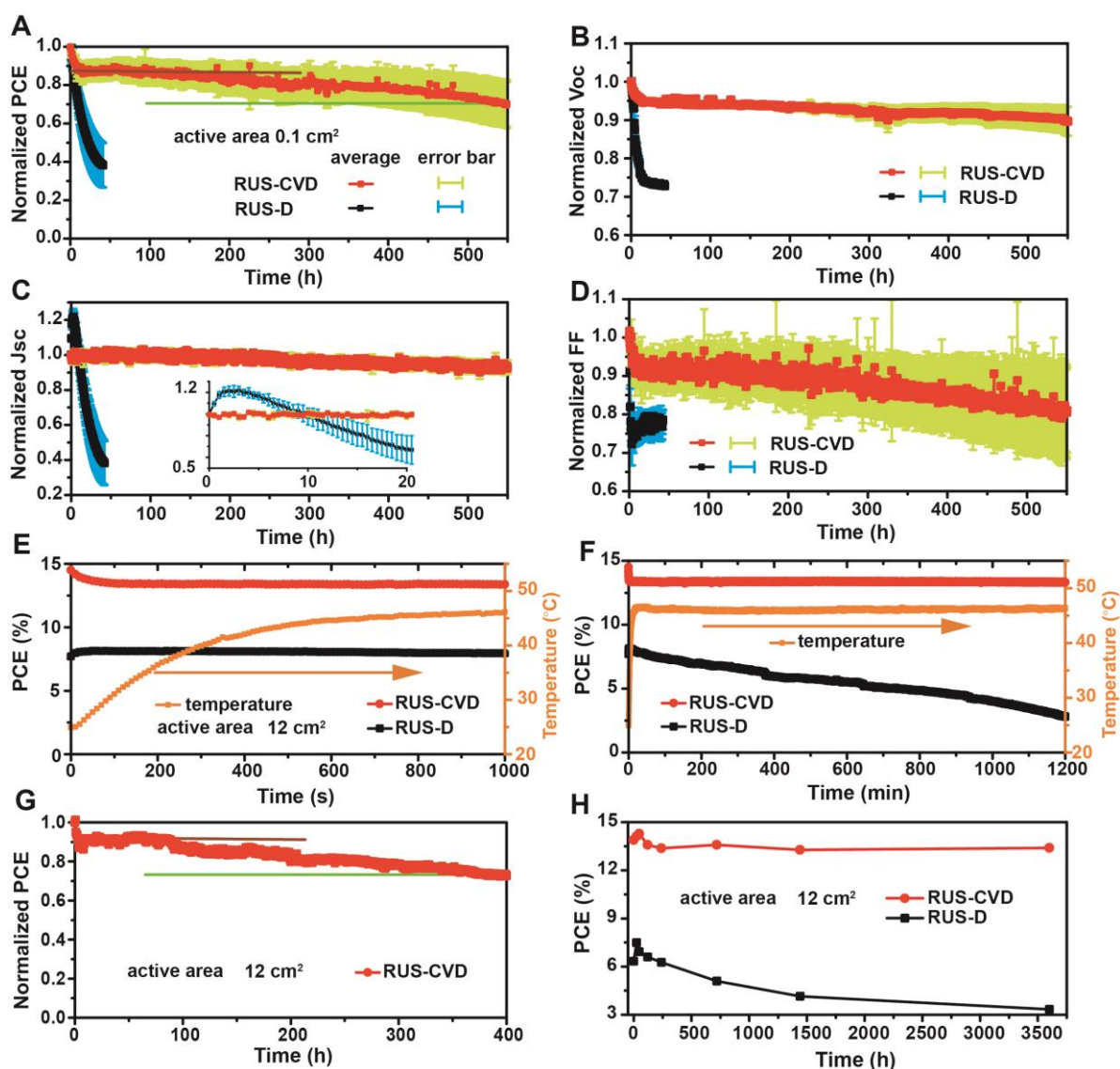
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 2 **Figure 4.** Perovskite film composition and optical property. (A) Schematic drawing showing
 3 the 6 positions for the AFM, SEM, XRD, and UV-Vis measurements. (B-C) XRD pattern, (D)
 4 UV-Vis absorbance spectra of $\text{FAPb}(\text{I}_{0.85}\text{Br}_{0.15})_3$ perovskite films. (E) Br 3d, (F) C 1s and (G)
 5 N 1s HRXPS spectra on $\text{FAPb}(\text{I}_{0.85}\text{Br}_{0.15})_3$ perovskite films. (H-I) false-color monochrome PL
 6 mapping images of the $\text{FAPb}(\text{I}_{0.85}\text{Br}_{0.15})_3$ films. (J) PL intensity histogram extracted from
 7 Figure 4H-I. Perovskite films converted by CVD and dipping have the similar composition of
 8 $\text{FAPb}(\text{I}_{0.85}\text{Br}_{0.15})_3$. The Perovskite films converted by CVD show complete conversion with
 9 higher perovskite crystallinity, absorbance and PL intensity than the dipping converted
 10 perovskite films.

11



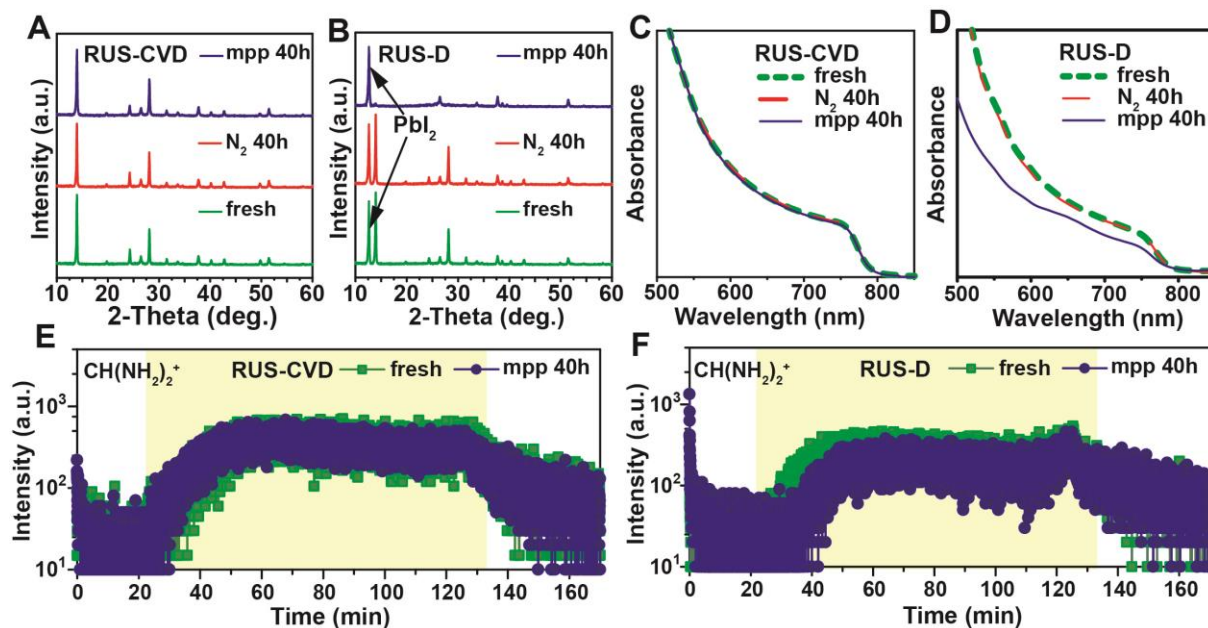
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 2 **Figure 5.** Perovskite solar module performance. (A) Photograph of a 5 cm × 5 cm
 3 $\text{FAPb}(\text{I}_{0.85}\text{Br}_{0.15})_3$ perovskite module. (B-C) J-V curves of the champion perovskite modules
 4 prepared by (B) RUS-CVD and (C) RUS-D method. (D) Solar cell and module performance as
 5 a function of active area. The RUS-CVD method shows higher module performance and lower
 6 substrate-size dependence than the RUS-D method. Statistical results of the module (E) PCE,
 7 (F) current density, (G) V_{oc} and (H) fill factor. A total of 16 modules (8 modules prepared by
 8 RUS-CVD and 8 modules prepared by RUS-D) are prepared for the statistical analysis. The
 9 RUS-CVD prepared modules show higher performance than the RUS-D prepared modules
 10 because of slightly higher J_{sc} and significantly higher V_{oc} and FF. False-color monochrome
 11 EL mapping images of perovskite modules prepared by (I) RUS-CVD and (J) RUS-D methods.
 12 (K) EL intensity histogram extracted from Figure 5I-J. The inset is the histogram with low
 13 maximum frequency in Y axis. The RUS-CVD prepared module shows higher EL intensity,
 14 suggesting the RUS-CVD prepared perovskite has much less non-radiative recombination
 15 centers.

16



1
 2 **Figure 6.** Stability of the perovskite solar cells and module. (A) Normalized average efficiency,
 3 (B) V_{oc} , (C) J_{sc} and (D) FF obtained on 4 unencapsulated perovskite solar cells (active area =
 4 0.1 cm^2). Devices are kept at 1 sun, N_2 atmosphere (<5% relative humidity), at their maximum
 5 power point and measured by step J-V scans every 30 min. The inset of (C) is the enlarged
 6 region of (C) between 0-20 h. J_{sc} of the RUS-D samples increases in the first 2 h until reach
 7 the maximum value and then decreases. (E-F) Steady-state maximum power output (V_{mpp} of
 8 4.50 V for RUS-CVD and 3.10 V for RUS-D) of the champion perovskite modules (active area
 9 = 12 cm^2). Measurements are performed at 1 Sun, MPP condition, N_2 atmosphere, <5% relative
 10 humidity and without encapsulation. (G) Normalized efficiency obtained on a RUS-CVD
 11 prepared perovskite module under the MPP condition. (H) Storage stability of the perovskite
 12 solar modules. Modules are stored in dark, N_2 atmosphere. For the RUS-CVD sample (Figure
 13 6A, 6G), the brown line indicates the starting point of the linear region and the green line shows
 14 the time when PCE decays to 80% with respect to the starting point. The perovskite solar
 15 cells/module prepared by RUS-CVD show higher operational and storage stability.

16



1
 2 **Figure 7.** Effect of perovskite deposition methods on device operational stability. (A-B) XRD
 3 patterns and (C-D) UV-vis absorbance spectra of fresh, storage and operated devices. Gold
 4 electrodes are removed before measurements. Under the same operational condition (mpp 40
 5 h), the RUS-CVD sample do not decompose but the RUS-D sample decomposes significantly.
 6 (E-F) SIMS depth profile of FA⁺ upon degradation. Measurements are taken on the fresh and
 7 operated devices that prepared by (E) RUS-CVD and (F) RUS-D. Under the same operational
 8 condition (mpp 40 h), the RUS-CVD sample does not show FA⁺ ion migration but the RUS-D
 9 sample shows obvious ion migration from the perovskite film surface to bulk. Different
 10 perovskite film decomposition and FA⁺ ion migration behavior result in different device
 11 operational stability.

12
 13

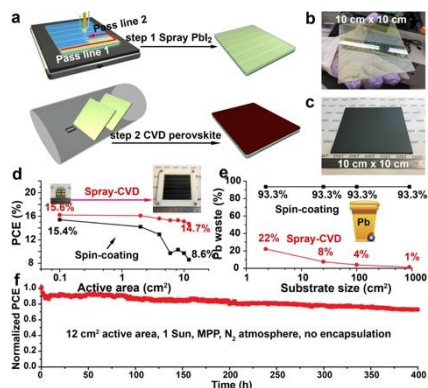
1 **A negligible-Pb-waste and upscalable perovskite film processing method** combining raster
 2 ultrasonic spray coating and chemical vapor deposition is developed. Planar-structured
 3 perovskite solar module shows a PCE of 14.7% on an active area of 12 cm², much lower
 4 substrate-size dependence than the spin-coating method, and outstanding operational stability
 5 near the maximum power point under 1 Sun light illumination (T₈₀ lifetime of 388 h).

7 **Keyword:** perovskite, solar module, upscalable, Lead waste, stability

10 Yan Jiang, Mikas Remeika, Zhanhao Hu, Emilio J. Juarez-Perez, Longbin Qiu, Zonghao Liu,
 11 Taehoon Kim, Luis K. Ono, Dae-Yong Son, Zafer Hawash, Matthew R. Leyden, Zhifang Wu,
 12 Lingqiang Meng, Jinsong Hu, and Yabing Qi*

15 **Negligible-Pb-Waste and Upscalable Perovskite Deposition Technology for High**
 16 **Operational-Stability Perovskite Solar Modules**

18 ToC figure



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