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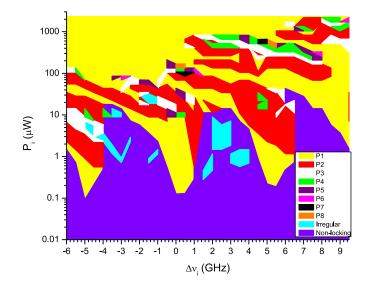
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Nonlinear Dynamics Induced by Optical Injection in Optical Frequency Combs Generated by Gain-Switching of Laser Diodes

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Abstract: We present experiments and numerical simulations of optical frequency combs generated by gain-switching a single mode laser diode when subject to optical injection. Our analysis focuses on the combs with a frequency separation f_R in the GHz range. We present experimental maps in the parameter space spanned by the detuning and the strength of the optical injection that identify the boundaries between regions with different dynamical states. A rich variety of nonlinear behaviors including injection-locked, unlocked and irregular combs are observed and analyzed. The dynamical state corresponding to an injection locked comb, PN, is characterized by an optical phase oscillation with a well defined amplitude in such a way that repeats or changes in 2π with an N/f_R period, where N is a natural number. Different regions of locked combs with a tongue shape around detuning values given by multiples of f_R appear in the maps. P1 and P2 are the most widespread locked states for large values of the modulation amplitude. As this amplitude decreases a much larger variety of PN states with large values of N appear in small area regions of the map. Our numerical simulations are in very good agreement with experimental results.

Index Terms: Optical frequency combs, gain-switching, laser diode, optical injection, non-linear dynamics.

1. Introduction

Optical frequency combs (OFCs) are coherent light sources consisting of evenly spaced discrete spectral components. From their early applications, mainly in the field of frequency metrology and high accuracy spectroscopy [1], OFCs have also been used in optical ranging [2], high-speed

optical communications [3]–[5], optical arbitrary waveform generation [6] and gas-sensing [7], [8]. One possibility for generating OFCs is to use semiconductor lasers due to their acknowledged advantages: high efficiency, small footprint, and low cost. Four different approaches have been used to generate OFCs in laser diodes: mode-locking [9], electro-optic modulation [10], micro-ring resonators [11], and gain switching (GS) [12].

Gain switching technique consist in driving the semiconductor laser by a radio-frequency (RF) current, typically sinusoidal, superimposed to a direct bias current. From the early demonstration of OFC generation by GS [12], [13] considerable attention has been paid to this technique [4], [5], [14]–[24]. Additional advantages of the technique are flexibility in the selection of the frequency spacing, low losses, compactness, low energy consumption, and easy implementation [12]. Applications of OFCs generated by GS include radio-over-fiber [5] and multi-carrier optical communications [3], [4], [25], absorption spectroscopy [20], [21], and sub-THz generation [26]. The key parameters determining the temporal and spectral characteristics of the generated OFCs are the amplitude and frequency of the RF current together with the bias current applied to the laser diode. Experimental analysis of key issues for OFCs applications, like phase noise/linewidth, frequency span, jitter, and frequency chirp, have been recently performed [14], [22], [27], [28]. These issues also have been analyzed from a theoretical point of view using rate equations-based numerical models [15]–[17]. Very recently a systematic experimental and simulation analysis of the effect of the driving conditions on the OFCs characteristics has been performed [24].

External optical injection (OI) in semiconductor lasers has also been a subject of interest for many years [29], [30]. OI in continuous wave (CW) single-mode lasers induces a wide variety of nonlinear dynamical regimes, including injection locking, four-wave mixing, and periodic and chaotic behaviours [30]. Injection locking improves the laser emission characteristics by reducing the frequency chirp and noise, and by enhancing the intrinsic frequency response [30]. Injection of OFC into a single-mode CW slave laser has received recently a lot of attention [31]–[35]. As the slave's frequency is detuned by a rational fraction of the injected OFC spacing, it becomes frequency locked [31]. These locked states are more commonly known as Arnol'd tongues.

The complementary situation, in which light from a CW laser is injected in gain-switched lasers, has also been analyzed. In this case OI improves the spectral characteristics of the OFCs when performed under specific injection conditions. For instance, OI can transform a broad noisy optical spectrum from a sinusoidally GS single-mode laser into a high quality OFC [12]. This transformation has been demonstrated to be particularly dramatic for pulsed GS lasers for which broad OFCs with small line separations (smaller than 500 MHz) were experimentally obtained [23]. Another advantage of injection locking in GS lasers is that a significant reduction of the linewidth of individual comb lines can be obtained by using a narrow linewidth CW master laser (ML), because the low linewidth of the ML is transferred to the OFC lines [17], [22], [27]. Numerical simulations also show that the locking range for GS lasers is considerable greater than that corresponding to CW lasers because the OFC can be locked by injecting close to one of the central lines of the comb [17]. Detrimental characteristics like time jitter, phase noise and relative intensity noise (RIN) can also be reduced by appropriate external OI [12], [14], [16], [36], [37]. In fact theoretical analysis show that reduction of the pulse-to-pulse phase noise, time jitter and RIN causes a large increase of the carrier-to-noise ratio (CNR), as well as a decrease of the linewidth of each comb line [16].

In a recent work we have performed a systematic analysis of the OI conditions for improving the spectral quality of a GS single-mode laser showing a broad noisy spectrum without injection [24]. This theoretical and experimental analysis mainly focused on the 10 dB spectral width and the CNR, that are two of the most important parameters for characterizing the quality of an OFC. However, a systematic analysis on how OI conditions affect the nonlinear dynamics of the GS laser has not been reported yet.

In this paper we perform that analysis for the first time to the best of our knowledge. This is done by using numerical simulations and experiments on a gain-switched single-mode laser subject to external optical injection. Contrary to [24] we focus on the effect of OI on a good quality OFC. The OFC generator is a single-mode semiconductor laser, which is driven in GS operation

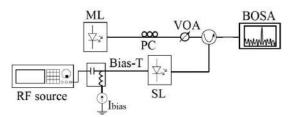


Fig. 1. Experimental setup for performing optical injection in GS operation. SL: slave laser, ML: master laser, PC: polarization controller, VOA: variable optical attenuator, and BOSA: Brillouin optical spectrum analyzer.

using a bias current and a sinusoidal signal with a frequency f_R in the GHz range. We perform a first experimental measurement of maps, in the injected power-frequency detuning plane, in which we observe injection-locked, non-locked and irregular combs regions. We perform numerical simulations of the system by using the model of [24]. We find different types of locked combs characterized by a frequency spacing equal to rational fractions of f_{B} . We term PN the dynamical state corresponding to a locked comb with f_R/N frequency separation between consecutive lines of the optical spectrum, where N is a natural number. The good agreement found between the simulations and the experimental results permits us to characterize the PN state also by its phase locking behavior: optical phase oscillates with a well defined amplitude in such a way that repeats or changes in 2π with an N/f_B period. Our experimental maps show that P1 and P2 are the most widespread locked states for large values of the modulation amplitude. When decreasing this amplitude a much larger variety of PN states appear in small area regions of the map. PN states with large values of N, up to N = 14, are observed for the first time, as far as we know. Locking range of combs is much larger than that of CW lasers for which there is only a single locking range, in agreement with previously reported simulations [17]. The presented locking scenarios can be used to generate optical combs with different frequency spacing values.

2. Experimental Techniques

Experimentally we attain GS of a laser diode, with or without OI, by using the setup shown in Fig. 1. The laser is a high-bandwidth 1550 nm discrete mode laser (DML) (Eblana Photonics EP1550-0-DM-H19-FM). This is a multi-quantum well device in a ridge waveguide with index perturbations, in order to allow single-mode operation [38]. The threshold current of this laser is $l_{th} = 14$ mA and its nominal modulation bandwidth is 10 GHz. More details can be found in [24]. The CW bias current, l_{bias} , and the temperature of the laser were controlled with a laser driver and a temperature controller (Luzwavelabs LDC/E-Current200 and LDC/E-Temp3), respectively. The temperature of the device was held constant at 25 °C. In all the experiments we have used a bias current, $l_{bias} = 30$ mA, for which the relaxation oscillation frequency, v_{ROF} , is approximately 6 GHz. In order to achieve GS operation the laser was driven by a superposition of l_{bias} and a sinusoidal modulation current at a frequency $f_R = 5$ GHz provided by a microwave/RF generator (Keysight N5173B).

Light from a tunable master laser (ML) (Pure Photonics PPCL300), with a narrow linewidth (75 kHz), was injected into the DML, operating as a slave laser (SL), by using an optical circulator. A polarization controller (PC) was used for maximizing the power injected into the SL. The level of injected power into the SL was controlled by using a variable optical attenuator (VOA). The optical injection was characterized by its strength given by the value of the power measured in front of the SL, P_i , and by its optical frequency, v_i . The output of the SL is spectrally characterized with a high-resolution (10 MHz) Brillouin optical spectrum analyser (BOSA) (Aragon Photonics BOSA 210). The quality of OFCs was characterized by means of the 10 dB spectral width (Δf_{10}) and the average carrier-to-noise ratio (CNR) of the lines within Δf_{10} [22].

3. Theoretical Model

The dynamics of a single-mode semiconductor laser subject to external optical injection can be modelled by using the following set of rate-equations [24], [39]:

$$\frac{dN}{dt} = \frac{I(t)}{eV_{act}} - R(N) - \frac{v_g g(N)S}{1 + \epsilon S}$$
(1)

$$\frac{dS}{dt} = \left[\frac{\Gamma v_g g(N)}{1 + \epsilon S} - \frac{1}{\tau_p}\right] S + 2k_c \sqrt{SS_i} \cos \Phi + \beta \Gamma BN^2 + \sqrt{2\beta \Gamma BN^2 S} F_S(t)$$
(2)

$$\frac{d\Phi}{dt} = \frac{\alpha}{2} \left[\Gamma v_g g(N) - \frac{1}{\tau_p} \right] - 2\pi \left(\Delta v_i + \Delta v \right) - k_c \sqrt{\frac{S_i}{S}} \sin \Phi + \sqrt{\frac{\beta \Gamma B N^2}{2S}} F_{\Phi}(t)$$
(3)

where N(t) is the carrier density, S(t) the photon density and $\Phi(t)$ the optical phase in the reference frame of the master laser, so the electrical field is $E(t) = \sqrt{S(t)}e^{i(2\pi v_i t + \Phi(t))}$, where v_i is the frequency of the master laser. In these equations I(t) is the injected current, V_{act} the active volume, *e* the electron charge, R(N) the carrier recombination rate, v_g the group velocity, g(N) the material gain, ϵ the non-linear gain coefficient, Γ the optical confinement factor, τ_p the photon lifetime, β the fraction of spontaneous emission coupled into the lasing mode and α the linewidth enhancement factor. The carrier recombination is $R(N) = AN + BN^2 + CN^3$, where *A*, *B* and *C* are the non-radiative, spontaneous, and Auger recombination coefficients, respectively. The material gain g(N) is given by $g(N) = \frac{dg}{dN}(N - N_{tr})$, where $\frac{dg}{dN}$ is the differential gain and N_{tr} the transparency carrier density. Neglecting high-frequency electrical effects, the injected current I(t) is given by:

$$I(t) = I_{bias} + C_{loss}(f_R) \frac{2\sqrt{2}V_{RF}}{Z_0 + Z_l} \sin(2\pi f_R t),$$
(4)

where V_{RF} is the root-mean-square (RMS) voltage of the signal generator applied to an ideal 50 Ω load, $C_{loss}(f_R)$ is a loss coefficient accounting for the frequency dependent electrical cable attenuation, Z_0 is the generator output impedance, and Z_l the impedance of the laser module. The output power coupled to the fiber is given by

$$P(t) = S(t) \frac{\eta_f h c V_{act}}{\lambda_{cw} \Gamma \tau_{\rho}}$$
(5)

where η_f is the in-fiber external quantum efficiency, λ_{cw} is the CW wavelength, and *h* is the Planck constant. The Langevin terms $F_S(t)$ and $F_{\Phi}(t)$ in Eqs. (2)–(3), represent fluctuations due to spontaneous emission, with the following correlation properties, $\langle F_i(t)F_j(t') \rangle = 2\delta_{ij}\delta(t-t')$, where $\delta(t)$ is the Dirac delta function and δ_{ij} the Kronecker delta function with the subindexes *i* and *j* referring to the variables *S* and Φ .

Terms describing the external optical injection appear in Eq. (2) and Eq. (3). In these terms k_c is the master-slave coupling coefficient, and S_i is the photon density of the injected laser field. S_i is obtained from the power injected by the ML, P_i , using an expression similar to Eq. (5). Two frequency terms appear in these equations. The first one is the frequency detuning between the ML and the free-running SL when operated in CW at I_{bias} , $\Delta v_i = v_i - v_{cw} = v_i - c/\lambda_{cw}$, where v_{cw} is the frequency corresponding to λ_{cw} , and *c* is the speed of light in vacuum. The second frequency term in Eq. (3), Δv , is the frequency detuning between v_{cw} and the frequency of the free-running SL at threshold v_{th} , $\Delta v = v_{cw} - v_{th}$. This is a non-vanishing term due to the gain saturation effect. When Eq. (3) is considered for the free-running SL at I_{bias} it gives

$$\Delta v = v_{cw} - v_{th} = \frac{1}{2\pi} \frac{\alpha}{2} \left(\Gamma v_g g(N) - \frac{1}{\tau_p} \right)$$
(6)

This detuning can be evaluated in terms of I_{bias} , I_{th} , and the nonlinear gain coefficient, ϵ , as follows. Solving the deterministic version of Eqs. (1), (2) in the steady state with $\kappa_c = 0$, and neglecting noise terms ($\beta = 0$), we find for the photon density at I_{bias} , $S_0 = (I_{bias}/(eV_{act}) - R(N_{th}))\Gamma\tau_p$, where N_{th} is the threshold carrier density. Applying $I_{th} = R(N_{th})eV_{act}$ we get $S_0 = (I_{bias} - I_{th})\Gamma\tau_p/(eV_{act})$. The

Symbol	Laser values	Units
Vact	1.53 x 10 ⁻¹⁷	m ³
Г	0.06	-
N_{tr}	1.23 x 10 ²⁴	m ⁻³
В	1.5 x 10 ⁻¹⁶	m^3s^{-1}
$\frac{dg}{dN}$	4.38 x 10 ⁻²⁰	m^2
n_g	3.5	-
$ au_p$	2.17 x 10 ⁻¹²	s
Α	2.8 x 10 ⁸	s^{-1}
С	9.0 x 10 ⁻⁴¹	m^6s^{-1}
β	5.3 x 10 ⁻⁶	-
ϵ	1.97 x 10 ⁻²³	m ³
α	3	-
Z_0	50	Ω
Z_l	50	Ω
$C_{loss}({\rm at}5{\rm GHz})$	0.7	-
η_f	0.17	-

TABLE 1
Simulation Parameters

substitution in Eq. (6) of the relation obtained from $\dot{S} = 0$, $\Gamma v_g g(N) = (1 + \epsilon S_0) / \tau_p$, and the previous expression for S_0 gives

$$\Delta \nu = \frac{\alpha \epsilon \Gamma (l_{bias} - l_{th})}{4\pi e V_{act}}$$
(7)

If we use $\Delta \nu$ given by Eq. (7), $\dot{\Phi}$ for the SL at I_{bias} satisfies $\dot{\Phi} = -2\pi \Delta \nu_i$ and then, $\Phi(t) = -2\pi \Delta \nu_i t + \Phi_0$, where Φ_0 is constant. Therefore, $E(t) = \sqrt{S_0}e^{i(2\pi\nu_{cw}t + \Phi_0)}$, as required. In the same way, for injection locked CW laser we impose $\dot{N} = \dot{S} = \dot{\Phi} = 0$. This means that Φ is constant and the laser emits at ν_i , as expected.

We have used the laser parameters [24] that were extracted for a laser similar to that used in our experiments. The main differences with our laser are that the threshold current was 14.8 mA instead of $l_{th} = 14$ mA, and that the emission wavelengths are slightly different. We show the laser parameters in Table 1. In order to calculate the optical spectrum we integrate Eqs. (1)–(3) using a 0.01 ps integration time step. We have checked that with this integration time step the photon density is always positive. Fast Fourier transform of the optical field written in the reference frame of the emission frequency of the slave laser operating in CW without optical injection, $\mathcal{E}(t) = \sqrt{P(t)}e^{i(2\pi\Delta v_i t + \Phi(t))}$, are performed using a 2.5 ps sampling time and a 40.96 ns temporal window. Optical spectra are calculated by averaging over 20 temporal windows.

4. Results and Discussion

We first discuss the results obtained without optical injection. We consider driving conditions leading to a high quality OFC: a modulation voltage $V_{RF} = 1$ V, repetition frequency $f_R = 5$ GHz, and $I_{bias} = 30$ mA [24]. In this case the coherence of the pulses emitted by the free-running gain-switched SL is maintained because the laser is not completely switched-off between pulses [16], [24]. Fig. 2(a) shows the experimental optical spectrum. The frequency separation between consecutive lines is 5 GHz, that approximately corresponds to 0.04 nm wavelength separation. This

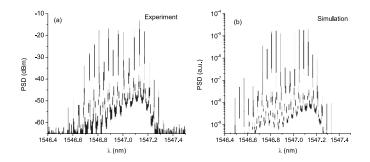


Fig. 2. Experimental (a) and simulated (b) optical spectra (PSD: Power Spectral Density) of the gainswitched laser ($I_{bias} = 30$ mA, $f_R = 5$ GHz, and $V_{RF} = 1$ V) without optical injection.

spectrum shows a high value of CNR (> 35 dB) and a spectral width Δf_{10} > 50 GHz. The optical spectrum of the SL in CW operation shows a well defined line at 1546.985 nm wavelength. As V_{RF} is increased, this comb line moves towards a longer wavelength and new comb lines begin to appear due to the modulation of the bias current. For conditions corresponding to Fig. 2(a) the CW line has shifted to 1547.005 nm. This redshift is due to the temperature increase caused by the sinusoidal excitation of the bias current in comparison with the constant value corresponding to CW operation. In our simulations this redshift does not appear because our model does not consider thermal effects. Therefore we consider in our calculations $\lambda_{cw} = 1547.005$ nm for obtaining the best comparison between experimental and simulation results. The theoretical optical spectrum corresponding to Fig. 2(a) is shown in Fig. 2(b). Both spectra are very similar, in terms of shape, flatness, CNR and width, the main difference being the absence of the BOSA background noise, which has not been taken into account in our simulations.

From now on we will analyze, using experiments and simulations, the effect of optical injection on the respective OFCs. We first analyze how the OFCs obtained with a large modulation voltage, like those of Fig. 2, change when applying OI. In order to compare between experimental and simulation results we have to estimate the master-slave coupling coefficient, k_c . This is done by fixing a value of Δv_i and searching for the value of k_c for which the minimum injected power required to achieve locking of the slave OFC to the master laser equals the experimental value. When following this procedure for $\Delta v_i = -2$ GHz we obtain $k_c = 5.5 \times 10^{10} \text{ s}^{-1}$, which is similar to the value obtained in [24] for a similar device in a similar set-up.

We show in Fig. 3 experimental and simulated OFCs obtained when the injected power, P_i , is increased for a fixed value of the detuning, $\Delta v_i = -2$ GHz. In this way we illustrate the effect of OI on the high quality OFC shown in Fig. 2.

When P_i is very small the optical spectrum is mainly composed of two OFCs with the same frequency spacing f_R , as it is shown in Fig. 3(a) and (f). The most intense OFC is very similar to that corresponding to the GS free-running SL. The second OFC is due to the injected master field because its lines appear at wavelengths $\lambda_i + n \times 0.04$ nm (with *n* being an integer). Four wave mixing (FWM) components also appear due to the beating between a line from the SL OFC and the closest frequency from the modulated fields of the injected laser. The presence of FWM terms indicates the absence of locking. As P is increased, the SL OFC begins to undergo some frequency pulling (see Fig. 3(b) and (g)) and eventually the slave comb locks to the master laser (see Fig. 3(c) and (h)). These last spectra are centered at λ_i with a frequency spacing of f_B . We denote the dynamic state corresponding to these spectra as P1. Fig. 3(a)-(c) experimentally confirm the transition to P1 that was first theoretically described in [17]. When P_i is further increased combs centered at λ_i with a frequency spacing equal to rational fractions of the repetition frequency, f_R/N (N being a natural number), are obtained. We denote these dynamical regimes as PN because the temporal trace of the output power has a period given by N/f_B . An example of OFCs corresponding to P2 is shown in Fig. 3(d) and (i). Further increase of P_i leads again to P1 dynamics (see Fig. 3(e) and (j)) in which CNR has increased and Δf_{10} has decreased. Fig. 3 shows that there is a very good agreement between simulations and experiments.

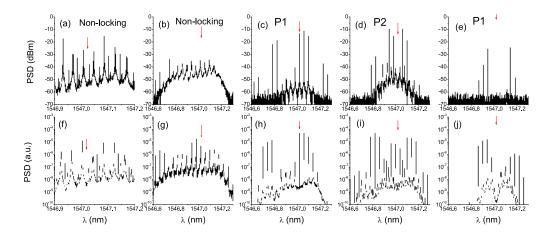


Fig. 3. Experimental (upper row) and simulated (lower row) optical spectra of the gain-switched laser ($l_{bias} = 30 \text{ mA}$, $f_R = 5 \text{ GHz}$, and $V_{RF} = 1 \text{ V}$) with optical injection at detuning $\Delta v_i = -2 \text{ GHz}$ and different values of injected power P_i , (a), (f) 41 nW, (b), (g) 1.9 μW , (c), (h) 3.67 μW , (d), (i) 14 μW , and (e), (j) 415.4 μW . The injection frequency is indicated with an arrow.

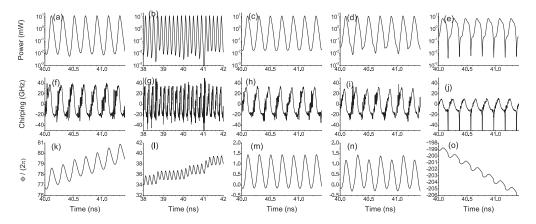


Fig. 4. Simulated power (upper row), frequency chirping (middle row) and optical phase (lower row) of the gain-switched SL ($l_{bias} = 30 \text{ mA}$, $f_R = 5 \text{ GHz}$, and $V_{RF} = 1 \text{ V}$) with optical injection at detuning $\Delta v_i = -2 \text{ GHz}$ and different values of injected power P_i , (a), (f), (k) 41 nW, (b), (g), (l) 1.9 μW , (c), (h), (m) 3.67 μW , (d), (i), (n) 14 μW , (e), (j), (o) 415.4 μW .

That similarity indicates that the analysis of the internal variables can be used for a better understanding of the effect of the OI on the OFC dynamics. We show in Fig. 4 the simulated temporal profiles of the output power, the frequency chirp, $\frac{1}{2\pi} \frac{d\Phi}{dt}$, and the optical phase, $\Phi(t)$, corresponding to Fig. 3. We have plotted the chirp because it plays a double role: on one hand, it gives a good idea on the evolution of the carrier density [24] and on the other hand, it helps to understand the evolution of the optical phase.

Fig. 4(a) shows that the optical power for a very low value of P_i is almost deterministic: in fact, minimum values of power are well above the power level where the fluctuations due to spontaneous emission dominate the evolution (around 10^{-7} mW). Power, chirping (Fig. 4(f)) and phase (Fig. 4(k)) are very similar to those corresponding to an OFC without OI [24]. Φ oscillates around a value that increases linearly with time with a slope given by $-2\pi \Delta v_i$ because the OFC is centered at v_{cw} and Φ is defined in the OI reference frame. The evolution of Φ shown in Fig. 4(I) and (m) illustrates the transition to locked OFC. Fig. 4(I) shows that just before locking, the increase shown

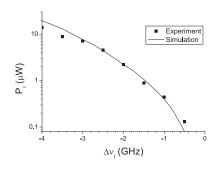


Fig. 5. Experimental (squares) and simulated (solid line) injected power necessary to get P1 dynamical regime as a function of the frequency detuning. In this figure $l_{bias} = 30$ mA, $f_R = 5$ GHz, and $V_{RF} = 1$ V.

in Fig. 4(k) disappears because there are regions in which Φ oscillates around a constant value with random duration. When the OFC locks to OI (Fig. 4(m)), Φ maintains its oscillation around a constant value for all times. P1 state is also characterized by smaller power fluctuations (compare Fig. 4(c) and (a)), smaller chirping fluctuations (compare Fig. 4(h) and (f)), and smaller fluctuations in the amplitude of phase oscillations. Smaller fluctuations due to locking explain that the spectra corresponding to P1 have higher CNR than those corresponding to free-running OFCs (compare Figs. 3(h) and 2(b)). However Δf_{10} in these spectra are similar because the frequency chirping and the Full Width at Half Maximum (FWHM) of optical power pulses for locked and free-running OFCs are similar (around 50 GHz and 32 ps, respectively). Fig. 4(d), (i) and (n) illustrate the dynamics for P2 regime corresponding to Fig 3(i). Phase and power traces show a clear repetition each $2/f_B$. Φ is a bounded quantity, as it was for P1 regime in Fig. 4(m), because frequency chirping excursions around zero value are symmetric (in the sense that the area above zero chirping equals to the area below). However the bounded character of Φ is not always maintained for locked OFCs. As P_i is increased Φ oscillates around a value that decreases linearly with time with $2\pi f_R$ slope, as it is illustrated in Fig. 4(o). Nevertheless the periodic character of the phase is maintained in a reference system centered at $v_i - f_R$ (instead of v_i) since Φ decreases 2π after each period. Φ decreases with time because chirping is no longer symmetric around zero, taking mostly negative values. Chirping excursions decrease [40], becoming smaller than those of previous cases, while the FWHM of the pulses increases (64 ps in Fig. 4(e)). In this way Δf_{10} decreases when P_i increases, as it can be observed in the experimental results shown in Fig. 3(e).

The main difference between the evolution of the optical phase in non-locked and locked OFCs becomes apparent when the evolution of the phase is analyzed in the reference frame of the SL at CW operation, ϕ_{cw} , instead of Φ , for the case of Fig. 4(k). For unlocked OFCs ϕ_{cw} also oscillates with similar amplitudes to those of Fig. 4(m) but the value around which oscillation occurs performs a Brownian motion that becomes apparent in a longer time scale (μ s) than that considered in Fig. 4. Also fluctuations in the amplitudes of ϕ_{cw} are much larger than those observed in Fig. 4(m). Phase behavior of the unlocked case of Fig. 4(k) is very similar to that observed for free-running OFCs. This was analyzed in [16] by assuming that the phase remains constant over the duration of the pulse and only varies from pulse to pulse. Our results are in agreement with those obtained with the assumption of a pulse-to-pulse phase performing a Brownian evolution while preserving some memory of the phase of the preceding pulses [16]. In contrast with free-running OFCs, when locked OFCs are considered Φ oscillates with a well defined amplitude around a constant value (see Fig. 4(m)), or around a value that changes linearly with time with a 2π phase change in each period (see Fig. 4(o)).

We characterize now the transition to P1 as a function of the frequency detuning. Fig. 5 shows experimental and simulation values of the minimum P_i required to achieve locking of the SL OFC to the ML. Experimentally this is done by fixing Δv_i and searching for the value of P_i for which we first get a spectrum similar to that of Fig. 3(c). Theoretically we look for the P_i value for which we first get a bounded Φ similar to that of Fig. 4(m). Good agreement is found between experimental

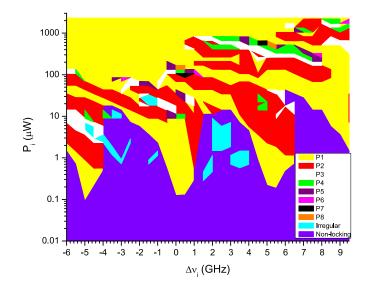


Fig. 6. Experimental values of the injected power as a function of the frequency detuning at which different dynamical regimes are observed for $I_{bias} = 30$ mA, $f_R = 5$ GHz, and $V_{RF} = 1$ V.

and theoretical results. Experimental results show that $\sqrt{P_i}$ decreases linearly with Δv_i : a linear fit gives $\sqrt{P_i} = -0.995 \Delta v_i - 0.362$, with $R^2 = 0.992$. This dependence coincides with that theoretically found for the saddle-node bifurcation that appears in CW lasers subject to OI [30]. However we note that the P_i required to lock an OFC is significantly smaller than that needed to lock a CW laser: for instance, for $\Delta v_i = -2$ GHz, the CW laser locks when $P_i = 6\mu$ W while the OFC locks when $P_i = 2.2 \mu$ W.

We now present experimental maps in the P_i vs Δv_i plane identifying the boundaries between regions with different nonlinear dynamics. We show in Fig. 6 the map obtained for $I_{bias} = 30$ mA, and $V_{RF} = 1$ V. The map is obtained by fixing Δv_i and increasing P_i by using the variable attenuator, without switching-off the ML. We obtain different dynamical behaviours including PN, unlocked, and irregular dynamics. We consider that a PN regime occurs when there are comb lines with an amplitude greater than 25 dB with respect to the noise level and this ratio is greater than 10 dB for some comb lines separated by f_R/N . Irregular dynamics is characterized by low values of the ratio between the intensity of comb lines and noise level. We consider that this irregular behaviour occurs when this ratio is smaller or equal than 25 dB for all comb lines. Other unlocked regions are labelled as Non-locking in Fig. 6.

The minimum injected power required to achieve P1 has local minima for detunings given by nf_R , i.e. injecting close to one of the comb lines. We obtain several regions of locked combs with a tongue shape around detuning values given by multiples of f_R . Map displays a clear asymmetry between negative and positive detuning regions. This asymmetry is due to the amplitude-phase coupling. For large values of P_i , P1 dynamics prevails when Δv_i is negative, while a much larger variety of PN regimes is observed when Δv_i is positive. Importantly, P1 is observed over a very wide Δv_i range, much larger than that observed for CW lasers under OI [30], in agreement with previous numerical simulations [17]. Then, an extended locking range is obtained showing that the locking capabilities of gain-switched lasers are higher than those of CW lasers where only a single locking range exists, provided that a different longitudinal mode is not excited.

Fig. 6 shows that P1 and P2 are the most widespread locked OFCs dynamics in the map. PN regions tend to appear as structures of Arnol'd tongue type. These structures can appear when periodically driven nonlinear oscillators are considered. They have been recently observed when an OFC is injected into a single-mode CW slave laser at detunings corresponding to rational fractions of f_R [31], [32]. This system is complementary to ours because the periodic forcing appears in the

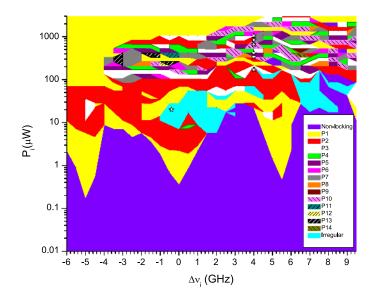


Fig. 7. Experimental values of the injected power as a function of the frequency detuning at which different dynamical regimes are observed for $l_{bias} = 30$ mA, $f_R = 5$ GHz, and $V_{RF} = 0.5$ V. White stars correspond to cases illustrated in Figs. 8 and 10.

electrical field equation while in our case that forcing appears in the carrier density equation. So in our case Arnol'd tongues can appear when the frequency detuning becomes resonant with a rational fraction of f_R and the OFC becomes frequency locked.

We also show in Fig. 7 the map obtained under the same conditions of Fig. 6 but decreasing the amplitude of the modulation, V_{RF} to 0.5 V. In this case the simulated optical spectrum without optical injection shows CNR = 47 dB and $\Delta f_{10} = 35$ GHz. Although some of the main features are similar to those of Fig. 6, we observe many more PN regions with higher values of N, and with smaller areas. We observe a larger variety of PN states when fixing a Δv_i value and increasing the P_i value, specially for positive values of the detuning. Dynamics is more complex than in Fig. 6 because the smaller value of V_{RF} causes a larger impact of the OI on the dynamical evolution. The level of complexity in the dynamics of a CW single-mode semiconductor laser when subject to optical injection [30] is much larger than that corresponding to a single-mode gain-switched laser without optical injection [41]. This is the reason why as V_{RF} decreases the dynamics of our system becomes more similar to the optically injected laser diode case, and therefore more complex dynamics can be expected.

We now discuss the evolution of the dynamical variables for PN states with large values of N for which a detailed comparison with simulations is desirable. In order to do this comparison we need to change the value of κ_c because Figs. 6 and 7 were obtained in different experiments to those discussed in Figs. 3 and 5. Values of optical power injected in the SL in experiments corresponding to Figs. 6 and 7 were smaller than those of Figs. 3 and 5 because light was more efficiently coupled in the SL in the experiments of Figs. 3 and 5. This can also be seen in the slight vertical shift downwards of the curve of Fig. 5 when compared to the corresponding curve in Fig. 6. For the case of $V_{RF} = 0.5$ V, we obtain that $\kappa_c = 1.5 \times 10^{11} s^{-1}$ when comparing experimental and simulated P_i needed to achieve locked OFCs at $\Delta v_i = -2$ GHz. We show in Fig. 8(a)–(f) experimental optical spectra obtained when increasing P_i for $\Delta v_i = 4$ GHz. These spectra correspond to the following sequence of PN states: P2, P5, P3, P10, P7, and P6. These cases are indicated with white stars in Fig. 7. PN spectra show a clear frequency locking because comb lines appear at $v_i + nf_R/N$, where *n* is an integer. We compare also the P2, P5, and P3 cases with the simulated spectra for similar values of P_i , shown in the last row of Fig. 8. We obtain a good agreement that permits us to explore the dynamical evolution of optical power, chirping and optical phase, that we show in Fig. 9.

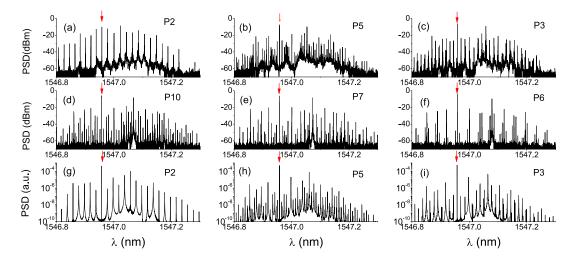


Fig. 8. Experimental (a–f) and simulated (g–i) optical spectra for $l_{bias} = 30$ mA, $f_R = 5$ GHz, and $V_{RF} = 0.5$ V with detuning $\Delta v_i = 4$ GHz and different values of injected power P_i . Experimental spectra correspond to P_i values of (a) 170 μW , (b) 331 μW , (c) 416 μW , (d) 663 μW , (e) 838 μW , and (f) 1060 μW . Simulated spectra correspond to P_i values of (g) 250 μW , (h) 338 μW , and (i) 416 μW . The injection wavelength is indicated with an arrow. In this figure $\kappa_c = 1.5 \times 10^{11} s^{-1}$.

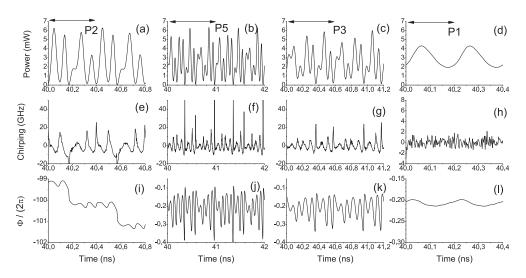


Fig. 9. Simulated power (upper row), chirping (middle row) and phase (lower row) of the gain-switched SL laser ($I_{bias} = 30 \text{ mA}$, $f_R = 5 \text{ GHz}$, and $V_{RF} = 0.5 \text{ V}$) with optical injection at detuning $\Delta v_i = 4 \text{ GHz}$ and different values of injected power P_i , (a), (e), (i) 250 μW , (b), (f), (j) 338 μW , (c), (g), (k) 416 μW , (d), (h), (i) 2300 μW . In this figure $\kappa_c = 1.5 \times 10^{11} s^{-1}$.

Fig. 9(a), (e), and (i) illustrate the dynamics for the P2 regime corresponding to Fig 8(g). The period has been indicated with an horizontal arrow. Power and chirping traces show a clear repetition each $2/f_R$. Phase is locked because Φ decreases 2π each $2/f_R$ in a similar way to the change of 2π each $1/f_R$ observed in Fig. 4(o). Our condition for phase locking goes beyond that of [42] because we consider that also a system with unbounded phase can be phase locked if the phase changes in 2π after each period of the dynamics. Dynamics for P5 and P3 regimes, shown in the second and third column of Fig. 9, repeat each $5/f_R$ and $3/f_R$, respectively. Phases are bounded and locked because they repeat with the previous periodicities, as seen in Fig. 9(j) and (k). This is

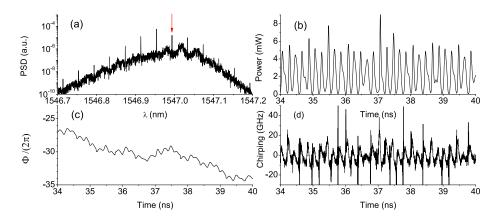


Fig. 10. Simulated (a) optical spectrum, and time traces of (b) power, (c) optical phase, and (d) frequency chirping at $l_{bias} = 30$ mA, $f_R = 5$ GHz, $V_{RF} = 0.5$ V, $\Delta v_i = -0.4$ GHz, and $P_i = 20 \ \mu W$. In this figure $\kappa_c = 1.5 \times 10^{11} s^{-1}$. The wavelength of the optical injection is indicated with an arrow.

also the situation shown in the last column of Fig. 9 in which we illustrate that P1 is obtained when P_i is large enough, as obtained also experimentally.

We now illustrate the irregular dynamical behavior that appears in the maps of Figs. 6 and 7. Fig. 10 shows the simulated optical spectrum and the time traces corresponding to the highlighted point in the largest irregular region of Fig. 7. The optical spectrum features a broad pedestal on which comb lines separated by the repetition frequency f_R are still visible. Therefore, though the optical power emission is still pulsed with a repetition frequency f_R , the pulses are irregular in shape, height and width, as it is shown in Fig. 10(b). Fig. 10(c) shows the irregular and unbounded character of the optical phase. This behaviour is dominated by the deterministic evolution because the gain-switched SL is not completely switched-off between pulses (the minimum value of power in Fig. 10(b) is 10^{-4} mW). Then the observed irregular dynamics can correspond to chaotic dynamics. In fact, we have checked that similar behavior is obtained when a much smaller value of β factor is considered ($\beta = 10^{-12}$).

In the non-locking region we can find combs that are frequency-locked but do not fulfill the phase locking condition. These are for instance those obtained for low values of P_i when the MLs frequency becomes resonant with a rational fraction of f_R . One example is when light is injected at the middle of the two main tongues, $\Delta v_i = -2.5$ GHz, and $P_i = 50$ nW. The optical spectrum is similar to that of P2. However the dynamical state is not P2 because the phase is not locked. When plotted in the reference frame of the SL at CW operation the phase oscillates around a value performing a Brownian evolution, so it is not repeated after a $2/f_R$ time.

Finally, we discuss the presence of multistability in our system. Multistability is characterized by the coexistence of several stable states for a fixed set of parameters. We have checked that a similar map to that of Fig. 6 is obtained when repeating the experiment in the same way. However, if we consider an alternative measurement method in which we fix P_i and change the ML frequency we observe that some dynamical regions appearing in Fig. 6 do not appear in the new measurements. These preliminar results seem to indicate that there is multistable behaviour in our system because there are differences between maps obtained by using different measurement procedures. Further investigations would be desirable to characterize multistability but they are outside the scope of this paper.

5. Conclusion

We have presented an experimental and theoretical study on the effect of optical injection on a high quality OFC generated by gain-switching a single-mode semiconductor laser. We have focused

on the nonlinear dynamics obtained when the bias current is modulated with a sinusoidal signal of f_{B} frequency. By using high-resolution optical spectra, we have measured two maps in which we have observed dynamics corresponding to injection-locked, unlocked and irregular combs. Injection-locked combs have been characterized in terms of their frequency and phase locking behavior. Several types of injection-locked combs have been obtained in which the frequency spacing between lines is equal to rational fractions of f_R . In the maps we have found different regions of locked combs with a tongue shape around detuning values given by multiples of f_{R} . An extended locking range for OFCs has been obtained when compared to CW lasers subject to optical injection. For large values of the modulation amplitude, locked regions mainly include combs with small values of the period, typically $1/f_R$ or $2/f_R$. For smaller values of the modulation amplitude, the map is characterized by the appearance of many small-size locked regions with larger values of the period, N/f_R , with N > 2 and up to 14. A very good agreement has been obtained between numerical simulations and experimental results. Our results have shown that optical frequency combs with different values of the frequency spacing can be obtained by using appropriate optical injection. PN dynamics can be useful for improving the resolution in dual-comb spectroscopy using gain-switched lasers while maintaining the large values of the spectral width obtained when f_R is close to the relaxation oscillation frequency.

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