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NONLINEARITY MINIMUMS AND MAXIMUMS OF  
A PHASE-SENSITIVE DETECTION SYSTEM\*

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June 1969

Abstract — Two generalized criteria for minimums and maximums of essential nonlinearity of a phase-sensitive detection system are presented. Minimums and maximums are calculated and plotted by a digital computer over a wide dynamic range of operating conditions, assuming that the input signal is in the narrow-band Gaussian noise.

Recent investigations [1], [2] have shown that in the instrumentation of experimental research the total nonlinearity of a phase-sensitive detection system is of prime importance. In most cases of practical interest, the total system nonlinearity is determined by the essential nonlinearity of the characteristics of the phase-sensitive detector used. The nonlinearity minimums  $N_{BMIN}$  and maximums  $N_{CMAX}$  of the detector characteristics are particularly important. Both nonlinearities were calculated in previous work [2] for a number of discrete values of the input signal-to-noise ratio  $X = V_s/V_\sigma$ , and the reference wave-to-noise ratio  $\mu = V_c/V_\sigma$ ; where  $V_s$  is the amplitude of the input sine wave,

$V_{\sigma}$  is the rms value of the input narrow-band noise, and  $V_c$  is the amplitude of the reference wave. Johnson [3] has pointed out a possibility of the existence of additional nonlinearity minimums and maximums which can be larger or smaller in value than those calculated in [2], due to the relatively complicated formulas expressing conditions for  $N_{\text{BMIN}}$  and  $N_{\text{CMAX}}$  as well as to the  $N_{\text{BMIN}}$  and  $N_{\text{CMAX}}$  calculations made by a relatively small number of discrete values of  $V_s$ ,  $V_c$ ,  $V_{\sigma}$ , and  $\psi$  ( $\psi$  is the phase angle between the input signal and the reference wave).

Based on reference [2], careful investigations show that a generalized criterion for  $N_{\text{BMIN}}$  is given by

$$w[f(x_B)] \left\{ \gamma^*(x_B, \mu, \psi) s[v(x_B)] - \phi^*(x_B, \mu, \psi) m[t(x_B)] + y[t(x_B)] - u[v(x_B)] \right\} - \left( \frac{x_B}{2} \right)^2 K[f(x_B)] \left\{ y[t(x_B)] - u[v(x_B)] \right\} = 0, \quad (1)$$

where functions  $w[f(x_B)]$ ,  $\gamma^*(x_B, \mu, \psi)$ ,  $s[v(x_B)]$ ,  $\phi^*(x_B, \mu, \psi)$ ,  $m[t(x_B)]$ ,  $y[t(x_B)]$ ,  $u[v(x_B)]$ , and  $K[f(x_B)]$  are given by:

$$w[f(x_B)] = {}_1F_1 \left( \frac{1}{2}; 2; -\frac{\mu^2 + x_B^2}{2} \right) \quad (2)$$

$$\gamma^*(x_B, \mu, \psi) = \frac{x_B^2}{2} + \frac{\mu \cos \psi}{2} x_B \quad (3)$$

$$s[v(x_B)] = {}_1F_1 \left( \frac{1}{2}; 2; -\frac{\mu^2 + x_B^2 + 2\mu x_B \cos \psi}{2} \right) \quad (4)$$

$$\phi^*(x_B, \mu, \psi) = \frac{x_B^2}{2} - \frac{\mu \cos \psi}{2} x_B \quad (5)$$

$$m[t(x_B)] = {}_1F_1 \left( \frac{1}{2}; 2; -\frac{\mu^2 + x_B^2 - 2\mu x_B \cos \psi}{2} \right) \quad (6)$$

$$y[t(x_B)] = {}_1F_1 \left( -\frac{1}{2}; 1; -\frac{\mu^2 + x_B^2 - 2\mu x_B \cos \psi}{2} \right) \quad (7)$$

$$u[v(x_B)] = {}_1F_1 \left( -\frac{1}{2}; 1; -\frac{\mu^2 + x_B^2 + 2\mu x_B \cos \psi}{2} \right) \quad (8)$$

$$K[f(x_B)] = {}_1F_1 \left( \frac{3}{2}; 3; -\frac{\mu^2 + x_B^2}{2} \right). \quad (9)$$

where  ${}_1F_1$  denotes the confluent hypergeometric function.

By means of computer-aided analysis, using numerical solutions of Eq. (1), and high-density discrete-value calculations, the minimum nonlinearity expressed as

$$N_{BMIN} = f^*(x_B)_{\mu, \psi} \quad (10)$$

is calculated and plotted in Fig. 1. From curves it can be seen that  $N_{BMIN}$  is a monotonously decreasing function of  $x_B$  having a fast rate of decrease of almost a half order of magnitude for  $x_B \leq 10$ .  $N_{BMIN}$  varies less than 16% for  $x_B \geq 10$  and  $\psi \leq \pi/6$ . For  $x_B \geq 10$  and  $\psi \geq \pi/6$ ,  $N_{BMIN}$  has approximately a constant value with variation of  $x_B$ . Furthermore, there are  $N_{BMIN}$  accumulation points at  $x_B = 2.37295$  for  $\mu \leq 0.1$  and for any value of  $\psi$ . The  $N_{BMIN}$  accumulation points are maximum values of  $N_{BMIN}$  for a given value of  $\psi$ .

Similarly, a generalized criterion for the maximum nonlinearity  $N_{\text{CMAX}}$  is given by

$$\left\{ \phi[g(x_C)] - z[h(x_C)] \right\} \left\{ y^*(x_C, \mu, \psi) m[t(x_C)] - w^*(x_C, \mu, \psi) s[v(x_C)] \right\} + \left\{ s^*(x_C, \mu) \rho[g(x_C)] - v^*(x_C, \mu) \ell[h(x_C)] \right\} \left\{ u[v(x_C)] - y[t(x_C)] \right\} = 0, \quad (11)$$

where functions  $m[t(x_C)]$ ,  $s[v(x_C)]$ ,  $u[v(x_C)]$ , and  $y[t(x_C)]$  are given by relations (6), (4), (8), and (8), respectively. Other functions are defined by:

$$\phi[g(x_C)] = {}_1F_1 \left[ -\frac{1}{2}; 1; -\frac{(\mu + x_C)^2}{2} \right] \quad (12)$$

$$z[h(x_C)] = {}_1F_1 \left[ -\frac{1}{2}; 1; -\frac{(\mu - x_C)^2}{2} \right] \quad (13)$$

$$y^*(x_C, \mu, \psi) = \frac{x_C}{2} - \frac{\mu}{2} \cos \psi \quad (14)$$

$$w^*(x_C, \mu, \psi) = \frac{x_C}{2} + \frac{\mu}{2} \cos \psi \quad (15)$$

$$s^*(x_C, \mu) = \frac{x_C + \mu}{2} \quad (16)$$

$$\rho[g(x_C)] = {}_1F_1 \left[ \frac{1}{2}; 2; -\frac{(\mu + x_C)^2}{2} \right] \quad (17)$$

$$v^*(x_C, \mu) = \frac{x_C - \mu}{2} \quad (18)$$

$$\ell[h(x_C)] = {}_1F_1 \left[ \frac{1}{2}; 2; -\frac{(\mu - x_C)^2}{2} \right] \quad (19)$$

The maximum nonlinearity expressed as

$$N_{\text{CMAX}} = \varphi^*(x_C)_{\mu, \psi} \quad (20)$$

is calculated and plotted in Fig. 2 using a high-density discrete-value calculations approach. From the curves in Fig. 2 we see that  $N_{\text{CMAX}}$  is a monotonously increasing function of  $x_C$ , having a fast rate of increase depending upon  $\psi$  value.  $N_{\text{CMAX}}$  accumulation points are again at  $x_C = 2.37295$  for  $\mu \leq 0.1$  and for any value of  $\psi$ . Generally  $N_{\text{CMAX}}$  accumulation points are minimum values of  $N_{\text{CMAX}}$  for a given value of  $\psi$ .

Furthermore, applying the same method as in previous considerations, it is also of interest to calculate over a wide dynamic range of operating conditions the normalized form of the phase-sensitive detector characteristics as a function of  $\psi$ , for various values of  $\mu$  and calculated values of  $x_B$  and  $x_C$ , considering above given criteria. According to [2], normalized forms of the detector characteristics as a function of  $\psi$ , with  $\mu$ ,  $x_B$ , and  $x_C$  as parameters are given by

$$\left( \frac{v_0}{\eta_d v_{\sigma}} \right)_B = \left( \frac{\pi}{2} \right)^{1/2} \left\{ u[v(x_B)] - y[t(x_B)] \right\} \quad (21a)$$

and

$$\left( \frac{v_0}{\eta_d v_{\sigma}} \right)_C = \left( \frac{\pi}{2} \right)^{1/2} \left\{ u[v(x_C)] - y[t(x_C)] \right\}, \quad (21b)$$

where  $v_0$  and  $\eta_d$  are the detector output signal and detector efficiency, respectively.



Calculations shown that the numerical values of  $x_B$  and  $x_C$  are very close over a wide range of  $\mu$  and  $\psi$ , although  $x_B$  gives the condition for minimum nonlinearity, and  $x_C$  for maximum nonlinearity. Consequently, both functions (21a) and (21b) are represented by one curve for a set of value of  $\mu$ ,  $\psi$ , and  $x_B$  or  $x_C$ . Curves show that the normalized output signal is almost independent of the phase angle for a ratio  $\psi \leq 0.2$ . For a  $\psi \geq 0.2$  ratio, the normalized output signal considerably decreases its value, achieving  $V_0/\eta_d V_\sigma = 0$  for  $\psi = \pi/2$ .

From conclusions derived from generalized criteria (1), (11), (21a), and (21b), as well as from curves in Figs. 1, 2, and 3 follows a full agreement with results presented in [1] and [2] for  $N_{BMIN}$  and  $N_{CMAX}$ . Of course, the generalized criteria give more information about behaviour of minimum and maximum nonlinearities than previously published results.

#### ACKNOWLEDGEMENT

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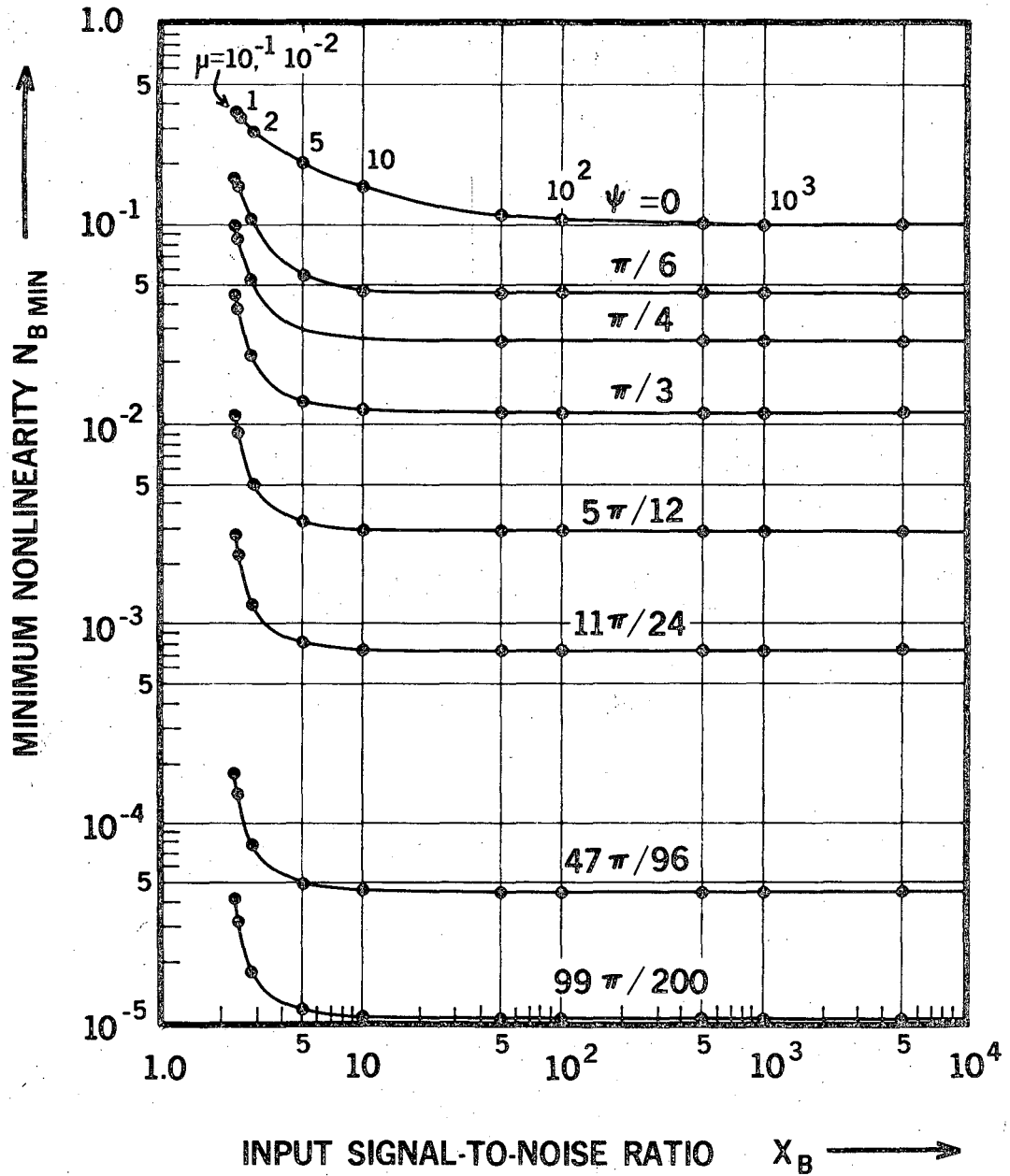
1. B. Leskovar, Phase-Sensitive Detector Nonlinearity at the Signal Detection in the Presence of Noise, IEEE Transactions on Instrumentation and Measurements, Vol. IM-16, No. 4, pp. 285-294, 1967.
2. B. Leskovar, Essential Nonlinearity of Phase-Sensitive Detector Characteristics, in Proceedings of the 6th Allerton Conference on Circuit and System Theory, Urbana, Illinois, 1968.
3. A. R. Johnson, private communication, 1969.

#### Figure Legends

Fig. 1. Minimum nonlinearity  $N_{BMIN}$  as a function of the optimum value of the input signal-to-noise ratio  $x_B$ , with the phase angle  $\psi$  and the reference wave-to-input noise ratio  $\mu = 10^{-2}, 10^{-1}, 1, 2, 5, 10, 10^2, \text{ and } 10^3$  as parameters.

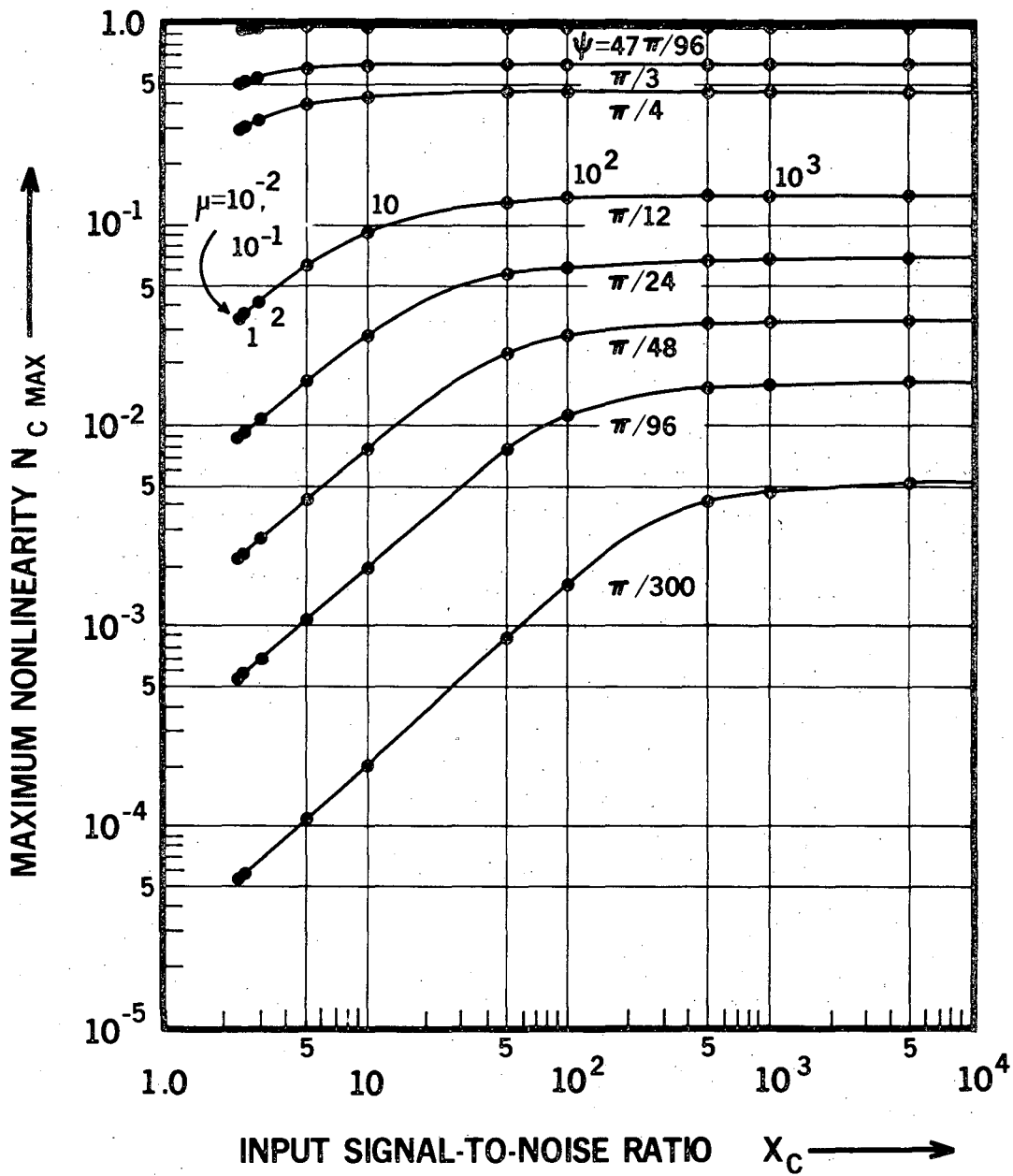
Fig. 2. Maximum nonlinearity  $N_{CMAX}$  as a function of the nonoptimum value of the input signal-to-noise ratio  $x_C$ , with the phase angle  $\psi$  and the reference wave-to-input noise ratio  $\mu = 10^{-2}, 10^{-1}, 1, 5, 10, 10^2, \text{ and } 10^3$  as parameters.

Fig. 3. The normalized phase-sensitive detector characteristics as a function of the phase angle  $\psi$ , with the optimum values  $x_B$ , the nonoptimum values  $x_C$ , and the reference wave-to-input noise ratio  $\mu = 10^{-2}, 10^{-1}, 1.0, 10, 10^2, 10^3 \text{ and } 10^4$  as parameters.



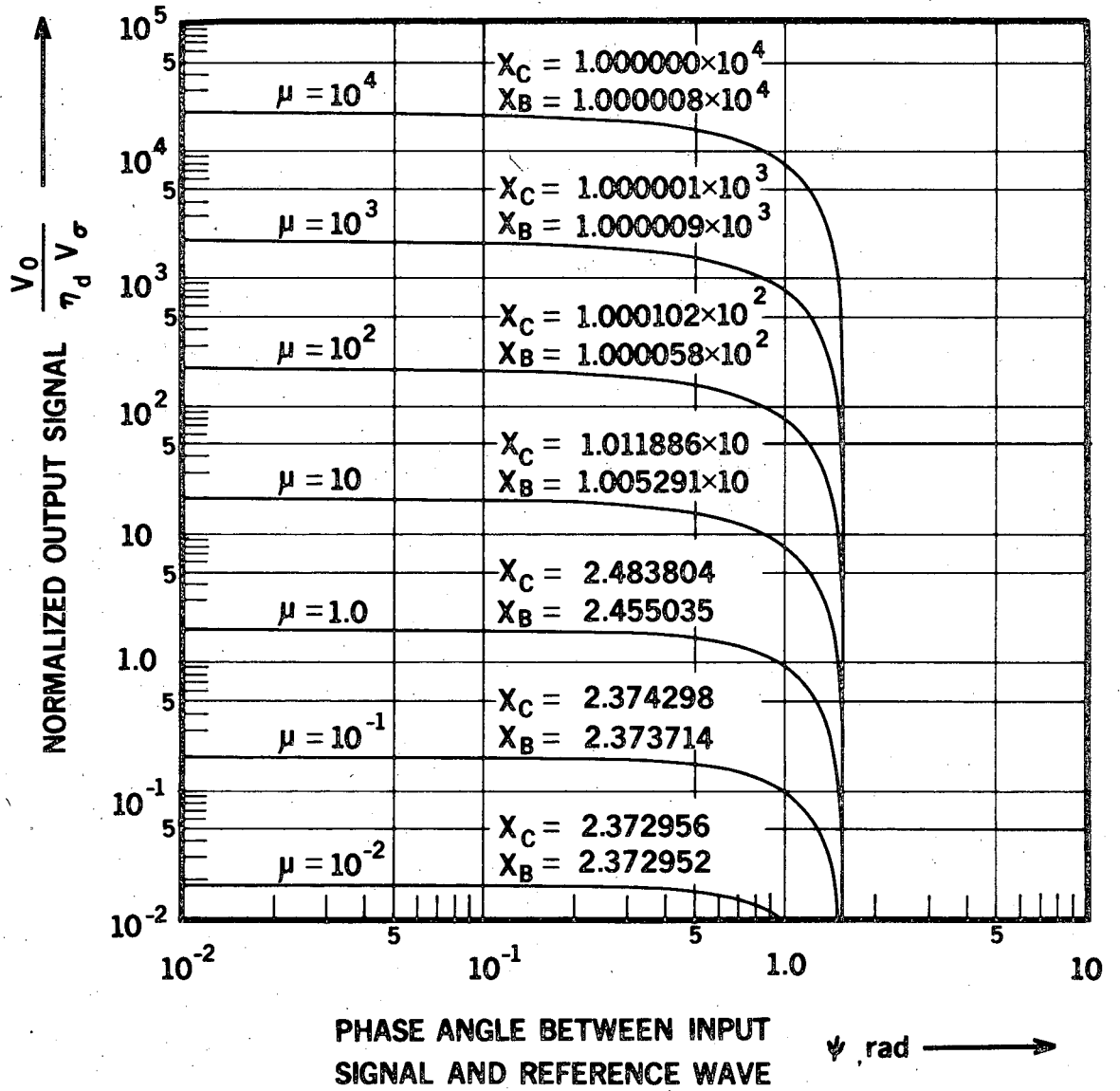
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Fig. 1



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Fig. 2



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Fig. 3

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