

Research Article

Novel Method for Optimal Synthesis of 5G Millimeter Wave Linear Antenna Array

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We will propose a useful method for 5G mm wave antenna array synthesis, based on Genetic Algorithm for the synthesis of linear array with nonuniform interelement spacing. Our design method was used to obtain the optimal position of the elements in order to get the minimum side lobe level and nulls in desired directions. The simulation results verify that proposed method outperforms the previously published methods in terms of suppression side lobe level while maintaining nulls in specified directions. The flexibility of proposed algorithm shows good potential for the antenna array synthesis.

1. Introduction

In order to satisfy necessary 5G quality-of-standard criteria and meet user mobility, due to the higher path loss at mm wave frequency range, multiple antenna arrays are typically used in outdoor mm wave systems for providing additional gain [1, 2]. They play an important role in detecting and processing signals arriving from different directions. The performance of the systems depends on the efficient design of the antenna arrays. The desired radiation pattern can be realized by choosing geometrical shape of antenna array, element excitation amplitude, element excitation phase, and element spacing. The objectives in design of the antenna arrays are archiving minimum side lobe level (SLL) and narrow first null beam width (FNBW). Interference issues will become of crucial importance for coexistence of 5G devices, since number of mm wave devices will grow extensively in near future [3]. The increasing growth of 5G devices number will prompt the study of array pattern nulling techniques. This problem will reach its culmination in future dense mm wave application, such as for the 60 GHz dense indoor communication, and various outdoor mm wave 5G communication in densely populated urban areas [4]. So the goal of antenna array synthesis is to achieve the minimum SLL with narrow

FNBW and obtaining narrow or broad nulls in directions of interfering signals. The broad nulls are needed when the direction of arrival of interference may vary slightly with time.

For the linear array geometry, by optimizing the spacing between the elements while keeping the uniform excitation we can suppress side lobe level while preserving the gain of the main beam and can control nulling.

Methods used for the antenna array synthesis can be classified in two categories: deterministic and stochastic. There are several deterministic methods: Schelkunoff Polynomial Method [5], Dolph-Chebyshev Method [6, 7], Woodward-Lawson Method [8, 9], and Fourier Transform Method [6, 8, 9]. In modern research the most common methods are stochastic, because stochastic methods can almost all be proven to find a global minimum with asymptotic convergence in probability. The biggest advantages of using stochastic methods are their ability in dealing with large number of optimization parameters and avoiding getting stuck in local minima. Some of the methods used for the antenna array synthesis are Evolutionary Algorithms (EA) [10], Genetic Algorithms (GA) [11–13], Tabu Search (TS) [11, 14], Particle Swarm Optimization (PSO) [15–17], Ant Colony Optimization (ACO) [18], Nature-Inspired Cuckoo Search

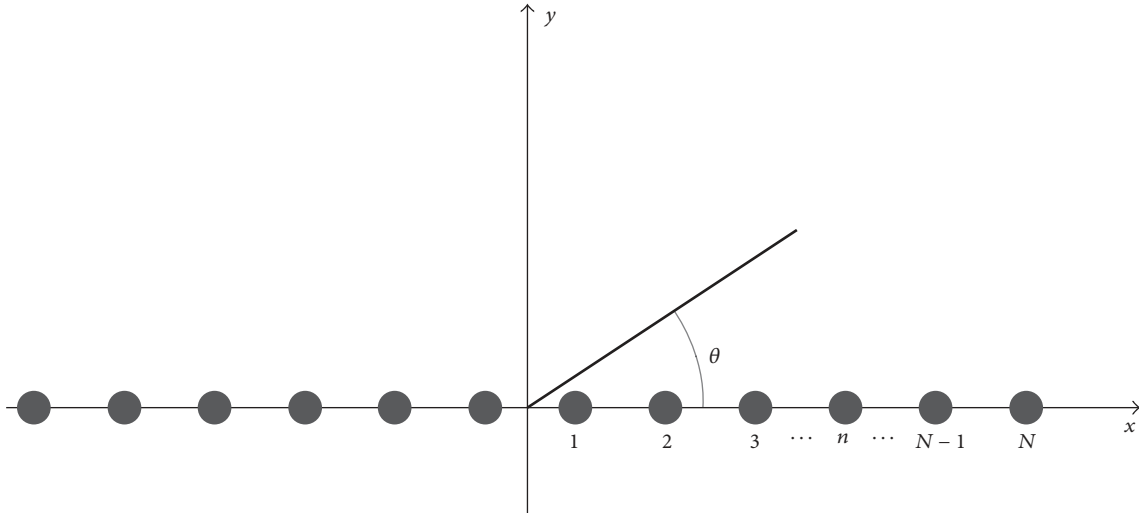


FIGURE 1: Geometry of $2N$ -element linear antenna array.

(CS) [19, 20], Combination of Global and Local Search [21], and Cat Swarm Optimization [22]. All the above-mentioned methods have shown the capability of searching for global solution in electromagnetic optimization problems.

In this paper, we proposed a useful method based on combination of two global searches. The main idea comes from method based on combination of global and local search [21]. Changing local search into global search we avoid getting stuck in local minimum and this leads to better exploration of feasible region. Better exploration leads to better solution of optimization problem. Presented algorithm was used to obtain the optimal position of the elements in order to get the minimum side lobe level and nulls in desired directions. We applied for optimization the same radiation pattern requirements of the selected papers. The simulation results reveal that design of antenna arrays using the presented method provides considerable enhancements compared with the synthesis obtained from other published methods. In this approach we will concern arrays of isotropic point sources; this is of great value because the pattern of any antenna can be regarded as being produced by an array of point sources.

Description of antenna array design problem is given in Section 2. In Section 3, a description of the used algorithm is presented. Results are presented in Section 4. Finally, the conclusion of this work is presented in Section 5.

2. Problem Formulation

The antenna array radiation pattern (RP) may be found according to the pattern multiplication theorem (see, e.g., Ch. 6 from [6, 24] and Ch. 3 from [25]):

$$\text{RP} = \text{EL} \cdot \text{AF}. \quad (1)$$

EL (element pattern) is the pattern of the individual array element.

AF (array factor) is a function dependent on the physical placement of antenna elements, amplitude, and phase of excitation.

If we replace each element of the antenna array with an isotropic point source the resulting pattern is the array factor, because the element pattern of isotropic point source is equal to 1. The geometry of the linear antenna array with $2N$ isotropic elements placed symmetrically along the x -axis is given in Figure 1.

In this paper linear antenna array has identical elements with nonuniform interelement spacing and uniform excitation. Array factor in the azimuth plane can be expressed as follows (for more see [6, 8, 9, 24–26]):

$$\text{AF}(\theta) = 2 \sum_{n=1}^N I_n \cos [kd_n \sin(\theta) + \varphi_n], \quad (2)$$

where $k = 2\pi/\lambda$ is wave number, λ is the wavelength, I_n is excitation amplitude of n th element, φ_n is excitation phase of n th element, d_n is location of n th element, and θ is angle between the line of observer and the source position.

If we assume a uniform excitation of phase as $\varphi_n = 0$ for each antenna array element, the array factor can be written in a simple form as follows:

$$\text{AF}(\theta) = 2 \sum_{n=1}^N I_n \cos [kd_n \sin(\theta)]. \quad (3)$$

In the field of electromagnetism the decibel (dB) is often used as a unit of measurement for array factor. Normalized array factor and normalized array factor in dB are given by

$$(\text{AF}(\theta))_{\text{norm}} = \frac{|\text{AF}(\theta)|}{|\max(\text{AF}(\theta))|}, \quad (4)$$

$$(\text{AF}(\theta))_{\text{norm,db}} = 20 \log \frac{|\text{AF}(\theta)|}{|\max(\text{AF}(\theta))|}. \quad (5)$$

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Begin
Set an initial solution  $x^1$ ;
Define  $k_{\max}$ ,  $R$  and  $l_{\max}$ ;
Set  $k \leftarrow 1, l \leftarrow 1, \text{SLL}^* = 0, x^* = 0$ ;
if (cost function is with nulls) set  $\text{depp}_k^* = -60$  dB;
Global search for  $\theta$ . Solution of the search is  $\theta^1$ ;
While ( $l < l_{\max}$ )
  Global search for  $x$ . Solution of the search is  $x^{l+1}$ ;
  Global search for  $\theta$ . Solution of the search is  $\theta^{l+1}$ ;
  Set  $\text{SLL}^{l+1} = \text{AF}(\theta^{l+1})_{\text{norm}}$ ;
  if (cost function is with nulls)  $\text{depp}_k = \text{AF}(\theta_k)_{\text{norm}}$ ;
  end
  if (cost function is with nulls)
    if ( $\text{SLL}^{l+1}$  is better than  $\text{SLL}^*$  and  $\text{depp}_k < \text{depp}_k^*$ )
      set  $k \leftarrow 1, \text{SLL}^* = \text{SLL}^{l+1}$  and  $x^* = x^{l+1}$ ; end
    else
      if ( $\text{SLL}^{l+1}$  is better than  $\text{SLL}^*$ ) set  $k \leftarrow 1, \text{SLL}^* = \text{SLL}^{l+1}$  and  $x^* = x^{l+1}$ ; end
    end
  If ( $k \geq k_{\max}$ ) STOP;
  end
   $l \leftarrow l + 1$ ;
   $k \leftarrow k + 1$ ;
end
Outputs of the algorithm are  $\text{SLL}^*$  and  $x^*$ ;
end

```

ALGORITHM 1

3. Algorithm

The presented algorithm is applied to achieve the desired radiation pattern with minimum SLL and narrow or broad nulls in specified directions. Our approach uses a combination of two global searches: global search with respect to θ and global search with respect to x . The global searches were performed using Genetic Algorithm with existing function “ga” from MATLAB software package (R2016a). The global search with respect to θ was performed on region $[\theta_{11}, \theta_{12}]$ with fixed permanent solution x^l for the cost function (4). With this global search we locate maximum side lobe level.

The cost function for step global search for x following expression was used:

$$\text{Cost} = \max \left(\text{AF}(\theta)_{\text{norm}} \Big|_{\theta_{11}}^{\theta_{12}} \right) + \sum_k \text{AF}(\theta_k)_{\text{norm}}. \quad (6)$$

First term in (6) is employed to minimize the side lobe level between the desired angles θ_{11} and θ_{12} , whereas the second one is for achieving deep nulls in desired directions θ_k . For reducing mutual coupling effects between the elements of the antenna array the following conditions must be satisfied:

$$\begin{aligned} |x_i - x_j| &> 0.25\lambda, \\ \min(x_i) &> 0.125\lambda, \quad i = 1, 2, \dots, N, \quad i \neq j. \end{aligned} \quad (7)$$

The global search with respect to x on a small neighbourhood of current solution was performed with fixed θ^l . Lower

and upper bounds for each coordinate of vector x^l are defined using the following expression:

$$\begin{aligned} \text{LOW}_i &= (x_i^l - R), \quad i \in N, \quad R \in \mathfrak{R}, \\ \text{UP}_i &= (x_i^l + R), \quad i \in N, \quad R \in \mathfrak{R}. \end{aligned} \quad (8)$$

Pseudocode of proposed algorithm is given in Algorithm 1.

4. Simulation Results

In the first experiment we performed the synthesis of $2N = 28$ element antenna array in order to get the minimum side lobe level and nulls at $\theta_1 = 30^\circ$, $\theta_2 = 32.5^\circ$, and, $\theta_3 = 35^\circ$. In this paper we performed experiments for $R = 0.05$ and 0.1 (with respect to $\lambda/2$) where $\theta_{11} = 4^\circ$ and $\theta_{12} = 90^\circ$.

The cost function for the algorithm following expression was used:

$$\text{Cost} = \max \left(\text{AF}(\theta)_{\text{norm}} \Big|_{4^\circ}^{90^\circ} \right) + \sum_k \text{AF}(\theta_k)_{\text{norm}}. \quad (9)$$

We can see that in this paper cost function is not same as that in paper [23]. The main reason why the form of the cost function (9) was taken, rather than form (10), is that the value of the second part of cost function tends towards negative infinity for $\text{AF}(\theta_k)_{\text{norm}} = 0$. This case would adversely affect the search in such a way that the search for the second part of (10) would be predominant. In this case, we took normalized

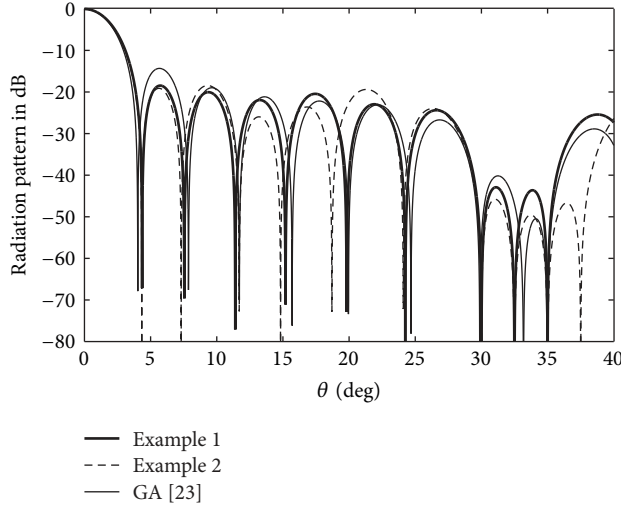


FIGURE 2: The normalized radiation pattern of 28-element linear array.

array factor and therefore it is unlikely that such a case could occur.

$$\text{Cost} = 20 \log \left\{ \max \left(\text{AF}(\theta)_{\text{norm}} \Big|_{4^{\circ}}^{90^{\circ}} \right) \right\} + 20 \log \left\{ \sum_k \text{AF}(\theta_k)_{\text{norm}} \right\}. \quad (10)$$

The radiation pattern has been shown in Figure 2. As it is seen from Figure 2 obtained results give lower side lobe level than results from paper [23]. Region $[30^{\circ}, 35^{\circ}]$ is under -40 dB and it is lower than obtained region from published work. The optimal locations with respect to λ obtained by using the provided algorithm are shown in Table 1. In Table 2 SLL, FNBW, and nulls depth at $\theta_1 = 30^{\circ}$, $\theta_2 = 32.5^{\circ}$, and $\theta_3 = 35^{\circ}$ are shown. Convergence characteristics in terms of side lobe level versus the number of iterations are shown in Figure 3. It is observed that the cost function value converges to the optimum result quickly.

The observed results were better for $R = 0.05$. From Table 2, it is seen that the results provide side lobe level lower than -18 dB, with nulls deeper than -100 dB. Minimum side lobe level of the array optimized using presented algorithm showed improvement (4 dB) over the published works GPS [23], ACO [18], and CSO [22] (Table 3). All three nulls are deeper than -100 dB and all nulls are deeper than nulls from published works. The FNBW is slightly higher than previously published works.

In the second experiment, we performed the synthesis of $2N = 20$ elements' antenna array with fixed excitation Dolph-Chebyshev amplitudes, which form the side lobe level at -30 dB. Excitation amplitudes have values = $[1, 0.97, 0.912, 0.831, 0.731, 0.620, 0.504, 0.391, 0.285, 0.325]$. Null is located at the position of $\theta_1 = 20^{\circ}$, whereas $\theta_{11} = 8^{\circ}$ and $\theta_{12} = 90^{\circ}$.

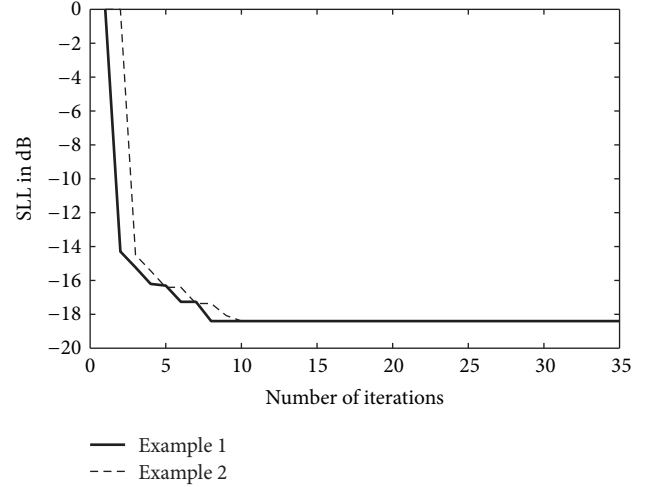


FIGURE 3: The convergence characteristics of side lobe level for optimization of a 28-element linear array.

TABLE 1: Element position of the 28-element linear array (normalized with respect to λ).

Element	Example 1 ($R = 0.05$)	Example 2 ($R = 0.1$)	GA [23]
± 1	0.1901	0.2081	0.252
± 2	0.6309	0.6048	0.752
± 3	1.0720	1.0688	1.251
± 4	1.5273	1.4997	1.754
± 5	2.0043	1.8792	2.257
± 6	2.4929	2.4284	2.756
± 7	2.9220	3.0077	3.284
± 8	3.5061	3.5671	3.792
± 9	3.9975	4.1606	4.291
± 10	4.4910	4.5425	4.790
± 11	5.2269	5.2225	5.463
± 12	5.9271	6.0085	5.965
± 13	6.4800	6.5472	6.465
± 14	7.1298	7.2607	7.094

TABLE 2: Comparative results for $2N = 28$ elements' linear array.

	SLL	FNBW	Null depth in dB		
			30°	32.5°	35°
Example 1 ($R = 0.05$)	-18.41	8.7	-163.19	-100.01	-186
Example 2 ($R = 0.1$)	-18.39	8.6	-171.77	-140.42	-164.82

For the objective function the following relations were taken:

$$\text{Cost} = \max \left(\text{AF}(\theta)_{\text{norm}} \Big|_{8^{\circ}}^{90^{\circ}} \right) + \text{AF}(20^{\circ})_{\text{norm}}. \quad (11)$$

Mutual coupling effects were under consideration during the processing. In this experiment, we fixed $R = 0.1$. The optimal locations with respect to λ obtained by using the provided algorithm are shown in Table 4 together with the results obtained in [23].

TABLE 3: Comparison with published results for $2N = 28$ elements optimized with respect to position.

	SLL	FNBW	Null depth in dB		
			30°	32.5°	35°
Example 1 ($R = 0.05$)	-18.41	8.7	-163.19	-100.01	-186
GPS [23]	-14.39	7.8	-71.89	-46.87	-74.13
ACO [18]	-14.88	8.4	-57.42	-59.20	-60.46
CSO [22]	-13.23	8.2	-75.00	-67.05	-65.32

TABLE 4: Element position of the 20 element linear array (normalized with respect to λ).

Element	Obtained results	GPS [23]	GA [23]
± 1	0.2387	0.25	0.264
± 2	0.7396	0.75	0.779
± 3	1.2454	1.25	1.283
± 4	1.7750	1.787	1.840
± 5	2.2821	2.338	2.382
± 6	2.7785	2.838	2.884
± 7	3.2473	3.338	3.389
± 8	3.7092	3.838	3.897
± 9	4.2077	4.338	4.419
± 10	4.8180	4.990	5.079

TABLE 5: Comparison with published results for $2N = 20$ elements optimized with respect to position.

	SLL	FNBW	Null depth in dB at 20°
Obtained results	-28.5025	16.8	-233.00
GPS [23]	-27.7376	16.9	-61.01
GA [23]	-26.6344	16.4	-80.06

Figure 4 shows a radiation pattern produced by the presented method together with radiation pattern obtained in the work [23]. We can notice that the resulting null is at the position of 20°. In Table 5 SLL, FNBW, and null depth at $\theta_1 = 20^\circ$ are shown. We can also notice that SLL obtained by presented method is -0.8 dB lower than the examined results obtained in [23]. Radiation pattern obtained with the presented method has a deeper null than the published work [23]. FNBW has a negligible difference.

5. Conclusion

In the presented work, we proposed a new algorithm for finding the optimal position of the 5G mm wave antenna array elements which minimize side lobe level and placing nulls in desired directions. In both experiments, suppression of SLL was achieved, while nulls were maintained in specified directions and cost function value of presented method converges to the optimum result quickly. Given algorithm provides better results than the compared methods and shows good potential for the 5G mm wave antenna array synthesis.

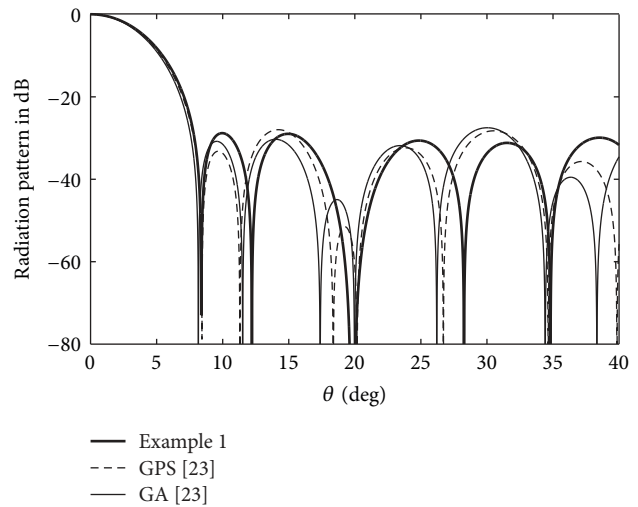


FIGURE 4: The normalized radiation pattern of 20-element linear array.

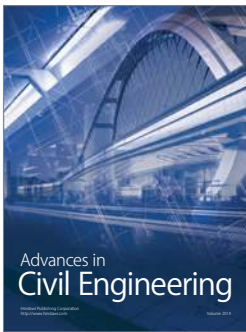
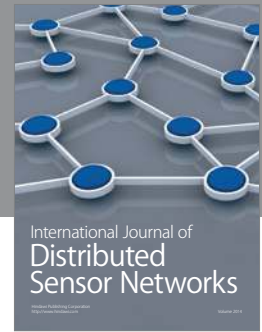
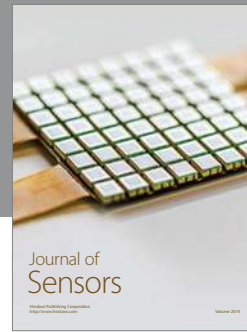
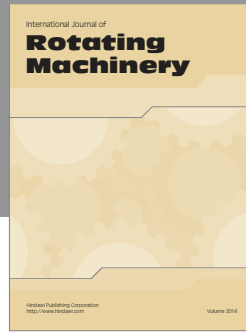
Conflicts of Interest

The authors declare that they have no conflicts of interest.

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