

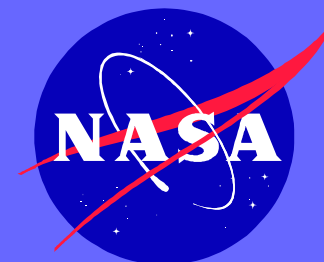
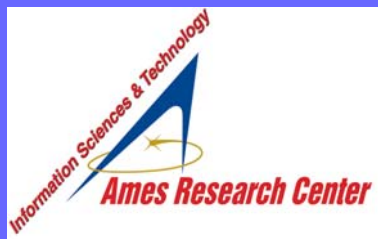
On-line, gyro-based mass-property identification for thruster-controlled spacecraft using recursive least squares

Edward Wilson, Chris Lages, Robert Mah

ed.wilson@intellization.com

chris.lages@intellization.com

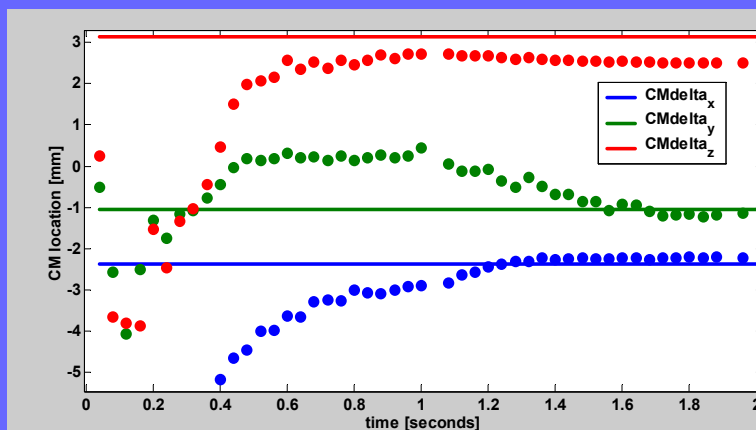
rmah@mail.arc.nasa.gov



Research objective: For thruster-controlled spacecraft, **identify mass properties** (I , CM) using gyros, under normal vehicle control. Applicable for **adaptive control** or FDI. Develop and validate through application on realistic simulations and hardware.

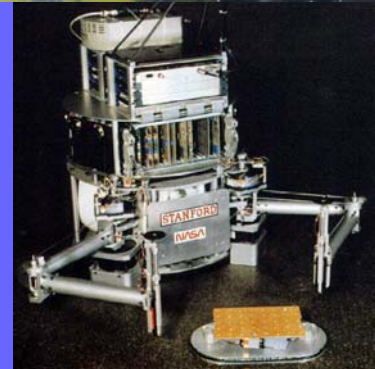
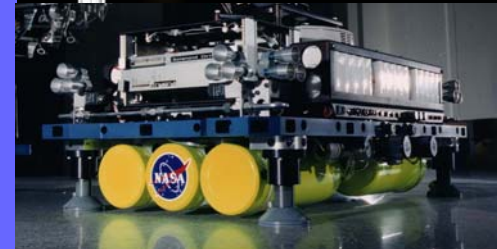
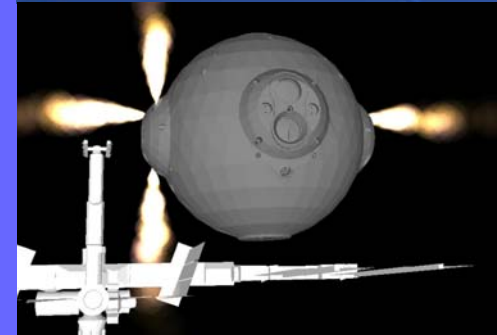
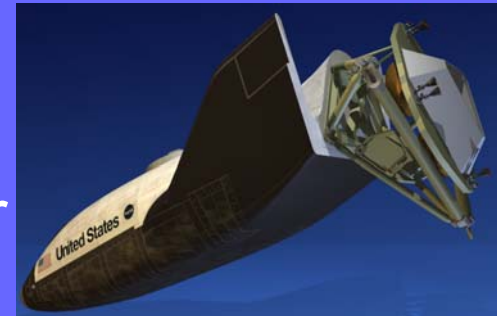
Outline:

- Introduction:
 - Problem statement
 - LS ID
- Solution:
 - Approach
 - Algorithms
 - Results, Demo
- Conclusions



Introduction: Mass-property ID

- Problem statement:
 - For a thruster-controlled spacecraft, with relatively low rotation rates, realistic sensor noise models, realistic thrust variability, using gyros only
 - ID mass center and inertia matrix
 - For use with adaptive control, Fault detection and isolation (FDI)
- Related Research:
 - Tanygin and Williams (1997) – spinning, coasting, LS
 - Bergmann *et al* (1987) – Kalman filter
 - Wilson and Rock (1994) – RLS combined thruster/mass ID; used for on-line neural-network control reconfiguration following multiple thruster failures



Least-squares identification (LS ID)

- Cast governing equations into form $Ax = b + \varepsilon$
- Noise appears in ε
- Parameters to ID appear (linearly) in x
- Closed form solution minimizes sum squared error: $\hat{x} = (A^T W A)^{-1} A^T W b$
- Batch or equivalent recursive solutions (RLS)
- *Challenge is in manipulating governing equations into correct form, $Ax = b + \varepsilon$*

Problem characteristics / Approach

- Full dynamics involve:
 - Thruster strength and alignment
 - Inertia matrix
 - CM location, Mass
- Variability:
 - Pulse-to-pulse thruster variation
 - Sensor noise
 - Disturbance forces and torques
- Parameters appear in governing equations of motion (EOM) coupled, nonlinear
- Approach: divide into separate approximate linear solutions
- Separate RLS IDs for inertia, CM, thruster strength

Mass-center ID algorithm

Equations of motion:

$$\dot{\omega} = I^{-1}((L \times D)B(F_{nom} + F_{bias} + F_{random,k})T_k + \tau_{disturb} - \omega \times (I\omega))$$

Manipulated EOM:

$$C \equiv C_{nom} + \Delta; L = L_{nom} - \Delta[1 \quad 1 \quad \dots \quad 1]$$

$$I^{-1} \begin{bmatrix} 0 & -c_3 & c_2 \\ c_3 & 0 & -c_1 \\ -c_2 & c_1 & 0 \end{bmatrix}_k \begin{bmatrix} \Delta_1 \\ \Delta_2 \\ \Delta_3 \end{bmatrix} = \dot{\omega} + I^{-1}(\omega \times (I\omega)) - I^{-1}(L_{nom} \times D)F_{nom}T_k; c_k \equiv DF_{nom}T_k$$

LS (or RLS) formulation: $A_k x = b_k$

$$A_k = I^{-1} \begin{bmatrix} 0 & -c_3 & c_2 \\ c_3 & 0 & -c_1 \\ -c_2 & c_1 & 0 \end{bmatrix}_k; x = \begin{bmatrix} \Delta_1 \\ \Delta_2 \\ \Delta_3 \end{bmatrix}; b_k = \dot{\omega} + I^{-1}(\omega \times (I\omega)) - I^{-1}(L_{nom} \times D)F_{nom}T_k$$

(inverse) Inertia ID algorithm

Equations of motion:

$$\dot{\omega} = I^{-1}((L \times D)B(F_{nom} + F_{bias} + F_{random,k})T_k + \tau_{disturb} - \omega \times (I\omega))$$

Manipulated EOM:

$$\begin{bmatrix} a_1 & & & & & & & & \\ & a_2 & & & & & & & \\ & & a_3 & & & & & & \\ & & & a_1 & & & & & \\ & & & & a_2 & & & & \\ & & & & & a_3 & & & \\ & & & & & & I_{11}^{-1} & & \\ & & & & & & I_{22}^{-1} & & \\ & & & & & & I_{33}^{-1} & & \\ & & & & & & I_{12}^{-1} & & \\ & & & & & & I_{13}^{-1} & & \\ & & & & & & I_{23}^{-1} & & \end{bmatrix} = \dot{\omega}; a_k \equiv (L \times D)F_{nom}T_k - \omega \times (I\omega)$$

LS (or RLS) formulation:

$$A_k x = b_k \quad A_k = \begin{bmatrix} a_1 & & & & & & & & \\ & a_2 & & & & & & & \\ & & a_3 & & & & & & \\ & & & a_1 & & & & & \\ & & & & a_2 & & & & \\ & & & & & a_3 & & & \\ & & & & & & I_{11}^{-1} & & \\ & & & & & & I_{22}^{-1} & & \\ & & & & & & I_{33}^{-1} & & \\ & & & & & & I_{12}^{-1} & & \\ & & & & & & I_{13}^{-1} & & \\ & & & & & & I_{23}^{-1} & & \end{bmatrix}; x = \begin{bmatrix} I_{11}^{-1} \\ I_{22}^{-1} \\ I_{33}^{-1} \\ I_{12}^{-1} \\ I_{13}^{-1} \\ I_{23}^{-1} \end{bmatrix}; b_k = \dot{\omega}$$

RLS, batch LS solution

- RLS implementation: use A_k , b_k at each update, either exponentially weighted or unweighted. Use standard RLS equations.
- Batch LS: concatenate A_k matrices and b_k vectors, using any desired weighting

$$A = \begin{bmatrix} A_1 \\ A_2 \\ \vdots \\ A_k \end{bmatrix}; b = \begin{bmatrix} b_1 \\ b_2 \\ \vdots \\ b_k \end{bmatrix}$$

- Solve using standard batch LS solution

$$\hat{x} = (A^T W A)^{-1} A^T W b$$

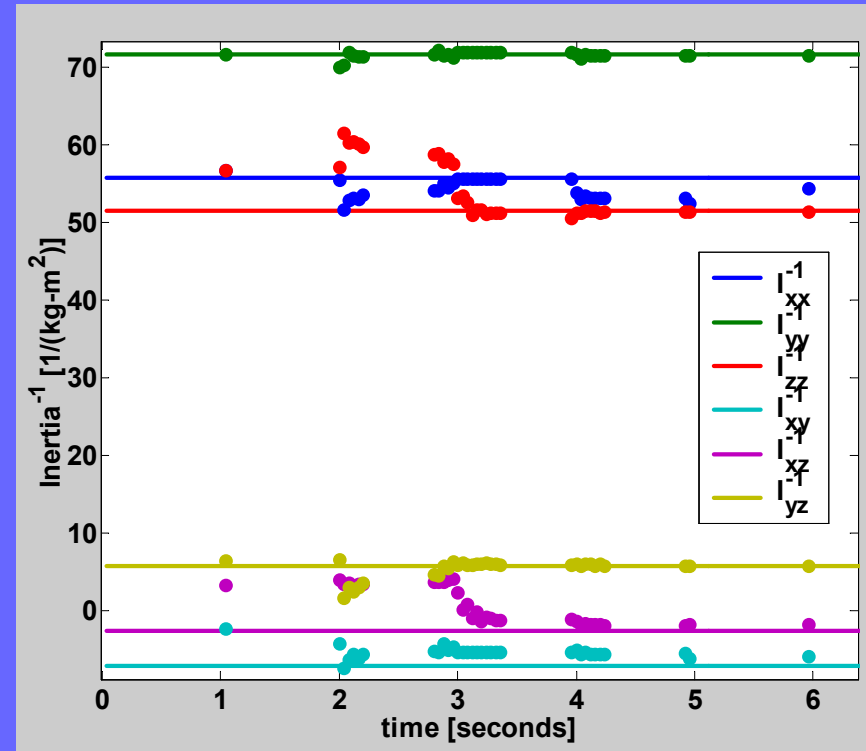
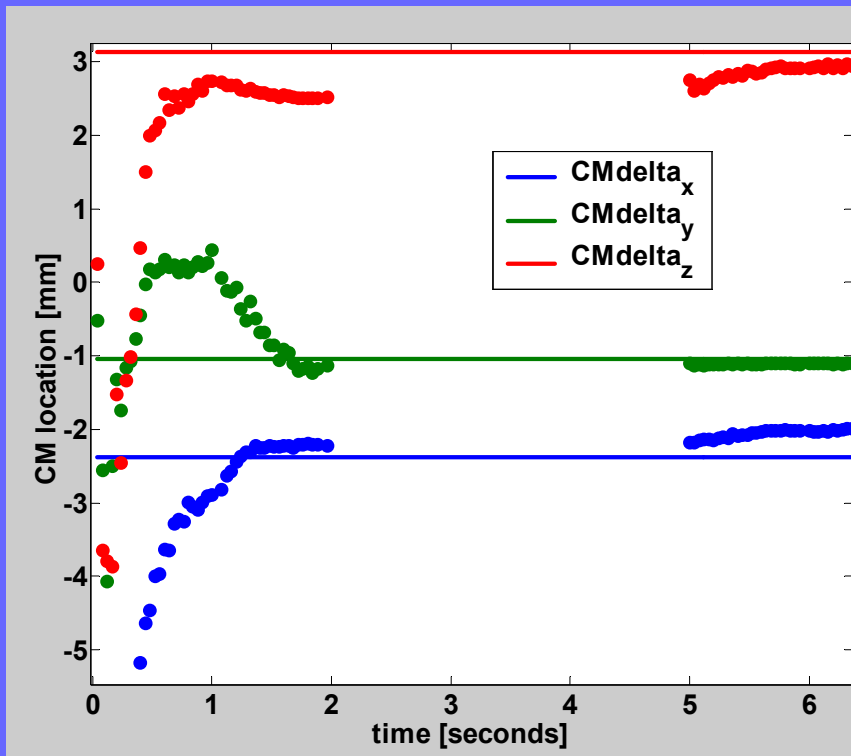
$$\hat{x} = (A^T A)^{-1} A^T b$$

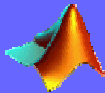
Deviations from correct LS form

- $\hat{x} = (A^T A)^{-1} A^T b$ is optimal if $Ax = b + \varepsilon$ form can be achieved.
- Not strictly possible due to form of EOM. Depending on rates, disturbances, sensor accuracy, thruster variability, control policy, etc., different formulations may be better.
- Deviations from correct LS form:
 - Noisy measurements appear in the $\omega \times (I\omega)$ term in the A matrix. Negligible for slow rotational speeds in many spacecraft applications.
 - Other terms in A and b are not known perfectly: L , D , B , F_{bias} , etc. are all estimated or nominal values.
 - Random variables $F_{random,k}$ and $\tau_{disturb}$ (set to zero) do not appear directly in the ε term as they should.
 - CM ID uses nominal or estimated values for I and I^{-1} . Inertia ID uses nominal or estimated values for CM.

Results

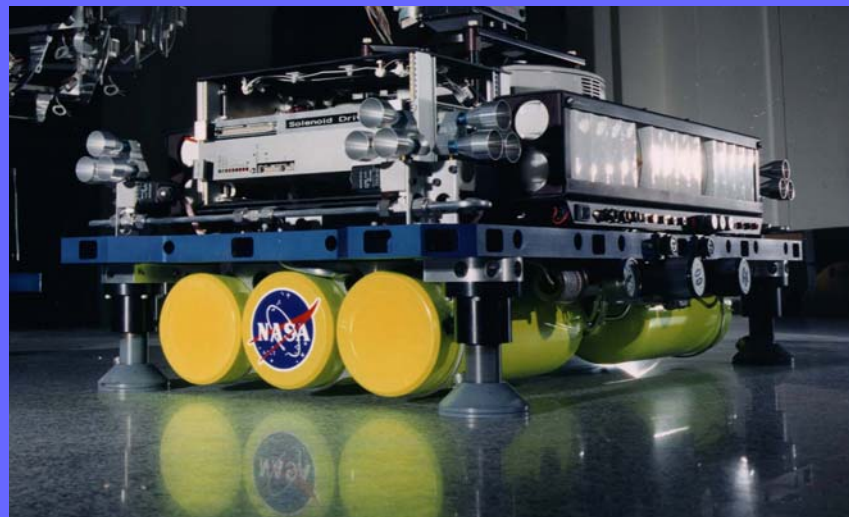
- Accuracy depends on sensor noise, thruster variability, variability in non-ID'ed parameters.
- Applied to 3 vehicles (X-38, Mini-AERCam, S4) in simulation, being applied in hardware on S4 (same code).



- More accurate than ground analysis/meas. (Mini-AERCam)
- MATLAB demo 

Extensions, continuing work

- Use of translational accelerometers
- Integration of on-line mass-property ID with FDI
- Implementation on air-bearing vehicle
 - Same MATLAB code runs on X-38 sim, Mini-AERCam sim, S4 sim, S4 hardware
- Standing by for X-38, Mini-AERCam programs



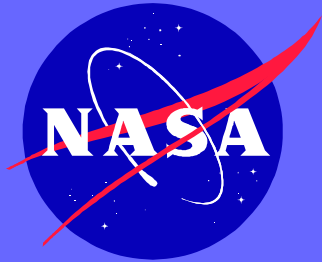
Smart Systems Spacecraft Simulator (S4)

Conclusions

- Algorithms presented provide mass-property ID for thruster-controlled spacecraft
- Non-invasive – uses existing gyros, no special motions required
- Generic algorithm - applied to 3 vehicles in simulation, 1 in laboratory hardware
- Useful for adaptive control, FDI, especially applicable to vehicles with changing payload, fuel mass, configuration

- Paper and presentation are available at <http://intellization.com/files/>

Acknowledgements



- Funded by NASA Headquarters, HQ AA, PWC 349-00: William Readdy and Gary Martin
- Problem definition from NASA JSC: Rodolfo Gonzalez, Dr. Steven Fredrickson, Tim Straube, Dave Hammen
- NASA Ames SSRL members help on 3D visualization: Richard Papasin, Alan Gasperini, Rommel Del Mundo

