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# One-dimensional off-chip beam steering and shaping using optical phased arrays on silicon-on-insulator

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**Abstract**—Optical beam steering can find applications in several domains such as laser scanning, LiDAR (Light Detection And Ranging), wireless data transfer and optical switches and interconnects. As present beam steering approaches use mechanical motion such as moving mirrors or MEMS (MicroElectroMechanical Systems) or molecular movement using liquid crystals, they are usually limited in speed and/or performance. Therefore we have studied the possibilities of the integrated silicon photonics platform in beam steering applications. In this paper, we have investigated a 16 element one-dimensional optical phased array on silicon-on-insulator with a field-of-view of  $23^\circ$ . Using thermo-optic phase tuners, we have shown beam steering over the complete field-of-view. By programming the phase tuners as a lens, we have also shown the focusing capabilities of this one-dimensional optical phased array. The field-of-view can easily be increased by decreasing the width of the waveguides. This clearly shows the potential of silicon photonics in beam steering and scanning applications.

**Index Terms**—Silicon on insulator technology, grating couplers, beam steering, optical phased arrays, thermo-optic effects.

## I. INTRODUCTION

OPTICAL beam steering has a great potential in diverse applications. Free-space beam steering can on the one hand be used in laser scanning applications such as LiDAR (Light Detection And Ranging), optical wireless links, remote node interrogation ... but can also find applications in the very short range such as in optical switches and optical interconnects. As interconnects are currently becoming a bottleneck in increasing chip speed, this has gained a lot of interest [1].

While beam steering can be done mechanically, this is usually less stable and limited in speed. Optical Phased Arrays (OPAs) provide a way to efficiently steer an optical beam without any mechanical motion, making them insensitive to acceleration. Liquid crystals have received a lot of attention in OPA technology, but suffer from limited steering angle and limited speed. In these systems, the orientation of the liquid

crystal induces a change in refractive index and they thus act as a programmable lens that can steer the light [2].

In this paper, we have investigated the use of the silicon photonics platform in beam steering applications. While silicon photonics gives us many integrated functions on-chip, the interface between the outside world is very important. This becomes increasingly difficult when one does not couple to an optical fiber, but directly to free-space, such as in free-spacing interconnecting, sensing or scanning applications. Beam steering on this platform has already been investigated in [3] and [4] where a one- and two-dimensional OPA on silicon-on-insulator (SOI) has been demonstrated, respectively. In the former, the beam could be steered to a small angle as there was only one heater electrode. In the latter, sidelobe levels were high due to the very small fill factor of the OPA. In [5], the same platform has been used with irregularly spaced optical phased arrays for one-dimensional large angle beam steering using thermo-optic phase shifters. This relaxes the  $\lambda/2$  constraint to avoid the different output orders of the optical phased arrays. However the sidelobe level becomes quite high.

Here we present a design that combines both fixed and thermo-optic beam steering. Due to the grating used at the output, light is coupled off-chip and the wavelength can be used to steer the beam in the other dimension. As has been shown in [6], a beam can also be steered in the two-dimensional space using wavelength tuning only. By changing the input waveguide of the star coupler, fixed steering is accomplished. Making use of a star coupler will also give us better far-field characteristics as there is a Gaussian envelope across the light emitting elements due to the free propagation region of the star coupler.

The 3dB field-of-view (FOV) is limited to about  $23^\circ$ , but can easily be increased by reducing the width of the grating coupler waveguides. A trade-off has to be made between the FOV and the beam width, as the number of addressable spots in free-space depends on the number of radiating elements of the OPA. Using a grating etched on a 450nm wide photonic wire, the FOV can become as large as  $160^\circ$ .

We have also demonstrated focusing capabilities of an OPA on SOI. As the OPA is actually a one-dimensional programmable lens, light can be focused above chip in one dimension. This becomes increasingly interesting when one wants to use a photonic integrated circuit (PIC) for sensing applications, such as in on-chip laser Doppler velocimetry [7]

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or Optical Coherence Tomography (OCT) [8]. Light is for example focused on the skin and reflected back in the PIC for further processing. The beam can then be shaped to optimize the link losses.

In the next Section, we will discuss the design and fabrication of the components. In Section III, the measurement setup is discussed. Section IV gives the measurement results. A conclusion is finally formulated in Section V.

II. DESIGN AND FABRICATION

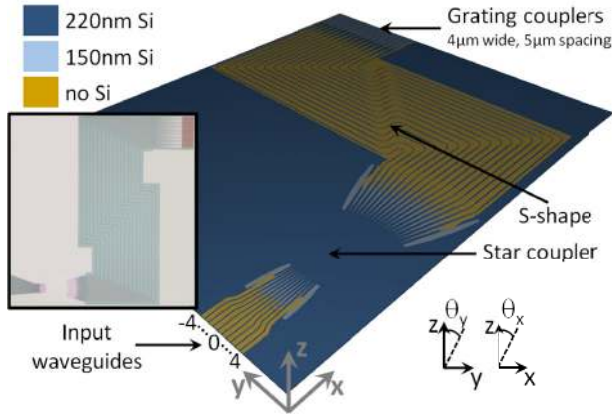


Fig. 1. Virtual fabrication of a one-dimensional OPA on SOI. Light enters through the input waveguides of the star coupler and couples off-chip using grating couplers, on the S-shape heaters are processed (not shown in the Figure) to tune the respective phases of the different grating couplers. The inset shows a microscope image of the fabricated component before heater processing.

The beam steering component shown in Fig. 1 was fabricated in imec, Leuven through ePIXfab (www.epixfab.eu) which uses standard CMOS (Complementary Metal Oxide Semiconductor)-compatible processes to fabricate photonic integrated circuits [9]. An SOI wafer with a 2μm thick buried oxide layer and a 220nm top silicon layer was used. Two deep-UV (UltraViolet) lithography etch steps are then used: one of 220nm to pattern the waveguides and the star coupler and one of 70nm to pattern the out-coupling gratings and the tapering sections of the star coupler. Using a two-step tapering approach, the insertion loss of the star coupler is reduced to less than 1.5dB [10].

The waveguides in the S-shape (Fig. 1) are 800nm wide as wider waveguides are more tolerant to fabrication deviations and reduce the corresponding phase errors in the waveguides. At each bend, the waveguide tapers back to a 450nm wide single mode wire, which allows very sharp bends of less than 3μm, without significant loss. This S-shape ensures all waveguides are in phase and allows us to use a large waveguide spacing which is needed to reduce the crosstalk of the thermo-optic heaters which are processed afterwards. A total of 16 waveguides were used in the S-shape, bringing the number of resolvable spots in the far field to 16. Increasing this number will further decrease the beam width and will allow more accurate steering. After the S-shape, the waveguides taper to a 4μm width on which a 70nm deep grating is etched with a period of 630nm and a duty cycle of 0.5. The gratings are separated 5μm.

Afterward a BCB (benzocyclobutene) layer of about 800nm is spun on top of the component on which 2.5μm wide heaters are processed using contact mask lithography. Each heater has a total length of 450μm. These heaters are used to tune the phases of the different elements. They consist of a 100nm Ti layer and a 20nm Au layer to avoid oxidation of the heater. In a final stage, a 500nm gold layer is processed on the contact pads of the heaters. A cross-section of the S-shape on which the heaters are processed is shown in Fig. 2(a).

The input waveguides shown in Fig. 1 are connected with a grating coupler which is optimized for near vertical coupling of infrared light from a fiber to the fundamental TE-like mode of an integrated circuit [11]. These are used to excite our structure. For the remainder of this paper, we assume to work only with TE-like light.

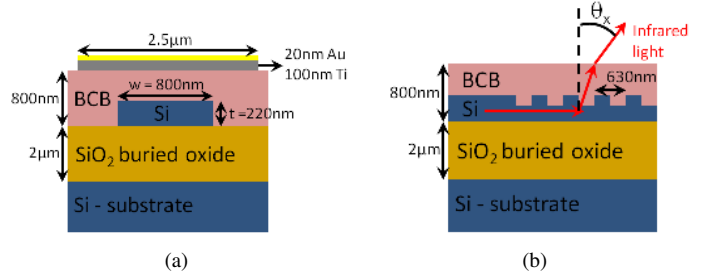


Fig. 2. Cross-sectional view of the (a) thermo-optic phase tuners, (b) grating coupler.

To split the light into 16 waveguides, two approaches can be taken: using an MMI (MultiMode Interference) splitter, or using a star coupler. When using an MMI-splitter, all waveguides will have an equal amount of power. This will result in an increased sidelobe level in the far-field. By making use of a star coupler, a natural apodization of the field over the OPA is obtained, and the simulation shows a sidelobe level decrease of 13dB as can be seen in Fig. 3. In this Figure the simulated far-field of the beam steering component in the  $\theta_y$ -direction is shown for the two different cases at a wavelength of 1550nm. The FWHM (full-width-half-maximum) beam width becomes a bit larger and increases from 0.98° to 1.26°.

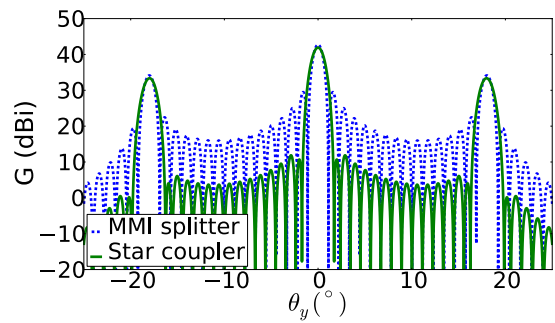


Fig. 3. Simulated far-field of a 16 element 1D OPA with equal amount of power in each element (MMI splitter) or with apodization (star coupler). A sidelobe reduction of 13dB can be seen.

By using thermo-optic phase tuners, the beam can be shaped and steered in the  $\theta_y$ -direction. Silicon has a high thermo-optic coefficient ( $\partial n / \partial T = 1.84 \times 10^{-4} \text{K}^{-1}$ ) and different

designs have been investigated in literature to optimize their performance [5], [12]. Here a simple heater design was used, which was proven to be sufficient to demonstrate the steering and focusing capabilities. The power needed for a  $\pi$  phase shift at 1550nm was measured to be around  $P_\pi = 15 - 20$ mW. This can be reduced by more elegant heater designs, such as insulating trenches. Different phase tuning approaches have been reported on silicon such as the use of liquid crystals [13], carrier depletion [14] or more recently using a NEMS (Nano-ElectroMechanical Systems) approach [15] which all require a small amount of power as they work capacitively. Depending on the wanted speed and performance, these can be integrated in the current design. Our current heaters have a speed which is limited to about 20kHz, with a 10%-90% rise and fall time of 12.5 $\mu$ s and 7.2 $\mu$ s, respectively. This is shown in Fig. 4, where the heater performance is measured in a balanced Mach-Zehnder interferometer (MZI) where one arm is heated. The heater is driven by a 20kHz voltage signal for which the peak voltage corresponds to a  $\pi$  phase shift.

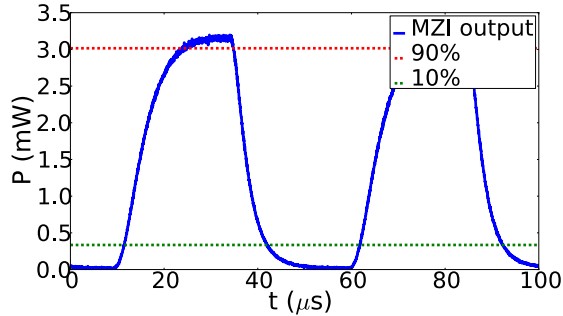


Fig. 4. Dynamic behavior of the heater. The output of a balanced Mach-Zehnder interferometer is shown where one arm is heated. The heater is driven by a 20kHz voltage signal which gives a  $\pi$  phase shift at the peak voltage.

While there are a lot of degrees of freedom in the  $\theta_y$ -direction, there is limited freedom in the  $\theta_x$ -direction. The beam characteristics in this direction are determined by the out-coupling grating. This is a second order grating which will send the light off-chip at an angle given by the grating equation:

$$\sin \theta_x = \frac{\Lambda_{gr} n_{eff,gr} - \lambda}{n_{ct} \Lambda_{gr}}, \quad (1)$$

with  $\Lambda_{gr}$  the period of the grating ( $\Lambda_{gr}=630$ nm),  $\lambda$  the free-space wavelength,  $n_{eff,gr}$  the effective index of the guided mode in the grating area and  $n_{ct}$  the refractive index of the background which is air ( $n_{ct} = 1$ ) in this case. Using wavelength tuning, the beam can be steered in the  $\theta_x$ -direction. A cross-sectional view of the grating coupler is shown in Fig. 2(b).

### III. MEASUREMENT SETUP

The far-field characteristics of the beam steering component are investigated using a Fourier imaging setup. The far-field is imaged on the back-focal plane of a high numerical aperture (NA=0.5) microscope objective (MO). This image is brought back to an infrared camera using two lenses as shown in

Fig. 5 [16]. Every point in the Fourier plane corresponds to a specific direction of emission and thus represents the far-field of the beam steering component. Light from a tunable laser is sent through a polarization controller and is then coupled into the beam steering component using a grating coupler for near-vertical coupling. The radiated light is then imaged using the Fourier imaging setup. A probe card is placed in front of the sample to drive the different heaters.

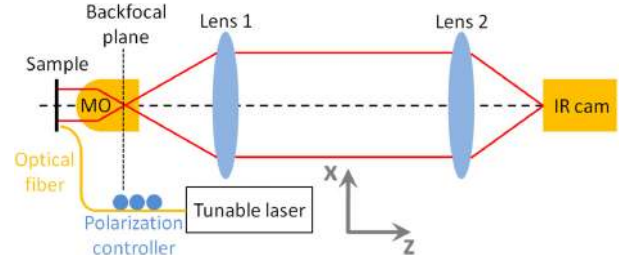


Fig. 5. A Fourier imaging setup is used to study the far-field characteristics of the beam steering component.

The focusing capabilities of the component are studied with the setup shown in Fig. 6. The structure is again excited using a tunable laser and a polarization controller. At a certain distance  $f$ , a single mode optical fiber is placed to capture the light radiated from the structure. The sample is positioned at a certain angle  $\theta_x$  which is the out-coupling angle of the grating. The light is then focused in the  $yz$ -plane on the tip of the fiber in one-dimension and the received power is measured.

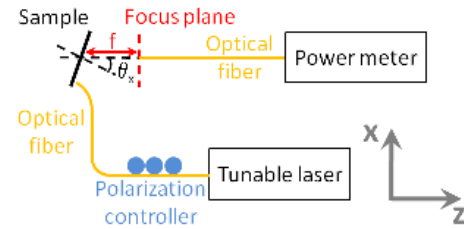


Fig. 6. Using a fiber at a distance  $f$  of the sample, the focusing capability of the structure is investigated.

## IV. MEASUREMENT RESULTS AND DISCUSSION

First we discuss the far-field pattern of the beam steering component. Next, we investigate the wavelength and thermo-optic steering behavior. Then we look into the focusing capabilities of the OPA. Finally a short discussion is given on the power efficiency of the OPA.

### A. Far-field pattern

In Fig. 7, the measured far-field of the beam steering component is shown at a wavelength of 1550nm. A broad beam in the  $\theta_x$ -direction can be seen, which is determined by the out-coupling grating and centered around  $\theta_x = 10^\circ$  being the out-coupling angle of the grating given by Eq. (1). In the  $\theta_y$ -direction, a typical OPA far-field pattern can be seen. The beam is narrow and the different output orders are visible with a spacing of  $18^\circ$ . This spacing can be increased by

decreasing the waveguide spacing. For 450nm wide integrated waveguides on SOI operating at a wavelength of  $1.55\mu\text{m}$ , the minimal center-to-center spacing is about  $1.3\mu\text{m}$  to avoid optical coupling between the waveguides. In the next sections, we will investigate cross-sectional views of the far-field of the beam steering component to study the wavelength steering and thermo-optic steering and shaping behavior.

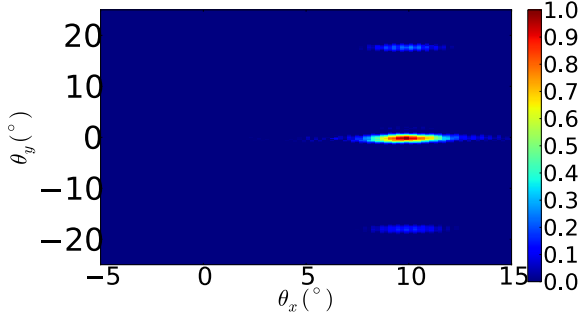


Fig. 7. Measured far-field pattern of the beam steering component at a wavelength of 1550nm.

### B. Wavelength steering

By tuning the wavelength, the beam shifts in the  $\theta_x$ -direction. Fig. 8 shows the far-field pattern along the  $\theta_x$ -direction for three different wavelengths. The FWHM beam width is measured to be  $3.0^\circ$ ,  $2.8^\circ$  and  $1.6^\circ$  for a wavelength of 1520nm, 1550nm and 1580nm, respectively and the beam is steered over a  $6.7^\circ$  range for a 60nm wavelength shift.

As the field that leaves a grating coupler with a fixed grating period is an exponential decaying field, the far-field pattern does not look very nice as can be seen in Fig. 8. The smaller beam width for increasing wavelength can be explained due to the fact that the grating couples the light out less efficiently, so that the exponential tail becomes larger and the far-field beam width will decrease. The wavelength dependent steering can simply be removed by cleaving the chip and using the end facet of the waveguides as radiating elements which is the approach taken in [5].

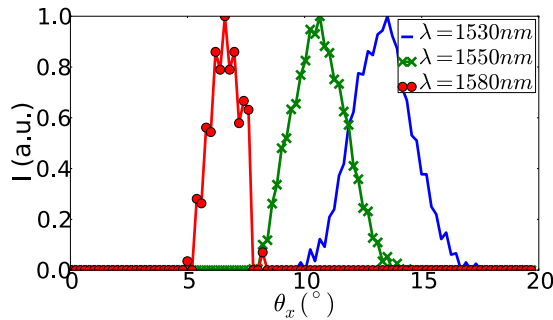


Fig. 8. Measured far-field in the  $\theta_x$ -direction using wavelength steering.

### C. Fixed beam steering

By using a different input waveguide of the star coupler as shown in Fig. 1, fixed steering of the beam in the  $\theta_y$ -direction

is observed. The free spectral range of the far-field in the  $\theta_y$ -direction is equal to  $\arcsin(\lambda/\Lambda_y)$  with  $\lambda$  the wavelength and  $\Lambda_y$  the spacing of the grating couplers ( $\Lambda_y=5\mu\text{m}$ ). At  $\lambda = 1.55\mu\text{m}$ , this corresponds to  $18^\circ$ . We have chosen 9 access waveguides and each waveguide results in a shift of  $2^\circ$  so that the complete FOV is covered. A cross-sectional view of the far-field in the  $\theta_y$ -direction for different access waveguides is shown in Fig. 9. In this Figure, only the far-fields for 5 input waveguides are plotted in order not to overload the Figure. The envelope of the far-field pattern is shown as well and has a FWHM of  $23^\circ$  which is determined by the width of the grating couplers. The beam width is  $1.27^\circ$  which compares well to the simulated value of  $1.26^\circ$ . The different output orders at a spacing of  $18^\circ$  are visible as well.

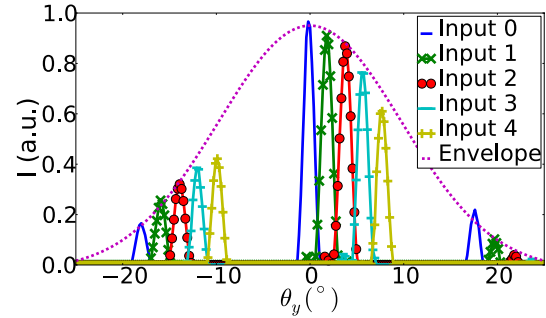


Fig. 9. Measured far-field in the  $\theta_y$ -direction for different input waveguides (Fig. 1) at 1550nm. The dashed line shows the envelope of the far-field pattern.

### D. Thermo-optic beam steering

By using the thermo-optic phase tuners, we can now steer the beam over the complete FOV in the  $\theta_y$ -direction. As the phase change  $\phi$  is directly proportional to the dissipated power in the heater, and the latter is proportional to the applied voltage  $V$  squared, we use the simple model:

$$\phi = \beta V^2 \quad (2)$$

Where  $\beta$  is a fixed parameter. Using this simple model, the  $2\pi$  phase resets can be taken into account. To steer the beam at an angle  $\theta_y$ , the phase difference  $\Delta\phi$  between each waveguide is equal to:

$$\Delta\phi = \frac{2\pi\Lambda_y}{\lambda} \sin \theta_y \quad (3)$$

In Fig. 10, a cross-sectional view of the far-field in the  $\theta_y$ -direction is shown when the beam is steered at different angles. When steering at an  $\theta_y$ -angle of  $18^\circ$ , the far-field coincides with the original far-field at  $0^\circ$  which proves the validity of our simple model.

### E. Beam focusing

By programming the phase tuners as to act as a lens, light is focused above the chip in one-dimension. Using a scalar approach, we simulated the coupling efficiency from the OPA to the fiber as a function of the distance  $f$  between the chip and the fiber (Fig. 6) as shown in Fig. 11. For very small  $f$ ,



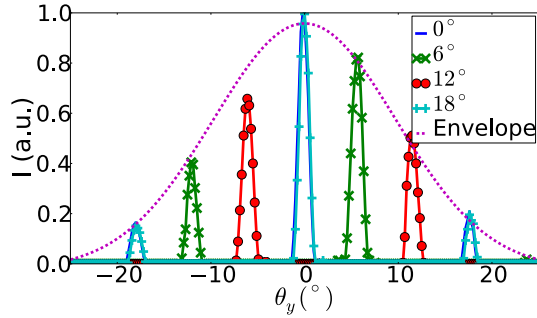


Fig. 10. Measured far-field in the  $\theta_y$ -direction using thermo-optic steering (Fig. 1) at 1550nm. The beam is steered to the angles  $0^\circ$ ,  $6^\circ$ ,  $12^\circ$  and  $18^\circ$ . The dashed line shown the envelope of the far-field pattern.

the NA of the fiber is too small to capture this light and a low efficiency is seen. At a distance of 0.33mm, an optimum is found, when the NA of the component matches the one of the optical fiber. Note that this loss of 2dB is only the loss in one dimension and is due to the fill-factor of the OPA.

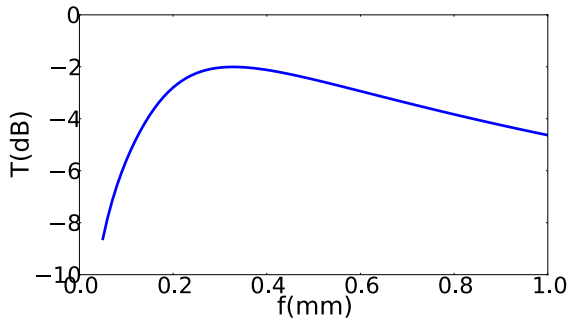


Fig. 11. One-dimensional simulated coupling efficiency of the 16 element OPA to an optical fiber as a function of distance between the OPA and the fiber at a wavelength of 1550nm. For each point, the phases are set to focus the light onto the fiber.

In Fig. 12 the measured power into the fiber is given for the case when the light is focused onto the fiber and when no focusing is used at a wavelength of 1550nm. The power shown is relative to the power received when the fiber is exactly on top of the structure ( $f=0$ mm) and no focusing is used. At first instance, a simple model is used to focus the light, as explained above. Afterward a rough optimization run did not show any significant improvement. There is an optimum focus point at  $f=0.4$ mm, which shows the focusing capabilities of the 1D OPA. An increase of 3dB in received power is observed. By using an apodized grating, light can also be focused in the other dimension at a fixed point.

#### F. Power budget

The out-coupling efficiency of the  $4\mu\text{m}$  wide waveguides has been investigated in 2D using the eigenmode expansion tool CAMFR (CAvity Modelling FRamework, <http://camfr.sourceforge.net/>). The out-coupling efficiency is about 38-40% over a 100nm wavelength range around 1550nm, but this can be easily increased to over 70-80% using a silicon

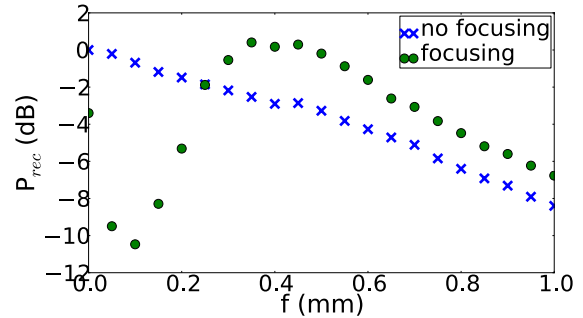


Fig. 12. Measured relative received power into an optical fiber at a distance  $f$  of the 16 element OPA at a wavelength of 1550nm. For each point, the phases are set to focus to light onto the fiber. The power is relative to the power received at  $f=0$ mm when no focusing is used.

overlay [17]. The loss of the star coupler is less than 1.5dB. The waveguide loss is about 3dB/cm, bringing the total waveguide losses in the component to only 0.2dB

#### V. CONCLUSION

We have shown a 16 element one-dimensional optical phased array on silicon-on-insulator. Using a star coupler to split the light into 16 waveguides, the sidelobe level is reduced by 13dB. The star coupler further allows us to demonstrate fixed beam steering by changing the input waveguide. The field-of-view was  $23^\circ$  using  $4\mu\text{m}$  wide grating couplers spaced  $5\mu\text{m}$ . The different output orders of the array were spaced  $18^\circ$ . This field-of-view and output order spacing could easily be increased by decreasing the waveguide width and spacing, respectively, but will result in a broader beam as the number of elements stays constant. The beamwidth was  $1.27^\circ$ . Using thermo-optic phase tuners, the beam was steered over its complete field-of-view. By programming the phase tuners as a lens, focusing capabilities have been shown as well.

#### ACKNOWLEDGMENT

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