



Performance Boundaries in Nb₃Sn Superconductors

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Acknowledgments



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...



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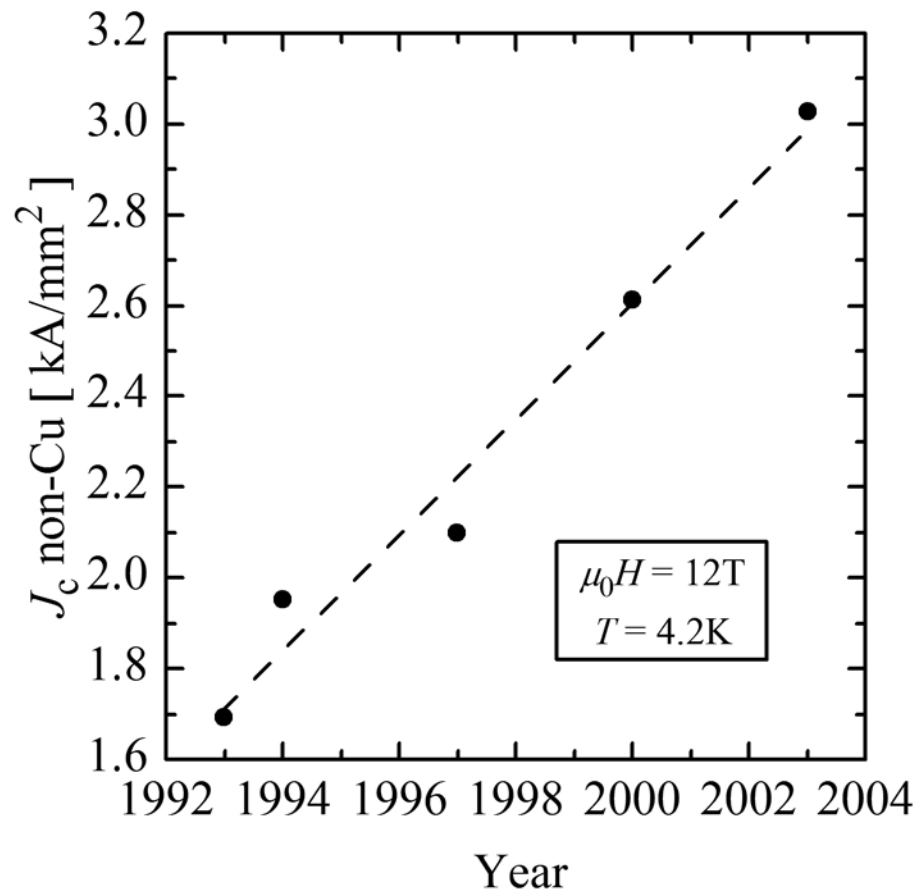
David Larbalestier
Peter Lee
Alex Gurevich
Matt Jewell
Chad Fischer
...

Outline



- **Critical current density and critical current**
- **Composition variation in Nb₃Sn wires**
- **Composition and $H_{c2}(T)$**
- **Pinning capacity, grain boundary pinning, grain size**
- **Composition and J_c**
- **Strain dependence (*time allowing*)**
- **Present status and future prospects**

Wire J_c progress versus time

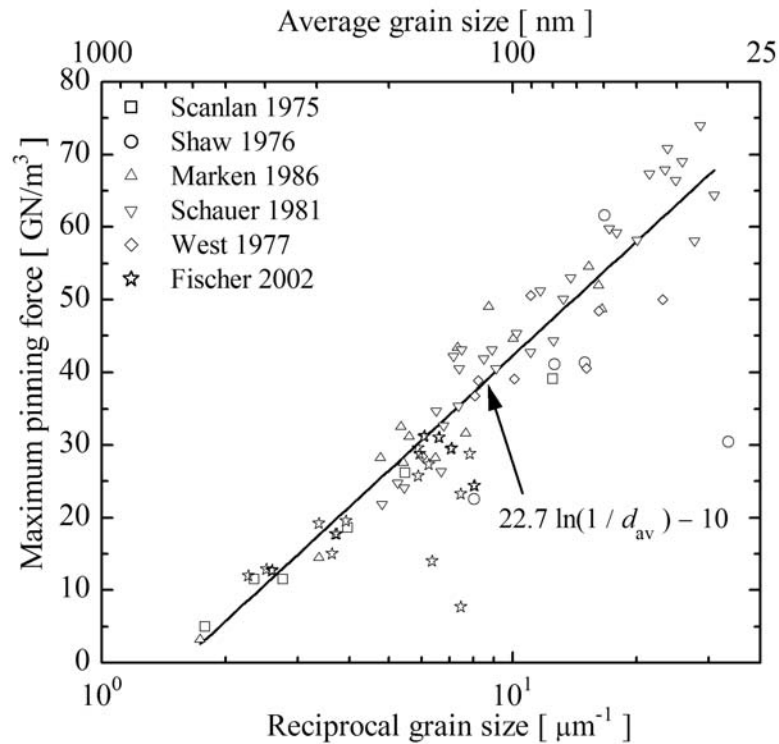


● **Parrell, ACE 2004**

What determines J_c ?

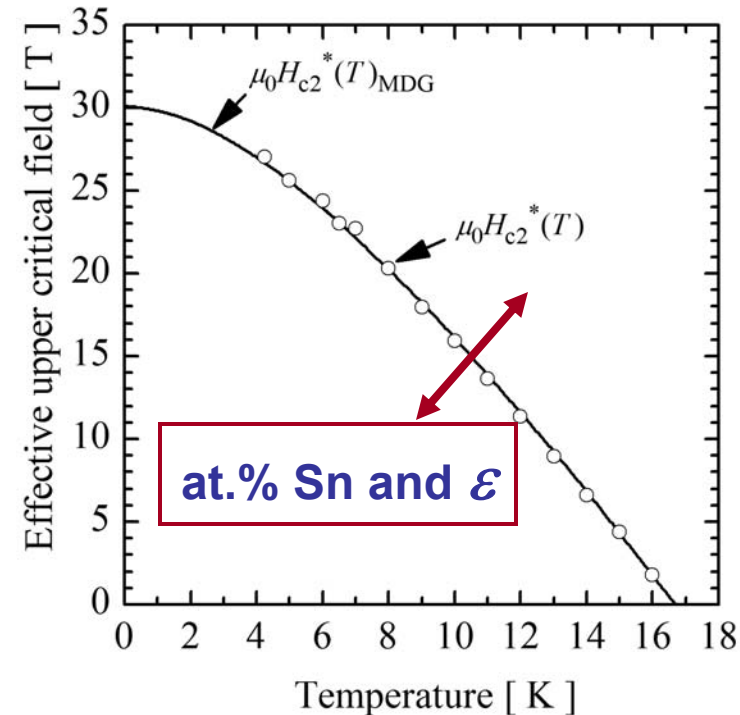


Pinning capacity



- Average grain size

Effective $H - T$ phase boundary

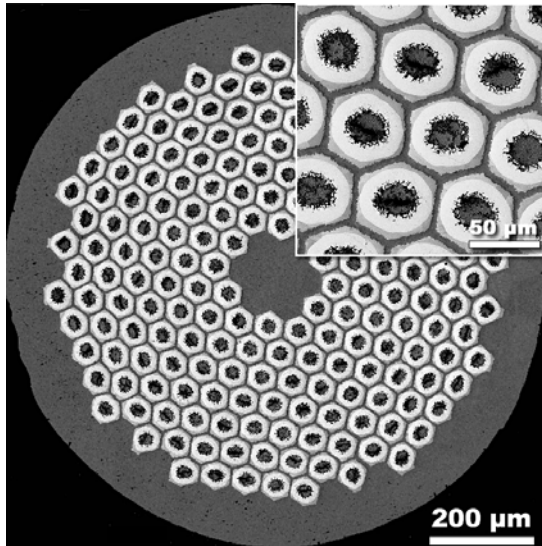


- Composition
- Strain state

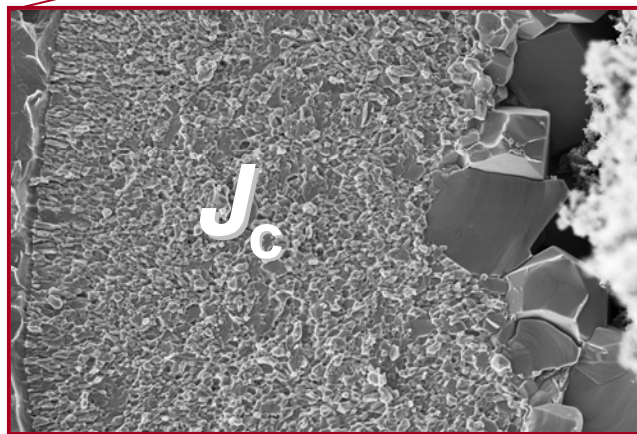
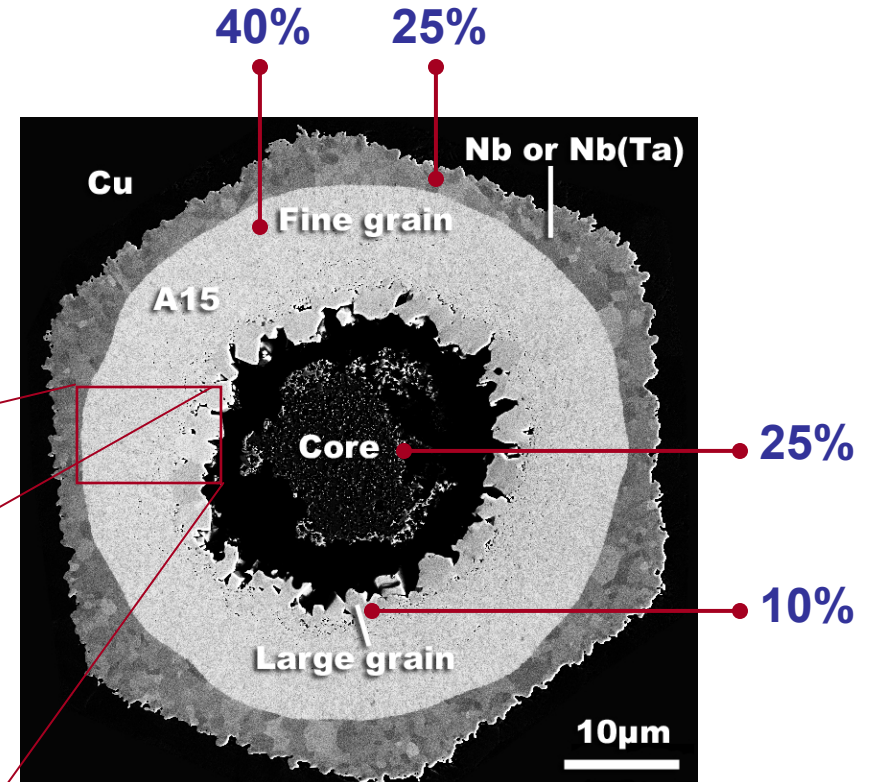
$$J_c \rightarrow I_c ?$$

What determines I_c ?

- Powder-in-tube wire (SMI)



- 50% Non – Cu fraction



- Only 20% of the wire carries J_c

Outline

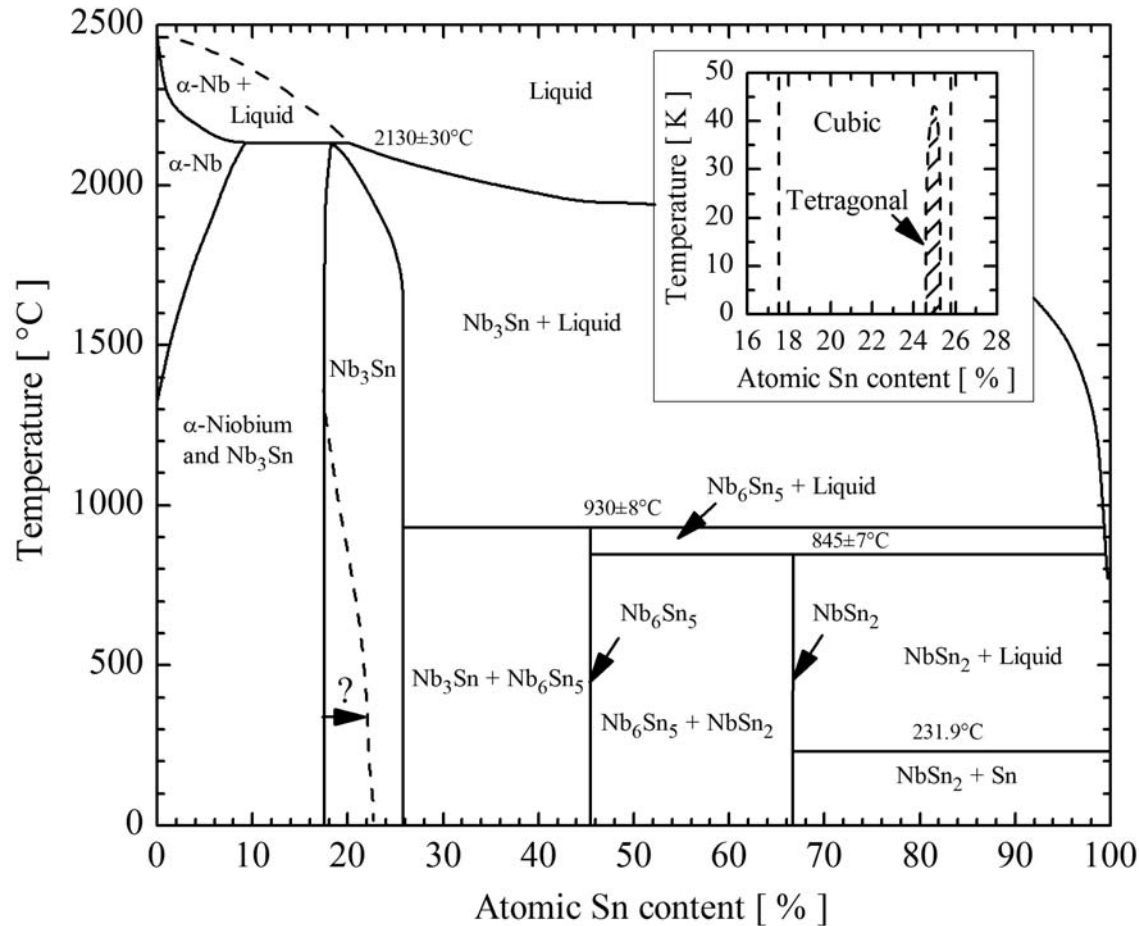


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Composition: $\text{Nb}_3\text{Sn} \rightarrow \text{Nb}_{1-\beta}\text{Sn}_\beta$



- Binary phase diagram \rightarrow 18 to 25 at.% Sn \rightarrow 'A15'

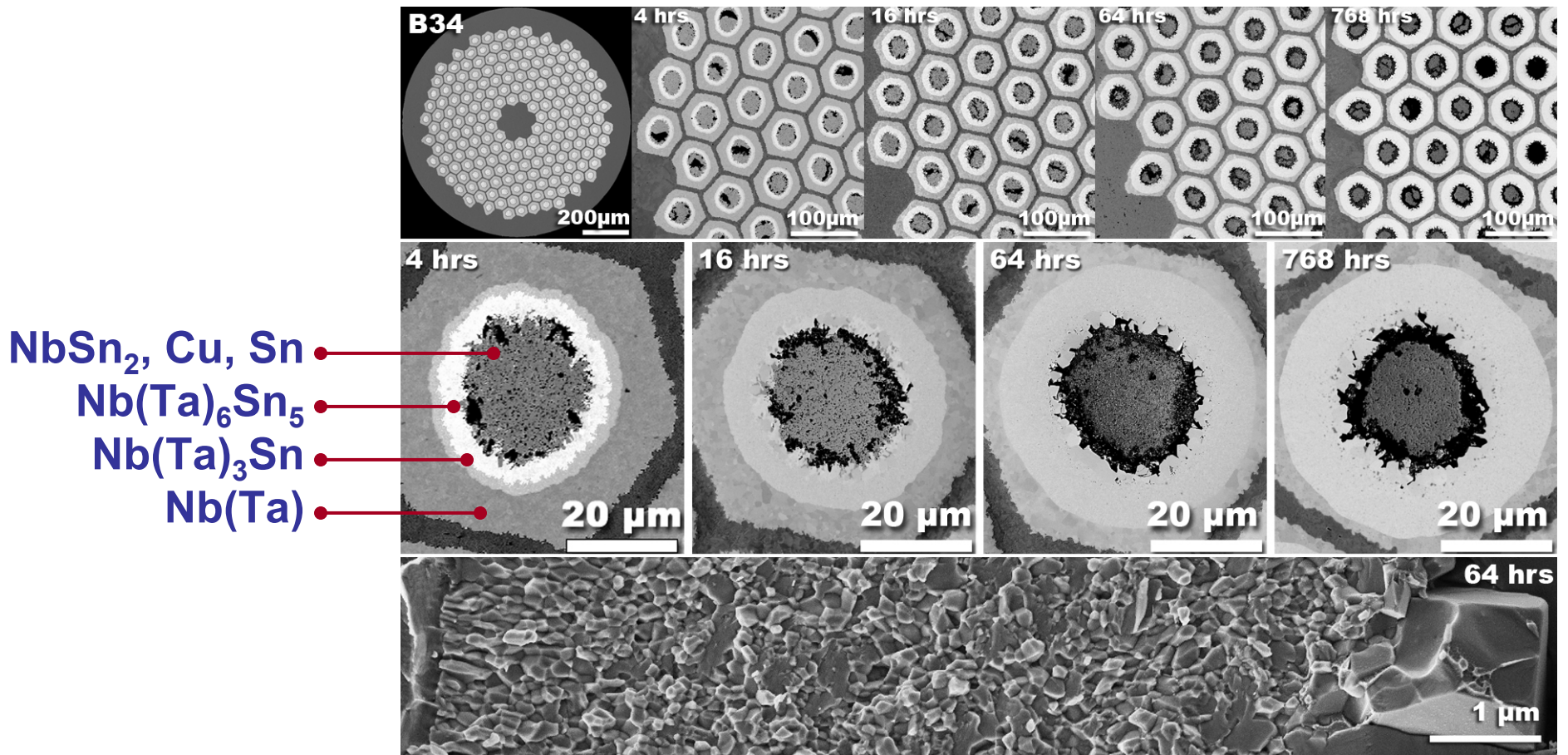


➔ Charlesworth, JMS 1970, Flükiger, ACE 1982

Nb₃Sn diffusion reaction in wires



- Reaction at 675°C vs time in Powder-in-Tube wire (SMI)

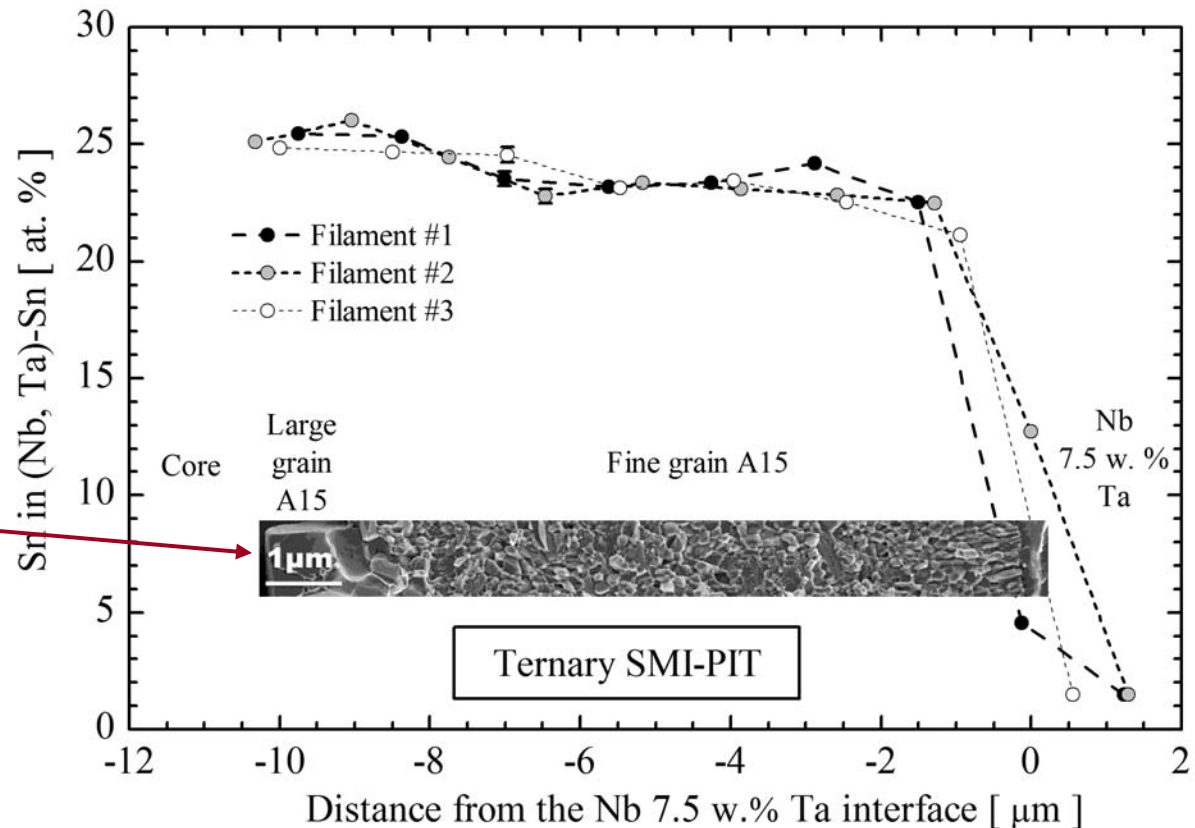
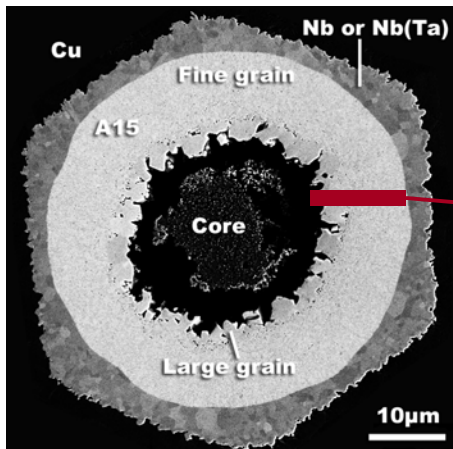


Composition variation in wires

- Composition analysis on SMI Powder-in-Tube wire

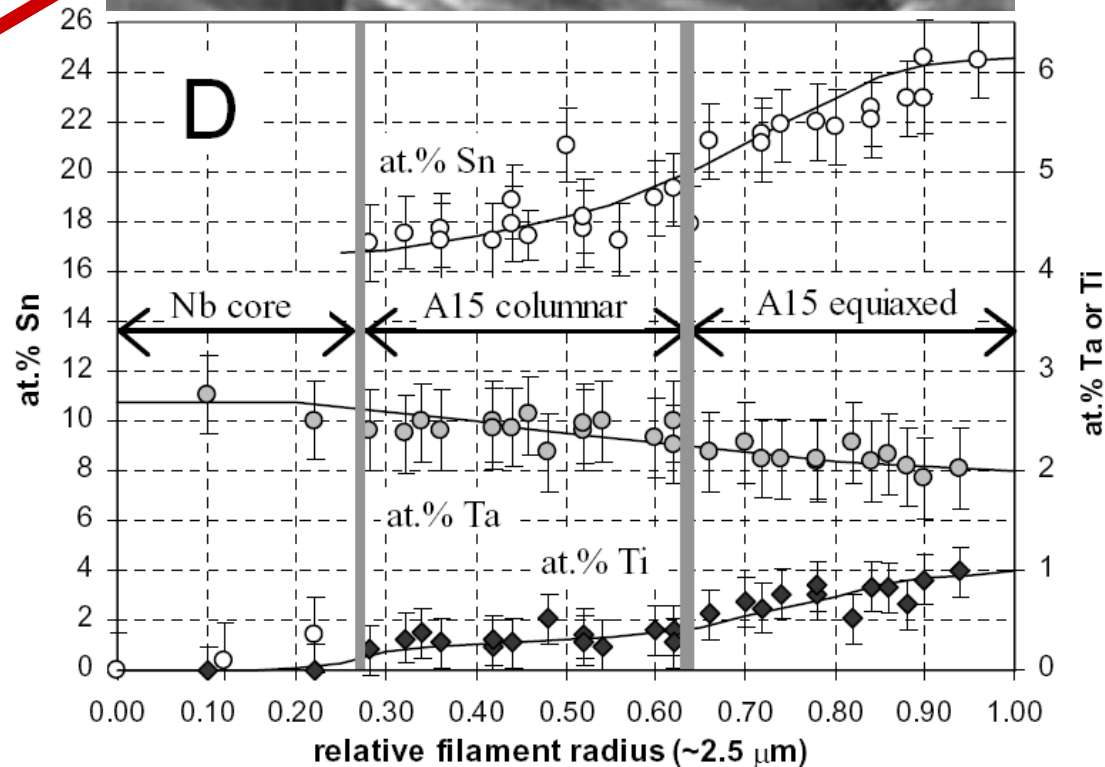
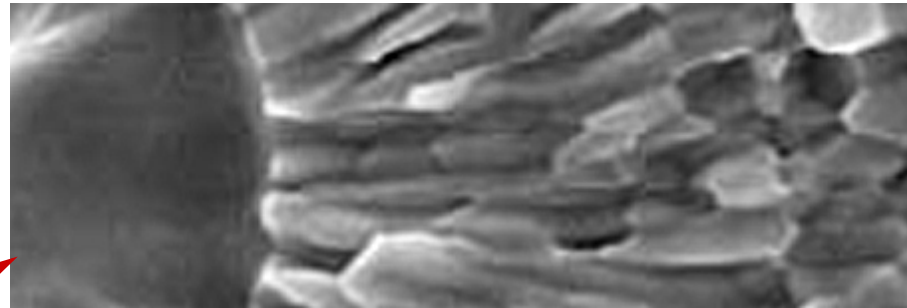
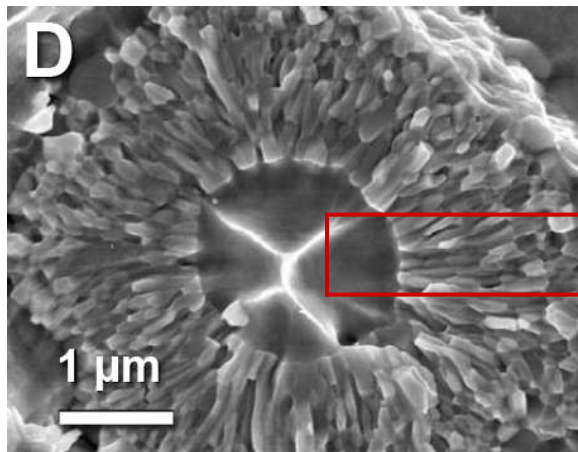
- 0.3 at.% Sn/ μm

- $J_c(12T, 4.2) = 2250 \text{ A/mm}^2$



Composition variation in wires

- Bronze process wire
Univ. of Geneva

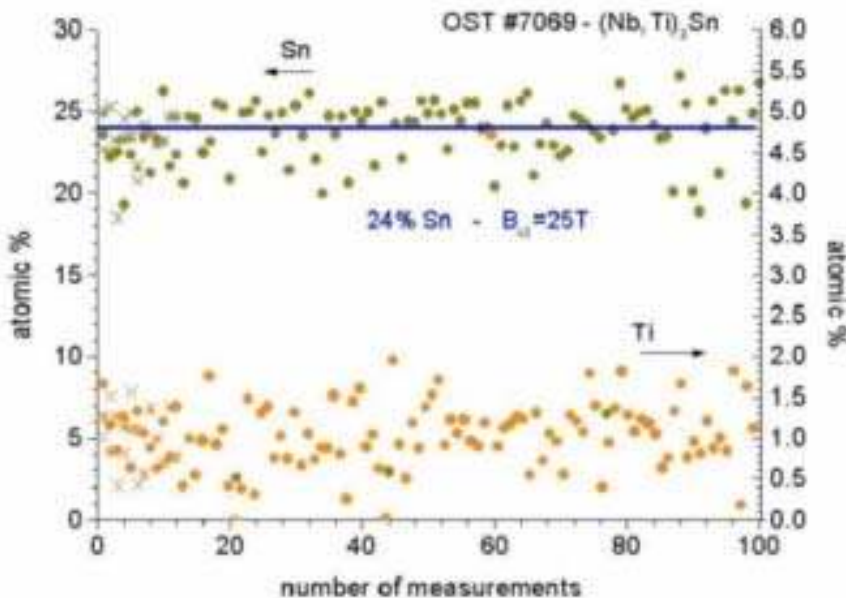


- 4 at.% Sn/μm
- $J_c(12T, 4.2) = 720 \text{ A/mm}^2$

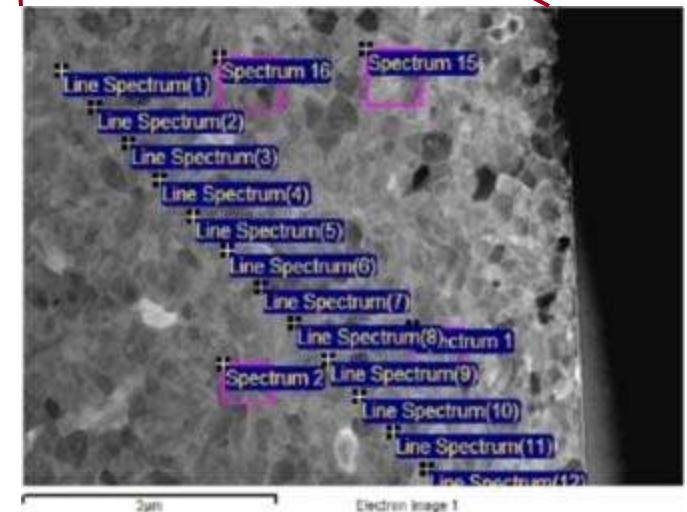
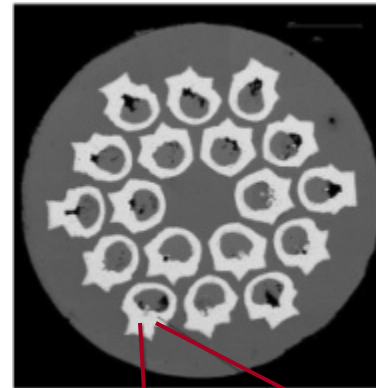
■ Abächerli,
TAS 2005

Composition variation in wires

- OST Internal-Tin wire
- Flat Sn content at 24 at.%
- $J_c(12T, 4.2) = 3000 \text{ A/mm}^2$



■ Uglietti, MT19 2005



Increasing J_c with increasing Sn



Geneva Bronze Process	25 at.% Sn @ source 4 at.% Sn/ μm gradient	$J_c(12\text{T}, 4.2) = 720 \text{ A/mm}^2$
SMI Powder-In-Tube	25 at.% Sn @ source 0.3 at.% Sn/ μm gradient	$J_c(12\text{T}, 4.2) = 2250 \text{ A/mm}^2$
OST Internal Tin	24 at.% Sn no gradient	$J_c(12\text{T}, 4.2) = 3000 \text{ A/mm}^2$

Sn richer
Higher J_c
Why?

Outline



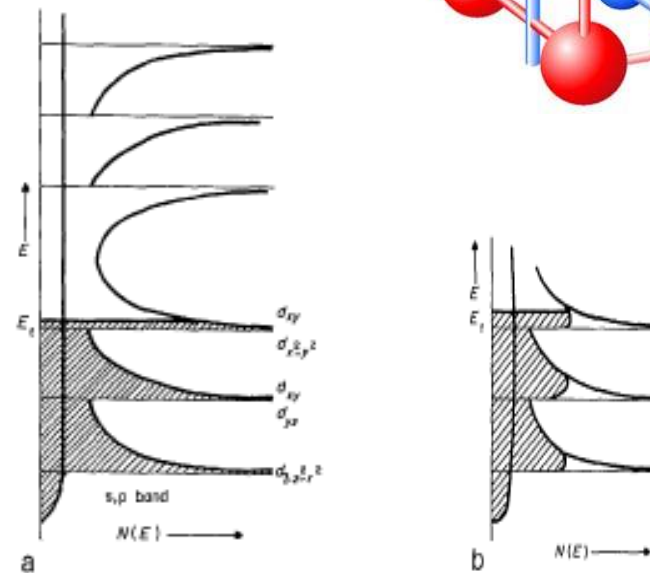
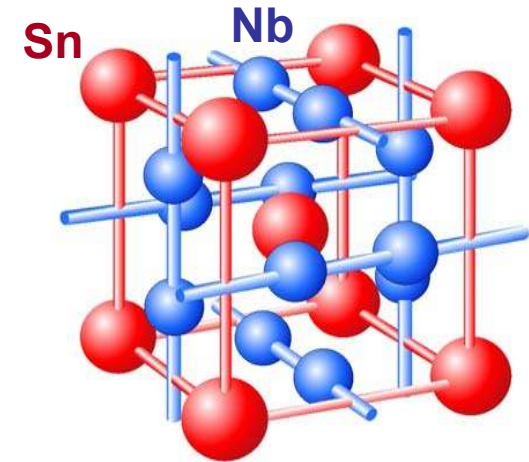
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What happens with changing Sn content?



- Pure Nb
 - *bcc* Nb spacing 0.286 nm
 - $T_c = 9.2$ K
- $\text{Nb}_3\text{Sn} \rightarrow$ A15 unit cell
 - *bcc* Sn, orthogonal Nb chains
 - Nb spacing 0.265 nm
 - High peaks in d-band DOS
 - Increased $T_c = 18$ K
- Off-stoichiometry
 - Sn vacancies unstable
 - Excess Nb on Sn sites
 - Additional d-band
 - Less electrons for chains
 - Rounded off DOS peaks
 - Reduced T_c

A15 lattice and DOS



■ Dew-Hughes, Cryogenics 1975

Nb chain continuity, $N(E_F)$, λ_{ep} , T_c , H_{c2}



In general

- Sn deficiency
 - ➔ 24.5 – 25 at.% Sn
- Tetragonal distortion
- Strain
- Alloying (Ti, Ta, ...)
- Dislocations
- Anti-site disorder

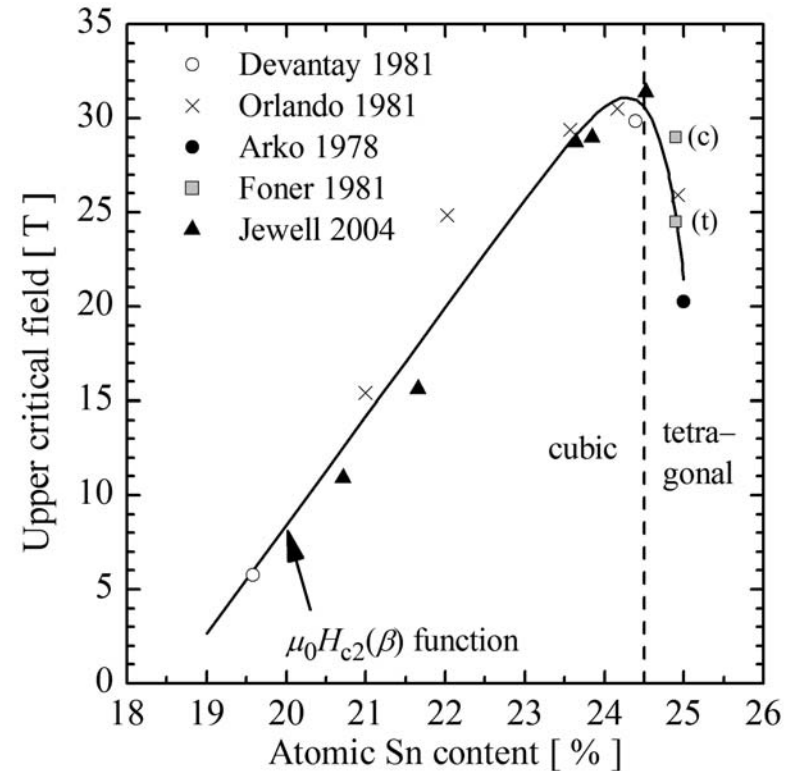
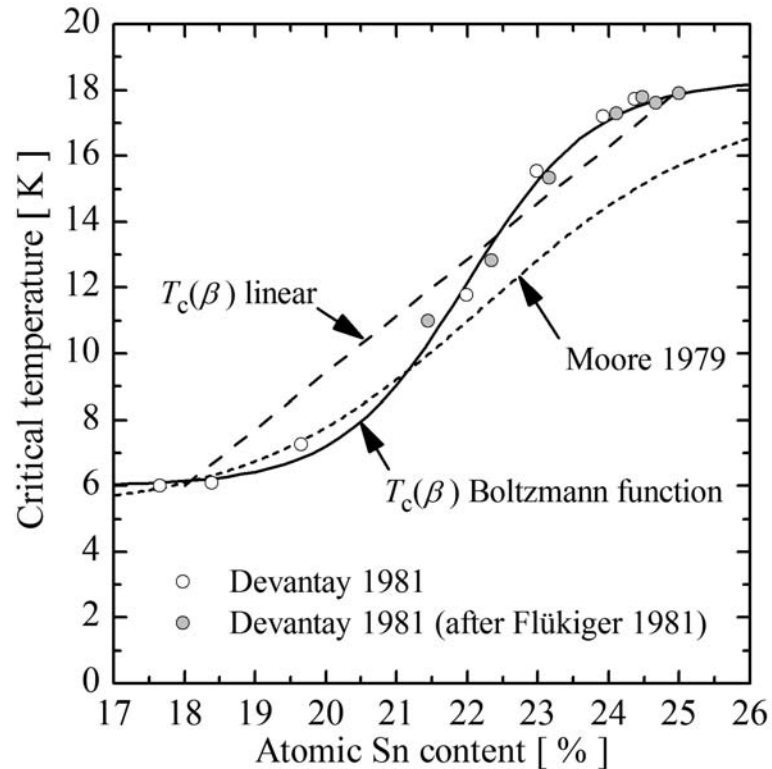
All affect Nb chain integrity ('Long Range Order')

- And thus $N(E_F)$ and λ_{ep}
- And thus T_c and H_{c2}

T_c and H_{c2} versus Sn content



Single crystal, bulk and thin film samples



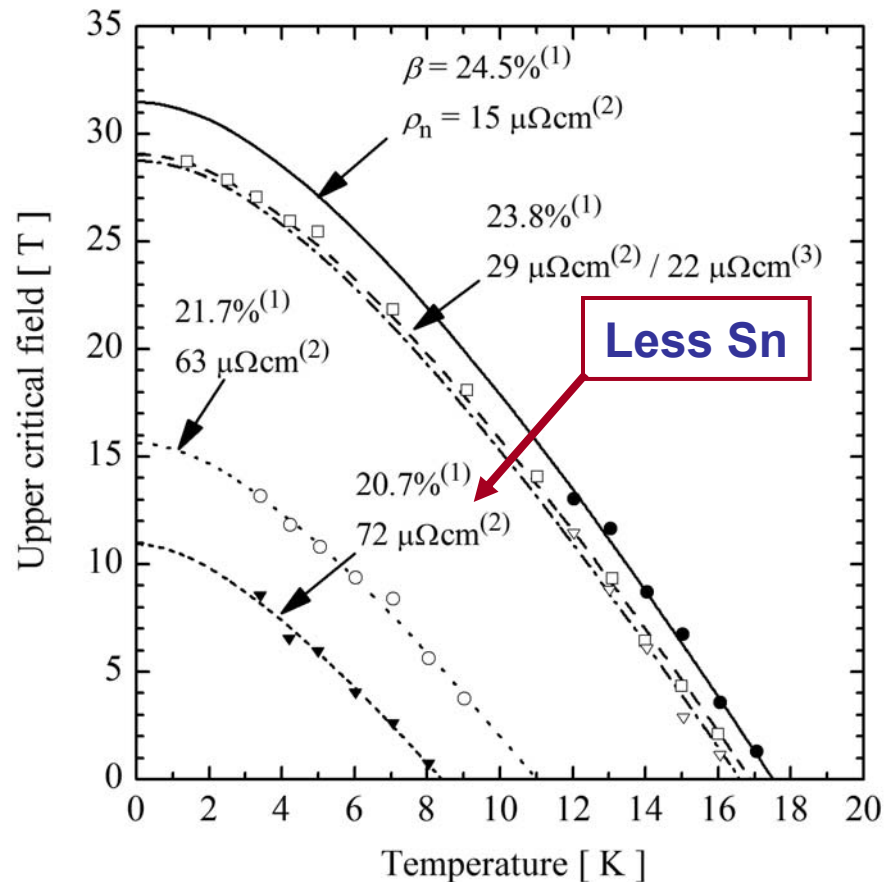
$$T_c(\beta) = \frac{-12.3}{1 + \exp\left(\frac{\beta - 0.22}{0.009}\right)} + 18.3$$

$$\mu_0 H_{c2}(\beta) = -10^{-30} \exp\left(\frac{\beta}{0.00348}\right) + 577\beta - 107$$

$H_{c2}(T)$ versus Sn content



■ Jewell, ACE 2004, bulk samples

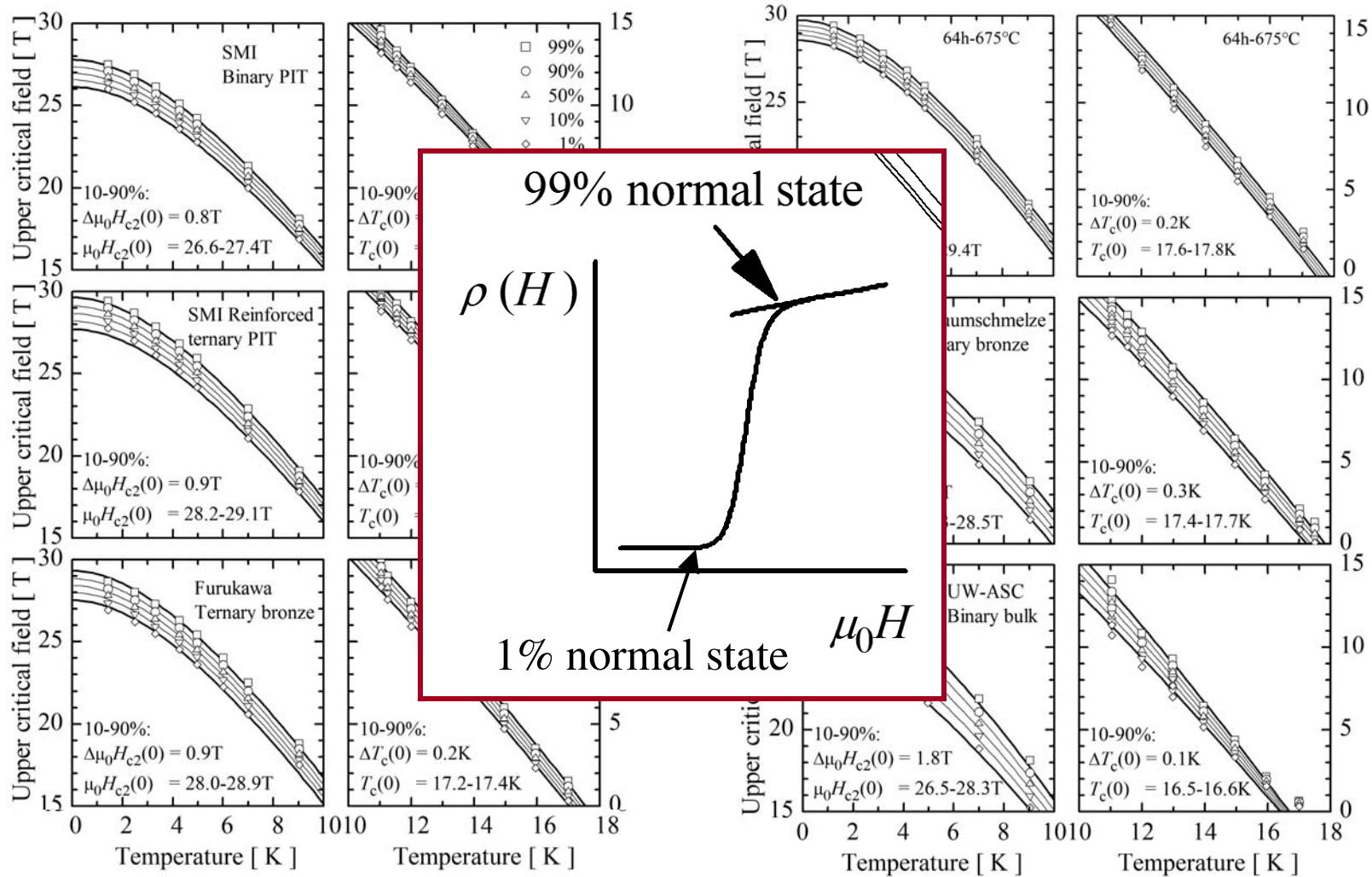


● Sn richer A15 has higher $H_{c2}(T)$ (until ~ 24.5 at.% Sn)

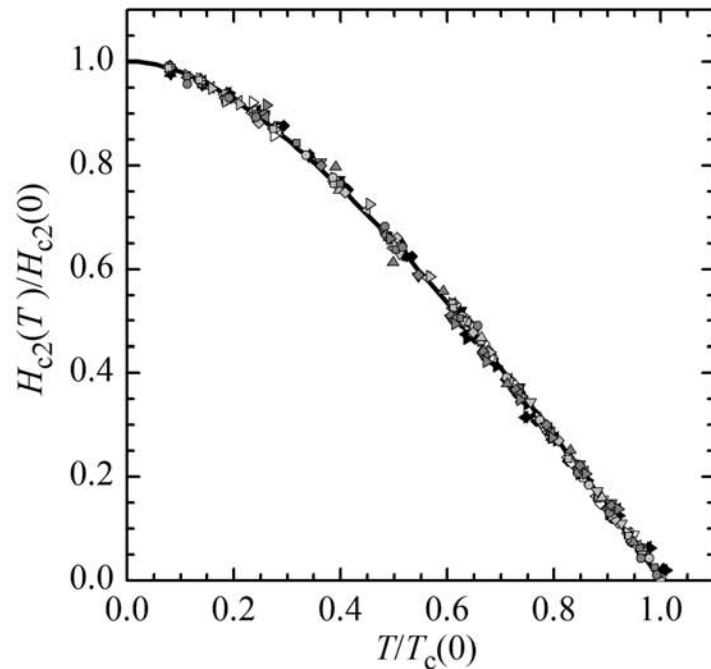
$H_{c2}(T)$ in wires



• $H_{c2}(T)$ from small current, resistive transitions



Normalized $H_{c2}(T)$ all available results



Ternary

- SMI PIT 4h/675°C 26.3-28.8T, 16.6-17.3K
- SMI PIT 16h/675°C 26.9-29.0T, 16.8-17.5K
- △ SMI PIT 64h/675°C 28.6-29.7T, 17.5-17.9K
- ▽ SMI PIT 768h/675°C 28.8-29.7T, 17.3-17.8K
- ◀ SMI PIT single fil.#1 28.3-30.3T, 16.7-17.3K
- ▶ SMI PIT single fil.#2 28.4-30.4T, 16.6-17.2K
- ◁ SMI reinforced PIT 27.7-29.6T, 17.7-18.0K
- Fur. br. on Ti-6Al-4V 27.5-29.3T, 17.0-17.5K
- Fur. br. on Brass 27.0-28.9T, 16.9-17.4K
- ▲ Fur. br. on Stainless 27.1-29.0T, 16.9-17.4K
- ▼ Fur. br. Free 27.5-29.4T, 16.9-17.5K
- ◇ Vac. bronze 26.6-29.2T, 17.2-17.8K
- ▽ $FUR \mu_0 H_K(T)$ 100 μ V/m
- ◇ $FUR \mu_0 H_K(T)$ 10 μ V/m
- ◀ $VAC \mu_0 H_K(T)$ 100 μ V/m
- ▶ $VAC \mu_0 H_K(T)$ 10 μ V/m

Binary

- ◁ Foner single crystal cubic 28.8T, 17.8K
- ▶ Foner single crystal tetr. 24.3T, 17.6K
- Foner poly-crystal mart. 25.2T, 17.8K
- Foner poly-crystal cubic 28.6T, 17.7K
- Orlando thin film 9 $\mu\Omega$ cm 26.3T, 17.4K
- △ Orlando thin film 35 $\mu\Omega$ cm 29.5T, 16.0K
- ▽ Orlando thin film 60 $\mu\Omega$ cm 25.4T, 13.2K
- ◇ Orlando thin film 70 $\mu\Omega$ cm 15.1T, 10.4K
- SMI PIT 26.1-27.8T, 17.8-17.9K
- ▲ UW-ASC bulk 19.3at.% Sn 10.9T, 8.4K
- ◆ UW-ASC bulk 24.4at.% Sn 25.5-29.3T, 16.4-16.7K

— Maki-DeGennes

● Shape $H_{c2}(T)$ independent of

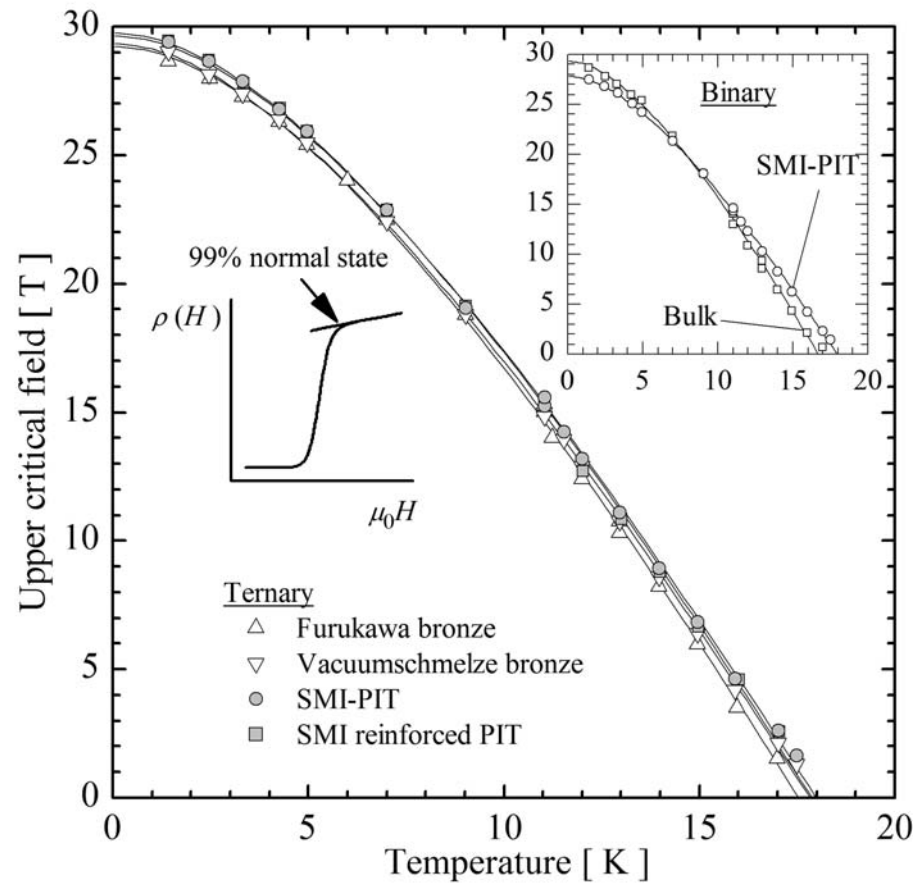
- Composition
- Morphology
- Strain state
- Applied critical state criterion

$$\ln\left(\frac{T}{T_c(0)}\right) = \psi\left(\frac{1}{2}\right) - \psi\left(\frac{1}{2} + \frac{\hbar D \mu_0 H_{c2}(T)}{2 \phi_0 k_B T}\right)$$

Approximation:

$$\frac{H_{c2}(t)}{H_{c2}(0)} \cong 1 - t^{1.52}, \quad t = \frac{T}{T_c(0)}$$

Highest $H_{c2}(T)$ in wires



$\mu_0 H_{c2}(0) = 30 \text{ T}$, $T_c(0) = 18 \text{ K}$ is upper limit

Outline

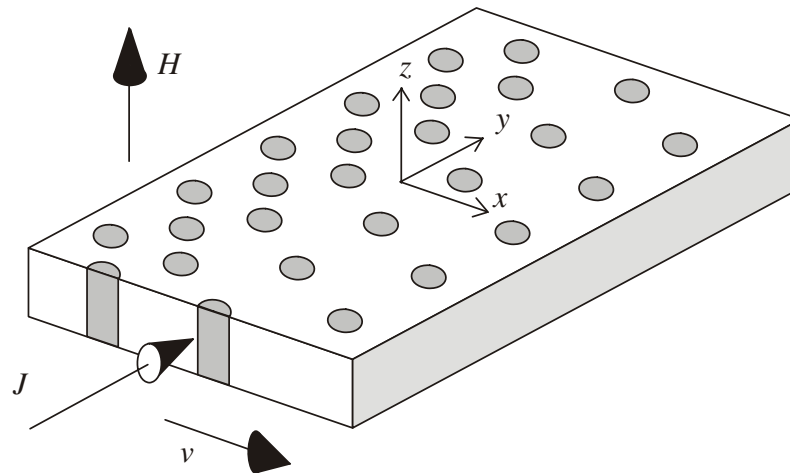


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Pinning: Why does Nb₃Sn need it?



- Nb₃Sn slab in $H_{c1} < H < H_{c2}$
- Field quanta $\phi_0 = h / 2e$ (flux-lines) penetrate slab



- Transport current ($\nabla \times \mathbf{B} = \mu_0 \mathbf{J}$) causes gradient B_x
- Flux-lines repel \rightarrow move ($\nabla \times \mathbf{E} = -d\mathbf{B}/dt$) $\rightarrow E_y \rightarrow$ Loss
 - Need to be 'pinned' at 'pinning centers' by 'pinning force' F_p
- Optimal pinning at 1 pinning center / flux-line

What determines pinning capacity?



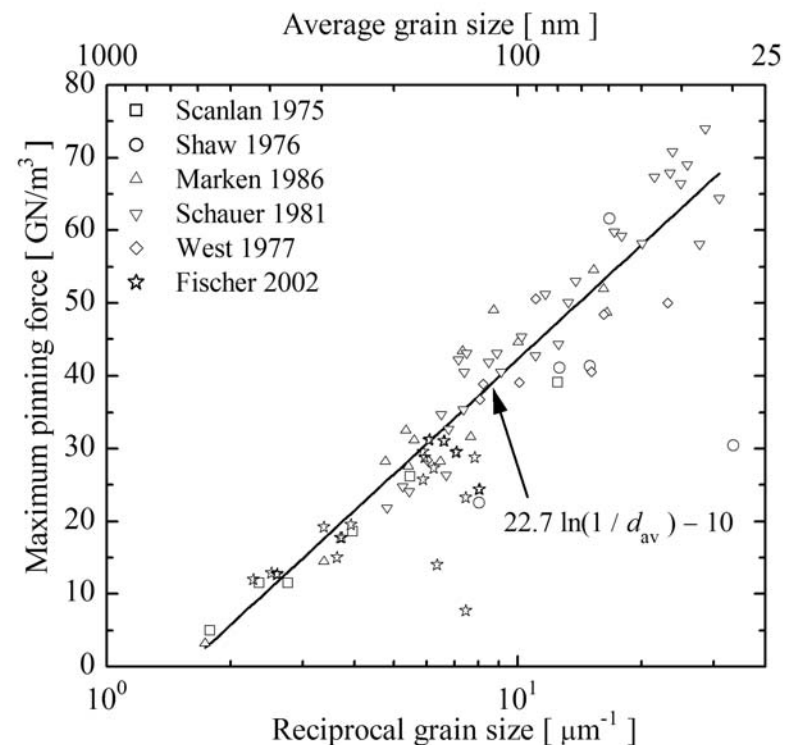
Pinning centers

- Positions with minima in SC wave function

- Normal regions
- Grain boundaries
- Lattice imperfections
- ...

- **Nb₃Sn**

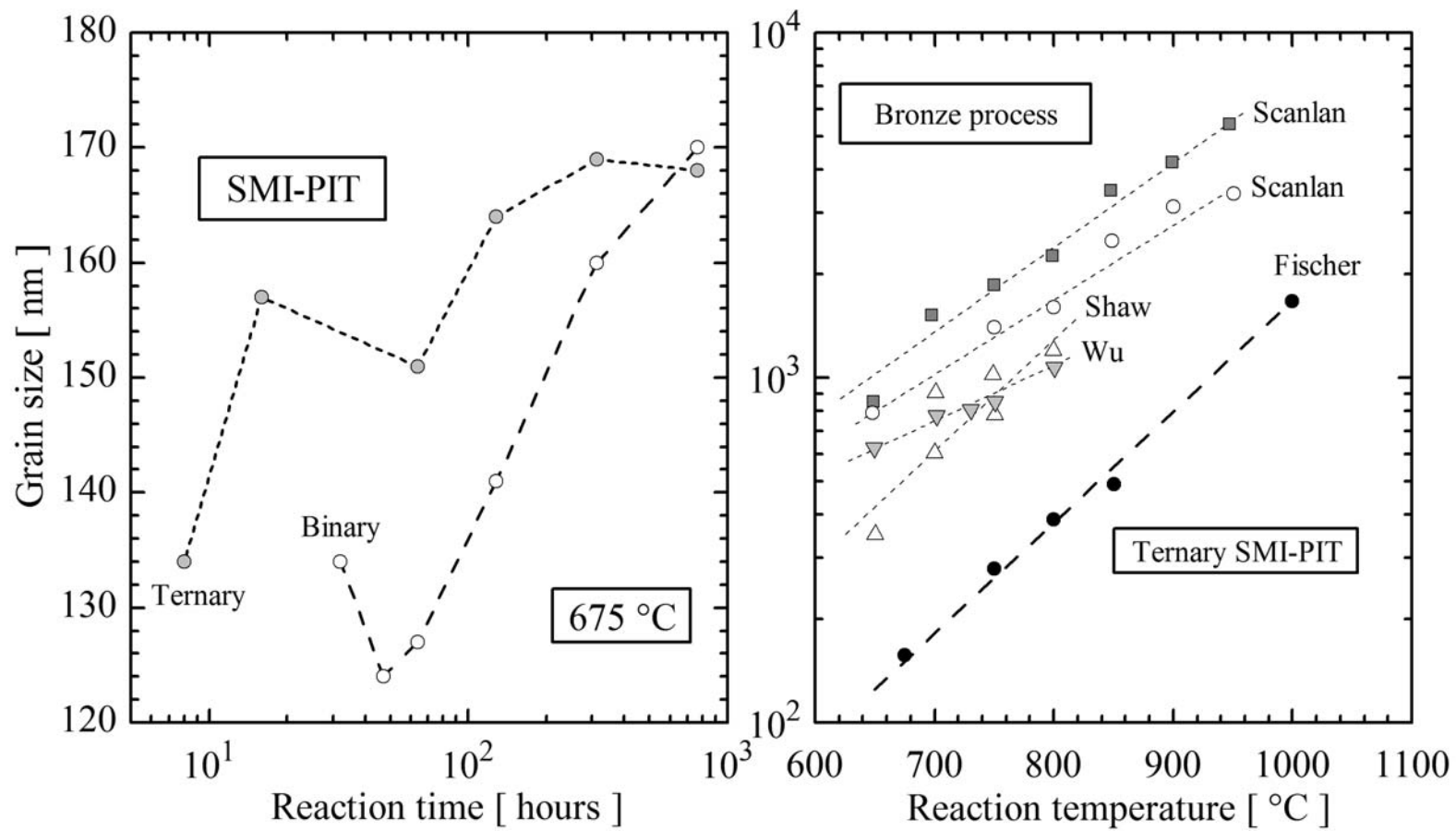
- Grain boundaries
→ Main pinning centers
- Grain size determines F_{Pmax}



What determines grain size?



- Presence of grain nucleation points
- Reaction time and temperature



What is an optimal grain size?



Ideal: One pinning center per flux-line $\rightarrow a_{\Delta} \approx d_{av}$

- **Flux-line spacing \rightarrow field dependent**
 - E.g. at 12 T $a_{\Delta} = (4/3)^{1/4}(\phi_0/\mu_0 H)^{1/2} = 14$ nm
 - Grain size in Nb₃Sn wires \rightarrow 100 – 200 nm
 - Order of magnitude from optimal

- **For any practical field $a_{\Delta} \ll d_{av}$**
 - Collective pinning ('shearing' of FLL)
 - $a_{\Delta} \rightarrow d_{av}$ only for $\mu_0 H \ll 1$ T

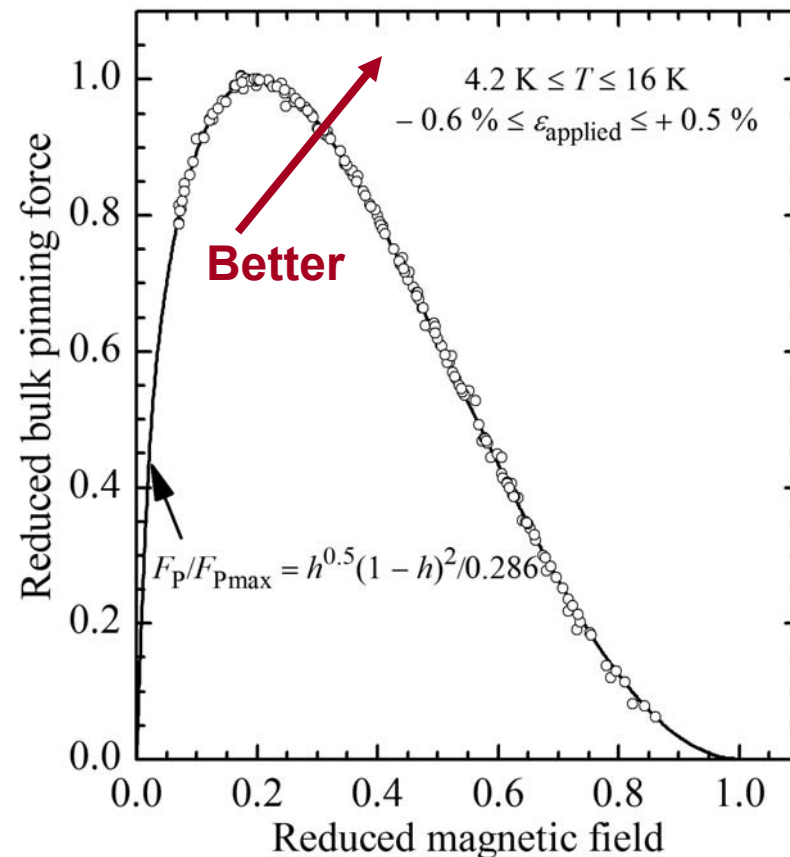
- **NbTi in contrast**
 - Nano-scale distribution of α -Ti precipitates
 - $a_{\Delta} \approx \alpha$ -Ti distribution for application fields
 - NbTi is fully optimized

What does $a_{\Delta} \ll d_{av}$ mean in practice?



- De-pinning → Synchronous shearing of FLL
- F_{Pmax} at $H/H_{c2} = 0.2$
 - About 6 T for Nb_3Sn
 - Far below application fields
- Grain refinement / APC
 - F_{Pmax} to higher field
 - $F_{Pmax} \rightarrow H/H_{c2} > 0.4$ shown by Cooley, ACE 2002
 - Higher fields accessible with Nb_3Sn
- Much room for improvement!

- Example: Bronze processed ITER wire (Furukawa)



Alternative presentation $a_{\Delta} \ll d_{av}$



- Flux shear model

- ▶ Kramer JAP 1973

$$F_P(H) = 12.8 \frac{(\mu_0 H_{c2})^{2.5}}{\kappa_1^2} \frac{h^{0.5} (1-h)^2}{(1 - a_{\Delta}(H)/d_{av})^2}, \quad h = \frac{H}{H_{c2}} \quad [\text{GN/m}^3]$$

$$\therefore J_c^{0.5} (\mu_0 H)^{0.25} = \frac{1.1 \times 10^5}{\kappa_1} \frac{\mu_0 (H_{c2} - H)}{(1 - a_{\Delta}(H)/d_{av})}$$

- $a_{\Delta} \ll d_{av}$: Kramer plot

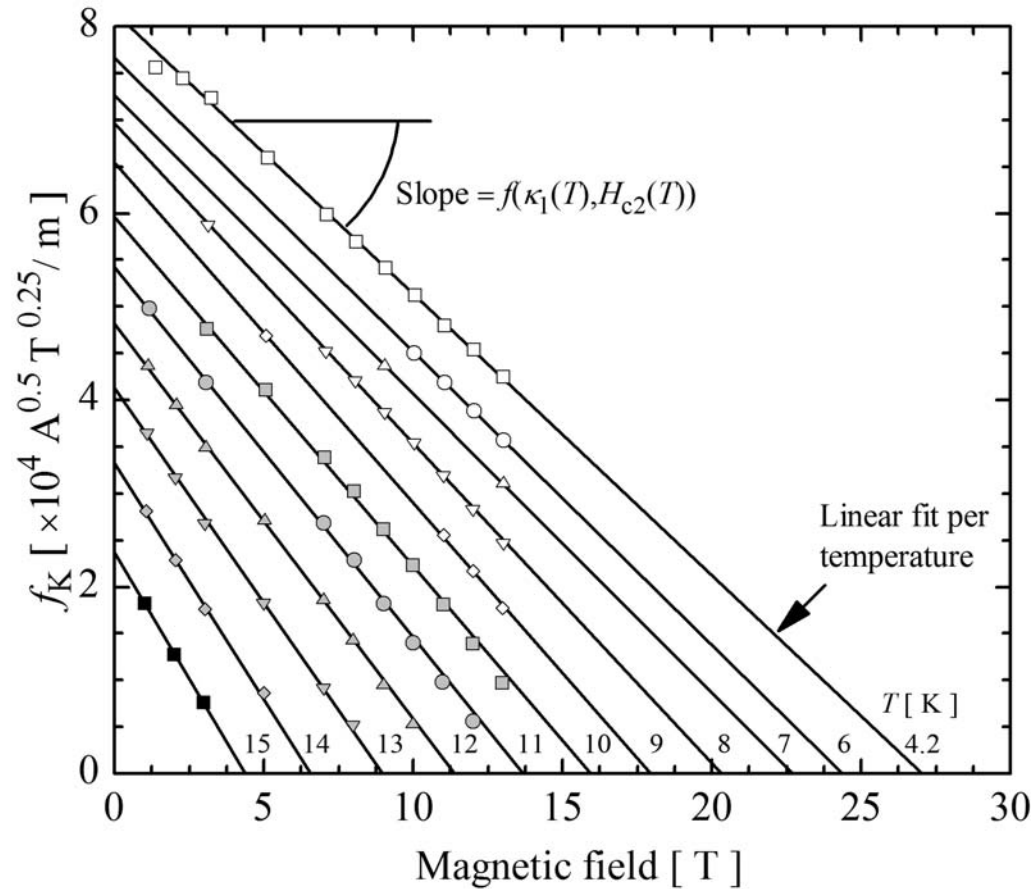
$$f_K(H) \equiv J_c^{0.5} (\mu_0 H)^{0.25} \cong \frac{1.1 \times 10^5}{\kappa_1} \mu_0 (H_{c2} - H) \quad \therefore f_K(H) \propto H$$

- Linear in H

'Kramer' plot



- Plot of $f_K(H)$ at various temperatures



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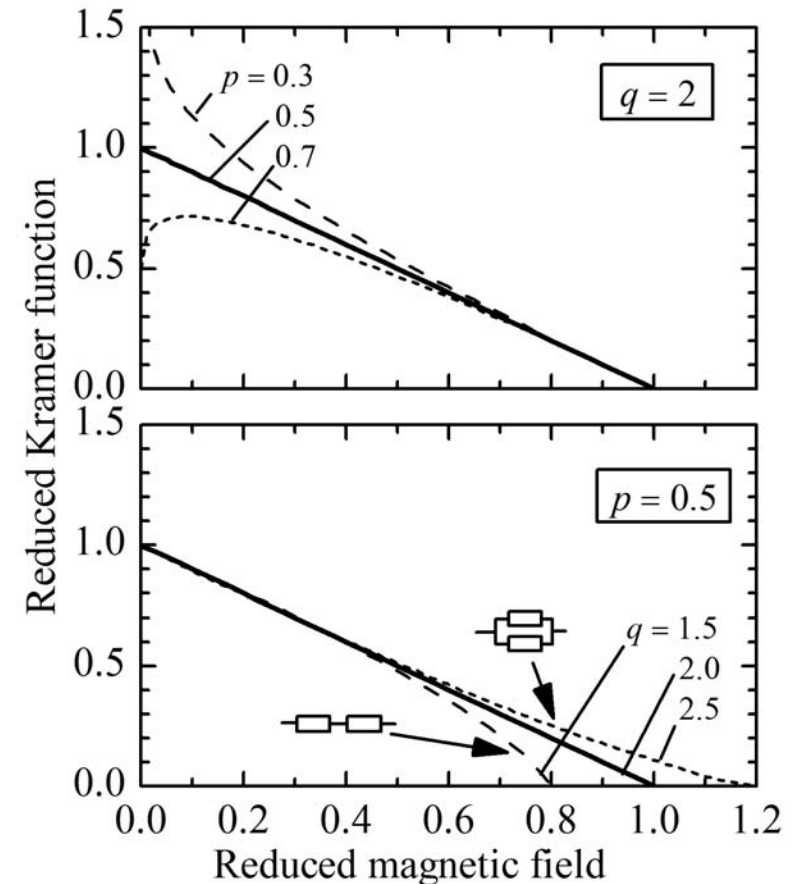
Are Kramer plots linear?



$$F_P(h) = 12.8 \frac{(\mu_0 H_{c2})^{2.5}}{\kappa_1^2} h^{0.5} (1-h)^2 \quad a_\Delta \ll d_{av}$$

$$\hat{=} F_P(h) = F_{Pmax} h^p (1-h)^q \quad p = 0.5, \quad q = 2$$

- **Linearity from $h \cong 0.03$ to 0.8**
 - Confirmed by measurements
- **$a_\Delta \cong d_{av}$ only below $h \cong 0.03$**
- **Different pinning mechanism?**
 - only below $h \cong 0.03$
- **Non-linearity below $h \cong 0.03$**
 - Different pinning mechanism
- **Non-linearity above $h \cong 0.8$**
 - Inhomogeneity artifacts
 - Averaging over H_{c2} distribution

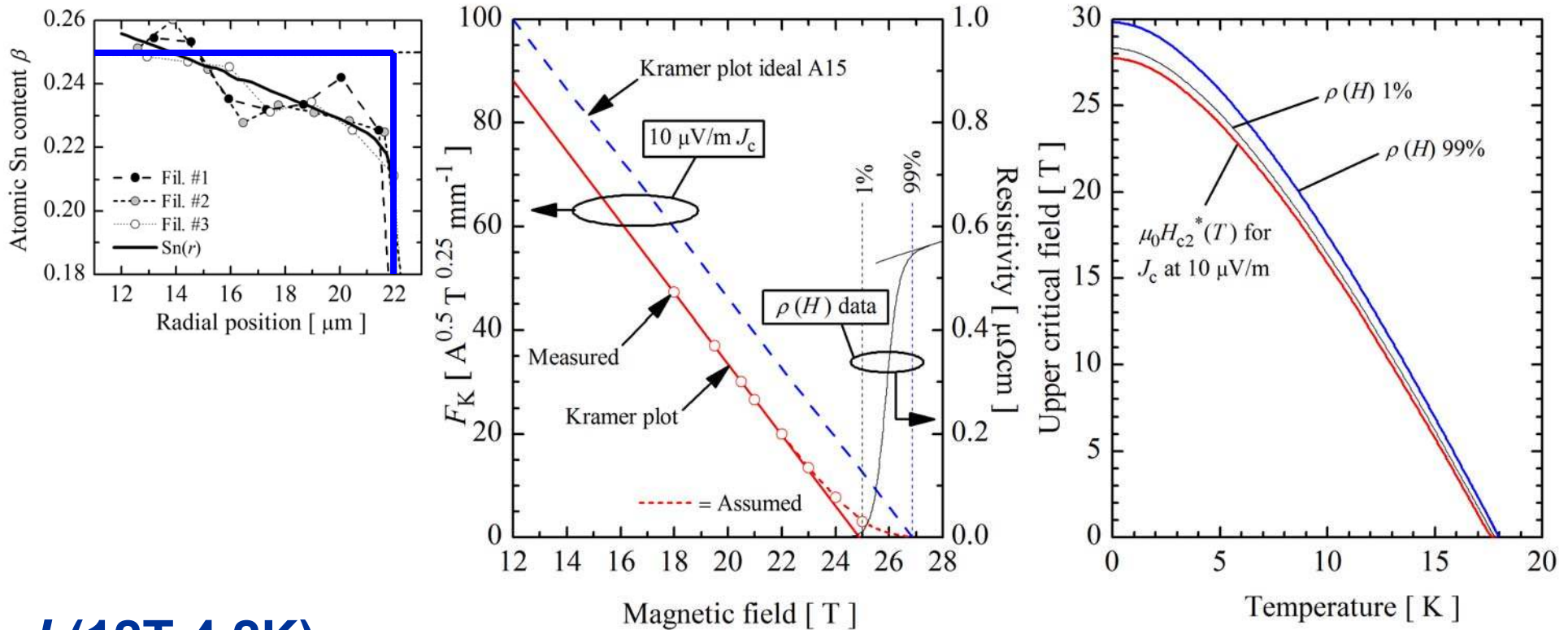


Effective $H_{c2}(T)^*$ for J_c



J_c scales with 'some' average $H_{c2}(T)^*$

- J_c gain if all A15 is stoichiometric?



$J_c(12\text{T}, 4.2\text{K})$

- From 2250 A/mm^2 to 2900 A/mm^2

Outline

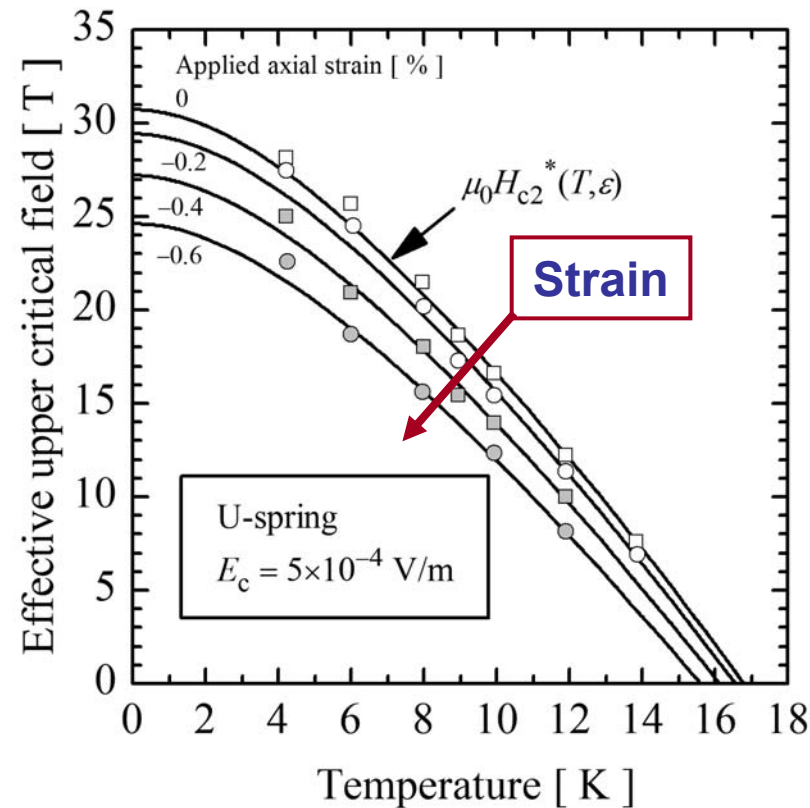


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Strain sensitivity of $H_{c2}(T)$

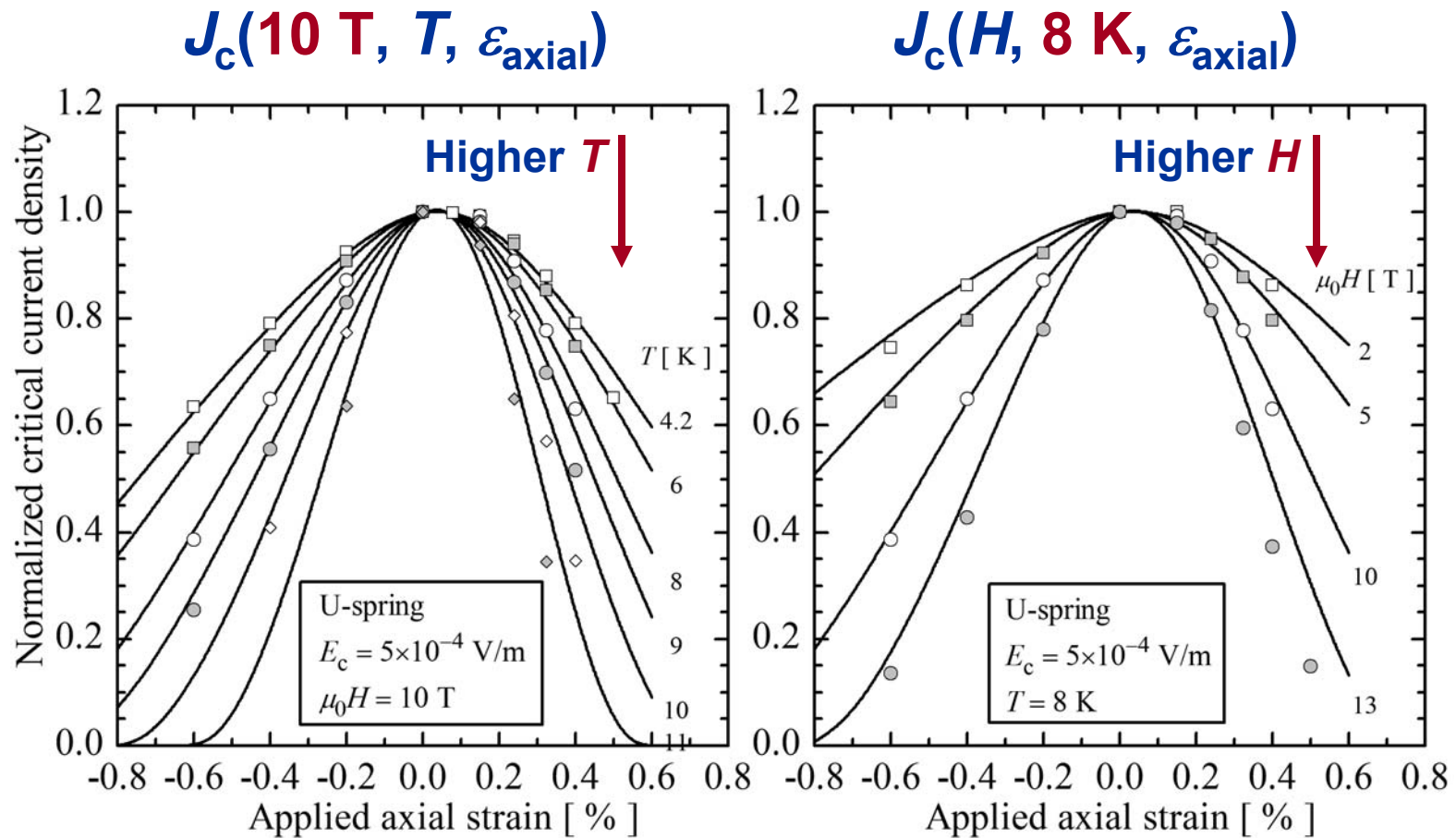


- Longitudinal strain effects on effective $H_{c2}(T)^*$



- Strain and composition have similar effects
 - Need for a separation of parameters

Strain sensitivity of $J_c(H, T)$



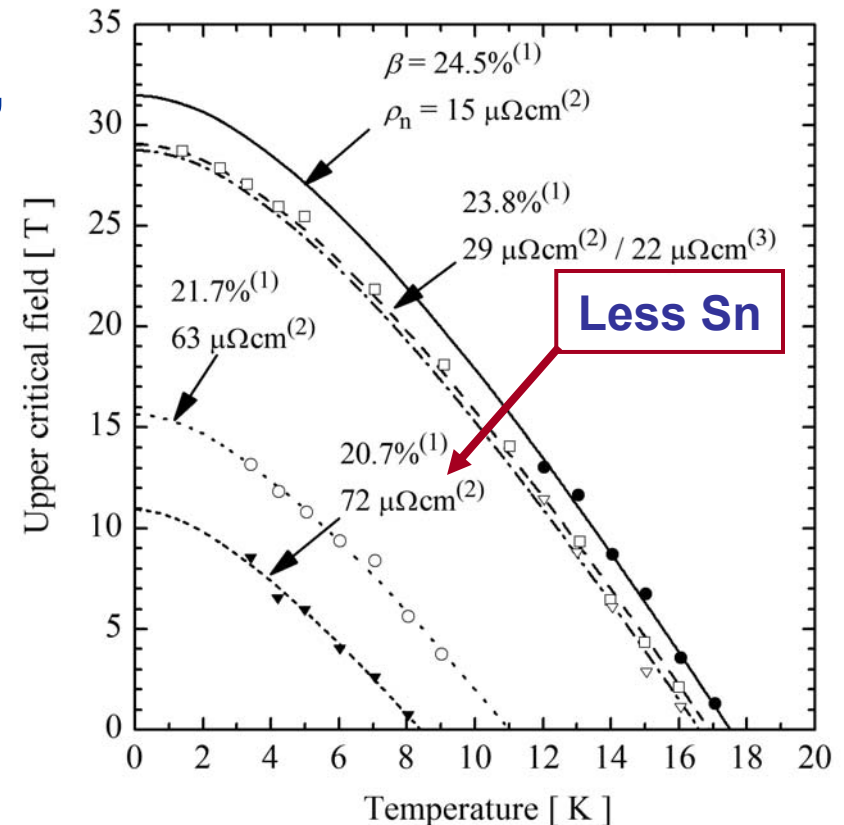
- Why is strain sensitivity increased at higher H and T ?

Strain sensitivity versus composition



At higher H and T

- Low Sn A15 sections “die out”
 - Benefit PIT and IT vs Bronze:
 - ➔ Larger volume fraction high Sn
 - High Sn sections determine SC properties
- Increased strain sensitivity
 - Is Sn rich A15 more strain sensitive than Sn poor A15 ?

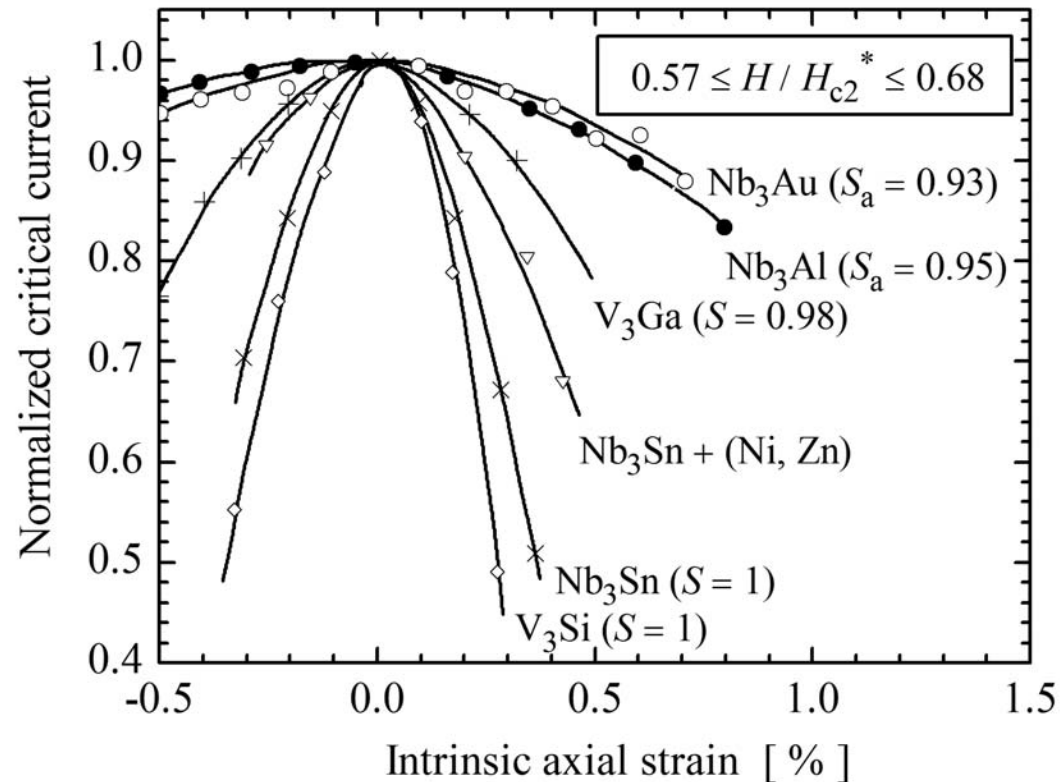


- Does wire optimization through Sn enrichment cause higher strain sensitivity?

Strain sensitivity versus LRO



- $S \rightarrow$ Bragg-Williams order parameter



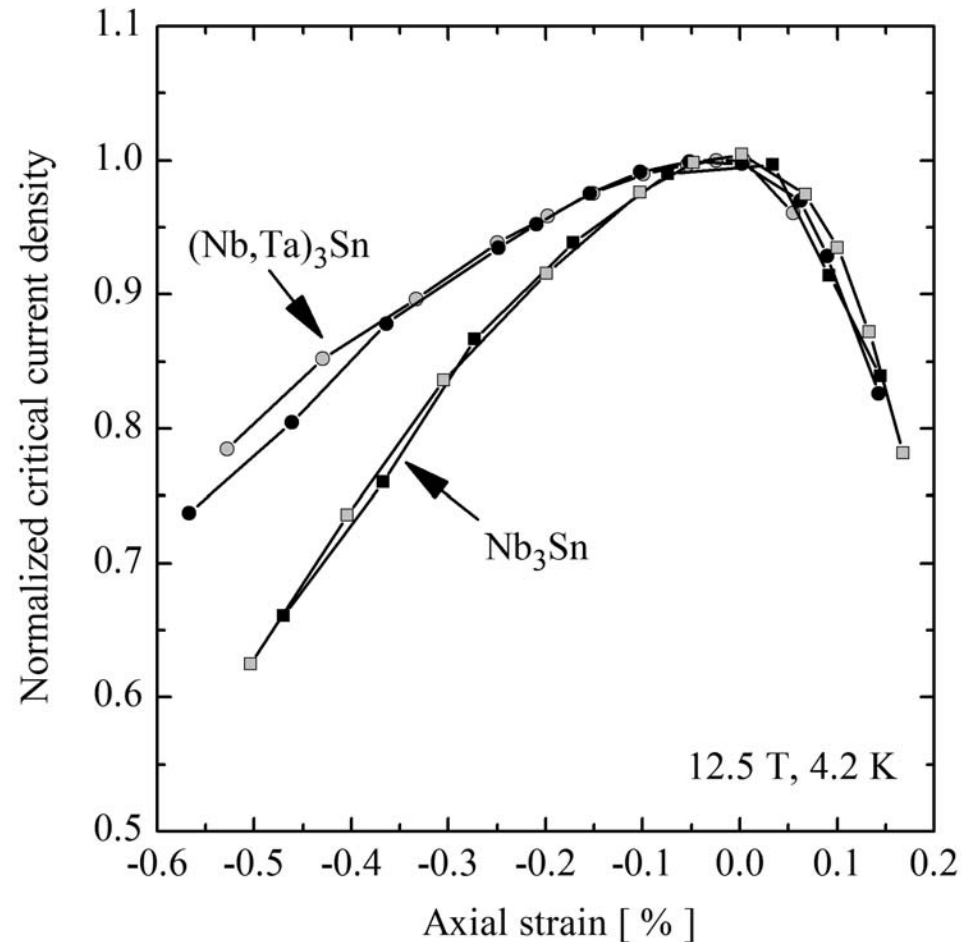
■ Flükiger, ACE 1984

- Higher LRO ($\hat{=}$ more Sn) \rightarrow larger strain sensitivity

Strain in ternary and binary wires



- Alloyed \rightarrow more disorder \rightarrow reduced strain sensitivity?

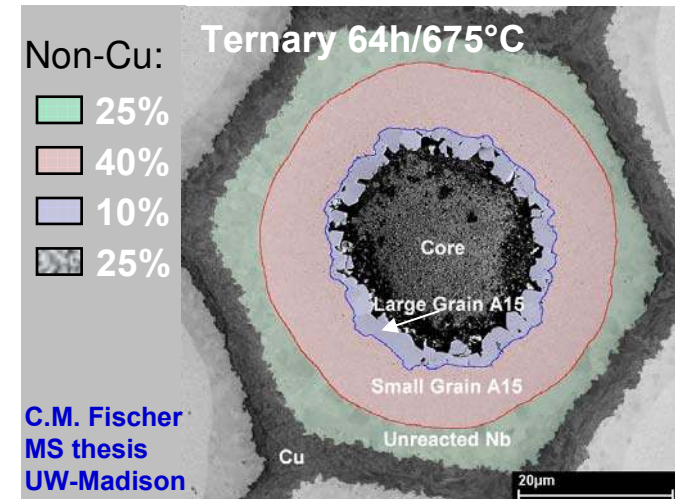
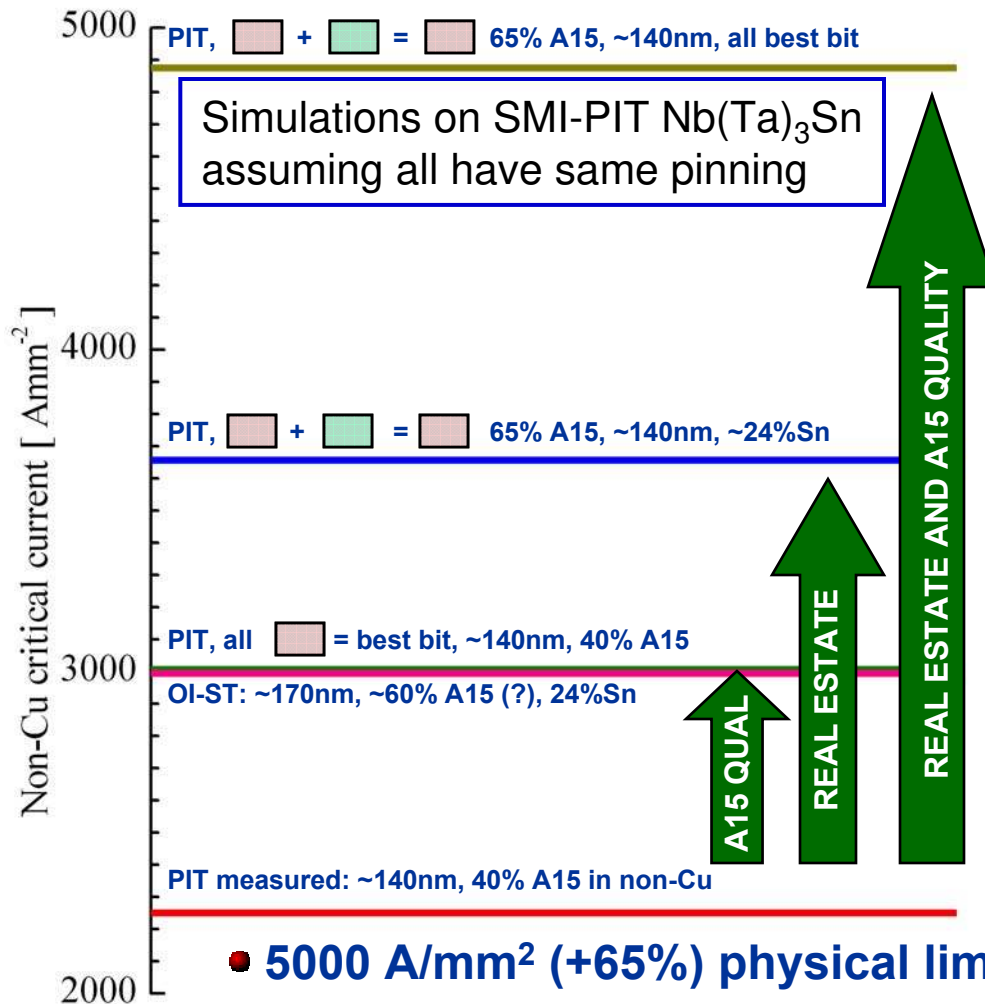


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Prospects for critical current density



- **Pinning?**
 - SMI-PIT grains ~ 140 nm
 - OST-IT grains ~ 170 nm
 - 12 T → $a_{\Delta} = 14$ nm
- **Large gains possible**

- **5000 A/mm² (+65%) physical limit with present wire designs?**
 - Unless pinning is improved
- **4000 A/mm² realistic optimization goal?**

Summary



Wire optimizations past decade

- Sn enrichment
- A15 fraction in non-Cu optimization
- Physical limit 5 kA/mm², realistic limit 4 kA/mm²

Grain refinement / APC

- The next big step?
- Grain size one order above optimal
- Grain 10 – 20 nm desired → nano technology

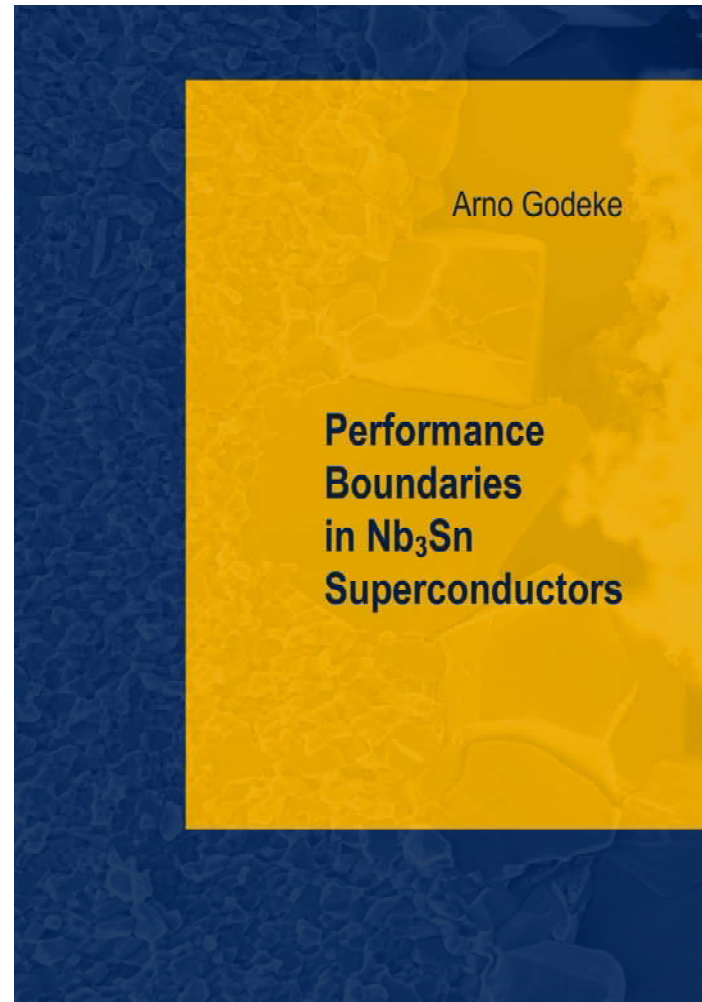
Strain

- Strain and composition parameter separation needed
- Sn enrichment = more strain sensitivity?
- Much work to be done (3D, theory, bulk, film,...)

More information



- Available on request → agodeke@lbl.gov





Optional theory section

$N(E_F)$ and $\lambda_{ep} \rightarrow T_c$ and H_{c2}



• Weak coupling (BCS based)

$$T_c(0) \cong \frac{2e^{\gamma_E}}{\pi k_B} \hbar \omega_c \exp\left[-\frac{1}{V_0 N(E_F)}\right] \quad \therefore \quad T_c(0) \cong 1.134 \Theta_D \exp\left[-\frac{1}{\lambda_{ep}}\right]$$

$$\mu_0 H_{c2}(0) \cong k_B e N(E_F) \rho_n T_c(0) = \frac{3e}{\pi^2 k_B} \gamma \rho_n T_c(0)$$

• Interaction strength independent (Eliashberg based)

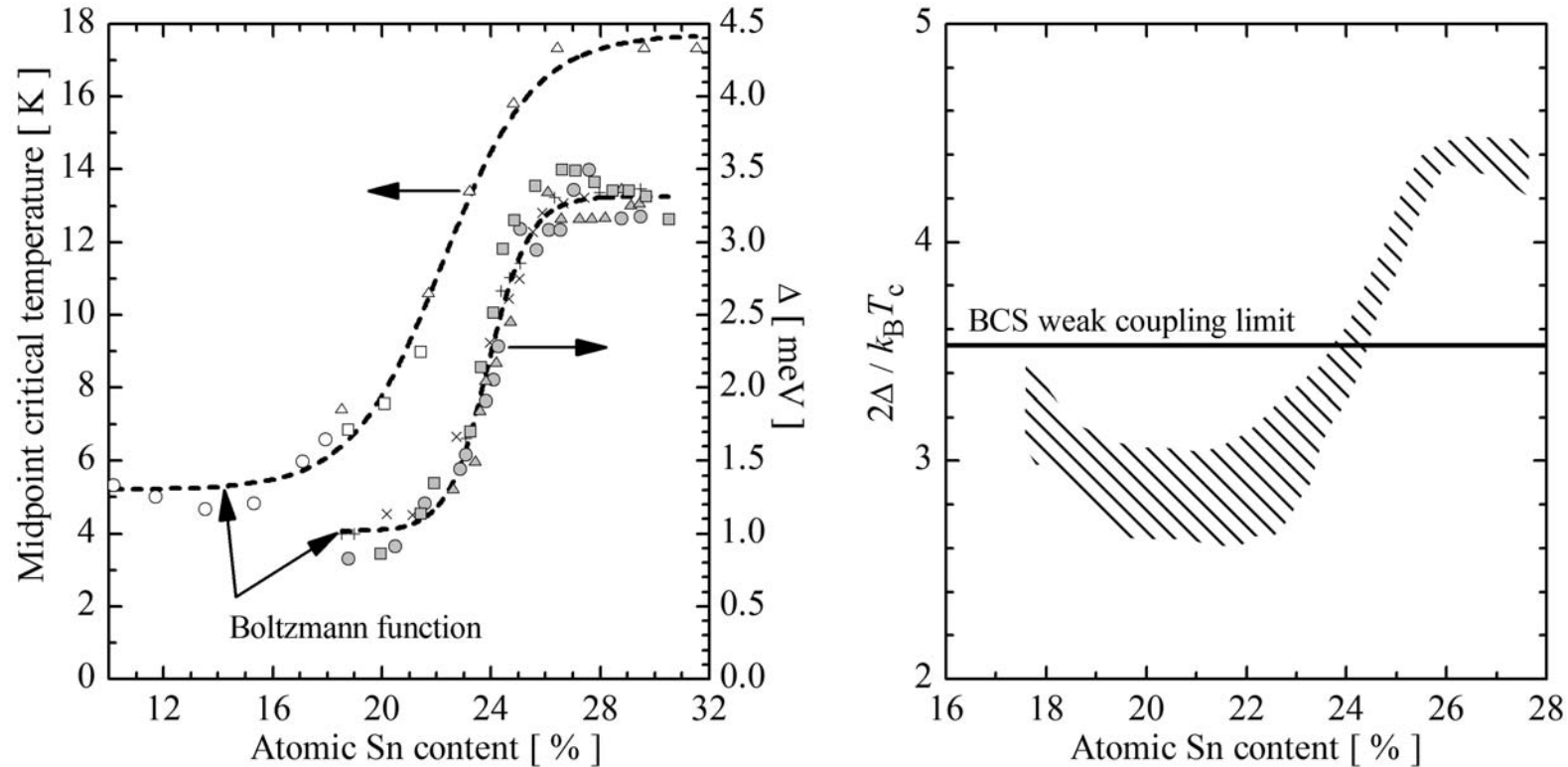
$$\lambda_{ep} = 2 \int \frac{\alpha^2(\omega) F(\omega)}{\omega} d\omega \quad \lambda_{\text{eff}} = \frac{(\lambda_{ep} - \mu^*)}{(1 + 2\mu^* + 1.5\lambda_{ep}\mu^* e^{-0.28\lambda_{ep}})}$$

$$T_c = \frac{0.25 \langle \omega^2 \rangle^{\frac{1}{2}}}{(e^{2/\lambda_{\text{eff}}} - 1)^{\frac{1}{2}}} \quad \mu_0 H_{c2} = \dots$$

Is Nb_3Sn weak or strong coupling?



■ Moore, PRB 1979, thin film samples



- Weak coupling below 23 – 24 at.% Sn
- Strong coupling approaching stoichiometry

Applicable theory



$N(E_F)$ and $\lambda_{ep} \rightarrow T_c$ and H_{c2}

- Wires \rightarrow 18 – 25 at.% Sn, polycrystalline
- Interaction strength independent theory
- Not done for entire composition range
- $N(E_F)$ and $\lambda_{ep} \rightarrow T_c$ and H_{c2} remains empirical

Promising recent work

- Eliashberg-based description of $T_c(\varepsilon)$ and $H_{c2}(\varepsilon)$
 - Markiewicz, Cryogenics 2004
 - Oh, JAP 2006