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Photoinduced Controlled Radical Polymerizations Performed in Flow: Methods, Products, and Opportunities†

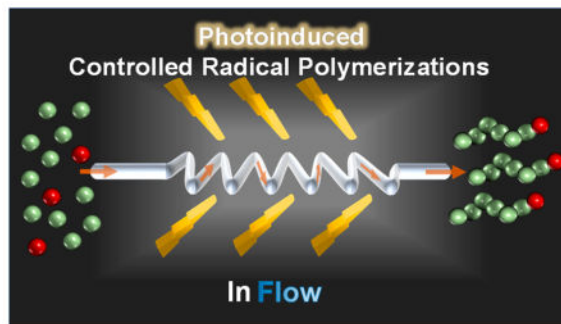
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Abstract

Photoinduced controlled radical polymerizations (CRPs) have provided a variety of approaches for the synthesis of polymers possessing targeted structures, compositions, and functionalities with the added capability for spatial and temporal control, presenting the potential for new materials development. However, the scalability and reliability of these systems can be limited as a consequence of dependence on uniform irradiation of the reaction to produce well-defined products. In this perspective, we highlight the utility and promise of photo-CRP approaches through an overview of the adaptation of these methodologies to photo-flow reactor systems. Special emphasis is placed on the current state-of-the-art in polymerization scalability, reactor design, and polymer scope.

Graphical Abstract



1. INTRODUCTION

Polymeric materials have shaped the modern world, becoming integrated into all facets of society. While commodity plastics are undoubtedly important, polymeric materials have also emerged to address challenges in biomedical, electronic, and energy-storage fields.¹ The

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Notes

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discovery of living anionic polymerization by Szwarc in 1956 enabled precise control over polymer properties, stemming from well-defined polymer compositions, architectures, control over molecular weight growth, and narrow molecular weight distributions.^{2,3} Other polymerization methodologies with these capabilities have since been developed and include living or controlled coordinative chain-transfer,⁴ cationic,⁵ ring-opening,⁶ ring-opening metathesis,⁷ group-transfer,⁸ and controlled radical polymerizations (CRPs).⁹

Despite the inherent presence of termination events, CRPs have been shown to be effective in their ability to impart a high level of control over desirable polymer characteristics while providing access to a wide scope of materials.^{10,11} Radical polymerization approaches, including CRPs and “uncontrolled” free radical polymerizations, benefit from functional group tolerance, wide thermal stability, compatibility with a variety of reaction conditions, and simplicity of operation. As such, free radical polymerizations have been broadly implemented industrially,¹² but due to pervasiveness of radical termination events, the synthesis of polymers possessing well-defined or complex compositions and architectures is challenging. In CRPs, control over polymer composition and architecture gives rise to unique properties which can be precisely modulated to meet desired applications (Figure 1).^{13,14} For example, an important asset of CRP systems is the presence of a functional chain-end group, determined by the structure of the initiating species, allowing for facile post-polymerization transformations to install additional functionality as well as sequential additions of monomer to produce block copolymers with distinct chemical domains.

All CRP techniques rely on the formation of a dynamic equilibrium between dormant and active propagating states of the growing polymer chain. Control over radical reactivity is predominantly established either through a “degenerative chain transfer” process or through a “reversible deactivation” mechanism (Figure 2). Degenerative chain-transfer CRPs rely on a fast and selective exchange equilibrium between active radicals and dormant chain-transfer agents, maintaining constant radical concentrations.²¹ Reversible addition–fragmentation chain transfer (RAFT) is a widely studied degenerative chain-transfer approach.²²

In reversible deactivation CRPs, radical concentrations remain low through the reversible activation of the propagating radical species, followed by reformation of a dormant polymer chain through the deactivation by either a reversibly coupling species or through an atom-transfer mechanism (Figure 2B). Traditionally, the dormant polymer species is thermally activated, but can also be activated through the presence of external stimuli, including photo-, electro-, and mechano-approaches. Atom-transfer radical polymerization (ATRP),²³ metal-catalyzed living radical polymerization,¹⁰ nitroxide-mediated polymerization (NMP),¹⁴ and cobalt-mediated radical polymerization (CMRP)²⁴ are the most common examples of reversible deactivation approaches. In both classifications, a controlled polymerization consists of a linear increase of molecular weight (MW) with respect to monomer conversion, dispersity (D) less than 1.5, and initiator efficiencies (F^*) ideally close to 100%. F^* is an important parameter, which compares the theoretical number-average molecular weight (M_n) to the experimentally measured M_n , evidencing the control over the polymerization.

The initial development of CRPs relied on thermally activated catalysts or initiators. In recent years, several photoinduced CRP (photo-CRP) variants have been developed,

introducing the added potential for spatial and temporal control over polymerization.^{25–27} The earliest established methodologies used direct photolysis of an initiating species to begin monomer propagation, for example in NMP,²⁸ organotellurium-mediated radical polymerization,²⁹ RAFT,³⁰ photo-iniferter polymerization,²⁵ and CMRP,³¹ the latter three of which are discussed in greater detail later in this perspective. Photoredox catalysis,^{32–35} which has been broadly applied in small molecule transformations, has expanded the capabilities of CRP systems. This focus uses photoredox catalysts (PCs) to mediate a photoredox catalytic cycle, minimizing photo-degradation of dormant polymer species and chain-end groups while introducing an additional avenue to tailored control over polymer properties and functions.

Due to facile reaction conditions and components the development of photo-CRPs has typically been carried out in batch-style reactors with small reaction volumes. In batch reactors, large reaction volumes are difficult to uniformly irradiate, and therefore scalability of these reactions while maintaining a high level of control over polymerization can be difficult and unreliable. For photo-CRP systems, application of these rapidly evolving approaches to the industrially relevant production of materials with tailored properties and applications requires reliable reaction scalability.

Flow reactor systems have been shown to be powerful alternatives to batch reactors in small molecule and polymer synthesis, with original adaptation performed for thermally mediated systems and expanded to include photochemical approaches.^{36,37} This actualization can be widely accredited to improved scalability,^{38,39} control over process parameters,⁴⁰ enhanced reliability,⁴¹ and decreased reaction times.⁴² Furthermore, flow chemistry is viewed as a sustainable approach toward chemical production and processing, offering potential for increased reaction efficiency and limitations in solvent usage and byproduct formations.⁴³ These benefits, while initially applied toward small molecule transformations, have also translated to a large range of thermally mediated polymerization approaches.^{44–47} While photo-CRP techniques have seen rapid expansion in reaction development and specialized materials design, to fully utilize the capabilities of CRPs expansion into reactor systems capable of refining reaction control and improving product scalability needs to be realized.

In this Perspective, an overview of the development of photo-CRP processes in flow reactor systems is presented, beginning with a description of flow reactor systems and experimental design, and also highlighting useful information for adapting photo-CRPs to flow from batch polymerizations. A thorough description of the current scope of photo-CRP reactions produced in continuous flow is presented, classified by either degenerative chain-transfer or reversible deactivation mechanisms for comparison within similar polymerization approaches. Special emphasis is placed on the effect of polymerization mechanism on reactor design, the current scope of polymer products reported, and future directions to expand the growing field of photo-CRPs.

2. ADVANTAGES AND MOTIVATIONS FOR FLOW REACTORS SYSTEMS

2.1. Key Characteristics of Photochemical Flow Reactors

One of the key advantages of flow reactor systems for photochemically mediated processes stems from the ability to improve the irradiation of the reaction mixture. In a typical batch reactor system, irradiation is attenuated toward the center of the reactor with an increasing path length, as is supported by the Beer–Lambert law,

$$A = \epsilon cl \quad (1)$$

where ϵ is the molar absorptivity of the photoactive species, c is the concentration of the photoactive species, and l is the optical path length of the system, or in this case the diameter of the photoreactor. In cases where photochemistry is applied for the synthesis of small molecules, non-uniform irradiation may result in slower reaction rates, non-productive side reactions, and subsequently lower reaction yields. For photo-CRPs, attenuating irradiation in solution causes non-concurrent initiator activation, a subsequent non-uniform formation of polymer chains, and the potential for loss in control over polymer MW and \mathcal{D} , as well as increased reaction times. In cases where a strong absorber with a high ϵ is used to mediate polymerization, the effect of reactor diameter can be more dramatic. For example, the light transmission through a solution of the common photoredox catalyst $\text{Ru}(\text{bpy})_3\text{Cl}_2$, ($\epsilon = 13\,000\text{ cm}^{-1}\text{ M}^{-1}$) was found to decrease by over 50% with an increase in reactor diameter from 0.5 mm to 1.0 mm, which was mitigated by decreasing catalyst concentrations to improve irradiation of the mixture.⁴⁸ Uniform irradiation, as provided by narrow diameter and high surface-area-to-volume flow reactors, can lessen catalyst and photo-initiator absorption concerns, while providing an avenue for increased scalability, as dictated by the amount of reaction mixture at the reactor source (Figure 3).

Other important advantages in flow reactor systems stem from the high surface area-to-volume ratio of the reactor itself, facilitating fast reaction times, efficient heat and mass transfer, reduction of batch-to-batch variations, improved safety, and fast mixing.⁴⁹ As propagation in CRP reactions is thermally controlled while the reactions themselves are exothermic, the isothermal nature of flow systems inherently leads to improved reaction consistency. Furthermore, the mixing behavior in flow systems is typically uniform in comparison to the convective mixing of batch reactors, which is largely driven by mechanical agitation and results in heterogeneous solution movement and nonuniform reaction component distributions.^{50,51} The characteristics of mixing in a flow reactor are directly dependent on the diameter of the reactor and can be described by a calculation of Reynold's number, shown by eq 2.

$$Re = \frac{uL}{\nu} \quad (2)$$

and which relates the flow rate (u) and reactor diameter (L) to the kinematic viscosity (ν) of the solution. When Re is less than 1, a laminar flow regime is accessed and viscous forces dominate over inertial forces, making solution mixing dependent on diffusion and preventing the formation of concentration gradients within the reactor, which can result in accessing ideal plug-flow behavior at small reactor diameters. In the context of CRPs, which are reliant on uniform activation to produce well-defined polymers, homogeneous mixing and distribution of the reaction components is important.

Perhaps one drawback to an increased surface-area-to-volume ratio of the flow reactor is the increased presence of wall shear, causing non-uniform polymer chain elongation along the reactor wall (Figure 4). In study of this effect using thermally mediated ATRP, shear rate was found to increase with increasing reactor lengths at constant residence times and increasing residence times using constant reactor lengths.⁵² Increased polymer elongations results in wider residence time distributions,⁵³ and in CRPs could result in a rise in an increase in \bar{D} and loss of control over MW if not mitigated.

The effect of shear on residence time distributions highlights the requirement for additional reactor and reaction considerations when performing a polymerization in a flow reactor system. Besides consideration of reaction stoichiometry, reaction times, and polymer scope, as is typical of any batch reactor system, the added flow reactor component requires additional attention to the effects of solution viscosity, flow regimes, and mixing behavior on polymerization. As the polymer chain length increases during the course of polymerization, all the above parameters will change, introducing additional complexity into comprehensive reaction engineering using photo-CRPs in flow.

2.2. Reactor Design and Development

In practice, there are nearly infinite variations of flow reactors employed for small molecule and macromolecular synthesis in both academic research laboratories and on the industrial scale; however, in the studies discussed in this perspective, there are two principal types of photo-flow reactors employed: glass chip microflow reactors and continuous-flow tubular millireactors.⁵⁴ The use of glass as a reactor material can be advantageous in terms of low oxygen permeability and high chemical compatibility, but also does not readily allow for customization. The second class of reactors, continuous flow tubular millireactors, also typically with larger diameters and volumes, facilitate reaction scalability while also giving potential for placement of inlets and outlets at any point in the reactor.⁵⁵ The wide possibilities for reactor configurations gives additional avenues for producing tailored materials using this approach. Commercially available tubing materials, typically made from inert perfluorinated polymeric materials, exhibit an expansive range of optical characteristics, chemical compatibility, and oxygen permeability and can be selected based on the polymerization conditions employed.

Furthermore, straightforward reactor configuration design can be exploited to synthesize complex polymer architectures, including block copolymers. For example, in this Perspective we highlight two principal methods for block copolymer synthesis. These include chain-extension, where an isolated polymer is reintroduced to the flow reactor under polymerization conditions to grow a new polymer domain. Also, use of multi-step

continuous reactors has been reported, which perform photo-CRP to high monomer conversions for formation of the first polymer block, followed by addition of a second monomer to form block copolymers with a slight gradient. An additional avenue toward customized reactor design lies in the choice of light source. Diverse light sources have been employed in photo-CRPs, with overlap of light source emission and photoactive species absorption being a key consideration. As such, design of current flow reactor systems primarily encompasses use of commercially available LEDs, fluorescent lamps, or mercury lamps that emit wavelengths of light across the UV and visible regimes.

In a typical photo-CRP performed in flow reactors, a reaction mixture is pushed through a reactor using either a syringe or peristaltic pump. The reaction mixture can either be from one source, or multiple inlets can simultaneously introduce different components into the reactor through a mixing connection. After reaction components are introduced, the mixture is pushed through the reactor and irradiated. Ultimately the reaction is quenched, and the resulting polymer product is collected at the end of the reactor. The reaction time is solution is irradiated. Residence time is calculated as

$$\text{residence time} = \frac{\text{reactor volume}}{\text{flow rate}} \quad (3)$$

and can be readily modulated through changes in flow rate, resulting in polymers with different monomer conversions and MWs.

3. DEGENERATIVE CHAIN-TRANSFER-CONTROLLED RADICAL POLYMERIZATIONS IN FLOW

3.1. Degenerative Chain Transfer Controlled through Direct Photolysis

Photo-iniferter controlled radical polymerization (PI-CRP), relies on direct photolysis of a chain-transfer agent to mediate polymerization. These chain transfer agents, such as commonly employed sulfur compounds, can serve as initiator-transfer-agent-terminators, or “iniferters”, and can also be referred to as RAFT agents. In PI-CRP, iniferters are directly activated by irradiation, causing homolytic cleavage of the carbon–sulfur bond and beginning propagation (Figure 5A). Photo-RAFT follows a similar polymerization propagation mechanism but relies on activation by an exogenous photo-initiator to generate the active species (Figure 5B). In either case, the degenerative chain-transfer is dominated by a fast exchange equilibrium between dormant iniferter and growing polymer chain, resulting in control over polymerization. For photocontrol, the active iniferter radical can combine with a propagating polymer chain to produce a dormant chain, which is then reactivated photochemically. Use of photo-RAFT can be advantageous in that it minimizes iniferter decomposition due to high energy irradiation typically required for PI-CRP. However, recent structural modifications of iniferters have extended the absorption profiles of these molecules for PI-CRP under visible light.⁵⁶ Advantageously, in PI-CRP the lack of initiator leads to lower termination events by unreacted or excess initiator fragments, which can result in products with higher chain-end fidelity and concomitantly lower dispersities.

PI-CRP was first introduced in 1982 using batch conditions for the synthesis of poly(methyl methacrylate) (pMMA) and poly(styrene) using UV light irradiation.⁵⁷ This technique has been further expanded to include thiocarbonylthio, trithiocarbonates, and disulfides as iniferters capable of mediating PI-CRP.^{58,25,59} Depending on the structure and relative radical stability of the iniferter, a wide range of monomers with diverse functional groups can be polymerized, including methacrylates, acrylates, acrylamides, and acetates. PI-CRP has been expanded to include the synthesis of telechelic polymers,⁶⁰ hyper-branched polymers,⁶¹ multi-block copolymers,⁶² ultra-high-MW polymers,⁶³ and brush polymers.⁶⁴

The first report of a PI-CRP adapted to a flow reactor was demonstrated by Johnson and co-workers in 2015.⁶⁵ Using a trithiocarbonate iniferter, a successful continuous flow polymerization of acrylamide and acrylate monomers with dispersities ranging from 1.11 to 1.22 was achieved. Previous mechanistic analysis of PI-CRPs in batch systems suggested decreased light intensity may facilitate control over polymerization due to the effect of irradiation on increased bimolecular termination events.⁶⁶ In that regard, a comparison between reactors with disparate irradiation profiles was performed, finding a reactor with the UV light source placed at 3 cm from the reactor resulted in \mathcal{D} lowered to 1.10 from 1.23, produced using a reactor with tubing wrapped directly around the UV lamp (Table 1, entry 1). Poly(dimethylacrylamide) (pDMA) with a range of targeted MWs was synthesized, with MWs as high as $M_n = 105.8$ kDa and $\mathcal{D} = 1.22$ (Table 1, entry 2). The synthesis of pDMA was scaled to over 2.95 g of isolated material, while also reducing reaction times from 240 min in batch to 60 min in flow for comparable monomer conversions. Block copolymers were successfully synthesized from chain-extension of isolated pDMA synthesized in flow with ethylene glycol methyl ether acrylate (EGMEA), yielding pDMA-*b*-pEGMEA-*b*-pDMA with $M_n = 34.9$ kDa and $\mathcal{D} = 1.17$ (Table 2, entry 1).

Recently, visible-light-induced PI-CRP of methacrylates using a variety of trithiocarbonyl iniferters has been reported.⁶⁷ Using a continuous flow reactor under oxygen-free conditions at 90 °C, fast reaction times were observed, reaching full monomer conversions at 60 min of residence time with \mathcal{D} ranging from 1.20 to 1.30 (Table 1, entry 3). After optimization of reaction conditions, MWs up to 10 kDa of pMMA were successfully synthesized in a controlled fashion. Other methacrylate-based polymers with \mathcal{D} ranging from 1.20 to 1.40 were synthesized with well-controlled MW reaching high monomer conversions after 60 min residence time. Multi-block copolymers could also be synthesized through sequential chain-extension reactions, using MMA and EMA (ethyl methacrylate) to ultimately give pMMA-*b*-pEMA-*b*-pMMA with $M_n = 7.9$ kDa and $\mathcal{D} = 1.32$ (Table 2, entry 2). Minimizing the need for tedious purification steps, a multi-step continuous process was employed for the synthesis of diblock copolymers with a small gradient between blocks to realize pMMA-*b*-pMMA with $M_n = 5.3$ kDa and $\mathcal{D} = 1.26$ as well as a polymer with a second poly(2-hydroxyethyl methacrylate) block to produce pMMA-*b*-pHEMA of $M_n = 5.8$ kDa and $\mathcal{D} = 1.30$ (Table 2, entry 3).

The effect of irradiation conditions for PI-CRP and photo-RAFT in the synthesis of poly(methacrylates) and poly-(acrylamides) was investigated by Gardiner and co-workers using a tubular continuous flow reactor through the systematic modulation of irradiation profiles and intensities while employing conventional photo-initiators, focusing on the

ability to achieve decreased reaction times in flow.⁶⁸ Irradiation between 310 and 380 nm resulted in conversions of 75% after 30 min residence time with $D = 1.30$ in the polymerization of *N,N*-dimethylacrylamide (DMA) paired with 2-benzyl-2-(dimethylamino)-1-[4-(4-morpholinyl)phenyl]-1-butanone as photo-initiator (Table 1, entry 4), resulting in a significant decrease in reaction times from batch reactor systems paired with the added benefit of scalability. Additionally, polymerizations with no photo-initiator were performed in a PI-CRP approach, but resulted in an increase in D to above 1.70. This loss of control was attributed to continuous activation of the iniferter, resulting in decomposition and partial end-group removal and further highlights the necessity to consider irradiation conditions for each approach employed in flow.

The ability to precisely control polymer structural fidelity in photo-RAFT systems was further explored in continuous flow by Junkers and co-workers using a glass chip microreactor, focusing on the interplay of stoichiometry, thermal, and irradiation reaction conditions on the performance of this photochemically mediated polymerization.⁶⁹ An optimized photo-RAFT system using 1 equiv of 2-[(dodecylsulfanyl)-carbonothioyl]sulfanylpropanoic acid chain transfer agent to 0.25 equiv of photo-initiator benzoin, 365 nm irradiation at 30 mW/cm² and 60 °C resulted in well-defined poly(butyl acrylate) (pBA) with $M_n = 3.1$ kDa and $D = 1.18$ after 20 min residence time (Table 1, entry 5). This system was further used to synthesize block copolymers using chain-extension with methyl acrylate (MA), resulting in pBA-*b*-pMA with $M_n = 4.0$ kDa and $D = 1.30$ (Table 2, entry 4). An examination of first-order kinetic plots for reactions using several photo-initiators, as well as no initiator, revealed the interplay between the photo-RAFT and potential photo-iniferter mechanisms. The removal of the photo-initiator resulted in lower D and slower reaction rates relative to photo-RAFT systems (Table 1, entry 6). Furthermore, it was demonstrated that after initiator consumption the RAFT equilibrium can still occur, concluding that a hybrid between photo-RAFT and photo-iniferter mechanisms must be present.

3.2. Degenerative Chain Transfer through Photo-redox Catalysis

Photoredox catalysis offers opportunities in CRP approaches to improve control over photoactivation through use of a photocatalyst (PC), capable of controlling the necessary activation and deactivation of active radical species for photocontrol. To that end, photoinduced electron transfer RAFT (PET-RAFT) has recently been developed as a method to increase reaction rates while achieving a level of polymerization control characteristic of thermally mediated RAFT systems.⁵⁸ PET-RAFT relies on the photoexcitation of a ground-state PC to produce an excited state (PC*), which then performs single electron transfer (SET) to reduce the thiocarbonylthio or trithiocarbonate chain transfer agent to give an active propagating species and ${}^2\text{PC}^{*+}$ paired with the anion of the chain transfer agent. This radical can either initiate polymerization and the RAFT equilibrium or be deactivated by the oxidized ${}^2\text{PC}^{*+}$ to regenerate PC and the dormant polymer chain, which can reenter the catalytic cycle anew (Figure 6). Advantageously, the formation of a chain transfer agent anion as an intermediate minimizes decomposition byproducts that can be formed through PI-CRP or photo-RAFT approaches.

In 2014, PET-RAFT was reported by Boyer et al. using *fac*-Ir(ppy)₃ as PC.⁷⁰ Since that time, this method has been expanded to include a diverse library of transition-metal and organic⁷¹ photoredox catalysts, in some cases capable of absorbing far-red and near-IR irradiation.⁷² PET-RAFT has also been demonstrated capable of synthesizing a wide scope of polymers and can be readily photocontrolled. Currently, the scope of PET-RAFT has been expanded to include multiblock copolymers,⁷³ stereoregular polymers,⁷⁴ polymer–protein conjugates,⁷⁵ functionalized cell surfaces,⁷⁶ and nanoparticle synthesis,⁷⁷ as well as oxygen tolerance under the appropriate conditions.⁷⁸ PET-RAFT has also been combined with other polymerization approaches in orthogonal polymerizations to produce well-defined complex architectures.⁷⁹

One challenge in CRP systems is reliance on oxygen-free conditions to prevent side reactions, termination, and catalyst quenching in photoredox systems.⁸⁰ The first report of PET-RAFT in a photo-flow system exemplified the oxygen tolerance of the reaction conditions through the polymerization of *N,N*-diethylacrylamide (DEA) in continuous flow. This system used zinc tetraphenylporphyrin (Figure 7, PC 1) as PC and 2-(((dodecylthio)carbonylthio)thio)propanoic acid (DTPA) as chain transfer agent under low-energy green light irradiation in a continuous-flow tubular reactor.⁸¹ The mechanism of oxygen tolerance is dependent on the generation of triplet–triplet annihilation of ground-state oxygen by photoactivated ZnTPP, followed by consumption of singlet oxygen by the solvent, DMSO. Applied in a photo-flow system, PET-RAFT of DEA targeting several molecular weights, was successfully performed without any previous deoxygenation of reaction components to give polymers with dispersities ranging from 1.05 to 1.12. Block like gradient copolymers, PDEA-*co*-PDMA (Table 2, entry 5), were also synthesized through addition of the second monomer feedstock directly into the reactor system after reaching <90% conversion of the first block to give a product with $M_n = 22.5$ kDa and $D = 1.06$.

Leveraging their previous work, the Boyer group reported a thorough study of the ability to modulate D in continuous flow.⁸² Control over D imparts control over the properties of the polymeric product⁸³ and is typically achieved through mixing of polymers with different D after production.⁸⁴ Using DMA as the model monomer, automated in-line D alteration was achieved through the use of gradient residence times, light intensity alterations, and modification of the wavelength of irradiation. For example, when changing the intensity of the irradiation from 0.3 to 3.8 W/m² during collection, a bimodal distribution of polymer molecular weights was obtained, compared to the typical monomodal distribution seen when one intensity is employed. Interestingly, this work also included an examination of the impact of reactor flow profiles on the results of D . Namely, an analysis of the results using different reactor volumes and the introduction of 20 different polymer fractions showed that this system deviates from the posited ideal and predicted plug flow behavior,⁸⁵ impacting the mixing of the system and the resulting D .

Most recently, PET-RAFT in photo-flow systems has been reported by Chen et al. for the polymerization of traditionally challenging semi-fluorinated acrylate monomers.⁸⁶ These monomers can be used to make materials with unique properties but are challenging to successfully polymerize to high monomer conversions in a controlled fashion. Using a visible light absorbing phenothiazine-based photoredox catalyst (Figure 7, PC 2), the

polymerization of several semifluorinated acrylates and methacrylates were studied in a batch reactor, then adapted for the synthesis of block copolymers in continuous flow using white LEDs. Notably, 4.6 g of PHFBA-*b*-PMA (Table 3, entry 6) with $M_n = 10.8$ kDa and $\mathcal{D} = 1.07$ was obtained with a decrease in reaction time by 75% in comparison to batch conditions.

4. REVERSIBLE DEACTIVATION CRPS IN FLOW

4.1. Reversible Deactivation through Direct Photolysis

One of the first studies of reversible end-capping CRPs in flow was the examination of photoinduced copper-mediated polymerization (CuMP) of methyl acrylate (MA).⁸⁷ Improving issues with activator regeneration found in thermal ATRP, Cu(II) is directly photochemically reduced to the active Cu(I) (Figure 8A). Like ATRP, CuMP relies on an equilibrium between oxidation states of copper species to reversibly end-cap the growing polymer chain with a halogen. Similar to thermally mediated ATRP, single electron transfer–living radical polymerization (SET-LRP) operates a copper mediated radical polymerization reliant on reversible activation and deactivation of alkyl halides, but also can be challenging to incorporate into flow systems due to insolubility of copper(II) complexes and salts. These two methodologies yield similar polymer products, but use different reaction conditions, such as solvent polarity and reaction temperature.⁸⁸

Using reaction conditions similar to a typical SET-LRP (or supplemental activators and reducing agents-ATRP), Junkers and co-workers investigated the comparison between a small volume (19.5 μ L) glass chip microreactor and a larger volume (11 mL) continuous tubular microreactor system irradiated by UV light under oxygen-free conditions. Using either reactor, CuMP can be performed with the ability to reach high monomer conversions after 20 min of residence time when targeting MWs less than 5 kDa and yielding polymers with \mathcal{D} ranging from 1.10 to 1.30. To confirm the ability to maintain the “living-ness” of the CRP, the chain-end group fidelity of the system was analyzed using electrospray ionization mass spectrometry through an analysis of termination products at low polymer MWs. Block copolymers were also synthesized through chain-extension. An isolated PMA macroinitiator with $M_n = 3.1$ kDa and $\mathcal{D} = 1.10$ synthesized in the tubular reactor was reintroduced to polymerization in the tubular reactor with butyl acrylate (BA) as monomer, resulting in pMA-*b*-pBA with $M_n = 5.0$ kDa and $\mathcal{D} = 1.16$ (Table 2, entry 7).

Using a similar CuMP approach, star polymers with four PMA “arms” were synthesized in continuous flow.⁸⁹ After initial optimization in batch reactors, the study of star polymer synthesis using a core-first approach was performed, focusing on the effect of Cu loading and reaction loading on the formation of star–star coupling termination products. Finding that a diluted system with reactions stopped between 50 and 70% monomer conversion produced the least amount of coupling reactions, with dispersities remaining low at 1.11 for 53% monomer conversion.

Cobalt-mediated radical polymerization (CMRP) has been employed for the polymerization of vinyl acetate in both milli- and microflow reactors.⁹⁰ CMRP is operated by reversible chain-end trapping by a redox active cobalt complex, which serves as both the light

absorbing species and polymer chain-end group (Figure 8B). As a consequence of the photolabile nature of the cobalt–carbon bond, this polymerization can be either thermally or photochemically mediated. In batch conditions, UV irradiation leads to a loss of control over polymer MW and chain architecture.⁹¹ CMRP can polymerize a broad monomer scope, including vinyl monomers with unstabilized carbon-centered radicals. Junkers and co-workers investigated the performance of a glass chip milli reactor (19.5 μ L) compared to that of a tubular continuous-flow reactor (11 mL) in the polymerization of vinyl acetate (Table 3, entries 1 and 2) using Co(acac)₂ as catalyst (see Figure 10, catalyst 3). In a comparison of thermally driven CMRP and UV supported CMRP at the same temperatures, reaction rates were significantly increased with UV irradiation without loss of polymerization control, reaching 53% monomer conversion after 2 h of residence time compared to 7% conversion with only thermal activation. Using the microreactor, this system was utilized as a tool for screening copolymerizations of vinyl acetate and 1-octene to study relative comonomer reactivity ratios (Table 2, entry 8).

4.2. Reversible Deactivation through Photoredox Catalysis

Another reversible deactivation approach is photo-induced ATRP, which can be mediated by both metal and organic photoredox catalysts. The catalytic cycle can proceed either through reductive or oxidative quenching pathways. Photoredox catalysts such as Ru(bpy)₃Cl₂,⁹² Eosin Y,^{93,94} and other photo-initiators⁹⁵ can mediate ATRP through a reductive quenching pathway. However, these catalysts are not sufficiently reducing to directly activate an alkyl halide, and a supplemental electron donor is required. Furthermore, this electron donor can induce side reactions,⁹⁶ which may lead to increased \bar{D} .

The oxidative quenching pathway, which does not rely on any sacrificial electron donors, has been applied to photo-flow systems. In this approach, polymerization proceeds through a photo-redox-oxidative quenching catalytic cycle, where a ground-state PC absorbs light to reach an excited state where it can directly reduce an alkyl halide initiator through a SET event. This reduction generates an active propagating radical as well as ²PC^{•+}, forming an ion-pair with the halide anion. Control over polymerization lies in deactivation, where the active radical is “end-capped” by the halide, returning the growing polymer chain to the dormant state and catalyst to the ground state, completing the catalytic cycle (Figure 9).

An analysis of the polymerization of MMA using photo-induced ATRP mediated by *fac*-Ir(ppy)₃ (Figure 10, PC 4) under UV irradiation was performed in continuous flow, with emphasis on choice of tubing reactor materials for effective polymerization under oxygen sensitive conditions.⁹⁷ While an advantageous in terms of uniform irradiation and heat exchange, this can also allow for greater rate of oxygen permeability and subsequent quenching or side reactions. Four different fluorinated tubing materials with differing oxygen permeability and transparency characteristics were investigated, identifying oxygen permeability as an influential factor in imparting reaction control. Ethylene chlorotrifluoroethylene, known as Halar and with oxygen permeability of 25 cm³/100 in.², was found to perform significantly better in comparison to the more widely used perfluoroalkoxy alkane (PFA) tubing, with an oxygen permeability of 881 cm³/100 in.². Enhanced performance was demonstrated through a comparison of results after 220 min

residence time, producing polymers with $M_n = 5.4$ kDa and $\mathcal{D} = 1.21$ using Halar and $M_n = 3.3$ kDa and $\mathcal{D} = 1.23$ with PFA (Table 3, entries 3 and 4). Furthermore, kinetic studies revealed a less controlled increase in MW when PFA was employed with relatively higher \mathcal{D} , reaching up to 1.90. Further experiments using Halar focused on MW control and on comparison to batch reactions, demonstrating a 50% increase in reaction rate.

A metal-free variant of photoinduced ATRP is organo-catalyzed atom transfer radical polymerization (O-ATRP), which was first reported in 2014.^{98,99} Removal of the reliance on precious metal PCs allows for improved sustainability and potential expansion of the application scope, for example in electronic fields.¹⁰⁰ O-ATRP uses organic PCs capable of directly reducing an alkyl halide initiator, a property that is rare in organic compounds. Catalysts from *N,N*-diaryl dihydrophe-nazine,^{101,102} *N*-arylphenoxazine,^{103,104} *N*-arylphenothiazine,⁹⁹ polycyclic aromatic hydrocarbon,^{98,105} carbazole,¹⁰⁶ and conjugated thienothiophene¹⁰⁷ families have been developed. A central focus in the development of O-ATRP to date has centered on mechanistic elucidation^{108,109} and catalyst design.^{110–112} However, O-ATRP has also been adapted in batch systems to produce star polymers,¹¹³ hyperbranched polymers,¹¹⁴ surface-grafted polymers,¹¹⁵ and application of bio-based monomers for homopolymer synthesis.¹¹⁶

To understand the capabilities of this methodology, the importance of irradiation conditions and O-ATRP catalyst performance was examined in continuous flow conditions, comparing the catalytic performance of three established O-ATRP catalyst families (Figure 10, PCs 5–8) in the polymerization of MMA using visible light in a tubular Halar reactor (Table 3, entries 5–8).¹¹⁷ Generally, polymerization results were found to be superior in flow relative to batch conditions, showing enhanced control over polymerization at low monomer conversions, paired with high \bar{P}^* values. Using the best performing catalyst, 3,7-di(4-biphenyl)-1-naphthalene-10-phenoxazine (Figure 10, PC 8), catalyst loadings could be dramatically reduced to 0.1 mol % and MWs over 20 kDa were synthesized. The monomer scope was extended to a scope of functionalized, hydrophobic and hydrophilic methacrylates with a high degree of control over molecular weight at all monomer conversions. Finally, block copolymers pMMA-*b*-pBnMA ($M_n = 102.4$ kDa and $\mathcal{D} = 1.60$) and pMMA-*b*-pBuMA ($M_n = 75.9$ kDa and $\mathcal{D} = 1.32$) could be synthesized (Table 2, entries 9 and 10).

O-ATRP has further been applied in continuous flow in a PFA tubing reactor in the polymerization of MMA and methacrylic acid (MAA) using a phenylphenothiazine (Figure 10, PC 9) based photocatalyst under UV light irradiation.¹¹⁸ A loss of chain-end group fidelity was observed in both batch and flow conditions in the polymerization of MMA, as supported by bromine elimination observed using ESI-MS techniques and an increase in \mathcal{D} . In a comparison between the two methods, a loss of control was observed, with \mathcal{D} rising from 1.55 in batch to 2.18 in flow. The polymerization of MAA, a traditionally challenging monomer in many ATRP systems, showed a significantly decreased reaction time in flow systems.

5. SUMMARY AND OUTLOOK

Integrating photo-CRP approaches into flow systems has provided crucial information regarding necessary reactor design and materials, catalytic abilities, and accessible MW ranges as well as highlighting the overall ability to provide improved results of polymerization relative to their batch reactor counterparts. The scope of monomers that have been polymerized include methacrylates, acrylates, acrylamides, and acetates. Block copolymers with a variety of compositions have also been synthesized (Table 3) using chain-extension and inline multistep continuous approaches, already providing to non-experts an avenue to access polymers with a diverse scope of materials properties. However, further work is required as most studies of photo-CRP systems have been performed using model systems, resulting in limited diversity in demonstrated molecular weights, especially above 20 kDa. Additionally, the capabilities to synthesize complex architectures in flow reactor systems using photo-CRPs, including multiblock stars, brushes, and combs has yet to be explored.

To build upon the existing foundation and increase the potential of photo-CRPs, three key areas should be studied. First, adaptation of current approaches to more complex reactor systems with multiple reactors, inlets, outlets, and light sources will enable rapid and readily customizable polymeric materials synthesis. Second, understanding of the effects of photopolymerizations on fluid dynamics in these reactor systems should be established. Viscosity changes from MW growth are well understood in thermally mediated polymerization systems, but elucidation of the effect of these changes on catalytic behavior and chain-end group fidelity can have wide consequences for all photo-CRPs. Third, further reactor design and process engineering is required to fully utilize the potential of flow reactor systems in mechanistic elucidation and further polymerization reaction development. Real-time, in situ studies have already been employed for batch photopolymerization systems.^{66,119} Merging these spectroscopic techniques with the high throughput reaction condition screening possible with flow reactors would greatly facilitate further development of these burgeoning photo-CRP methodologies.

The potential benefits of flow reactor systems in photo-CRPs are numerous. In particular, flow chemistry offers the powerful promise to leverage the “green-ness” of these approaches through solvent reductions, waste prevention, and heightened energy efficiency.⁴³ Certainly, the current scope of work provides a strong foundation for future maturation of photo-CRP systems using flow reactors, offering potential for bridging the gap from an academic pursuit to the industrially relevant production of advanced materials to solve the problems of the modern age.

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Biographies

Bonnie Buss is a Ph.D. candidate in the chemistry department at Colorado State University in Fort Collins, Colorado. Born in Wichita, Kansas, she earned her B.S. degree in chemistry from the University of Arkansas in 2015 while performing research in glycoside catalysis. Her current research interest in the group of Dr. Garret Miyake focuses on the development of organocatalyzed atom-transfer radical polymerization for application in functional polymer design and synthesis. Furthermore, she is inspired by green chemistry and recently won a Joseph Breen Memorial Fellowship.

Garret M. Miyake earned his B.S. in chemistry from Pacific University (USA). He completed his Ph.D. studies with Eugene Chen at Colorado State University before conducting postdoctoral research with Robert Grubbs at the California Institute of Technology as a Camille and Henry Dreyfus Environmental Chemistry Postdoctoral Fellow. He started his independent career at the University of Colorado–Boulder in 2014 before returning to Colorado State University in 2017. He has been named a Sloan Research Fellow and a Cottrell Scholar and received the 2017 American Chemical Society Division of Polymer Chemistry Mark Young Scholar Award.

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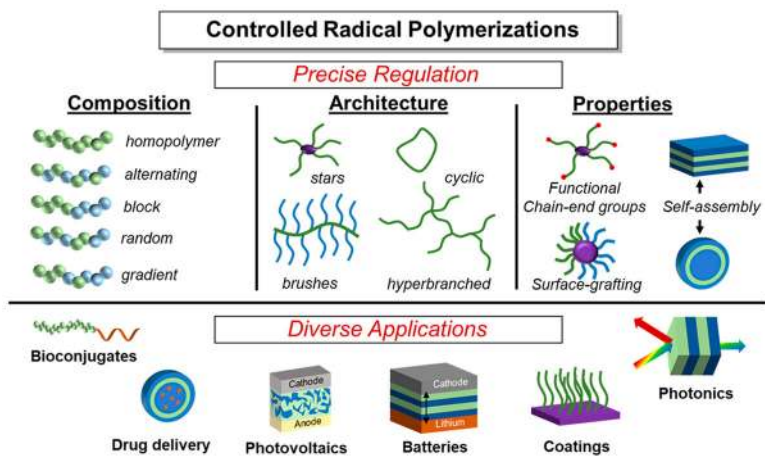


Figure 1. Overview of the capabilities of controlled radical polymerizations, highlighting their use in diverse applications such as bioconjugates,¹⁵ drug delivery,¹⁶ photovoltaics,¹⁷ batteries,¹⁸ coatings,¹⁹ and photonics.²⁰

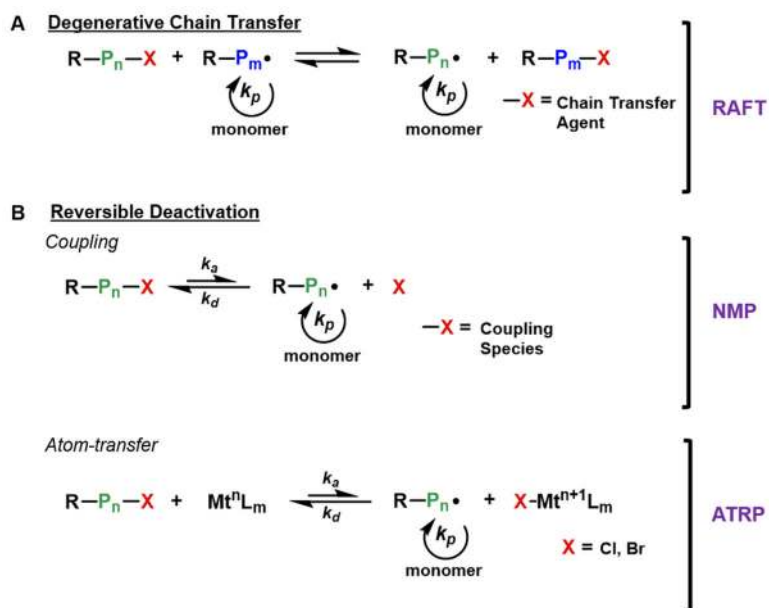


Figure 2. General reaction schemes for CRPs following degenerative chain-transfer (A) and reversible deactivation (B) mechanisms.

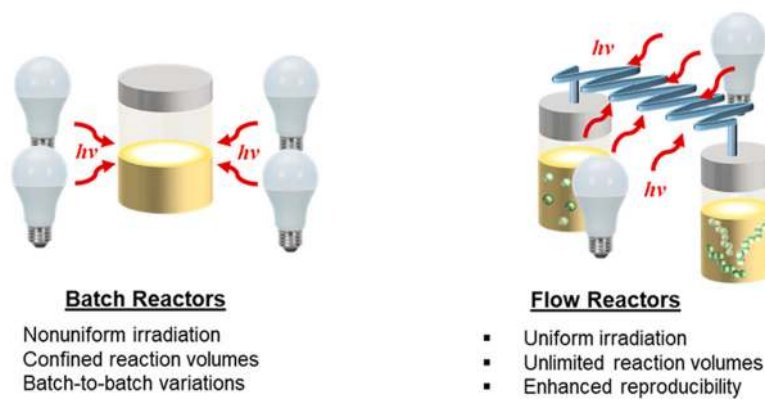


Figure 3. Schematic representations and comparisons of batch and flow reactor systems in photochemically induced polymerizations.

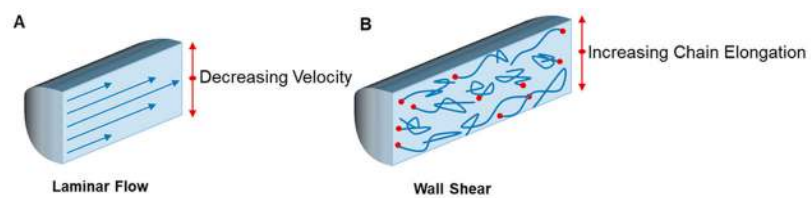


Figure 4. Graphical representation of laminar flow regime in flow reactors (A) and the effect of wall shear on polymerizations (B).

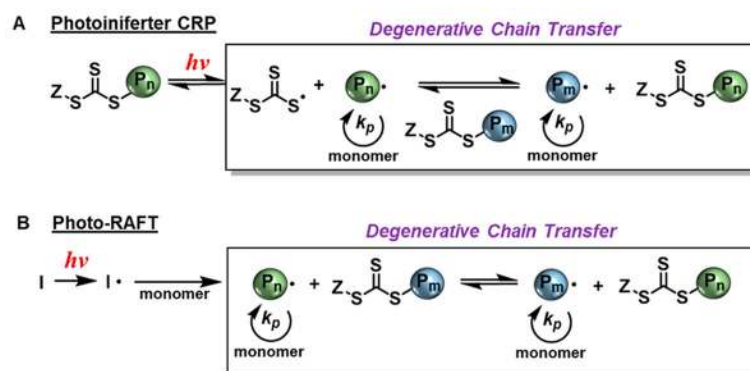


Figure 5.
General mechanisms for photo-iniferter controlled radical polymerization (A) and photo-RAFT (B).

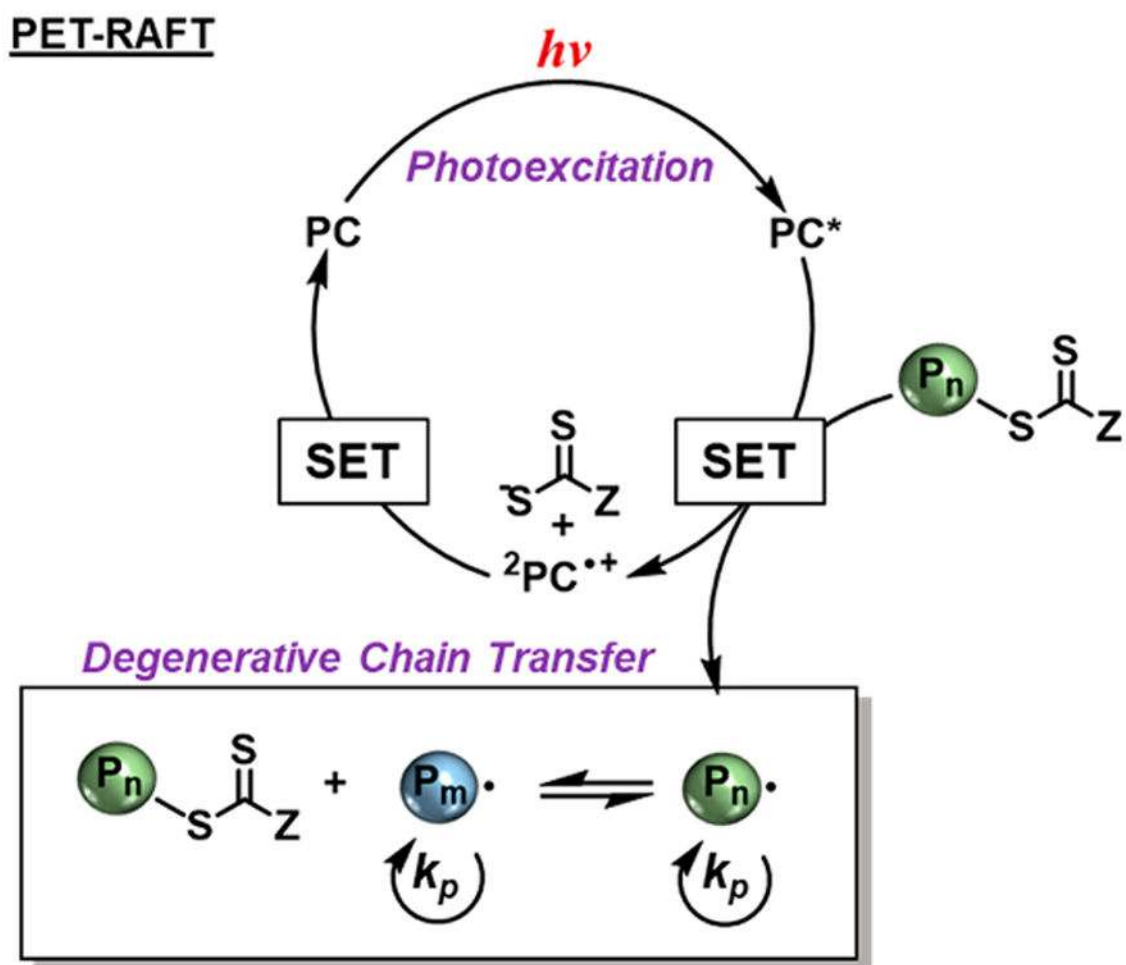


Figure 6.
General mechanism of PET-RAFT.

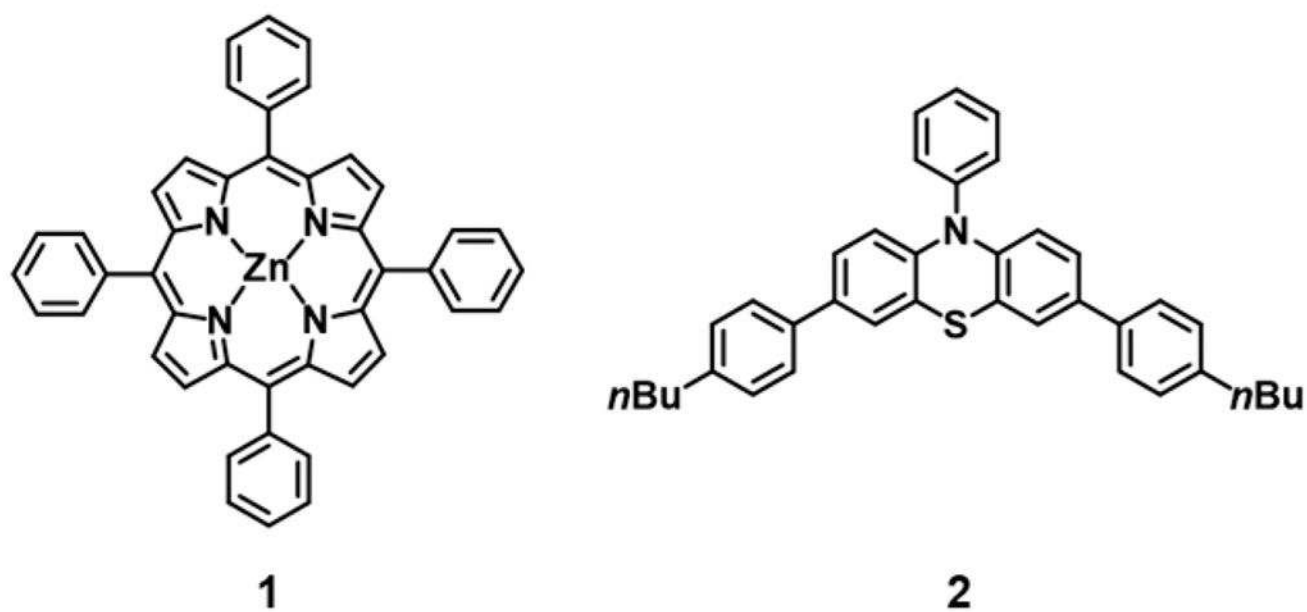


Figure 7.
Structures of photoredox catalysts used for PET-RAFT in flow reactors.

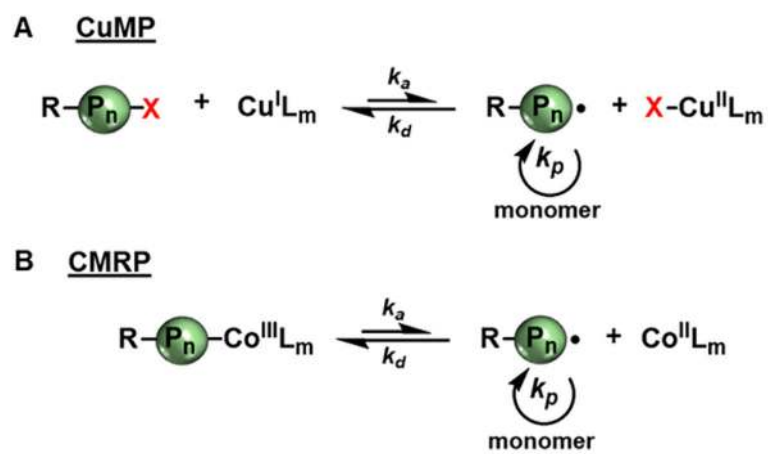


Figure 8. General mechanisms for copper-mediated polymerization (A) and cobalt-mediated radical polymerization (B).

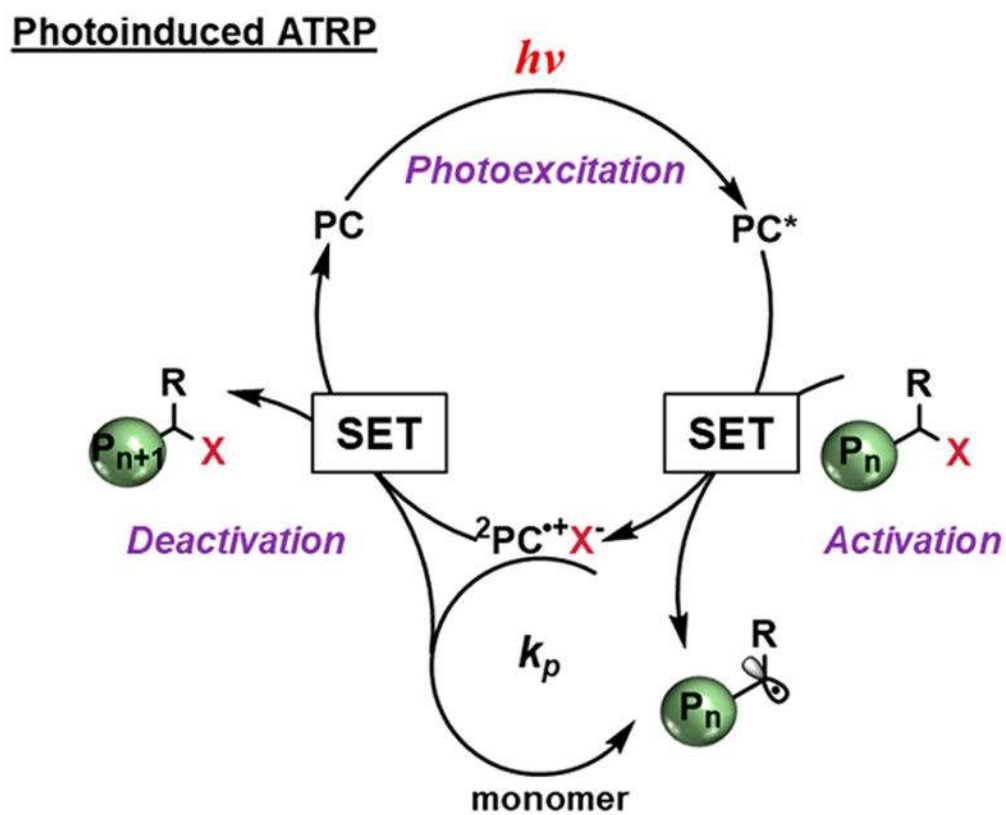


Figure 9. General mechanism for photoredox controlled ATRP proceeding through an oxidative quenching catalytic pathway.

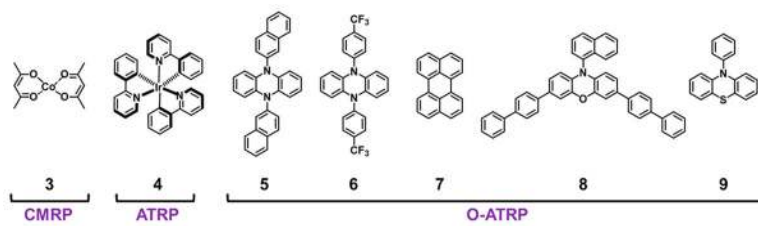


Figure 10.
Structures of catalysts employed in CMRP, ATRP, and O-ATRP in flow reactor systems.

Summary of Results of Polymerization Using Degenerative Chain Transfer Approaches Performed in Photo-flow Reactors

Table 1

entry	method	irradiation (nm)	monomer ^d	t_R^b (min)	$M_n(\text{theor})^c$ (kDa)	M_n (kDa)	D^d	ref
1	PI-CRP	352	DMA	40	22.0	24.9	1.11	65
2	PI-CRP	352	DMA	40	109.4	105.8	1.22	65
3	PI-CRP	450	MMA	60	2.5	2.8	1.25	67
4 ^e	photo-RAFT	330–380	DMA	30	7.4	13.9	1.30	68
5 ^f	photo-RAFT	365	<i>n</i> -BA	20	2.7	3.1	1.18	69
6	PI-CRP	365	<i>n</i> -BA	20	7.2	6.8	1.12	69
7	PET-RAFT	515–525	DEA	60	18.7	14.2	1.06	81
8	PET-RAFT	515–525	DMA	10.2	27.7	28.0	1.14	82
9	PET-RAFT	white LED ^g	HFBA	30	4.7	4.7	1.06	86

^aDMA = *N,N*-dimethylacrylamide, MMA = methyl methacrylate, *n*-BA = butyl acrylate, DEA = *N,N*-diethylacrylamide, HFBA = hexafluorobutyl acrylate.

^bResidence time = (reactor volume/flow rate).

^cTheoretical molecular weights are based off reaction stoichiometry provided in the main source.

^d $D = M_w/M_n$.

^eUsing 2-benzyl-2-(dimethylamino)-1-[4-(4-morpholinyl)phenyl]-1-butanone as photo-initiator.

^fUsing benzoin as photo-initiator.

^gWhite LEDs have broad emission in the visible regime.

Table 2
Block Copolymers Synthesized in Flow Using Degenerative Chain Transfer CRPs and Reversible End-Capping CRPs

entry	method	irradiation (m)	method	composition ^a	M_n (kDa)	D	ref
1	PI-CRP	352	chain extension	pDMA- <i>b</i> -pEGMEA- <i>b</i> -pDMA	34.9	1.17	65
2	PI-CRP	450	chain extension	pMMA- <i>b</i> -pEMA- <i>b</i> -pMMA	7.9	1.32	67
3	PI-CRP	450	multi-step continuous	pMMA- <i>b</i> -pHEMA	5.8	1.30	67
4	photo-RAFT	365	chain extension	pBA- <i>b</i> -pMA	4.0	1.30	69
5	PET-RAFT	515–525	multi-step continuous	PDEA- <i>co</i> -PDMA	22.5	1.06	81
6	PET-RAFT	white	chain extension	PHFBA- <i>b</i> -PMA	10.8	1.07	86
7	Cu-MRP	320–500	chain extension	pMA- <i>b</i> -pBA	5.0	1.16	87
8	CMRP	320–500	statistical copolymers	pVA- <i>b</i> -pOct	11.9	1.83	90
9	O-ATRP	white	chain-extension	pMMA- <i>b</i> -pBzMA	102.4	1.60	117
10	O-ATRP	white	chain-extension	pMMA- <i>b</i> -pBA	75.9	1.32	117

^aEGMEA = ethylene glycol methyl ether acrylate, EMA = ethyl methacrylate, HEMA = 2-hydroxyethyl methacrylate, HFPMA = hexafluorobutyl methacrylate, MA = methyl acrylate, BA = butyl acrylate, VA = vinyl acetate, Oct = 1-Octene, BzMA = benzyl methacrylate. See Table 1 for other details.

Table 3

Results of Polymerizations in Flow for Reversible Trapping/End-Capping CRPs

entry	method	irradiation (nm)	catalyst	monomer ^a	t_R (min)	M_n (theor) (kDa)	M_n (kDa)	\mathcal{P}	ref
1	CMRP	320–500	3	VA	20	5.5	6.1	1.19	90
2	CMRP	320–500	3	VA	120	24.1	17.5	1.50	90
3	ATRP	380	4	MMA	220	4.2	5.4	1.21	97
4	ATRP	380	4	MMA	220	3.1	3.3	1.23	97
5	O-ATRP	white	5	MMA	90	6.6	11.1	1.07	117
6	O-ATRP	white	6	MMA	120	4.9	6.6	1.18	117
7	O-ATRP	white	7	MMA	90	5.0	18.9	1.10	117
8	O-ATRP	white	8	MMA	120	6.5	5.8	1.19	117
9	O-ATRP	365	9	MAA	120	5.6	5.6	n/a	118
10	O-ATRP	365	9	MMA	120	5.3	4.7	2.18	118

^aMAA = methacrylic acid. See Table 1 for other details.