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Photoinduced Organocatalyzed Atom Transfer Radical Polymerization Using Continuous Flow

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Abstract

Organocatalyzed atom transfer radical polymerization (O-ATRP) has emerged as a metal-free variant of historically transition-metal reliant atom transfer radical polymerization. Strongly reducing organic photoredox catalysts have proven capable of mediating O-ATRP. To date, operation of photoinduced O-ATRP has been demonstrated in batch reactions. However, continuous flow approaches can provide efficient irradiation reaction conditions and thus enable increased polymerization performance. Herein, the adaptation of O-ATRP to a continuous flow approach has been performed with multiple visible-light absorbing photoredox catalysts. Using continuous flow conditions, improved polymerization results were achieved, consisting of narrow molecular weight distributions as low as 1.05 and quantitative initiator efficiencies. This system demonstrated success with 0.01% photocatalyst loadings and a diverse methacrylate monomer scope. Additionally, successful chain-extension polymerizations using 0.01 mol % photocatalyst loadings reveal continuous flow O-ATRP to be a robust and versatile method of polymerization.

Graphical abstract



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Introduction

Photoinduced controlled radical polymerizations (CRPs) have become powerful tools for polymer synthesis to yield polymers with targeted molecular weights (MWs), low molecular weight dispersities (), and controlled compositions with the added potential for spatial and temporal control.^{1–5} In the past two decades atom transfer radical polymerization (ATRP) has emerged as the most widely applied CRP.^{6,7} The popularity of ATRP is largely due to use of readily available reagents, robust implementation, and functional group tolerance. The ability of ATRP to preserve a functional chain-end group makes this methodology wellsuited for the synthesis of advanced architectures, such as block copolymers.⁸ In ATRP, control over the polymerization relies on strict regulation over the equilibrium between a dormant alkyl halide and an active propagating radical species in order to maintain a low radical concentration and minimize undesirable bimolecular termination reactions.⁹ Traditionally, ATRP has employed transition metal catalysts to mediate this equilibrium, which ultimately contaminates the polymer product and can restrict the application potential of the polymer, especially in electronic applications. Significant advancements have enabled the use of lower levels of transition metal catalysts^{10–13} and increased ability for polymer purification,^{14–16} while recently organocatalyzed ATRP (O-ATRP) has risen as an approach to entirely eliminate metal contamination of the polymer product.^{17–22}

A proposed mechanism for O-ATRP proceeds through photoexcitation of the ground state photoredox catalyst (PC) to generate the singlet excited state (¹PC*) and subsequent intersystem crossing to a highly reducing triplet excited state (³PC*) (Figure 1A). The ³PC* activates an alkyl halide through reduction to simultaneously form the PC radical cation halide anion ion pair (²PC*+X⁻) and the active carbon-centered radical species for polymerization propagation. The ²PC*+X⁻ species deactivates the growing polymer chain via an oxidative event, generating a halide end-capped polymer. For CRPs, control over polymerization relies on a faster rate of deactivation than rate of activation or monomer propagation. Furthermore, the irradiation of the PC plays an important role in the efficiency of PC photoexcitation and thus relative concentrations of every PC species in the polymerization reaction, which culminates in control over the polymerization. As such, we hypothesized developing O-ATRP in continuous flow would enhance irradiation efficiency and facilitate the synthesis of well-defined polymers.

In 2014, perylene¹⁷ and *N*-aryl phenothiazines¹⁸ were presented as PCs able to orchestrate O-ATRP through an oxidative quenching pathway using visible and UV irradiation, respectively. Recently, our group has revealed *N*,*N*-diaryl dihydrophenazines¹⁹ and *N*-aryl phenoxazines,²⁰ as strongly reducing visible-light-absorbing PCs efficient for O-ATRP. Mechanistic studies of O-ATRP mediated by *N*-aryl-phenothiazine catalysts highlighted the necessity for fast activation and deactivation for controlled polymerizations.²³ Further studies have shown the importance of photoinduced charge transfer states of the PC and solvent stabilization of the resulting ²PC^{•+}X⁻ ion pair in *N*,*N*-diaryldihydrophenazine catalysts for the synthesis of well-defined polymers using O-ATRP.²⁴ These studies reveal the free energy of ²PC^{•+}X⁻, which is influenced by solvent polarity, to play a key role in efficient deactivation and to achieve control over the polymerization.

As an alternative to traditional batch reactors, photomediated continuous flow reactors have materialized as an excellent approach in both small molecule^{25–28} and macromolecular^{29–31} syntheses to promote efficient and uniform irradiation conditions. According to the Beer–Lambert law, in a photomediated batch reaction the ability for photons to travel in the reaction medium decreases exponentially with increasing path length, equating to nonuniform irradiation and limiting the efficiency of the reaction. In particular, for photo-induced CRP reactions poor irradiation control leads to broad molecular weight distributions, slower reaction times, and limited scalability.^{26,33} In contrast to batch reactors, continuous flow offers a high surface-area-to-volume ratio of reactor to solution, allowing uniform irradiations, and facile scalability (Figure 1C). ^{26,28,34} Considering reaction design, reaction parameters can be easily adjusted during polymerization by modulating flow rates, irradiation intensity, and reaction stoichiometry.³⁵

To date, the scalability and irradiation efficiency of O-ATRP have been constrained by limitations inherent to batch reactor systems. Reports of continuous flow approaches have been presented for nitroxide-mediated polymerization (NMP),^{36,37} reversible addition–fragmentation chain transfer (RAFT),^{31,38} and metal-catalyzed ATRP.^{39,40} This method has been further extended to photoinduced RAFT,^{41–43} and photoinduced metal-catalyzed ATRP, ^{44,45} but photoinduced O-ATRP in continuous flow has not yet been reported. With that in mind, we hypothesized that the favorable characteristics of photomediated continuous flow systems, namely control over irradiation, would facilitate further study of the capabilities of recently developed organic PCs through heightened control over activation and deactivation, accessing enhanced results of polymerization. To that end, this work reports a study of the integration of visible-light-mediated O-ATRP into a continuous flow approach, improving and expanding the utility of the methodology while offering an energy-efficient method for producing polymers on scale.

Experimental Section

Continuous Flow Setup

A continuous flow tubular reactor system was designed from commercially available components consisting of a syringe pump, stainless steel syringe, Halar tubing, and a fluorescent tubular light bulb (see Supporting Information for full details). Halar tubing was used for the flow reactor based on studies optimizing a continuous flow reactor system using photo-induced ATRP catalyzed by *fac*-Ir(ppy)₃.⁴⁴

General Polymerization Procedure

A vial was charged with PC, brought inside a glovebox, and loaded under nonphotoactive lighting with *N*,*N*-dimethylacetamide (DMA), methyl methacrylate (MMA), and alkyl bromide initiator while stirring. Once the PC was fully dissolved, the reaction mixture was loaded into a stainless steel syringe to prevent undesired irradiation exposure during polymerization. The syringe was fitted with the first section of tubing (Figure S1), then brought outside of the glovebox, and quickly attached to the next section of tubing reactor. Once the syringe pump was started with the desired flow rate, the system was allowed to

reach steady-state conditions by loading the reactor with the reaction mixture and running for 1.5 residence times. Residence time is defined as the amount of time the polymerization solution is exposed to irradiation conditions (see Supporting Information for a detailed explanation). The polymer product was collected and quenched by placing the third section of tubing into a 20 mL scintillation vial containing deuterated chloroform with 50 ppm BHT. The tubing reactor was flushed with DMA after polymerization was complete. The system was allowed to reach steady-state temperature conditions by turning on the light for 1 h before polymerization. The temperature of the system was monitored continuously during polymerization and remained at constant 60 $^{\circ}$ C, unless otherwise noted.

Polymer Characterization

Monomer conversion was determined by ¹H NMR analysis immediately following collection by comparison of the integrations of the methyl ester monomer peak at 3.73 ppm to the corresponding methyl ester polymer peak at 3.57 ppm. The volatiles were removed from the remainder of the collected sample, and then the sample was dissolved in THF for molecular weight analysis using gel permeation chromatography (GPC) coupled to multiangle light scattering.

Results and Discussion

Synthesis of PMMA Using Visible-Light-Absorbing PCs

To examine the performance of O-ATRP using a continuous flow reactor, we investigated multiple previously reported PCs studied in a batch reactor system for the polymerization of methyl methacrylate (MMA). The PCs used in this study were selected due to absorption profiles in the visible light regime and familial diversity (Figure 1B). For a direct comparison of polymerization trends, similar reaction conditions were used to those reported in batch, including reaction stoichiometry and choice of alkyl bromide initiator. In batch conditions using broad spectrum white LEDs for irradiation for PC **1** and **2**, typically ranged from 1.10 to 1.18 and 1.03, respectively, with initiator efficiency (I^*)⁴⁶ values reaching 66% and 46%.¹⁹ For PC 3, batch conditions gave of 1.3–1.8 but low I^* (14–22%) and a lack of control over MW as polymerization proceeded.¹⁷ In the case of PC 4, in typical batch reactions of 1.25–1.17 and I^* of ~100% were reported.²⁴ A summary of key photophysical and redox properties of these PCs can be found in Table 1.

The results for polymerizations using PCs 1, 2, 3, and 4 in continuous flow all showed similar trends of enhanced polymerization performance in comparison to batch reactor conditions, as demonstrated by improved predictability in MW and lowered (Figure 2). When employing 1, ranged from 1.10 to 1.18 over the course of polymerization, reaching 49% conversion after a 2 h residence time. In the case of 2, ranged from 1.05 to 1.14 while reaching 64% conversion after a 1.5 h residence time. Using PC 3 showed distinct improvement over batch reactions and was able to produce PMMA with a as low as 1.10. Although inferior to the *N*,*N*-diaryl dihydrophenazine and *N*-aryl phenoxazine catalysts, 3 still exhibited a linear growth in MW, a marked change in comparison to reported batch reaction results. The performance of PC 4 in continuous flow is highlighted by near 100% *I**, a predictable increase in MW, and 1.20 (Figure 2D).

Most notably, for *N*,*N*-diaryldihydrophenazine catalysts **1** and **2**, at low monomer conversion continuous flow demonstrated superior control in comparison to batch reactors, with experimentally measured MWs near theoretically predicted MWs resulting in nearly quantitative *I**. These results can be explained through analysis of the proposed mechanism of O-ATRP in the context of continuous flow. In the O-ATRP mechanism, the rate of deactivation must be higher than activation in order to maintain control over the propagating radical species.²³ This phenomenon is facilitated by the concentration, availability, and oxidation potential of the ²PC^{•+}X⁻ deactivator species. Low concentrations of ²PC^{•+}X⁻ hinder effective deactivation, limiting control over propagation via reversible end-capping of the active polymer chain. However, in a photoflow reactor a higher surface-to-volume ratio allows for more efficient irradiation and PC photo-excitation, subsequent activation, and therefore an indirect increase in deactivator concentrations. These conditions allow for control over propagation and result in enhanced control over MW at low polymer conversions for **1** and **2**.

In total, these results demonstrate that a continuous flow approach can provide significant improvements in polymerization metrics using a variety of PCs, especially in regards to results at low monomer conversions. In a continuous-flow system, the maximum I^* was reached at lower monomer conversions than in batch. This can be attributed to uniform irradiation resulting in higher concentrations of ³PC* and subsequent fast activation of the alkyl halide initiator. Because of low and consistently high I^* values near 100%, **4** was chosen as PC for additional study of continuous flow techniques using O-ATRP.

The effect of relative solvent volume on results of polymerization was explored using PC 4 (Table S7). Polymerization results did not vary significantly with varying reaction solution concentrations. The conditions tested included 1:1, 2:3, 1:2, and 1:3 ratios of MMA to DMA by volume. For all conditions, remained relatively low, typically below 1.25, and MW predictability was conserved with I^* near 100%. The most concentrated solution tested, a 1:1 ratio of MMA:DMA, exhibited the fastest reaction rate; however, remarkably increased viscosity upon reaching conversions above 70% posed issues with the continuous flow system. For fast reaction times and lower viscosities, a ratio of 2:3 MMA:DMA by volume was chosen for subsequent polymerizations.

As photoflow reactors facilitate efficient and homogeneous irradiation of the reaction solution due to increased surface-to-volume area of the reactor, ³² we hypothesized sufficient concentrations of excited state ³PC* for successful polymerizations could be achieved using decreased PC loadings. To test this hypothesis, O-ATRP of MMA was performed using varying concentrations of **4**. For mol % levels spanning 0.1%–0.01%, all loadings were well-controlled above 40% conversion (Table 2, runs 1-4). However, for 0.04–0.01% (runs 2–4), early stages of polymerization (<40% conversion) showed slightly higher MW polymers in comparison to theoretical MWs (Figure S4). This is likely a consequence of an insufficient concentration of critical deactivating ²PC*⁺X⁻ species at low monomer conversions. Lowering the PC loading to 0.005% (Table 2, run 5) resulted in a loss of control over MW growth. A control experiment with no PC in the system resulted in low monomer conversions and 1.85 (Table S4). To continue a comparison of general trends in batch

reaction systems and continuous flow, PC loadings of 0.1% were employed in further studies.

To validate that this system can be used to synthesize polymers with targeted MWs with a high level of control, the O-ATRP of MMA was performed with the goal of synthesizing PMMA with a range of MWs (Figure 3). These data showed well-controlled polymerizations through conversions above 80%, first-order kinetic behavior, nearly constant and relatively low $\$, and a linear increase in MW paired with quantitative I^* .

To synthesize PMMA with tunable MWs in continuous flow, concentrations of either monomer or initiator were adjusted while maintaining a constant [4] (Table 3). Through altering the stoichiometry, predictable MWs and relatively low were obtained for low-MW polymers. However, when targeting high monomer-to-initiator loadings, increased above 1.5 and I^* exceeded 100%, showing a loss of control over the polymerization. This loss of control in continuous flow at high MW may be attributed to increased solution viscosities provided by high-MW polymers, which can cause increased shear rates within the reactor and poor diffusional mixing of the solution.⁴⁷ As such, even at uniform flow rates polymer chains become elongated and move through the reactor at varying rates, leading to broadened residence time distributions that likely contribute to a higher .³⁵

Application of O-ATRP for the Polymerization of Other Monomers

The expansion of this polymerization to a diverse group of methacrylate monomers using O-ATRP in continuous flow was investigated (Table 4). Polymerizations of benzyl methacrylate and ethyl methacrylate produced polymers with 's of 1.38 and 1.26, respectively, and linear increases in MW with monomer conversion (Table 4, runs 1 and 2). Synthesis of poly(2-ethylhexyl methacrylate) resulted in polymer with 98% *I** and of 1.40 (Table 4, run 3). The polymerizations of lauryl methacrylate and isodecyl methacrylate were well-controlled until reaching 60% and 66% conversion, respectively, although 's increased at higher monomer conversions (Table 3, runs 4 and 5). Applying this polymerization approach to diethylene glycol methyl ether methacrylate showed control over MW throughout polymerization with a polymer with of 1.14 at 66% conversion (Table 4, run 7). Highlighting the robustness of O-ATRP in continuous flow, no additional optimization was necessary in order to accomplish a well-controlled polymerization of methacrylate monomers possessing varying functionalities.

Chain Extension of PMMA Synthesized in Continuous Flow

To further demonstrate the controlled nature of O-ATRP in a continuous flow system, chainend group fidelity was validated by chain extension from a PMMA macroinitiator synthesized on large scale in continuous flow. The large-scale synthesis of the PMMA macroinitiator was carried out to obtain 3.3 g of purified PMMA macroinitiator in a 73% yield (see Supporting Information: Macroinitiator Synthesis and Chain-Extension Experiments). Low PC loadings were implemented for all steps (0.01 mol % of 4), and chain extensions were performed with isobutyl methacrylate or benzyl methacrylate. Macroinitiator chain-end group fidelity was confirmed through successful chain extension of

macroinitiator to block copolymer, as shown by baseline-resolved shifts in GPC traces from the PMMA macroinitiator to higher molecular weight block copolymers (Figure 4B).

Conclusions

Photoinduced O-ATRP performed in continuous flow has been established as a robust and efficient method of polymerization. For each photoredox catalyst tested, results show good control over all metrics of polymerization to produce polymers with relatively low and high MW predictability. Control over the course of the polymerization was maintained when catalyst loadings were lowered to 0.01 mol %. Further, this technique has been successfully applied to the polymerization of a diverse scope of methacrylate monomers with no further optimization required and provides the capability for the scalable synthesis of well-defined block copolymers. The success of O-ATRP in this system is enhanced by the efficient irradiation characteristics offered by continuous flow.

Supplementary Material

Refer to Web version on PubMed Central for supplementary material.

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Figure 1.

(A) Proposed mechanism for O-ATRP proceeding through an oxidative quenching pathway.(B) Visible-light-absorbing PCs used in this study include *N*,*N*-diaryl phenazines (1 and 2), perylene (3), and *N*-aryl phenoxazines (4). (C) Photomediated flow reactors offer significant advantages to batch systems.



Figure 2.

Plots of M_n (black diamonds) and (red triangles) with respect to monomer conversion during the polymerization of MMA catalyzed by **1** (A), **2** (B), **3** (C), or **4** (D) performed in continuous flow at steady-state conditions and under different residence times. Shown is the theoretical evolution of M_n (dashed line) with respect to monomer conversion. Conditions for all plots: [1000]:[10]:[1] of [MMA]:[initiator]:[PC]; 3.73 mM PC; initiators are ethyl α bromophenylacetate (EBP) when using **1–3** and diethyl 2-bromo-2-methylmalonate (DBMM) when using **4**; 2:3 MMA to DMA by volume; 160 cm of tubing reactor, irradiated by 3000 K fluorescent light. See Supporting Information for flow rates and residence times used.



Figure 3.

Results of the polymerization of MMA catalyzed by 4 performed in continuous flow at steady-state conditions and under different residence times: (A) first-order kinetic plot; (B) plot of the molecular weight (\blacklozenge) in comparison to theoretical molecular weight (dashed line) with respect to monomer conversion and dispersity (\blacktriangle); (C) GPC traces of the polymers corresponding to points shown in (A) and (B), color coded. Conditions used are [MMA]:[DBMM]:[4] = [1000]:[10]:[1]; 3.73 mM of PC, 2:3 MMA:DMA by volume, irradiated by 3000 K fluorescent lamp. See Supporting Information for flow rates and residence time used.



Figure 4.

(A) Chain extension using O-ATRP from a PMMA macroinitiator extended with BzMA (purple) and iBuMA (red). (B) Gel permeation chromatography traces of the polymers are shown with corresponding color schemes.

Table 1
Summary of Redox and Photophysical Properties for PCs 1–4 ^a

PC	$E^{\bullet}(^{2}\mathrm{PC}^{*+}/^{3}\mathrm{PC}^{*})^{a}$	$E^{\bullet}(^{2}\mathrm{PC}^{\bullet+}/^{1}\mathrm{PC})^{a}$	$\lambda_{\max}(nm)$	$e_{max} (M^{-1} cm^{-1})$
1^{b}	-1.80	0.29	370	4700
2^b	-1.71	0.19	340	6300
3 ^c	-0.70	0.98	436	38500
$_4b$	-1.80	0.65	388	26635

^aRedox potentials are in V vs SCE.

 b Values are from previous O-ATRP reports and were determined experimentally. 19,20

^CDetermined computationally as described in ref 19.

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Table 2

run. no.	[PC 4] (mol %)	conv (%) b	$M_{ m n}~({ m kDa})^{c}$	$(M_{\rm w}/M_{\rm n})^{c}$	theor $M_{ m n}~({ m kDa})^d$	$I^{*}(\%)^{\ell}$
-	0.1	61	6.4	1.23	6.11	95
2	0.04	69	6.9	1.22	6.86	100
ю	0.02	68	6.2	1.26	6.82	110
4	0.01	71	7.9	1.27	7.09	06
S	0.005	72	6.7	1.60	7.25	108

 a [MMA]:[DBMM]:[4] = [1000:[10]:[X]; 2:3 of MMA to DMA by volume and 160 cm tubing reactor irradiated by 3000 K fluorescent lamp. Results shown were achieved with a 90 min residence time at a flow rate of 8.11 μ /min.

 $b_{\rm Determined by } {}^{\rm 1}_{\rm H}$ NMR.

 $^{\mathcal{C}}$ Measured using GPC.

 $d_{Calculated}^{d}$ by (Conv × [Mon]/[Init] × $M_{W,Mon}$)/1000.

 e^{t} Initiator efficiency (*I**) calculated by (Theor $M_{\rm h}/{\rm Calcd}~M_{\rm h}) \times 100.$

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Table 3

Results of O-ATRP of MMA in Continuous Flow for the Synthesis of PMMA with Tunable Molecular Weights^a

$_{w}$ (kDa) M_{n} (kDa) (M_{n}) (M_{n}) Theo. M_{n} (kDa) I^{*} (%)	6.3 5.4 1.17 3.6 68	3.7 3.0 1.24 3.2 108	9.0 7.2 1.25 6.9 95	25.2 19.3 1.30 15.3 79	43.0 24.4 1.77 30.4 125	2.2 1.8 1.18 1.3 69	4.3 3.8 1.13 3.1 81	18.9 13.6 1.39 12.7 94	21.3 15.4 1.38 15.2 98	29.9 20.5 1.46 23.6 115	
	73	48	69	76	61	50	61	85	76	79	74
[MMA]:[DBMM]:[4] Co	[1000]:[20]:[1]	[1000]:[15]:[1]	[1000]:[10]:[1]	[1000]:[5]:[1]	[1000]:[2]:[1]	[250]:[10]:[1]	[500]:[10]:[1]	[1500]:[10]:[1]	[2000]:[10]:[1]	[3000]:[10]:[1]	[4000]:[10]:[1]
un no.	1	2	33	4	5	9	٢	8	6	10	11

"[MMA]:[DBMM]:[4] = [X]:[Y]:[1]: 3.73 mM of 4, with 2:3 of MMA to DMA by volume and 160 cm tubing reactor irradiated by 3000 K fluorescent tubular lamp. Results were achieved using a 120 min residence time at a flow rate of 5.41 µL/min.

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 a [Monomer]:[DBMM]:[PC 4] = [1000]:[10]:[1] 3.73 mM of 4, with 2:3 of MMA to DMA by volume and 160 cm tubing reactor irradiated by 3000 K fluorescent lamp.