

# Polarization-selective magneto-optical modulation

Banoj Kumar Nayak  ; Eyal Buks  



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Banoj Kumar Nayak and Eyal Buks

## AFFILIATIONS

Andrew and Erna Viterbi Department of Electrical Engineering, Technion, Haifa 32000, Israel

<sup>a)</sup>Author to whom correspondence should be addressed: eyal@technion.ac.il

## ABSTRACT

We study magneto-optical coupling in a ferrimagnetic sphere resonator made of yttrium iron garnet. We find that the resonator can be operated in the telecom band as a polarization-selective optical modulator. The input state of polarization (SOP) contributing to the Stokes sideband is orthogonal to the one contributing to the anti-Stokes sideband. In the region of single sideband modulation, the SOP of both sidebands is nearly orthogonal to the SOP of the incident light. Intermodulation gain can be employed in the nonlinear regime for amplification.

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## I. INTRODUCTION

Information is commonly transmitted by modulating a monochromatic carrier wave. The method of single sideband modulation (SSM) allows reducing both transmission power and bandwidth, in comparison with simpler methods such as amplitude, frequency, and phase modulation.<sup>1</sup> In the radio frequency band, SSM can be implemented using electronic circuits, however, SSM implementation in the optical band is challenging, since it requires that different out of phase modulation methods are simultaneously applied.<sup>2,3</sup>

Magneto-optical (MO) coupling<sup>4–10</sup> in ferrimagnetic sphere resonators (FSRs) can be used for optical modulation of signals in the microwave band. Such a modulation has been demonstrated before<sup>11–21</sup> by exciting individual whispering gallery FSR optical modes using either a tapered optical fiber or a prism. Here, we employed a modified experimental setup, in which light in the telecom band is transmitted through the FSR bulk. Driving the FSR near its resonance generates sidebands in the transmitted optical spectrum. We find that the FSR can be used as a polarization-selective SSM. The polarization selectivity is attributed to angular momentum conservation in photon-magnon scattering.<sup>22–27</sup> We demonstrate that intermodulation gain can be exploited in the nonlinear regime for amplification.

## II. EXPERIMENTAL SETUP

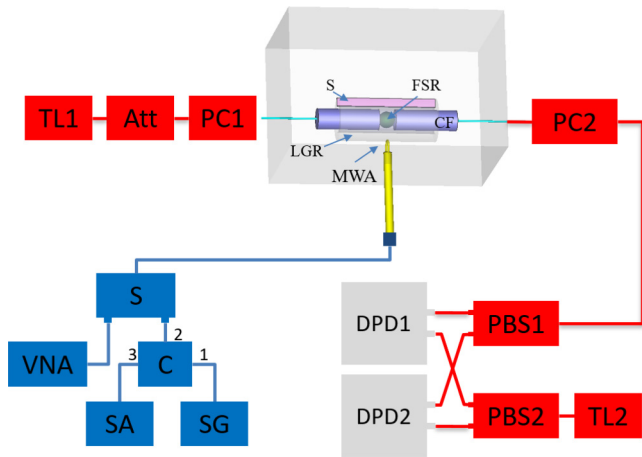
The experimental setup is schematically shown in Fig. 1. Optical components and fibers are red colored, whereas blue color

is used to label microwave (MW) components and coaxial cables. A MW cavity made of a loop gap resonator (LGR) allows achieving a relatively large coupling between magnons and MW photons.<sup>29–32</sup> The LGR is fabricated from a hollow concentric aluminum tube. A sapphire (S) strip of 260 μm thickness is inserted into the gap in order to increase its capacitance, which in turn reduces the frequency  $f_c$  of the LGR fundamental mode. An FSR made of yttrium iron garnet (YIG) having a radius of  $R_s = 125 \mu\text{m}$  is held by two ceramic ferrules (CFs) inside the LGR. The two CFs, which are held by a concentric sleeve, provide transverse alignment for both input and output single mode optical fibers. Fiber vertical alignment is performed by maximizing optical transmission.

The angular frequency of the Kittel mode  $\omega_m$  is approximately given by  $\omega_m = \mu_0 \gamma_e H_s$ , where  $H_s$  is the static magnetic field,  $\mu_0$  is the free space permeability, and  $\gamma_e/2\pi = 28 \text{ GHz T}^{-1}$  is the gyromagnetic ratio.<sup>10</sup> The applied static magnetic field  $\mathbf{H}_s$  is controlled by adjusting the relative position of a magnetized neodymium using a motorized stage. The static magnetic field is normal to the light propagation direction  $\mathbf{k}$ , and the magnetic field of MW drive is nearly parallel to  $\mathbf{k}$ . The LGR-FSR coupled system is encapsulated inside a metallic rectangular shield made of aluminum. The LGR is weakly coupled to a microwave loop antenna (MWA).

The plot in Fig. 2 exhibits a vector network analyzer (VNA) reflectivity measurement of the LGR-FSR coupled system. The static applied magnetic field  $H_s$  in this measurement is varied near the value corresponding to avoided-crossing between the FSR and LGR resonances.

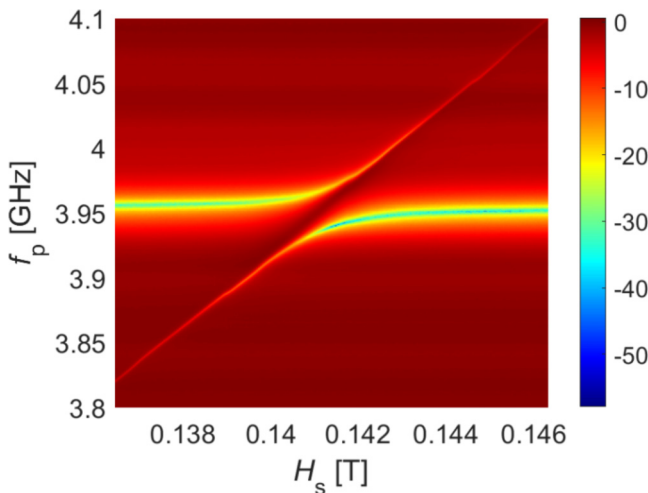
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**FIG. 1.** Experimental setup. Optical fibers are installed on both sides of the FSR for transmission of light through the sphere. Optical components [TL (tunable laser), Att (optical attenuator), PC (polarization controller), and PBS (polarization beam splitter)] and fibers are red colored, and MW components [MWA (microwave loop antenna), S (splitter), C (circulator), VNA (vector network analyzer), SA (spectrum analyzer), and SG (signal generator)] and coaxial cables are blue colored. TL2 together with two PBSs (labeled as PBS1 and PBS2) and two differential photodetectors (labeled as DPD1 and DPD2) operate as a polarization-selective optical spectrum analyzer.<sup>28</sup> A power amplifier is serially connected to the SG. The MWA is weakly coupled to the FSR-LGR system.

### III. OPTICAL SIDEBANDS

Optical sidebands are observed in the transmission spectrum when the driving microwave frequency  $\omega_p/(2\pi)$  is tuned close to the FSR resonance at  $\omega_m/(2\pi)$ . The plot shown in Fig. 3 exhibits

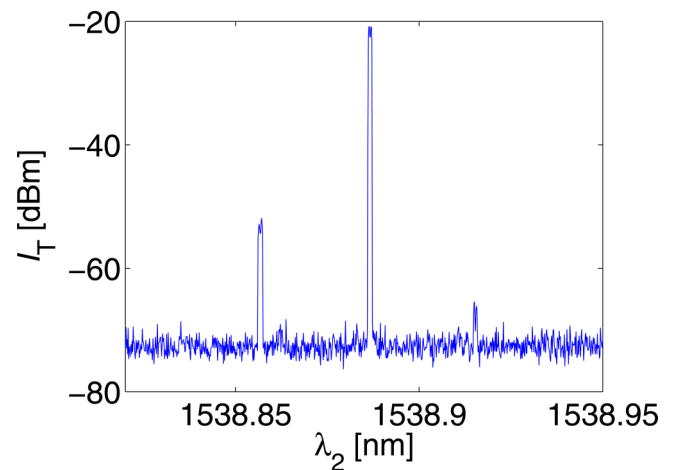


**FIG. 2.** VNA reflectivity in dB units as a function of magnetic field  $H_s$  at an applied microwave power of  $-30$  dBm.

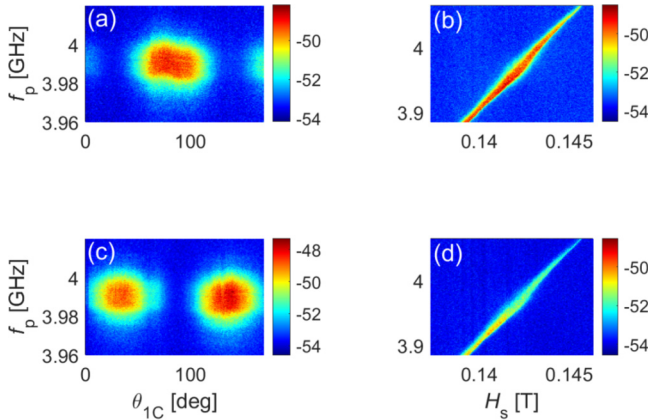
the measured total optical intensity  $I_T = I_{DPD1} + I_{DPD2}$  as a function of the wavelength  $\lambda_2$  of TL2, where  $I_{DPD1}$  and  $I_{DPD2}$  are the intensities measured by the two differential photodetectors (labeled as DPD1 and DPD2 in Fig. 1). The sideband wavelengths are given by  $\lambda_L \pm \lambda_{SB}$ , where  $\lambda_{SB} \simeq \lambda_L^2 \omega_p / (2\pi c)$ , and  $\lambda_L$  is the TL1 wavelength, which is related to the TL1 frequency  $\omega_L / (2\pi)$  by  $\omega_L = 2\pi c / \lambda_L$ , where  $c$  is the speed of light in vacuum. The value of  $\lambda_{SB} = 30.0$  pm is obtained for TL1 wavelength of  $\lambda_L = 1539$  nm and FSR driving frequency of  $\omega_p / (2\pi) = 3.79$  GHz.

Both motorized polarization controllers (labeled as PC1 and PC2 in Fig. 1) have three optomechanical components (paddles), which act as either quarter or half wave plates. The paddles' angles of PC1 (PC2) are denoted by  $\theta_{1A}$ ,  $\theta_{1B}$ , and  $\theta_{1C}$  ( $\theta_{2A}$ ,  $\theta_{2B}$ , and  $\theta_{2C}$ ). The incident light state of polarization (SOP) can be manipulated using PC1. We observe that the intensity of lower wavelength  $\lambda_L - \lambda_{SB}$  anti-Stokes sideband and higher wavelength  $\lambda_L + \lambda_{SB}$  Stokes sideband depends on the input SOP. SSM in the transmission spectrum, with either single anti-Stokes sideband or single Stokes sideband, can be obtained by adjusting PC1. The plot shown in Fig. 4(a) exhibits the measured anti-Stokes sideband intensity as a function of microwave driving frequency  $f_p = \omega_p / (2\pi)$  and PC1 angle  $\theta_{1C}$  near the avoided-crossing region. The plot shown in Fig. 4(c) exhibits simultaneously measured Stokes sideband intensity in the same region. We clearly observe appreciable anti-Stokes and Stokes intensity in Figs. 4(a) and 4(c), respectively, when driving frequency  $\omega_p / (2\pi)$  becomes close to FSR resonance  $\omega_m / (2\pi)$ . However, they are asymmetric. For a certain range of PC1 position, SSM is obtained, i.e., only one sideband, either anti-Stokes or Stokes, is observed. Contrary to other experimental setups, in which the FSR is optically coupled by either a tapered optical fiber or a prism, for our setup, for which the measured optical transmission only weakly depends on the input wavelength  $\lambda_L$ , SSM can be obtained in a wide range of  $\lambda_L$ .

19 September 2023 06:11:03



**FIG. 3.** The transmitted optical spectrum. For this measurement, the TL1 is set at an optical power of 31 mW and a wavelength  $\lambda_L$  of 1538.887 nm, and the driving microwave is set at a frequency  $\omega_p / (2\pi)$  of 3.79 GHz and a power of  $P_p$  of 20 dBm.

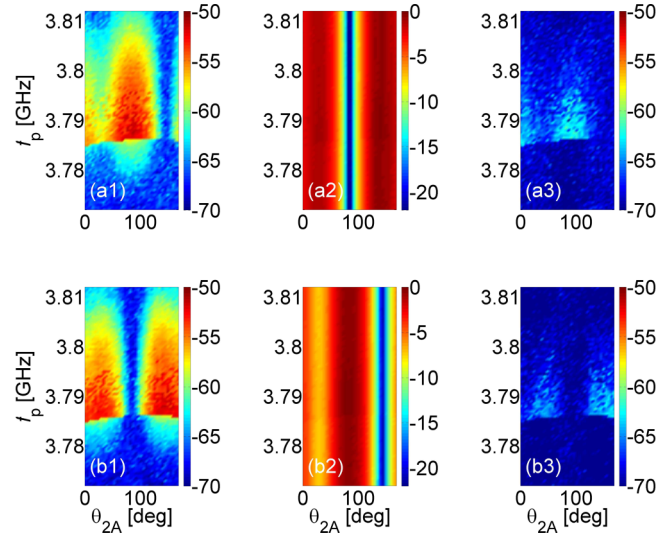


**FIG. 4.** Sidebands in dBm units. (a) Anti-Stokes intensity as a function of PC1 angle  $\theta_{1C}$ . (b) Anti-Stokes intensity as a function of magnetic field  $H_s$ . (c) Stokes intensity as a function of  $\theta_{1C}$ . (d) Stokes intensity as a function of  $H_s$ . The magnetic field  $H_s$  in (a) and (c) is tuned near the avoided-crossing regime. TL1 is set at an optical power of 31 mW and a wavelength of  $\lambda_L$  of 1537.7 nm, and the driving microwave power is set at  $P_p = 20$  dBm. In (a) and (c),  $\theta_{1A} = 170^\circ$  and  $\theta_{1B} = 85^\circ$ , and  $\theta_{1C}$  is varied from  $0^\circ$  to  $170^\circ$ , whereas in (b) and (d)  $(\theta_{1A}, \theta_{1B}, \theta_{1C}) = (170^\circ, 85^\circ, 60^\circ)$  (for this setting, both Stokes and anti-Stokes peaks are clearly visible near the FSR resonance).

A rotating lambda plate polarimeter is employed to measure the input SOP. The polarimeter measurements reveal that the input SOP for the two extreme cases (SSM of either anti-Stokes or Stokes peak) are orthogonal to each other (i.e., separated by a diameter on the Poincaré sphere).

The plots shown in Figs. 4(b) and 4(d) exhibit anti-Stokes and Stokes intensity, respectively, as a function of microwave driving frequency  $f_p$  and static magnetic field  $H_s$ . The FSR resonance changes as we vary the static magnetic field  $H_s$ . Accordingly, from Figs. 4(b) and 4(d), we see that both anti-Stokes and Stokes intensities get pronounced when driving frequency  $\omega_p/(2\pi)$  is within the bandwidth of FSR resonance at  $\omega_m/(2\pi)$ .

Our experimental setup (see Fig. 1) allows measuring the SOP of both sidebands. While the plots shown in Fig. 4 display the total optical intensity  $I_T = I_{DPPD1} + I_{DPPD2}$ , the intensity  $I_{DPPD1}$  ( $I_{DPPD2}$ ) is separately displayed in the top (bottom) row plots shown in Fig. 5. These two intensities  $I_{DPPD1}$  and  $I_{DPPD2}$  represent two orthogonal SOP, which can be set by adjusting PC2 (see Fig. 1). The left (right) column plots in Fig. 5 display the measured intensity of the left anti-Stokes (right Stokes) sideband at wavelength  $\lambda_L - \lambda_{SB}$  ( $\lambda_L + \lambda_{SB}$ ), whereas the intensity at the central wavelength  $\lambda_L$  is displayed by the central column plots in Fig. 5. For the measurements shown in Fig. 5, PC1 is set to a nearly SSM state. By varying the setting of PC2, we find that the central peak at wavelength  $\lambda_L$  is maximized (minimized) in the same region where the sidebands at wavelength  $\lambda_L \pm \lambda_{SB}$  are minimized (maximized). This observation implies that in the region of SSM, the SOP of the sidebands is nearly orthogonal to the SOP of the incident light. This orthogonality can be exploited at the receiver end of a data transmission system based on our proposed MO modulation, since it allows demodulation by polarization filtering-out of the carrier at wavelength  $\lambda_L$ .



**FIG. 5.** Sideband SOP. The measured intensity  $I_{DPPD1}$  ( $I_{DPPD2}$ ) is shown (in dBm units) in the plots labeled by the letter “a” (“b”). The intensity at wavelengths  $\lambda_L - \lambda_{SB}$ ,  $\lambda_L$  and  $\lambda_L + \lambda_{SB}$  is shown in the plots labeled by the numbers “1,” “2,” and “3,” respectively. The TL1 is set at an optical power of 31 mW and a wavelength of  $\lambda_L$  of 1538.9 nm, the driving microwave is set at a power  $P_p$  of 20 dBm.

#### IV. MO COUPLING

The MO coupling giving rise to the optical sidebands originates from an interaction term in the system’s Hamiltonian, which is denoted by  $V_{SB}$ . This term  $V_{SB}$  is commonly derived from the classical energy density associated with the interaction between magnetization and optical modes. For the case where only whispering gallery FSR optical modes participate in the interaction, the term  $V_{SB}$  was derived in Refs. 11–19, whereas for our experimental configuration we consider the case where light propagates through the FSR bulk.

Consider an incident I (scattered S) optical field, having right and left handed circular polarization amplitudes  $E_{I+}$  and  $E_{I-}$  ( $E_{S+}$  and  $E_{S-}$ ), respectively. The time-averaged energy density  $u_m$  associated with MO coupling is given by  $u_m = (1/4)\text{Re}\mathcal{U}_m$ , where

$$\mathcal{U}_m = \begin{pmatrix} E_{S+}^* & E_{S-}^* \end{pmatrix} \epsilon_m \begin{pmatrix} E_{I+} \\ E_{I-} \end{pmatrix}, \quad (1)$$

and where  $\epsilon_m = \epsilon_{m0} + \epsilon_{m+m_{+'}} + \epsilon_{m-m_{-}}$  is a transverse permittivity tensor. The static part  $\epsilon_{m0}$  is given by Eq. (A2) of Appendix A. The diagonal elements of  $\epsilon_{m0}$  give rise to the static Faraday effect, whereas the static Voigt (Cotton–Mouton) effect originates from the off-diagonal elements of  $\epsilon_{m0}$  [see Eq. (A2)]. The terms  $\epsilon_{m+m_{+}}$  and  $\epsilon_{m-m_{-}}$  account for the effect of magnetization precession, where  $\epsilon_{m\pm}$  is given by Eq. (A3) of Appendix A, and  $m_{\pm}$  represent amplitudes of magnetization precession. Note that the matrix  $\epsilon_{m\pm}$  is proportional to  $e^{\pm i\varphi}$ , where  $\varphi$  is the azimuthal angle

[see Eq. (A3)]. The spherical symmetry of the FSR is partially broken by the two CFs that are employed for holding it (see Fig. 1).

In the semiclassical approximation,  $V_{SB}$  is derived from  $u_m = (1/4)\text{Re}\mathcal{U}_m$  [see Eq. (1)]. Consider a pair of optical modes having normalized scalar spatial waveforms, which in spherical coordinates are expressed as  $u_{n'}(r, \theta, \varphi)$  and  $u_{n''}(r, \theta, \varphi)$ , respectively. The contribution of this pair to the total interaction term  $V_{SB}$ , which is denoted by  $V_{n',n''}$ , is expressed as

$$V_{n',n''} = a_{n'}^\dagger a_{n''} (g_{n',n'',+} b^\dagger + g_{n',n'',-} b) + \text{h.c.}, \quad (2)$$

where  $a_n$  ( $b$ ) is an annihilation operator for the  $n$ th optical mode (magnon mode), and h.c. stands for Hermitian conjugate. The coupling coefficients  $g_{n',n'',\pm}$  are given by (recall that in our experiment the static magnetic field is normal to the light propagation direction)

$$\hbar^{-1} g_{n',n'',\pm} \simeq g_0 \int d\mathbf{r}' e^{\pm i\varphi} u_{n'}(\mathbf{r}') u_{n''}^*(\mathbf{r}'), \quad (3)$$

where  $g_0 = \omega_L Q_s / (8n_0^2 N_s^{1/2})$  and  $N_s$  is the number of FSR spins ( $N_s = 3.4 \times 10^{16}$  for the FSR under study). For YIG in the telecom band (free space wavelength  $\lambda_0 \simeq 1550$  nm), the refractive index is  $n_0 = 2.19$ , and the dimensionless MO coupling coefficient is  $Q_s \simeq 10^{-4}$ ,<sup>33</sup> and thus  $g_0/(2\pi) = 2.7$  Hz. The overlap integral in Eq. (3) represents a photon-magnon scattering selection rule.<sup>11,12</sup>

The ratio of sideband output optical power to the input optical power is denoted by  $\eta_{SB}$ . The largest value of  $\eta_{SB}$  is obtained at the triple resonance,<sup>11</sup> for which the MW driving is tuned to the FSR resonance  $\omega_m$ , the laser frequency  $\omega_L$  matches the frequency of one optical mode, and the second one has a frequency detuned from  $\omega_L$  by  $\omega_m$ . For this case  $\eta_{SB} \simeq (2n_0 R_s g_0 / c)^2 N_m$  [it is assumed that the overlap integral in Eq. (3) is of order unity], where  $N_m$  is the averaged number of excited magnons in steady state. For the case where the MWA is nearly critically coupled to the FSR, at resonance  $N_m \simeq P_p / (\hbar\omega_m \kappa_m)$ , where  $\kappa_m$  is the FSR damping rate. The values of  $P_p = 20$  dBm,  $\omega_m/(2\pi) = 3.8$  GHz and  $\kappa_m/(2\pi) = 1$  MHz yield  $\eta_{SB} \simeq 10^{-5}$ . This rough estimate agrees with the experimentally observed value of  $\eta_{SB}$  (see Fig. 5).

## V. KERR NONLINEARITY

Magnetic anisotropy gives rise to Kerr nonlinearity in the FSR response.<sup>34</sup> The nonlinearity can be exploited for modulation amplification.<sup>35</sup> The anisotropy-induced Kerr coefficient  $K_M$  is given by  $K_M = \hbar\gamma_e^2 K_{c1} / (V_s M_s^2)$ , where  $K_{c1}$  is the first-order anisotropy constant,  $V_s = 4\pi R_s^3 / 3$  is the FSR volume, and  $M_s$  is the saturation magnetization.<sup>34</sup> For YIG  $K_{c1} = -610$  J/m<sup>3</sup> at 297 K, and  $M_s = 140$  kA/m, hence for  $R_s = 125$   $\mu$ m the expected value of the Kerr coefficient is given by  $K_M/(2\pi) = -2.0 \times 10^{-9}$  Hz. The Kerr nonlinearity is expected to give rise to bistability in the FSR response to externally applied driving.

Modulation measurements in the nonlinear regime are shown in Fig. 6. The results indicate that the Kerr coefficient  $K_M$  is negative (giving rise to softening). For the plots shown in the top (bottom) row of Fig. 6, the microwave driving frequency is swept

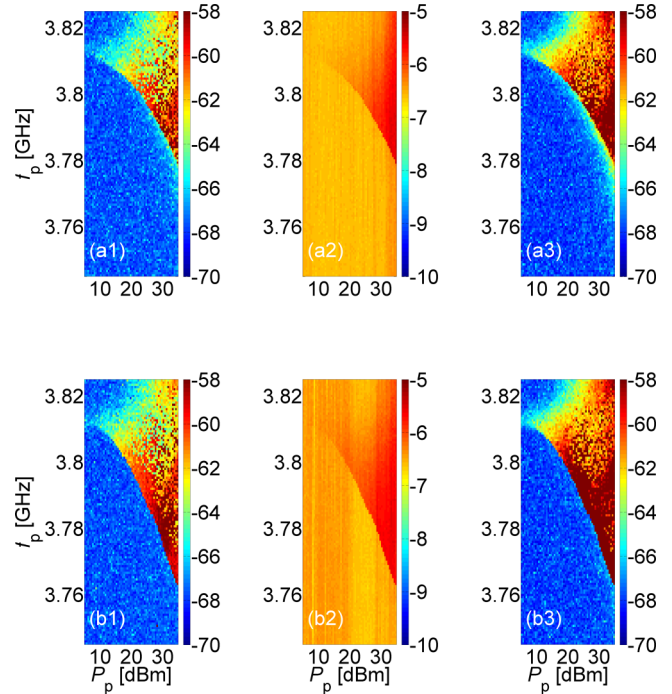


FIG. 6. Spectral peaks (in dBm units) in the nonlinear regime as a function of MW driving power  $P_p$ . The intensity of the left (right) sideband at wavelength  $\lambda_L - \lambda_{SB}$  ( $\lambda_L + \lambda_{SB}$ ) is shown in the plots in the left (right) column, whereas the plots in the central column show the intensity of the central optical peak (at TL1 wavelength  $\lambda_L$ ). For the plots shown in the top (bottom) row, the frequency  $f_p$  is swept upwards (downwards).

19 September 2023 06:11:03

upwards (downwards). The dependency on sweeping direction is attributed to nonlinearity-induced bistability, which, in turn, gives rise to hysteresis.

## VI. SUMMARY

In summary, polarization-selective SSM in the telecom band is achieved using an FSR strongly coupled to an LGR. The modulator can be used in a wide optical band, and it is compatible with ultra low temperatures. Future study will explore potential applications, including quantum state readout of superconducting circuits.

## ACKNOWLEDGMENTS

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## AUTHOR DECLARATIONS

### Conflict of Interest

The authors have no conflicts to disclose.

Author Contributions

**Banoj Kumar Nayak:** Data curation (lead); Investigation (lead); Writing – original draft (equal). **Eyal Buks:** Formal analysis (lead); Supervision (lead); Writing – original draft (equal).

DATA AVAILABILITY

The data that support the findings of this study are available from the corresponding author upon reasonable request.

APPENDIX A: TRANSVERSE PERMITTIVITY TENSOR

The evolution of electromagnetic waves propagating inside a magnetized medium is governed by a  $3 \times 3$  permittivity tensor.<sup>36–38</sup> Consider a Cartesian coordinate system  $(x, y, z)$ , for which the propagation direction is parallel to the  $z$  direction. In this system, the static magnetic field (magnetization vector) is parallel to a unit vector denoted by  $\hat{h}$  ( $\hat{m}$ ). The angle between  $\hat{h} = (h_x, h_y, h_z) = (\sin \theta \cos \varphi, \sin \theta \sin \varphi, \cos \theta)$  and  $\hat{m} = (m_x, m_y, m_z)$  is assumed to be small.

From the  $3 \times 3$  permittivity tensor, a  $2 \times 2$  transverse permittivity tensor  $\epsilon_T$  can be derived. In a basis of circular SOP,  $\epsilon_T$  is given by  $\epsilon_T = n_0^2 I + \epsilon_m$ , where  $n_0$  is the medium refractive index,  $I$  is the  $2 \times 2$  identity matrix, and the  $2 \times 2$  matrix  $\epsilon_m$  (in a basis of circular SOPs) is given by<sup>39</sup>

$$\frac{\epsilon_m}{n_0^2} = \begin{pmatrix} Q_s m_z & Q_s^2 m_-^2 \\ Q_s^2 m_+^2 & -Q_s m_z \end{pmatrix}, \tag{A1}$$

where  $m_{\pm} = (m_x \pm im_y)/\sqrt{2}$ . For YIG in the telecom band, the refractive index is  $n_0 = 2.19$ , and the dimensionless MO coupling coefficient is  $Q_s \simeq 10^{-4}$ .<sup>33</sup>

The eigenvalues of  $\epsilon_m/n_0^2$  (A1) are given by  $\pm Q_s \sqrt{m_z^2 + Q_s^2 m_{\pm}^2}$ . For the Faraday configuration, for which  $m_x = m_y = 0$  and  $m_z = 1$ , i.e.,  $\hat{m}$  is parallel to the propagation direction, the eigenvectors of  $\epsilon_m/n_0^2$  represent circular SOPs, the corresponding eigenvalues are  $\pm Q_s$ , and MO coupling gives rise to circular birefringence, whereas for the Voigt (Cotton–Mouton) configuration, for which  $m_z = 0$  and  $m_x^2 + m_y^2 = 1$ , i.e.,  $\hat{m}$  is perpendicular to the propagation direction, the eigenvectors of  $\epsilon_m/n_0^2$  represent colinear SOPs, the corresponding eigenvalues are  $\pm Q_s^2/2$  [note that  $m_x^2 m_y^2 = (m_x^2 + m_y^2)^2/4$ ], and MO coupling gives rise to colinear birefringence. Note that for the Faraday configuration, the SOP rotation angle that is accumulated over a traveling distance of a single optical wavelength is  $2\pi Q_s$ .

To describe the effect of magnetization precession on  $\epsilon_m$ , it is convenient to express  $\hat{m}$  (magnetization unit vector) as a sum of parallel and perpendicular components, with respect to  $\hat{h}$  (magnetic field unit vector). In a Cartesian coordinate system  $(x', y', z')$ , for which the static magnetic field is parallel to the  $z'$  direction, the unit vector parallel to the magnetization vector is expressed as  $\hat{m}' = m_x \hat{x}' + m_y \hat{y}' + m_z \hat{z}' = m_+ \hat{u}'_+ + m_- \hat{u}'_- + m_z \hat{z}'$ , where  $\hat{u}'_{\pm} = (\hat{x}' \pm i\hat{y}')/\sqrt{2}$ , and where  $m_{\pm} = (m_x \mp im_y)/\sqrt{2}$ . The unit vectors  $\hat{m}$  and  $\hat{m}'$  are related by  $\hat{m} = R_{\hat{h}}^{-1} \hat{m}'$ , where for a given unit

vector  $\hat{h}$ , the rotation matrix  $R_{\hat{h}}$  is defined by the relation  $R_{\hat{h}} \hat{h} = \hat{z}$  and, thus,  $\hat{m} = m_+ \hat{v}_+ + m_- \hat{v}_- + m_z R_{\hat{h}}^{-1} \hat{z}'$ , where  $\hat{v}_{\pm} = R_{\hat{h}}^{-1} \hat{u}'_{\pm}$ . The matrix elements of the  $3 \times 3$  rotation matrix  $R_{\hat{h}}$  are given by  $R_{11} = 1 + (\cos \theta - 1) \cos^2 \varphi$ ,  $R_{22} = 1 + (\cos \theta - 1) \sin^2 \varphi$ ,  $R_{12} = R_{21} = (1/2)(\cos \theta - 1) \sin(2\varphi)$ ,  $R_{31} = -R_{13} = \sin \theta \cos \varphi$ ,  $R_{32} = -R_{23} = \sin \theta \sin \varphi$ , and  $R_{33} = \cos \theta$ . The following holds  $\hat{v}_{\pm} = \cos^2(\theta/2) \hat{u}_{\pm} - e^{\pm 2i\varphi} \sin^2(\theta/2) \hat{u}_{\mp} - 2^{-1/2} e^{\pm i\varphi} (\sin \theta) \hat{z}$ , hence  $\hat{m} = \mu_+ \hat{u}_+ + \mu_- \hat{u}_- + \mu_z \hat{z} + m_z \hat{h}$ , where  $\mu_{\pm} = m_{\pm} \cos^2(\theta/2) - m_{\mp} e^{\mp 2i\varphi} \sin^2(\theta/2)$  and  $\mu_z = -2^{-1/2} (m_+ e^{i\varphi} + m_- e^{-i\varphi}) \sin \theta$  and, thus,  $m_{\pm} = \mu_{\mp} + 2^{-1/2} m_z e^{\mp i\varphi} \sin \theta$ .

The assumption that the angle between the static magnetic field and the magnetization vector is small implies that  $m_z \simeq 1$  and  $|m_{\pm}| \ll 1$ . To first order in  $|m_{\pm}|$ ,  $\epsilon_m$  can be expanded as  $\epsilon_m = \epsilon_{m0} + \epsilon_{m+} m_+ + \epsilon_{m-} m_-$ , where  $\epsilon_{m0}$ , which is given by [compare with Eq. (A1)]

$$\frac{\epsilon_{m0}}{n_0^2} = \begin{pmatrix} Q_s \cos \theta & \frac{Q_s^2 e^{2i\varphi} \sin^2 \theta}{2} \\ \frac{Q_s^2 e^{-2i\varphi} \sin^2 \theta}{2} & -Q_s \cos \theta \end{pmatrix}, \tag{A2}$$

accounts for static magnetization, and where  $\epsilon_{m\pm}$ , which is given by

$$\frac{\epsilon_{m\pm}}{n_0^2} = \frac{Q_s e^{\pm i\varphi} \sin \theta}{\sqrt{2}} \begin{pmatrix} -1 & \pm Q_s (1 \pm \cos \theta) \\ \mp Q_s (1 \mp \cos \theta) & 1 \end{pmatrix}, \tag{A3}$$

accounts for magnetization precession.

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19 September 2023 06:11:03

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