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# Practical Roadmap and Limits to Nanostructured Photovoltaics

Richard R. Lunt,\* Timothy P. Osedach, Patrick R. Brown, Jill A. Rowehl, and Vladimir Bulović \*

The significant research interest in the engineering of photovoltaic (PV) structures at the nanoscale is directed toward enabling reductions in PV module fabrication and installation costs as well as improving cell power conversion efficiency (PCE). With the emergence of a multitude of nanostructured photovoltaic (nano-PV) device architectures, the question has arisen of where both the practical and the fundamental limits of performance reside in these new systems. Here, the former is addressed a posteriori. The specific challenges associated with improving the electrical power conversion efficiency of various nano-PV technologies are discussed and several approaches to reduce their thermal losses beyond the single bandgap limit are reviewed. Critical considerations related to the module lifetime and cost that are unique to nano-PV architectures are also addressed. The analysis suggests that a practical single-junction laboratory power conversion efficiency limit of 17% and a two-cell tandem power conversion efficiency limit of 24% are possible for nano-PVs, which, when combined with operating lifetimes of 10 to 15 years, could position them as a transformational technology for solar energy markets.

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# 1. Introduction

Harvesting sunlight with photovoltaic (PV) cells could generate enough electrical energy to meet the world's increasing energy demand while simultaneously enabling a reduction in the environmental impact associated with present modes of electricity production.<sup>[1]</sup> Scaling of PV installations to the needed terawatt scale, however, will require significant improvements in the cost-effectiveness of installed PVs, including improvements in their power conversion efficiencies (PCE) as well as reductions in the cost of PV module installation through streamlined fabrication and innovations in rapid and lightweight PV deployment.

Advancements in the field of nanostructured PVs (nano-PVs) have led to rapid improvements over the past decade in the power conversion efficiencies of this broad class of solar cells,<sup>[2]</sup> in which we include molecular, organic, polymeric, dyesensitized, and colloidal quantum dot (CQD) PVs due to the similarity of the

physical processes that govern their operation and fabrication. In general, we define nano-PVs as solar cells that 1) consist of thin films (<2  $\mu$ m) of semiconductor material, 2) incorporate nanometer-scale optoelectronic materials that 3) have excitonic or quantum-confinement character and 4) can be fabricated entirely with low-temperature (<300 °C) processing steps. The compatibility of many nanostructured PV materials with the use of low-temperature processing can enable the use of flexible, lightweight substrates,<sup>[3,4]</sup> potentially leading to a lower cost of solar module fabrication and installation. A particular advantage of nanostructured materials is the tunability of their optical and electronic properties, which may enable the implementation of "third-generation" approaches (i.e., strategies for reducing thermal losses) for improved PV power conversion efficiencies.<sup>[5]</sup>

Here, we first review the fundamental limits to the performance of solar cells and then consider those limits in the context of various nano-PV technologies that are currently under investigation. We review the state of the art for PV technologies in each material class and calculate practical and semiempirical limits to their efficiency, taking into account the prospect for the application of third-generation concepts such as multiple exciton generation (MEG), singlet fission, and stacked-tandem WAIERIA www.advmat.de



device architectures. We also address critical considerations related to cost and module lifetime that are unique to nanostructured PV architectures.

### 2. Theoretical Limits of PV Operation

Single-junction photovoltaic cells are typically limited by four fundamental loss mechanisms:<sup>[6,7]</sup> 1) incomplete solar spectrum absorption, 2) thermalization of hot carriers (or excitons) in the form of excess heat, 3) chemical potential (thermodynamic) losses dictating that the photovoltage must be less than band gap ( $E_G$ ) for relaxed carriers, and 4) radiative recombination. The presence of other non-radiative losses (e.g., Auger recombination,<sup>[8]</sup> internal or phonon conversion, surface recombination,<sup>[8,9]</sup> etc.) can further reduce cell performance.<sup>[10]</sup> Considering only radiative losses, Shockley and Queisser (SQ) predicted a limiting power efficiency of 30% under simulated black body radiation,<sup>[7]</sup> that has been subsequently recalculated as 33% under AM 1.5 solar irradiance.<sup>[6,10]</sup>

The power conversion efficiency (PCE) is defined as

$$\eta_{\rm p} = \frac{J_{\rm SC} V_{\rm OC} F F}{P_0} \tag{1}$$

where  $V_{OC}$  is the open circuit voltage,  $J_{SC}$  is the short circuit current, *FF* is the fill factor, and  $P_0$  is the incident power. Starting from the SQ limit, where the ideal diode equation describes the current density (*J*)–voltage (*V*) characteristics vis

$$J = \frac{R_{\rm p}}{R_{\rm S} + R_{\rm p}} \left\{ J_{\rm S} \left[ \exp\left(\frac{q\left(V - J R_{\rm S}\right)}{nkT}\right) - 1 \right] + \frac{V}{R_{\rm p}} \right\} - J_{\rm SC} \quad (2)$$

where  $R_P$  is the shunt resistance,  $R_S$  is the series resistance, V is the voltage across the solar cell,  $J_{SC}$  is the photocurrent, n is the ideality factor, k is the Boltzmann constant, T is the temperature, and  $J_s$  is the reverse saturation dark current. The photocurrent is calculated by convolving the cell photoresponse with the solar spectrum as

$$J_{\rm SC} = q \int S(\lambda) E Q E(\lambda) d\lambda$$
(3)

where *q* is the charge of the electron, *S* is the solar photon flux, and *EQE* is the external quantum efficiency at wavelength  $\lambda$ . Rearranging Equation 2 for the open circuit condition (when *J* = 0) and assuming that the shunt resistance is very large compared to the series resistance, the *V*<sub>OC</sub> can be expressed as

$$V_{\rm OC} = \frac{nkT}{q} \ln\left(\frac{J_{\rm SC}}{J_{\rm S}} + 1\right) \tag{4}$$

In the SQ limit (n = 1), neglecting the photon chemical potential,<sup>[11]</sup>  $J_S$  is determined by radiative recombination as<sup>[7]</sup>

$$J_{\rm S} \approx qg \int_{E_{\rm G}}^{\infty} \frac{E^2 E \, QE}{\exp(E/nkT) - 1} \mathrm{d}E \tag{5}$$

where  $g = 2\pi/(c^2h^3)$ , *c* is the speed of light, and *h* is Plank's constant. Correspondingly, the *FF* is (for n = 1 and  $R_P \rightarrow \infty$ ):



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Vladimir Bulović is a Professor of Electrical Engineering at MIT, leading the Organic and Nanostructured Electronics Laboratory and co-directing the MIT-ENI Solar Frontiers Center. His interests include studies of physical properties of organic and organic/ inorganic nanocrystal composites, and development

of novel optoelectronic organic and hybrid nanoscale devices.

$$FF = \frac{J_{\rm M} V_{\rm M}}{J_{\rm SC} V_{\rm OC}}$$
$$\approx \left(\frac{q V_{\rm OC}/kT - \ln(1 + q V_{\rm OC}/kT)}{1 + q V_{\rm OC}/kT}\right) \left(1 - \frac{J_{\rm SC} R_{\rm S}}{V_{\rm OC}}\right) \tag{6}$$

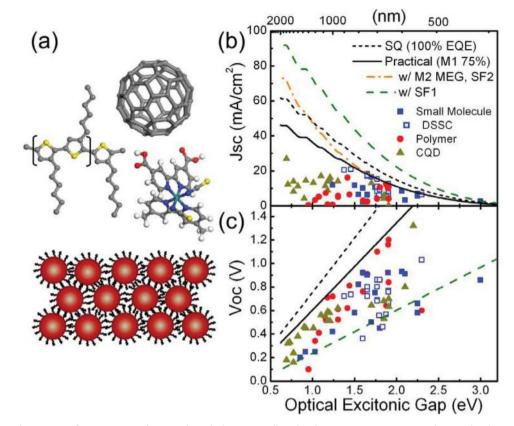
where  $J_M V_M$  is the maximum power operating point on the J-V curve and the resistance term is neglected in the SQ limit.

# 3. Practical Demonstrations of Nano-PVs Operation

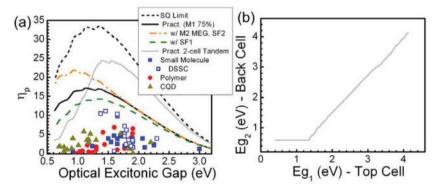
We now consider how the operating parameters for a broad range of reported nano-PV structures compare with these theoretical limits. **Figure 1** and **2** are plots of  $J_{SC}$ ,  $V_{OC}$ , and  $\eta_P$  as a function of the optical gap.<sup>[12]</sup> This data is also tabulated in **Table 1**.While not exhaustive, this list provides a representative range of efficiencies for each nano-PV type, including the presently highest-reported and certified values.

Five decades since Shockley and Queisser derived the power conversion efficiency limit of single-junction photovoltaic cells, researchers have still not demonstrated such high performance for any photovoltaic device system.<sup>[10]</sup> For example, the power conversion efficiency of the best single-crystal-Si single-junction PVs is  $\eta_P = 25\%$  (without solar concentration),<sup>[2,10]</sup> which is only





**Figure 1.** Illustrated structure of nanostructured materials including a) small molecule ( $C_{60}$ ), organic (Ru-complex), and polymer (P3HT) materials along with ligand-coated CQDs. Calculations of the SQ, practical, and various MEG characteristics of b) photocurrent ( $J_{sc}$ ) and c) open circuit voltage ( $V_{OC}$ ) under AM 1.5G illumination as a function of optical or excitonic gap. Note that the  $V_{OC}$  for the M1 and M2 MEG cases are nearly identical (the M2 line is therefore emitted for clarity). A range of measured device performance is shown for organic small molecule, dye-sensitized solar cell (DSSC), polymer, and CQD where the gap was estimated from the photoresponse edge (±0.1 eV). The maximum reported photocurrents under AM 1.5G illumination follow the curve for the practical photocurrent limit (M1) defined by 75% *EQE* across the spectrum to  $E_G$ . M2 MEG is a two-staircase multiplication, SF1 is a lone singlet fission material (or paired with a bandgap larger than the triplet level), and SF2 is a singlet-fission material paired with acceptor that has an optical gap equal to the triplet level of the SF material.



**Figure 2.** a) Calculations of the SQ, practical, MEG, SF, and two-cell tandem power conversion efficiency ( $\eta_p$ ) under AM 1.5G illumination versus optical gap or front-cell gap. A range of measured device performance is shown for organic small molecule, DSSC, polymer, and CQD. b) Calculation of the optimum bandgap pairing for the two-cell tandem as function of top (front)-cell optical gap.

76% of the SQ limit. Hence, in evaluating the achievable performance of a comparatively new PV technology, such as nano-PVs, it is prudent and necessary to make an estimate of the upper limit of the achievable  $\eta_P$  by numerically evaluating trends of the

best technical demonstrations. Our literature survey of nano-PV technologies (Table 1) collects device data of the best experimentally reported performance in terms of EQE, FF, and  $V_{OC}$  over the last two decades. From this data a semiempirical estimate for the practical upper limit to the power conversion efficiency of nano-PVs is derived. For example, the maximum demonstrated EQE across the spectrum is ≈75% with internal quantum efficiencies approaching 100% (Table 1); the losses in EQE are due primarily to combined optical losses (≈10% loss from the transparent conductive oxide electrode absorption, ≈5% reflection from the front facet of the substrate, and ≈10% loss from internal reflections), which likely will be difficult to eliminate in a practical device structure. Assuming this average

maximum *EQE* of 75% is maintained at wavelengths extending to the band edge of the optically active semiconductor of the PV cell, upper limits of  $J_{SC}$  are calculated as a function of optical bandgap (labeled "M1") according to Equation 3. For estimates of



 Table 1. Representative device performance of various single-junction nanostructured photovoltaic cells under 1-sun illumination.

Donor <sup>a)</sup>	Acceptor	Е <sub>G</sub> [eV]	V <sub>oc</sub> [V]	J <sub>sc</sub> [mA cm <sup>-2</sup> ]	FF	$\eta_{P}$ [%]	Ref.
Small Molecule							
NPD	C <sub>60</sub>	3.0	0.86	2.5	0.51	1.1	[125]
Tetracene	C <sub>60</sub>	2.3	0.58	7.0	0.57	2.3	[126]
PtOEP	C <sub>60</sub>	2.3	0.66	5.6	0.57	2.1	[127]
DIP	C <sub>60</sub>	2.1	0.93	8.4	0.74	3.9	[128]
Rubrene	C <sub>60</sub>	2.1	0.91	3.2	0.53	1.5	[129]
DBP	C <sub>60</sub>	1.9	0.92	6.3	0.65	3.6	[130]
PtTPBP	C <sub>60</sub>	1.8	0.69	4.5	0.63	1.9	[131]
CuPc	C <sub>60</sub>	1.7	0.50	16.5	0.56	4.5	[132]
SubNc	C <sub>60</sub>	1.7	0.79	6.1	0.49	2.5	[133]
3P	Ind-C <sub>60</sub>	1.7	0.75	10.5	0.65	5.2	[134]
DCV6T	C <sub>60</sub>	1.7	0.90	6.5	0.64	3.8	[135]
SQ	PC <sub>70</sub> BM	1.6	0.92	12.0	0.5	5.5	[15]
ZnPc	C <sub>60</sub>	1.5	0.58	11.7	0.62	3.9	[136]
CIAIPc	C <sub>60</sub>	1.5	0.82	6.5	0.58	3.0	[137]
SnPc	C <sub>60</sub>	1.2	0.42	7.6	0.63	1.9	[138]
PT Psub	C <sub>60</sub>	1.0	0.25	-	_	_	[139]
PT Pfused	C <sub>60</sub>	0.9	0.20	-	_	-	[139]
CNT	C <sub>60</sub>	0.9	0.25	-	0.51	0.6	[39]
DSSC							
0131	TiO <sub>2</sub> , P3HT HTL	2.3	1.03	6.3	0.60	3.9	[140]
Zn5S	TiO <sub>2</sub>	1.9	0.67	7.2	0.67	3.1	[141]
Cu-Complex 1	TiO <sub>2</sub>	1.9	0.57	5.3	0.64	1.9	[142]
Ru-TPA-NCS	TiO <sub>2</sub> ,HTL	1.9	0.77	5.7	0.34	1.5	[143]
Ru-TPD-NCS	TiO <sub>2</sub> ,HTL	1.9	0.76	12.7	0.35	3.4	[143]
Ru Complex	TiO <sub>2</sub>	1.8	0.68	15.3	0.69	7.1	[144]
(68	TiO <sub>2</sub>	1.8	0.86	11.0	0.68	5.1	[145]
ГСРР	TiO <sub>2</sub>	1.8	0.46	_	0.62	3.5	[146]
Cu-Complex 1	TiO <sub>2</sub>	1.8	0.56	5.9	0.70	2.3	[142]
2101	TiO <sub>2</sub> ,spiro-MeOTAD	1.8	0.80	8.2	0.69	4.5	[48]
0149	TiO <sub>2</sub> , PEDOT HTL	1.8	0.86	9.3	0.75	6.1	[52]
RuL2(SCN)2	TiO <sub>2</sub>	1.7	0.72	18.2	0.73	10.0	[147]
CYC-B6S	TiO <sub>2</sub>	1.7	0.78	19.8	0.63	9.7	[148]
Ru-Complex	TiO <sub>2</sub>	1.7	0.80	17.0	0.74	10.1	[43]
A6141	TiO <sub>2</sub>	1.7	0.80	17.6	0.73	10.3	[45]
ZnPcTyr	TiO <sub>2</sub>	1.6	0.36	2.3	0.67	0.5	[149]
Black Dye	TiO <sub>2</sub>	1.5	0.74	20.9	0.72	11.1	[150]
RuL(NCS)3	TiO <sub>2</sub>	1.4	0.72	20.5	0.70	10.4	[44]
Polymer							
23HT	PC70BM -TiO2	1.9	0.64	12.4	0.51	4.1	[49]
23HT	PCBM	1.9	0.64	11.3	0.69	5.2	[120,151]
APFO-3	PC <sub>70</sub> BM	1.9	1.16	10.0	_	_	[152]
P3HT	Indene-C <sub>60</sub>	1.9	0.84	10.6	0.73	6.5	[153]
8TBT	P3HT	1.9	1.20	4.0	_	1.8	[31]
PCDTBT	PC <sub>70</sub> BM	1.8	0.86	10.6	0.64	6.0	[154]



Table 1. Continued



Donor <sup>a)</sup>	Acceptor	E <sub>G</sub> [eV]	V <sub>oc</sub> [V]	J <sub>sc</sub> [mA cm <sup>-2</sup> ]	FF	$\eta_{P}$ [%]	Ref.
F8TBT	PCBM	1.8	1.10	4.0	-	1.3	[31]
PFDPP2T-c	PCBM	1.7	0.91	2.4	0.40	0.9	[155]
PBDTTT-CF	PCBM	1.6	0.76		0.66	6.8	[33]
MDMO-PPV	PCBM	1.6	0.92	3.0	_	_	[152]
PCPDTBT	PC <sub>70</sub> BM	1.4	0.62	16.2	0.55	5.5	[156]
APFO-9	PCBM	1.4	0.81	6.5	0.44	2.3	[30]
PCPDTDPP2T-c	PCBM	1.3	0.61	5.7	0.49	1.7	[155]
P1TPQ	PCBM	1.2	0.71	0.8	0.58	0.3	[32]
P3TPQ	PC <sub>70</sub> BM	1.2	0.52	7.3	0.54	2.1	[32]
ртвенво	PCBM	1.2	0.72	0.6	0.53	0.2	[157]
P3	PCBM	1.1	0.41	5.2	0.29	0.6	[158]
LBPP1	PCBM	1.0	0.34	3.3	0.34	0.4	[159]
PBTTQ	PCBM	1.0	0.10	0.3	0.35	0.01	[160]
CQD							
PbS	_	2.2	1.32	_	0.42	2.9	[161]
CdSe	_	2.1	0.80	_	_	_	[162]
CdSe	_	1.9	0.53	6.2	0.53	1.8	[163]
CdSe QD	_	1.9	0.70	0.2	0.40	0.1	[164]
CdSe TP	_	1.9	0.63	4.8	0.52	1.5	[164]
CdSe NR	_	1.8	0.68	4.2	0.38	1.1	[164]
Sb <sub>2</sub> S <sub>3</sub>	TiO <sub>2</sub> ,P3HT	1.7	0.65	13.0	0.61	5.13	[54]
PbS	-	1.2	0.55	11.4	0.56	3.5	[62]
PbS	-	1.2	0.59	8.9	0.56	2.9	[64]
PbS	-	1.2	0.51	16.2	0.58	5.1	[165]
PbS	-	1.2	0.51	14.0	0.51	3.6	[166]
PbS	-	1.2	0.58	15	0.42	3.5	[167]
PbS	-	1.1	0.56	17.0	0.61	5.7	[63]
PbS	-	1.0	0.45	13.2	0.35	2.1	[165]
PbS	-	0.9	0.45	14.5	0.60	3.9	[62]
PbS	-	0.9	0.46	4.2	0.62	1.3	[69]
PbS	-	0.8	0.16	8.2	0.38	0.5	[69]
PbS	-	0.8	0.24	14.0	0.50	1.7	[69]
PbS	-	0.8	0.38	11.3	0.21	0.9	[165]
PbSe	-	0.7	0.18	27.0	0.35	1.7	[68]
PbS	-	0.7	0.33	_	_	-	[168]
PbS	_	0.7	0.32	12.3	0.44	1.8	[168]

<sup>a)</sup>Chemical abbreviations: NPD - *N*,*N*'-diphenyl-N,N'-bis(1-naphthyl)-1,1'biphenyl-4,4'' diamine; PtOEP - 2,3,7,8,12,13,17,18-octaethyl-21H,23H-porphine platinum(II); DIP - di-indenoperylene; DBP - dibenzo{[f,f'] - 4,4',7,7'-tetraphenyl}diindeno[1,2,3-cd:1',2',3'-lm]perylene; PtTPBP - platinum tetraphenylbenzoporphyrin; CuPc - copper phthalocyanine; SubPc - boron subphthalocyanine; BP - tetrabenzoporphyrin; DCV6T - bis-(dicyanovinylen)-sexithiophene; SQ - 2,4-bis[4-(*N*,*N*-diisobutylamino)-2,6-dihydroxyphenyl]squaraine; ZnPc - zinc phthalocyanine; ClAIPc - chloro-aluminum phthalocyanine; SnPc - tin phthalocyanine; PT Psub - diporphyrin–pyrene; PT Pfused - pyrene-fused diporphyrin; CNT - carbon nanotube; P3HT - poly(3-hexylthiophene); APFO-3 - poly[(9,9-dioctylfluoren)-2,7-diyl)-alt-5,-(40,70-di-2-thienyl-20,10,30-benzothiadiazole]]; F8TBT - poly((9,9-dioctylfluoren)-2,7-diyl-alt-[4,7-bis(3-hexylthien-5-yl)-2,1,3-benzothiadiazole]-2',2''-diyl); PBDTT-CF - poly[4,8-bis(2-ethylhexylo-ybenzo[1,2bi-4,5-b']dithiophene-2,6-diyl-alt-(4-octanoyl-5-fluoro-thieno[3,4-b]thiophene-2-carboxylate)-2,6-diyl]; MDMO-PPV - poly[2-methoxy-5-0]y<sup>\*</sup>,7'-dimethyloctyloxy)-1,4-phenylene 'unylene]; PCPDTBT - poly[2,1,3-benzothiadiazole-4,7-diyl](4,4-bis(2-ethylhexyl)-4H-cyclopenta[2,1-b:3,4-b']dithiophene-2,6-diyl]; P3 - 6,7-diphenyl-4,9-bis-(thiophen-'2,9l)-[1,2,5]thiadiazolo[3,4-g]quinoxaline/9-triarylamino-9H-carbazole; PCBM - [6,6]-phenyl-C61-butyric acid methyl ester; spiro-OMeTAD - (2,2(,7,7(-tetrakis-(N,N-dipmethoxyphenylamine)9,9(-spirobifluorene); PEDOT - poly(3,4-ethylenedioxythiophene); HTL - hole transport layer. ROGRESS REPORT

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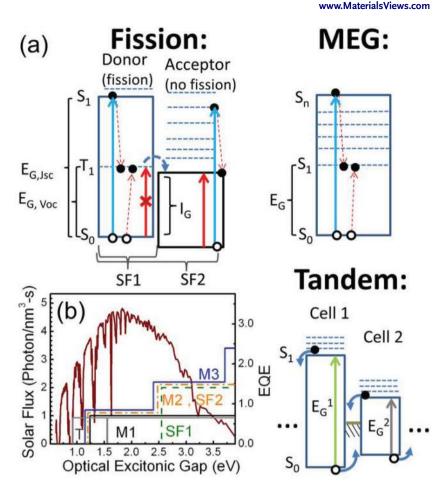
the best practical device performance, upper limits for the *FF* as a function of optical gap are similarly assumed to be that of the highest reported (i.e., FF = 0.75) across the spectrum (Table 1). Deviations in FF from the SQ limit generally stem from a combination of large series resistance (R<sub>s</sub>) and low shunt resistance  $(R_{\rm P})$ . While many empirical forms have been proposed for the dependence of  $V_{\rm OC}$  as a function of  $E_{G}$ ,<sup>[13,14]</sup> it is found that maximum demonstrated photovoltages follow a trend of reaching 80% of the value predicted by the SQ limit (Equation 4); the difference can be attributed to a number of recombination phenomena including internal conversion, interface recombination, and exciton binding losses, as discussed below.<sup>[15]</sup> Nonetheless, this threshold in  $V_{\rm OC}$  is consistent with the framework of the SQ limit and can be used in combination with the practical upper limits in photocurrents and fill-factors to estimate the ultimate laboratory efficiency limits of nano-PVs, as shown in Figure 2a. We find that a semiempirically derived maximum efficiency of 17% is achievable for a single-junction cell with a bandgap in the range of 1.1 eV to 1.4 eV. This maximum efficiency is lower than that reported in recent semitheoretical studies in which practical considerations described above are not taken into account and which led to maximum exciton-limited efficiencies ranging from 22-27%.<sup>[15]</sup> Also plotted in Figure 2a are  $\eta_{\rm P}$  versus. bandgap curves calculated with Equation 3-5 based on the implementation of various third-generation concepts (shown in Figure 3) that will be described in detail below; for two-cell current-matched nanostructured tandems, the optimal efficiency as function of top-cell bandgap is shown in Figure 2a, where the corresponding optimal pairing of the backcell gap is plotted in Figure 2b.

# 4. Analysis of Performance of Nano-PV Technologies

In the remainder of this article, we review the challenges associated with each type of nano-PV device and suggest particular areas for improvement in order to approach the efficiency limits. We then discuss third-generation concepts particularly relevant to nanostructured materials that can allow for efficiencies beyond the single-junction limit and, finally, consider these efficiency limits in the context of the nano-PV module cost and operating lifetime.

### 4.1. Small Molecule and Polymer PVs

One of the distinguishing features of molecular, organic, and polymeric semiconductors is the presence of strongly bound

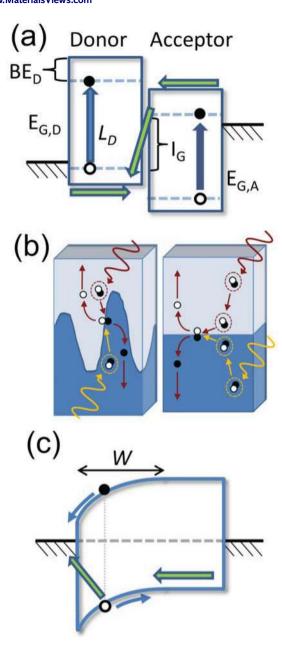


**Figure 3.** a) Schematic of various methods relevant in nanostructured materials to reduce thermal losses including singlet exciton fission, multiple exciton generation, and tandem stacking.  $E_{G,Jsc}$  (singlet level) and  $E_{G,Voc}$  (triplet level) are the gaps used to calculate the  $J_{sc}$  and  $V_{OC}$  in the SQ limit, respectively, for singlet fission case SF1, where there is negligable oscillator strength between the triplet and singlet levels for photocurrent generation. Solid arrows are optical transition, red dashed arrows are electronics transistions associated with multiple exciton generation and the blue dashed line designates charge transfer exciton dissociation. b) AM 1.5G solar photon flux as a function of energy and the representative external quantum efficiency profiles of various cell configurations. Profiles are offset slightly from the M1 (practical) line for clarity; M2 and M3 MEG are a two-staircase and three staircase multiplication profile, respectively; SF1 is a lone singlet fission material paired with an acceptor bandgap larger than the triplet level) and SF2 is a singlet-fission material paired with acceptor that has an optical gap equal to the triplet level of the SF material; T is the 2-cell current-matched tandem scenario where the vertical lines indicate the two bandgaps.

excited states, known as Frenkel excitons.<sup>[16]</sup> These excitons have a significant impact on many of the processes in photovoltaic devices, from photocurrent generation to the characteristically pronounced absorption features.<sup>[3]</sup> For example, organic semiconductors typically exhibit static dielectric constants in the range of 2 to 5<sup>[16]</sup> and, accordingly, exhibit large exciton binding energies of between 0.2 eV and 0.8 eV.

To overcome this exciton binding energy, bilayer donoracceptor architectures have become common to promote exciton separation to free carriers<sup>[17–19]</sup> as shown in **Figure 4**. However, there still remains an inherent tradeoff between the light absorption efficiency within the nano-PV device layers (quantified by the absorption constant,  $\alpha$ ) and exciton diffusion efficiency (quantified by the exciton diffusion length,

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**Figure 4.** Illustration of the energy diagram for a) a donor–acceptor heterojunction under short-circuit conditions (fully depleted) where the  $V_{OC}$ -limiting recombination current is highlighted by green arrows and b) a bulk-heterojunction architectures utilized in small-molecule, organic, and polymer cells. c) Energy diagram for a Schottky junction under short-circuit condition.  $E_{G,D}$ and  $E_{G,A}$  are the optical gap of the donor and acceptor, respectively; BE<sub>D</sub> is the exciton binding energy in the donor,  $L_D$  is the exciton diffusion length, and I<sub>G</sub> is the donor–acceptor interface gap for recombination.

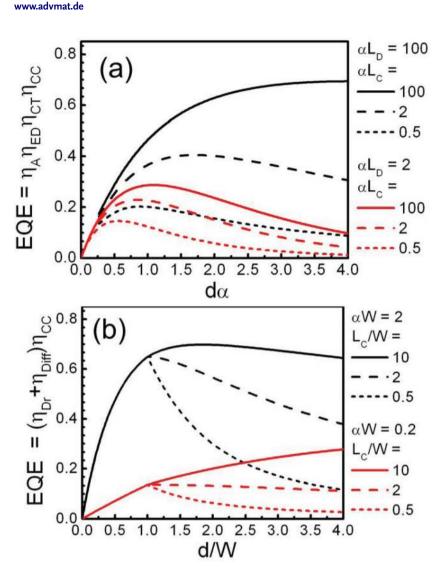
 $L_{\rm D}$ ) to the exciton-dissociating bilayer interfaces. As thicker layers are needed to absorb more light and thinner layers are desired to facilitate excitons reaching dissociative bilayer interfaces, the tradeoff requires optimization of the nano-PV layer thickness for the maximized device performance. The *EQE* can therefore be described in terms of the constituent efficiencies as  $EQE = \eta_A \eta_{\rm ED} \eta_{\rm CT} \eta_{\rm CC}$  where  $\eta_A$  is the absorption efficiency,  $\eta_{\rm ED}$  is the exciton diffusion efficiency,  $\eta_{\rm CT}$  is the charge-transfer or dissociation efficiency, and  $\eta_{\rm CC}$  is the charge collection efficiency. In the absence of optical interference,  $\eta_{\rm A} = T(1 - \exp(-\alpha d))$  where *T* is the total transmission through the substrate and the transparent conductive oxide electrode to the active layer (typically limited to at most 75%),  $\alpha$  is the absorption coefficient, and *d* is the active layer thickness;  $\eta_{\rm ED} = \exp(-d/L_D)$ ;  $\eta_{\rm CT} \approx 1$  for a large donor–acceptor energy offset that drives efficient exciton dissociation at the bilayer interface;  $\eta_{\rm CC} = L_{\rm C}/d(1 - \exp(-d/L_{\rm C}))$ , where  $L_{\rm C}$  is the charge collection length.<sup>[20,21]</sup> This model for the *EQE* is plotted in **Figure 5** as a function of  $\alpha d$  for various values of  $\alpha L_{\rm D}$  and  $\alpha L_{\rm C}$ . Typical values for  $\alpha L_{\rm D}$  are  $\leq 1$  so that for planar PV structures, exciton diffusion is the limiting process.<sup>[3]</sup>

Bulk-heterojunction (BHJ) structures aim to decouple these two limiting efficiencies through the use of interpenetrating networks of donor and acceptor (shown schematically in Figure 4b), which enable the surface area of the dissociating interface to be dramatically increased. This effect manifests as an effective enhancement of  $L_{\rm D}$  which, in turn, enables the optimal device thickness to be increased as shown in Figure 5. However, as the interpenetration of the donor-acceptor network increases the pathways for charge collection become hindered, which is also a common limitation even in planar structures where  $\alpha L_{\rm C}$  can be <1. Indeed the mobility ( $\mu$ ) of organic semiconductors is generally quite low, in the range of  $10^{-7}$  cm<sup>2</sup> V<sup>-1</sup> s<sup>-1</sup>) to 10 cm<sup>2</sup> V<sup>-1</sup> s<sup>-1.[22]</sup> Thus, there is a sensitive interplay between high photocurrent generation and charge collection that requires careful morphology optimization. While solid state BHJ structures typically suffer from the hindered carrier transport, they nonetheless remain the highest-performing solid-state nano-PV cells to date. Alternative approaches to simultaneously increase  $\eta_{\rm ED}$  and  $\eta_{\rm CC}$  include 1) long-range ordering which can effectively increase both  $L_{\rm D}^{[23-25]}$  and charge mobility<sup>[22]</sup> or 2) molecular design of highly absorptive materials (with high values of  $\alpha$ ) or effective light trapping schemes to reduce the required thicknesses while maintaining high absorption efficiency.<sup>[26]</sup>

The energy-level offset at the bilayer junction interface impacts the open-circuit voltage. For such donor–acceptor organic cells, the maximum  $V_{OC}$  has been shown in several studies to be proportional to the "interface gap" as outlined in Figure 4, where the dark current is limited through charge recombination at the heterojunction interface due the energylevel offset at the junction.<sup>[27,28]</sup> Non-optimized electrode work functions can further reduce  $V_{OC}$  from this maximum by creating charge collection barriers that can result in a build-up of space charge.<sup>[29]</sup> For ohmic contacts, the maximum  $V_{OC}$  for bilayer organic cells can be expressed as<sup>[28]</sup>

$$V_{\rm OC}^{\rm Max} \le E_{\rm A}^{\rm LUMO} - E_{\rm D}^{\rm HOMO} - \Delta E_{\rm BE} \tag{7}$$

where  $E_{\rm A}^{\rm LUMO}$  is the acceptor lowest unoccupied molecular orbital (LUMO) energy,  $E_{\rm D}^{\rm HOMO}$  is the donor highest occupied molecular orbital (HOMO) energy, and  $\Delta E_{\rm BE}$  is the interface charge-transfer (CT) state binding energy. With optimized donor–acceptor energy levels, the interface gap is still ultimately constrained by the smaller of the optical gaps minus the binding energy. Accordingly, organic heterojunctions exhibit a wide range of photovoltages for various donor/acceptor combinations with similar optical gaps, as shown in Figure 1. For



**Figure 5.** a) Calculation of the *EQE* in the absence of singlet fission for donor-acceptor heterojunction as a function of the exciton diffusion length,  $L_D$ , absorption coefficient,  $\alpha$ , and carrier diffusion length  $L_C$  highlighting the exciton diffusion bottleneck. For the absorption efficiency ( $\eta_A$ ) the transmission to the active layers is taken as T = 75%, limiting the maximum *EQE*. b) Calculated *EQE* for Schottky diodes (or p-n junctions with optical transparent p (or n) region) in the absense of multiexciton generation as a function of depletion width *W*, absorption coefficient,  $\alpha$ , and carrier diffusion length,  $L_C$ .

the surveyed nano-PVs we find the photovoltage constrained to 80% of the SQ voltage, which is roughly equivalent to replacing  $E_{\rm G}$  in Equation 5 with  $E_{\rm G} - \Delta E_{\rm BE}$  and fitting the heuristic of  $\Delta E_{\rm BE} \approx 0.17 E_{\rm G}$ . Although polymer solar cells are similarly limited in photovoltage by Equation 7, reduction of this loss has recently led to  $V_{\rm OC}$ 's surpassing those of other nano-PV technologies.<sup>[30–32]</sup>

Certified power conversion efficiencies reaching 6% to 8% have already been reported for both vapor-deposited small molecule and polymer solution-processed cells with spectral responsivities from  $\lambda = 350$  nm to  $\lambda = 800$  nm.<sup>[33–37]</sup> Future improvements will need to focus on maintaining low interface recombination (i.e., through interface engineering), extending absorption deeper into the infrared while simultaneously maintaining the high photocurrents and charge



collection efficiencies already achieved in the best devices. Accordingly, this will require a combination of morphology optimization and material engineering of molecules with long diffusion length, high carrier mobilities, and smaller bandgaps. Indeed, engineering optical gaps in organic molecules into the infrared remains a significant challenge, one that may be overcome through the use of hybrid material systems such as organic/colloidal-quantum-dot or organic/nanotube<sup>[38,39]</sup> combinations. Stacked structures in which each stacked cell can be optimized for a different wavelength range may also be key to enabling efficient harvesting of light at longer wavelengths.<sup>[3,36,40,41]</sup>

#### 4.2. Dye-Sensitized Solar Cells (DSSC)

High efficiency, DSSC cells with certified  $\eta_{\rm p}$  = 11% have been demonstrated utilizing Rubased organic dyes with absorption from the UV to  $\lambda = 800$  nm (Figure 1,2).<sup>[34,42]</sup> These high power conversion efficiencies are largely attributable to near unity internal quantum efficiencies (IQE) and fill factors around 70%. DSSCs are a form of organic BHJ structure that have demonstrated nearly complete decoupling of exciton diffusion and absorption efficiency through the formation of an intercalated dissociating interface between a monolayer of dye molecules and a nanostructured acceptor layer. The high fill-factors stem from the replacement of molecular acceptors with a high electron-mobility inorganic semiconductor, typically a sintered mesoporous TiO<sub>2</sub>, along with a highly conductive liquid electrolyte to efficiently extract charges. Although little advance has been made in terms of increasing  $\eta_{\rm P}$  since the early reports, a number of different dye systems have approached this high level of performance (Figure 2).<sup>[43–45]</sup> Recent reviews of DSSC

PVs can be found in ref. [13] and [46]. Exploring the divergence of the demonstrated DSSC power conversion efficiencies from the calculated limits indicates that the shortfall in efficiency is mostly due to the low photovoltage. This low  $V_{OC}$  likely results from a combination of direct charge recombination from the TiO<sub>2</sub> to the triiodide redox mediator and the low conduction band energy of TiO<sub>2</sub>, or low interface gap, where Equation 7 is directly applicable to DSSC cells. Indeed, the observed  $V_{OC}$ values remain significantly lower than other organic–polymer cells of similar bandgap.

Operational stability may also be an issue in liquid-phase DSSC due to the volatile electrolyte. Recent efforts have therefore focused on the development of solid-state hole transport layers (HTL), with record efficiencies for these devices of around 5–6%.<sup>[47–52]</sup> In several of these cases direct substitution

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of the tri-iodide electrolyte solution for a solid state HTL typically reduced the efficiency by approximately two-fold due to reduction in the *FF* and  $J_{SC}$  and is suggestive of a need for higher mobility solid state HTLs in both DSSC and OPV structures. Again, tailoring organic dyes with absorption into the near-infrared (with1.1 eV bandgap) remains a challenge for improving DSSC efficiencies as well. Alternatively, DSSC devices with colloidal quantum dot light absorption centers with near infrared bandgaps could be viable in generating higher  $V_{OC}$ .<sup>[51,53–55]</sup>

### 4.3. Colloidal Quantum Dot PVs

CQDs are hybrid materials composed of nanocrystal cores of inorganic semiconductors, capped with (typically) organic ligands. The distinguishing feature of colloidal quantum dots is the finite nanocrystal size that leads to electronic confinement, tunable band structure, and improved processability as compared to their bulk semiconductor counterparts. CODs, compared to most small molecule and polymer semiconductors, exhibit very large effective dielectric constants. For example<sup>[56,57]</sup>  $\varepsilon_{\rm PbS} = 15-20$  (bulk PbS<sup>[58]</sup> = 170) and  $\varepsilon_{\rm PbSe} = 12-50$  (bulk PbSe<sup>[58]</sup> = 210) for ethylene-dithiol-capped PbS CQD. These large bulk dielectric constants lead to large effective Bohr radii (of between 10 and 20 nm) and hence make quantum confinement effects important in particles of this size. Confinement can impact the optical gap<sup>[59]</sup> which can be tuned over a range of meV to eV, providing a method to move through  $E_{\rm G}$ -space in Figure 1,2. The exciton binding energy, which is proportional<sup>[60]</sup> to  $1/\varepsilon^2$ , is therefore small (<*kT*), indicating that free-carrier and field-driven dissociation are typically dominant, at least within individual CQDs.<sup>[61]</sup> Therefore, in contrast to molecular, polymeric, and DSSC PVs, the CQD PVs do not require a heterojunction for carrier dissociation, but rather excitons can dissociate within the COD thin film bulk. Solution-deposited CQD Schottky diodes have recently been constructed with benzenediothiol (BDT)-capped-PbS CQDs exhibiting  $\eta_{\rm P} \approx 4\%$  and internal quantum efficiencies approaching 80%.<sup>[62]</sup> Metal oxide/ PbS-CQD n-p junctions have also been reported with  $\eta_{\rm P}$  = 5.7%<sup>[63]</sup> and >1000 hour lifetime.<sup>[64]</sup>

Without the bottleneck of exciton diffusion, CQD PVs are limited only by low light absorption efficiencies, low charge carrier mobility, and depletion widths that limit the optimal film thickness. The charge transport through CQD films is similar to organic semiconductors in that various forms of variablerange carrier hopping have been observed,<sup>[57]</sup> while charge carrier mobilities are similar in magnitude to the amorphous and crystalline organic layers.<sup>[65,66]</sup>

For Schottky diodes (or p–n junctions with an optically transparent wide-bandgap p-region) with CQD layer thickness of *d*, the external quantum efficiency is a function of both the efficiency of current generation in the depleted ( $\eta_{\text{Dr}}$ ) and quasineutral regions ( $\eta_{\text{Diff}}$ ) of the CQD film, where  $E QE = (\eta_{\text{Dr}} \eta_{\text{CT}} + \eta_{\text{Diff}} \eta_{\text{CT}})\eta_{\text{CC}}$ . For d < W (where W is the width of the charge depletion region),  $\eta_{\text{Diff}} = 0$ ,  $\eta_{\text{CC}} = 1$  due to drift collection, and  $\eta_{\text{Dr}} = T(1 - \exp(-\alpha d))$  where  $\eta_{\text{CT}}$  is the field-dependent charge dissociation efficiency, assumed to be 1 due to the small exciton binding energy. For d > W,  $\eta_{\text{Dr}} = T(1 - \exp(-\alpha W))$ ,

 $\eta_{\text{Diff}} = T(1 - \exp(-\alpha (d - W))) \exp(-\alpha W)$ , and the charge region<sup>[20,21]</sup> the collection through diffusion is  $\eta_{\rm CC} \approx \frac{L_{\rm C}}{d-W} \left(1 - \exp\left(-\frac{d-W}{L_{\rm C}}\right)\right)$ . The *EQE* is plotted in Figure 5b as a function of d/W for various values of  $\alpha W$  and  $L_{\rm C}/W$ . Photocurrent is primarily generated in the depletion region of width, W, where exciton dissociation and carrier drift are aided by the built-in potential. For large carrier collection efficiencies, current can also be contributed from the quasineutral region. Therefore, finding techniques to increase the carrier mobility of these films, for example by employing inorganic ligands,<sup>[67]</sup> decreasing inter-CQD spacing,<sup>[68]</sup> or employing superlattice ordering of CQDs,<sup>[61]</sup> could lead to larger optimal devices thicknesses and a near doubling of photocurrents over devices at the present state of the art. The near-IR response of CQD solar cells is currently limited by low absorption coefficients and low optimum thicknesses of the CQD layers. Additionally, the ability to control the doping levels<sup>[69]</sup> and tune the effective dielectric constants in capped CODs via ligand control can lead to enhanced depletion widths, which has already been shown to be critical in controlling the performance of CQD devices.<sup>[68]</sup>

# 5. Ultimate Performance of the Third-Generation PV Concepts

A number of architectures have been proposed for reducing losses in solar cells in order to overcome the SQ single-junction limit. These include hot carrier solar cells,<sup>[13,70]</sup> intermediate band solar cells,<sup>[13,71]</sup> up- and down-converters,<sup>[72]</sup> and concentrators,<sup>[13,73]</sup> as well as cells that utilize multiple-exciton generation,<sup>[6,74]</sup> exciton fission,<sup>[6,74]</sup> and tandem stacking.<sup>[11,13]</sup> While all of these approaches hold promise, this review focuses on the latter three, in which nanostructured materials are particularly relevant.

### 5.1. Multiple Exciton Generation in PVs

One approach for overcoming the SQ single-junction limit in CQD systems is through the use of multiple exciton generation (MEG). The MEG process is shown in Figure 3 whereby multiple carriers are generated from one hot-excited state. In quantum confined materials, it is suggested that the increased discretization of energy levels should lead to reduced carrier cooling rates, allowing MEG to become competitive with carrier relaxation.<sup>[59]</sup> MEG efficiency limits have recently been reviewed by Nozik, where theoretical maximum efficiencies with MEG ("infinite staircase") in the SQ limit were calculated to be  $\eta_{\rm P}$  = 44%, significantly exceeding the  $\eta_{\rm P}$  = 33% of the single-junction limit.<sup>[74]</sup> The onset threshold for ideal MEG occurs at  $nE_G$ , where is *n* is an integer multiplication number. Under AM1.5 illumination, PVs enhanced by the MEG process can add substantial additional photocurrent only when the PV photoactive layer has  $E_{\rm G}$  < 1.5eV. This can be seen in Figure 1,2 where we calculate the practical efficiency limit for the idealized "two-staircase" MEG (labeled "M2 MEG") and show that the practical efficiency limit increases from 17.1% for the single junction cell with no MEG to 21.8% for PVs enhanced by M2 MEG. To date, no PV efficiency improvements resulting in EQE > 100% have been

www.advmat.de reported, hence the benefit of the MEG enhancement in PVs has not yet been demonstrated. As the measurements of MEG processes are still evolving, we can assess the practical benefit of implementing the MEG process in PVs by comparing it to equivalent processes that have been extensively studied such as the impact ionization (or the reverse of the Auger recombination process), which to date has been demonstrated to be only weakly present in most bulk inorganic semiconductors.<sup>[75]</sup> Likewise, recent measurements show that the overall magnitude of MEG in CQD films is also limited, with onset thresholds and multiplication-profiles that are far from ideal<sup>[59,76-79]</sup> or overestimated due to charging effects.<sup>[80,81]</sup> Calculations show that if the MEG profile onset thresholds are less than M2 MEG, the expected achievable  $\eta_{\rm P}$  is nearly identical to that for PV cells without MEG.<sup>[74,78]</sup> Altogether, this limits the potential for  $\eta_{\rm P}$ 

5.2. Singlet Exciton Fission in PVs

process can be achieved for small gap materials.

The singlet exciton fission (SF) in organic semiconductors is a nearly equivalent analog of MEG in CQDs. In the SF process, one high energy singlet exciton at the band edge spontaneously separates to form two triplet excitons, each with  $\leq 1/2$ (singlet energy)  $\pm kT$ . While this process has been observed for a range of polyacene crystals,<sup>[82–85]</sup> the quantum mechanical mechanism has only recently been explored.<sup>[86]</sup> Ideal SF can result in a doubling of the photogenerated current at a given bandgap<sup>[87]</sup> and has been suggested as a method for slightly increasing multijunction PV efficiencies through improved current matching.<sup>[6,88]</sup> Moreover, it has been speculated that access to the triplet state could lead to enhanced diffusion lengths and bridge the gap between experimentally observed and theoretically predicted maximum photocurrents.<sup>[87,89]</sup> Although triplet diffusions lengths can sometimes exceed those of the singlet exciton,<sup>[24,25]</sup> triplet formation in the absence of singlet fission results in additional thermalization losses that lower the maximum efficiency below the practical limit calculated here. This is highlighted in a recent report of IQE > 100% for SF in a pentacene-C<sub>60</sub> and tetracene-C<sub>60</sub> bilayer architectures where overall EQE at zero bias and power efficiency still remain lower than other combinations of similar optical gap.<sup>[87,90]</sup>

enhancements through an MEG process, with the benefit of

MEG enhancement of PVs only present if nearly ideal MEG

The triplet states have negligible oscillator strength (even smaller than the MEG process) and there are rarely other optically absorptive states between the lowest singlet and triplet levels. Therefore, for our analysis  $E_G = E_S$  is used as the optical gap in Equation 3 to determine the photocurrent resulting from the absorbed incident light, while  $E_G = E_T = 1/2E_S$  is used in Equation 5 to determine the carrier level or  $V_{OC}$  for spontaneous fission. In Figure 1,2 we refer to this case as "SF1". We note that while the ideal MEG process in CQD films acts similarly to stacking tandem PV cells (as discussed below), singlet fission in a single organic thin film layer does not. In the SF1 case the maximum achievable  $\eta_P$  is lower than for the single junction cells that do not exhibit singlet fission because the decrease in the open circuit voltage is more severe than the gain in the photocurrent (Figure 1). If the  $V_{OC}$  scaled exactly as



 $E_{\rm G}$  (i.e., without an offset) as assumed by Beard and Nozik, then the efficiency limit would be unchanged from the M1 case.<sup>[91]</sup>

An alternative device configuration utilizing SF in a PV is with a donor-acceptor pair consisting of an SF material with large bandgap that forms a junction with a non-SF material whose gap is half as large (vis, same as the triplet gap). This case, which we refer to as "SF2" in Figure 1,2, results in the same maximum  $\eta_P$  as the M2 MEG case. Additionally, this approach would require structured absorption in the lowgap material so that higher energy photons are preferentially absorbed only within the SF layer and not thermalized in the non-SF layer. The SF2 pairing would therefore be less compatible with BHJ and DSSC architectures<sup>[90,92]</sup> where such optical engineering becomes more challenging and would result in thermal losses approaching the M1 scenario. Figure 3 outlines both SF1 and SF2 schemes.

### 5.3. Tandem PVs

The tried method for simultaneously reducing thermalization and absorption losses is to stack multiple cells with varying bandgaps, so that each cell absorbs a different part of the solar spectrum. Indeed, this approach has led to record PV efficiencies of 42.3% with GaInP/GaInAs/Ge two-terminal, triple junction cells.<sup>[2]</sup> While tandem stacking of high efficiency inorganic cells is limited by epitaxial growth considerations (i.e., lattice matching) and can add substantial cost to PV fabrication, nanostructured materials do not have such restrictions. This makes tandem growth of nano-PVs feasible on arbitrary substrates and with arbitrary combinations of subcells, as already demonstrated for molecular PV structures.<sup>[93]</sup>

Tandem stacking of multiple cells requires matching the photocurrents (for series connection) or photovoltages (for parallel connection) of the stacked subcells (i.e., matching maximum power points). Series matching generally leads to higher efficiencies since cells in parallel are limited by the voltage of the lowest gap cell.<sup>[72]</sup> However, parallel tandem junctions can also exhibit better light-shading stability where the photovoltage is logarithmic with light intensity and therefore could be useful under highly variable illumination conditions.<sup>[94]</sup> Therefore, in contrast to the MEG and SF approaches, excess thermal energy in tandem structures can be utilized to build either current (in parallel integration) or voltage (in series stacking). Utilizing the assumptions of SQ, the maximum efficiency for series two-cell, three-cell, and infinite number of tandem cells are 43%, 48%, and 67%, respectively.<sup>[74]</sup> However, assuming a non-idealized PV performance (discussed before for the M1 case in Figure 2), we calculate a maximum practical laboratory power conversion efficiency of 24% for a stacked, current-matched, two-cell nano-PV tandem structure (compared to the predicted 43.4% in the SQ limit). This performance is slightly better than the maximum  $\eta_{\rm P}$  for M2 MEG or SF2.

While tandem architectures for small-molecule and polymer PVs have been demonstrated, full optimization of such structures will require subcells with responsivity deeper into the near IR (NIR). Accordingly, tandem PVs could be designed from a combination of CQD and organic containing subcells, where the infrared responsivity of CQD layers can complement



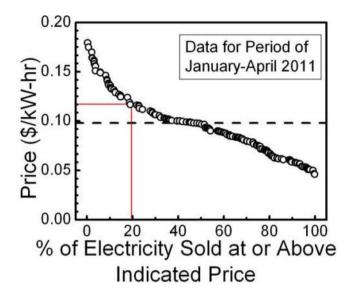
the visible spectrum response of organic layers, provided that future CQD subcells can be optimized for complete NIR absorption. We also note that tandem stacking of two or more identical PV cells (cells with the same  $E_{\rm G}$ ) can help in overcoming deleterious effects of series resistance that reduce  $FF.^{[95]}$  For a given light absorption, such a stacked geometry would reduce the active layer thicknesses of individual subcells, which would diminish exciton diffusion and charge collection losses, particularly for CQD devices with fixed depletion widths or organic materials with fixed exciton diffusion lengths.<sup>[36,96,97]</sup>

### 6. Projected Cost of Nano-PV Technologies

As the efficiencies of nanostructured solar cells advance toward the limits discussed above, the critical determinant of their commercial viability will be the levelized energy cost (LEC) of electricity they produce, in \$  $kW^{-1}$  h<sup>-1</sup>, relative to the incumbent means of energy production including electricity from fossil fuel power plants and from other PV technologies. The LEC is a suitable metric because it can readily be compared to the present-day costs of coal and gas-generated electricity. It also accounts for variable module lifetime, to be discussed in detail in the next section, as well as the balance of systems (BOS) costs.<sup>[98]</sup>

Presently, the PV contribution to USA electricity generation is less than 0.2%.<sup>[99]</sup> If the USA PV deployment continues to rise at the recently seen<sup>[100]</sup> 40% year-to-year growth rate, it would take 15 years for PV technologies to account for 20% of USA electricity production (note that at a slower, but still high, year-to-year growth rate of 25%, it would take over 20 years to reach 20% of USA electricity production). We set 20% as a target PV penetration in USA electricity production, since for the foreseeable future, inputs into the USA electrical grid from intermittent renewable energy sources, such as PVs, are expected to be limited to between 10% and 20% due to issues of grid stability.<sup>[101]</sup> Advancements of energy storage and "smartgrid" technologies would increase the allowable fraction of intermittent power sources on the electrical grid. Therefore, we expect that in the next two decades PV technology can aim to displace at most 20% of the non-renewable energy generation, with the biggest economic benefit provided when displacing the presently most expensive electrical energy. To estimate the LEC cost targets that need to be met, we plot in Figure 6 the cost of USA electricity across all sectors (residential, commercial, and industrial) integrated over kW h consumed.<sup>[102]</sup> The 20% of the most expensive electricity consumed in the USA cost more than  $0.12 \text{ kW}^{-1} \text{ h}^{-1}$ , setting this as a near-term target of the cost-competitive LEC for the nano-PV generated electricity. LEC of approximately \$0.05 kW<sup>-1</sup> h<sup>-1</sup> would be needed to compete with all modes of electricity generation across all sectors. We note that subsidies for oil and fossil fuel-based energy have been estimated to outnumber those for renewable sources of energy by roughly a factor of three.<sup>[103]</sup> A reversal in this trend could substantially shift the LEC competition point in a direction favorable for PV technologies.

To assess LEC sensitivity to lifetime, efficiency, and module cost, we estimate the LEC according to:<sup>[104,105]</sup>



**Figure 6.** Estimate of the fraction of electrical energy paid in the USA at or above a given price; data adapted from ref. [102]. The average end-use price is highlighted by the dashed line and the price point to fill the cost-liest 20% of USA electricity is highlighted by solid red lines.

$$LEC = \frac{ICC1000CRF}{CF8760} + O\&M$$
(8)

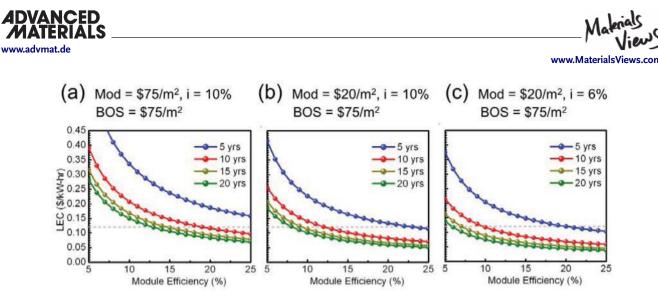
*ICC* is the installed capital cost (\$ $W_P^{-1}$ ) (where  $W_P$  refers to the watts of power generated under peak illumination conditions), defined as the sum of the module and BOS costs (\$ $m^{-2}$ ) divided by power ( $W m^{-2}$ ) produced; *CF* is the capacity factor, which takes into account considerations such as diurnal and seasonal variation in insolation, assumed to be 15.5% (e.g., Kansas City);<sup>[105,106]</sup> O&M are operations and maintenance costs, assumed to be 0.001 \$ $kW^{-1} h^{-1}$ .<sup>[104,107]</sup> Finally, CRF is the capital recovery factor:

$$CRF = \frac{i(i+1)^n}{i(i+1)^n - 1}$$
(9)

The interest rate (i) is assumed to be either 6% or 10% and n is the useful operating lifetime of the PV module system.

For reference, the module costs of OPV and DSSC modules have been previously estimated to be in the range of 20 to 40 \$ m<sup>-2</sup> and 45 to 120 \$ m<sup>-2</sup>, respectively.<sup>[106]</sup> BOS costs have been estimated for several types of module installation including ground-mounted systems (40 to 90 \$ m<sup>-2</sup>), commercial rooftop mounting with glass substrates/superstrates (75 to 135 \$ m<sup>-2</sup>), and rooftop systems with modules based on flexible laminates (54 to 99 \$ m<sup>-2</sup>).<sup>[106,107]</sup> These figures are based on the assumption that best practices for manufacturing and installation are similar to those of other thin film PV technologies (e.g., CdTe, copper indium gallium (di)selenide (CIGS), amorphous(a)-Si).<sup>[108]</sup>

In **Figure 7**a we consider a conservative scenario in which the nano-PV module cost is 75 \$  $m^{-2}$  and the rooftop-mounted BOS cost is also 75 \$  $m^{-2}$ . The LEC is calculated for such modules with lifetimes ranging from 5 to 20 years and with power conversion efficiency ranging from 5% to 25%. Additionally, we



**Figure 7.** Estimated levelized energy cost ( $kW^{-1} h^{-1}$ ) as a function of both module efficiency and lifetime for various cost scenarios: a) Scenario of an intermediate BOS cost (75  $m^{-2}$ ) (estimated for rooftop mounting) and a conservative module cost (75  $m^{-2}$ ). b) Scenario of lower-limit module cost (20  $m^{-2}$ ). c) Best-case scenario with lower-limit module costs and also a reduced financing rate (*i* = 6%). Note that a laboratory efficiency has to be scaled by roughly 0.75 to estimate the losses in scaling to a module efficiency.

consider in Figure 7b the impact of realizing the full low-cost potential of nano-PV by calculating the LEC assuming the lowest estimated module cost of 20 \$ m<sup>-2</sup>. Finally, Figure 7c shows the same calculations from Figure 7b, but with the interest rate lowered from i = 10% to i = 6% (the best-case cost scenario).

For each of the plots in Figure 7 we find that the LEC flattens out as the module efficiency or lifetime increases suggesting that the steepest gains in LEC occur with improvements of relatively low module efficiencies and lifetimes. For the most conservative assumptions of module and BOS cost utilized (Figure 7a), modules with lifetimes  $n \ge 15$  years and  $\eta_P \ge 15\%$ result in the cost-competitive LEC  $\leq 0.12$  \$ kW<sup>-1</sup> h<sup>-1</sup>, enabling their market penetration. By lowering the module cost from 75 \$ m<sup>-2</sup> to 20 \$ m<sup>-2</sup> (as in Figure 7b), nano-PVs can reach costcompetitive LEC with a 10 year lifetime and  $\eta_{\rm P} \ge 12\%$ , a power conversion efficiency achievable within the practical efficiency limits estimated above. Reduction in the financing interest (as in Figure 7c) would further reduce the requirements for nano-PVs with cost-competitive LEC to  $\eta_P \ge 10\%$  and 10 year lifetime. In this case, if nano-PV modules are realized close to our estimated practical efficiency limits and with lifetimes of between 10 and 20 years, LECs for M1 single and two-junction tandem cells of between 0.10 and 0.06 \$ kW<sup>-1</sup> h<sup>-1</sup> and between 0.07 and 0.04 \$ kW<sup>-1</sup> h<sup>-1</sup> are possible, respectively (we take the practical laboratory efficiency limits of 17% and 24% for singleand tandem-junction cells, respectively, and multiple by 0.75 to estimate the practical module efficiency limits).<sup>[109]</sup> Thus, the degree of market penetration will be highly dependent on the ability to fully realize the low-cost manufacturing of nano-PVs as well as advances in both efficiency and cell lifetime.

Manufacturing cost structures required to reach these LECs may be enabled by processing active layers with low-temperature vapor-phase or solution processing techniques, often employed in the fabrication of nano-PVs. While the ultimate and relative cost advantages of these two processing techniques remain unclear, the ability to process active layers at low temperatures and onto inexpensive flexible substrates should enable a reduction in the manufacturing as well as infrastructure costs. For example, flexible and light-weight PV modules will likely have a greater amenability to integration with existing infrastructure (building-integrated photovoltaics), which could significantly reduce the amount of dedicated framing/support required for installation. Such optimization and integration is expected to substantially lower BOS costs.<sup>[107,110]</sup>

## 7. Operating Lifetime of Nano PVs

The inherently nanostructured forms of DSSCs, molecular and polymeric organic PVs (OPVs), and CQD PVs can lead to instabilities in their operation under thermal and optical stress, which do not affect conventional monolithic inorganic PVs. For example, DSSCs could suffer electrolyte leakage under thermal expansion and bleaching or desorption of the photopactive dye;<sup>[111]</sup> OPVs could undergo morphological change to the active layer and photo-oxidation under environmental exposure;<sup>[112,113]</sup> and COD PVs are often subject to loss of ligands that passivate the QD surface and can undergo rapid oxidation of the semiconductor shell/core.<sup>[114]</sup> Additional degradation mechanisms include indium diffusion from the indium tin oxide (ITO) electrode<sup>[115]</sup> and delamination or oxidation of the low-work-function cathode.<sup>[116]</sup> Nonetheless, some of these challenges have already been overcome in the similar field of organic light-emitting diodes, where long lifetimes (>10 years)<sup>[117,118]</sup> have been demonstrated and commercialization is well underway.

Plots in Figure 7 shows us that in an assessment of a nano-PV technology in terms of \$ kW<sup>-1</sup> h<sup>-1</sup>, the useful lifetime of the device, typically reported as  $T_{80}$  (the time for the device to decay to 80% of its initial performance under standard operating conditions), is as important as the initial efficiency. Standardized conditions and procedures for lifetime testing are thus necessary for the effective comparison of different device architectures and encapsulation methods. A frequently employed accelerated lifetime testing method consists of a 1000 hour light soak under constant AM1.5G illumination (100 mW cm<sup>-2</sup>) and elevated temperature (50–60 °C) with continual monitoring of the photovoltaic operational parameters ( $J_{SC}$ ,  $V_{OC}$ , *FF*, and PCE).<sup>[111,119]</sup> This submits the device to roughly the same





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number of optical excitations experienced during  $\approx 0.5$  years of outdoor operation in North America, where the annual mean level of irradiance is  $\approx 5$  kW hr m<sup>-2</sup> d.<sup>[107]</sup> A representative collection of 1000-hour lifetime testing results for various nano-PV architectures is compiled in Table 2.

It should be noted that nano-PVs rarely undergo a simple linear decay<sup>[120]</sup> in the efficiency with time, but are often characterized by a "burn-in" period involving a relatively rapid increase or decay of the initial performance, followed by a period of slow, linear decay.<sup>[119,121]</sup> Because of O<sub>2</sub> and H<sub>2</sub>O sensitivity<sup>[120]</sup> of many of the active layers to deg-

radation, packaging technology will be crucial.<sup>[121]</sup> Accordingly, catastrophic failures in packaging may also rapidly degrade the performance at any point during the test. Given the unpredictable nature of device degradation, extended lifetime tests under conditions approximating those expected under normal operation, either in an outdoor environment or under repeated illumination and heating cycles, are particularly relevant. A sample of extended lifetime testing results for DSSCs and OPVs is compiled in Table 3 and indicates that, with effective encapsulation strategies, the lifetime of these nanostructured PVs can be relatively long. Toyoda et al. report a relative degradation of only 16% for a DSSC after 2.5 years of outdoor testing,<sup>[122]</sup> and Pfeiffer et al. observe no significant degradation of a 6% tandem OPV after 5000 hours of constant 1.5 sun illumination under open-circuit conditions.<sup>[95]</sup> Ultimately, addressing lifetime and efficiency simultaneously will be critical in determining the adequacy of nano-PV technologies for electricity production. Device efficiency and lifetime are not necessarily independent. Sensitivity to UV photons, for instance, may contribute to a slightly higher initial PV cell efficiency, but at the expense of a faster cell degradation.

Table 2. 1000 hour constant-illumination nanostructured PV testing.

Active material	Device architecture	Initial $\eta_{ m p}$ [%]	After 1000 h light soak [% of initial]	Temperature [°C]	Ref.
DSSC					
Z907	Polymer gel electrode	6.1	96	55	[169]
K77	Nonvolatile electrode	9	99	60	[170]
C103	Ionic liquid electrode	8.5	94	60	[171]
CYC-B11	Low-volatility liquid electrode	8.2	93	60	[172]
C217 (Ru-free)	Ionic liquid electrode	8.1	96	60	[173]
OPV					
P3HT:PCBM	BHJ (flexible)	3	85	65	[174]
ZnPc:C <sub>60</sub>	Planar heterojunction	2.8	84	50	[175]
ZnPc:C <sub>60</sub>	Tandem (same subcells)	4.1	100	50	[95]
QDPV					
РЬS	ZnO/PbS np heterojunction	3	95	20	[64]

Table 3. Extended nanostructured PV lifetime testing.

Material	Device architecture	Initial η <sub>p</sub> [%]	Duration [h]	Condition	After test [% of initial]	Ref.
DSSC						
N719	Ionic liquid electrode	-	22000	Outdoors	84	[122]
OPV						
P3HT:PCBM	Polymer BHJ	1	10000	Outdoors	103	[176]
P3HT:PCBM	Polymer BHJ	4.0	4400	Light soak	74	[121]
PCDTBT:PCBN	Л Polymer BHJ	5.5	4400	Light soak	69	[121]
Undisclosed	Small-molecule BHJ (tandem)	6.07	5000	Light soak	100	[36]

**Table 4.**  $CO_2$  emission factors (EF) for organic photovoltaic modules. Data adapted from ref. [36] where the embodied  $CO_2$  and energy input from module production is estimated to be 110 kg m<sup>-2</sup> and 2800 MJ m<sup>-2</sup>, respectively, and the average irradiance is taken to be 5 kW h m<sup>-2</sup> d.

Module efficiency	Lifetime [yr]	Generated power [kW h]	CO <sub>2</sub> EF [g CO <sub>2</sub> kW <sup>-1</sup> h <sup>-1</sup> ]	
5%	5	340	330	
5%	10	680	165	
10%	10	1360	83	
13%	20	3536	32	
18%	20	4896	23	
European Wall (2006)	-	_	411	

Beyond commercial viability, PV cell lifetime is acute in the lifecycle analysis and carbon footprint. To have any impact on reducing carbon emission, solar cells require lifetimes longer than the energy payback time; since the present PV cells will be produced by using electricity that is primarily generated through burning of the fossil fuels, the CO<sub>2</sub> emission factor of PVs is then inversely proportional to the cell lifetime and efficiency. For example, one recent study calcuated that the energy payback time is 4 and 2 years for a 5% and 10% OPV, respectively.<sup>[123]</sup> For a lifetime of 15 years, the carbon emission factors for 5% and 10% efficient modules are 110 and 55 kg CO<sub>2</sub> kW<sub>P</sub><sup>-1</sup>, respectively, which compares favorably to, for example, the average 2006 European electricity CO<sub>2</sub> emission factor of 400 kg CO<sub>2</sub> kW<sup>-1</sup> (Table 4).<sup>[123,124]</sup> A reduction in the lifetime to 5 years would significantly diminish the carbon footprint advantage of nano-PVs, particularly if  $\eta_{\rm P}$ remain below 10%. While the cell lifetime has only a small impact on overall cost for n > 10 years (Figure 7), extending lifetimes well beyond this range will have a significant role in the ability to produce and promote "clean" renewable energy. Nonetheless, with widespread adoption of solar and other renewable energy generation, carbon emission factors in PV production can be further reduced to approach near-zero carbon footprints.

# 8. Conclusions

We have reviewed the limits to the performance of molecular, organic, polymeric, dye-sensitized, and CQD-based solar cells.



We have considered the specific challenges associated with improving the power conversion efficiency of each and analyzed benefits of several approaches for reduced thermal losses beyond the single bandgap limit. Critical considerations related to the module lifetime and cost that are unique to nano-PV architectures have been quantified. While there may be substantial niche markets for low-cost and low-efficiency PV (i.e., point of source PV utilization), the scaling required to have a significant impact on energy markets will most likely be achieved through PV systems for grid power generation. Our analysis suggests that a practical single-junction laboratory PCE limit of 17% and a two-cell tandem PCE of 24% are achievable. When combined with operating lifetimes of 10 to 15 years, such performance could indeed position nano-PV cells as a transformational technology for solar energy markets.

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