PROPERTIES AND STRUCTURE OF VITREOUS SILICA. I

R. BRÜCKNER

Max-Planck Institut für Silikatforschung, Würzburg, Germany

Received 29 January 1970

This review is concerned with the properties and structure of silica glass. The following topics are treated:

Types of silica glasses;

The vitreous state of silica glasses: thermodynamical approach, atomistic approach;

Optical properties: absorption and fluorescence, refractive index and homogeneity;

Mechanical and thermal properties: specific volume, volume relaxation, volume and pressure, elastic and internal friction behaviour, heat capacity and heat conduction, strength, crystallization.

Introduction

The ability of silica to form a series of not less than 22 modifications¹) (not all are modifications in the strong crystallographic sense) from the nearly perfect crystalline quartz to the highly disordered amorphous silica-M, an amorphous phase formed by the action of high speed neutrons, and to the silica glass, is responsible for the great interest in the chemically simple substance SiO₂. Furthermore three main reasons are responsible for another great practical and theoretical interest in SiO₂, especially in that of silica glass: a) the excellent physical (mechanical, thermal and optical) properties simultaneously connected with excellent chemical resistance, b) the characteristic anomalies of silica glass in comparison to other glasses of mixed type, among these also is the group of silicate glasses, and other glass formers, and c) last but not least, is the significance of SiO₂ as the chief component of the wide variety class of silicate glasses.

It is beyond the scope of this article to present a complete stand of knowledge of the head-line topic, because this would demand a book-like scale. But it will be tried under this restriction to give a review with considerations and aspects on more recent developments in the termed field with befitting regard to the respectable precedent investigations.

1. Types of silica glasses

The increasing and different demands in the properties of silica glasses in

the last two decades required increasing effort in melting processes of silica. This development has not come to an end yet but is still in vigorous progress. To day we have to distinguish between different kinds of silica glasses with respect to properties and structure, there are about four types commercially available ²):

Type I – silica glasses are produced from natural quartz by electrical fusion under vacuum or under an inert gas atmosphere. They contain nearly no OH-groups (about 5 ppm or less) but relatively high metallic impurities of the order of 30–100 ppm Al and 4 ppm Na (all in weight fractions). Commercial names are Infrasil³), IR-Vitreosil⁴), G. E. 105, 201, 204⁵).

Type II – silica glasses are produced from quartz crystal powder by flame fusion (Verneuille-process). Because of the partial volatilization and the absence of any crucible material the metallic impurities are less than in type I silica glasses, but the atmosphere of the hydrogen-oxygen flame causes an OH-content of about 150–400 ppm. Trade names are Herasil, Homosil, Optosil³), O.G. Vitreosil⁴), G.E. 104⁵). A special thermal treatment in oxygen atmosphere, causing a good optical transparency in the ultraviolet range, leads to Ultrasil³) silica glass.

Type III – silica glasses are synthetic vitreous silicas produced by hydrolyzation of SiC1₄ when spraying into an oxygen-hydrogen flame. This material is practically free from metallic impurities, but contains a high amount of OH, in the order of 1000 ppm, and because of the starting material Cl in quantities of the order of 100 ppm. Trade names: Suprasil³), Spectrosil⁴), Corning 7940⁶).

Type IV – silica glasses are also synthetic vitreous silicas produced from SiCl₄ in a water vapour–free plasma flame. These silica glasses are similar to type III but contain only about 0.4 ppm OH and about 200 ppm Cl. Trade names: Suprasil W³), Spectrosil WF⁴), Corning 7943⁶). Another type was produced but only in a single case and on a laboratory scale⁶). The starting material was silicon of semiconductor-quality which was oxidized in pure oxygen high-frequency plasma flame. The impurity content, especially the OH-content, was extremely low.

The different types of silica glasses have different selective properties and therefore characteristic differences in their network fine structure. This fact and especially the numerous anomalous properties of silica glass at all will be considered in the following sections.

2. The vitreous state of silica glasses

2.1. THERMODYNAMICAL APPROACH

Silica has the ability to form a supercooled liquid by cooling down from

temperatures above the melting point of the high temperature modification of cristobalite and to freeze-in to a solid glass. In spite of the fact that the silicate glasses owe their ability of glass-forming mostly to the silica content, the properties of the silica glass itself differ widely from those of the silicate glasses, although silica is the chief component of all silicate glasses.

If one considers the typical behaviour of a common silicate glass as a function of temperature, it is evident, that for a glass-forming substance on cooling down the melt will undercool, freeze-in 9) and change to a glass measurable by a discontinuity in form of a crack of any thermodynamical property, the enthalpy H, the free energy F, or the volume V respectively, or in a break of the first differential quotient. This crack is neither a transformation point of a first nor such of a second order in the sence of Ehrenfest 8), but a transition, in the English terminology: a glass transition "point", $t_{\rm g}$. The characteristic difference between such a point and a second-order transformation point t_2 is given by the kinetic behaviour of these points. When a substance with a second-order transition point is quenched from high temperatures, that point will be shifted to lower temperatures in comparison to a slower cooling rate.

On the other hand the glass transition point will be shifted to higher temperatures by those two treatments (fig. 1). This is the typical behaviour which differentiates the group of glasses from other materials, especially from crystalline and possibly from most other amorphous materials 9)*.

In the case of silica glass we have to consider a first anomalous behaviour 11). The volume–temperature curve shows a minimum at a temperature of about $1500\,^{\circ}$ C in the structural (metastable) equilibrium of the (undercooled) melt 12) and also a minimum at about $-80\,^{\circ}$ C in the glassy state. The volume behaviour on quenching in the high-temperature branch of the equilibrium curve (above $1500\,^{\circ}$ C, see fig. 2) is the same as in the case of the common silicate glasses (fig. 1) but not measurable (because of crystallization and of too short relaxation times). In the anomalous region ($1000-1500\,^{\circ}$ C) the behaviour is different, especially if one considers the volume behaviour on reheating of a quenched sample (arrows in fig. 2). The volume shifts in the direction of the equilibrium curve are contrary to those of common silicate and other glasses (compare fig. 1): but the qualitatively similar behaviour is the direction of the temperature-shift of the glass transition "point" on quenching to higher temperatures with increasing quenching rate. Therefore vitreous silica is "really a glass".

For experimental determination, when the metastable structural equili-

^{*} It was tried theoretically to correlate these two points t_2 and t_g , and pointed out in ref. 10 that under the special case of very low cooling rates t_g may be considered as a t_2 -point and treated as that to a certain degree.

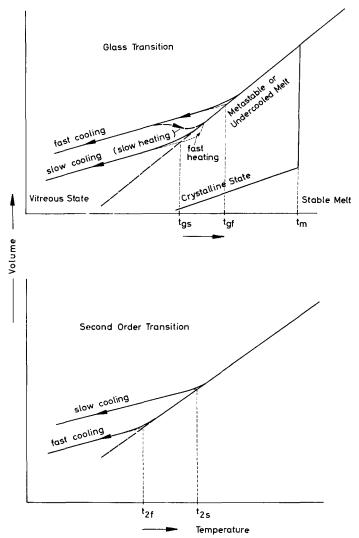


Fig. 1. Schematic diagram of volume-temperature plot for common glasses under various cooling rates in comparison to substances with a second-order transition. Here, $t_g = \text{glass}$ transition temperature; $t_2 = \text{second}$ order transformation temperature; f = fast, s = slow cooling rate; $t_m = \text{melting}$ or liquidus temperature.

brium curve of any substance expected to be a glass is not so easily available as in the case of typical glasses (because crystallization or decomposition might occur at temperatures above $t_{\rm g}$), the following method may be applied. The quenched sample is held at a constant temperature below the presumable $t_{\rm g}$ at which the volume relaxation times are experimentally desirable and at which the sample is not altered by crystalli-

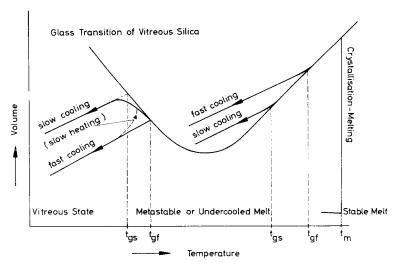


Fig. 2. Schematic diagram of volume-temperature plot for vitreous silica (types I and II). On the abscissa, $t_{\rm gs}$ means glass transition temperature for slow and $t_{\rm gf}$ for fast cooling. On the left side of the minimum, the cooling time may range from seconds ("fast" cooling) up to days ("slow" cooling), however, on the right side, they may be of the order of milliseconds (or shorter) for "fast" cooling, and one tenth of a second for "slow" cooling.

zation or decomposition, and the volume change is observed after different quenching rates. This procedure is repeated at several, or at least at two, temperatures. Two informations are obtained from those experiments: the sign and possibly also the amount of the slope of the metastable equilibrium curve and the shift of t_g with increasing quenching rate of the sample, and therefore the decision whether the material in question is a real glass or not.

2.2. Atomistic approach

As known from X-ray¹³⁻²⁰) and neutron diffraction ^{21,22}) of silica glass the structural unit consists, like that of most crystalline modifications of silica, of four oxygen atoms placed at the corners of a tetrahedron with a silicon atom at the center. This statement is well accepted by all authors, as well as the distances between Si-O (1.58 Å), O-O (2.6 Å), and Si-Si (3.2 Å) but not the arrangement of the tetrahedrons forming the cooperative structure.

The geometrical structure concept of oxide glasses at all are very closely related to those of the silica glass structure and may be divided into four groups.

Group I is due to the concept of the random network hypothesis originally stated by Zachariasen²³), X-ray proofed by Warren et al. $^{13-15}$), confirmed

and modified by a series of authors as Dietzel²⁴), Stevels^{25–27}), Sun²⁸) and Huggins²⁹).

Group II is based on the concept of the crystallite hypothesis by Lebedev³⁰), X-ray examined by Randall, Rooksby et al.¹⁸), Hartleif¹⁹) and modified by Porai-Koshits²⁰) and Botvinkin³¹).

Group III is based on the microheterogeneous structure concept first claimed by Dietzel^{24,51}) as "latent decomposition" in systems with an S-shaped liquidus curve, put forward by Vogel^{32–34}) and brought to a thermodynamic-statistical base of phase separation, nucleation and decomposition by Cahn^{35,36,38}), Hillig³⁷), Turnbull^{39,40}) and Charles⁴¹).

Group IV includes all those hypotheses which are based either on a special a priori-model as that of Tilton's 42) vitron model (pentagonal dode-cahedra), Robinson's 43) rod-like model and so on, or based on pure statistical models of certain partitition functions as put forward by Bell, Dean et al. 44,45).

Besides these geometrical pictures of glass structure, the more energetic structural concepts of oxide glasses are to be distinguished; they may be divided into two other groups.

Group V is characterized by the mixed binding concept of Smekal 46,47). In oxide glasses the mixed binding forces are of covalent and heterovalent character and in silica glass this mixture is about 50:50%. Similar statements were made by Grjotheim and Krogh-Moe 48) who postulated electronegativities around 2 ± 0.2 eV as a supposition for glass forming. Winter 49) suggested that the p-electrons should be responsible for glass forming. In addition to Smekal's concept a third kind of binding force is discussed by Noll 50), the double bonding between Si and O, so that three mixed binding forces, with almost equal proportions, are acting in silica.

Group VI is due to the concept of the field strength after Dietzel 24,51), based on the simple electrostatic Coulomb attraction force and due to the concept of the screening theory after Weyl 52,53). In both concepts the important factor is the polarization of anions and cations, which, as a first approximation, might be regarded as the covalent part of the mixed binding force concept.

To day, glass scientists tend to regard the groups I and II as ideal types or as limit models of possible glass structures and in this sense they are very helpful for the understanding of special kinds of behaviour of glasses. A better approach to the real glass structure gives group III when groups I and II are included, while group IV starts from a more formalistic point of view. All these geometrical concepts give no answer to the question: why is a substance able to go into the vitreous state? Interpretations were tried on account of the more or less polymeric overall network, that the undercooled

melt of substances of that kind has a high viscosity in the neighbourhood of the glass transition range and therefore nucleation and crystallization rates are very low. That means, that the glass forming process is a kinetic problem and therefore depends in principle only on the rate of quenching. But this is not a true interpretation, because it only shifts the problem from one property to another one.

In the author's opinion the energetic structural concepts are going back to deeper origins. While the field strength concept is concerned with the binding forces between cations and anions, the screening theory ⁵³), and also former considerations on the coordination tendency ⁵¹), consider the relations in and between the polyeders, and factors are to be regarded as the polarization, the coordination number and, in the case of multi-component glasses, the ratio of network forming to network modifying cations, trying to regard the whole cooperative problem of the structure of glasses.

Possibly a further step forward in the future will be made in a more definite way than was done by Smekal's mixed binding hypothesis (many non-glass-forming substances have also mixed binding forces) by the application of the hybrid-function concept, which was successfully applied to amorphous semiconductor materials and non-oxide glasses (chalcogenide glasses) by Krebs⁵⁴). While the former concept only claims a mixed bonding in general, the hybrid-function concept may give a more specified selection of glass-forming substances because one may get information on the directions of the covalent part of the binding forces and possibly on their distribution around the building units.

3. Optical properties

3.1. Absorption and fluorescence

The optical absorption behaviour of silica glasses is determined by impurities and defects in the structural arrangement in addition to transitions of the electrons of the bridging oxygens into the conduction band (uv-edge) and of the Si-O atomic resonance vibrations (infrared bands).

a) The ultraviolet-edge limits the transmission of an electromagnetic wave to the high frequency side by the interaction with the electrons of a material. This interaction will occur at higher frequencies for stronger bonded electrons. That means not only in the case of glasses will the uv-edge be shifted to shorter wavelengths, but this will also occur where higher binding strengths between the atoms and cations and a smaller amount of weak crystalline or amorphous network defects are. Therefore the most "perfect" silica glasses, regarded as especially "pure", like the type III and IV silica glasses, have the best transmittance properties [(fig. 3, see also b), next page].

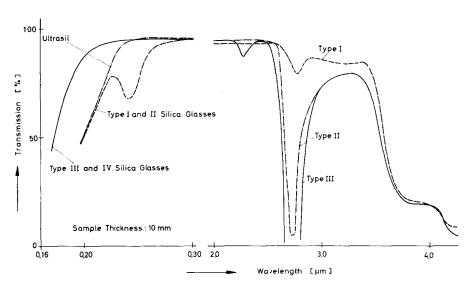


Fig. 3. Transmission curves as a function of wavelength 72).

b) The effect of *impurities* and *network imperfections* on the absorption of light is due to the energy loss produced by the so-called colour centers consisting of electrons and defect electrons, possibly forming a paramagnetic centre. Those centres give rise to absorption at definite frequencies of electromagnetic waves.

The absorption band near 0.240 μ m (fig. 3) observed in type I and II silica glasses only, corresponds to the fluorescence radiation at 0.280 and 0.390 μ m. Its origin is not yet totally clear but it may be contributed to both reduction and impurities, above all germanium and aluminium ^{55–58}). Partial reduction of SiO₂ to SiO_{2-x}, where x is of the order of 10^{-4.5} (ref. 56), especially at locations of impurity atoms, causes a weakening of the network bonding which means that the electrons at these centres are pushed into the conduction band and have lower energies than those of the network and therefore absorb lower energy of light.

Type III and IV silica glasses do not show the 0.240 µm absorption and the corresponding fluorescence radiation because they contain nearly no impurities, except hydroxyl groups. But the binding force of the proton is so strong that the energy of the electrons at the SiOH-centres will not be reduced in comparison to those of the perfect SiO₂-network. This is independent of the fact, that OH-groups weaken the glass network as a whole considerably (see sections 4.4. and 5.4.)

When silica glasses of type I and II are irradiated by X-rays, γ-rays or

neutrons they become as brown as smoky quartz and show three absorption bands near 0.220, 0.300 and 0.550 μm ; these bands are stronger for type I than for type II at comparable doses ^{59,60}). This is due to colour centres with adequate lower energy states of the corresponding electrons. These energy states depend on the type of the network imperfections especially caused by Al-centres damaged in different manners for which Stevels ⁶¹) gives special structural plausible interpretations, according to which the removal of an oxygen from the AlO₄-complex leaves behind a vacancy (0.550 μ m band) or is excited by radiation processes into an existing vacancy of a double Al-centre (0.300 μ m band). It is possible to heal the defect centres by heating the glass to moderate temperatures (\sim 400 °C); meanwhile definite luminescence glow curves are observed at 160, 215 (weak) 380 and 590 °K ⁶²⁻⁶⁴).

In irradiated silica glasses of type III and IV no visible colour effects occur, but only the $0.220\,\mu m$ absorption band is slightly shifted to $0.215\,\mu m$. The origin of this absorption is not clear, a certain connection with OH-groups is believed to be evident $^{59}, ^{60}$) by optical and ESR-measurements. Possibly it is due to an electron transition of a non-bridging oxygen into the conduction band. The corresponding electron transition of a bridging oxygen is due to an absorption below $0.180\,\mu m$.

- c) Going to longer wave lengths one observes the next absorption at 2.78 μm with higher combination vibrations or overtones at 2.4 and 2.2 μm , produced by the *oscillations of the OH-group*. As in other oxide glass formers (B₂O₃, GeO₂), only the free OH-group exists in silica glasses, contrary to the mixed silicate glasses in which also bonded OH-groups with more or less strong hydrogen bridges to other non-bridging oxygens exist corresponding to 3.6 and 4.2 μm absorption bands respectively 65,66).
- d) The Si-O oscillations produce absorptions at 9.0, 12.5 and 21 μ m in the infrared and at 12.5 μ m in the Raman-spectrum in the form of broad bands in comparison to quartz and cristobalite. The broadening effect is usual for all glasses and is the result of the amorphous structure giving rise to a broader distribution of the possible oscillations than in the ordered arrangements of the corresponding crystalline modifications. The 9.0 μ m band is associated with the antisymmetrical Si-O valency vibration (μ Si-O μ Si), the 21 μ m band with the bending vibration of Si-O-Si and O-Si-O respectively, and the 12.5 μ m band with the symmetrical Si-O valency vibration (μ Si-O-Si μ Si) which should be infrared inactive and which is the strongest Ramanline 67-69). Possibly anisometrical influences resulting from cooperative network deformations give rise to an antisymmetrical component of the symmetric pumping vibration at 12.5 μ m with an electric dipole moment.

With reference to thermal history, there was observed a slight but measurable shift of the $12.5 \mu m$ band in transmitting light to shorter wave lengths

with increasing density 70) as a function of fictive temperature (see section 4.1.); no shift of the other two bands was observed. On the other hand, also a shift of the 9.0 and 21 μ m band, but to longer wave lengths, was observed in reflecting light⁷¹).

A calculation of the force constants ⁶⁸) leads to a value of $K_{\rm Si-O} = 4.0 \times 10^5$ dyne/cm, which is higher in comparison to the GeO₂ and BeF₂-glasses by a factor of 1.2 and 3.6 respectively being in good agreement with calculated relative Coulombic binding forces.

3.2. Refractive index and homogeneity

The refractive index is shown in fig. 4^{72}) as a function of wavelength, from which the dispersion function may be obtained by differentiation.

There is a very slight difference (in the order of about 0.0002) between the

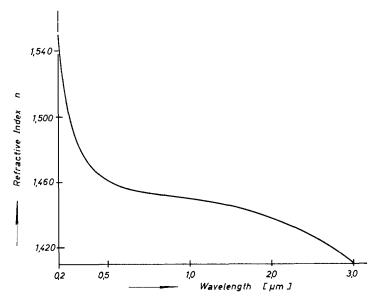


Fig. 4. Refractive index as a function of wavelength 72).

refractive index [and density⁷⁵)] of type III and type II silica glasses, the index of the natural silica glasses being the higher one. It is obvious that this difference is due to the water content, according to ref. 73, in contrast to mixed silicate glasses ⁷⁴) and to B_2O_3 glass ^{75,76}). This behaviour may be interpreted as follows: in silica glass only the free OH-group, without hydrogen bonding, is existent, whereas in mixed silicate glasses the existence of hydrogen bonding causes shrinkage in the glass network, which results in

an increase in the refractive index (and also in the density) ⁷⁴) with increasing OH-content*.

The temperature function of the refractive index n is connected to the thermal expansion coefficient α :

$$\frac{\mathrm{d}n}{\mathrm{d}T} = \frac{\partial n}{\partial T} + \frac{\partial n}{\partial \rho} \frac{\partial \varrho}{\partial T} = \frac{\partial n}{\partial T} - 3\alpha\varrho \frac{\partial n}{\partial \rho}, \qquad \varrho = \text{density}.$$

Usually the total temperature coefficient dn/dT is measured. For silica glasses this value is positive and of the order of 95 to 103×10^{-7} between 15

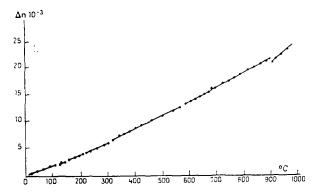


Fig. 5. Refractive index as a function of temperature 78).

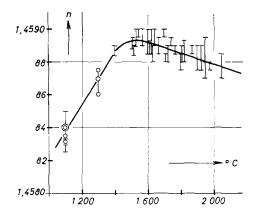


Fig. 6. Refractive index as a function of fictive temperature.

^{*} That the B_2O_3 -glass shows an increase of n with increasing water content although only free OH-groups are present as in the case of silica, is interpreted by local network contractions in the neighbourhood of free OH-groups caused by the lower valency and the flat arrangement of the BO_3 -group; if a B-O-bond is "broken" by one proton and an OH-group, the connection of B to the network is only two-fold leading to a closer contact of a BOH-group to the network and to a general contraction 77).

and 35°C. But for changes of optical lengths in optical arrangements not only dn/dT but also $\partial n/\partial T$ is of importance.

In fig. 5 the total temperature dependence of n is given for a type II silica glass. The discontinuities at 250 and 500 °C are regarded as a result of crystalline structural units⁷⁸).

As a function of thermal history, the refractive index shows a maximum as in the case of the density (see section 4.1.) at a fictive temperature of about $1500\,^{\circ}$ C (fig. 6)⁷⁵). The values are measured from water-quenched samples which were brought into structural equilibrium at the corresponding fictive temperature. Structural equilibrium means that no changes in n take place with time at constant fictive temperature. The scattering of measurements mainly arises from the birefringence of the quenched samples, caused by thermal stresses. This effect and also the discontinuities of n=n (T) are discussed later in connection with volume and diffusion.

Two kinds of optical inhomogeneities are observed in silica glasses: steady changes of the refractive index and the so-called grain structure. To day, qualities are produced with long range inhomogeneities of the order of

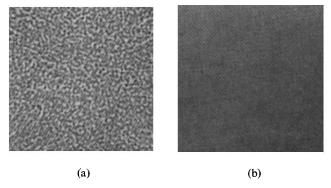


Fig. 7. Pin-hole pictures of Herasil (a) and Homosil sillica glass (b) 72)

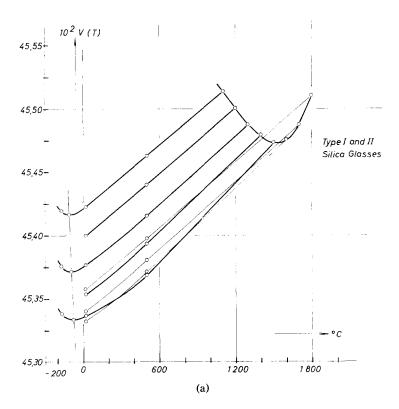
 $\Delta n = 2.5 \times 10^{-6}$ or better^{79,80}). Silica glasses which are not carefully homogenized (second and third class quality) show a grain structure (fig. 7) when observed with the pin hole method⁷²). This grain structure obviously is the result of an uncomplete melting process.

4. Mechanical and thermal properties

4.1. Specific volume

The principal volume-temperature behaviour was already described in section 2.1., fig. 2, but it should be shown in more detail with respect to two

groups of silica glasses, the type I and II (natural) and type III (synthetic silica glasses) respectively (figs. 8 and 9) 70, 75). Both groups differ distinctly and are well measurable in density at room temperature; both groups show the characteristic maximum corresponding to a fictive temperature of 1550 °C (type I/II glasses) and 1460 °C (type III glasses) respectively. But if one calculates the specific volume for the metastable equilibrium fictive temperatures with the help of thermal expansion measurements (see fig. 12), two qualitatively and quantitatively different structural equilibrium curves are obtained (figs. 8a and 8b). While the type I/II silica glasses show a minimum volume at 1550°C, the type III silica glasses do not show this; the "anomalous" volume branch from 1000 to 1500 °C is turned to a more "normal" branch with a very low positive volume-temperature coefficient. This coefficient is so small with respect to that of the glass, that at room temperature still an "anomalous" volume behaviour results (fig. 9). The high-temperature volume behaviour (fig. 8) is easy to understand if the action of the high OHcontent of the type III glasses is similar to that of the alkalioxides, because if one regards the OH-content as impurity, the type III glasses are more im-



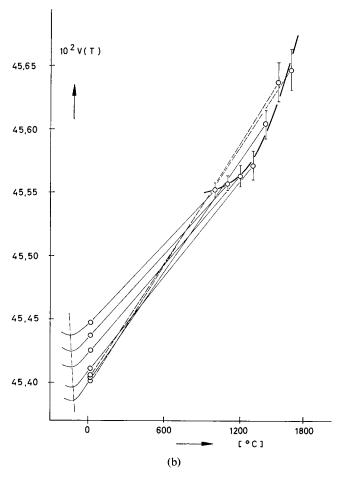


Fig. 8. Volume-temperature plot for type I/II (a) and for type III silica glasses (b) respectively.

pure than the type I/II silica glasses. Therefore, the behaviour of the "water"-rich silica glasses in fig. 8b may be regarded as a first step from the "classical" type I/II silica glasses in the direction of the common multi-component silicate glasses.

The volume-temperature behaviour in the metastable region of the silica melt is completed in fig. 10 by density measurements ⁸¹) in the stable melt at temperatures above the melting point of cristobalite. As it is seen from this figure the high temperature branch has a steeper slope than that found from the measurements in the metastable range below 1720 °C. The reason of this is, that at temperatures of about 1600 °C and above the volume relaxation times

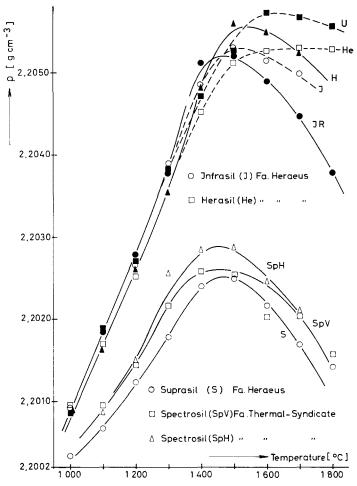


Fig. 9. Density, of different silica glasses of type I/II and III, as a function of fictive temperature. ● Vitreosil (JR) Fa. Thermal-Syndicate; ▲ Homosil (H) Fa. Heraeus; ■ Ultrasil (U) Fa. Heraeus.

become smaller than the quenching time of the samples* [concerning the method of these measurements in the metastable range it is referred to the original literature ⁷⁵)].

The volume-temperature behaviour in the glassy state is shown in fig. 11

* Within the scope of this review it only may be said that the metastable equilibrium curve of fig. 8 is obtained by keeping the (thin) samples as long, at constant temperatures, as a constant density is measured at room temperature after quenching into water. Corrections of the room temperature values to the fictive temperature were carried out by thermal expansion measurements (see below) of samples with the same thermal history (fictive temperatures).

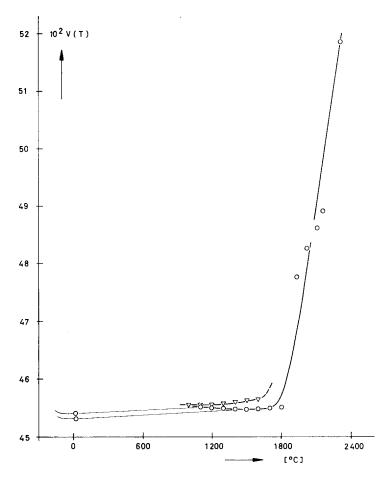


Fig. 10. Volume-temperature diagram including measurements ⁸¹) at temperatures above the melting point of cristobalite. ○ type I/II; ∇ type III silica glasses.

in the form of thermal expansion curves of type II silica glass samples of different fictive temperatures. Those samples with a fictive temperature corresponding to the minimum of the specific volume at 1550 °C or 1460 °C respectively have the highest thermal expansion, those of higher or lower fictive temperatures have a lower thermal expansion (fig. 12). This is in agreement with the Grüneisen relation:

$$\beta c_n/\alpha V = \text{constant}$$
,

where β =compressibility, c_v = specific heat, α =expansion coefficient and V=specific volume.

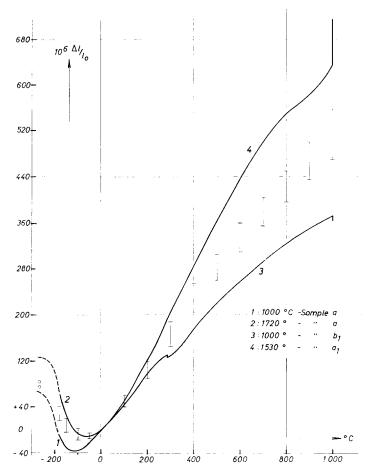


Fig. 11. Thermal expansion of silica glasses (type I/II) of different fictive temperatures. Vertical bars: range of older literature data; ○: values at 5°K after Keesom and Doborzynski⁸²).

In the low temperature range, below room temperature, another relation between fictive temperature and volume exists. A characteristic point is the low temperature minimum of the volume. It is shifted to higher temperatures with increasing fictive temperature, regardless of the high temperature volume minimum. There is a linear relationship between minimum temperature and fictive temperature within the limit of error (fig. 13). Again a difference between the group of natural and synthetic silica glasses is found. According to a lower high temperature minimum of the synthetic silica

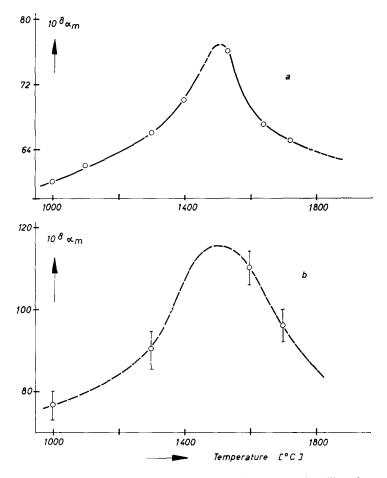


Fig. 12. Thermal expansion coefficient of type I/II (a), and III (b), silica glasses as a function of fictive temperature.

glasses, a lower low temperature minimum is found in comparison to the natural silica glasses.

The effect of low temperature negative thermal expansion of vitreous silica, as well as that of high-cristobalite and high-quartz, may be understood qualitatively with special regard to the transverse vibrations of the oxygen atoms and with the concept that the major contribution to the thermal behaviour is from transverse oxygen vibrations ⁸³), due to the openness of structure and the great freedom of transverse vibrations. It should be expected that most frequencies of the vibrations in an ionic crystal increase when the structure shrinks, because the ions have to move against the strong

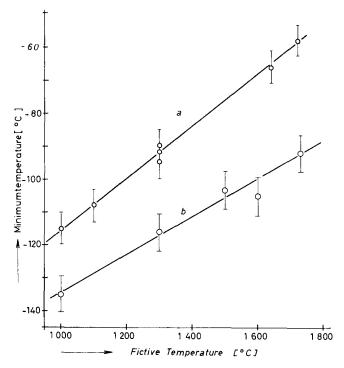


Fig. 13. Minimum temperature (range -135 to -60 °C) as a function of fictive temperature: (a) type I/II, (b) type III silica glasses.

repulsive forces of the approaching neighbours. If the structure permits one or more of the natural frequencies to decrease as the structure shrinks, there will be a possibility for negative expansion, and this seems to be the case for vitreous silica among other substances (Si, Zn S, and InSb), being not only connected to the vitreous state.

4.2. VOLUME RELAXATIONS

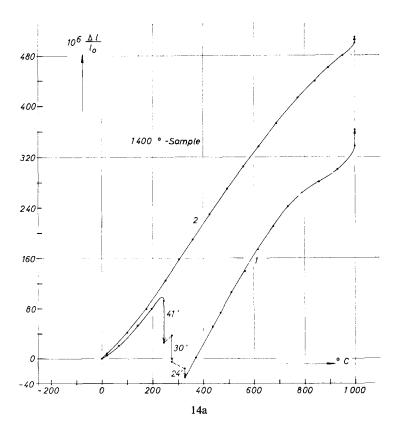
Three kinds of volume relaxation can be observed during the measurement of thermal expansion of heat-treated and quenched silica glass samples (fig. 14) 70,75).

a) At 1000°C the influence of the glass transition is perceivable, the sample tends to the metastable equilibrium curve as already shown in principle in fig. 1; in the example of fig. 14a a sample with a fictive temperature of 1400°C shows the same effect. The relaxation time at 1000°C is of the order of few hours, depending on the fictive temperature and accordingly on the "distance" from the metastable equilibrium curve. It is estimated that the

glass transition temperature is about 1100 °C for the group of natural silica glasses.

The group of artificial silica glasses has a lower glass transition temperature at about 1000 °C. This may be seen from fig. 14b as an example of a 1300 °C fictive temperature sample. The trend to the metastable equilibrium curve starts at 800 °C and at 1000 °C no isothermal volume change is detected within the time of measurement.

b) Between 750 and 950°C a tendency of volume contraction is observed in samples of natural silica glasses in the first expansion curve after quenching (fig. 14). The higher the fictive temperature the larger is this effect. The same is true for artificial silica glass at lower temperatures (500–700°C, fig. 14b). These contractions may be attributed to the relaxation of internal structural stresses produced by quenching, because these contractions almost disappeared in the second expansion curves. It is suggested that the relaxation process in this temperature range is partly connected with a healing process for "open bonds" and that during the first heating up chance



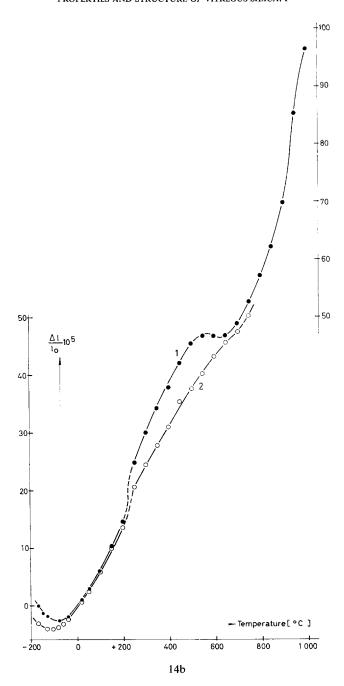


Fig. 14. Thermal expansion curves of type I/II (a), and type III silica glass (b), quenched from fictive temperatures of $1400\,^{\circ}\text{C}$ (a) and $1300\,^{\circ}\text{C}$ (b).

occasional linking of Si-O bonds by regroupings of SiO₄-tetrahedra occurs.

Accordingly, it should be pointed out that in silica glasses there is the possibility for compression stresses as well as for tension stresses in the outer part of a sample, and vice versa for the interior part. If a sample is quenched from temperatures above 1550°C, the usual permanent stress distribution is built up by the latter contraction of the interior rather than the outer part. This produces tension in the temperature range of possible flow in the interior, and a compressive stress in the outer part. But if a sample is quenched from below 1550°C in a not too rapid manner, the latter expansion of the interior part in comparison to the outer one (see fig. 2) produces, by flow in the corresponding temperature range of low enough viscosity, a compression stress in the interior and a tension stress in the outer part.

c) A third volume relaxation of quenched samples is found in the temperature range of 200–300 °C. The characterization of this volume change is the relatively large amount of change, the short relaxation time and the disappearance after reheating and slow cooling of the samples. There are two further characterizations, first, that these volume changes are only found in samples which were quenched from temperatures below 1550 °C, and secondly, that the natural silica glasses show a contraction whereas the artificial silica glasses show a dilatation (figs. 14a and 14b). Again the relaxation time is shorter for the latter than for the former, possibly due to the high OH-content. It is remarkable, that the relaxation times in this low temperature range are shorter than those at 1000 °C; for example, the mean relaxation times for a natural silica glass at 1000 °C are extensively larger than 1000 sec, whereas at 200–300 °C they are distinctly smaller than 1000 sec. The relaxation process is a very complicated one and cannot be described by only one mean relaxation time ⁷⁵).

Some indications predict that also at 500–600°C volume changes take place 75). Although this effect is small as compared to that at 200–300°C, however, it is not definite that the real effect is also small. This effect is only small in the sense of the sensibility of the thermal expansion measurements and of sample condition, because the volume relaxation at 500–600°C is only measurable after that at 200–300°C, which causes a decrease in the sensitivity for volume relaxation by a partly healing process in the form of a destruction of internal structural stress caused by transition processes 75,84).

An interpretation of the complex volume behaviour (sections 4.1 and 4.2) was attempted in the following manner ⁸⁴) with the help of temperature or density fluctuations and by the existence of preordered regions. Suppose, in the temperature range between the melting point of cristobalite and about $150\,^{\circ}$ C below the melting point these fluctuations lead to agglomerations of $SiO_{4/2}$ -tetrahedron fragments having properties very similar to those of the

corresponding crystalline phase. These heterophasic* fluctuations could be understood from a statistical point of view in the sense of "embryos" after Volmer and Weber⁸⁶), and Fischer, Hollomon and Turnbull⁸⁷), being very small and having a high degree of disorder so that by X-ray diffraction no crystallinity will be detectable.

With the help of the postulate of preordered regions the complex volume behaviour may be interpreted**.

- a) The branch of the negative thermal expansion (1550–1000 °C) may be connected to the negative expansion coefficient of cristobalite in this range; that means, the preordered regions are very similar to cristobalite. Above 1550 °C a "thermal decomposition" or a "premelting" of the preordered regions takes place and the volume temperature curve behaves normally. The "water"-content of the synthetic silica glasses causes a lower viscosity (see section 5.4.) and therefore a lower premelting temperature.
- b) The contractions of the natural silica glasses at 200–300 °C will be due to the volume shrinkage of the rapidly quenched preordered regions which will still have "high temperature modification" character and which have the chance, on slow heating during the measurement, to change to the "low-temperature modification". The observated volume expansion instead of a contraction in the synthetic silica glasses is attributed to the looser and more open structure and to the higher mobility of the tetrahedra caused by the "water"-content. Therefore the high-temperature preordered state will not be frozen in by quenching as in the case of the natural silica glasses and so a slight and rapid expansion occurs instead of a shrinkage.
- c) The negative expansion at low temperatures may be a result of a preferred oscillation of the bending (transverse) vibration mode opposed to longitudinal vibration modes 83) (see last paragraph of section 4.1). The shift in the minimum temperature region with thermal history (-135 to -60°C) seems to be connected to internal structural stresses caused by the quenching process and to the more or less open structure with a different degree of open bonds.

4.3. VOLUME AND PRESSURE

The effects of pressure on glasses can be divided into three categories. First, the applied pressure on the glass below the glass transition temperature

^{*} The concept "heterophasic" should be understood not in the classical thermodynamical sense, but in the sense of the statistical theories of fluctuations 85), where the one phase is the undercooled melt and the other one the preordered regions.

^{**} For a more detailed discussion it is referred to ref. 84.

[†] Instead of the expression "modification" it would be better to say "preordered state", or high- or low-temperature preordered state respectively; instead of transformation point: transition range etc. 84)

may be low enough for reversibility of the density to be guaranteed; this behaviour is characterized by the volume compressibility. The pressure range of reversibility is strongly dependent on the kind of the pressure cell in question or on the amount of applied shear ⁹⁴). The better the isostatic condition is realized the larger is the pressure range of volume reversibility (fig. 17). The best isostatic conditions are obtained by a silver chloride cell or by any liquid pressure cell.

Second, the applied pressure or the amount of the shear component is large enough to produce "irreversible" or "permanent" (with regard to low enough temperature) volume changes (densification) of glasses in the rigid state.

Third, the glass may be compressed at or above the glass transition temperature where the volume relaxation times are usually shorter. Here, large increase in density is possible under relative low applied pressures (below 10 kbar). Cooling under pressure makes the densification "permanent" if the end temperature is low enough.

a) The reversible volume changes may be expressed by the mean coefficient of compressibility 88,89):

$$\beta_{\rm m} = a(T) + b(T) p, \qquad \beta_{\rm m} = \frac{1}{V_0} \frac{V_0 - V_{\rm p}}{p - p_0},$$

$$a(T) = (26.43 - 0.0025 T) \times 10^{-7} \,\text{cm}^2/\text{kP},$$

$$b(T) = (43.6 - 0.080 T) \times 10^{-12} \,(\text{cm}^2/\text{kP})^2,$$

where T is in $^{\circ}$ C.

These data are valid in the temperature range of 22-260°C and in the pressure range of 0-3000 kg/cm². Up to 12 kbar no permanent volume

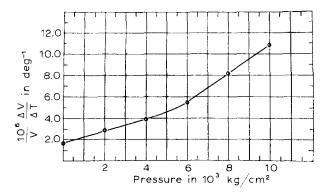


Fig. 15. Thermal expansion coefficient of silica glass between 11 and 390°C as a function of pressure calculated ⁹⁰) after compressibility measurements ⁹¹) in the reversible range of volume and pressure.

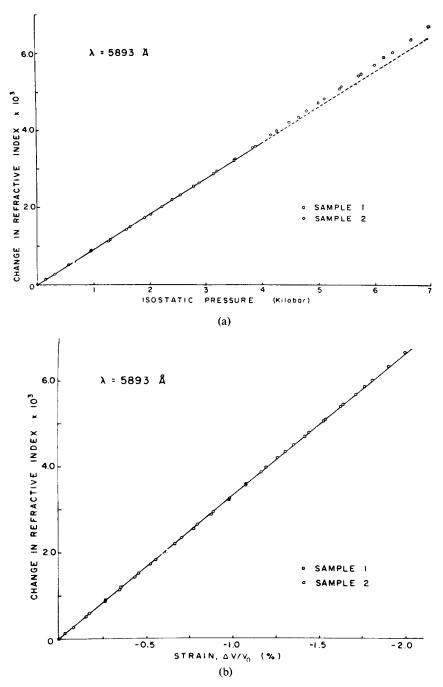


Fig. 16. Change of refractive index as a function of pressure (a) and strain (b) in the reversible volume-pressure range ⁹²).

change was detectable. As a result, vitreous silica is also unusual in its compressibility behaviour because its compressibility increases with pressure whereas that of quarts and most other substances decreases with pressure. Remarkable is also the decrease of the pressure dependency of β_m with increasing temperature. This gives rise to a marked increase in the thermal expansion coefficient with increasing pressure as is calculated and shown in fig. 15^{90} , 91).

It might be supposed that a normal negative pressure dependency will occur from a certain temperature upwards. Also, from a certain compression onward where the density of cristobalite is reached, a normal pressure dependence might be expected, because cristobalite, and also quartz, behave normal.

Further the actual strain produced in vitreous silica is higher than the value calculated from linear elasticity theory. Also, the change of refractive index, of vitreous silica, with pressure is nonlinear above 4 kbar (fig. 16a) 92) but exactly reversible. If the change of refractive index is plotted over the Lagrangian strain, linearity is obtained over the pressure range up to 7 kbar (fig. 16b). From this it follows in connection with Mueller's theory of photo

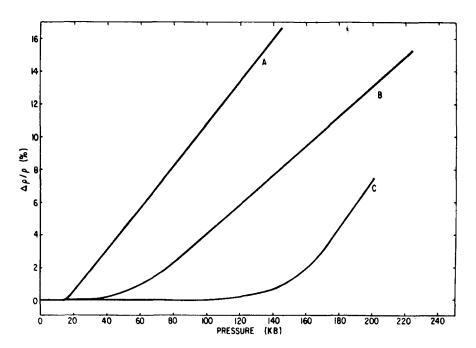


Fig. 17. Irreversible volume changes at room temperature caused by different types of pressure cells ⁹⁴). (A) high shear component ⁹⁵); (B) low shear ⁹⁶); (C) very low shear component ⁹⁷).

elasticity ⁹³), that the voids in vitreous silica are gradually being filled when the medium is elastically compressed. The most probable mechanism may be the gradual movement of some of the voids surrounding oxygen ions by a preferred displacement of the oxygen ions towards the voids in connection with the transverse optical vibration modes of the Si–O–Si bond^{101,102}).

b) At higher pressures, with more or less shear stress components, *irreversible volume changes* take place up to 15% densification even at room temperature (fig. 17). At higher temperatures the densification process is facilitated, for instance at 400°C a permanent volume change of 14% at a pressure of 80 kbar, of 4% at 60 kbar and no change at 40 kbar is observed in a silver chloride cell 94), whereas no change at 80 kbar pressure is obtained at room temperature. The mechanism of densification is mainly connected with "flow" under shear action (fig. 18) 94). First the material undergoes elastic shrinkage. At higher, not entirely isostatic pressure, rupture of some SiO bonds is produced. The compression in conjunction with a shear stress leads to an interlocking of two parts of the network; this can be attributed to variations in the mutual orientation of SiO₄ tetrahedra.

The densification process is influenced by the impurities of vitreous silica. At a constant pressure of 50 kbar at 500 and 600 °C, the densification increases in the following manner: Type IV (Suprasil W) \rightarrow type III (Suprasil) \rightarrow type I (Infrasil)⁹⁷). This behaviour may be attributed to the more open

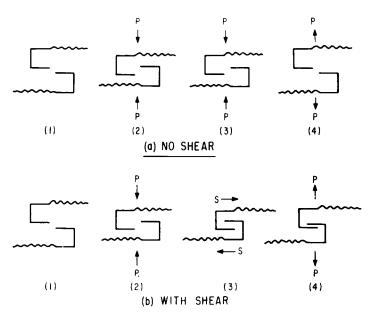


Fig. 18. Possible role of shear on densification of rigid glass (schematic) 94).

structure of Suprasil due to the high hydroxil content (1200 ppm) as compared with Suprasil W (250 ppm C1). However this does not hold for Infrasil. But, obviously, the higher content of metallic impurities, and the oxygen deficiency of Infrasil (240 nm absorption), may affect a densification much more strongly than do hydroxyl groups.

The annealing or the volume expansion with time at atmospheric pressure is a very complex process as shown in figs. 19 and 20 94). At the beginning of annealing, a rapid volume increase within a few minutes is observed. The higher the annealing temperature, the higher is this first volume increase. Later, the rate of volume change decreases markedly. The annealing process is dependent on the mechanical and thermal history. A densified sample, partly annealed at 500 °C, shows another annealing behaviour when further

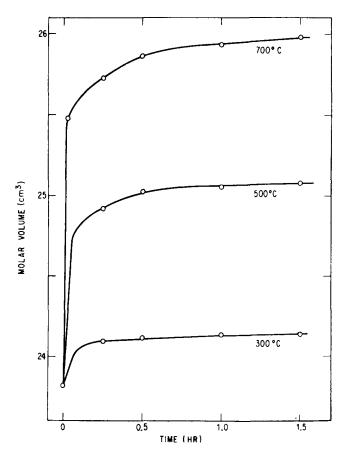


Fig. 19. Annealing of densified silica glass of $V_0 = 23.83$ cm³/mole at 300, 500 and 700 °C ⁹⁴).

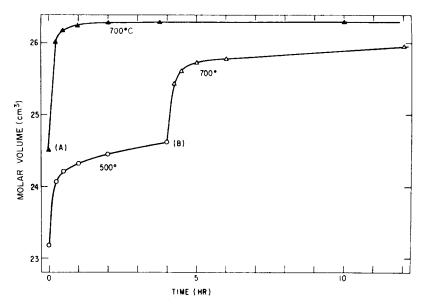


Fig. 20. Annealing of two specimens of densified silica glass. Effect of thermal history on initial annealing behaviour at A and B 94).

annealed at 700 °C as compared to a less densified sample which was not preannealed at 500 °C (fig. 20) in spite of the fact that the starting point is the same for both samples (A and B) before the treatment at 700 °C.

Usually, the rate of the first volume increase is the higher the larger the densification. The extent of internal deformations of the network under the applied high pressures is seen from the fact that at the surface of samples, with densities above 2.33 g/cm³, cristobalite is formed during annealing at a temperature as low as 500 °C.

An estimation of the activation energy of internal "flow" from initial slopes of the annealing curves gives surprisingly low values of 1–10 kcal/mole ⁹⁴). A further phenomenological treatment of the second part of the annealing curves by a mathematical formalism of a distribution (spectrum) of activation energies leads to somewhat higher values ranging from 34 to 76 kcal/mole with a sharp maximum at 41 kcal/mole and two broad maxima centred at about 54 and 70 kcal/mole ⁹⁸.) All values are considerably lower than the activation energies of viscous flow. Care must be taken of the physical significance of these data, but an indication may be given that the comparatively low activation energies can be interpreted as being mainly due to reorientations of SiO₄ tetrahedra with occasional linking of Si–O bonds taking place during annealing in contrary to real viscous flow.

Measurements of microhardness on densified silica glasses of type III at room temperature show interesting irregularities at those densifications (varying from 2.2021 to 2.567 g/cm³), corresponding to the densities of cristobalite, quartz, keatite and stishovite. Also the refractive index shows a similar relation to these modifications ⁹⁹). This fact is of interest with regard to the concept of preordered regions (section 4.2.). For still higher pressures (up to 120 kbar) and temperatures at which a transition to the crystalline modifications (quartz, coessite, stishovit) takes place, the reader is referred to Stöffler and Arndt ⁹⁹).

c) Densification near and above the glass transition temperature is already obtained at pressures as low as, for instance, 114 bar (fig. 21)¹¹). At a tempe-

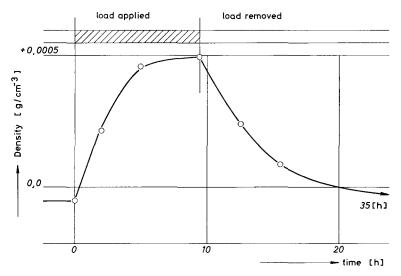


Fig. 21. Densification by a pressure of 114 atm. at $1080\,^{\circ}$ C and annealing of silica glass at $1080\,^{\circ}$ C¹¹).

rature of $1080\,^{\circ}$ C a densification of 5×10^{-4} g/cm³ is reached after 10 hr which can be frozen in by cooling under load. Relaxation of the compressed volume without load at the same temperature is maintained after nearly another 10 hr in the manner of a viscoelastic body.

If the annealing process of a silica glass densified above the glass transition temperature is made at temperatures below the glass transition temperature, the relaxation process is more complex and differs considerably from that of a glass densified below the glass transition temperature. The most significant difference of both densification mechanisms is the minimum annealing temperature at which isothermal volume flow is observed ¹⁰⁰). In table 1 a

Table 1					
Comparison of minimum temperature T_0 at which annealing is observed in 30 min for					
densified glasses ¹⁰⁰)					

	Glass transition temperature (°C)	Minimum temperature (°C)	
		In rigid state densified glass	In non-rigid state densified glass melt
B_2O_3	230	25	150
SiO ₂	1200	200	700

comparison between this minimum temperature is listed for densified SiO_2 and B_2O_3 -glass whereby the annealing time of 30 min is arbitrarily chosen.

In the case of silica densifications of $100 \Delta \varrho/\varrho = 3.71$ to 3.76 were measured at 1600 °C and 15 kbar, in the case of B_2O_3 a densification of 5.80 at 650 °C is obtained at 15 kbar and of 7.50 at 900 °C at a 20 kbar pressure¹⁰⁰).

For a structural consideration these results show that the amount of densification increases qualitatively with increasing free volume, viz. with increasing temperature, and further more, the densification process in the non-rigid state leaves far less open Si-O or B-O bonds than in the rigid state, because above the glass transition temperature the densification is accompanied by a real viscous flow, and during cooling under pressure, it is accompanied by a thermal healing process. Therefore the glass which is densified in the non-rigid state behaves more stable, below the glass transition temperature, than the rigid state densified glass.

4.4. ELASTIC AND INTERNAL FRICTION BEHAVIOUR

It is a well-known fact, that the elastic moduli also show anomalous behaviour in two points: the temperature coefficient and the coefficient of large longitudinal elastic strain (of fibers) of the elastic moduli are positive. The latter may be expressed by the experimentally determined expressions¹⁰³):

$$E = 7.33 (1 + 5.75 \varepsilon) \times 10^3 \text{ kg/mm}^2,$$

 $G = 3.21 (1 + 3.06 \varepsilon) \times 10^3 \text{ kg/mm}^2,$

were E is Young's modulus, G is the rigidity modulus and ε the elongation. This behaviour was not only measured on fibers but also on silica glass rods¹⁰⁴). This is a consequence of the positive pressure coefficient of the compressibility (see section 4.3a), viz. the equation

$$K = \frac{1}{\beta_{\rm m}} = \frac{1}{a + bp} \sim a - bp = \frac{E}{3(1 - 2v)},$$

where K is the bulk modulus and ν Poisson's ratio, holds for compression stress, that means E must increase with increasing tensile stress. Therefore it will be referred to section 4.3a for a discussion on this point.

Both, Young's and the shear modulus versus temperature are increasing in the temperature range -200 to $1000^{\circ}C^{105,106,108}$). Nearly linearity is found from 25 to $800^{\circ}C$. Near $60^{\circ}K$ the moduli have a minimum¹⁰⁷) accompanied by an internal friction peak in the neighbourhood of $35^{\circ}K$ at 50-100 kc/s. Above $60^{\circ}K$ together with the moduli (Young's and shear) also the Poisson's ratio increases continuously with increasing temperature.

The increase in Young's modulus is in a qualitative way most easily interpreted as being analogous to the case of rubber stretching^{104,108}). But also other interpretations were given, reducing the problem to the extreme low coefficient of expansion^{109,110}). Considering any modulus M as a function of volume V and temperature T, M = M(V, T), the total temperature dependence is given by

$$\frac{\mathrm{d}M}{\mathrm{d}T} = \alpha V \left(\frac{\partial M}{\partial V}\right)_T + \left(\frac{\partial M}{\partial T}\right)_V,$$

$$\alpha = \frac{1}{V} \left(\frac{\partial V}{\partial T}\right)_P = \text{coefficient of expansion}.$$

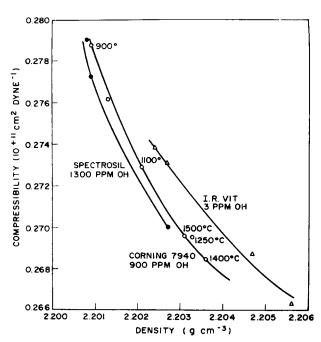


Fig. 22. Compressibility of three silica glasses as a function of density¹¹¹).

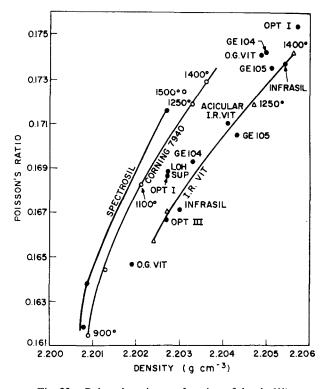


Fig. 23. Poisson's ratio as a function of density¹¹¹).

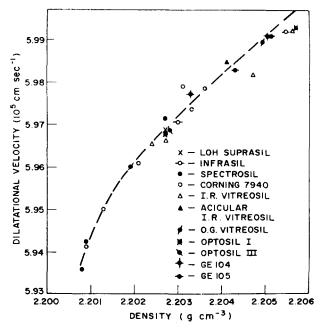


Fig. 24. Dilatational velocity as a function of density for various silica glasses 111).

It follows from this equation that the sign of dM/dT will be governed by the sign of $(\partial M/\partial T)_V$, if α is negligibly small. As well in the case of a Born-von Kármán solid as in the case of a Debye and Grüneisen solid it was shown^{109,110}), that dM/dT is negative at low temperature and large α , and positive at high temperature and small α . For the positive temperature coefficient of M of silica glass the small thermal expansion coefficient plays two important roles: first, the small value of α eliminates the always negative volume term $(\partial M/\partial V)_T$ and second, at small α the pure temperature term $(\partial M/\partial T)_V$ becomes positive from a moderate temperature upward.

As a function of density, produced by thermal history and "water"-content, elastic properties measured at room temperature at acoustic frequencies show the following behaviour. The shear velocity, the shear modulus and the compressibility decrease with increasing density, whereas the dilatational velocity, the Lamé parameter λ and Poisson's ratio increase with increasing density¹¹¹) (figs. 22–25). While the behaviour of compressibility, Poisson's ratio and Young's modulus (from dilatational velocity and from the density itself and from the Grüneisen equation: $\beta c_v = \text{const.} \times \alpha V$, and from the Lamé parameter λ) is immediately well understood, an interpretation of the behaviour of the shear velocity and shear modulus seems to

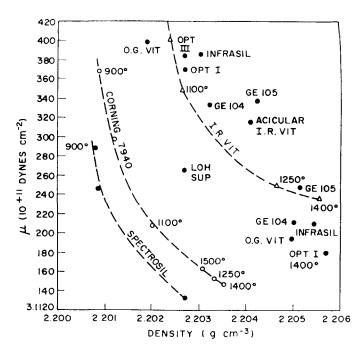
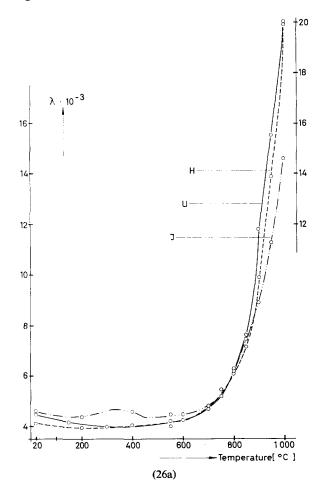


Fig. 25. Shear modulus (rigidity) as a function of density for a number of silica glasses 111).

be difficult, but it may be indicated that internal stresses in the quenched samples and open bonds or other kinds of inhomogeneities such as the preordered regions in the random glass network matrix section (4.2) may be responsible for the shear velocity dependence.

According to the general theory of dispersion any change of an energy-connected variable is related to an energy absorption peak. The deviation of Young's modulus from linear positive temperature dependency at 800 to 1000 °C is connected with an increase of internal friction measured at about 10 c/s in air (fig. 26)⁷⁰). In this temperature range the low temperature side of the glass-transition-internal-friction peak is noticeable. Structurally, this friction loss is related to the initial break-down of the polymer network from a rigid glassy state to an undercooled liquid metastable state. As in many other cases again a marked difference is found between the "water"-rich



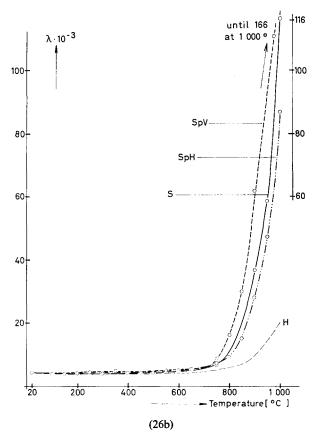


Fig. 26. Internal friction of type I/II and of type III silica glasses (b) as a function of temperature (fictive temperature = 1300°C). H = Homosil, U = Ultrasil, I = Infrasil (types I/II); S = Suprasil, SpV = Spectrosil, SPH = Spectrosil H (types III).

artifical and the "water"-poor natural silica glasses (type I/II). The higher "water"-content of the type III silica glasses causes a shift in the glass-transition temperature to lower temperatures. Here an example exists where silica glasses show a similar behaviour as multi-component silicate and other oxide glasses. The influence of OH-content on internal friction in the glass-transition range is closely connected to the viscosity (see section 5.4), which is lowered considerably by the incorporation of OH-groups.

At very low temperatures and high frequencies (ultrasonic, longitudinal waves in the kc/s and Mc/s range) another internal-friction peak is observed together with a minimum of rigidity^{107,112}). The peak and also the minimum of rigidity shift to higher temperatures with increasing frequencies (figs. 27

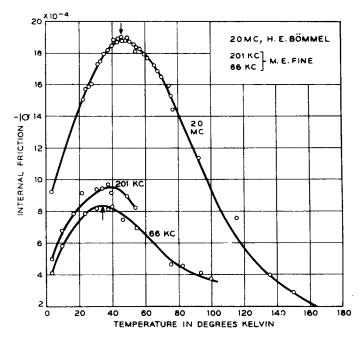


Fig. 27. Internal friction peak at low temperatures at different frequencies 112).

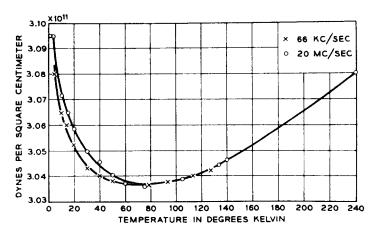


Fig. 28. Rigidity at low temperatures at different frequencies 107).

and 28) indicating that the mechanical losses are due to a relaxation mechanism. It has been demonstrated by analysis that a particular distribution of activation energies, each of which associated with a relaxation time would account for the shape of the experimental curves¹¹²). It is remarkable that the absorption does not occur in the corresponding crystalline quartz struc-

ture. The amount of the measured activation energy of 1.03 kcal/mole will be too small for an atomic diffusion process or for a molecular rotation, but too large for the absorption of a shear elastic wave. Therefore the losses are interpreted 112) as being due to Si–O–Si bond deformation vibrations of those oxygen atoms having alternative positions of equal energies. This hypothesis is confirmed by the successful extrapolation of the relaxation frequencies from the ultrasonic range at low temperatures (35 to 48 °K) to the Raman frequency of 30 cm⁻¹ at room temperature after the Eyring-type equation

$$\tau_0 = \frac{kT}{h} e^{-q/kT}$$
 with $q = 1.03$ kcal/mole.

Again, differences were observed between type I and type III silica glasses. The temperature of maximum ultrasonic loss is 43.5°K for an Infrasil "water"-free and 47.5°K for a Suprasil synthetic silica glass containing about 10³ ppm OH ions, both samples measured at a frequency of 20 Mc/s (longitudinal)¹¹³).

It could be confirmed by recent measurements and by an extend on other fundamental oxide glass formers like GeO_2 , B_2O_3 and $As_2O_3^{114}$), as well as sodium germanate glasses¹¹⁵), that the low temperature internal friction effect is attributed to a relaxation of transverse vibrating bridging oxygen atoms¹¹²) in spite of the fact that also a two-bond-length model, based on studies of fast neutron irradiated specimens of silica glass, involving a longitudinal motion of bridging oxygen atoms which have two stress-sensitive equivalent equilibrium positions, can explain the effect¹¹⁴).

4.5. HEAT CAPACITY AND HEAT CONDUCTION

According to the expression for the temperature dependency of specific heat

$$c_v = 3R \sum E_i(X_i),$$

in which E is the Einstein function

$$E(x) = x^2 e^x/(e^x - 1)^2$$
,

where

$$x = hv/kT = \theta/T,$$

h= Planck's constant, v= frequency of proper oscillation, k= Boltzmann's constant, R= gas constant and $\theta=$ Debye temperature, Smyth and coworkers ¹¹⁶) calculated the specific heat of vitreous silica and showed that best agreement with experimental values is obtained (fig. 29) if the following three characteristic temperatures are chosen: $\theta_s=1100\,^{\circ}$ K for each of the

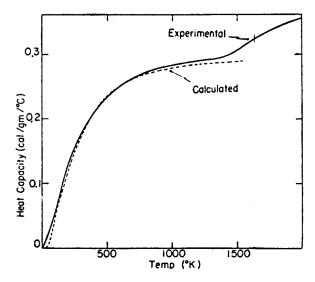


Fig. 29. Heat capacity of vitreous silica as a function of temperature. Solid line: measured 117); dashed line: calculated 116).

three silicium vibrations, $\theta_T = 370$ °K for each of the three transverse oxygen vibration modes, and $\theta_L = 1220$ °K for each of the two longitudinal oxygen oscillations; the θ_i correspond to vibrations in the infrared range of 23×10^{12} , 7.7×10^{12} and 25.4×10^{12} c/s.

The experimental data in fig. 29, composed by Sosman¹¹⁷), show a discontinuity at about 1100 °C. It is remarkable that not all authors have measured this increase. Possibly, this increase of the heat content is of structural origin and may depend on thermal history, because in this temperature range the glass transition of silica takes place. Similar to the increase of the heat content at the transformation of a crystal to its melt, also an increase may be expected, when a glass is heated across the transition temperature, which is called the "regrouping" heat by some authors¹¹⁸), because endotherm peaks in differential thermoanalysis of some glasses were measured.

It is of further interest to note, that an excess specific heat of vitreous silica exists at very low temperatures 119), whereas no such excess is observable in quartz and other crystalline substances. This excess heat is the difference between C_v measured, and C_v calculated from the Debye temperature and the elastic constants:

$$\begin{split} C_{v(\text{excess})} &= C_{v(\text{meas.})} - C_{v(\text{calc.})} \\ &= C_{v(\text{meas.})} - \text{SD}\left(\frac{\theta_{(\text{elastic})}}{T}\right), \\ C_{v(\text{meas.})} &\sim 2 \text{ to } 5 \times C_{v(\text{calc.})}, \end{split}$$

where

$$\theta_{(\text{elastic})} = \frac{h}{k} \left(\frac{n}{4\pi V_{\text{c}}} \right)^{\frac{1}{3}} c_{\text{m}},$$

h= Planck's constant, k= Boltzmann's constant, $c_{\rm m}=$ mean sound velocity determined from the density and the elastic constants, n= number of degrees of freedom per cell for lattice vibrations, $V_{\rm c}=$ volume per cell, $D(\theta/T)$ is the Debye formula and S=3R for Si-O-Si, or $S=\frac{9}{4}$ R for the SiO₄ tetrahedron as a vibrational unit. Although no exact explanation can be given for the excess specific heat at temperatures below 20 °K, especially below 5 °K, it is important that, in a qualitative way [inconsistent with lattice dynamics 120)], a model in which the Si-O-Si bending vibrations can be made responsible for all the low-temperature specific heat 1119) and that all of the frequencies required to account for this heat capacity are to be found in the region of optical modes of very low frequencies with an intense continuum extending from 560 cm⁻¹ down to 8 cm⁻¹ as can be shown directly by the Raman spectrum and the Brillouin scattering spectra of silica glass 121, 122).

A characteristic difference between the vitreous and crystalline state is evident through the temperature dependence of heat-conduction (fig. 30).

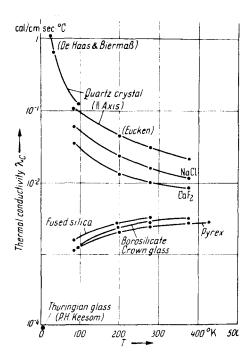


Fig. 30. Thermal conductivity in crystalline and glassy materials 123'124).

In analogy with the photons in optical energy transport, the conception of the phonons (high frequency thermoelastic lattice waves), with certain mean free paths, proved important in heat conduction problems (phonon conduction). The longer the mean free path l, the higher the thermal conductivity $\lambda_{\rm th}$:

$$\lambda_{\rm th} = \frac{1}{3} cvl$$
, $q = -\lambda_{\rm th} \Delta T/\Delta x$,

where c is the heat capacity per unit volume, v the average sound velocity, q the rate of heat transfer through a unit area per unit time, and Δx the space between the temperature drop ΔT . According to the regular atomic arrangements in crystal layers the crystals have large l-values at low temperatures and therefore a great λ_{th} . The lack of periodicity and symmetry of a lattice in glasses causes large interchange energies between thermoelastic waves such that the mean free path, l is short. It is stated¹²⁵) that in case of glasses l is constant, independent of temperature, except for long wave lengths at low temperatures. Therefore λ_{th} is widely proportional to the specific heat at most temperatures. This is shown for silica glass in fig. 31¹²⁶) for tempe-

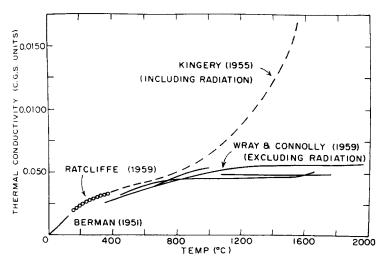


Fig. 31. Thermal conductivity of silica glass at high temperatures ¹²⁶).

ratures above room temperature. Here, the radiation conductivity (photon conduction)

$$\lambda_{\rm r} = \frac{16\sigma n^2 T^3}{3\kappa},$$

(σ =Stefan-Boltzmann constant, n=refractive index, and κ =absorption coefficient) is eliminated (difference between dashed and solid line)¹²⁷).

The proportionality between $\lambda_{\rm th}$ and c_v is valid to temperatures as low as liquid-oxygen temperature. At lower temperatures the conductivity decreases more slowly corresponding to an increase in mean free path of the low-frequency thermal waves. In general this is plausible because the disorder of the silica network becomes less important for longer wave lengths. But a more sensitive analysis at temperatures below 20°K have led to difficulties in interpreting the higher values and the "knee" in the thermal conductivity curve around 10°K (fig. 32). These were overcome by assuming a much

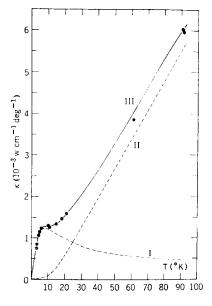


Fig. 32. Thermal conductivity of silica glass at very low temperatures, calculated (curves I, II, III)¹²⁵) and measured¹³⁰). Explanations see text.

longer mean free path for the longitudinal than for the transverse waves^{129,130}): At high frequencies and temperatures, a strong interaction between the two polarization branches, by means of three-phonon processes, result in an effective mean free path of the longitudinal waves, which is nearly the same as that of the transverse waves. This results in a conductivity, given by curve II of fig. 32. At lower frequencies the three-phonon processes are not sufficiently numerous to tie the mean free path of both, longitudinal and transversal, waves. This leads to completely uncoupled longitudinal waves with lengths very much longer than those of the transverse waves,

giving rise to an additional conductivity proportional to T in the range of 0-5°K. Above this temperature the partial coupling causes a decrease (curve I) and the superposition leads to the measured "knee" of the total conductivity (curve III). As in some foregoing sections (4.1 and 4.4), it is remarkable that the available experimental data cannot be explained without the assumption that very low frequency waves exist in both the optical and the acoustical branch.

Besides thermal fluctuations, also defects and voids with low-frequency mechanical resonances are to be considered giving rise to spin-"lattice" interactions and relaxations, and to unusual scattering of phonons which influence the short mean free path especially of the transverse phonons¹³¹). Therefore, a dependence of thermal conductivity, on thermal history and on type I/II as well as on type III silica glasses, is to be expected, and possibly vice versa, from that information on the structural defects.

4.6. STRENGTH

The expression "strength" usually refers to the tensile or bending strength of a material. It is obvious that this property depends on the weakest part of the material and this is mainly the surface, because the surface will be attacked chemically or mechanically. Surface flaws are usually cracks. A glass surface, which was thoroughly fire-polished or etched by hydrofluoric acid, should be free of cracks and should have theoretically maximum tensile fracture strength of $\frac{1}{5}$ of Young's modulus. In the case of silica, this means a strength of about 1.43×10^3 kP/mm², or taking into consideration the relation $E = E_0 (1 + \alpha \epsilon)$ from section 4.4, the intrinsic cohesive strength of vitreous silica is expected to exceed 2.25×10^3 kP/mm². The highest observed strengths reported for silica glass fibers are: 1.5 and 1.6×10^3 kP/mm² 132 , 133); the highest strength observed for bulk vitreous silica at 78 °K is 1.38×10^3 kP/mm² 104).

The slightest mechanical damage, such as produced by touching the sample with dirty fingers, causes a serious weakening. Therefore, the usual values are around 600 kP/mm². The causes of surface damage are studied extensively and described in refs. 104 and 134. Here, only very briefly, should be listed the different types of strength lowering effects: cracks, crystallization, condensation and adsorption of fluids (especially water) and gases, stress corrosion, "static fatigue", and volume fluctuations.

It seems, that a fluctuation process is a practical barrier in achieving the ultimate strength experimentally. But it was shown¹⁰⁴), that at a temperature of 78 °K the fluctuations are unimportant and that further lowering of the temperature causes no apparent increase in ultimate strength. It can be concluded that the volume fluctuation processes are the reason why the

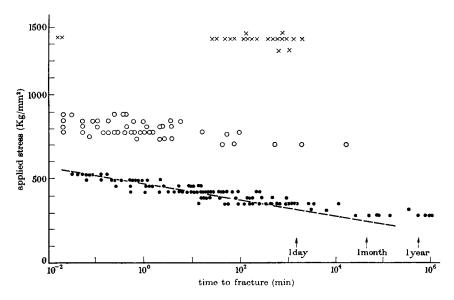


Fig. 33. Tensile strength and static fatigue of silica glass fibers at room temperature in air (\blacksquare) and in vacuo (\bigcirc), and at -196 °C in vacuo (\times)¹³³).

strength of silica glass increases with decreasing, and not with increasing, temperature as it could be expected according to the increase in Young's modulus.

Fig. 33 shows the features of the two main reasons of static fatigue of carefully prepared silica glass fibers (20 to 40 μ m, drawn from a 1 mm diameter Vitreosil rod, i.e. type I silica-glass)¹³³); in vacuo at 78 °K nearly no fatigue is observed, in vacuo at room temperature only about half of the strength at 78 °C is observed, and fatigue is measured (fluctuation processes), and in air at room temperature, the strength is about $\frac{1}{3}$ that at 78 °K and a stronger fatigue than in vacuo is observed (stress corrosion by water vapour)¹³⁴).

Regarding the ultimate strengths (at $78\,^{\circ}$ K) of silica glass $rods^{104}$) ($1.38 \times 10^3 \text{ kP/mm}^2$) and silica glass fibers^{132,133}) ($1.5 \times 10^3 \text{ and } 1.6 \times 10^3 \text{ kP/mm}^2$), one might come to the conclusion, that the strength will be practically equal in both cases and the small difference will be due to the greater probability to get a flawless piece of silica glass in the case of fibers. But, if one compares the measurements at room temperature in air, not only between different author groups^{104,132,133}), but also among one and the same team¹³³), a similar difference is found between the strength of about 1 mm rods (580 for the ultimate and 520 kP/mm² for the most probable strength) and the strength of fibers (710 for the ultimate and 620 kP/mm² for the most probable

strength) in spite of the fact, that the air condition reduces the strength, as compared to vacuo and low temperatures, far more by surface attack and fluctuations than the indicated differences. This fact should give rise to the conclusion that the structure of a drawn fiber is different from that of the bulk glass. This seems to be confirmed in the literature on glass fibers of multi-component composition*, although, partly very inconsistent conclusions, and experimental suppositions, yet fiber drawing conditions and results were found. An analysis of the possible silica glass fiber structure was pointed out¹⁴⁰) which led to a model as pictured in fig. 34. This figure does

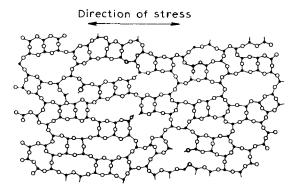


Fig. 34. Possible structure of silica glass fibers in regions of no preordered habitus.

not show the whole structure but that part of the deformed fluid-like structure without the preordered regions of section 4.2. It will be noted that there are three characteristic points differing from the isotropic structure: first, preferred orientation of silicon tetrahedra rows (double "chain-like") and deformation of the free volume in the drawing direction (arrow); second, the tetrahedra are distorted, slightly stretched in the drawing direction and slightly contracted perpendicular to it; third, the "broken" or "open" bonds may be partly of thermal and partly of mechanical origin. This picture is based on the anisotropy of silica glass fibers, of refractive index (birefringence $\Delta n \sim 270$ nm/cm of 12 μ m fibers), of density, of infrared absorption bands and of oriented crystallization (section 4.7).

4.7. CRYSTALLIZATION

Vitreous silica is one of the few interesting oxide glasses in which the composition of the crystalline phase is the same as the glass. Heterogeneous

* It is outside the scope of this article to consider that literature; the reader will be directed to refs. 108, 135–139, where also further literature will be cited.

168 r. brückner

crystallization seems to be the only method to transform pure silica glass into cristobalite as the only modification. The heterogeneities are either surface or impurity centres.

Even under very pure furnace conditions, very pure vitreous silica crystallizes in the surface at, and above, $1100\,^{\circ}\text{C}$ after sufficient long time. Measurable differences are to be expected between different silica glasses. It is also expected that the crystallization from the surface obeys a reaction law of zero order, i.e. the growth rate is constant (linear kinetics), and that the "water"-rich silica glasses will crystallize faster than type I/II silica glasses from the surface, whereas the latter will also crystallize from impurity centres if these are of sufficient concentration.

This concept holds true without one exception: the type I silica glasses ("water"-poor, electrically melted) have diffusion-controlled growth kinetics in both water vapour and in oxygen atmospheres $^{141-143}$). It is evident, that this behaviour is determined by oxygen deficiency and by the absence of structurally-combined water in this silica glass, i.e. in type I (SiO_{2-x}, where x is of the order of $10^{-4.5}$) 56), and that the growth mechanism is controlled by diffusion of oxygen bearing species too, and by the activation at the glass-crystal interface 142). The observed growth rates at 1460 °C in a 478 mm water vapour atmosphere are: $0.98 \, \mu \text{m/min}$ for type III, and $132 \, \mu \text{m}^2/\text{min}$ for an oxygen-deficient (SiO_{2-x}) silica glass which was prepared from type III by de-watering and melting with 70 ppm of silicon (the x-value being undefinite)*.

An increase of the crystallization rate is found with increasing temperature, of course, with increasing water vapour pressure (from a certain pressure on the growth rate proportional to the square root of water vapour pressure) in both types, and with increased oxygen pressure only in the non-stoichiometric silica glass, the influence of water vapour being larger, by a factor of more than two, than that of oxygen. In the absence of oxygen, the crystallization of the latter will also occur, but at a lower rate 143,144). It can be concluded, that an oxygen atmosphere is only important if there is an oxygen deficiency in the glass, and that a water vapour atmosphere is accelerating the crystallization in two ways: H_2O acts as a source of oxygen and as a

^{*} The value of 132 μ m²/min in parabolic form represents a slower mean diffusion velocity than the linear one of 0.98 μ m/min, i.e. after the same comparable time the thickness of the crystallized layer will be larger in the linear case (0.98 μ m/min) than in the parabolic case (132 μ m²/min). The crystallization rates, of type I silica glasses, are of the same order as that of the de-watered and reduced type III silica glass (100–200 μ m²/min at 1460°C and 480 mm water vapour pressure) depending on the impurity content other than OH and on the degree of oxygen deficiency. It is remarkable that a type IV silica glass (Corning 7943) shows also parabolic growth kinetics (about 30 μ m²/min only), that means, it was produced under reducing conditions 141).

source of weakening the glass structure by the incorporation of H₂O; nearly each molecule forming two hydroxyl groups causes rupture of a Si-O bond.

In table 2 a comparison is given between different crystallization conditions of a de-watered type III silica glass for a temperature of 1486 °C after Wagstaff et al.¹⁴¹, ¹⁴²).

TABLE 2

Atmosphere	Crystallization rates (µm/min) from surface
452 mm H ₂ O	1.02
Dry N2 or O2	0.42
Vacuo	0.12

The addition of only 0.32 wt% Na₂O causes an increase of the crystallization rate up to 670 μ m/min at the temperature of maximum crystallization rate (1400 °C)¹⁴⁵). This shows the effect of impurities, which in turn, greatly intensify the needed mobility for crystallization. In connection with the concept of the preordered regions this mobility is well understood ⁸⁴).

Now, the question arises as to what the true crystallization rate of silica glass is. In high purity silica glass (type II to IV) no crystallization in the interior of the bulk glass could be observed. But recently in Vitreosil (type I) internal devitrification, heterogeneously nucleated by very small impurity regions (of the order of a few microns), has been observed 144). This fact is important in a twofold way: firstly, high-cristobalite crystals are obtained metastable, below their normal transformation temperature even down to liquid helium temperature, as a result of the tensile stresses developed across the boundary during cooling; and secondly, intrinsic growth rates can be maintained to allow the possibility of repeated increments of crystal growth to be measured on the same growing crystal, as long as the cristobalite does not transform. On cooling some crystals change to low cristobalite, and if the tensile stress is released mechanically by grinding, etching, cracking etc., spontaneous transformation occurs, at room temperature, of the left metastable high cristobalite crystals. This fact is interesting in connection with the conclusions drawn in section 4.2 about the preordered regions. In spite of the fact that not less than 70 hours are needed for the production of crystals of a few microns in size at 1480°C, and that impurity inclusions are necessary to form a stable nucleus, a certain relation to the concept of the preordered regions will not to be rejected.

Another fact is important in connection with table 2 and with the intrinsic

crystal growth rate. At a temperature of 1486° C a growth rate of $0.02 \,\mu\text{m/min}$ occurs and an activation energy very similar to that of viscosity (see section $5.4.)^{144}$). This indicates, that even in vacuo very small quantities of impurity cannot be totally excluded. A further fact is, that the growth rate is linear with time, although an electrically melted silica glass of type I (oxygen deficiency) was used; this shows the overwhelming effect of the presence of oxygen on surface crystallization for type I silica glasses.

The crystallization of pure silica glass to tridymite or quartz under normal atmospheric conditions has not yet been observed. The tridymite transformation above 870°C and the quartz transformation below 870°C is only possible in the presence of mineralizers^{1,146}).

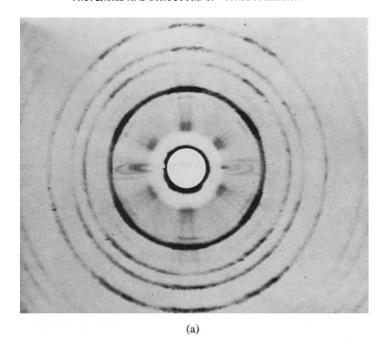
Under the action of high pressure the high pressure modifications of silica are obtained: keatite, coesite (above 20–40 kbar), and stishovite (above 97–130 kbar). A complete phase diagram is recently presented ¹⁴⁷) including quartz, cristobalite, tridymite, coesite and stishovite.

A remarkable fact is, that the transformation under pressure to quartz and to coesite from silica glass is again dependent on water content of the surrounding atmosphere and of the compressed silica glass sample, and on the OH-content in the silica glass sample¹⁴⁸). As a result, at a temperature of 500°C and a pressure of 40 kbar, the rate of crystallization to quartz and coesite decreases in the series: silica gel→GE 204 (wet loading) →GE 204 and spectrosil (air loading)→spectrosil (dry loading)→GE 204 (dry loading) →GE 204 (ultra-dry loading). The difference between the higher crystallization rate, of the "water"-rich sample spectrosil and that of the "water"-poor sample GE 204 on the one hand, and the difference between the higher crystallization rate in water vapour and the lower one in dry atmosphere on the other hand, gives rise to the conclusion that water vapour and OH content have a catalytic influence on the crystallization mechanism. It is suggested, that a possible existence of a water-rich region in the vicinity of the interface should be responsible for this behaviour¹⁴⁸). Both these effects, the catalytic influence and the water-rich region, should be enhanced by pressure.

Preferred orientation of cristobalite crystallization on the surface of vitreous silica was observed in two cases.

First, the devitrified surface of a silica glass plate heated at 1200 °C for 6 hours shows a habit plane or an orientation to some degree with respect to the surface, but only for the (101) planes of the low-temperature cristobalite, whereas, a completely random orientation is found for the other major α -cristobalite planes (111), (102) and (200)¹⁴⁹).

Second, silica glass fibers, when crystallized at 1200 or 1300 °C, show preferred orientation of high- and also of low-temperature crystobalite (fig. 35a). This is only the case if the fibers were fresh and not annealed before



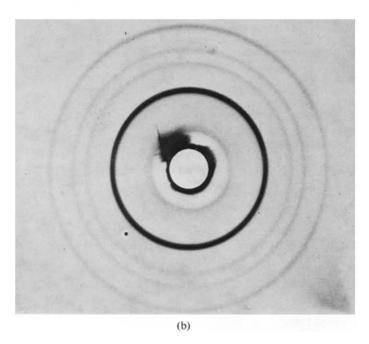


Fig. 35. Crystallization of silica glass fibers; (a) crystallized at 1270°C without annealing before crystallization; (b) crystallized at 1270°C after annealing at 1000°C.

crystallization, because annealing causes structural regroupings and a loss of the glass fiber anisotropy. Therefore no preferred orientation of the crystallized fiber is detectable when a 10 hours annealing at 1000 °C preceded the crystallization (fig. 35b). This behaviour is regarded as an evidence that no surface-influenced crystallization leads to the texture effect as in the former case, but that the influence of the anisotropic structure of the silica glass fiber to cristobalite.

References

- 1) R. B. Sosman, The Phases of Silica (Rutgers Univ. Press, New Brunswick, N.J., 1964).
- G. Hetherington, K. H. Jack and M. W. Ramsay, Phys. Chem. Glasses 3 (1962) 129;
 6 (1965) 6.
- 3) Trademark of W. C. Heraeus-Schott Comp., Germany, and Amersil Quartz Division, Engelhard Industries, Inc.
- 4) Trademark of Thermal Syndicate Ltd., England.
- 5) Trademark of General Electric Comp., U.S.A.
- 6) Trademark of Corning Glass Comp., U.S.A.
- 7) J. H. Rosolowski, Am. Ceram. Soc. Bull. (1966) 68, 381; Annual Meeting of the Am. Ceram. Soc.
- 8) P. Ehrenfest, Commun. Kamerlingh Onnes Lab. Leiden Suppl. 75b (1933).
- 9) E. Jenckel, Die glasige Erstarrung der Hochpolymere, in: Die Physik der Hochpolymeren, Vol. III, Ed. H. A. Stuart (Springer, Berlin, 1955) pp. 608-638;
 - F. Simon, Z. Anorgan, Allgem. Chem. 233 (1931) 219;
 - C. Tammann, Der Glaszustand (Leipzig, 1933);
 - R. Haase, Thermodynamik der Mischphasen (Springer, Berlin, 1956).
- J. H. Gibbs, Nature of the Glass Transition and the Vitreous State, in: Modern Aspects of the Vitreous State, Vol. I, Ed. J. D. Mackenzie (Butterworth, London, 1960) p. 152;
 - J. H. Gibbs and E. A. DiMarzio, J. Chem. Phys. 28 (1958) 373.
- 11) R. W. Douglas and J. O. Isard, J. Soc. Glass Technol. 35 (1951) 206.
- 12) R. Brückner, Glastech. Ber. 37 (1964) 459.
- 13) B. E. Warren, Z. Krist. 86 (1933) 349.
- 14) B. E. Warren, H. Krutter and O. Morningstar, J. Am. Ceram. Soc. 19 (1936) 202.
- 15) B. E. Warren and J. Biscoe, J. Am. Ceram. Soc. 21 (1938) 49.
- 16) W. O. Milligan, H. A. Levy and S. W. Peterson, Phys. Rev. 83 (1951) 226.
- 17) J. Zarzycki, in: Compt. Rend. IVe Congr. Intern. du Verre, Paris, 1956, p. 323.
- 18) J. T. Randall, H. P. Rooksby and B. S. Cooper, J. Soc. Glass Technol. 14 (1930) 219.
- 19) G. Hartleif, Z. Anorgan. Allgem. Chem. 238 (1938) 353.
- 20) E. A. Porai-Koshits, in: Structure of Glass (Acad. Sci. U.S.S.R., Moscow, 1960) (Transl. 1960) pp. 9-16.
- R. J. Breen and A. H. Wever, Glass Structure Research Fellowship, St. Louis Univ. Rept. July 1, 1952.
- 22) E. Lorch, Brit. J. Phys. C (Solid State Phys.) 2 (1969) 229.
- 23) W. H. Zachariasen, J. Am. Chem. Soc. 54 (1932) 3841; Glastech. Ber. 11 (1933) 120.
- 24) A. Dietzel, Glastech. Ber. 22 (1948) 41, 81, 212.
- 25) J. M. Stevels, *Progress in the Theory of the Physical Properties of Glass* (Elsevier, Amsterdam, 1948).
- 26) J. M. Stevels, Glass Ind. 35 (1954) 69, 100, 102, 135, 160.
- J. M. Stevels, Philips Techn. Rev. 22 (1960/61) 300, 337.
- 28) K. H. Sun, J. Am. Ceram. Soc. 30 (1947) 277.

- 29) M. L. Huggins, J. Am. Ceram. Soc. 38 (1955) 172.
- A. A. Lebedev, Tr. Gos. Optich. Inst. Leningrad 2 (1921) No. 10; Bull. Acad. Sci. USSR, Sci. Phys. 4 (1940) 584.
- 31) O. A. Botvinkin, in: Compt. Rend. IVe Congr. Intern. du Verre, Paris, 1956, p. 451.
- 32) W. Vogel and K. Gerth, Glastech. Ber. 31 (1958) 15.
- 33) W. Vogel, Silikat Tech. 10 (1959) 241; Proc. All-Union Conf. Glassy State Leningrad 3 (159) 17.
- 34) W. Vogel and H. G. Byhan, Silikat Tech. 15 (1965) 212, 239.
- 35) J. W. Cahn and J. E. Hilliard, J. Chem. Phys. 31 (1959) 688.
- 36) J. W. Cahn, J. Chem. Phys. 42 (1965) 93.
- 37) W. B. Hillig, in: Symp. Nucleation and Crystallization in Glasses and Melts, Toronto, 1961 (Ceramic Soc., Columbia, Ohio, 1962) p. 78.
- 38) J. W. Cahn and R. J. Charles, Phys. Chem. Glasses 6 (1965) 181.
- 39) D. Turnbull, J. Phys. Chem. 66 (1962) 609; J. Appl. Phys. 21 (1950) 1022.
- 40) D. Turnbull, in: Symp. Nucleation ans Crystallization of Glasses and Melts, Toronto, 1961 (Ceramic Soc., Columbia, Ohio, 1962) p. 75.
- 41) R. J. Charles, J. Am. Ceram. Soc. 46 (1963) 235; 47 (1964) 559; 49 (1966) 55.
- 42) L. W. Tilton, J. Res. Natl. Bur. Std. 59 (1957) 139.
- 43) H. A. Robinson, J. Phys. Chem. Solids 26 (1965) 209.
- 44) R. J. Bell and P. Dean, Nature 212 (1966) 1354.
- 45) R. J. Bell, N. F. Bird and P. Dean, Brit, J. Phys. C (Proc. Phys. Soc.) [2] 1 (1968) 299.
- 46) A. Smekal, Novo Acta Leopoldina NF 11 (1942).
- 47) A. Smekal, Glastech. Ber. 22 (1949) 278; J. Soc. Glass Technol. 35 (1951) 411.
- 48) K. Grjotheim and J. Krogh-Moe, Glastek. Tidskr. 11 (1956) 47.
- 49) A. Winter, J. Am. Ceram. Soc. 40 (1957) 54.
- 50) W. Noll, Naturwissenschaften 49 (1962) 505; Angew. Chem. 75 (1963) 123.
- 51) A. Dietzel, Z. Elektrochem. 48 (1942) 9.
- 52) W. A. Weyl, J. Soc. Glass Technol. 35 (1951) 421; Glastech. Ber. 30 (1957)
- 53) W. A. Weyl and E. Ch. Marboe, *The Constitution of Glasses; A Dynamic Interpretation*, Vols. 1 and 2 (Wiley-Interscience, New York, 1962, 1965).
- 54) H. Krebs, Angew. Chem. 70 (1958) 615; 78 1966) 577.
- 55) V. Garino-Canina, Verres Réfractairees 10 (1956) 63, 151.
- 56) T. Bell, G. Hetherington and K. H. Jack, Phys. Chem. Glasses 3 (1962) 141.
- 57) A. J. Cohen, Phys. Rev. 105 (1957) 1151.
- 58) A. J. Cohen, J. Chem. Phys. 23 (1955) 765.
- 59) J. S. van Wieringen and A. Kats, Philips Res. Rept. 12 (1957) 423.
- 60) R. A. Weeks and E. Lell, J. Appl Phys. 35 (1964) 1932.
- 61) J. M. Stevels, Glastech. Ber. 32 (1959) 307; Philips Res. Rept. 11 (1956) 103; in: NonCrystalline Solids, 1958, Ed. V. D. Fréchette (Wiley, New York, 1960) pp. 412-448.
- 62) R. Yokota, Phys. Rev. 91 (1953) 1913.
- 63) M. Lautout, J. Chim. Phys. 52 (1955) 169.
- 64) S. Cohen, Bull. Soc. Franc. Ceram. No. 56 (1962) 29; Verres Réfractaires 23 (1969) 189
- 65) A. J. Harrison, J. Am. Ceram. Soc. 30 (1947) 362.
- 66) H. Scholze, Glastech, Ber. 32 (1959) 81, 142.
- 67) E. R. Lippingcott, A. van Valkenburg, Ch. E. Weir and E. N. Bunting, J. Res. Natl. Bur. Std. 61 (1958) 61.
- 68) J. Zarzycki and F. Naudin, Verres Réfractaires 14 (1960) 1.
- 69) P. H. Gaskell, Trans. Faraday Soc. 62 (1966) 1493, 1505.
- 70) R. Brückner, Glastech. Ber. 37 (1964) 500.
- 71) P. H. Gaskell and F. J. Grove, in: Compt Rend. VIIe Congr. Intern. du Verre, Brussels, 1965, No. 363.
- 72) H. Mohn, in: 60 Jahre Quarzglas, 25 Jahre Hochvakuumtechnik, Ed. W. C. Heraeus (1961) pp. 105-130.

- 73) G. Hetherington and K. H. Jack, Phys. Chem. Glasses 3 (1962) 129.
- 74) H. Scholze, H. Franz and L. Merker, Glastech. Ber. 32 (1959) 421.
- 75) R. Brückner, Glastech. Ber. 37 (1964) 459; 38 (1965) 153.
- 76) W. Poch, Glastech. Ber. 37 (1964) 533.
- 77) H. Scholze, Glas-Email-Keramo-Tech. 19 (1968) 389.
- 78) A. Winter and M. J. Cabannes, Compt. Rend. (Paris) 240 (1955) 2397.
- 79) H. Rau, in: 60 Jahre Quarzglas, 25 Jahre Hochvakuumtechnik, Ed. W. C. Heraeus (1961) pp. 77-104.
- 80) V. Garino-Canina, Rev. Opt. Théor. Instr. 34 (1955) 323.
- 81) J. F. Bacon, A. A. Hasapis and J. W. Wholley, Phys. Chem. Glasses 1 (1960) 90.
- 82) W. H. Keesom and D. W. Doborzynski, Physica 1 (1934) 1058.
- 83) H. T. Smyth, J. Am. Ceram. Soc. 38 (1955) 140.
- 84) R. Brückner, Glastech. Ber. 37 (1964) 536.
- J. I. Frenkel, Statistische Physik (Akademie-Verlag, Berlin, 1957) ch. IX;
 J. I. Frenkel, Theory of Fluids (Akademie-Verlag, Berlin, 1957) ch. VII.
- 86) M. Volmer and A. Wever, Z. Physik. Chem. 119 (1926) 277.
- 87) J. C. Fischer, J. H. Hollomon and D. Turnbull, J. Appl. Phys. 19 (1948) 775.
- 88) P. W. Bridgman, Am. J. Sci. 10 (1925) 359.
- 89) J. Reitzel, J. Simon and J. A. Walker, Rev. Sci. Instr. 28 (1957) 828.
- C. L. Babcock, S. W. Barber and K. Fajans, in: III Congr. Intern. de Vetro, Venezia, 1953, p. 202.
- 91) F. Birch and R. B. Dow, Bull. Geol. Soc. Am. 47 (1936) 1235.
- 92) K. Vedam, E. D. D. Schmidt and R. Roy, J. Am. Ceram Soc. 49 (1966) 531.
- 93) H. Mueller, Physica 6 (1935) 179.
- 94) J. D. Mackenzie, J. Am. Ceram. Soc. 46 (1963) 461, 470.
- 95) R. Roy and H. M. Cohen, Nature 190 (1961) 789; Phys. Chem. Glasses 6 (1965) 149.
- 96) E. B. Christiansen, S. S. Kistler and W. B. Gogartz, J. Am. Ceram. Soc. 45 (1962) 172.
- P. W. Bridgman and J. Simon, J. Appl. Phys. 24 (1953) 405;
 J. Arndt, J. Am. Ceram Soc. 52 (1969) 285.
- 98) R. M. Kimmel and D. R. Uhlmann, Phys. Chem. Glasses 10 (1969) 12.
- J. Arndt and D. Stöffler, Phys. Chem. Glasses 10 (1969) 117;
 D. Stöffler and J. Arndt, Naturwissenschaften 56 (1969) 100.
- 100) J. D. Mackenzie, J. Am. Ceram. Soc. 47 (1964) 76.
- 101) H. T. Smyth, J. W. Londree and G. E. Lorey, J. Am. Ceram. Soc. 36 (1953) 238.
- 102) H. T. Smyth, J. Am. Ceram. Soc. 42 (1959) 276.
- 103) F. P. Mallinder and B. A. Proctor, Phys. Chem. Glasses 5 (1964) 91.
- 104) W. B. Hillig, in: Symposium sur la Résistance Méchanique du Verre et les Moyens de l'Améliorer, Florence, 1961 (Union Scientifique Continentale du Verre, Charleroi, Belgium, 1962) pp. I-1/1-31.
- 105) J. W. Marx and J. M. Sivertsen, J. Appl. Phys. 24 (1953) 81.
- 106) H. J. McSkimin, J. Appl. Phys. 24 (1953) 988.
- 107) M. E. Fine, H. van Duyne and N. T. Kenney, J. Appl. Phys. 25 (1954) 402.
- 108) E. Deeg, Glastech. Ber. 31 (1958) 124;S. Spinner and G. W. Cleek, J. Appl. Phys. 31 (1960) 1407.
- 109) G. J. Dienes, J. Phys. Chem. Solids 7 (1958) 290.
- 110) O. L. Anderson and G. J. Dienes, in: Non-Crystalline Solids, 1958, Ed. V. D. Fréchette (Wiley, New York, 1960) pp. 449-490.
- 111) D. B. Fraser, J. Appl. Phys. 39 (1968) 5868.
- 112) O. L. Anderson and H. E. Bömmel, J. Am. Ceram. Soc. 38 (1955) 125.
- 113) J. T. Krause, J. Am. Ceram. Soc. 47 (1964) 103.
- 114) R. E. Strakna and H. T. Savage, J. Appl. Phys. 35 (1964) 1445.
- 115) C. R. Kurkjian and J. T. Krause, J. Am. Ceram. Soc. 49 (1966) 134.
- 116) H. T. Smyth, H. S. Skogen and W. B. Harsell, J. Am. Ceram. Soc. 36 (1953) 327.
- 117) R. B. Sosman, The Properties of Silica (The Chemical Catalog Comp., New York, 1927) p. 313.

- 118) W. Geffcken and N. Neuroth, Glastech. Ber. Sonderband 32K (1959) V/48-53.
- 119) O. L. Anderson, J. Phys. Chem. Solids 12 (1959) 41.
- 120) M. Born and K. Huang, Dynamic Theory of Lattices (Oxford Univ. Press, 1954) ch. 3.
- 121) P, Fulbacher, A. J. Leadbetter, J. A. Morrison and B. P. Stoicheff, J. Phys. Chem. Solids 12 (1959) 53;
 - A. J. Leadbetter, J. Chem. Phys. 51 (1969) 779.
- 122) St. M. Shapiro, R. W. Gammon and H. Z. Cummins, Appl. Phys. Letters 9 (1966) 157
- 123) J. M. Stevels, in: *Encyclopedia of Physics*, Vol. 13, Ed. S. Flügge (Springer, Berlin, 1962) p. 577.
- 124) C. Kittel, Phys. Rev. 75 (1949) 972.
- 125) P. G. Klemens, in: Non-Crystalline Solids, 1958, Ed. V. D. Fréchette (Wiley, New York, 1960) pp. 508-528.
- 126) W. D. Kingery, J. Am. Ceram. Soc. 38 (1955) 251; 44 (1961) 302.
- 127) K. L. Wray and T. J. Connolly, J. Appl. Phys. 30 (1959) 1702.
- 128) E. H. Ratchiff, Brit. J. Appl. Phys. 10 (1951) 108.
- 129) P. G. Klemens, Proc. Roy, Soc. (London) A 208 (1951) 108.
- 130) R. Berman, Proc. Roy. Soc. (London) A 208 (1951) 90.
- 131) P. G. Klemens, J. G. Castle and D. W. Feldman, Phys. Chem. Glasses 2 (1964) 104.
- 132) J. G. Morley, P. A. Andrews and J. Whetney, Phys. Chem. Glassew 5 (1964) 1.
- 133) B. A. Proctor, I. Whitney and J. W. Johnson, Proc. Roy. Soc. (London) A 297 (1967) 534.
- 134) R. J. Charles and W. B. Hillig, in: Symposium sur la Résistance Méchanique du Verre et les Moyens de l'Améliorer, Florence, 1961 (Union Scientifique Continentale du Verre, Charleroi, Belgium, 1962) pp. II-3/1-17.
- 135) J. B. Murgatroyd, J. Soc. Glass Technol. 28 (1944) 368, 388.
- 136) S. Bateson, J. Soc. Glass Technol. 37 (1953) 302.
- 137) W. F. Thomas, Nature 181 (1958) 1006; Phys. Chem. Glasses 1 (1960) 4.
- 138) W. H. Otto, J. Am. Ceram. Soc. 44 (1961) 68.
- 139) L. Merker, in: Symposium sur la Résistance Méchanique du Verre et les Moyens de l'Améliorer, Florence, 1961 (Union Scientifique Continentale du Verre, Charleroi, Belgium, 1962) pp. 567-687.
- 140) R. Brückner, in: Compt. Rend. VIIe Congr. Intern. du Verre, Brussels, 1965 No. 38/1-12, 1,3,2.
- 141) F. E. Wagstaff, S. D. Brown and I. B. Cutler, Phys. Chem. Glasses 5 (1964) 76.
- 142) F. E. Wagstaff and K. J. Richards, J. Am. Ceram. Soc. 48 (1965) 382; 49 (1966) 118.
- 143) J. Hlavac and L. Vaskova, Silicaty 9 (1965) 237.
- 144) F. E. Wagstaff, J. Am. Ceram. Soc. 51 (1968) 449.
- 145) A. Dietzel and H. Wickert, Glastech. Ber. 29 (1956) 1.
- 146) O. W. Flörke, Ber. Deut. Keram. Ges. 38 (1961) 89.
- 147) D. Stöffler and J. Arndt, Naturwissenschaften 56 (1969) 100.
- 148) D. R. Uhlmann, J. F. Hays and D. Turnbull, Phys. Chem. Glasses 7 (1966) 159.
- 149) R. F. Hochman and J. D. Fleming, J. Am. Ceram. Soc. 47 (1964) 104.