Reconfigurable all-dielectric metalens with diffraction-limited performance

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Article

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ABSTRACT

Active metasurfaces, whose optical properties can be modulated post-fabrication, have emerged as an intensively explored field in recent years. The efforts to date, however, still face major performance limitations in tuning range, optical quality, and efficiency especially for non-mechanical actuation mechanisms. In this paper, we introduce an active metasurface platform combining phase tuning covering the full 2π range and diffraction-limited performance using an all-dielectric, low-loss architecture based on optical phase change materials (O-PCMs). We present a generic design principle enabling binary switching of metasurfaces between arbitrary phase profiles and propose a new figure-of-merit (FOM) tailored for active meta-optics. We implement the approach to realize a high-performance varifocal metalens operating at 5.2 μm wavelength. The metalens is constructed using $Ge_2Sb_2Se_4Te_1$ (GSST), an O-PCM with a large refractive index contrast ($\Delta n > 1$) and unique broadband low-loss characteristics in both amorphous and crystalline states. The reconfigurable metalens features focusing efficiencies above 20% at both states for linearly polarized light and a record large switching contrast ratio of 29.5 dB. We further validate aberration-free and multi-depth imaging using the metalens, which represents the first experimental demonstration of a non-mechanical active metalens with diffraction-limited performance.

INTRODUCTION

The ability to reconfigure an optical component, thereby tuning its optical response to meet diverse application demands at will, has been a Holy Grail for optical engineers. Traditionally, such dynamic reconfigurability often requires bulky mechanical moving parts, for example in a zoom lens. The approach, however, usually comes with the price of increased system size and complexity. Unlike conventional optics which rely on geometric curvature to mold the propagation phase of light, metasurfaces afford on-demand control of an optical wavefront using sub-wavelength antenna arrays patterned via standard planar microfabrication technologies[1–7]. In addition to their potential Size, Weight, Power, and Cost (SWaP-C) benefits, they also present a versatile suite of solutions to realizing reconfigurable optical systems, leveraging so-called "active metasurfaces", whose optical responses can be dynamically tuned.

Over the past few years, active metasurfaces have been investigated intensively[8–16]. Mechanical deformation or displacement of metasurfaces is an effective method for tuning metasurface devices or adaptively correcting optical aberrations[17–22]. On the other hand, non-mechanical actuation methods, which allow direct modulation of optical properties of meta-atoms, can offer significant advantages in terms of speed, power consumption, reliability, as well as design flexibility. A variety of tuning mechanisms such as free carrier[23], thermo-optic[24], electro-refractive[25], and all-optical[26] effects have been harnessed to create active metasurface devices. However, these effects are either relatively weak (e.g., thermo-optic, electro-refractive, and all-optical effects) or incur excessive optical loss (e.g., free carrier injection). Consequently, the tuning range and optical efficiency of these active metasurfaces are often limited.

Phase change and phase transition materials (exemplified by chalcogenide compounds and correlated oxides such as VO_2, respectively) offer another promising route for realizing active metasurfaces[15,27–29]. The extremely large refractive index contrast associated with material phase transformation (e.g. $\Delta n > 1$) uniquely empowers metasurface devices with ultra-wide tuning ranges. Many studies have achieved amplitude or spectral tailoring of light via metastructures made of these materials[30–39]. Tunable optical phase or wavefront control, which is essential for realizing multifunctional meta-optical components, such as, metalenses and beam steering devices, has also been demonstrated[40–43]. However, that meta-optical devices had relatively low efficiencies, and their phase precision, a key metric which dictates optical quality of metasurface devices, has not been quantified. Moreover, the designs often suffer from significant crosstalk between the optical states which causes ghosting across the variable states and severe image quality degradation in imaging applications. As a result, it is not clear yet whether active meta-optical devices can possibly attain diffraction-limited, low-crosstalk performances rivaling their traditional bulky refractive counterparts.

Besides experimental implementation, the design of wavefront-shaping devices based on active metasurfaces also poses a largely unexplored challenge. The presence of two or more optical states vastly increases the complexity of design targets. Additionally, modulating the optical properties of meta-atoms in general concurrently modifies their phase and amplitude responses, both of which impact the device performance in its different optical states. Optimization of active meta-optical devices, therefore, requires a computationally-efficient design composition and validation approach to generate meta-atom libraries that allow down selection of optimal meta-atom geometries, which yield the desired optical performance at each state.

In this paper, we present a generic design methodology enabling switching of metasurface devices to realize arbitrary phase profiles. A new figure-of-merit (FOM) suited for active meta-optics is developed to facilitate efficient and accurate metasurface performance prediction without
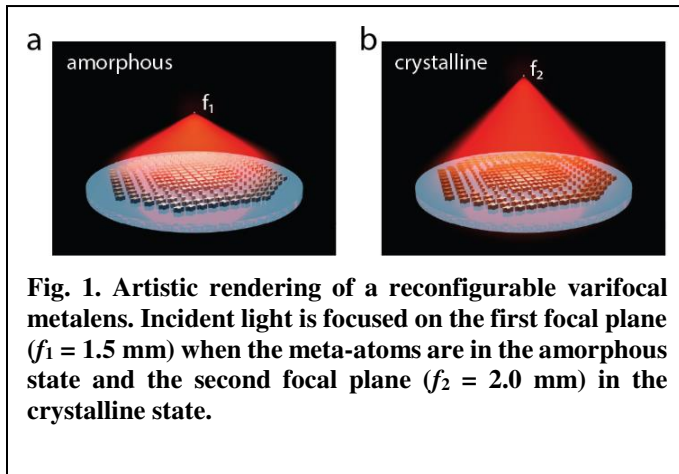
84 resorting to computationally intensive full-system simulations. The design framework is validated
85 through demonstration of a high-performance varifocal metalens. The concept of a varifocal lens
86 based on phase change materials was first elegantly implemented in the pioneering work by Yin
87 *et al.*[43]. Their design relied on two groups of plasmonic antennae sharing the same lens aperture
88 on top of a blanket phase change material film, each of which responded to incident light at either
89 the amorphous or crystalline state of the film. The shared-aperture layout and the use of metallic
90 meta-atoms limited the focusing efficiencies to 5% and 10% in the two states. Focal spot quality
91 of the lens was also not reported. Our device instead builds on all-dielectric meta-atom structures
92 optimized via design methodology to simultaneously minimize phase error (thereby suppressing
93 crosstalk) and boost optical efficiency. The design FOM allows computationally-efficient
94 synthesis of the active metasurface without performing simulations for each optical system during
95 the optimization process, and thus it is scalable to designs with increased complexity and
96 functionalities. We have further experimentally demonstrated diffraction-limited imaging free of
97 aberration and crosstalk at both states of the metalens, for the first time proving that active
98 metasurface optics based on O-PCM technologies can indeed attain a high level of optical quality
99 matching that of their conventional bulk counterparts while taking full advantage of their flat
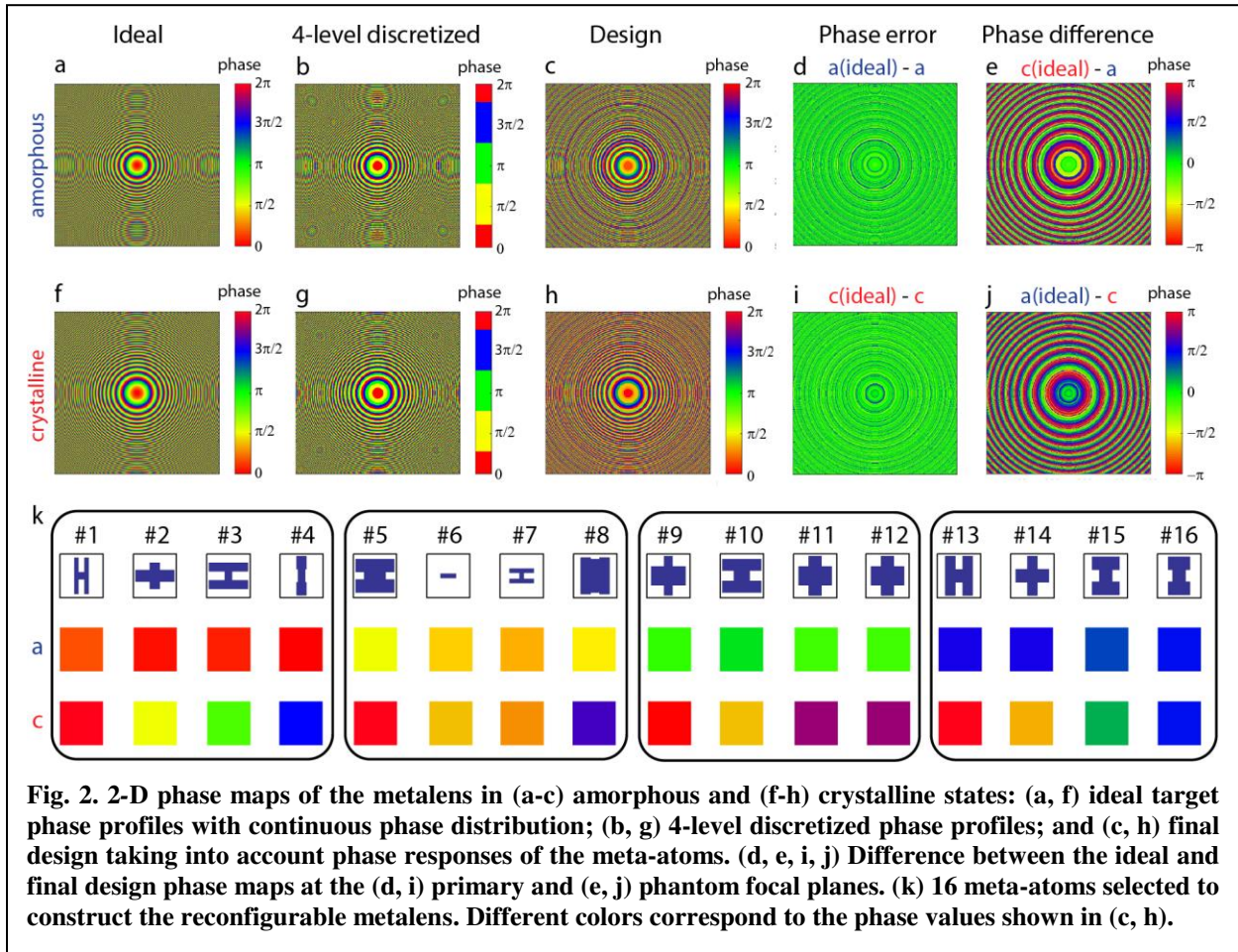100 optical architecture.
101

102 **RESULTS**

103 **On-demand composition of bi-state meta-optical devices: concept and design methodology**

104 We select $Ge_2Sb_2Se_4Te_1$ (GSST) as the O-PCM to construct the metasurface operating at the
105 wavelength $\lambda_0 = 5.2$ μm. Compared to the classical $Ge_2Sb_2Te_5$ (GST) phase change alloy, GSST
106 offers exceptionally broadband transparency in the infrared spectral regime for both its amorphous
107 and crystalline phases, a feature critical to optical loss reduction, while maintaining a large
108 refractive index contrast between the two states[44–46]. The metasurface consists of patterned,
109 isolated GSST Huygens meta-atoms sitting on a CaF_2 substrate (Fig. 1). The Huygens-type meta-
110 atom design features an ultra-thin, deep sub-wavelength profile ($< \lambda_0/5$) which facilitates a simple
111 one-step etch fabrication process[47–50]. While here we use a bi-state varifocal metalens as our proof-
112 of-concept demonstration, our device architecture and design approach are generic and applicable
113 to active metasurfaces switchable between arbitrary phase profiles. The design can also be readily
114 generalized to active metasurfaces supporting more than two optical states, for instance leveraging
115 intermediate states in O-PCMs[51,52].

Fig. 1. Artistic rendering of a reconfigurable varifocal metalens. Incident light is focused on the first focal plane ($f_1 = 1.5$ mm) when the meta-atoms are in the amorphous state and the second focal plane ($f_2 = 2.0$ mm) in the crystalline state.

The design procedure of the active metalens with a dimension of 1.5×1.5 mm^2 is illustrated in Fig. 2. The design process starts by defining the target phase maps in the two optical states. For the varifocal metalens under consideration, two hyperbolic phase profiles (with 2π phase wraps) yielding focal lengths of $f_1 = 1.5$ mm (amorphous, a-state) and $f_2 = 2$ mm (crystalline, c-state) are plotted in Figs. 2a and 2f, respectively. The design corresponds to numerical aperture (NA) values of 0.45 and 0.35 in the amorphous

129 and crystalline states, respectively. We then choose to discretize the continuous 0 to 2π phase
130 profiles into $m = 4$ phase levels, i.e., 0, $\pi/2$, π, and $3\pi/2$ (Figs. 2b and 2g). To enable switching
131 between two arbitrary phase profiles with four discrete phase levels, a total of $m^2 = 16$ meta-atom
132 designs are needed, each of which provides a distinct combination of two of the four discrete phase
133 values during the phase transition. An ideal meta-atom design must minimize phase error while
134 maximizing optical efficiency at both states. Realistic designs however often face trade-offs
135 between phase error and efficiency given the inherent complexity associated with the bi-state
136 design targets, as detailed next.

Fig. 2. 2-D phase maps of the metalens in (a-c) amorphous and (f-h) crystalline states: (a, f) ideal target phase profiles with continuous phase distribution; (b, g) 4-level discretized phase profiles; and (c, h) final design taking into account phase responses of the meta-atoms. (d, e, i, j) Difference between the ideal and final design phase maps at the (d, i) primary and (e, j) phantom focal planes. (k) 16 meta-atoms selected to construct the reconfigurable metalens. Different colors correspond to the phase values shown in (c, h).

138   To obtain the 16 optimal meta-atom designs, a pool of Huygens meta-atoms with various
139 regular geometries, such as 'I', 'H', and "+" shapes, were first generated by sweeping the
140 geometric parameters in a full-wave electromagnetic solver (Supplementary Information,
141 Section I), and then grouped according to the four phase levels and phase variances between the
142 two states. Different sub-groups of meta-atoms were then mapped onto the evenly-discretized
143 metasurface phase profiles. Using the generated phase/amplitude masks and following generalized
144 diffraction efficiency calculation of multi-level diffractive optical elements[53], we develop a new
145 performance FOM suitable for evaluating and optimizing meta-atom designs without resorting to
146 full-scale system simulations. Derivation of the FOM is detailed in Supplementary Information,
147 Section III. The 16 meta-atoms were selected from the design pool based on the following FOMs:

$$148 \quad FOM_{1,a} = T_{avg,a} \cdot \left(\frac{\sin\left(2\left\langle \left| \phi_{meta,a} - \phi_{target,a} \right| \right\rangle \right)}{2\left\langle \left| \phi_{meta,a} - \phi_{target,a} \right| \right\rangle} \right)^2 \quad (1)$$

$$149 \quad FOM_{2,c} = T_{avg,c} \cdot \left(\frac{\sin\left(2\left\langle \left| \phi_{meta,c} - \phi_{target,c} \right| \right\rangle \right)}{2\left\langle \left| \phi_{meta,c} - \phi_{target,c} \right| \right\rangle} \right)^2 \quad (2)$$

$$150 \quad FOM_{eff} = \sqrt{FOM_{1,a} \cdot FOM_{2,c}} \quad (3)$$

151 where $FOM_{1,a}$ and $FOM_{2,c}$ correlate with the metasurface performances on Focal Plane 1 in the
152 amorphous state and Focal Plane 2 in the crystalline state, respectively. $T_{avg,a(c)}$, $\phi_{target,a(c)}$ and
153 $\phi_{meta,a(c)}$ are the average meta-atom transmittance, target phase values and simulated actual phase
154 values in the amorphous (crystalline) state. Maximization of FOM_{eff} ensures good focal spot
155 quality and focusing efficiency at both optical states, which provides quantitative evaluation of the
156 trade-offs between efficiency and phase error. This in turn enables the synthesis of a metasurface
157 with the best meta-atom structures without performing full-scale simulations of the entire optical
158 system. Implementation of the aforementioned FOM evaluation method can be further extended
159 from the metasurface level to the meta-atom level before constructing a specific metasurface
160 design, by applying weighting factors to different meta-atom geometries according to the
161 metasurface phase map.
162   In imaging applications involving active metalenses, crosstalk is another extremely important
163 metric, since crosstalk results in ghost image formation which severely degrades image quality.
164 The FOM defined above can be revised to further take into account crosstalk between the two
165 states, which is characterized by the switching contrast ratio CR:

$$166 \quad CR = 10\log_{10}\left(\frac{P_{1,a}}{P_{2,a}} \cdot \frac{P_{2,c}}{P_{1,c}} \right) \quad \text{(in dB)} \quad (4)$$

167 where $P_{1(2),a(c)}$ denotes the focused optical power (defined as the power confined within a radius
168 of $5\lambda_0$) at focal spot 1 (2) at the amorphous (crystalline) state. Since the ideal phase profiles are
169 already defined in Figs. 2a and 2f, the focused power at the "phantom" focal spot (i.e., focal spot
170 2 in the a-state and focal spot 1 in the c-state) is solely determined by the "difference" in the two
171 phase profiles. In practice, the CR can be compromised by incomplete switching of the meta-atoms
172 and is thus also an essential measure of the metalens' optical quality. For the cases of diffractive
173 optical elements (DOEs) or metasurfaces (the latter of which are sometimes regarded as multi-
174 level DOEs with a subwavelength array), phase deviations mostly originate from random errors
175 due to the phase sampling process, as compared to continuous and systematic wavefront distortions
176 which are typically encountered in refractive bulk optics. Consequently, the RMS phase errors of
177 such devices mostly contribute to scattered loss or crosstalk between optical states, as analyzed for
178 multi-level DOEs in Ref. [53]. We note that FOMs defined in Eqs. 1 and 2 scale directly with
179 diffraction efficiency, or specifically in the case of a metalens, the focusing efficiency on a
180 particular focal plane in a particular state. The equations can therefore be equally applied to
181 correlate light intensities at the phantom focal spots with the metasurface design. Thus, a FOM
182 taking CR into account can be developed based on Eqs. (1), (2) and (4):

$$183 \qquad FOM_{2,a} = T_{avg,a} \cdot \left(\frac{\sin\left(2\left\langle \left| \phi_{meta,a} - \phi_{target,c} \right| \right\rangle \right)}{2\left\langle \left| \phi_{meta,a} - \phi_{target,c} \right| \right\rangle} \right)^2 \qquad (5)$$

$$184 \qquad FOM_{1,c} = T_{avg,c} \cdot \left(\frac{\sin\left(2\left\langle \left| \phi_{meta,c} - \phi_{target,a} \right| \right\rangle \right)}{2\left\langle \left| \phi_{meta,c} - \phi_{target,a} \right| \right\rangle} \right)^2 \qquad (6)$$

$$185 \qquad FOM_{CR} = \frac{FOM_{1,a}}{FOM_{2,a}} \cdot \frac{FOM_{2,c}}{FOM_{1,c}} \qquad (7)$$

186 where $FOM_{2,a}$ and $FOM_{1,c}$ relate to the metasurface's "ghosting" performance on Focal Plane 2 in
187 the amorphous state and Focal Plane 1 in the crystalline state, respectively, and are proportional to
188 the optical efficiencies of the ghost images in both states.
189   The FOMs were evaluated for metalens design variants assembled from meta-atoms within the
190 pool. Specifically, phase masks with phase and amplitude responses of the meta-atoms simulated
191 from full-wave models were employed to simulate the metasurface performance using the
192 Kirchhoff diffraction integral, a physically rigorous form of the Huygens-Fresnel principle[54]. The
193 diffraction integral allows computationally efficient validation of the metalens performance not
194 constrained by the large lens size (1.5 mm × 1.5 mm square aperture). 16 meta-atom geometries
195 which yield the maximum FOM were chosen to assemble the final metalens design (as shown in
196 Fig. 2k). More details on the selected meta-atom shapes and optical responses are available in
197 Supplementary Information, Section II. The phase deviations of the final design (Figs. 2c and 2h)
198 from the ideal phase profile are shown in Figs. 2d and 2i with a negligible average phase error of
199 less than 0.013 λ_0 for both states, root-mean-square (RMS) errors of 0.11 λ_0 and 0.17 λ_0; average
200 meta-atom transmittance was 67% and 71%, in the amorphous and crystalline states, respectively.
201 In contrast, the phase errors on the phantom focal planes are significantly larger (Figs. 2e and 2j).
202 Simulations using the diffraction integral model incorporating the phase/amplitude masks yield
203 Strehl ratios close to unity (> 0.99) for both states and focusing efficiencies of 39.5% and 25.4%
204 in the amorphous and crystalline states, respectively. The optical efficiencies are mainly restricted
205 by the small number of phase discretization levels ($m = 4$) and limited transmittance of the meta-
206 atoms. The simulations further yield power ratios of approximately $P_{1,a} / P_{2,a} = 453$ and $P_{2,c} /$
207 $P_{1,c} = 36$ in amorphous and crystalline states, respectively, corresponding to a theoretical CR of
208 42.1 dB.

209 **Metalens fabrication and characterization**

210 The metalens was patterned in thermally evaporated GSST films on a CaF$_2$ substrate using electron
211 beam lithography (EBL) and standard plasma etching. More details of the metalens fabrication are
212 furnished in the Methods section. Figure 3 presents scanning electron microscopy (SEM) images
213 of the fabricated metasurfaces. The meta-atoms show negligible surface roughness, almost vertical
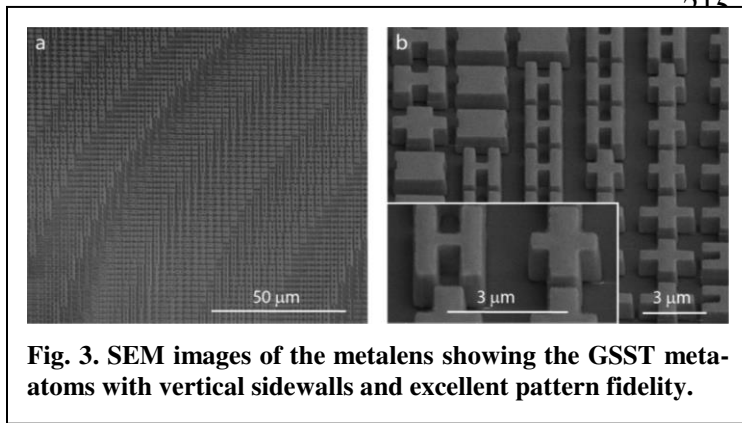214 sidewalls with a sidewall angle > 85°, and excellent pattern fidelity consistent with our design.

Fig. 3. SEM images of the metalens showing the GSST meta-atoms with vertical sidewalls and excellent pattern fidelity.

The metalens was characterized using an external cavity tunable quantum cascade laser (QCL) emitting linearly polarized light at 5.2 µm wavelength. The collimated laser beam was focused by the metalens and images of the focal spots were first magnified with a double-lens microscope assembly (with a calibrated magnification of 120) and then recorded by a liquid nitrogen cooled InSb focal plane array (FPA) camera on the two focal planes ($f_1 = 1.5$ mm and $f_2 = 2$ mm). The focal spot images are shown in Fig. 4 insets and the main panels in Fig. 4 plot the optical intensity profiles across the center planes of the focal spots along with those of ideal aberration-free lenses of the same NAs. The metalens features high Strehl ratios of > 0.99 and 0.97 in the amorphous and crystalline states, respectively, implying that the lens operates in the diffraction-limited regime at both states. We further experimentally measured the focused power ratios between the true and phantom focal spots, yielding $P_{1,a} / P_{2,a} = 10$ and $P_{2,c} / P_{1,c} = 90$. The result corresponds to a large CR of 29.5 dB, the highest reported value to date in active metasurface devices (see Table S3 in Supplementary Information, Section IV).
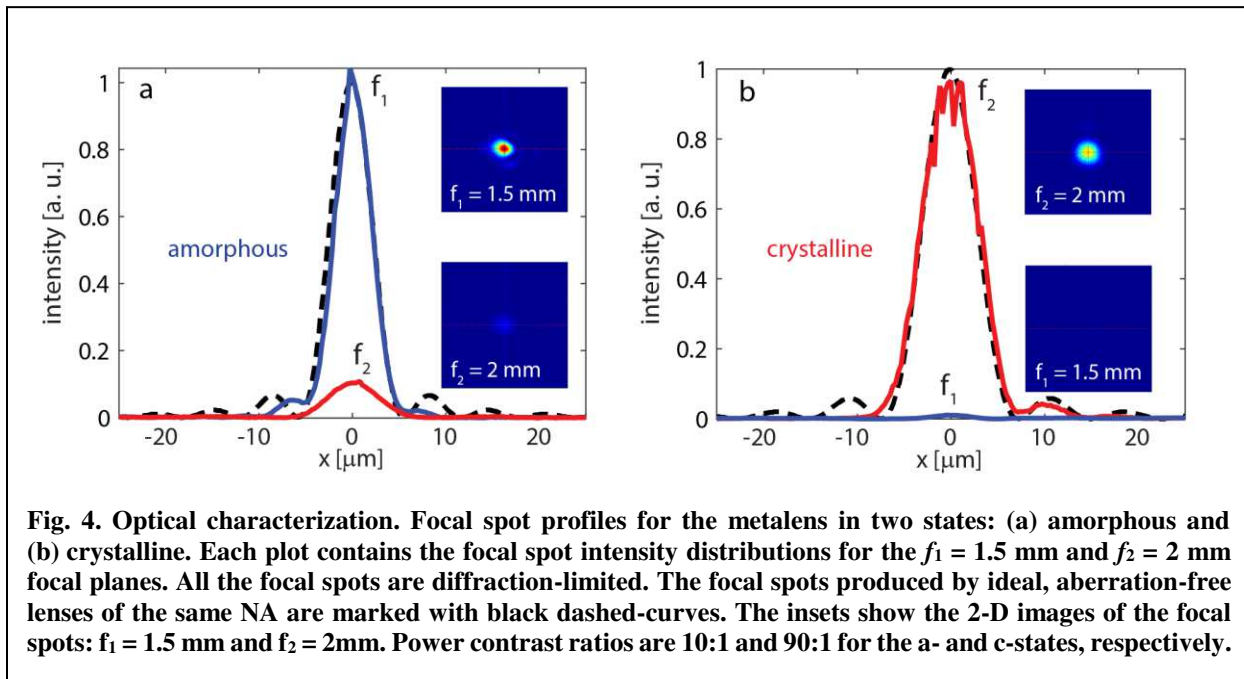

Fig. 4. Optical characterization. Focal spot profiles for the metalens in two states: (a) amorphous and (b) crystalline. Each plot contains the focal spot intensity distributions for the $f_1 = 1.5$ mm and $f_2 = 2$ mm focal planes. All the focal spots are diffraction-limited. The focal spots produced by ideal, aberration-free lenses of the same NA are marked with black dashed-curves. The insets show the 2-D images of the focal spots: $f_1 = 1.5$ mm and $f_2 = 2$mm. Power contrast ratios are 10:1 and 90:1 for the a- and c-states, respectively.

Focusing efficiency of the metalens was quantified following our previously established measurement protocols[55]. Focusing efficiencies of 23.7% and 21.6% were measured for the amorphous and crystalline states, respectively. The difference between the experimental results and theoretical predictions are primarily due to meta-atom geometry and refractive index deviations in the fabricated device. However, the demonstrated performance still represents major improvements over prior state-of-the-art in varifocal metalens (Table S1).

Finally, we demonstrated high-resolution, low-crosstalk imaging using our reconfigurable metalens. Standard USAF 1951 resolution charts in the form of Sn patterns fabricated on CaF_2 discs were used as the imaging objects. The imaging object comprises one or two resolution charts coinciding with the two focal planes ($f_1 = 1.5$ mm and $f_2 = 2$ mm) which are flood-illuminated from the backside using the QCL. The metalens was used as an objective to project the resolution target images onto the camera. Figure 5a shows four images of the resolution charts captured using the setup when only a single resolution target was placed at one of the focal planes. The lens produced clearly resolved images of the USAF 6.2 (half-period 7 μm) and USAF 5.6 (half period 8.8 μm) patterns when the lens was in amorphous and crystalline states, respectively. This result agrees well with theoretical resolution limits of 7 μm and 9 μm in the two states, suggesting that our metalens can indeed achieve diffraction-limited imaging performance. In contrast, no image was observed when the resolution target was placed at the phantom focal plane.

We further show that the metalens can be used for imaging multi-depth objects with minimal crosstalk. In the test, two resolution targets were each positioned at one focal plane with 45° relative in-plane rotation with respect to the other target. At each optical state of the metalens, only one resolution target aligning with the focal plane was clearly imaged with no sign of ghost image resulting from the other target (Fig. 5b). These results prove that the active metalens is capable of diffraction-limited imaging free of optical aberrations and crosstalk across overlapping objects at different depths.
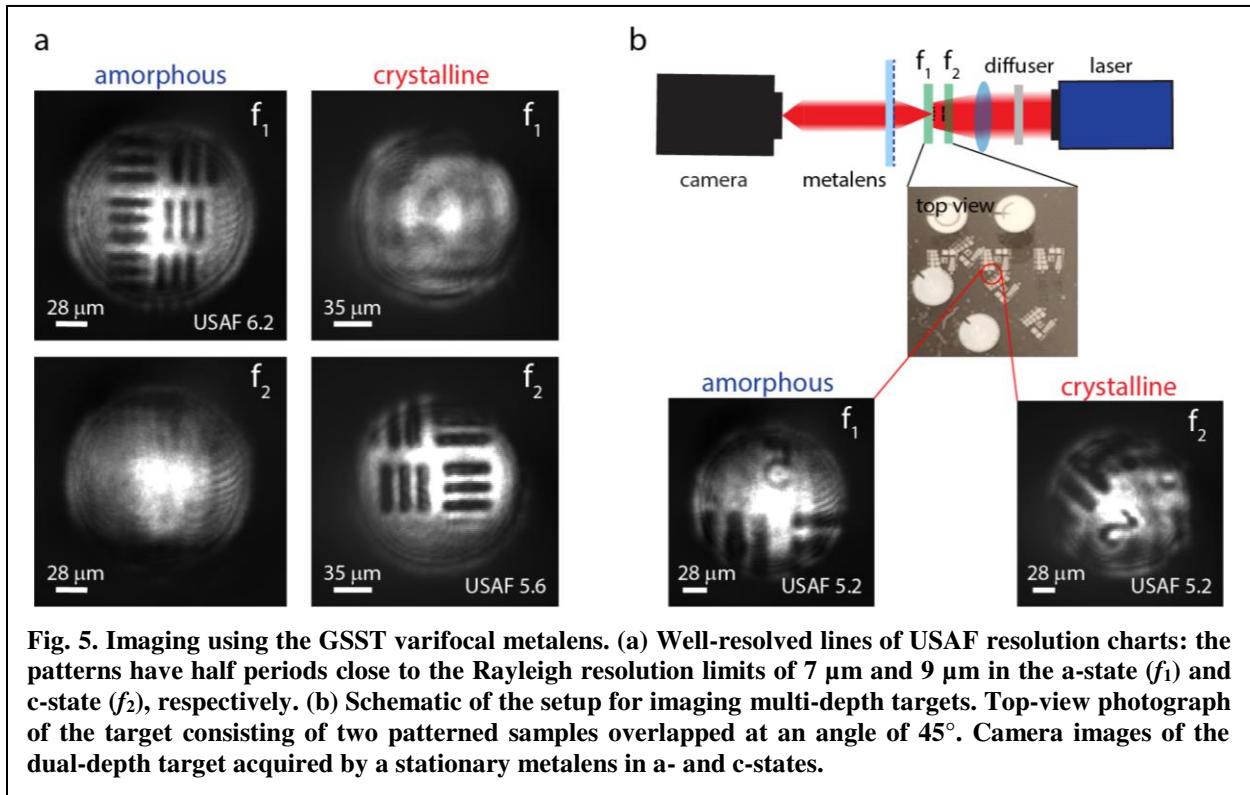

Fig. 5. Imaging using the GSST varifocal metalens. (a) Well-resolved lines of USAF resolution charts: the patterns have half periods close to the Rayleigh resolution limits of 7 μm and 9 μm in the a-state (f_1) and c-state (f_2), respectively. (b) Schematic of the setup for imaging multi-depth targets. Top-view photograph of the target consisting of two patterned samples overlapped at an angle of 45°. Camera images of the dual-depth target acquired by a stationary metalens in a- and c-states.

DISCUSSION

Our work demonstrates that judiciously engineered active metasurfaces can achieve high optical quality in the diffraction-limited regime rivaling the performance of traditional aspheric refractive

267 optics. The high-performance meta-optics as well as the efficient design approach will open up
268 many exciting applications involving reconfigurable or adaptive optics. For instance, the varifocal
269 metalens constitutes a key building block for a parfocal lens (a true zoom lens which stays in focus
270 while changing magnification) widely used in cameras, microscopes, telescopes, and video
271 recorders. Conventional parfocal zoom lenses necessarily involve multiple mechanically moving
272 elements required for aberration compensation while tuning the magnification, which severely
273 compromise the size, complexity, ruggedness, and often image quality. In contrast, our varifocal
274 metalens enables a drastically simplified step-zoom parfocal lens design consisting of only two
275 phase-change metasurfaces patterned on the top and bottom surfaces of a single flat substrate,
276 while maintaining diffraction-limited imaging performance. Besides imaging, the active
277 metasurface can potentially also enable other applications such as beam steering, adaptive optics,
278 and optical spectroscopy[56].
279   Switching from the amorphous to the crystalline phase was accomplished via furnace
280 annealing in our present prototype. Practical deployment of the active, reversible reconfigurable
281 metasurface will necessarily involve electrical switching of O-PCMs. We have recently
282 demonstrated highly consistent electrothermal switching of GSST over 1,000 phase transition
283 cycles using on-chip metal micro-heaters[44]. Additionally, reversible switching of GSST and other
284 phase change materials using transparent graphene and doped Si heaters have also been
285 validated[57–59]. In this regard, the use of GSST rather than the classical GST alloy uniquely benefits
286 from not only GSST's low optical attenuation but also its improved amorphous phase stability.
287 GST boasts a short crystallization time in the nanosecond regime[60], which is useful for ultrafast
288 switching but at the same time also limits the critical thickness amenable to fully reversible
289 switching to less than 100 nm. In comparison, while the detailed crystallization kinetics of GSST
290 has not yet been quantified[44], its crystallization time is likely in the order of microseconds. This
291 much longer crystallization time permits reversible switching of GSST films with thicknesses
292 exceeding 1 μm, presenting a critical benefit for their photonic applications. Indeed, we have
293 recently reported what we believe to be the first electrically reconfigurable metasurface based on
294 O-PCMs at the 1550 nm telecommunication band, where the entire meta-atoms (250 nm in
295 thickness) are made of GSST. The ensuing large optical modal overlap with the active O-PCM
296 enables spectral tuning of resonances across a record broad half-octave band[61]. These advances
297 define a clear path towards practical implementation of the active metasurface design with
298 integrated transparent heaters.
299   Finally, even though our metalens already claims exceptional optical quality, our generic
300 design principle points to several future improvements which can further enhance lens
301 performance and design versatility. Our present metalens uses four discrete phase levels, which
302 imposes ~ 20% efficiency loss due to discretization phase errors[62]. The conventional searching
303 method based on parameter sweeping limits the size of the accessible unit cell library in practice.
304 Increasing the number of phase discretization levels m contributes to mitigating phase errors and
305 increasing focusing efficiency. One can also scale the design approach to three or more arbitrary
306 optical states taking advantage of intermediate states and the large index contrast afforded by O-
307 PCMs[51,52]. In general, an active metasurface with j optical states ($j \geq 2$) each characterized by m
308 phase levels demands a minimum of m^j distinct meta-atoms. The design problem, whose
309 complexity escalates rapidly with increasing m and j, is best handled with deep learning based
310 meta-atom design algorithms[63,64] and will be the subject of a follow-up paper.
311   In conclusion, we propose a non-mechanical active metasurface design to realize binary or
312 multi-configuration switching between arbitrary optical states. We validated the design principle

313 by fabricating a varifocal metalens using low-loss O-PCM GSST, and demonstrated aberration
314 and crosstalk-free imaging. The work proves that non-mechanical active metasurfaces can achieve
315 optical quality on par with conventional precision bulk optics involving mechanical moving parts,
316 thereby pointing to a cohort of exciting applications fully unleashing the SWaP-C benefits of active
317 metasurface optics in imaging, sensing, display, and optical ranging.

318

319 **METHODS**

320 **Metasurface fabrication.** GSST films of nominally 1 μm thickness were deposited onto a double-
321 side polished CaF$_2$ (111) substrate (MTI Corp.) by thermal co-evaporation in a custom-made
322 system (PVD Products Inc.)[65]. The desired film stoichiometry was achieved by controlling the
323 ratio of evaporation rates of two isolated targets of Ge$_2$Sb$_2$Te$_5$ and Ge$_2$Sb$_2$Se$_5$. The deposition rates
324 were kept at 4.3 Å/s (Ge$_2$Sb$_2$Te$_5$) and 12 Å/s (Ge$_2$Sb$_2$Se$_5$) with a base pressure of 2.8×10^{-6} Torr
325 and a sample holder rotation speed of 6 rpm. The substrate was held near room temperature
326 throughout the film deposition process. Thickness of the film was measured with a stylus
327 profilometer (Bruker DXT) to be 1.10 μm (a-state) and 1.07 μm (c-state), indicating 3% volumetric
328 contraction during crystallization similar to other phase change materials[66,67]. The film was
329 patterned via EBL on an Elionix ELS-F125 system followed by reactive ion etching (Plasmatherm,
330 Shuttlelock System VII SLR-770/734). The electron beam writing was carried out on an 800-nm-
331 thick layer of ZEP520A resist, which was spin coated on top of the GSST film at 2,000 rpm for 1
332 min and then baked at 180°C for 1 min. Before resist coating, the sample surface was treated with
333 standard oxygen plasma cleaning to improve resist adhesion. To prevent charging effects during
334 the electron beam writing process, the photoresist was covered with a water-soluble conductive
335 polymer (ESpacer 300Z, Showa Denko America, Inc.)[68]. The EBL writing was performed with a
336 voltage of 125 kV, 120 μm aperture, and 10 nA writing current. Proximity error correction was
337 also implemented with a base dose time of 0.03 μs/dot (which corresponds to a dosage of 300
338 μC/cm^2). The exposed photoresist was developed by subsequently immersing the sample into
339 water, ZED-N50 (ZEP developer), methyl isobutyl ketone (MIBK), and isopropanol alcohol (IPA)
340 for 1 min each. Reactive ion etching was performed with a gas mixture of CHF$_3$:CF$_4$ (3:1) with
341 respective flow rates of 45 sccm and 15 sccm, pressure of 10 mTorr, and RF power of 200 W. The
342 etching rate was approximately 80 nm/min. The etching was done in three cycles of 5 mins with
343 cooldown breaks of several minutes in between. After completing the etching step, the sample was
344 soaked in N-methyl-2-pyrrolidone (NMP) overnight to remove the residual ZEP resist mask. After
345 optical characterization of the metalens in the amorphous (as-deposited) state, the sample was
346 transitioned to the crystalline state by hot-plate annealing at 250°C for 30 minutes. The annealing
347 was conducted in a glovebox filled with an ultra high purity argon atmosphere.

348 **Metasurface characterization.** The metalens sample was positioned on a 3-axis translation stage
349 and illuminated from the substrate side with a collimated 5.2 μm wavelength laser beam (Daylight
350 Solutions Inc., 21052-MHF-030-D00149). The focal spot produced by the metalens was magnified
351 with a custom-made microscope assembly (henceforth termed as magnifier), consisting of lens 1
352 (C037TME-E, Thorlabs Inc.) and lens 2 (LA8281-E, Thorlabs Inc.). The magnified image of the
353 focal spot was captured by a liquid nitrogen cooled InSb FPA with 320×256 pixels (Santa Barbara
354 Infrared, Inc.). Magnification of the microscope assembly was calibrated to be (120 ± 3) with a
355 USAF resolution chart. During focusing efficiency characterization, we measured optical powers
356 of the beam passing through a reference sample (CaF$_2$ substrate with a deposited square gold
357 aperture of same size as the metalens) and the metalens sample. The focusing efficiency is defined

as the ratio of the power concentrated at the focal spot (within a radius of $5\lambda_0$) over the power transmitted through the reference sample. In the metalens imaging test, we illuminated the object with a converging laser beam by placing a Si lens (LA8281-E, Thorlabs Inc.) in front of the object. A pair of singe-side polished Si wafers were inserted into the beam path as diffusers to reduce spatial coherence of the illumination beam and suppress speckles.

Device modeling. The full-wave meta-atom simulations were carried out with a frequency domain solver in the commercial software package CST Microwave Studio. For each meta-atom, unit cell boundary conditions were employed at both negative and positive x and y directions, while open boundary conditions were set along the z-axis. Each meta-atom was illuminated from the substrate side with an x-polarized plane wave pointing towards the positive z direction. Focusing characteristics of the metalens were modeled following the Kirchhoff diffraction integral using a home-made Matlab code. The model starts with computing the Huygens point spread function of the optical system. Diffraction of the wavefront through space is given by the interference or coherent sum of the wavefronts from the Huygens sources. The intensity at each point on the image plane is the square of the resulting complex amplitude sum.

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Author contributions

M.Y.S. fabricated the metalens. S.A., T.G. and C.F. designed and modeled the devices. M.Y.S. and T.G. performed device characterizations. T.G., M.Y.S. and S.A. analyzed the experimental data. M.K. prepared the target materials. Y.Z., P.S., C.R. and Q.D. contributed to device fabrication. F.Y. contributed to optical testing. V.L., J.B.C., C.M.R. and C. R.-B. performed material characterizations. M.Y.S., T.G., and J.H. drafted the manuscript. J.H., T.G., H.Z., K.R. and A.A. supervised and coordinated the research. All authors contributed to revising the manuscript and technical discussions.

Competing financial interests

The authors declare no competing financial interests.

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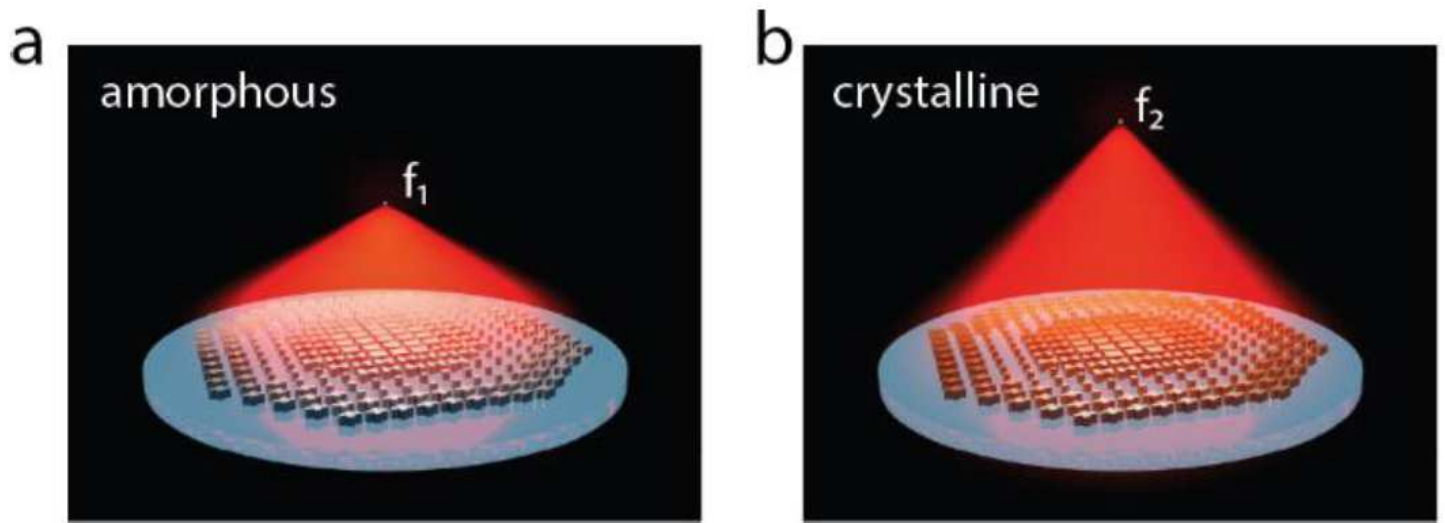532   **38**, 2779–2782 (2013).
533

Figures

Figure 1

Artistic rendering of a reconfigurable varifocal metalens. Incident light is focused on the first focal plane (f1 = 1.5 mm) when the meta-atoms are in the amorphous state and the second focal plane (f2 = 2.0 mm) in the crystalline state.
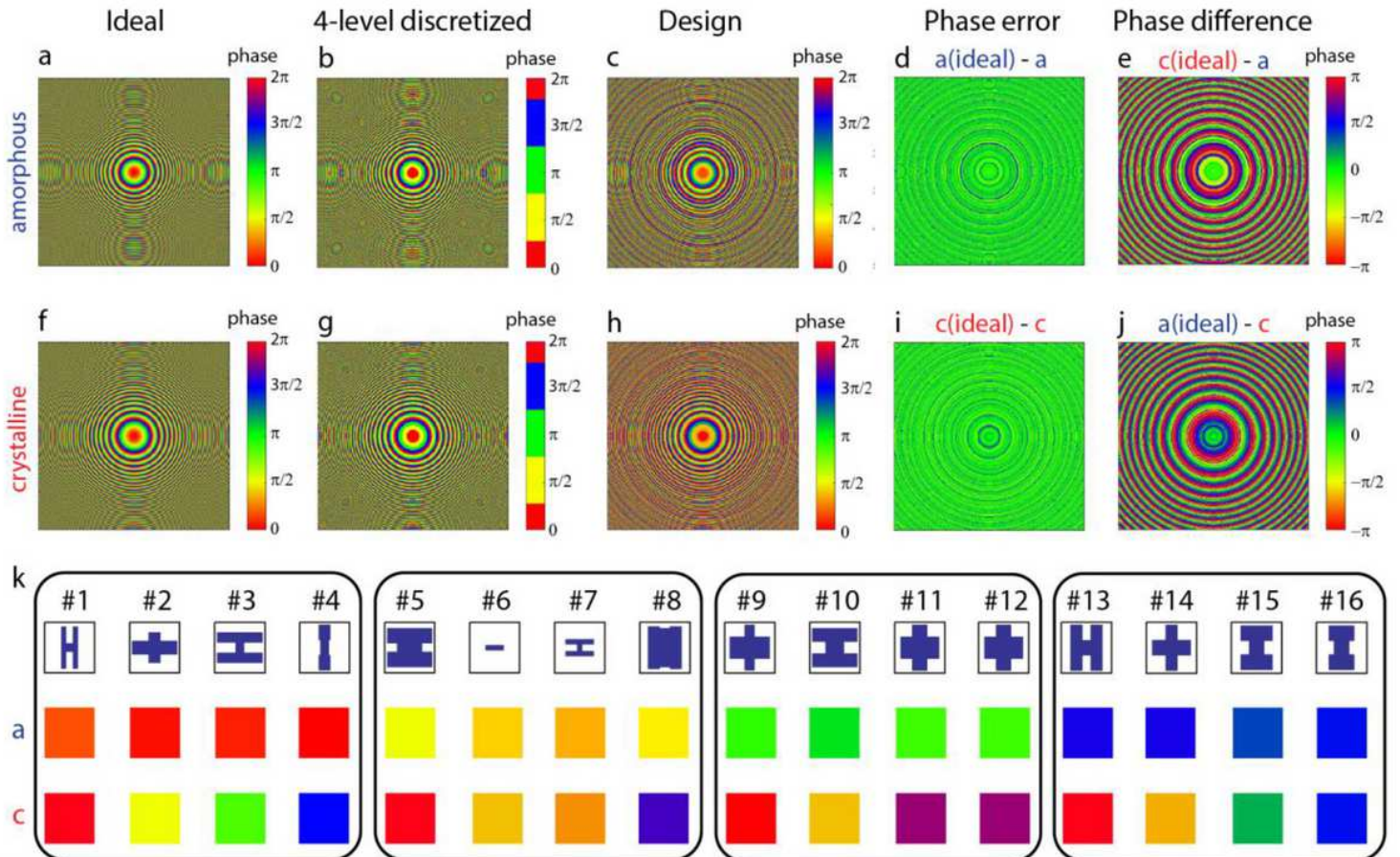
Figure 2

2-D phase maps of the metalens in (a-c) amorphous and (f-h) crystalline states: (a, f) ideal target phase profiles with continuous phase distribution; (b, g) 4-level discretized phase profiles; and (c, h) final design taking into account phase responses of the meta-atoms. (d, e, i, j) Difference between the ideal and final design phase maps at the (d, i) primary and (e, j) phantom focal planes. (k) 16 meta-atoms selected to construct the reconfigurable metalens. Different colors correspond to the phase values shown in (c, h).
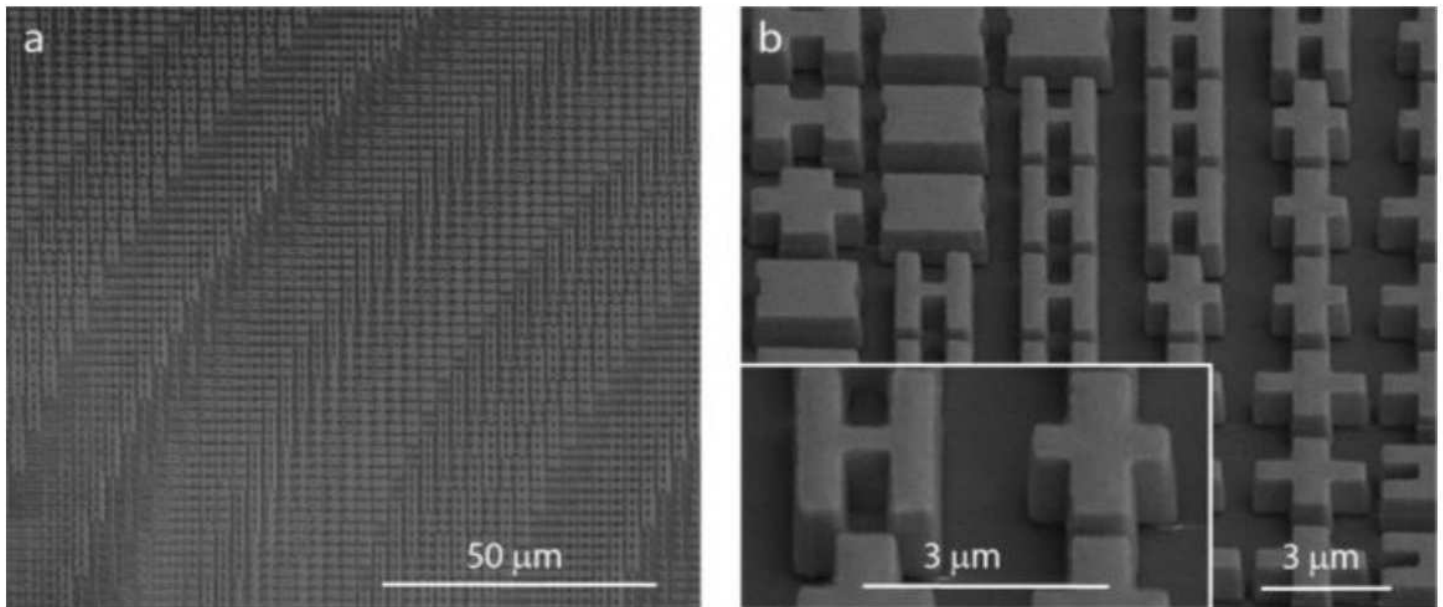

Figure 3

SEM images of the metalens showing the GSST meta-atoms with vertical sidewalls and excellent pattern fidelity.
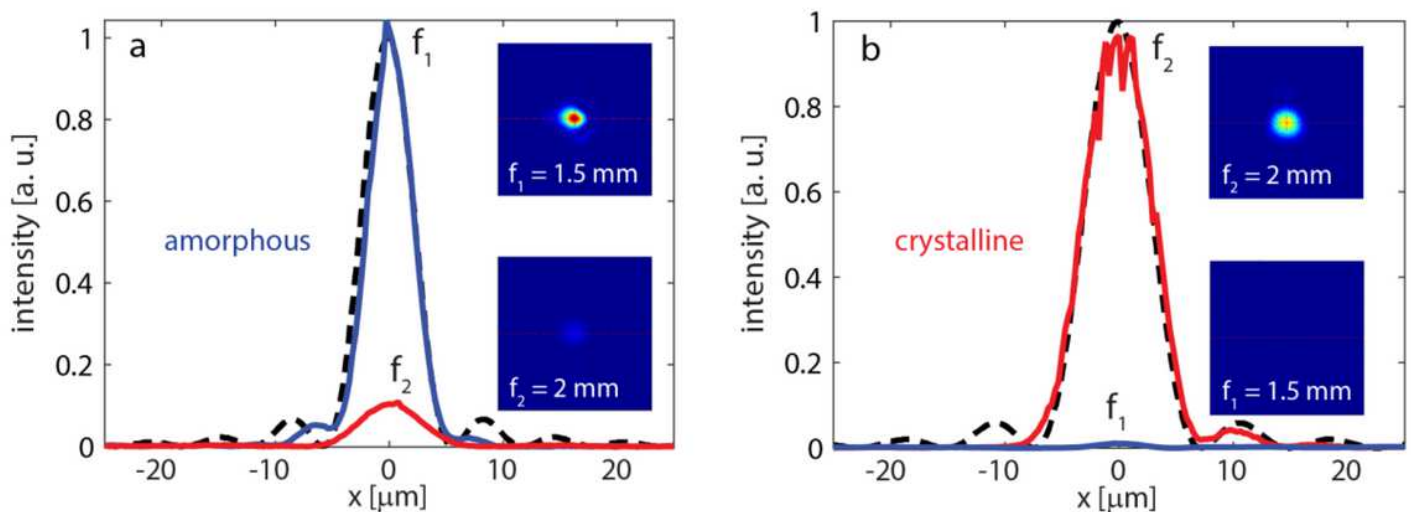

Figure 4

Optical characterization. Focal spot profiles for the metalens in two states: (a) amorphous and (b) crystalline. Each plot contains the focal spot intensity distributions for the f1 = 1.5 mm and f2 = 2 mm focal planes. All the focal spots are diffraction-limited. The focal spots produced by ideal, aberration-free lenses of the same NA are marked with black dashed-curves. The insets show the 2-D images of the focal spots: f1 = 1.5 mm and f2 = 2mm. Power contrast ratios are 10:1 and 90:1 for the a- and c-states, respectively.
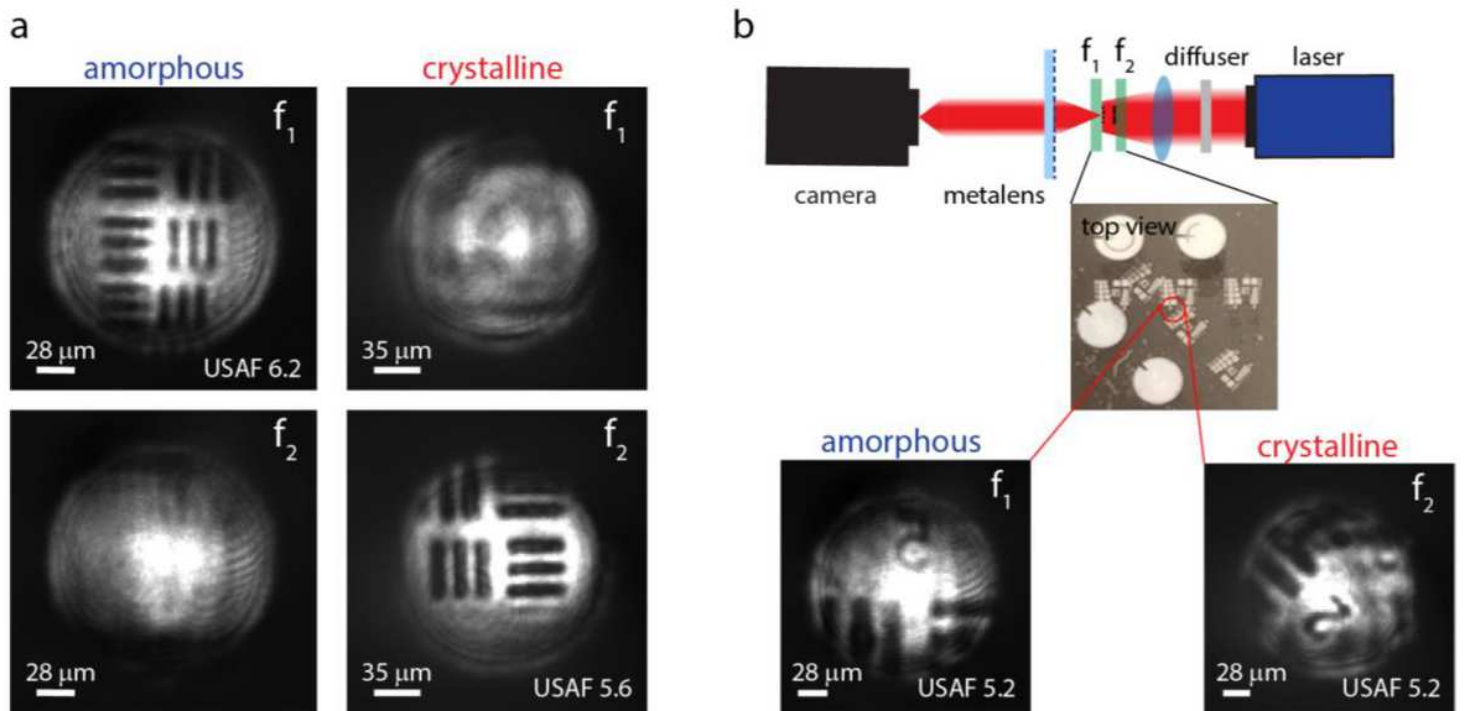

Figure 5

Imaging using the GSST varifocal metalens. (a) Well-resolved lines of USAF resolution charts: the patterns have half periods close to the Rayleigh resolution limits of 7 μm and 9 μm in the a-state (f1) and c-state (f2), respectively. (b) Schematic of the setup for imaging multi-depth targets. Top-view photograph of the target consisting of two patterned samples overlapped at an angle of 45°. Camera images of the dual-depth target acquired by a stationary metalens in a- and c-states.

Supplementary Files

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