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Reduction characteristics of copper oxide in cerium and zirconium oxide systems

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Abstract

The reduction of CuO dispersed on fluorite-type oxide catalysts, namely La-doped CeO₂ and Y-doped ZrO₂ was studied in this work. On both supports distinct copper species were identified as a function of copper content by temperature-programmed reduction (TPR) by H₂ and CH₄, X-ray photoelectron spectroscopy (XPS), X-ray powder diffraction (XRD) and scanning transmission electron microscopy/energy dispersive X-ray (STEM/EDX) analyses. At low copper loading (<15 at%), the copper phase is present as small clusters, which are reduced at lower temperature than bulk CuO. At higher Cu loading (>15 at%), in addition to clusters, larger CuO particles are present which are reduced at higher temperature close to the reduction temperature of bulk CuO. At copper loading lower than ca. 5 at%, copper is present as highly dispersed clusters or isolated Cu ions, which interact strongly with the fluorite-type oxide, thus requiring higher reduction temperature. However, the latter is still below the bulk CuO reduction temperature. Copper is more stabilized when dispersed in Ce(La)O₂ than in Zr(Y)O₂ matrix, so that reduction of copper oxide species requires lower temperatures on the Zr(Y)O₂-based catalysts. The reducibility of the doped ceria is enhanced by the presence of copper in both H₂- and CH₄-TPR. On the other hand no such interaction is present in CuZr(Y)O₂ system. The activity of various copper species for methane oxidation is discussed. © 1998 Elsevier Science B.V. All rights reserved.

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1. Introduction

CeO₂ is used as a promoter in the three-way catalyst (TWC) for automotive emission control and is a component of several oxidation catalysts [1]. Ceria is well known for its high oxygen storage capacity [2–4], stabilization of the surface area of the alumina

support, and interaction with the noble metals Rh, Pt and Pd [1,5–10]. The strong interaction between platinum metals and ceria enhances the metal dispersion and the oxygen storage capacity of ceria. Addition of noble metals (Pt, Pd) increases the reactivity of low-temperature oxygen species formed on ceria [11,12]. As a result, the reducibility of ceria at low temperatures is enhanced [13,14].

Recent reports have shown that the activity of ceria in complete oxidation reactions can be largely enhanced not only by the platinum metals but also

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by transition metals in general [15–17]. Large synergistic effects over copper-containing ceria were reported for CO oxidation [18,19], SO₂ reduction by CO to elemental sulfur [20,21], and the water-gas-shift reaction [22]. In a recent paper, Liu and Flytzani-Stephanopoulos [22] used a physical mixture of nano-CuO particles and ceria to show that association of copper and ceria results in enhanced reducibility of both oxides.

Furthermore, a copper-containing ceria was reported as a very active catalyst for the total oxidation of methane [18,19]. This catalyst showed higher activity than Pt/Al₂O₃ or perovskites [17]. Thus, it may offer a low-cost alternative to PdO_x-based catalysts, which are presently the most active catalysts for the complete oxidation of methane at low temperatures. In the literature, we also find mention of the high methane oxidation activity for copper oxide supported on zirconia [17–19,23].

It is interesting to compare the activity of these two types of copper-containing systems. While both ceria and zirconia can disperse copper oxide [17], the former is a reducible oxide that can itself participate in complete oxidation reactions.

The reducibility of copper species on ceria and zirconia can be used to characterize these systems. Several studies of the ceria reduction characteristics have appeared in the literature, especially of platinum metal-modified ceria, and more recently of solid solutions of ceria with zirconia. A good review is given by Trovarelli [1]. Temperature-programmed reduction (TPR) has been used to characterize the surface and bulk oxygen reducibility of these modified cerium oxide systems [3,4,13,24,25].

TPR has also been used to characterize supported copper oxide catalysts. Typically hydrogen was used as the reductant (H₂-TPR). In their study of deactivation of Cu–ZSM-5 zeolite catalysts for the selective catalytic reduction of NO, Yan et al. [26] used H₂-TPR to compare the reduction of copper on various supports. Bulk CuO has been reported to reduce at 200–300°C [27]. Support effects on the dispersion and reducibility of copper oxide have been documented in the literature [28,29].

In the case of H₂-TPR of silica-supported copper, Delk and Vavere [30] reported two reduction peaks (229°C and 268°C) for 1 and 4 wt% copper, respectively. Yan et al. [26] observed a H₂ consumption peak

at 200°C for 2 wt% Cu on silica. The same authors [26], for 1 wt% Cu on alumina observed reduction of small CuO clusters at 130°C, accompanied by a broad reduction peak in the range 100–500°C, attributed to copper aluminate. The Cu-exchanged ZSM-5 reduction profile had three reduction peaks located at 15°C, 165°C and 275°C [26]. The low-temperature peak (15°C) was assigned to the reduction of bridged oxocations to Cu⁺¹, the 165°C reduction peak was assigned to the reduction of isolated Cu⁺² ions to Cu⁺¹, and reduction of CuO clusters, while the high temperature peak (275°C) was assigned to the reduction of Cu⁺¹ to metallic copper [26,31,32]. Amenomiya et al. [33] observed two reduction peaks in H₂-TPR of CuO/ZrO₂: at low CuO loading (10 wt% CuO) reduction was observed at about 200°C, while at higher CuO loading (40 wt%) a second reduction peak was observed at around 300°C. Kung et al. [34] reported a similar reduction profile of the CuO/ZrO₂ system, but at lower reduction temperatures (134°C for 7.4 wt% copper and both 134°C and 180°C for 33 wt% copper). Dow and Huang [28] reported reduction of 1 and 5 wt% Cu on yttria-stabilized zirconia at 250°C and 274°C, respectively. Two reduction peaks were reported by Liu and Flytzani-Stephanopoulos [22] for physical mixtures of nano-CuO particles and ceria: reduction of copper oxide clusters, strongly interacting with ceria, was observed in the range 125–175°C with a peak at 167°C, while larger CuO nano-particles, non-associated with ceria were reduced at ~200°C. Wrobel et al. [35] observed copper reduction in the range 120–150°C in Cu–CeO₂ mixed oxides (20–67 at% Cu).

Differences in the reduction of copper oxide may be partially attributed to the range of operating conditions used. The type of the support is known to affect particle morphology, adsorption and catalytic properties. Farrauto et al. [36] have shown that the PdO reduction/oxidation hysteresis strongly depends on the nature of the support. In addition, several authors have reported an influence of particle size on the catalytic activity when noble metals are used for methane oxidation. Otto [37] found a maximum in the turnover frequency and a decrease in the apparent activation energy for methane oxidation with increasing Pt content on alumina from 0.03 to 30 wt%. These differences were attributed to the existence of two distinct Pt entities, namely dispersed and particulate Pt. Recently,

Fujimoto et al. [38] showed that the turnover rate of methane oxidation increases as the crystallite size increases up to 10 nm, while the activation energy stays constant, when Pd is supported on alumina or zirconia.

In this study we examined the interaction of CuO with two fluorite-type oxides, namely La-doped CeO₂ and Y-doped ZrO₂. Different copper species are formed on these supports depending on the copper content. We used H₂-TPR to study the reducibility of CuO species formed as a function of the CuO particle size and the type of the support. Catalyst structure was studied by X-ray powder diffraction (XRD), X-ray photoelectron spectroscopy (XPS) and scanning transmission electron microscopy/energy dispersive X-ray analysis (STEM/EDX). CH₄-TPR was used to study the reactivity of various copper species with methane. Finally, the activity of different copper species in the complete oxidation of methane was examined and discussed in terms of the light-off behavior and kinetic performance.

2. Experimental

The Cu-modified fluorite-type oxides were prepared in bulk form by coprecipitating nitrate salts by urea at about 100°C, according to a technique described by Amenomiya et al. [33] and Kung et al. [34]. After coprecipitation, the resulting gels of Ce and Zr were vigorously boiled for 8 h at 100°C. After aging, the precipitate was filtered, washed twice in boiling deionized water, and dried in a preheated vacuum oven (80–100°C) for 8–10 h. Dried samples were crushed and calcined in air for 6–8 h at 650°C (heating rate was 2°C/min). Selected catalysts were immersed in 70% nitric acid for 8 h to dissolve CuO particles, washed with deionized water, dried at 100°C (8–10 h) and calcined at 650°C for 4 h.

The catalyst composition throughout the paper is expressed as at% (metal/total metals × 100%). All catalysts used in this study were doped with 4.5 at% La (for CeO₂-based catalysts) or 4.5 at% Y (for ZrO₂-based catalysts).

For bulk composition analysis the CeO₂-based powder was dissolved in nitric acid containing a small amount of H₂O₂ diluted with deionized water and the resulting solution was analyzed by Inductively

Coupled Plasma (ICP) Atomic Emission Spectrometry (Perkin Elmer Plasma 40). ZrO₂-based catalysts could not be dissolved and analyzed by this method.

XRD analysis of catalyst samples was used for crystal phase identification. XRD was performed on a Rigaku 300 X-ray Diffractometer with Rotating Anode Generators and monochromatic detector using Cu K_α radiation.

The catalyst microstructure analysis was performed on a Vacuum Generator HB603 STEM equipped with a X-ray microprobe of 0.14 nm optimum resolution for EDX. For STEM analysis, the catalyst powder was dispersed on a nickel grid coated with a carbon film and elemental maps were obtained on a 128 × 128 data matrix.

The catalyst surface composition was studied by XPS using a Perkin Elmer-5100 system. A Mg electron source was used with a power setting at 300 W. Samples were introduced in the vacuum chamber without any pretreatment. The binding energy was adjusted to the C1s peak at 284.6 eV, which existed in all measurements. It is known that supported copper oxide can be reduced in the vacuum chamber. As in previous study of CuCe(La)O₂ by Liu and Flytzani-Stephanopoulos [19], each sample was analyzed after 1 h in the vacuum, to obtain stable spectra. Data were collected in the Multiplex mode with about 1 h acquisition time.

TPR studies with H₂ and CH₄ as reductants were performed in a Cahn 121 thermogravimetric analyzer (TGA). Typically about 5 mg of catalyst was used in the TGA for TPR analysis. Prior to reduction the catalyst was heated to 200°C (10°C/min) and left at that temperature for 30 min in 500 cm³/min (STP) He. The reduction gas was typically 5% H₂/He (or 5% CH₄/He) mixture flowing at 500 cm³/min (STP). The heating rate was typically 5°C/min.

CH₄-TPR by methane was also performed in a laboratory-scale packed-bed reactor. Typically 200 mg catalyst was used for testing. Pretreatment included heating the catalyst in a flow of 10% O₂/He mixture (60 cm³/min (STP)) to 650°C at a heating rate 10°C/min, followed by cooling to room temperature in O₂/He mixture, and flushing with He at room temperature. A 5% CH₄/He gas mixture at a flow rate of 60 cm³/min (STP) was used for reduction. The outlet gas was analyzed by a quadrupole mass spectrometer (MKS-model RS-1).

All catalysts were tested in a laboratory-scale packed-bed flow reactor, which consisted of 1 cm ID \times 50 cm long quartz tube with a porous quartz frit placed at the middle. An electric furnace was used to heat the reactor. Temperature was monitored by a K-type thermocouple placed at the top of the catalyst bed, and controlled by a Wizard temperature controller. The flow of reacting gases was measured by mass flow meters. The typical feed gas was 1% CH₄, 8% O₂ and balance He. All gases were certified calibration gas mixtures. The catalyst loading was 150 mg unless otherwise noted. The catalysts were tested as prepared without any pretreatment (particle size $<153\ \mu\text{m}$), and conversion measurements were conducted in ascending temperature mode (in 50°C steps), so that the light-off behavior could be recorded. These were followed by descending temperature tests (fall-off) to check for possible catalyst deactivation or hysteresis phenomena. A fixed contact time of 0.09 g s/cm³ (STP) was used in these experiments unless otherwise noted. The product gas stream was analyzed by an HP 5880A gas chromatograph equipped with a 1/4 in. Carbosphere column (for CO, CO₂ and CH₄ separation) and a thermal conductivity detector (TCD).

For kinetic measurements, the reactor was operated in the differential mode with the conversion not exceeding 10%. The total flow rate was 200 cm³/min (STP). The catalyst was diluted by silicon carbide particles to achieve the short contact times (0.024 g s/cm³) needed for operation in the kinetically controlled regime. The catalyst particle size used in the kinetic experiments was $<50\ \mu\text{m}$.

3. Results and discussion

3.1. Complete oxidation of methane activity tests

The activity of Cu-modified Ce(La)O₂ and Zr(Y)O₂ catalysts for the complete oxidation of methane was examined in terms of light-off behavior as shown in Fig. 1(a) and (b). At a contact time 0.09 g s/cm³ (STP), equivalent to a gas hourly space velocity, GHSV=72 000 h⁻¹, both CuCe(La)O₂ and CuZr(Y)O₂ are active for complete methane oxidation to CO₂ and H₂O in the temperature range 300–550°C. Only CO₂ was detected as the oxidation product under both oxygen-rich and oxygen-lean (data not shown)

conditions. CeO₂ itself is an active catalyst for the complete oxidation of methane [18,19,39] at temperatures higher than 400°C (Fig. 1(a)). Addition of Cu shifts the light-off curve to lower temperatures on both types of supports, indicating the formation of new active sites. A shift of more than 100°C is observed for both the 10% and 90% conversion of methane in Fig. 1(a) for copper loading up to 20 at%. At 40 at% Cu, the light-off performance is between the low copper content CuCe(La)O₂ and the Ce(La)O₂ catalysts. Similar trends are observed in Fig. 1(b) for the CuZr(Y)O₂ and Zr(Y)O₂ systems. In addition to CO₂, CO was detected as the oxidation product over Y-doped zirconia (in the absence of copper) as noted in Fig. 1(b). Undoped zirconia (monoclinic) is inactive for the complete oxidation of methane (Fig. 1(b)) in the temperature range studied. Different observations were made by Choudhary et al. [23] who reported $\sim 30\%$ conversion of methane at 600°C (1% CH₄ in air, GHSV=51 000 h⁻¹) on monoclinic zirconia (no CO was detected). However, Zamar et al. [39] reported only 5% methane conversion over zirconia at the same temperature (1% CH₄, 4% O₂, GHSV=34 000 h⁻¹) with significant amounts of CO produced (crystal structure was not reported).

3.2. Catalyst characterization

The conventional N₂O adsorption/decomposition method [40] could not be used to estimate the copper particle size because of the significant participation of CeO₂. However, STEM, having both high magnification and elemental analysis function, was found to be effective for the CuCe(La)O₂ catalyst characterization [17].

Fig. 2 shows STEM/EDX elemental mapping of copper in Zr(Y)O₂ catalysts. At low content ($<5\ \text{at}\%$), copper is well dispersed in the zirconia matrix (Fig. 2(a)). Atomic dispersion of Y was observed indicating the formation of oxide solid solution. This agrees with our XRD data (see below), where only the phase of cubic zirconia was observed. Addition of more copper (up to 15 at%) results in the formation of clusters, and their aggregation to larger particles ($\sim 10\ \text{nm}$), which are still dispersed in the zirconia matrix as shown in Fig. 2(b). Elemental mapping of 40% CuZr(Y)O₂ catalysts shows the presence of large CuO particles (Fig. 2(c)). Large CuO particles are

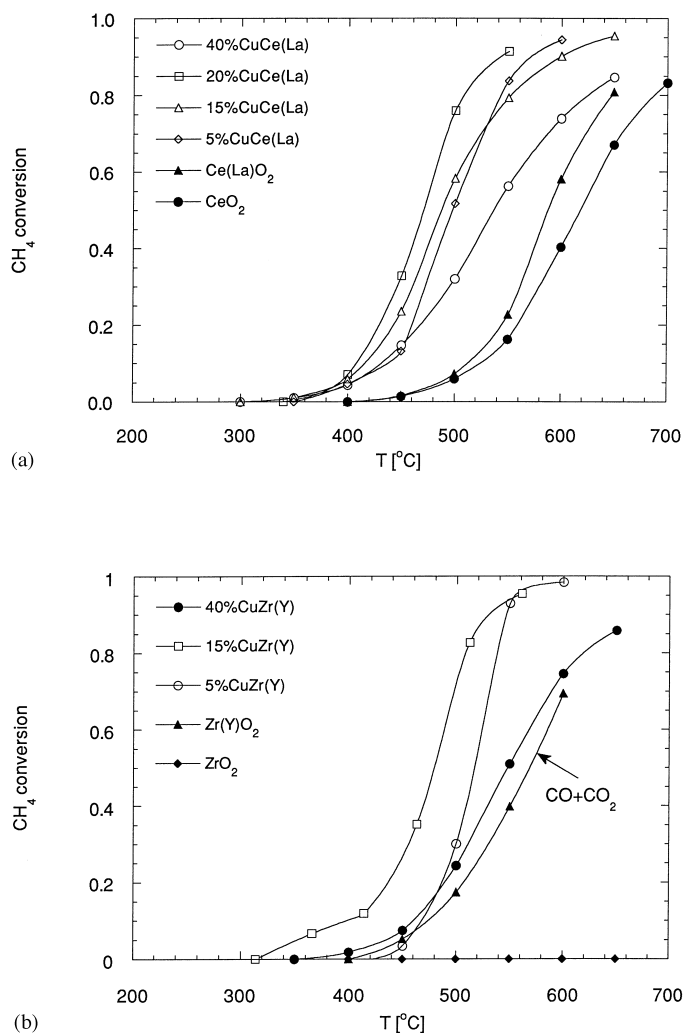


Fig. 1. (a) Activity of various Cu-modified Ce(La)O_2 -based catalysts: 2% CH_4 , 16% O_2 , balance He, 0.09 g s/cm^3 (STP); CeO_2 : 70.2 m^2/g ; Ce(La)O_2 : 69.1 m^2/g ; 5% CuCe(La) O_2 : 92.1 m^2/g ; 15% CuCe(La) O_2 : 32.3 m^2/g ; 20% CuCe(La) O_2 : 49.2 m^2/g ; 40% CuCe(La) O_2 : 36.5 m^2/g . (b) Activity of various Cu-modified Zr(Y)O_2 catalysts: 2% CH_4 , 16% O_2 , balance He, 0.09 g s/cm^3 ; ZrO_2 : 43.5 m^2/g ; Zr(Y)O_2 : 101.2 m^2/g ; 5% CuZr(Y) O_2 : 94.6 m^2/g ; 15% CuZr(Y) O_2 : 44.1 m^2/g ; 40% CuZr(Y) O_2 : 29.6 m^2/g .

covered by zirconia. However, the remaining copper is well dispersed in the zirconia matrix. Large CuO particles were removed with nitric acid treatment, as shown in Fig. 2(d). In addition, Fig. 2(d) shows that not all copper was dissolved in nitric acid, indicating that well dispersed copper clusters interact strongly with the zirconia support. This is similar to what has been reported by Liu [17] for the CuCe(La)O_2 system. It is interesting to note that zirconia is present as small (<15 nm) crystallites after calcination at 650 °C.

In their study of CuCe(La)O_2 catalysts, Liu and Flytzani-Stephanopoulos [19] showed that Cu in small amounts (few percent) associates strongly with the cerium oxide matrix. Clusters of copper (few nm) well dispersed in the cerium oxide matrix were clearly observed. At higher Cu loading, in addition to clusters, larger CuO particles (>10 nm) were formed. At high Cu contents (50 at%), bulk CuO particles were covered with smaller cerium oxide particles. On the other hand, at a very low content of copper (1 at%) atomic

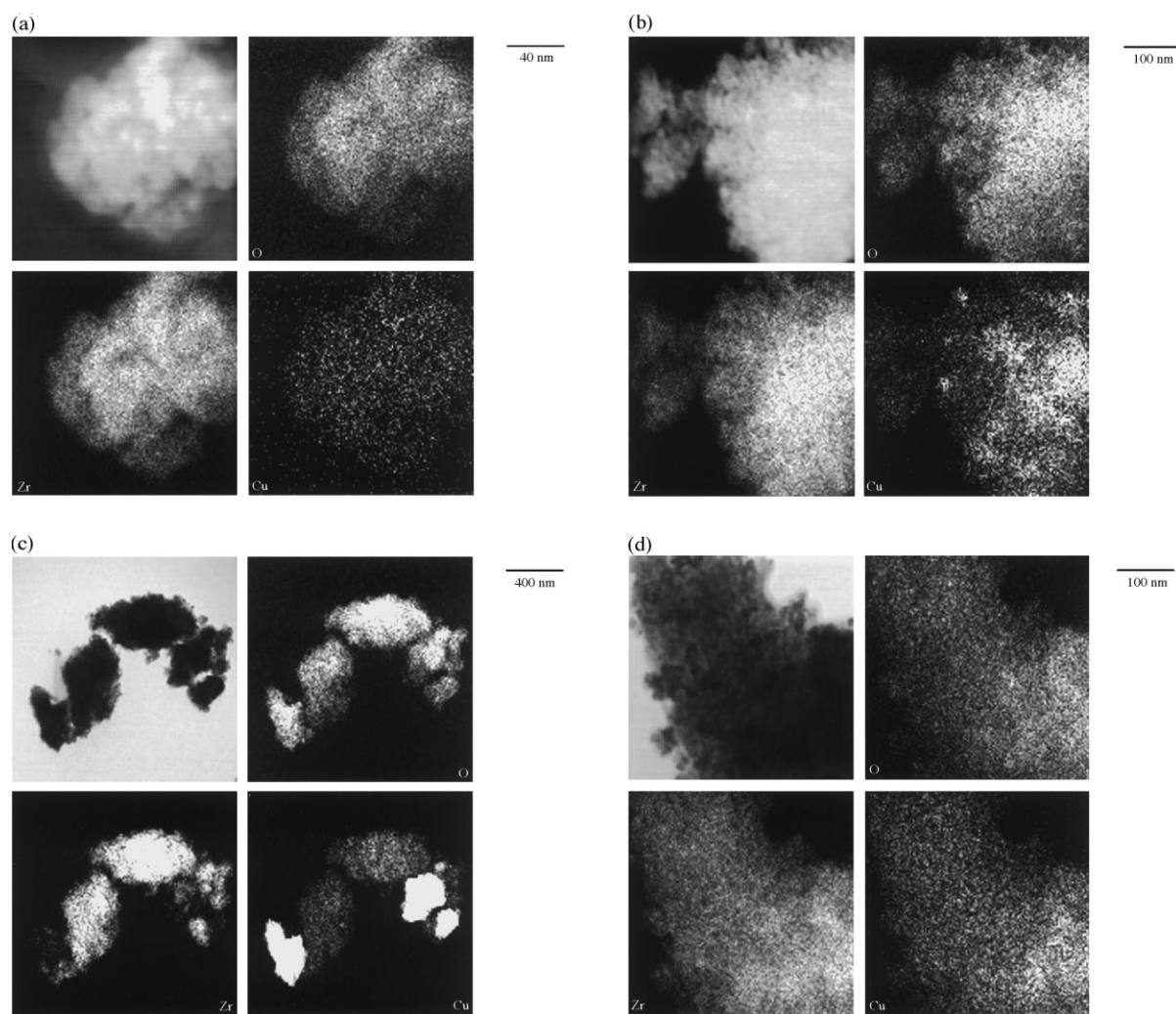


Fig. 2. STEM/EDX elemental mapping of Cu-modified Zr(Y)O_2 -based catalysts: (a) 5% CuZr(Y)O_2 ; (b) 15% CuZr(Y)O_2 ; (c) 40% CuZr(Y)O_2 ; (d) 40% CuZr(Y)O_2 after nitric acid treatment.

dispersion of copper in the cerium oxide matrix was possible by calcining in N_2 at low temperature (500°C). High-temperature treatment, however, drove the copper from the bulk to the surface, and caused the formation of copper clusters [19].

XRD analysis of Cu-modified CeO_2 and ZrO_2 catalysts did not identify the CuO phase for Cu contents lower than 15 at%. In a previous study by Liu and Flytzani-Stephanopoulos [19], XRD analysis of CuCe(La)O_2 catalysts with various copper contents identified CuO only at Cu levels higher than 15 at%. Similar behavior was found here for the CuZr(Y)O_2

catalysts as shown in Fig. 3. For Cu loading <15 at% only the zirconia phase was observed. At higher Cu loading, CuO reflections were observed indicating the formation of bulk CuO . As in the case of ceria, the type of CuO formed at low and high loading is different. Treating the catalyst overnight in nitric acid resulted in the removal of bulk CuO particles while highly dispersed clusters could not be removed. Nano-sized copper clusters identified by STEM/EDX are not detected by XRD. At low Cu loading CuO is either in the zirconia lattice as indicated by Choudhary et al. [23] or it is strongly bound and well dispersed on the

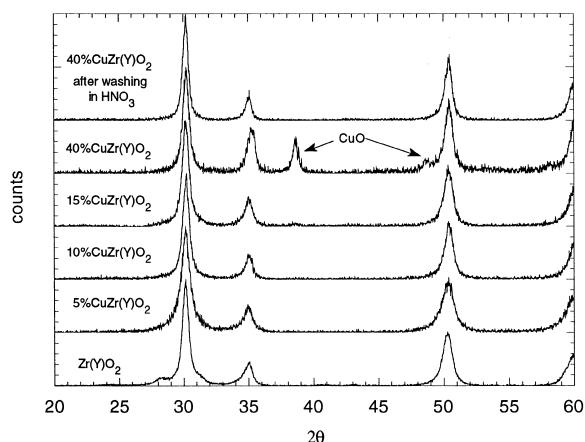


Fig. 3. XRD pattern of CuZr(Y)O_2 catalysts with different Cu content.

surface of zirconia. In the absence of copper, the major phase is cubic zirconia with trace amounts of the monoclinic phase, which can be seen at low diffraction angles (Fig. 3). In Cu-containing catalysts, only the presence of cubic zirconia is observed. This is in agreement with the work of Choudhary et al. [23], who reported the stabilization of cubic zirconia by the addition of transition metals. This means that some of the copper (apparently a very small amount) is incorporated in the zirconia lattice.

Catalyst surface composition was studied by XPS. Fig. 4 shows $\text{Cu}2p$ XPS of various CuZr(Y)O_2 catalysts. Binding energy of 933.0–933.8 eV for the

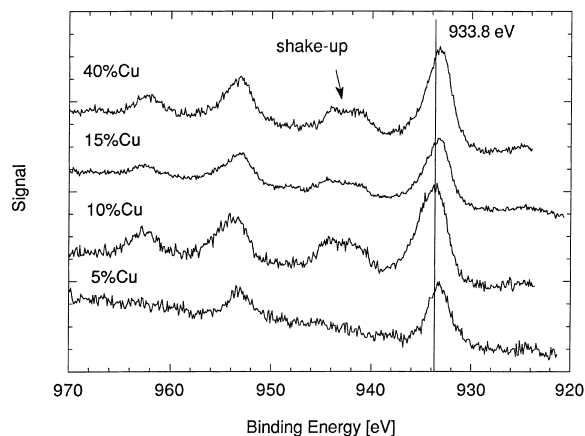


Fig. 4. $\text{Cu}2p$ XPS of CuZr(Y)O_2 catalysts.

Table 1

$\text{Cu}2p_{3/2}$ binding energies and surface composition determined by XPS of CuZr(Y) catalysts

Catalyst	$\text{Cu}2p_{3/2}$ binding energy (eV)	Surface composition (at% Cu)
5% CuZr(Y)	933.3	10.2
10% CuZr(Y)	933.7	25.9
15% CuZr(Y)	933.3	27.4
40% CuZr(Y)	933.2	36.99

$\text{Cu}2p_{3/2}$ peak and shake-up peaks are characteristic for CuO, while lower binding energy (932.2–933.1 eV) and absence of shake-up peaks is characteristic for Cu_2O [41]. The binding energy of $\text{Cu}2p_{3/2}$ peaks are listed in Table 1 for different copper contents. Our results indicate that copper is present as CuO at copper contents higher than 10 at% as indicated by shake-up peaks in Fig. 4. The absence of shake-up peaks in 5% CuZr(Y)O_2 catalysts suggests the presence of reduced copper species. It seems that small clusters of copper present at low copper contents, which could not be dissolved by nitric acid and which are identified by STEM (Fig. 2) do not have the identity of CuO. However, the measured binding energy is slightly higher than that for Cu_2O . It is known that nanosize particles have properties different than bulk oxides, and this mixed oxidation state could be the result of the defective structure of the small clusters. It is also possible that oxygen vacancies in Zr(Y)O_2 stabilize the Cu^+ species as was postulated by Dow and Huang [28] and Dow et al. [29]. Surface composition analysis shows that copper is mostly at the catalyst surface. Up to 15 at%, the surface copper content is higher than the bulk (Table 1). Only at 40 at% Cu, copper surface content is lower than the bulk. This is in agreement with STEM/EDX data which showed that excess copper at this high loading forms bulk CuO particles, which are covered by smaller zirconia particles, so that they are not detected by XPS. Similar behavior was previously reported for CuCe(La)O_2 [22,23].

3.3. TPR experiments

3.3.1. H_2 -TPR

In the TPR experiments reported here, TPR profiles were obtained by following the weight change of the

sample in the TGA. The experimental conditions used are different from those usually employed in TPR studies. A typical experimental setup for TPR includes a microreactor that can be heated by a furnace [42]. The uptake of hydrogen is then recorded as a function of temperature using a TCD. In this study, we performed TPR in the TGA using a small amount of catalyst (5 mg). Since reduction was followed by recording the weight change, the TPR profiles reflect changes occurring on the catalyst (water desorption) rather than H_2 uptake. In their study of ceria reduction by hydrogen, Zotin et al. [43] have shown that the extent of ceria reduction at low temperatures can be overestimated if only H_2 consumption is measured due to hydrogen adsorption on partially reduced ceria. In the conventional TPR method where hydrogen consumption is recorded using a TCD, typical flow conditions (low flow rate) do not provide effective water removal and hydrogen concentration changes throughout the catalyst bed. The advantage of using TGA experiments is that high flow rates are used, so that external mass transfer resistance is eliminated and H_2 consumption is much lower than the total H_2 supply, so that the hydrogen concentration is constant throughout the reduction process.

The reduction profile is markedly affected by the operating conditions, such as the initial amount of reducible species, total flow rate, hydrogen concentration, and heating rate, as shown by Fierro et al. [27], Malet and Caballero [44] and Monti and Baiker [45].

Interpretation of TPR profiles can be further complicated by H_2 adsorption/desorption phenomena (e.g. H_2 adsorption on or desorption from reduced metal or support sites), as pointed out recently by Fierro et al. [27] and Zotin et al. [43]. It is also important to note that adsorption/desorption of the reduction product (water) on the support can influence the TPR profile as discussed by Bethke et al. [46]. The typical TPR characteristics, namely, the temperature corresponding to the maximum reduction rate, and the shape of the profile itself, are affected by experimental operating variables [44,45]. Thus, it is important to carefully account for such effects in planning the TPR experiments.

The effect of operating conditions on the TPR profile of 15% CuZr(Y)O₂ catalyst was studied by changing the total flow rate and the heating rate. There was an effect of operating conditions on the maximum temperature peak and peak shape. In all experiments the initial amount of reducible species was approximately the same. When the flow rate was decreased from 500 to 300 cm³/min for the same heating rate, the peak maximum shifted slightly to higher temperatures (by 7°C). Also as the heating rate increases for the same flow rate, the peak becomes broader and as a consequence, the peak maximum shifts to higher temperature (by 10°C). The same effect of the operating conditions on the peak position was observed for the 5% CuZr(Y)O₂ and 15% CuCe(La)O₂ catalysts.

TPR profiles of CuZr(Y)O₂ catalysts with different copper loading are shown in Fig. 5. The reduction

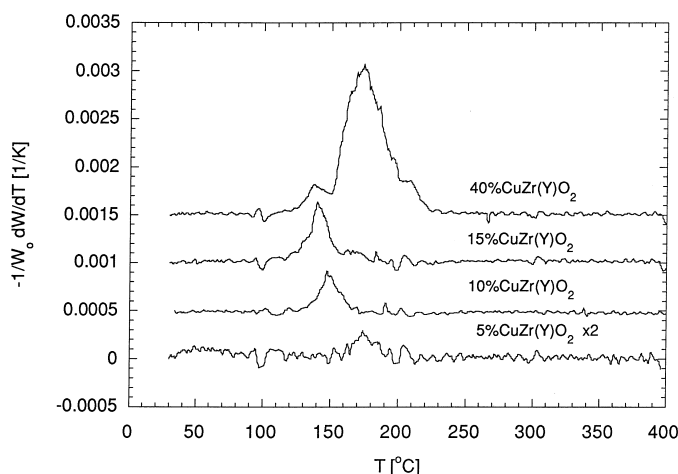


Fig. 5. H_2 -TPR of CuZr(Y)O₂ catalysts: TGA, 500 cm³ min⁻¹ (STP), 5% H_2 /He, 5°C/min.

profile changes significantly as the copper loading increases. The 10% CuZr(Y)O₂ gives only one reduction peak with a maximum at 140°C. As the Cu loading increases from 10% to 15%, a second reduction peak appears with a maximum at about 165°C. At a very high Cu content (40 at%), reduction starts at about 120°C, a large reduction peak is observed at 175°C and a small reduction peak at about 140°C. Similar reduction behavior was reported by Amenomiya et al. [33] and Kung et al. [34] for Cu–ZrO₂. Large differences in the reduction profiles between catalysts with different Cu contents suggests that the state of Cu significantly changes as the Cu content changes. For a low Cu content (5 at%), reduction starts at about 150°C and the peak maximum is observed at

175°C. The reduction extent calculated from the weight change is slightly lower than that necessary for the complete reduction of CuO to metallic copper (based on the nominal catalyst composition). Previous studies of Cu–ZrO₂ systems [33,34] have reported that complete CuO reduction occurs.

A similar effect of Cu loading is observed for the CuCe(La)O₂ catalysts as shown in Fig. 6. The reduction extent corresponds to complete reduction of CuO to Cu as shown in Table 2. At least three different Cu species are observed. At low Cu content (10–15 at%) the maximum reduction rate was observed at around 160°C. For the catalyst with high Cu content (40 at% Cu), reduction starts around 160°C, and the temperature for maximum reduction rate is observed at 200°C.

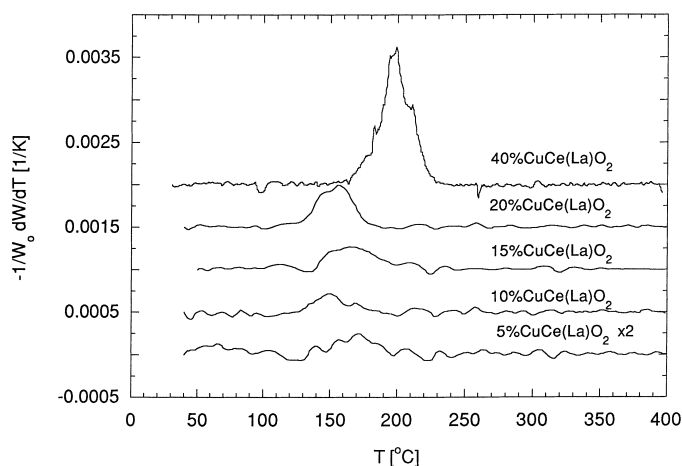


Fig. 6. H₂-TPR of CuCe(La)O₂ catalysts: TGA, 500 cm³ min⁻¹ (STP), 5% H₂/He, 5°C/min.

Table 2

Reduction extent of different CuCe(La)–O catalysts in H₂-TPR

Catalyst	Cu (at%)	CuO (wt%)	% Weight change for CuO reduction ^a	CuO peak area (wt%) ^b
5% CuCe(La)	4.94	2.35	0.47	0.83
10% CuCe(La)	9.00	4.37	0.88	1.06
15% CuCe(La)	12.87	6.39	1.29	1.31
20% CuCe(La)	17.60	8.98	1.81	1.88
HNO ₃ -washed				0.81
25% nano-CuO–CeO ₂	25.00	13.35	2.69	3.1
40% CuCe(La)	40.00	23.55	4.74	4.56
HNO ₃ -washed				0.6

^a Calculated for complete reduction of CuO to Cu.

^b Determined from weight change between 100°C and 250°C.

Finally, at very low levels of copper, similar to the case of 5% CuZr(Y)O₂, the 5% CuCe(La)O₂ material shows a broad reduction peak with a maximum at about 175°C.

The observed reduction behavior may be attributed to structural differences described above for different Cu contents. With Cu content in the range 5–20 at%, copper is mainly at the surface in the form of small copper clusters (Fig. 2(b) in [19]), which are reduced more easily than bulk CuO. The reduction peak at 150–160°C is 40–50°C lower than the peak temperature for bulk CuO reduction. At low Cu loading (~5%), Cu is present as highly dispersed clusters or as isolated Cu ions. Copper ions strongly interact with support, and reduction requires higher temperature of 175°C (Fig. 6). It is also possible that reduction at low Cu contents requires diffusion of H₂ into the lattice, or diffusion of lattice oxygen to the surface. Finally, at high Cu loading (40%), copper is mainly present as larger particles (Fig. 2(c)), and the reduction temperature approaches that for bulk CuO (230°C as reported by Fierro et al. [27]).

Fig. 7 compares the TPR profiles of several CuCe(La)O₂ catalysts with a catalyst prepared by mixing nano-CuO powder with CeO₂. The reduction profile of nano-CuO catalyst has two peaks: the first one at 150°C was assigned to small CuO crystallites in contact with CeO₂ [22]; the second peak at 180°C was assigned to larger CuO particles not in intimate

contact with CeO₂. Wrobel et al. [35] also observed lower reduction peak temperatures for the Cu–CeO₂ system (~130°C) in materials prepared by coprecipitation of corresponding nitrates by sodium hydroxide. Comparison with TPR profiles of coprecipitated catalysts suggests that the low TPR peaks of coprecipitated catalysts should be assigned to dispersed small CuO clusters in contact with CeO₂, while the high temperature peak should be assigned to larger CuO particles not in contact with CeO₂. Previous work of Liu [17] using STEM/EDS, XRD and XPS found that copper exists in CuCe(La)O₂ catalysts in three states: isolated Cu²⁺ ions, small clusters of CuO_x and as CuO particles. The reducibility of these species in H₂ is different. While the clusters are reduced at ~130–160°C, the larger CuO particles have more of the bulk oxide character and are reduced at ~200°C. We believe that the intermediate temperature of 180°C is characteristic of the reduction of isolated ions strongly associated with the support.

Reduction of Cu–ZrO₂ catalysts was studied by Amenomiya et al. [33]. At low Cu content (14.7 at%), the maximum reduction rate was observed at 200°C, whereas at high Cu content (50 at%), two reduction peaks were observed, a low-temperature one at 200°C and one at a high temperature, 300°C. Kung et al. [34] reported much lower temperatures for the reduction of Cu–ZrO₂ catalysts. For 11 at% Cu they observed a maximum reduction rate at 134°C, while

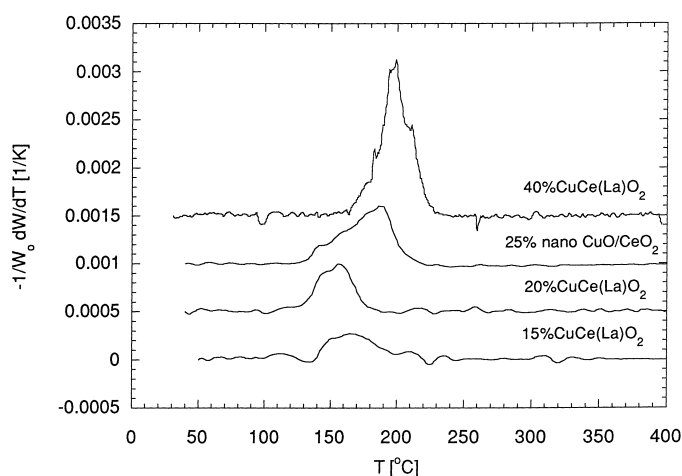


Fig. 7. Comparison of H₂-TPR of coprecipitated CuCe(La)O₂ catalysts with the H₂-TPR of physical mixture of nano-CuO and Ce(La)O₂: TGA, 500 cm³ min⁻¹ (STP), 5% H₂/He, 5°C/min.

for 43.3 at% Cu a low-temperature peak was observed at 150°C and a high-temperature reduction peak was observed at 180°C. The reduction profiles of Cu in Y-doped ZrO₂ repeated here are very similar to those observed by the latter group.

Comparison of the TPR profiles of catalysts as prepared and after treatment in HNO₃ (dissolving CuO, but not CeO₂ or ZrO₂), and calcination of the resulting material at 650°C is shown in Fig. 8. Inspection of the TPR profiles of 40% CuCe(La)O₂ (Fig. 8(a)) and 20% CuCe(La)O₂ (Fig. 8(b)) shows that after the larger CuO particles had been removed by HNO₃, the temperature for maximum reduction rate for both catalysts was 150–160°C. Similar behavior was observed for the 40% CuZr(Y)O₂ as shown in Fig. 8(c). All acid-washed catalysts had TPR profiles similar to low Cu-containing catalysts (Figs. 5 and 6). Liu and Flytzani-Stephanopoulos [22] have found only clusters of copper remaining in the acid-washed materials, which accounts for the present TPR data.

The above discussion focuses on the reducibility of CuO in CeO₂ and ZrO₂. However, it is also interesting to examine the reducibility of the oxide support itself. While a more extensive study of cerium oxide reducibility resulting from interaction with transition metals is presented elsewhere [46], we have a clear indication of ceria reduction by H₂ even at this low temperature (<200°C). In Table 2, the extent of reduction (expressed as wt% change) exceeds that corresponding to the complete reduction of copper oxide to the metal, almost 1.7 times for the 5% CuCe(La)O₂ sample. This excess oxygen reduction was especially pronounced for the low-content copper samples, where the copper clusters are strongly associated with ceria (see also [22]). Similar behavior was observed by Delk and Vavere [30] for copper supported on titania. No such interaction is present in the CuZr(Y)O₂ samples.

3.3.2. CH₄-TPR

Fig. 9 shows the CH₄-TPR profiles of copper-modified catalysts obtained by monitoring the product CO₂ by mass spectrometry. Reaction of methane with these oxidized catalysts gives CO₂ and H₂O as reduction products. Only trace amounts of CO were observed. Fig. 9 shows the CH₄-TPR of Cu-modified catalysts shown as CO₂ evolution vs. temperature. As it can be seen in Fig. 9(a), different Cu species on Zr(Y)O₂

react with methane in a different way. Generally, the same reduction behavior was observed as in the reduction by hydrogen. At low Cu loading (5 at%), only a single reduction peak was observed. These highly dispersed Cu species begin to react with methane at about 350°C, and the peak maximum is observed at ~400°C. On the other hand, at a Cu content >10 at%, reduction starts at 300°C, and a doublet is observed. A doublet is also present in the TPR profile of 40% CuZr(Y)O₂, suggesting that its origin is bulk CuO. The most reducible species appear to be Cu clusters (identified by STEM/EDX in the 15% CuZr(Y)O₂ catalysts, Fig. 2), which are in close contact with the support.

A similar reduction pattern is observed for CuCe(La)O₂ catalysts (Fig. 9(b)). The 5% CuCe(La)O₂ catalyst shows one peak in the CH₄-TPR, with maximum reduction at about 450°C. As the Cu content increases to 15 at%, a doublet appears in the reduction profile and reduction starts at about 300°C. As in H₂-TPR, copper clusters in close contact with CeO₂ support are more easily reduced than highly dispersed copper. The reason for this must be the strong interaction of dispersed copper species with the CeO₂ matrix. Comparison of the TPR profile of 40% CuCe(La)O₂ catalyst as prepared with the TPR of the catalyst treated with HNO₃ (where bulk CuO particles were removed) shows that copper clusters are more reducible than bulk CuO, also in agreement with what was observed in H₂-TPR (Fig. 8(a) and (b)). Reduction of bulk CuO (prepared by carbonate decomposition) is shown for comparison, indicating that the doublet in the reduction profile comes from bulk CuO reduction. Fig. 9(b) shows that the peak maximum shifts to higher temperatures as the copper content increases from 15% to 40%. To check for possible effect of the reduction conditions as the amount of reducible species increases, we performed CH₄-TPR in the TGA setup under significantly different conditions (~40 times less catalyst and ~10 times higher flow rate of the reducing gas). As shown in Fig. 9(c) for the 5%, 15%, and 40% CuCe(La)O₂ materials, reduction starts at about 300°C for high Cu loading (15% and 40% Cu), and at about 350°C for the low Cu loading (5 at%). A rather broad reduction peak (350–500°C) is observed at low Cu loading. The unusual peak shape at high Cu contents comes from the complex desorption (H₂O, CO₂) pattern during the reduction.

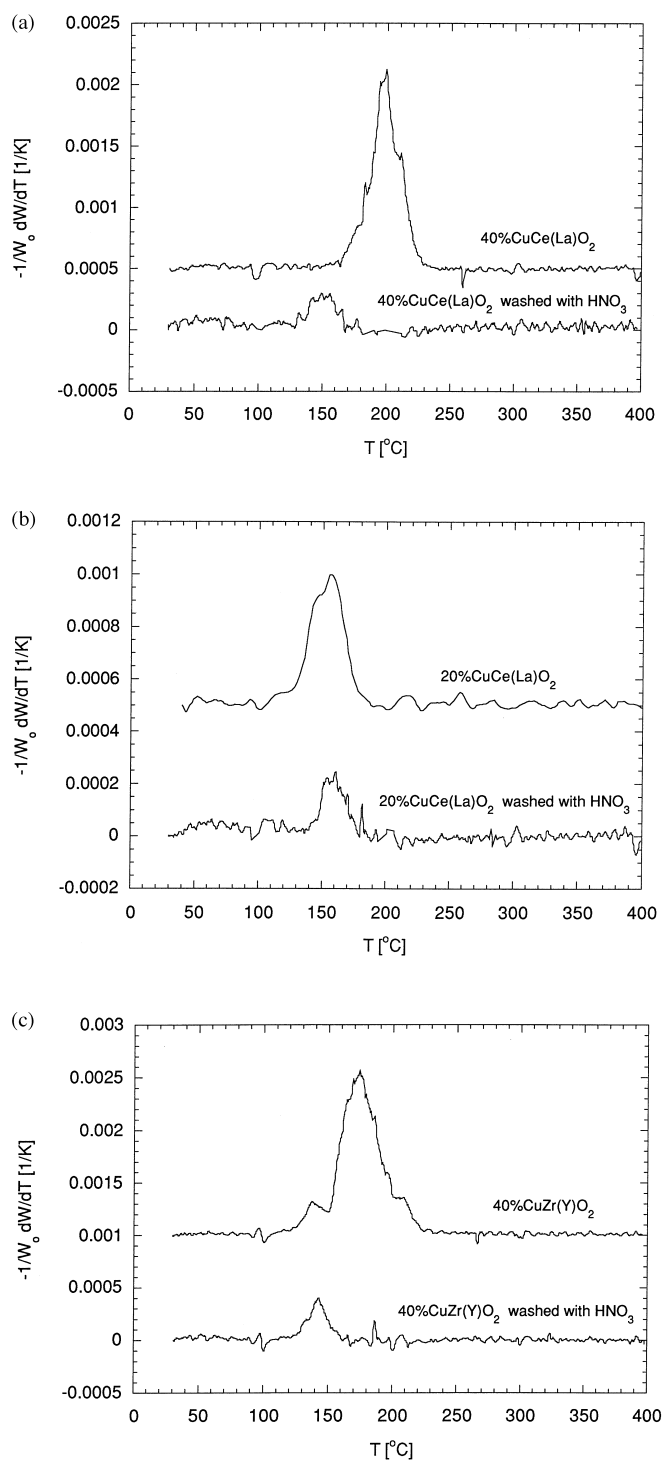


Fig. 8. H_2 -TPR of high CuO loading catalysts before and after nitric acid treatment (TGA, $500\text{ cm}^3\text{ min}^{-1}$ (STP), 5% H_2/He , 5°C/min): (a) 40% $CuCe(La)O_2$, (b) 20% $CuCe(La)O_2$, (c) 40% $CuZr(Y)O_2$.

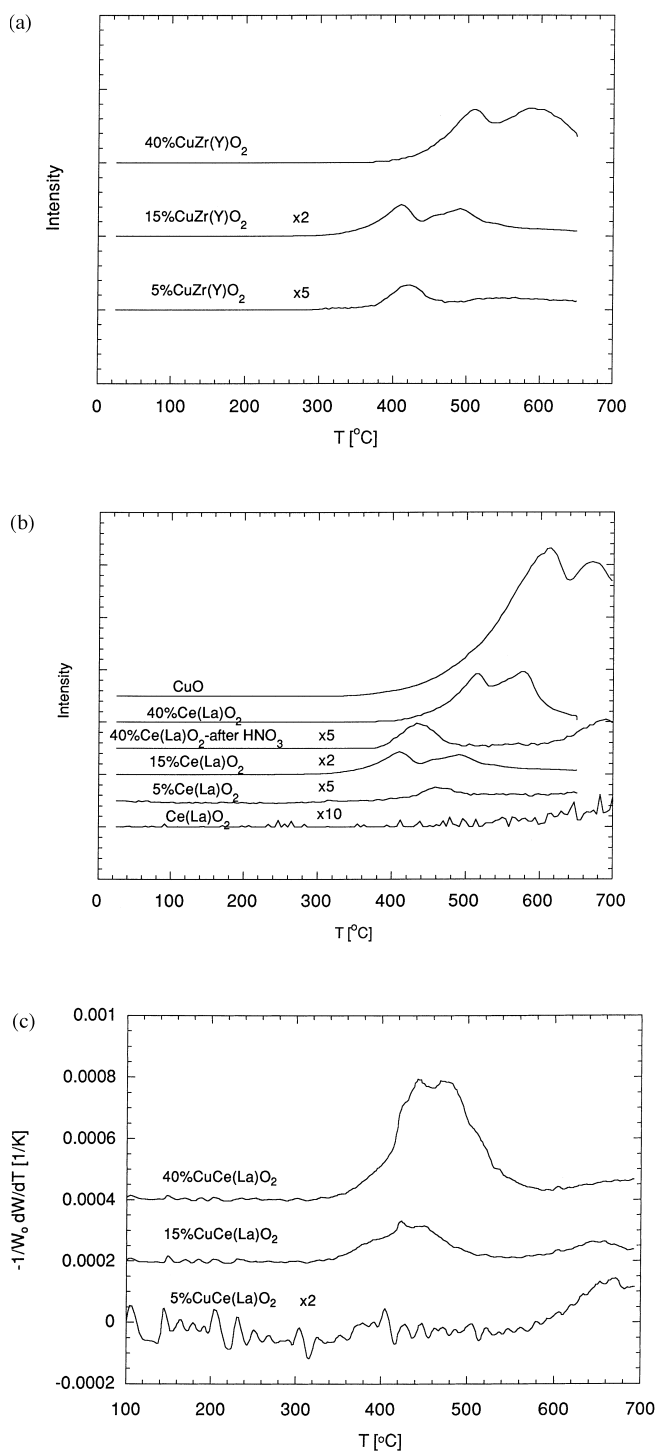


Fig. 9. (a) CH_4 -TPR of $\text{CuZr}(\text{Y})\text{O}_2$ catalysts with different copper loading: Reactor-MS, 200 mg catalyst, $50 \text{ cm}^3 \text{ min}^{-1}$ (STP), 5% CH_4/He , $10^{\circ}\text{C}/\text{min}$. (b) CH_4 -TPR of $\text{CuCe}(\text{La})\text{O}_2$ catalysts with different copper loading: Reactor-MS, 200 mg catalyst, $50 \text{ cm}^3 \text{ min}^{-1}$ (STP), 5% CH_4/He , $10^{\circ}\text{C}/\text{min}$. (c) CH_4 -TPR of $\text{CuCe}(\text{La})\text{O}_2$ catalysts with different copper loading: TGA, 5 mg catalyst, $500 \text{ cm}^3 \text{ min}^{-1}$ (STP), 5% CH_4/He , $10^{\circ}\text{C}/\text{min}$.

Table 3
Reduction extent of different CuCe(La)–O catalysts in CH₄-TPR

Catalyst	Cu (at%)	CuO (wt%)	% Weight change for CuO reduction ^a	CuO peak area (wt%)
5% CuCe(La)	4.94	2.35	0.47	0.86 ^b
15% CuCe(La)	12.87	6.39	1.29	1.36 ^b
40% CuCe(La)	40.00	23.55	4.74	4.77 ^c

^aCalculated for complete reduction of CuO to Cu.

^bDetermined from weight change between 300°C and 520°C.

^cDetermined from weight change between 300°C and 580°C.

The reduction extent in CH₄-TPR of CuCe(La)O₂ catalysts is shown in Table 3. As in the H₂-TPR (Table 2), the observed weight change at high Cu loading is close to the amount of oxygen removed if all CuO is reduced to metallic Cu. Only at low Cu content (5 at%), the amount reduced in both H₂- and CH₄-TPR is much higher than what would account for just the copper (as CuO). The additional oxygen removed is attributed to the reduction of ceria induced by the presence of Cu. As mentioned above, enhancement of ceria reducibility by addition of copper was reported [22] in reduction by H₂. Here we see that CH₄ can also be used to observe this enhancement. In addition, CH₄-TPR is useful as it identifies the temperature range where the mixed oxide system will show activity for the methane oxidation, assuming that the latter operates according to the redox mechanism.

3.4. Kinetic measurements

The activity of the various catalysts for methane oxidation was also compared under kinetic control. Complete kinetic studies were performed over the Ce(La)O₂ [47] and 15% CuCe(La)O₂ catalysts [20]. The reaction order with respect to methane partial pressure was found to be close to 1 on both catalysts, while the reaction order with respect to oxygen partial pressure is close to zero (0.23 for Ce(La)O₂, and 0.18 for the Cu-modified catalyst). Here we are reporting on rate measurements and apparent activation energies with the Ce(La)O₂ and Zr(Y)O₂-based catalysts. Fig. 10(a) and (b) show Arrhenius-type plots for the rate of methane oxidation over various CuCe(La)O₂ and CuZr(Y)O₂ catalysts. For all CeO₂-based catalysts, the rates of methane oxidation are similar at all Cu loading with activation energies ranging from 85.5

to 119 kJ/mol (Fig. 10(a)). Increase in Cu content from 5 to 15 at% slightly increases the activity for methane oxidation. Further addition of copper does not significantly change the activity as is evident from the activity of the 40% CuCe(La)O₂ sample as prepared and after bulk CuO was removed by nitric acid. Fig. 10(a) also shows the Arrhenius-type plot for CH₄ oxidation over the La-doped cerium oxide in the absence of copper. The activation energy is similar while the reaction rate is lower. This indicates that the enhancement of methane oxidation by addition of copper in Ce(La)O₂ is derived from an increase in the surface oxygen species.

The activity of CuZr(Y)O₂ catalysts for methane oxidation is shown in Fig. 10(b). The effect of Cu is more pronounced here than in the CuCe(La)O₂ samples. The methane oxidation rate increases as the copper loading increases from 5% to 15%, especially at low temperatures, indicating that copper clusters are more active for methane oxidation than highly dispersed copper. Further addition of copper (40%) forms bulk CuO particles, which do not contribute further to the catalytic activity.

Differences between the two supports are evident only for low Cu loading (5 at%), where CeO₂-based catalysts show higher activity at low temperatures than the ZrO₂-based materials. This is attributed to the participation of ceria in the reaction. At higher Cu loading, the surface of ceria is progressively covered with more copper so that the ceria does not contribute significantly to the activity. Overall, ceria appears to be a better support for copper as the activity of the 5% CuZr(Y)O₂ catalyst decreased significantly after a high-temperature treatment at 750°C (Fig. 10(b)), while that of the 5% CuCe(La)O₂ catalyst remained unaffected (shown in Fig. 10(a)). Thus, the interaction

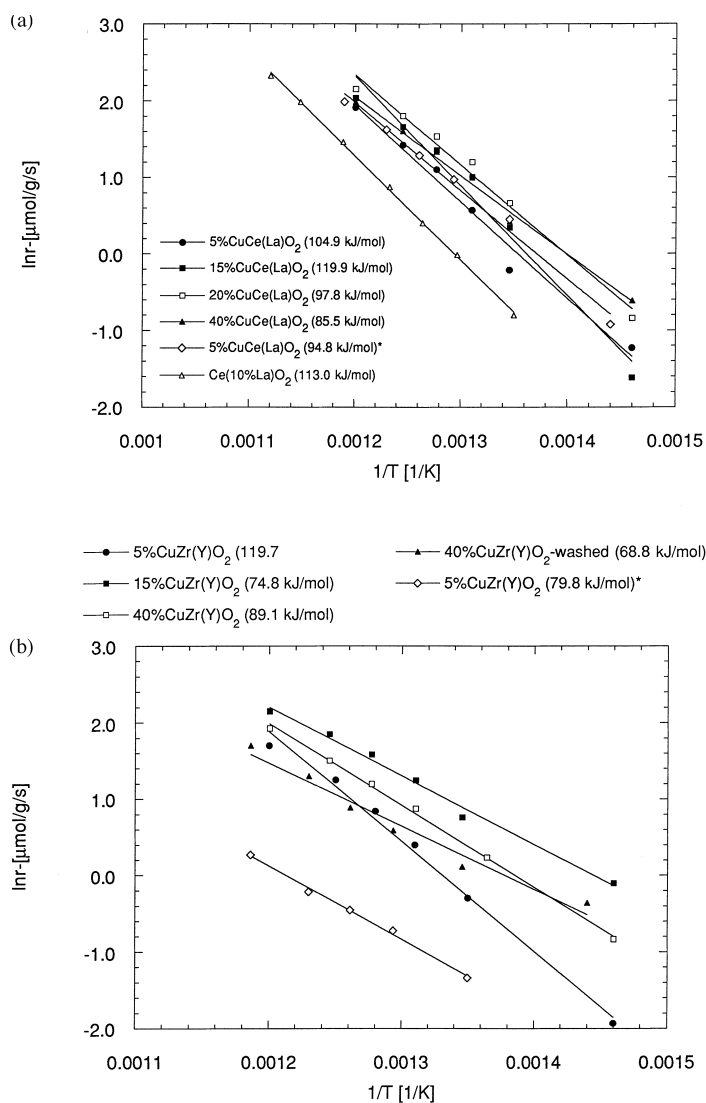


Fig. 10. (a) Arrhenius-type plot of the rate of methane oxidation on Cu-modified CeO_2 based catalysts (650°C -calcined): 0.024 g s/cm^3 , 1% CH_4 , 5% O_2 , balance He* (further heated in air at 750°C for 5 h). (b) Arrhenius-type plot of the rate of methane oxidation on Cu-modified ZrO_2 based catalysts (650°C -calcined): 0.024 g s/cm^3 , 1% CH_4 , 5% O_2 , balance He* (further heated in air at 750°C for 5 h).

of copper species with ceria reported earlier [17] prevents sintering and loss of surface oxygen, thus retaining a high methane oxidation activity.

In general, highly dispersed copper species are less active for methane oxidation than Cu clusters formed on each support at higher loading (5–20 at%). The observed behavior may be attributed to the higher reducibility of these clusters. Bulk CuO particles, which are formed at high Cu loading (40 at%) are

reduced at higher temperature and do not contribute to the overall catalytic activity (Fig. 10).

4. Summary

In this paper, the reducibility of Cu-containing cerium and zirconium oxide systems was studied both by H_2 -TPR and CH_4 -TPR and was correlated with the

various copper species present. Studies were complemented by characterization of the mixed oxides by STEM/EDX, XRD and XPS. Finally, the catalytic activity of these systems for the complete oxidation of methane at low temperatures was studied and correlated to the presence of the reducible oxide species.

Hydrogen reduction of CuO in the Ce(La)O₂ and Zr(Y)O₂ oxide systems was studied here to identify different copper species based on their reduction behavior. At low Cu loading (~5%), on both oxides studied, reduction by H₂ gives a broad peak with a maximum around 175°C. Copper is present as highly dispersed clusters or as isolated Cu ions. These interact strongly with the support, and the reduction requires a temperature of 175°C. At higher Cu content (5–20 at%), copper is mainly at the surface present as small clusters, which are reduced more easily so that the reduction peak is observed at lower temperature (145°C for Zr(Y)O₂-based catalysts and 160°C for Ce(La)O₂-based catalysts). On the other hand, at high Cu loading (~40%), copper is present mainly as larger CuO particles, which do not interact strongly with the support, as indicated by a reduction temperature approaching that for bulk CuO (180°C on Zr(Y)O₂-based catalysts and 200°C for the Ce(La)O₂-based catalysts).

There is a clear influence of the oxide host on the reducibility of copper. In turn, copper increases the reducibility of ceria. It seems that copper is more stabilized when dispersed in Ce(La)O₂ than in the Zr(Y)O₂ matrix, so that the reduction of copper species occurs at lower temperatures for the Zr(Y)O₂-based catalysts.

A similar TPR pattern was observed when methane was used as a reductant. At low copper content (5 at%), reduction starts at about 350°C and a single reduction peak was observed with a maximum at 400°C. As the copper content increases, a doublet appears in the reduction profile. Highly dispersed copper clusters react with methane at lower temperatures (reduction starts at about 300°C) in agreement with what was observed in H₂-TPR. Increase of ceria reducibility by the addition of copper was also observed during CH₄-TPR.

The reaction rates for methane oxidation on both CuCe(La)O₂ and CuZr(Y)O₂ are in the same range due to the similar activity of copper clusters present on

both supports. However, the importance of ceria, which is itself an active catalyst for methane oxidation, is manifested at low Cu loading and low temperatures, where the CeO₂-based material shows better performance than the ZrO₂-based one. CeO₂ also contributes to the higher thermal stability of the 5% Cu-containing catalyst, which retains its catalytic activity after a high-temperature treatment. The same high-temperature treatment (750°C, 5 h in air) significantly decreases the activity of 5% CuZr(Y)O₂. The copper clusters formed on both supports appear to be the most active component of the catalyst. Bulk CuO particles do not contribute to the overall catalytic activity. In general, strongly associated copper (ions) and large copper particles were both found to be less active than copper clusters dispersed on the support.

References

- [1] A. Trovarelli, *Catal. Rev.-Sci. Eng.* 38(4) (1996) 439.
- [2] S. Meriani, *Mater. Sci. Eng.* A109 (1989) 121.
- [3] G. Balducci, P. Fornasiero, R. Di Monte, J. Kaspar, S. Meriani, M. Graziani, *Catal. Lett.* 33 (1995) 193.
- [4] C. De Leitenburg, A. Trovarelli, F. Zamar, S. Maschio, G. Dolcetti, J. Llorca, *J. Chem. Soc., Chem. Commun.* (1995) 2181.
- [5] B. Harrison, A.F. Diwell, C. Hallett, *Plat. Met. Rev.* 32(2) (1988) 73.
- [6] G.S. Zafiris, R.J. Gorte, *J. Catal.* 139 (1993) 561.
- [7] H. Cordatos, R.J. Gorte, *J. Catal.* 159 (1996) 112.
- [8] H. Cordatos, T. Bunluesin, J. Stubenrauch, J.M. Vohs, R.J. Gorte, *J. Phys. Chem.* 100 (1996) 785.
- [9] E.S. Putna, J.M. Vohs, R.J. Gorte, *J. Phys. Chem.* 100 (1996) 17862.
- [10] T. Bunluesin, R.J. Gorte, G.W. Graham, *Appl. Catal. B* 339 (1997) 1.
- [11] A.L. Tarasov, L.K. Przhval'skaya, V.A. Shvets, V.B. Kazanskii, *Kinet. Katal.* 29(5) (1988) 1181.
- [12] C. Li, Y. Chen, W. Li, Q. Xin, in: T. Inui et al. (Eds.), *New Aspects of Spillover in Catalysis*, Elsevier Science, Amsterdam, 1993, p. 217.
- [13] H.C. Yao, Y.F. Yao, *J. Catal.* 86 (1984) 254.
- [14] J.G. Nunan, R.G. Silver, S.A. Bradley, in: R.G. Silver, J.E. Saeys, J.C. Summers (Eds.), *Catalytic Control of Air Pollution*, Chap. 17, ACS Symposium Series 495, American Chemical Society, Washington, DC, 1992.
- [15] A. Aboukais, A. Bennani, C.F. Aissi, M. Guelton, J.C. Vedrine, *Chem. Mater.* 4 (1992) 977.
- [16] J. Soria, J.C. Conesa, A. Martinez-Arias, J.M. Coronado, *Solid State Ionics* 63–65 (1993) 755.
- [17] W. Liu, *Development of Novel Metal Oxide Composite Catalysts for Complete Oxidation Reactions*, Sc.D. Thesis, MIT, 1995.

- [18] W. Liu, M. Flytzani-Stephanopoulos, *J. Catal.* 153 (1995) 304.
- [19] W. Liu, M. Flytzani-Stephanopoulos, *J. Catal.* 153 (1995) 317.
- [20] W. Liu, A.F. Sarofim, M. Flytzani-Stephanopoulos, *Chem. Eng. Sci.* 49(24A) (1994) 4871.
- [21] W. Liu, C. Wadia, M. Flytzani-Stephanopoulos, *Catal. Today* 28 (1996) 391.
- [22] W. Liu, M. Flytzani-Stephanopoulos, *Chem. Eng. J.* 64 (1996) 283.
- [23] V.R. Choudhary, B.S. Uphade, S.G. Pataskar, A. Keshavaraja, *Angew. Chem. Int. Ed. Engl.* 35(20) (1996) 2393.
- [24] V. Perrichon, A. Laachir, G. Bergeret, R. Frety, L. Tournayan, O. Touret, *J. Chem. Soc., Faraday Trans.* 90 (1994) 773.
- [25] P. Fornasiero, R. Di Monte, G. Ranga Rao, L. Kaspar, Meriani, A. Trovarelli, M. Graziani, *J. Catal.* 151 (1995) 168.
- [26] J.Y. Yan, G.-D. Lei, W.M.H. Sachtler, H.H. Kung, *J. Catal.* 160 (1996).
- [27] G. Fierro, M. Lo Jacono, M. Inversi, P. Porta, R. Lavecchia, F. Cioci, *J. Catal.* 148 (1994) 709.
- [28] W.-P. Dow, T.-J. Huang, *J. Catal.* 147 (1994) 322.
- [29] W.-P. Dow, Y.-P. Wang, T.-J. Huang, *J. Catal.* 160 (1996) 155.
- [30] F.S. Delk, A. Vavere, *J. Catal.* 85 (1984) 380.
- [31] J. Sárkány, J.L. d'Itri, W.M.H. Sachtler, *Catal. Lett.* 16 (1992) 241.
- [32] T. Beutel, J. Sárkány, G.-D. Lei, J.Y. Yan, M.H. Sachtler, *J. Phys. Chem.* 100 (1996) 845.
- [33] Y. Amenomiya, I. Ali Emesh, K. Oliver, G. Pleizier, in: M. Phillips, M. Ternan (Eds.), *Proceedings of the Ninth International Congress on Catalysis*, Chemical Institute of Canada, Ottawa, Canada, 1988, p. 634.
- [34] M. Kung, K. Bethke, D. Alt, B. Yang, H. Kung, in: U. Ozkan, S. Agrawal, G. Marcelin (Eds.), *ACS Symposium Series*, vol. 587, American Chemical Society, Washington, DC, 1995, p. 96.
- [35] G. Wrobel, C. Lamonier, A. Bennani, A. D'Huysser, A. Aboukais, *J. Chem. Soc., Faraday Trans.* 92(11) (1996) 2001.
- [36] R.J. Farrauto, J.K. Lampert, M.C. Hobson, M. Waterman, *Appl. Catal. B* 6 (1995) 263.
- [37] K. Otto, *Langmuir* 5 (1989) 1364.
- [38] K. Fujimoto, F.H. Ribiero, E. Iglesia, M. Avalos-Borja, *Symposium on Catalytic Combustion, Division on Petroleum Chemistry*, 213 National Meeting, American Chemical Society, San Francisco, CA, 1997.
- [39] F. Zamar, A. Trovarelli, C. De Leitenburg, G. Dolcetti, *J. Chem. Soc., Chem. Commun.* 9 (1995) 965.
- [40] J.J.F. Scholten, A.P. Pijpers, M.L. Hustings, *Catal. Rev. Sci. Eng.* 27(1) (1985) 151.
- [41] D. Brigs, M.P. Seah (Eds.), *Practical Surface Analysis by Auger and X-ray Photoelectron Spectroscopy*, Wiley, New York, 1983.
- [42] J.L. Falconer, J.A. Schwarz, *Catal. Rev. Sci. Eng.* 25(2) (1983) 141.
- [43] F.M.Z. Zotin, L. Tournayan, J. Varloud, V. Perrichon, R. Frety, *Appl. Catal. A* 98 (1993) 99.
- [44] P. Malet, A. Caballero, *J. Chem. Soc. Faraday Trans. 1* 84(7) (1988) 2369.
- [45] D.A. Monti, A. Baiker, *J. Catal.* 83 (1983) 323.
- [46] K.A. Bethke, M.C. Kung, B. Yang, M. Shah, D. Alt, C. Li, H.H. Kung, *Catal. Today* 26 (1995) 169.
- [47] Lj. Kundakovic, M. Flytzani-Stephanopoulos, *J. Catal.* (1998), submitted.