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Results are presented for a set of experiments de	signed to determine the
attenuation of shock waves passing through perfor	ated plates as a function of
The venting hole size was warded for a given perce	ntage of plate area vented.
(7.14  cm) as the vented area was varied from $1/8$ inch $(0)$	.32 cm) to 2-13/16 inches
plates were exposed to shock waves in a 4-inch (10	percent open. Ine perforated
of peak shock overpressures from 200 psi (1379 kP	a) down to 48 psi (331 kPa).
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#### AUTHORS' COMMENTS

Both the English system of units and SI units have been used in this report with the exception of the data tables where the gage calibrations and computer output for overpressure are in pounds per square inch. Dual scales were not used because the primary objective of the tables is to determine ratios and percentages of input pressure and transmitted pressure which would be the same in either system of units.

There is also a need to keep continuity of the present results with previously published results (Reference 1) conceived with the same subject matter. All equations developed in this report satisfy both systems of units.

#### I. INTRODUCTION

This is the second\* in a series of reports which define the parameters affecting the attenuation of shock waves passing through vented wall plates. Results are reported here for the attenuation of shock waves through single perforated plates as a function of the number and size of vent holes in a plate.

### A. Background

Under the US Army's Production Base Modernization (PBM) program for munition processing facilities, a two-phase program has been initiated to develop suppressive shields. One phase, the Category Shield program, will produce a series of shields for specific munition applications.

For the second phase, the Applied Technology Development Phase, a major responsibility has been given to the Ballistic Research Laboratory (BRL). The basic requirement of this phase is to develop a general technology base for suppressive shields. The basic design criteria require containment of fragments and attenuation of the blast wave from accidental explosions in munition processing plants. This report is concerned with the blast attenuation part of the requirement.

B. Objectives

1. Define and determine the suppressive structure parameters which affect the attenuation of the blast wave.

2. Develop an understanding of blast wave suppression so as to design an efficient blast suppressor.

The objective of this report is to present results obtained from a study of pressure attenuation of shock waves passing through perforated plates. The variables were hole size, number of holes, and incident peak overpressure.

#### **II.** EXPERIMENT

This section describes the experimental equipment and design of the perforated plates.

#### A. Instrumentation

The shock waves were generated inside a 4-inch (10.2 cm) inside diameter shock tube. The driver section used was 12 inches (30.48 cm)

<sup>\*</sup>The first report is entitled, "Shock Wave Attenuation by Single Perforated Plates," Charles Kingery and George Coulter, BRL Memorandum Report 2664, August 1976.

long; driver gas was helium. The test station was located 100 inches (254 cm) from the diaphragm at the driver section. Another 200 inches (508 cm) of tube was added downstream of the test station to delay the return of reflections from the closed end.

The short driver section was chosen so as to form a peaked decaying shock wave similar to that produced by a high explosive detonation. Calibrated aluminum and copper diaphragm materials were used to contain the driver gas in the compression chamber until the desired pressure was obtained. Figure 1 shows a sketch of the shock tube.

Pressure-time profiles of the shock waves were recorded at the locations shown in the sketch. The transducers were tourmaline crystal type, Model ST-4, manufactured by Susquehanna Instruments Company. They were threaded into the shock tube wall as nearly flush as possible. Charge amplifiers, Kistler Model 506; and oscilloscopes, Tektronix Model 502-A; completed the recording instrumentation.

### B. Plate Design

The perforated plates were designed to investigate the effect of number of holes and hole size on shock wave attenuation for different incident peak overpressures\*. Several vent areas,  $A_v$ , in the range from

5-50 percent were chosen for testing. The number and diameter of the holes were varied for each of the several percentages of area vented.

Single steel plates, 0.25 inch (0.64 cm) thick, were bolted between the flanges of the shock tube at the point shown in Figure 1. The number, diameter, and size of the holes in the various plates are listed in Table I. Sketches of the plates are shown in Figure 2.

#### III. RESULTS

The test results are presented in three sections covering the shock tube calibration, the transmitted pressure, and the pressure transmission ratio.

#### A. Shock Tube Calibration

The shock tube was calibrated by measuring the attenuation of the shock waves with distance along the shock tube when no plates were installed; i.e., when  $A_v = 100$  percent open.

This was done by measuring a series of shock over-pressure levels between gage Station 3 and Station 6. The earlier work, as noted in

<sup>\*</sup>All pressures discussed in this report are overpressures, not absolute values.





						A <sub>v</sub>
Plate No.	No. of Holes	Hole Di	ameter	Hole	Area	Area Vented Percent
		inches	(cm)	inches <sup>2</sup>	(cm <sup>2</sup> )	
1	3	0.50	( 1.27)	0.196	( 1.267)	4.69
2	52	0.125	( 0.32)	0.012	( 0.080)	5.1
3	5	0,50	( 1.27)	0.196	( 1,267)	7.81
4	6	0.50	( 1.27)	0.196	( 1.267)	9.37
5	105	0.125	( 0.32)	0.012	( 0.080)	10.2
6	16	0.50	( 1.27)	0.196	( 1.267)	25.0
7	256	0.125	( 0.32)	0.012	( 0.080)	25.0
8	68	0.25	( 0.64)	0.049	( 0.322)	26.6
9	307	0.125	( 0.32)	0.012	( 0.080)	30.0
10	392	0.125	( 0.32)	0.012	( 0.080)	38.2
11	105	0.25	( 0.64)	0.049	( 0.322)	41.0
12	1	2.81	(7.14)	6.202	(40.04)	49.4
13	32	0.50	( 1.27)	0.196	( 1.267)	50.0
_	1	4.0	(10.2)	12.566	(81.073)	100.

	Table	Ι.	Test	Plates
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 $A_{V} = \frac{\text{Hole Area x Number of Holes}}{\text{Cross-Section Area of Shock Tube}} \times 100$ 







Figure 2. (Cont'd) Arrangement of Holes in the Test Plates



PLATE II - 41 % OPEN 105 HOLES, 1/4" DIA.

PLATE 12-49.4% OPEN I HOLE, 2-13/16" DIA.

Figure 2. (Cont'd) Arrangement of Holes in the Test Plates



PLATE 13 - 50 % OPEN 32 HOLES, 1/2" DIA.

Figure 2. (Cont'd) Arrangement of Holes in the Test Plates

Reference 1, determined a calibration curve for the shock tube over a range of overpressure from 45 psi (310 kPa) to 218 psi (1503 kPa). This curve with data points is presented in Figure 3. The straight line fit is represented by Equation 1,

$$P_{\rm T} \ 100 = 0.7855 \ P_{\rm T} \tag{1}$$

when  $P_T$  100 is the transmitted pressure for  $A_v$  = 100 percent and  $P_I$  is the input pressure.

The peak overpressure measured at Station 6 when a perforated plate is in the shock tube will be compared to the value calculated from Equation 1 for the input pressure of a given shot.

Figures 4 through 6 show typical record traces within the calibrated range of the shock tube. The upper traces are the input condition at Station 3 and the lower traces are attenuated pressures recorded at Station 6 for the unobstructed shock tube.

#### B. Transmitted Pressure

Section A described the pressure transmitted down the unobstructed shock tube. This section will deal with the pressure transmitted down the shock tube when plates with various vented areas are inserted in the tube. Presented in Figure 7 is a typical set of traces from the shock tube when obstructed by a perforated plate. Other representative pressure-time traces are grouped in the Appendix.

Tables II through XIV list the attenuation results of the shock waveplate interactions. Columns 2 and 3 of the tables list the input pressure ( $P_I$ ) at Station 3 and the attenuated, transmitted pressure ( $P_T$ ) at Station 6, respectively. Column 5 lists the transmitted pressure for the unobstructed no-plate case ( $A_v = 100$ %) as calculated from Equation 1 above.

Figure 8 shows how the transmitted pressure  $(P_T)$  varies with input pressure  $(P_I)$  for various percentages of vented plate area. The family of curves (the solid lines) for the control plates with half-inch holes may be represented by the equation:

$$P_{T} = C P_{I}$$
(2)

<sup>&</sup>lt;sup>1</sup>Charles Kingery and George Coulter, "Shock Wave Attenuation by Single Perforated Plates," BRL Memorandum Report 2664, August 1976. (AD #B013764L)



PRESSURE (PT) PSI **DJTIMSNAAT** 

Input Pressure  $\mathbb{P}_{I}$  versus Transmitted Pressure  $\mathbb{P}_{T}$  for  $\mathbb{A}_{v}$  of 100 Percent Figure 3.

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SHOT 8 CH6 SUPPRESSIVE STRUCTURES



## (B) TRANSMITTED PRESSURE

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## (B) TRANSMITTED PRESSURE







# (B) TRANSMITTED PRESSURE







SHOT 13 CH6 SUPPRESSIVE STRUCTURES



# PLATE 6 - TRANSNITTED PRESSURE





Figure 8. Transmitted Pressure versus Input Pressure for Different Percentages of Area Vented

where C is a function of the plate area vented. Values of C were calculated from a simple ratio of the data  $P_T$  for x percent opening (Column 3) divided by  $P_I$  (Column 2). The C values are listed in Column 4 of Tables II through XIV.

It can be seen from the average values of C listed in Tables II through XIV that there is no significant effect of the hole size or number of holes in a plate with the exception of Plate 2 and Plate 5 both with 1/8-inch diameter holes consisting of 52 and 105 in number.

### C. Pressure Transmission Ratio

The last two columns of Tables II through XIV contain quantities that are helpful in defining the effectiveness of a perforated plate attenuator. The first quantity is defined as the transmission ratio ( $P_{\rm TR}$ ). It is defined as

$$P_{TR} = \frac{P_{T} \text{ with vented plate}}{P_{T} 100 \text{ without a plate}}, \qquad (3)$$

where  $P_{T}$  is the transmitted pressure in each case.

A second quantity, the percentage of attenuation may be more helpful in some cases. It is equal simply to  $(1 - P_{TR}) \times 100$ . The average values listed of these quantities in Tables II through XIV are summarized in Table XV.

An equation of the form

$$P_{TR} = B A_{V}^{N}$$
(4)

was used to fit the data for the transmission ratio  $(P_{TR})$  as a function of area vented  $(A_V)$ . B and N have the values of 0.1094 and 0.5135, respectively, for plates with half-inch holes for area vented below 50 percent.

The data from the new plates listed in Table XV show little scatter from the values established from plates with the one-half inch diameter holes.

For a given A  $_{\rm V}$  and P  $_{\rm I}$  the value of P  $_{\rm T}$  can be determined by calculating P  $_{\rm TR}$  from Equation 4 and P  $_{\rm T}$  100 from Equation 1 and substituting in to Equation 3 to obtain

$$P_{\rm T} = (0.7855 P_{\rm I}) P_{\rm TR}$$
(5)

It also follows that by dividing both sides of Equation 5 by  $P_{I}$ , one obtains from Equation 2,

$$C = 0.7855 P_{TR}$$
, and (6)

if C is determined from Tables II through XIV then

$$P_{\rm TR} = C/0.7855.$$
 (7)

A direct comparison of the experimental values of the Pressure Transmission Ratio  $(P_{TR})$  and the percent of pressure attenuation listed in Tables II through XIV has been made with values calculated using Equation 4. These comparisons are made in Table XV.

The values of pressure transmission ratio and pressure attenuation percent from Table XV have been plotted in Figures 9 and 10, respectively. The solid line represents the calculated values from Equation 4 which was established from the experimental values obtained from the plates with half-inch (1.27 cm) holes. The symbols indicate how well the data compare when obtained from plates with different hole sizes. The data from a A

of 5.1 and 10.2 percent differ most from the trend established from previous tests. It should be noted in Table XV that when plates with a similar  $\rm A_v$  are tested the values of attenuation percent are also similar.

#### IV. CONCLUSIONS

Based upon the experimental results obtained, a perforated plate did not change appreciably its ability to attenuate shock waves when the hole size was changed. It was only at the small values of  $A_v$  with 1/8 hole size that a deviation from the established trend was noted.

There was no trend established for pressure transmission ratio or attenuation percent as a function of input pressure  $(P_I)$  for a given  $A_V$ . The expression

$$P_T = C P_I$$

appears to be valid for range of pressures and vent areas tested.

Table II. Pressure Attenuation Plate 1, 3, 1/2-Inch Holes - 4.69 Percent Open

Attenuation Percent	76.8	74.2	78.5	75.4	78.2	74.6	75.8	77.1	76.3
Ratio (P <sub>TR</sub> ) P <sub>T</sub> 4.69/P <sub>T</sub> 100	0.232	0.258	0.215	0.246	0.218	0.254	0.242	0.229	0.237
Transmitted Pressure $(P_T)$ $A_V = 100$ %	154.5	150.6	94.8	96.8	99.6	38.6	38.5	40.1	
Ratio (C) P <sub>T</sub> 4.69/P <sub>I</sub>	0.182	0.203	0.169	0.193	0.171	0.199	0.189	0.180	0.185
Transmitted Pressure $(P_T)$ $A_v = 4.69$ % Psi	35.8	38.9	20.4	23.8	21.7	9.8	9.3	9.2	trage
Input Pressure (P <sub>I</sub> ) psi	197.0	192.0	120.9	123.3	127.0	49.3	49.1	51.2	Ave
Shot Number	18	19	20	21	22	23	24	25	

NOTE: Psi x 6.894757 = kPa.

Table III. Pressure Attenuation, Plate 2, 52, 1/8-Inch Holes - 5.1 Percent Open

Attenuation Percent	79.7	78.6	77.5	83.2	82.0	80.3	80.7	81.4	80.4
Ratio (P <sub>TR</sub> ) P <sub>T</sub> 5.1/P <sub>T</sub> 100	0.203	0.214	0.225	0.168	0.180	0.197	0.193	0.186	0.196
Transmitted Pressure $(P_T)$ $A_V = 100\%$	152,1	156.4	99.1	99.1	100.8	36.5	37.4	36.5	
Ratio C P <sub>T</sub> 5.1/P <sub>I</sub>	0.160	0.168	0.177	0.132	0.141	0.155	0.151	0.146	0,154
Transmitted Pressure $(P_T)$ $A_V = 5.1\%$ psi	30.9	33.5	22.3	16.6	18.1	7.2	7.2	6.8	srage
Input Pressure (P <sub>I</sub> ) psi	193.6	199.1	126.1	126.1	128.3	46.5	47.6	46.5	Ave
Shot Number	77	78	79	80	81	82	83	84	

Attenuation Percent	69.2	65.4	68.0	70.7	68.3
Ratio (P <sub>TR</sub> ) P <sub>T</sub> 7.81/P <sub>T</sub> 100	0.308	0.345	0.319	0.293	0.317
Transmitted Pressure $(P_T)$ $A_V = 100$ %	155.0	154.1	53.2	55.0	
Ratio C P <sub>T</sub> 7.8/P <sub>I</sub>	0.242	0.271	0.250	0.229	0.248
Transmitted Pressure $(P_T)$ $A_V = 7.81\%$ Psi	47.8	53.3	17.0	16.1	erage
Input Pressure $(P_{I})$ psi	197.6	196.4	67.9	70.2	Ave
Shot Number	296	297	282	283	

Table IV. Pressure Attenuation, Plate 3, 5, 1/2-Inch Holes - 7.81 Percent Open

Table V. Pressure Attenuation, Plate 4, 6, 1/2-Inch Holes - 9.37 Percent Open

Attenuation Percent	60.5	62.4	64.0	68.1	67.2	68.1	65.9	64.8	62.8	64.9
Ratio (P <sub>TR</sub> ) P <sub>T</sub> 9.37 P <sub>T</sub> 100	0.394	0.376	0.360	0.318	0.328	0.319	0.341	0.352	0.372	0.351
Transmitted Pressure $(P_T)$ $A_V = 100\%$	164.8	152.8	149.9	94.9	94.9	97.9	39.6	38.6	38.2	
Ratio C P <sub>T</sub> 9.3/P <sub>I</sub>	0.309	0.295	0.283	0.250	0.257	0.251	0.267	0.276	0.291	0.276
Transmitted Pressure $(P_T)$ $A_r = 9.37\%$ psi	65.0	57.5	54.0	30.2	31.1	31.2	13.5	13.6	14.2	Average
Input Pressure (P <sub>I</sub> ) psi	210.0	194.8	191.0	121.0	120.9	124.5	50.5	49.3	48.8	1
Shot Number	14	30	31	15	28	29	16	26	27	

Table VI. Pressure Attenuation, Plate 5, 105, 1/8-Inch Holes - 10.2 Percent Open

Attenuation Percent 69.5 67.5 60.9 63.9 68.89 64.0 66.8 P<sub>T</sub> 10.2/P<sub>T</sub> 100 Ratio (P<sub>TR</sub>) 0.312 0.360 0.305 0.325 0.332 0.331 0.361 Pressure (P<sub>T</sub>) Transmitted  $A_{\rm V} = 100\%$ 101.6 170.3 145.4 101.2 96.5 37.1 Ratio (C) P<sub>T</sub> 10.2/P<sub>T</sub> 0.245 0.240 0.283 0.255 0.260 0.284 0.261 Pressure (P<sub>T</sub>) Transmitted  $A_{\rm V} = 10.2\%$ 30.9 33.0 31.9 psi 53.2 52.4 13.4 Average Pressure Input 216.8 128.9 122.8 129.4 47.2  $(P_{I})$ 185.1 psi Number Shot 75 76 72 73 74 71

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Table VII. Pressure Attenuation, Plate 6, 16, 1/2-Inch Holes - 25 Percent Open

Attenuation Percent	38.5	38.2	37.8	43.3	42.3	40.6	44.1	41.0	43.8	41.1
Ratio (P <sub>TR</sub> ) P <sub>T</sub> 25/P <sub>T</sub> 100	0.615	0.617	0.622	0.567	0.576	0.594	0.559	0.590	0.562	0.589
Transmitted Pressure $(P_T)$ $A_v = 100\%$	160.9	153.0	149.9	94.9	97.1	93.1	40.1	38.3	38.6	
Ratio (C) P <sub>T</sub> 25/P <sub>I</sub>	0.483	0.486	0.488	0.445	0.452	0.466	0.438	0.454	0.440	0.461
Pressure $(P_T)$ $A_v = 25%$ psi	0.66	94.5	93.3	53.8	56.0	55.3	22.4	22.6	21.7	lerage
Input Pressure $(P_I)$ psi	205.0	195.0	191.0	121.0	123.8	118.6	51.2	49.8	49.3	A
Shot Number	11	32	33	12	34	35	13	36	37	

Shot Number	Input Pressure (P <sub>I</sub> ) psi	Pressure (P <sub>T</sub> ) A <sub>v</sub> = 25% psi	Ratio (C) P <sub>T</sub> 25/P <sub>I</sub>	Transmitted Pressure $(P_T)$ $A_V = 100\%$	Ratio (P <sub>TR</sub> ) P <sub>T</sub> 25/P <sub>T</sub> 100	Attenuation Percent
158	187.7	88.9	0.474	147.4	0.603	39.7
162	194.5	91.1	0.468	152.8	0.596	40.4
160	132.7	65.5	0.494	104.2	0.628	37.2
161	128.2	64.4	0.502	100.7	0.640	36.0
163	48.3	20.0	0.414	37.9	0.527	47.3
164	48.3	20.0	0.414	37.0	0.527	47.3
		Average	0.459		0.587	41.3

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Table VIII. Pressure Attenuation, Plate 7, 256, 1/8-Inch Holes - 25 Percent Open

Table IX. Pressure Attenuation, Plate 8, 68, 1/4-Inch Holes - 26.6 Percent Open

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tio (P <sub>TR</sub> ) Attenuation 26.6/P <sub>T</sub> 100 Percent	0.583 41.7	0.597 40.2	0.607 39.3	0.572 42.8	0.549 45.0	0.561 43.9	0.578 42.1	0.610 38.9	0.582 41.8
Transmitted Pressure $(P_T)$ Ra $A_V = 100\%$ $P_T$	153.3	155.1	91.1	93.0	93.0	37.1	37.9	38.3	
Ratio (C) P <sub>T</sub> 26.6/P <sub>I</sub>	0.458	0.469	0.476	0.449	0.432	0.441	0.454	0.479	0.457
Transmitted Pressure $(P_T)$ $A_V = 26.6\%$ Psi	89.4	92.7	55.3	53.2	51.1	20.8	21.9	23.4	werage
Input Pressure (P <sub>I</sub> ) psi	195.2	197.5	116.2	118.4	118.4	47.2	48.2	48.8	Ą
Shot Number	61	62	63	64	65	66	67	68	

Table X. Pressure Attenuation, Plate 9, 308, 1/8-Inch Holes - 30 Percent Open

Attenuation 00 Percent	31.8	30.7	33.8	33.0	33.8	41.5	42.9	43.6	36.4
Ratio (P <sub>TR</sub> P <sub>T</sub> 30/P <sub>T</sub> 1	0.682	0.693	0.662	0.670	0.662	0.585	0.571	0.564	0.636
Transmitted Pressure $(P_T)$ $A_V = 100$ %	148.3	147.4	102.8	106.0	102.4	38.6	40.5	40.0	
Ratio (C) P <sub>T</sub> 30/P <sub>I</sub>	0.535	0.544	0.520	0.527	0.520	0.459	0.449	0.443	0.500
Pressure (P <sub>T</sub> ) A <sub>v</sub> = 30% Psi	101.1	102.2	68.1	71.1	67.8	22.6	23.1	22.6	Average
Input Pressure $(P_{I})$ psi	188.8	187.7	130.9	135.0	130.4	49.2	51.2	51.0	
Shot Number	156	157	153	154	155	150	151	152	

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Table XI. Pressure Attenuation, Plate 10 392, 1/8-Inch Holes - 38.2 Percent Open

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Attenuation Percent	31.3	30.8	23.2	27.6	28.3	28.8	28.3
Ratio (P <sub>TR</sub> ) P <sub>T</sub> 38.2/P <sub>T</sub> 100	0.687	0.693	0.767	0.723	0.717	0.712	0.716
Transmitted Pressure $(P_T)$ $A_V = 100$ %	161.8	157.2	104.2	106.0	40.3	39.7	
Ratio (C) P <sub>T</sub> 38.2/P <sub>I</sub>	0.539	0.544	0.603	0.568	0.563	0.559	0.563
Pressure (P <sub>T</sub> ) A <sub>v</sub> = 38.2% Psi	111.1	108.9	80.0	76.7	28.9	28.3	Average
Input Pressure (P <sub>I</sub> ) psi	206.0	200.2	132.7	135.0	51.3	50.6	
Shot Number	165	166	167	168	169	170	

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Table XII. Pressure Attenuation, Plate 11, 105, 1/4-Inch Holes - 41.0 Percent Open

ot ber	Input Pressure (P <sub>I</sub> ) psi	Pressure $(P_T)$ A <sub>v</sub> = 41% psi	Ratio (C) P <sub>T</sub> 41/P <sub>I</sub>	Transmitted Pressure $(P_T)$ $A_V = 100\%$	Ratio (P <sub>TR</sub> ) P <sub>T</sub> 41/P <sub>T</sub> 100	Attenuation Percent
	201.5	110.6	0.549	158.3	0.699	30.1
	193.0	105.5	0.547	151.6	0.696	30.4
	197.4	110.6	0.560	155.1	0.713	28.7
	120.6	67.0	0.556	94.7	0.707	29.3
	118.4	66.0	0.557	93.0	0.710	29.0
	122.8	64.9	0.529	96.5	0.673	32.7
	49.3	28.7	0.582	38.7	0.741	25.9
	48.8	28.2	0.578	38.3	0.736	26.4
	47.7	28.7	0.602	37.5	0.766	23.4
		Average	0.562		0.716	28.4

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Table XIII. Pressure Attenuation, Plate 12, 1, 2-13/16-Inch Hole - 49.4 Percent Open

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Attenuat Percen	21.6	20.1	19.7	22.0	22.8	20.5	19.1	18.4	20.0	20.5
Ratio (P <sub>TR</sub> ) P <sub>T</sub> 49.4/P <sub>T</sub> 100	0.784	0.799	0.803	0.780	0.772	0.795	0.809	0.816	0.800	0.795
Transmitted Pressure $(P_T)$ $A_V = 100$ %	148.1	153.5	151.9	91.0	92.0	91.9	36.8	37.9	37.9	
Ratio (C) P <sub>T</sub> 49.4/P <sub>I</sub>	0.616	0.627	0.631	0.613	0.606	0.625	0.635	0.641	0.629	0.625
Pressure (P <sub>T</sub> ) A <sub>v</sub> = 49.4% psi	116.1	122.6	122.0	71.0	71.0	73.1	29.8	30.9	30.3	Average
Input Pressure (P <sub>I</sub> ) psi	188.6	195.4	193.4	115.9	117.1	117.0	46.9	48.2	48.2	
Shot Number	43	44	45	46	47	48	49	50	51	

Table XIV. Pressure Attenuation, Plate 13, 32, 1/2-Inch Holes - 50 Percent Open

Attenuation Percent	26.6	19.1	24.3	21.8	13.1	16.9	22.2	20.4	20.4	20.5
Ratio (P <sub>TR</sub> ) P <sub>T</sub> 50/P <sub>T</sub> 100	0.734	0.809	0.757	0.782	0.869	0.831	0.778	0.796	0.796	0.795
Transmitted Pressure $(P_T)$ $A_V = 100$ %	155.3	156.9	153.4	94.9	89.1	91.8	38.6	39.2	31.2	
Ratio (C) P <sub>T</sub> 50/P <sub>I</sub>	0.575	0.635	0.594	0.613	0.681	0.652	0.610	0.624	0.624	0.623
Pressure (P <sub>T</sub> ) A <sub>v</sub> = 50% Psi	114.0	127.0	116.1	74.2	77.4	76.3	30.0	31.2	31.2	werage
Input Pressure (P <sub>I</sub> ) psi	198.0	200.0	195.5	121.0	113.6	117.0	49.2	50.0	50.0	A
Shot Number	4	Ŋ	42	9	40	41	7	38	39	

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Vented
Area
versus
Attenuation
Pressure
.VX
Table

 $\mathbf{P}_{\mathrm{TR}}$ 

A

	Plate	Number	Area	Transmi	ssion	Attenus	ation
	Number	of Holes	Vented	Rat	io	Perce	ent
			Percent	Experimental	Calculated	Experimental	Calculated
	1	3*	4.69	0.237	0.242	73.6	75.8
	2	52***	5.10	0.196	0.253	80.4	74.7
	3	പ സ	7.81	0.317	0.314	68.3	68.6
	4	<b>6</b> *	9.37	0.351	0.345	64.9	65.5
	Ŋ	105***	10.2	0.332	0.360	66.8	64.0
	9	16*	25.0	0.589	0.571	41.1	42.9
	7	256***	25.0	0.587	0.571	41.3	42.9
	ø	68**	26.6	0.582	0.590	41.8	41.0
	6	308***	30.0	0.636	0.627	36.4	37.3
	10	392***	38.2	0.716	0.710	28.3	29.0
	11	105**	41.0	0.716	0.737	28.4	26.3
	12	1	49.4	0.795	0.810	20.5	19.0
	13	32*	50.0	0.795	0.815	20.5	18.5
*Hole	Diameter	0.50 in. (1	.27 cm).				
**Hole	Diameter	0.25 in. (0	.64 cm).				
***Hole	Diameter	0.125 in. (	(0.32 cm).				

Pressure Transmission Ratio ( $P_{TR}$ ) = 0.1094  $A_v^{0.5135}$ Pressure Attenuation Percent = (1 -  $P_{TR}$ ) x 100

 $A_{\rm V} < 55$ 



Figure 9. Pressure Transmission Ratio as a Function of Percent of Area Vented



Figure 10. Percent Pressure Attenuation as a Function of Percent of Area Vented

### APPENDIX

#### PRESSURE-TIME DATA

This Appendix shows a selection of records which represent the pressure as a function of time at Station 3 (CH3) and Station 6 (CH6). Station 3 was located 0.75 tube diameter upstream from the target plate. Station 6 was located 7 tube diameters downstream of the target plate - a distance sufficient to allow the transmitted shock wave  $(P_T)$  to reform

after passing the perforated plate.

Table A-I presents data for the target plates. Plate number, shot number, area vented, and hole diameter describe the target plates.

The pressure-time records are listed according to percent of area open. The upper trace (CH3) is the input record  $(P_T)$ . The initial peak

is the side-on value; the second peak is the portion of the shock wave reflected upstream from the target plate. The lower trace is the transmitted pressure at Station 6 (CH6).

Plate No.	Shot No.	Area Vented Percent	Hole Diameter
1	22	4.69	1/2
2	81	5.1	1/8
3	297	7.81	1/2
4	29	9.37	1/2
5	76	10.2	1/8
6	32	25.0	1/2
7	160	25,0	1/8
8	63	26.6	1/4
9	153	30.0	1/8
10	168	38.2	1/8
11	66	41.0	1/4
12	51	49.4	2-13/16
13	7	50.0	1/2

Table A-I. Data for Pressure-Time Records



PLATE I - TRANSMITTED PRESSURE

Figure A-1. Pressure-Time Traces Recorded at Stations 3 and 6 - 4.69 Percent Open



SHOT 81 CH6 SUPPRESSIVE STRUCTURES











PLATE 3-TRANSNITTED PRESSURE





# PLATE 4 - TRANSMITTED PRESSURE





PLATE 5-INPUT PRESSURE

SHOT 76 CH6 SUPPRESSIVE STRUCTURES



# PLATE 5-TRANSNITTED PRESSURE

Figure A-5. Pressure-Time Traces Recorded at Stations 3 and 6 - 10.2 Percent Open



PLATE G-TRANSNITTED PRESSURE





PLATE 7 - INPUT PRESSURE



# PLATE 7-TRANSMITTED PRESSURE







SHOT 63 CH6 SUPPRESSIVE STRUCTURES



PLATE 8-TRANSMITTED PRESSURE

Figure A-8. Pressure-Time Traces Recorded at Stations 3 and 6 - 26.6 Percent Open







PLATE 9 - TRANSMITTED PRESSURE

Figure A-9. Pressure-Time Traces Recorded at Stations 3 and 6 - 30 Percent Open







Figure A-10. Pressure-Time Traces Recorded at Stations 3 and 6 - 38,2 Percent Open



PLATE II - INPUT PRESSURE

SHOT 54 CH6 SUPPRESSIVE STRUCTURES

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# PLATE II-TRANSNITTED PRESSURE

Figure A-11. Pressure-Time Traces Recorded at Stations 3 and 6 - 41.0 Percent Open















# PLATE 13 - INPUT PRESSURE

SHOT 7 CH6 SUPPRESSIVE STRUCTURES



# PLATE 13 - TRANSNITTED PRESSURE

Figure A-13. Pressure-Time Traces Recorded at Stations 3 and 6 - 50 Percent Open

## LIST OF SYMBOLS

$$A_v$$
Percent of plate vented =  $\frac{\text{area vented}}{\text{area of tube}} \times 100$  $P_I$ Input peak overpressure $P_T$ Transmitted peak overpressure $P_T$ 100Transmitted peak overpressure for unobstructed tube $P_T$ Pressure transmission ratio =  $\frac{P_T \text{ for Plate}}{P_T 100}$ PsiPounds force per square inchPaPascal (newtons per square metre)NOTE:Psi x 6.894757 = kPa.

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Marine Corps Ln Ofc Dir, USAMSAA ATTN: Dr. J. Sperrazza Mr. R. Norman, GWD

Cdr, APG ATTN: STEAP-AD-R/RHA

Cdr, USAEA ATTN: SAREA-MT-T Mr. R. Thresher Dr. D. Katsanis Mr. B. Jezek Mr. J. McKivrigan