Simultaneous state and unknown inputs estimation with PI and PMI observers for Takagi Sugeno model with unmeasurable premise variables

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## Motivations

## Objective

Estimate simultanuously the state and unknown inputs of nonlinear systems described by a Takagi-Sugeno model using a Proportional Integral Observer (PIO) and Proportional Multiple Integral Observer (PMIO)

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## Difficulties

Unmeasurable premise variables

## Outline

(9) Takagi-Sugeno approach for modeling

- Takagi-Sugeno principle
- Takagi-Sugeno model


## (2) Proportional Integral Observer design

## (3) State and unknown input estimation

## 4 Numerical example

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2 Proportional Integral Observer design

3 State and unknown input estimation
(4) Numerical example
(5) Conclusions

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## Takagi-Sugeno approach for modeling

## Takagi-Sugeno principle

- Operating range decomposition in several local zones.
- A local model represent the behavior of the system in each zone.
- The overall behavior of the system is obtained by the aggregation of the sub-models with adequate weighting functions.


Nonlinear system

## Takagi-Sugeno approach for modeling

## Interests of Takagi-Sugeno approach

- Simple structure for modeling complex nonlinear systems.
- The specific study of the nonlinearities is not required.
- Possible extension of the theoretical LTI tools for nonlinear systems.


## Takagi-Sugeno model

The considered system is given by the following equations

$$
\left\{\begin{array}{l}
\dot{x}(t)=\sum_{i=1}^{r} \mu_{i}(\xi(t))\left(A_{i} x(t)+B_{i} u(t)\right) \\
y(t)=\sum_{i=1}^{r} \mu_{i}(\xi(t))\left(C_{i} x(t)+D_{i} u(t)\right)
\end{array}\right.
$$

- Interpolation mechanism : $\sum_{i=1}^{r} \mu_{i}(\xi(t))=1$ and $0 \leq \mu_{i}(\xi(t)) \leq 1, \forall t, \forall i \in\{1, \ldots, r\}$
- The premise variable $\xi(t)$ can be measurable (input $u(t)$,output $y(t), \ldots$ ) or unmeasurable (state $x(t), \ldots$ ).


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- Exact representation of the model $\dot{x}(t)=f(x(t), u(t))$.


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## Interests of T-S model with unmeasurable premise variables

- Exact representation of the model $\dot{x}(t)=f(x(t), u(t))$.
- Only one T-S model for FDI with observer banks.


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## Interests of T-S model with unmeasurable premise variables

- Exact representation of the model $\dot{x}(t)=f(x(t), u(t))$.
- Only one T-S model for FDI with observer banks.
- Exemple of application: security improvement in cryptography systems.


## Proportional Integral Observer design

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Let us consider the T-S system represented by

$$
\left\{\begin{array}{l}
\dot{x}(t)=\sum_{i=1}^{r} \mu_{i}(\xi(t))\left(A_{i} x(t)+B_{i} u(t)+E_{i} d(t)+W_{i} \omega(t)\right) \\
y(t)=C x(t)+G d(t)+W \omega(t)
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y(t)=C x(t)+G d(t)+W \omega(t)
\end{array}\right.
$$

## Assumption 1

Assume that the following assumptions hold:

- A1. The system is stable
- A2. The signals $u(t), d(t)$ and $\omega(t)$ are bounded.


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$$

## Assumption 1

Assume that the following assumptions hold:

- A1. The system is stable
- A2. The signals $u(t), d(t)$ and $\omega(t)$ are bounded.


## Assumption 2

The unknown inputs $d(t)$ are assumed to be constant:

- A3. $\dot{d}=0$
(This assumption will be relaxed in the PMIO design).


## Proportional Integral Observer design

Let us denote the estimated state by $\hat{x}$.

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The system can be re-written as follows:

$$
\dot{x}=\sum_{i=1}^{r} \mu_{i}(\hat{x})\left(A_{i} x+B_{i} u+E_{i} d+W_{i} \omega+v\right)
$$

where:

$$
v=\sum_{i=1}^{r}\left(\mu_{i}(x)-\mu_{i}(\hat{x})\right)\left(A_{i} x+B_{i} u+E_{i} d+W_{i} \omega\right)
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where:

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v=\sum_{i=1}^{r}\left(\mu_{i}(x)-\mu_{i}(\hat{x})\right)\left(A_{i} x+B_{i} u+E_{i} d+W_{i} \omega\right)
$$

The assumption A3. allows to write the system in the following augmented form:

$$
\left\{\begin{array}{l}
\dot{x}_{a}=\sum_{i=1}^{r} \mu_{i}(\hat{x})\left(\tilde{A}_{i} x_{a}+\tilde{B}_{i} u+\tilde{\Gamma}_{i} \tilde{\omega}\right) \\
y=\tilde{C} x_{a}+\tilde{D} \tilde{\omega}
\end{array}\right.
$$

where:

$$
\begin{gathered}
\tilde{A}_{i}=\left[\begin{array}{cc}
A_{i} & E_{i} \\
0 & 0
\end{array}\right], \quad \tilde{B}_{i}=\left[\begin{array}{c}
B_{i} \\
0
\end{array}\right], \quad \tilde{\Gamma}_{i}=\left[\begin{array}{cc}
1 & W_{i} \\
0 & 0
\end{array}\right], \quad \tilde{\omega}=\left[\begin{array}{l}
v \\
\omega
\end{array}\right] \\
\tilde{C}=\left[\begin{array}{ll}
C & G
\end{array}\right], \quad \tilde{D}=\left[\begin{array}{ll}
0 & W
\end{array}\right], \quad x_{a}=\left[\begin{array}{l}
x \\
d
\end{array}\right]
\end{gathered}
$$

## Proportional Integral Observer design

The proposed PI observer is given by the following equations:

$$
\left\{\begin{array}{l}
\dot{\hat{x}}=\sum_{i=1}^{r} \mu_{i}(\hat{x})\left(A_{i} \hat{x}+B_{i} u+E_{i} \hat{d}+K_{P i}(y-\hat{y})\right) \\
\hat{y}=C \hat{x}+G \hat{d} \\
\dot{\hat{d}}=\sum_{i=1}^{r} \mu_{i}(\hat{x}) K_{l i}(y-\hat{y})
\end{array}\right.
$$

where $\hat{x}$ and $\hat{d}$ are the estimates of $x$ and $d$.

## Proportional Integral Observer design

The proposed PI observer is given by the following equations:

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\dot{\hat{x}}=\sum_{i=1}^{r} \mu_{i}(\hat{x})\left(A_{i} \hat{x}+B_{i} u+E_{i} \hat{d}+K_{P i}(y-\hat{y})\right) \\
\hat{y}=C \hat{x}+G \hat{d} \\
\dot{\hat{d}}=\sum_{i=1}^{r} \mu_{i}(\hat{x}) K_{l i}(y-\hat{y})
\end{array}\right.
$$

where $\hat{x}$ and $\hat{d}$ are the estimates of $x$ and $d$.

A similar reasoning makes it possible to transform the proposed Pl observer in the following augmented form:

$$
\left\{\begin{array}{l}
\dot{\hat{x}}_{a}=\sum_{i=1}^{r} \mu_{i}(\hat{x})\left(\tilde{A}_{i} \hat{x}_{a}+\tilde{B}_{i} u+\tilde{K}_{i}(y-\hat{y})\right) \\
\hat{y}=\tilde{C} \hat{x}_{a}
\end{array}\right.
$$

where:

$$
\tilde{K}_{i}=\left[\begin{array}{c}
K_{P i} \\
K_{l i}
\end{array}\right]
$$

## Proportional Integral Observer design

Augmented state estimation error

$$
e_{a}(t)=x_{a}(t)-\hat{x}_{a}(t)
$$

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\begin{gathered}
e_{a}(t)=x_{a}(t)-\hat{x}_{a}(t) \\
\dot{e}_{a}=\sum_{i=1}^{r} \mu_{i}(\hat{x})\left(\left(\tilde{A}_{i}-\tilde{K}_{i} \tilde{C}\right) e_{a}+\left(\tilde{\Gamma}_{i}-\tilde{K}_{i} \tilde{D}\right) \tilde{\omega}\right)
\end{gathered}
$$

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Augmented state estimation error

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\end{gathered}
$$

## Objectives

The goal is to determine the gain matrices $\tilde{K}_{i}$ such that:

- The system which generates the state and unknown inputs errors is stable.

$$
\begin{aligned}
& \lim _{t \rightarrow \infty} e(t)=0, \quad \text { pour } \quad\|\tilde{\omega}\|_{2}=0 \\
& \|e(t)\|_{2}<\gamma\|\tilde{\omega}\|_{2} \text { pour }\|\tilde{\omega}\|_{2} \neq 0
\end{aligned}
$$

## Proportional Integral Observer design

## Lemma 1 [Tanaka and Wang 2001]

Consider the continuous-time TS-system defined by:

$$
\left\{\begin{array}{l}
\dot{x}(t)=\sum_{i=1}^{r} \mu_{i}(x(t))\left(A_{i} x(t)+B_{i} u(t)\right) \\
y(t)=C x(t)
\end{array}\right.
$$

The system is stable and verifies the $\mathscr{L}_{2}$-gain condition:

$$
\|y(t)\|_{2}<\gamma\|u(t)\|_{2}
$$

if there exists a symmetric positive definite matrix $P$ such that the following LMIs are satisfied for $i=1, \ldots, r$ :

$$
\left[\begin{array}{cc}
A_{i}^{T} P+P A_{i}+C^{T} C & P B_{i} \\
B_{i}^{T} P & -\gamma^{2} I
\end{array}\right]<0
$$

## Proportional Integral Observer design

## Theorem 1: PIO

The PI observer for the system is determined by minimizing $\bar{\gamma}$ under the following LMI constraints in the variables $P=P^{T}>0, M_{i}$ and $\bar{\gamma}$ for $i=1, \ldots, r$ :

$$
\left[\begin{array}{cc}
\tilde{A}_{i}^{T} P+P \tilde{A}_{i}-M_{i} \tilde{C}-\tilde{C}^{T} M_{i}^{T}+I & P \tilde{\Gamma}_{i}-M_{i} \tilde{D} \\
\tilde{\Gamma}_{i}^{T} P-\tilde{D}^{T} M_{i}^{T} & -\bar{\gamma} I
\end{array}\right]<0
$$

The gains of the observer are derived from:

$$
\tilde{K}_{i}=P^{-1} M_{i}
$$

and the attenuation level is calculated by:

$$
\gamma=\sqrt{\bar{\gamma}}
$$

## Proportional Multiple Integral Observer design

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Let us consider the T-S system represented by

$$
\left\{\begin{array}{l}
\dot{x}(t)=\sum_{i=1}^{r} \mu_{i}(\xi(t))\left(A_{i} x(t)+B_{i} u(t)+E_{i} d(t)+W_{i} \omega(t)\right) \\
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y(t)=C x(t)+G d(t)+W \omega(t)
\end{array}\right.
$$

## Assumption 3

The unknown input is assumed to be a bounded time varying signal with null $q^{\text {th }}$ derivative:

- A4. $d^{(q)}(t)=0$


## Proportional Multiple Integral Observer design

Consider the generalization of the proportional multiple-integral observer to T-S systems of the PMI observer:

$$
\left\{\begin{array}{l}
\dot{\hat{x}}=\sum_{i=1}^{r} \mu_{i}(\hat{x})\left(A_{i} \hat{x}+B_{i} u+E_{i} \hat{d}_{0}+K_{P i}(y-\hat{y})\right) \\
\hat{y}=C \hat{x}+G \hat{d} \\
\dot{\hat{d}}_{0}=\sum_{i=1}^{r} \mu_{i}(\hat{x}) K_{l i}^{0}(y-\hat{y})+\hat{d}_{1} \\
\dot{\hat{d}}_{1}=\sum_{i=1}^{r} \mu_{i}(\hat{x}) K_{l i}^{1}(y-\hat{y})+\hat{d}_{2} \\
\vdots \\
\dot{\hat{d}}_{q-2}=\sum_{i=1}^{r} \mu_{i}(\hat{x}) K_{l i}^{q-2}(y-\hat{y})+\hat{d}_{q-1} \\
\dot{\hat{d}}_{q-1}=\sum_{i=1}^{r} \mu_{i}(\hat{x}) K_{l i}^{q-1}(y-\hat{y})
\end{array}\right.
$$

where $\hat{d}_{i}, i=1,2, \ldots,(q-1)$ are the estimation of the $(q-1)$ first derivatives of the unknown input $d(t)$.

## Proportional Multiple Integral Observer design

The state and unknown inputs estimation errors are:

$$
e=x-\hat{x}, \quad e_{0}=\dot{d}-\dot{\hat{d}}_{0}, \ldots, \quad e_{q-1}=\dot{d}_{q-1}-\dot{\hat{d}}_{q-1}
$$

Their dynamics are given in the following form:

$$
\left\{\begin{array}{l}
\dot{e}=\sum_{i=1}^{r} \mu_{i}(\hat{x})\left(\left(A_{i}-K_{P i} C\right) e+\left(\Gamma_{i}-K_{P i} \bar{W}\right) \tilde{\omega}+\left(E_{i}-K_{P i} G\right) e_{0}\right) \\
\dot{e}_{0}=\sum_{i=1}^{r} \mu_{i}(\hat{x})\left(-K_{l i}^{0} C e+e_{1}-K_{l i}^{0} \bar{W} \tilde{\omega}-K_{l i}^{0} G e_{0}\right) \\
\dot{e}_{1}=\sum_{i=1}^{r} \mu_{i}(\hat{x})\left(-K_{l i}^{1} C e+e_{2}-K_{l i}^{1} \bar{W} \tilde{\omega}-K_{l i}^{1} G e_{0}\right) \\
\vdots \\
\dot{e}_{q-2}=\sum_{i=1}^{r} \mu_{i}(\hat{x})\left(-K_{l i}^{0} C e+e_{q-1}-K_{l i}^{q-2} \bar{W} \tilde{\omega}-K_{l i}^{q-2} G e_{0}\right) \\
\dot{e}_{q-1}=\sum_{i=1}^{r} \mu_{i}(\hat{x})\left(-K_{l i}^{q-1} C e-K_{l i}^{0} \bar{W} \tilde{\omega}-K_{l i}^{q-1} G e_{0}\right)
\end{array}\right.
$$

where:

$$
\Gamma_{i}=\left[\begin{array}{ll}
I_{n} & W_{i}
\end{array}\right], \quad \bar{W}=\left[\begin{array}{ll}
0 & W
\end{array}\right]
$$

## Proportional Multiple Integral Observer design

In the augmented form, we have:

$$
\begin{aligned}
\dot{\tilde{e}} & =\sum_{i=1}^{r} \mu_{i}(\hat{x})\left(\left(\tilde{A}_{i}-\tilde{K}_{i} \tilde{C}\right) \tilde{e}+\left(\tilde{\Gamma}_{i}-\tilde{K}_{i} \bar{W}\right) \tilde{\omega}\right) \\
{\left[\begin{array}{c}
e \\
e_{0}
\end{array}\right] } & =\bar{C} \tilde{e}
\end{aligned}
$$

where:

$$
\begin{gathered}
\tilde{e}=\left[\begin{array}{c}
e \\
e_{0} \\
e_{1} \\
\vdots \\
e_{q-2} \\
e_{q-1}
\end{array}\right], \quad \tilde{A}_{i}=\left[\begin{array}{cccccc}
A_{i} & E_{i} & 0 & \ldots & 0 & 0 \\
0 & 0 & l_{s} & \cdots & 0 & 0 \\
0 & 0 & 0 & \ddots & 0 & 0 \\
\vdots & \vdots & \vdots & \vdots & \vdots & \vdots \\
0 & 0 & 0 & 0 & 0 & I_{s} \\
0 & 0 & 0 & 0 & 0 & 0
\end{array}\right], \\
\tilde{K}_{i}=\left[\begin{array}{llll}
K_{P i}^{T} & K_{l i}^{0^{T}} & K_{l i}^{1 T} & \ldots \\
K_{l i}^{q-2^{T}} & K_{l i}^{q-1}{ }^{T}
\end{array}\right]^{T} \\
\tilde{C}=\left[\begin{array}{llllll}
C & G & 0 & \ldots & 0 & 0
\end{array}\right] \\
\tilde{\Gamma}_{i}=\left[\begin{array}{llll}
\Gamma_{i}^{T} & 0 & \ldots & 0
\end{array}\right]^{T}
\end{gathered}
$$

## Proportional Multiple Integral Observer design

In the following, we are only interested with particular components $e$ and $e_{0}$ of $\tilde{e}$ :

$$
\left[\begin{array}{c}
e \\
e_{0}
\end{array}\right]=\bar{C} \tilde{e}
$$

where:

$$
\bar{C}=\left[\begin{array}{cc|ccc}
I_{n} & 0 & 0 & \cdots & 0 \\
0 & I_{s}
\end{array}\right]
$$

0 represents null matrix with appropriate dimensions.

## Proportional Multiple Integral Observer design

## Theorem 2

The PMI observer for the system that minimizes the transfer from $\tilde{\omega}(t)$ to $\left[e(t)^{T} e_{0}(t)^{T}\right]$ is obtained by finding the matrices $P=P^{T}>0, M_{i}$ and $\bar{\gamma}$ that minimize $\bar{\gamma}$ under the following LMI constraints for $i=1, \ldots, r$ :

$$
\left[\begin{array}{cc}
\tilde{A}_{i}^{T} P+P \tilde{A}_{i}-M_{i} \tilde{C}-\tilde{C}^{T} M_{i}^{T}+\bar{C}^{T} \bar{C} & P \tilde{\Gamma}_{i}-M_{i} \bar{W} \\
\tilde{\Gamma}_{i}^{T} P-\bar{W}^{T} M_{i}^{T} & -\bar{\gamma} I
\end{array}\right]<0
$$

The gains of the observer are derived from:

$$
\tilde{K}_{i}=P^{-1} M_{i}
$$

and the attenuation level is calculated by:

$$
\gamma=\sqrt{\bar{\gamma}}
$$

## Numerical example

## Numerical example

Consider a continuous-time T-S system defined by:

$$
\begin{gathered}
A_{1}=\left[\begin{array}{ccc}
-2 & 1 & 1 \\
1 & -3 & 0 \\
2 & 1 & -8
\end{array}\right], A_{2}=\left[\begin{array}{ccc}
-3 & 2 & -2 \\
5 & -3 & 0 \\
1 & 2 & -4
\end{array}\right], \\
B_{1}=\left[\begin{array}{c}
1 \\
5 \\
0.5
\end{array}\right], \quad B_{2}=\left[\begin{array}{c}
3 \\
1 \\
-7
\end{array}\right], E_{1}=\left[\begin{array}{ll}
0 & 7 \\
0 & 5 \\
0 & 2
\end{array}\right], \\
E_{2}=\left[\begin{array}{ll}
0 & 6 \\
0 & 3 \\
0 & 1
\end{array}\right], \quad W_{1}=W_{2}=\left[\begin{array}{l}
1 \\
1 \\
1
\end{array}\right], W=\left[\begin{array}{l}
0.5 \\
0.5
\end{array}\right],
\end{gathered}
$$

and

$$
C=\left[\begin{array}{lll}
1 & 1 & 1 \\
1 & 0 & 1
\end{array}\right], \quad G=\left[\begin{array}{ll}
5 & 0 \\
1 & 0
\end{array}\right]
$$

$d(t)=\left[\begin{array}{ll}d_{1}(t)^{T} & d_{2}(t)^{T}\end{array}\right]^{T}$.

## Numerical example

The weighting functions depend on the first component $x_{1}$ of the state vector $x$ and are defined as follows:

$$
\left\{\begin{array}{l}
\mu_{1}(x)=\frac{1-\tanh \left(x_{1}\right)}{2}  \tag{1}\\
\mu_{2}(x)=1-\mu_{1}(x)
\end{array}\right.
$$

The weighting functions obtained without perturbations and unknown inputs are shown in figure 1 . This figure shows that the system is clearly nonlinear since $\mu_{1}$ and $\mu_{2}$ are not constant functions.


Figure: Weighting functions $\mu_{1}$ and $\mu_{2}$

## Numerical example



Figure: Unknown input estimation with a PI observer

## Numerical example



Figure: Unknown input estimation with a PMI observer

## Numerical example



Figure: State estimation error with a PI observer


Figure: State estimation error with a PMI observer

## Conclusions and perspectives

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- PI and PMI observers design for nonlinear systems represented by a Takagi-Sugeno structure.


## Perspectives

## Conclusions and perspectives

## Conclusions

- PI and PMI observers design for nonlinear systems represented by a Takagi-Sugeno structure.
- Study of the case where the premise variables are unmeasurable


## Perspectives

## Conclusions and perspectives

## Conclusions

- PI and PMI observers design for nonlinear systems represented by a Takagi-Sugeno structure.
- Study of the case where the premise variables are unmeasurable
- Comparison between the results obtained by PI and PMI observers


## Perspectives

## Conclusions and perspectives

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- Study and reduction of the conservatism when searching a common Lyapunov matrix $P$, which satisfies $r$ LMIs.


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## Perspectives

- Study and reduction of the conservatism when searching a common Lyapunov matrix $P$, which satisfies $r$ LMIs.
- Extension to fault tolerant control of nonlinear systems.


## Thank you for your attention!

