



Solving Low-Frequency EM-Ckt Problems Using the PEEC Method

Dipanjan Gope*

**Circuit Technology CAD
INTEL Corporation**



Albert Ruehli

**System Level Design
T.J. Watson IBM Research**



Vikram Jandhyala

**Electrical Engineering
University of Washington**





- **Numerical Problems for Low-Frequency EFIE**

- Low-Frequency in Circuits: Why Should We Bother?
- What are the Detrimental Numerical Effects?

- **Existing Solution Methods**

- **PEEC Low-Frequency Solution**

- Basic PEEC Cell
- Low-Frequency Strategies

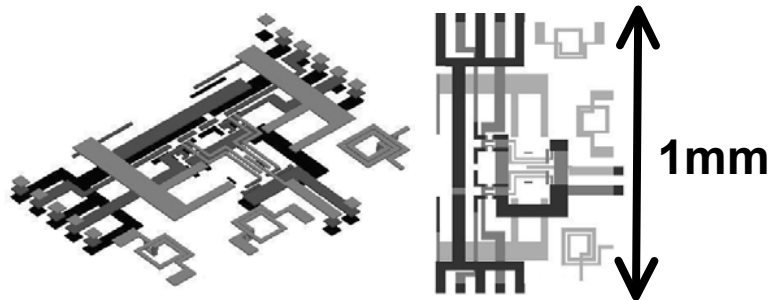
- **EFIE Low-Frequency Solution**

- **Results and Conclusions**

“Low Frequency” in Circuits



1. Electrically Small Structure



UW VCO Structure

$$f = 40\text{GHz}$$

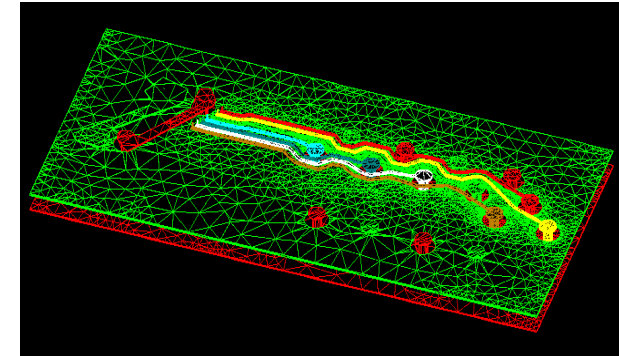
$$\lambda = 7.5\text{mm}$$

$$\frac{\text{dimension}}{\text{frequency}} \ll 1$$

Electrically Small

On-Chip

2. Local Refined Mesh



Courtesy: Ansoft Corporation

Boards
Packages

Electrostatic

$$\begin{bmatrix} C_{11} & C_{12} & C_{13} \\ C_{21} & C_{22} & C_{23} \\ C_{31} & C_{32} & C_{33} \end{bmatrix}$$

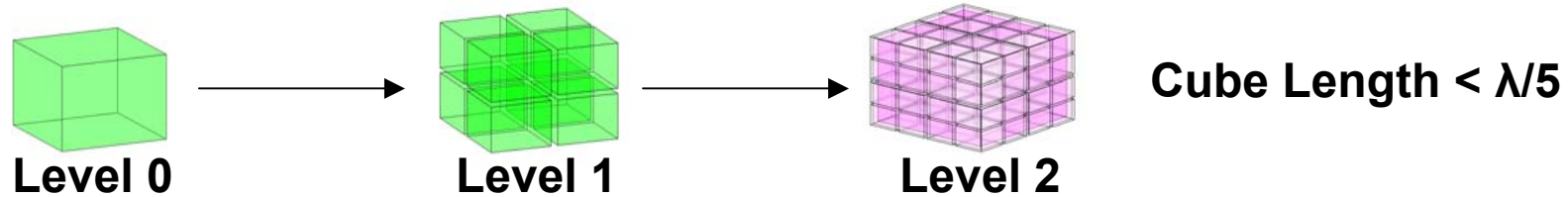
Magnetostatic

$$\begin{bmatrix} L_{11} & L_{12} & L_{13} \\ L_{21} & L_{22} & L_{23} \\ L_{31} & L_{32} & L_{33} \end{bmatrix}$$

ElectroMagnetic
Numerical Problems

$$\begin{bmatrix} S_{11} & S_{12} & S_{13} \\ S_{21} & S_{22} & S_{23} \\ S_{31} & S_{32} & S_{33} \end{bmatrix}$$

- “Low Frequency” Fast Solver Problem
 - Traditional FMM: Singularity in Hankel function



- Solution 1: Low Frequency FMM, Chew *etal.*
- Solution 2: QR-PEEC fast iterative solver, Ruehli *etal.* EPEP'04

- “Low Frequency” Mixed Potential Problem
 - Affects solver convergence: larger number of iterations
 - Affects accuracy even for direct solution



Frequency domain, Method of Moments

$$\mathbf{E}_{\text{tan}}^s(\mathbf{J}) + \mathbf{E}_{\text{tan}}^i = Z_s \mathbf{J}$$

Electric Field Integral Equation

$$\mathbf{E}^s(\mathbf{J}) = -j\omega\mathbf{A} - \nabla\Phi$$

Scattered Electric Field

$$\mathbf{A}(\mathbf{r}) = \frac{\mu}{4\pi s} \int \frac{e^{-jk|\mathbf{r}-\mathbf{r}'|} \mathbf{J}(\mathbf{r}')}{|\mathbf{r}-\mathbf{r}'|} ds'$$

Electric Vector Potential

$$\Phi(\mathbf{r}) = \frac{1}{4\pi\epsilon s} \int \frac{e^{-jk|\mathbf{r}-\mathbf{r}'|} \rho(\mathbf{r}')}{|\mathbf{r}-\mathbf{r}'|} ds'$$

Electric Scalar Potential

$$\nabla_s \cdot \mathbf{J}(\mathbf{r}) + j\omega\rho(\mathbf{r}) = 0$$

Continuity Equation

$$\mathbf{E}^s(\mathbf{J}) = -j\omega \frac{\mu}{4\pi s} \int \frac{e^{-jk|\mathbf{r}-\mathbf{r}'|} \mathbf{J}(\mathbf{r}')}{|\mathbf{r}-\mathbf{r}'|} ds' - \nabla \frac{1}{4\pi\epsilon s} \int \frac{e^{-jk|\mathbf{r}-\mathbf{r}'|} \rho(\mathbf{r}')}{|\mathbf{r}-\mathbf{r}'|} ds'$$

Vector and Scalar potential from EM Currents

Mixed Potential Problems

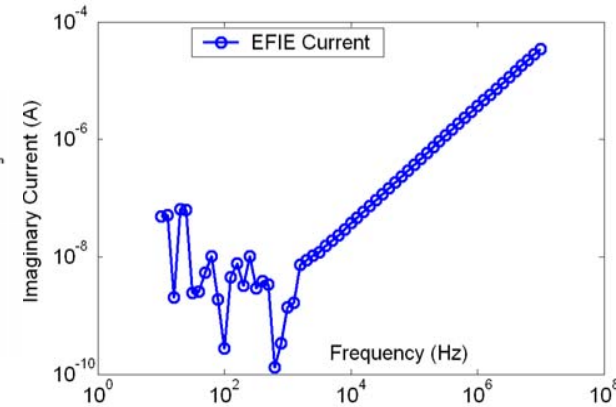
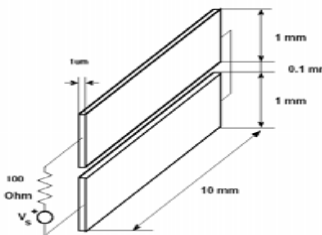
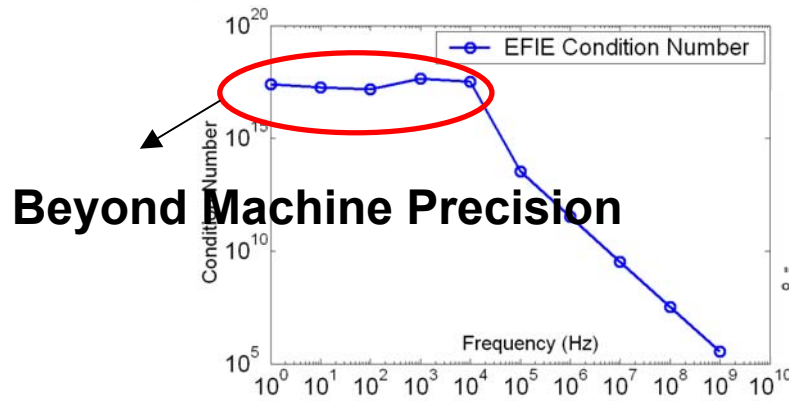


$$\begin{matrix} \updownarrow \\ N_e \end{matrix} \begin{matrix} \leftarrow \rightarrow \\ \text{Rank} = N_e \end{matrix} \begin{matrix} \boxed{j\omega \bar{\mathbf{L}}} \\ \leftarrow \rightarrow \\ N_e \end{matrix} + \frac{1}{j\omega} \bar{\mathbf{A}}_{N_e \times N_p} \times \begin{matrix} \boxed{\bar{\mathbf{P}}} \\ \leftarrow \rightarrow \\ N_p \end{matrix} \times \bar{\mathbf{A}}_{N_p \times N_e}^T = \begin{matrix} \updownarrow \\ N_e \end{matrix} \begin{matrix} \leftarrow \rightarrow \\ N_e \end{matrix} \begin{matrix} \boxed{\bar{\mathbf{Z}}} \\ \leftarrow \rightarrow \\ N_e \end{matrix}$$

$\leftarrow \rightarrow$ Rank = N_p

For a closed object: $N_e = 1.5N_p$

Effects



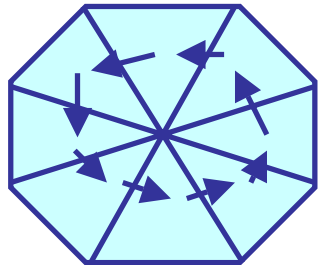
1. Fast Solver Convergence Suffers

2. Direct Solver Result Suffers

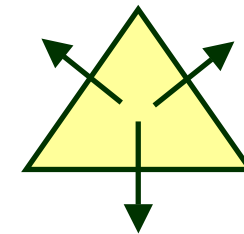
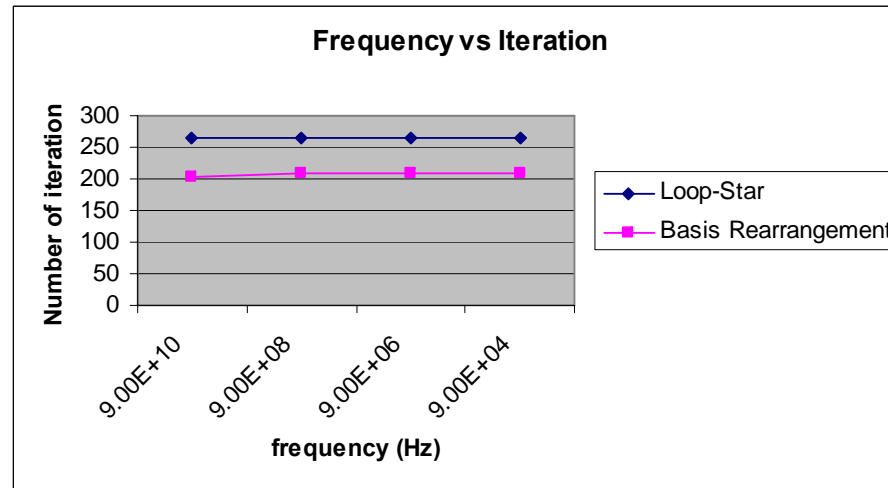


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Loop-Star Decomposition



Loop basis



Star basis

- **Loop basis for solenoidal current (Magneto-static)**
- **Star basis for curl-free current (Electrostatic)**
- **Frequency scaling for improved spectral property**
- **Number of iterations does not scale with frequency**

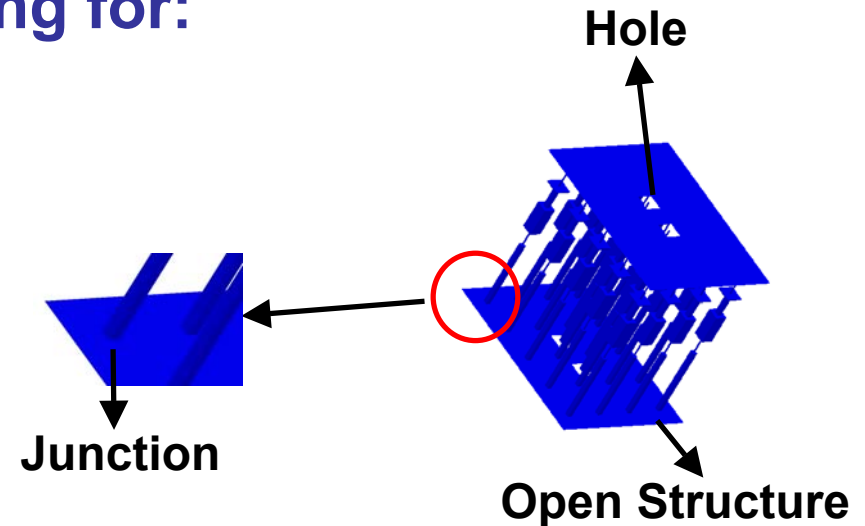
Courtesy: Slide by Swagato Chakraborty

Chew *etal.*



- **Loop Detection is Challenging for:**

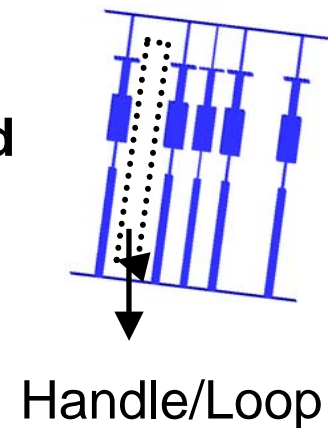
- Open structures
- Structure with holes
- Structure with handles
- Structures with junction



More Significant

- **Where to Apply Loop-Star Basis Functions**

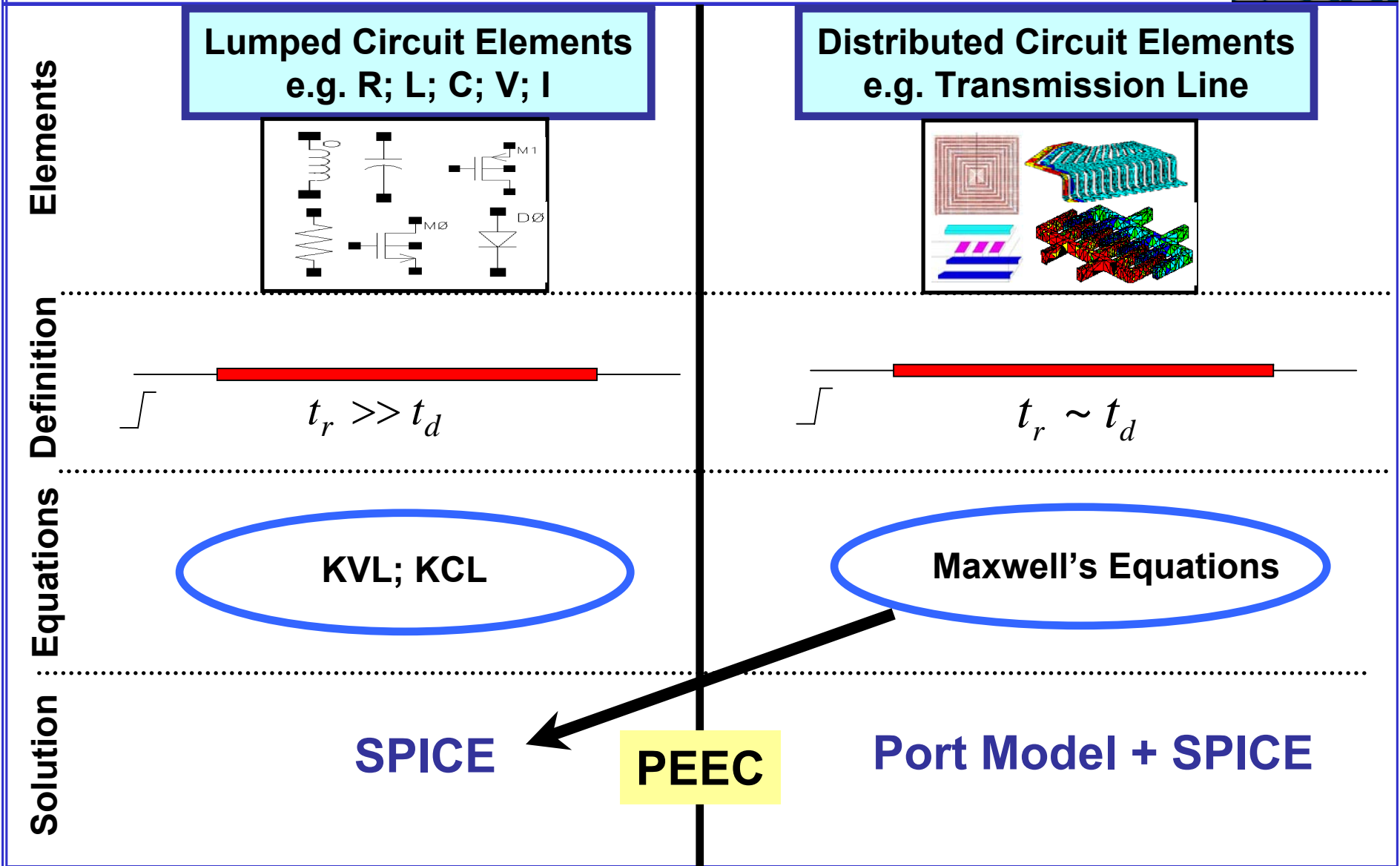
- Detection of mesh where loop-star should be applied
- Detrimental effects if applied wrongly





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PEEC Single Matrix: EM / Circuit





$$\bar{E}^i(\bar{r}, \omega) = \frac{\bar{J}(\bar{r})}{\sigma} + j\omega\mu \int_{v'} G(\bar{r}, \bar{r}') \bar{J}(\bar{r}) dv' + \frac{\nabla}{j\omega} \int_{v'} G(\bar{r}, \bar{r}') q(\bar{r}) dv'$$

Circuit Model Element Identification

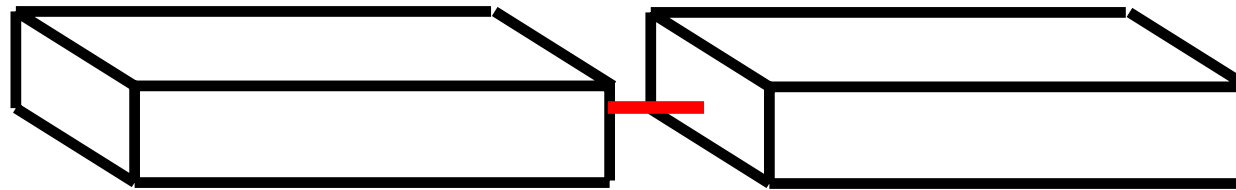
- KVL: Voltage = R I + sLp I + Q/sC
- RHS Term 1: Resistance
- RHS Term 2: Partial Inductance
- RHS Term 3: Coefficients of Partial Potential



PEEC Stick Example



Geometry



Conductor

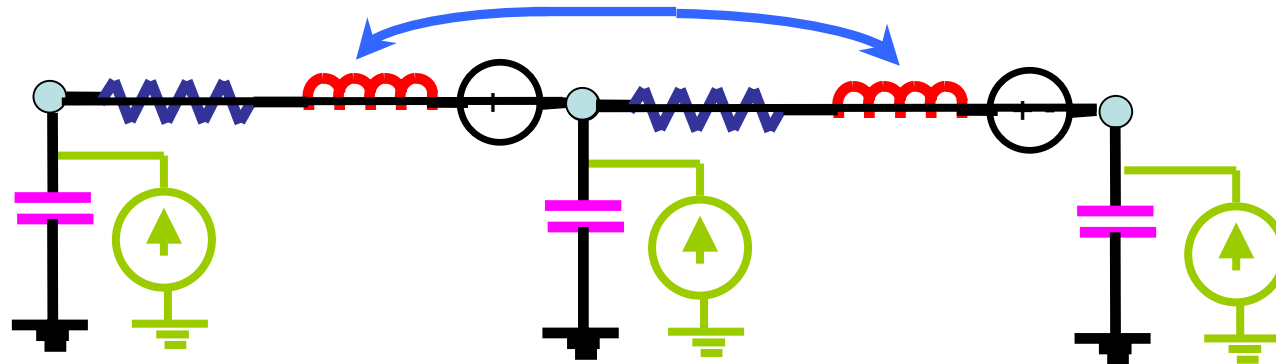
R1	N1	N2	1.202mOhms	
L1	N2	N3	5.887nH	
C1	N1	0	1.702pF	
K12	L1	L2	1.282nH	0.054ns
F12	N4	0	V1	0.124
				0.032ns

Possible Solution Schemes: .cap, .ind, .ac, .tran

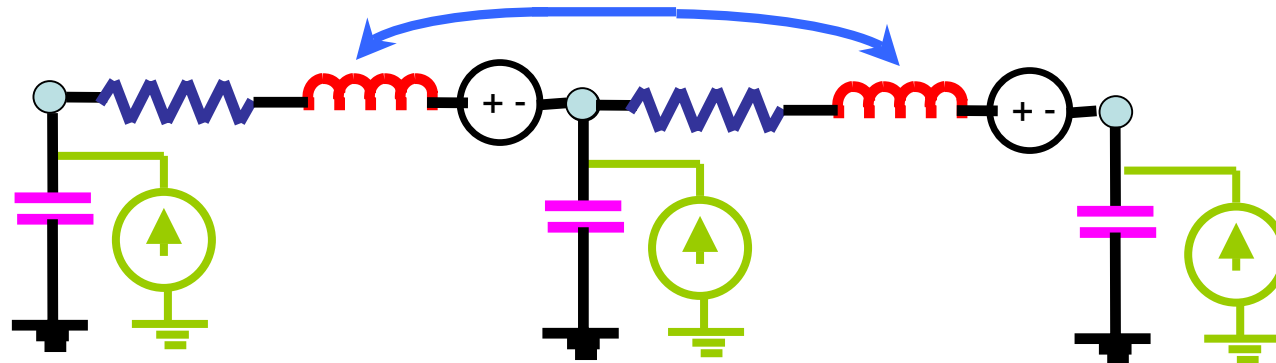


Continuity Equation $\nabla \cdot J = -j\omega\rho$ NOT Valid

- ElectroStatic: Short Inductors (.cap)

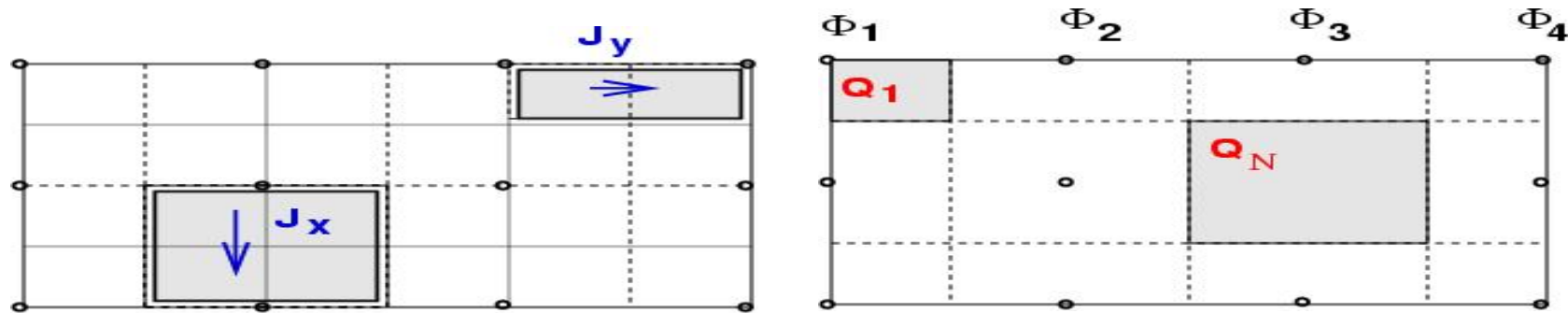


- MagnetoStatic: Open Capacitors (.ind)





Step 1: Separate Charge and Current Basis Functions



- Charge Basis is Not Derived From Current Basis (Unlike RWG Basis)
- Enables Stamping of Scalar and Vector Potentials Differently
 - Vector potential is stamped in the impedance form (KVL)
 - Scalar potential is stamped in the admittance form (KCL)
 - Both cases ω is in the numerator in matrix elements

In Contrast RWG-EFIE is Completely KVL

$$EFIE :: \left(j\omega \bar{\mathbf{L}}_{N_e \times N_e} + \frac{1}{j\omega} \bar{\mathbf{A}}_{N_e \times N_p} \bar{\mathbf{P}}_{N_p \times N_p} \bar{\mathbf{A}}_{N_p \times N_e}^T \right) \langle t_{i=0 \dots N_e}, E_{inc} \rangle$$



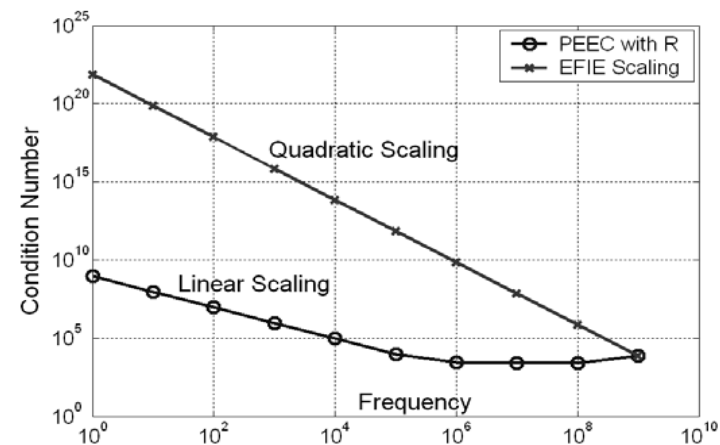
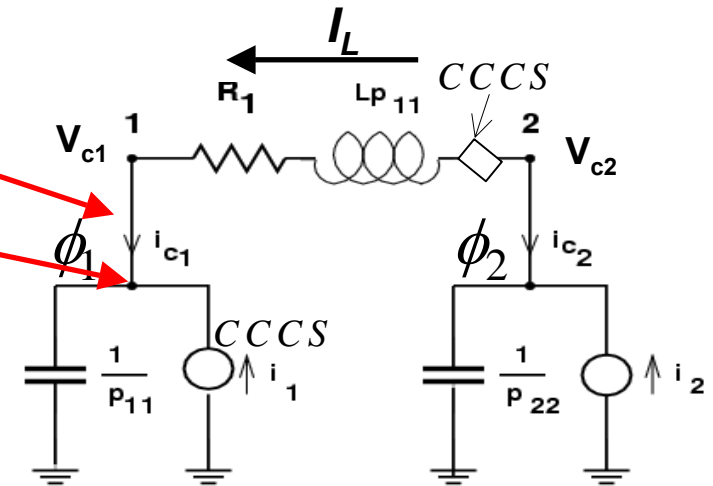
Step 1: Separate Charge and Current Basis Functions

1	-1	0	0	0	0	0						
0	$\frac{s}{P_{11}}$	0	0	-1	$\frac{P_{12}}{P_{11}}$	0						
0	0	1	-1	0	0	0						
0	0	0	$\frac{s}{P_{11}}$	$\frac{P_{21}}{P_{22}}$	-1	0						
0	0	0	0	1	0	1						
0	0	0	0	0	1	-1						
0	-1	0	1	0	0	$-R-sLp_{11}$						

KVL

$$\begin{bmatrix} \phi \\ V_{c1} \\ \phi_2 \\ V_{c2} \\ I_{c1} \\ I_{c2} \\ I_L \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ I_s \\ 0 \\ 0 \end{bmatrix}$$

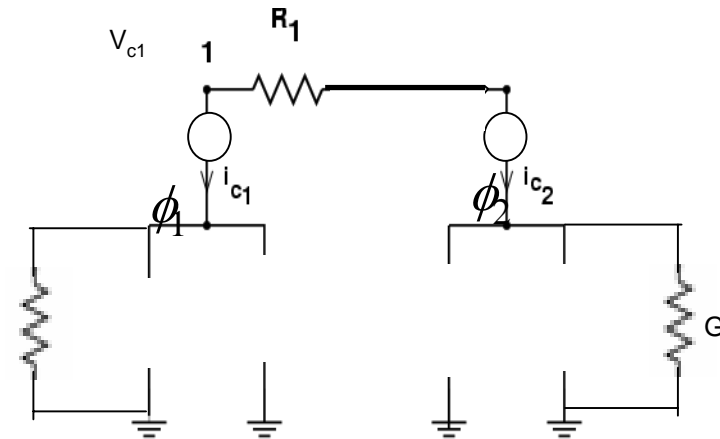
KCL



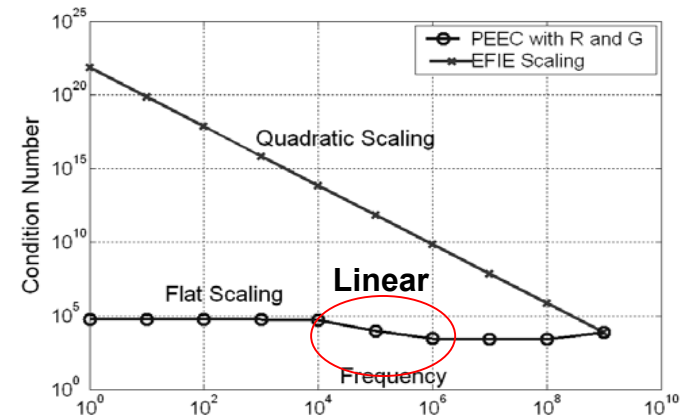
- No Extra Memory
- No Extra MatVec Product Time
- No ω in Denominator
- No ω in Off-Diagonal

Step 2: Incorporation of Dielectric Loss

$$\begin{bmatrix}
 1 & -1 & 0 & 0 & 0 & 0 & 0 \\
 0 & G + \frac{s}{P_{11}} & 0 & 0 & -1 & -\frac{P_{12}}{P_{11}} & 0 \\
 0 & 0 & 1 & -1 & 0 & 0 & 0 \\
 0 & 0 & 0 & G + \frac{s}{P_{11}} & -\frac{P_{21}}{P_{22}} & -1 & 0 \\
 0 & 0 & 0 & 0 & 1 & 0 & 1 \\
 0 & 0 & 0 & 0 & 0 & 1 & 1 \\
 1 & -1 & 0 & 0 & 0 & 0 & -R - sLP_{11}
 \end{bmatrix}$$

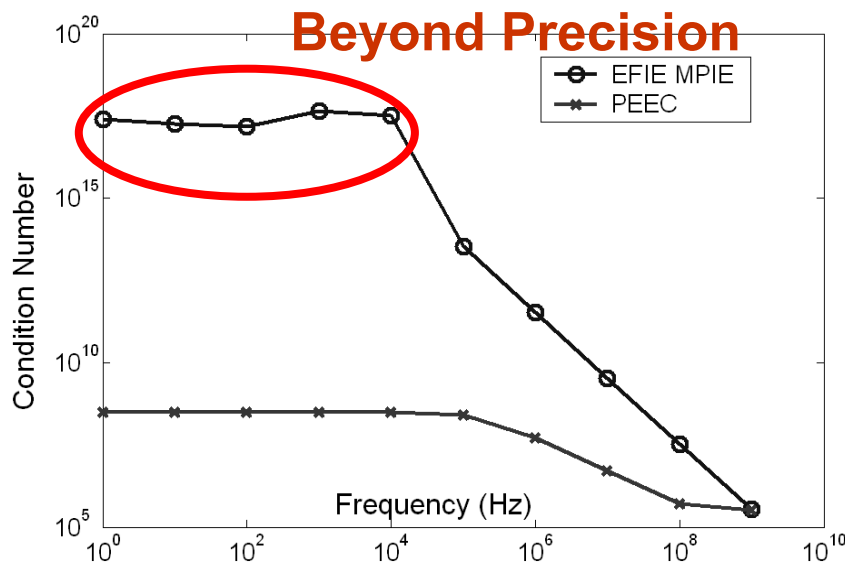
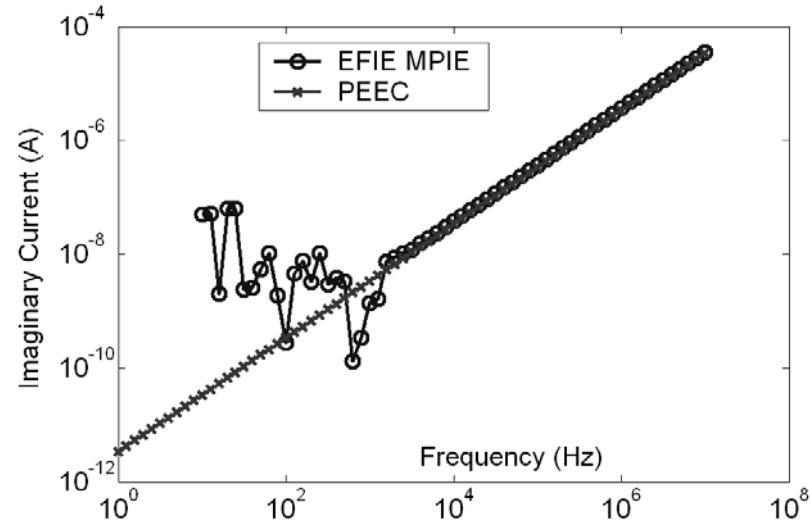
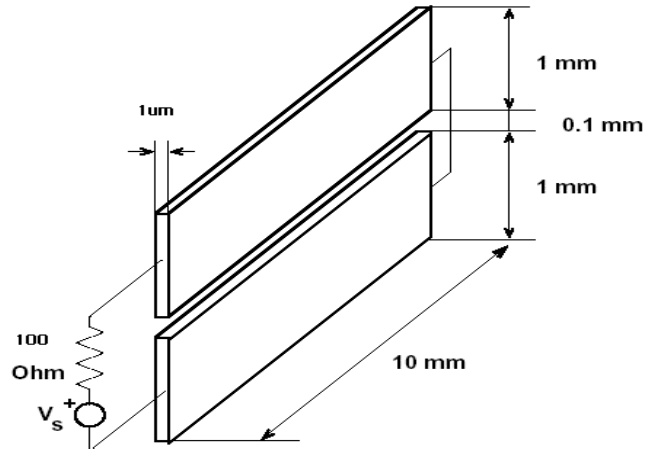


Seam Less Transition to DC



At Low Frequencies R and G Dominate

Transmission Line Example



PEEC Solver Results



Conclusions



- Separated Potential Enables Mixed KCL/KVL Form
- Loss Enables Flat Conditioning at Low Frequencies
 - Loss dominates over all effects at low frequencies
- Seam-Less Transition from .ac to .cap and .ind
- Does Not Harm Conditioning for Electrically Large Mesh
- No Requirement for Loop Detection

Highlight

