

Received December 20, 2019, accepted December 30, 2019, date of publication January 3, 2020, date of current version January 14, 2020.

Digital Object Identifier 10.1109/ACCESS.2019.2963768

# Sound Source Localization Based on GCC-PHAT With Diffuseness Mask in Noisy and Reverberant Environments

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This work was supported in part by the Institute for Information and Communications Technology Promotion (IITP) grant funded by the Korean Government Ministry of Science and ICT (MSIT) (Development of Human Enhancement Technology for Auditory and Muscle Support) under Grant 2017-0-00050, and in part by the National Research Foundation of Korea (NRF) grant funded by the Korean Government (MSIT) under Grant NRF-2017R1A2B4009964.

**ABSTRACT** Although sound source localization is a desirable technique in many communication systems and intelligence applications, the distortion caused by diffuse noise or reverberation makes the time delay estimation (TDE) between signals acquired by a pair of microphones a complicated and challenging problem. In this paper, we describe a method that can efficiently achieve sound source localization in noisy and reverberant environments. This method is based on the generalized cross-correlation (GCC) function with phase transform (PHAT) weights (GCC-PHAT) to achieve robustness against reverberation. In addition, to estimate the time delay robust to diffuse components and to further improve the robustness of the GCC-PHAT against reverberation, time-frequency (t-f) components of observations directly emitted by a point source are chosen by “inversed” diffuseness. The diffuseness that can be estimated from the coherent-to-diffuse power ratio (CDR) based on spatial coherence between two microphones represents the contribution of diffuse components on a scale of zero to one with direct sounds from a source modeled to be fully coherent. In particular, the “inversed” diffuseness is binarized with a very rigorous threshold to select highly reliable components for accurate TDE even in noisy and reverberant environments. Experimental results for both simulated and real-recorded data consistently demonstrated the robustness of the presented method against diffuse noise and reverberation.

**INDEX TERMS** Diffuseness mask, GCC-PHAT, reverberation, sound source localization.

## I. INTRODUCTION

Sound source localization is a desirable technique in various communication systems and intelligence applications, including speech enhancement in noisy and reverberant environments by forming a beam toward the target source [1], [2]. Typically, it can be achieved by exploiting the difference among the signals obtained by spatially separated microphones. If many microphones are available, the direction of arrival (DOA) of a sound source can be accurately estimated by numerous approaches combining various information based on the microphone signals (e.g., [3]–[6]), and

The associate editor coordinating the review of this manuscript and approving it for publication was Prakasam Periasamy.

learning-based approaches such as [7] may provide even better localization performance. They may result in successful localization of multiple sound sources in various real-world situations (e.g., [8]–[10]).

Given a pair of microphones possibly due to a limited resource or a compact size, the DOA of a source is related to the difference between the times taken by the sound from a source to reach the microphones. A lot of methods ranging from exploitation of interaural cues inspired by binaural processing to introduction of various techniques for mathematical analysis, even with learning from data, have been proposed (e.g., [11]–[18]). Among those methods, a class of cross-correlation-based methods is the most intuitive and popular approach, where the frame-wise relative time

delay can be estimated by determining the maximum of the cross-correlation function of signals acquired by the pair of microphones [18]. The localization would be easy if the two signals were merely delayed and scaled versions of each other. In real-world situations, however, the acquired signals are frequently prone to contamination by ambient noise. Furthermore, the signals may contain multiple attenuated and delayed replicas of the source signal caused by reverberation. The distortion caused by noise or reverberation makes the time delay estimation (TDE) a complicated and challenging problem [13], [19]. Over the past few decades, researchers have tackled this problem by exploiting different aspects of the observed signals and developed numerous algorithms [2].

Typically, the cross-correlation function is more affected by low-frequency components where most of the natural sound (including speech) energy is concentrated. Therefore, the cross-correlation function may frequently have a flatter peak that can disturb accurate TDE. To overcome this vulnerability, Knapp and Carter [18] introduced the generalized cross-correlation (GCC) function, which results in a cross-correlation function with a frequency weighting, and several weightings have been presented for accurate TDE in considered situations [1]. One of the most commonly used weightings is phase transform (PHAT) weighting, which makes the TDE robust against reverberation. Since the steered-response power (SRP) objective function can be expressed as a sum of the GCCs for different microphone pairs with many microphones available, the GCC function with PHAT weights (GCC-PHAT) is essentially the same as the SRP function with PHAT weights (SRP-PHAT) given a pair of microphones [20], [21]. However, this weighting is known to be sensitive to additive noise, and the sensitiveness can be overcome by the maximum-likelihood (ML) weighting. In order to combine the advantages of both the weightings, Wang and Chu proposed the MLR weighting that is robust to both noise and reverberation [1], [22].

In order to achieve further robustness, masks have been applied to remove time-frequency(t-f) components of observed signals that were harmful for source localization by containing noise or reverberation significantly (e.g., [14], [23]–[27]). Using the non-stationarity of speech, the transition noise masks were estimated [28], or masks were obtained by signal-to-noise ratios (SNRs) computed with stationary noise estimates [29]. Wilson and Darrell exploited cues corresponding to sudden increases in audio energy by finding a mapping from reverberated signal spectrograms to localization precision as a soft mask, which exhibited behavior consistent with the precedence effect [30], [31] from psychoacoustic studies [32]. Since deep-learning-based t-f masking has dramatically improved the performance of monaural speech separation and enhancement, deep neural networks (DNNs) estimated masks to identify t-f components harmful for accurate TDE (e.g., [33]–[36]). Whereas masks estimated by [28] and [29] assumed stationary noise, learning-based methods such as [32]–[36] might not obtain

successful masks with insufficient learning data or for an environment unmatched with training data.

A typical acoustic impulse response characterizing the propagation of sound from a source to a microphone consists of the direct impulse and the early and late reflections. Considering that an observed signal can be modelled by the corresponding source signal convolved with an acoustic impulse response, signal components through direct paths provide the DOAs corresponding to sound locations, contrary to the reflected sound. Since a direct path is the shortest path from a source to a microphone, a sound arrives earlier at a microphone through the direct path than others. Therefore, the auditory onset, that is, the start of a discrete event in an acoustic signal, is robust against reverberation because a microphone mainly obtains sound through a direct path from a source during the onset [14], [37], [38]. If two microphone signals contain only direct sounds emitted from a source, they are delayed and scaled versions of each other, and fully coherent, whereas other components caused by diffuse noise or reverberation may be assumed to be diffuse. Since the spatial coherence between two microphones, as an efficient measure to distinguish coherent components from diffuse components, was used for signal enhancement [39], heuristic methods for noise reduction and dereverberation have been proposed [40], [41]. Especially, the spatial coherence (as known as interaural coherence from binaural auditory studies) was used for source localization [42], [43].

In this paper, we describe a method that can efficiently achieve sound source localization in noisy and reverberant environments. This method is based on the GCC-PHAT to achieve robustness against reverberation. In addition, for the TDE robust to diffuse noise or reverberation, t-f components of observed signals directly emitted by a point source are selected by “inversed” diffuseness [44]. Instead of using the spatial coherence estimates directly, a diffuseness estimator that represents the contribution of diffuse components on a scale of zero to one is computed from the coherent-to-diffuse power ratio (CDR) based on the spatial coherence estimates, formerly used for dereverberation [45]. Especially, the “inversed” diffuseness is binarized with a very rigorous threshold, prior to masking the t-f components of observed signals, in order to use highly reliable components for accurate TDE even in noisy and reverberant environments. Experimental results confirmed the robustness of the proposed method with signals affected by diffuse noise or reverberation.

## II. REVIEW OF A DIFFUSENESS ESTIMATOR BASED ON A DOA-INDEPENDENT CDR

In performing the localization of sound sources, direct sound from a source is helpful, but diffuse components interfere with the localization. In the short-time Fourier transform (STFT) domain, let us consider the  $i$ -th microphone signal  $X_i(m, k)$  composed of a direct signal component  $S_i(m, k)$  and an interfering component  $N_i(m, k)$  as

$$X_i(m, k) = S_i(m, k) + N_i(m, k), \quad (1)$$

where  $m$  and  $k$  index time frame and frequency bin, respectively. The short-time complex spatial coherence function of signals acquired by a pair of omnidirectional microphones is estimated by

$$\hat{\Gamma}_X(m, k) = \frac{\hat{\Phi}_{X_1 X_2}(m, k)}{\sqrt{\hat{\Phi}_{X_1 X_1}(m, k) \hat{\Phi}_{X_2 X_2}(m, k)}}, \quad (2)$$

where  $\hat{\Phi}_{X_i X_j}(m, k)$  denotes a short-time auto- or cross-power spectral density estimate between  $X_i(m, k)$  and  $X_j(m, k)$  typically obtained by recursive averaging: [45]

$$\hat{\Phi}_{X_i X_j}(m, k) = \lambda \hat{\Phi}_{X_i X_j}(m-1, k) + (1-\lambda) X_i(m, k) X_j^*(m, k), \quad (3)$$

where  $\lambda$  is a constant between 0 and 1, and  $(\cdot)^*$  denotes the complex conjugate.

If two microphone signals contain only direct sounds emitted from a source, they are delayed and scaled versions of each other, and fully coherent, as mentioned in Section I. An estimate of the ratio between the coherent and diffuse components, termed as the CDR [45] can be derived from the spatial coherence functions by [45]

$$\widehat{\text{CDR}}(m, k) = \frac{\hat{\Gamma}_N(m, k) - \hat{\Gamma}_X(m, k)}{\hat{\Gamma}_X(m, k) - \hat{\Gamma}_S(m, k)}, \quad (4)$$

where  $\hat{\Gamma}_S(m, k)$  and  $\hat{\Gamma}_N(m, k)$  are estimates of the short-time complex spatial coherence functions of direct signal components  $S_i(m, k)$  and interfering components  $N_i(m, k)$ ,<sup>1</sup> respectively. Assuming a diffuse or spherically isotropic sound field for  $N_i(m, k)$ , an ideal coherence function of  $N_i(m, k)$  is real-valued time-invariant and given by [46]

$$\tilde{\Gamma}_N(k) = \frac{\sin(2\pi f_k d/c)}{2\pi f_k d/c}, \quad (5)$$

where  $f_k$  is the analog frequency at the  $k$ -th frequency bin.  $d$  and  $c$  denote the distance between the two microphones and the speed of sound, respectively.

Without the need for explicit DOA estimation to obtain  $\hat{\Gamma}_S(m, k)$ , the knowledge that the direct sound from a source is fully coherent derives the DOA-independent CDR estimator given by [45], [47]

$$\widetilde{\text{CDR}}(m, k) = \frac{\tilde{\Gamma}_N(k) \Re\{\hat{\Gamma}_X(m, k)\} - |\hat{\Gamma}_X(m, k)|^2 - \bar{\Gamma}(m, k)}{|\hat{\Gamma}_X(m, k)|^2 - 1}, \quad (6)$$

where

$$\begin{aligned} \bar{\Gamma}(m, k) &= \sqrt{\tilde{\Gamma}_N^2 \Re\{\hat{\Gamma}_X\}^2 - \tilde{\Gamma}_N^2 |\hat{\Gamma}_X|^2 + \tilde{\Gamma}_N^2 - 2\tilde{\Gamma}_N \Re\{\hat{\Gamma}_X\} + |\hat{\Gamma}_X|^2}. \end{aligned} \quad (7)$$

<sup>1</sup>In the context of the CDR, the direct signal and interfering components usually mean coherent and diffuse components, respectively. Background noise including late reverberation belongs to the diffuse components.

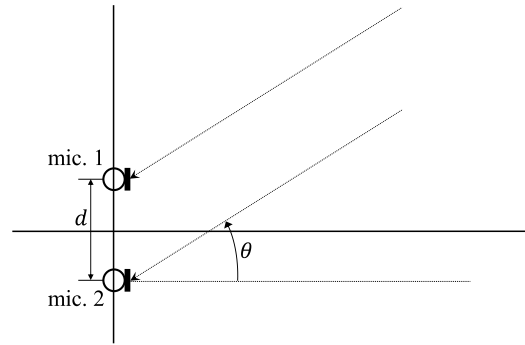


FIGURE 1. DOA estimation of a sound source using TDE for a pair of microphones.

The frame and frequency bin arguments are omitted for brevity.  $\Re$  and  $|\cdot|$  denote the real part and absolute values of a complex number, respectively.

Then, the contribution of diffuse components in the microphone signals on a scale of zero to one can be obtained by the diffuseness estimator defined as [45]

$$\tilde{D}(m, k) = \frac{1}{\widehat{\text{CDR}}(m, k) + 1}. \quad (8)$$

### III. PROPOSED SOUND SOURCE LOCALIZATION METHOD

In Fig. 1, the DOA of a sound source for a pair of microphones spaced by  $d$ , assuming that the distance from the source to the center of microphones is much larger than  $d$ , can be given by [1]

$$\theta \approx \arcsin\left(\frac{\tau_{\text{TDE}} \cdot c}{d}\right), \quad (9)$$

where  $\tau_{\text{TDE}}$  denotes the difference between the times taken by the sound from the source to reach the two microphones. Therefore, the source direction can be determined by TDE between signals acquired by the two microphones. The most intuitive and popular approach to obtain  $\tau_{\text{TDE}}$  is to find the time lag corresponding to the maximum of the GCC function of the two microphone signals: [1], [16], [18]

$$\tau_{\text{TDE}} = \frac{1}{f_s} \cdot \arg \max_t R_{12}(t), \quad (10)$$

where  $f_s$  and  $t$  are the sampling frequency and time sample index, respectively. The GCC function  $R_{12}(t)$  of the two signals can be efficiently computed by the inverse DFT of the cross-power spectral density function:

$$R_{12}(t) = \mathcal{F}^{-1}\{\Psi \odot \mathbf{X}_1 \odot \mathbf{X}_2^*\}, \quad (11)$$

where the vector  $\Psi$  represents the frequency weighting, and  $\mathbf{X}_i$  denotes a vector whose  $k$ -th element is  $X_i(m, k)$  with the omitted frame index.  $\odot$  and  $*$  represent the Hadamard product and the element-wise complex conjugate operation on the vector, respectively.

Among several weightings, the PHAT weight at frame  $m$  and frequency bin  $k$  is given by

$$\Psi(m, k) = \frac{1}{|X_1(m, k) X_2^*(m, k)|}. \quad (12)$$

The weighting normalizes the magnitudes to provide equal weights for all frequency bins to form sharp peaks. Therefore, the GCC-PHAT may provide the TDE robust against reverberation, but it is known to be sensitive to ambient noise as the normalization emphasizes frequency components with small powers.

As mentioned above, direct sound from a source is helpful for sound source localization, but components caused by diffuse noise or reverberation interferes with the localization. The direct sound and other components caused by diffuse noise or reverberation may be assumed to be fully coherent and diffuse, respectively. Because the diffuseness  $\tilde{D}(m, k)$  represents the contribution of diffuse components in microphone signals on the scale of zero to one, it can be used to select t-f components of the observed signals directly emitted by the source that are useful to achieve a TDE robust to diffuse components and to further improve the robustness of the GCC-PHAT against reverberation. Especially, in order to choose highly reliable components containing direct sound dominantly for accurate TDE in noisy and reverberant environments, the mask is binarized with a very rigorous threshold as

$$M(m, k) = \begin{cases} 0 & \text{if } \tilde{D}(m, k) > \delta_{\tilde{D}}, \\ 1 & \text{otherwise,} \end{cases} \quad (13)$$

where  $\delta_{\tilde{D}}$  denotes the threshold.<sup>2</sup> The GCC-PHAT on the masked observations estimates the DOA  $\theta$  by (9) after the mask is applied in the STFT domain by replacing (11) with

$$R_{12}(t) = \mathcal{F}^{-1}\{\Psi \odot \mathbf{M} \odot \mathbf{X}_1 \odot \mathbf{X}_2^*\}, \quad (14)$$

where  $\mathbf{M}$  denotes a vector whose  $k$ -th element is  $M(m, k)$  with the omitted frame index.

Furthermore, the time resolution of cross-correlation-based methods including the GCC-PHAT is limited by the sampling interval. To obtain an accurate DOA estimation at a low sampling frequency for two microphones in close proximity, the time resolution at a subsampling level should be investigated. It can be performed by interpolating the GCC function and determining its maximum. The interpolation of the GCC function can be efficiently accomplished by padding zeros to the weighted cross-power spectral density function in (11).

In summary, the overall procedure of the proposed sound source localization method is as follows:

- Begin
  - Step 1 Make a new frame of input data;
  - Step 2 Transform the frame into the frequency domain;
  - Step 3 Compute the DOA-independent CDR estimate by using (6) with (2), (5), and (7);
  - Step 4 Compute the diffuseness estimate by using (8);
  - Step 5 Compute the GCC function by using (14) with (12) and (13);

<sup>2</sup>The threshold is optimized empirically in pilot experiments.

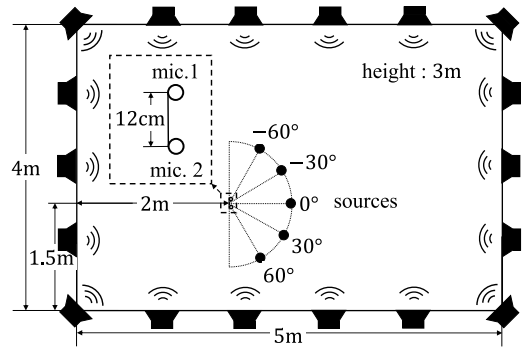


FIGURE 2. Source and microphone positions for experiments on simulated data.

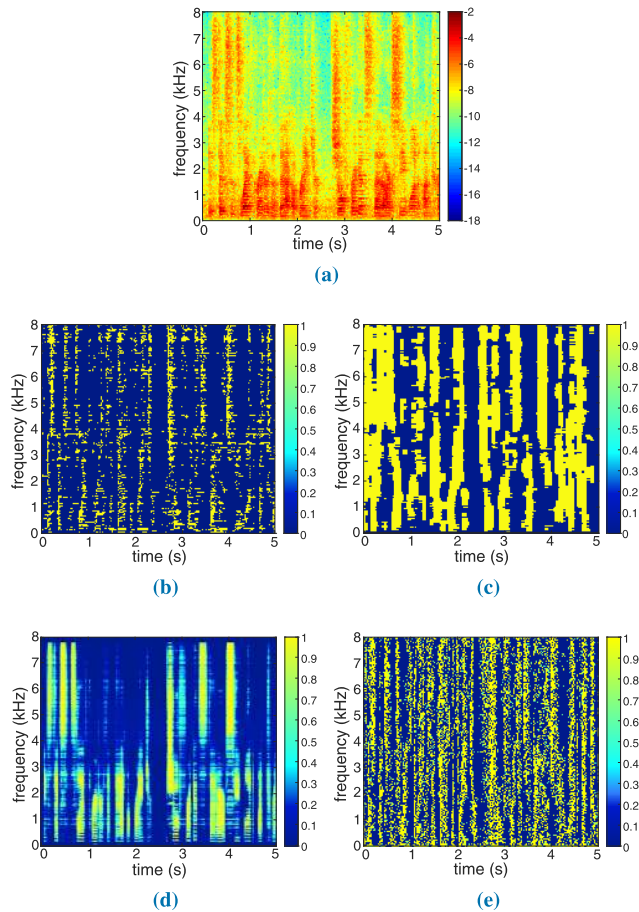
- Step 6 Estimate a localization angle by using (9) with (10);
- Step 7 Go to Step 1.

• End

#### IV. EXPERIMENTAL RESULTS

In order to evaluate the performance of the proposed sound source localization method in noisy and reverberant environments, we simulated signals observed at two 12-cm-apart microphones<sup>3</sup> from a source in a 5 m × 4 m × 3 m rectangular room. An observed signal was obtained by convolving the source signal with an impulse response that simulates the acoustics from the source to a microphone [48] and by adding diffuse noise. Fig. 2 describes configurations to generate observations. A sound source was placed in one of five different angles at a distance of 1 m from the center of the two microphones. The common height of the source and microphones was 1 m. The reflection coefficients were chosen to provide the reverberation times  $RT_{60s}$  of every 0.2 s from 0.2 s to 0.6 s. The source signal was composed of concatenated sentences uttered by a speaker from the TIMIT database [49]. The diffuse noise was simulated by summing up signals convolved with the generated impulse responses from virtual speakers playing randomly selected sections of babble noise from NOISEX-92 [50] that were placed at 1-m-spaced locations along walls with random heights. In the convolving process, the source signal was upsampled to 1024 kHz, convolved with acoustic filters generated at a sampling rate of 1024 kHz, and downsampled back to 16 kHz because the original sampling of 16 kHz was too low to simulate signal delay at the two microphones standing nearby. The length of the signals was fixed as 15 s. Noise components for both the microphones were scaled by the same factor to give a designated SNR at “mic. 1”. As the distance between the two microphones was 12 cm, the maximum time delay between the microphones was 5.565 samples at the sampling

<sup>3</sup>For a 16-kHz sampling rate, an alias-free microphone spacing is about 2.1 cm that is too close to acquire sufficiently different signals from each other. In a practical situation, acquired signals usually contain noise. If the microphone spacing is too close, the noise can be an important factor in preventing accurate source localization.



**FIGURE 3.** Spectrograms of (a) an input signal with an SNR of 20 dB and an  $RT_{60}$  of 0.4 s, (b) its binary diffuseness mask estimated when  $\lambda = 0.8$  and  $\delta_{\bar{D}} = 0.2$ , (c) its transition noise mask by [28], (d) its DNN-based masks by [36], and (e) its coherence mask by [42].

rate of 16 kHz. In order to obtain a sufficient time resolution, we padded 32,256 zeros to 512 STFT coefficients such that the maximum and minimum angle resolutions were  $0.16^\circ$  and  $4.3^\circ$ ,<sup>4</sup> respectively.

Fig. 3 displays the spectrograms of an input signal with an SNR of 20 dB and an  $RT_{60}$  of 0.4 s and its binary diffuseness mask estimated when  $\lambda = 0.8$  and  $\delta_{\bar{D}} = 0.2$ . To compare the diffuseness mask of the proposed method with t-f masks with a range of values between 0 and 1 estimated by other methods, Fig. 3 also shows a transition noise mask by [28], a DNN-based mask by [36], and a coherence mask by [42]. The parameters for source localization in [36] were optimized or trained by 600 utterances uttered by five male and five female speakers (disjoint from speakers for evaluation) at five different angles same as in Fig. 2 for four input SNRs and three  $RT_{60}$ s. Although the masks were similar to the mask estimated by the proposed method in that they distinguished t-f components dominated by a target speech signal, it is noteworthy that the mask obtained by the proposed

<sup>4</sup>Without the zero-padding, the maximum and minimum angle resolutions were about  $10^\circ$  and  $35^\circ$  for each sample delay, respectively.

method successfully and rigorously selected t-f components corresponding to auditory onsets that were helpful for robust source localization.

The median value of localization angle estimates obtained for all frames in an utterance was used as the estimated angle for the utterance. Instead of the mean value, the median value was used to remove outliers of the angle estimates at frames where the target utterance was not dominant. Then, the localization performance was evaluated in terms of the mean absolute error (MAE) of estimated angles defined as

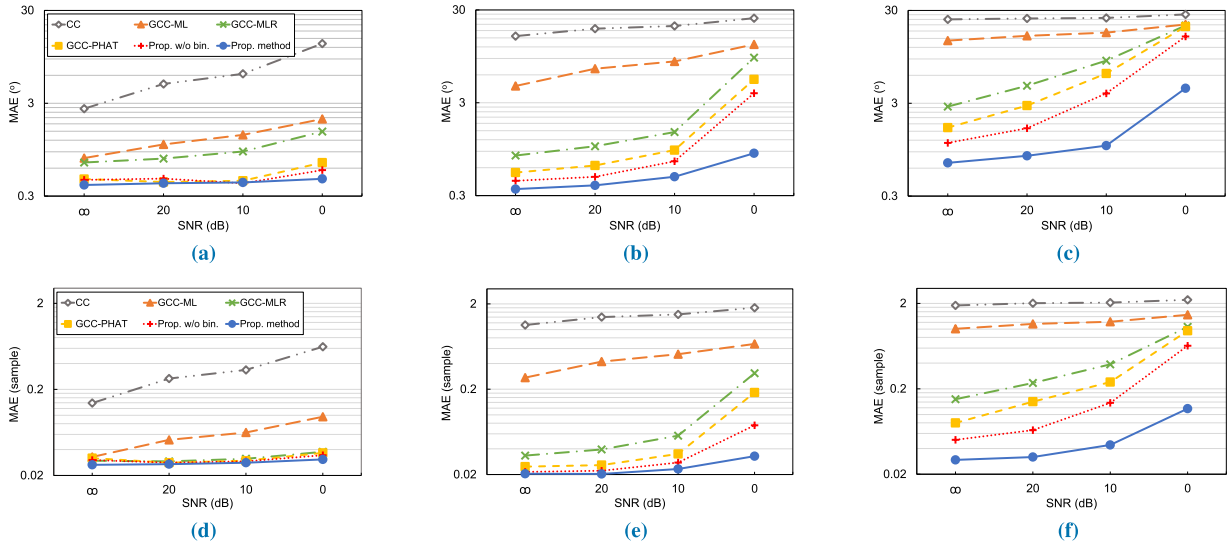
$$E_\theta = \frac{\sum_{u=1}^{N_u} |\theta_u^{\text{est}} - \theta_u^{\text{true}}|}{N_u}, \quad (15)$$

where  $\theta_u^{\text{est}}$  and  $\theta_u^{\text{true}}$  denote the estimated and true localization angles for the  $u$ -th utterance.  $N_u$  is the number of utterances, and we used 30 concatenated sentences uttered by three male and three female speakers at five different angles in this experiment. In addition, we also considered the MAE of estimated time delays to determine source directions because the conversion by (9) is not linear. The MAE of estimated time delays is defined as

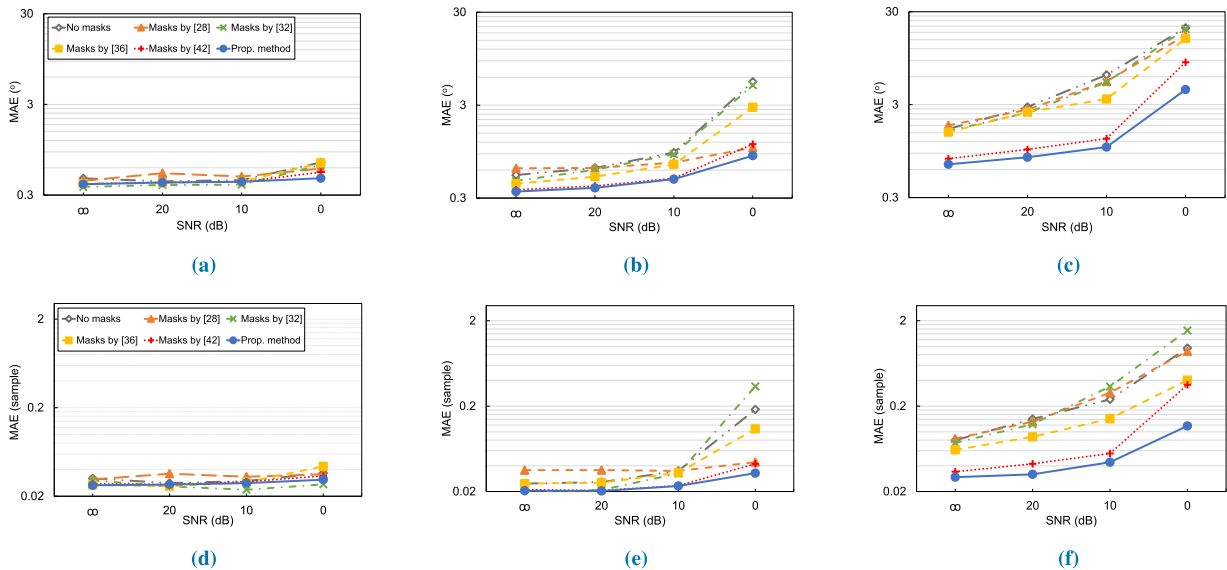
$$E_{\tau_{\text{TDE}}} = \frac{\sum_{u=1}^{N_u} |\tau_{\text{TDE}_u}^{\text{est}} - \tau_{\text{TDE}_u}^{\text{true}}|}{N_u}, \quad (16)$$

where  $\tau_{\text{TDE}_u}^{\text{est}}$  and  $\tau_{\text{TDE}_u}^{\text{true}}$  denote the median value of time delay estimates (with the zero-padding) obtained at all frames and the true time delay for the  $u$ -th utterance, respectively.

The MAEs of the proposed localization method are displayed in Fig. 4 for four different input SNRs and three different  $RT_{60}$ s. For comparison, we showed the results of the localization methods based on the conventional GCC function with uniform (CC), ML (GCC-ML), MLR (GCC-MLR), and PHAT (GCC-PHAT) weights. We further presented the results of the proposed method using a continuous diffuseness mask without binarization (Prop. w/o bin.). Regardless of the used methods, the MAEs increased in general as  $RT_{60}$  increased or the input SNR decreased. This is because an increase in  $RT_{60}$  or a decrease in the input SNR increased noisy or reverberant components interfering with the localization. Under all the tested cases, the proposed method considerably reduced the MAEs and consistently showed comparable or lower MAEs than the others. In particular, the proposed method provided comparable or better performance than the method using a diffuseness mask without binarization by choosing only t-f components highly reliable for accurate DOA estimation. In order to compare the proposed method with other methods based on t-f mask estimation, Fig. 5 displays the MAEs of the GCC-PHAT method with no applied masks (No masks), the transition noise masks by [28] (Masks by [28]), localization precision masks by [32] (Masks by [32]), DNN-based masks by [36] (Masks by [36]), coherence masks by [42] (Masks by [42]) and masks by the proposed method. The parameters for source localization in [32] were also optimized or trained by the same data as in [36] as mentioned above. Similar to Fig. 4, an increase in  $RT_{60}$  or a decrease in the input SNR generally increased the MAEs. The proposed



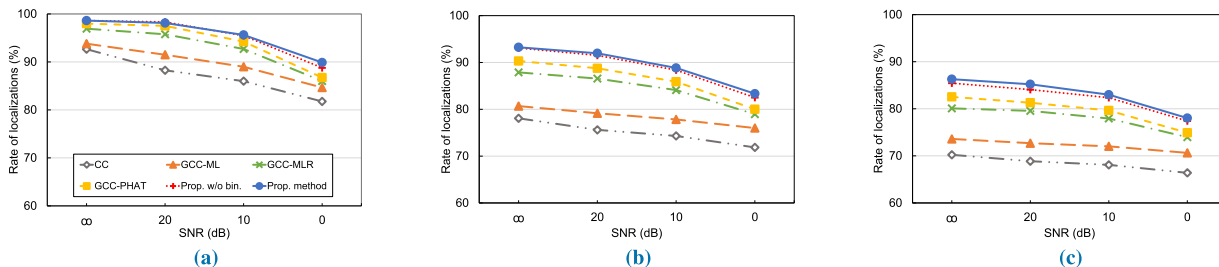
**FIGURE 4.** MAEs of estimated angles (in the upper row) and time delays (in the lower row) for the localization methods based on the conventional GCC function on 30 signals uttered by three male and three female speakers at five different azimuthal angles with  $RT_{60}$ s of 0.2 s (in the left column), 0.4 s (in the center column), and 0.6 s (in the right column). The infinite SNR means that no noise was added. MAEs of estimated angles on data at  $RT_{60}$ s of (a) 0.2 s, (b) 0.4 s, and (c) 0.6 s, and MAEs of estimated time delays on data at  $RT_{60}$ s of (d) 0.2 s, (e) 0.4 s, and (f) 0.6 s.



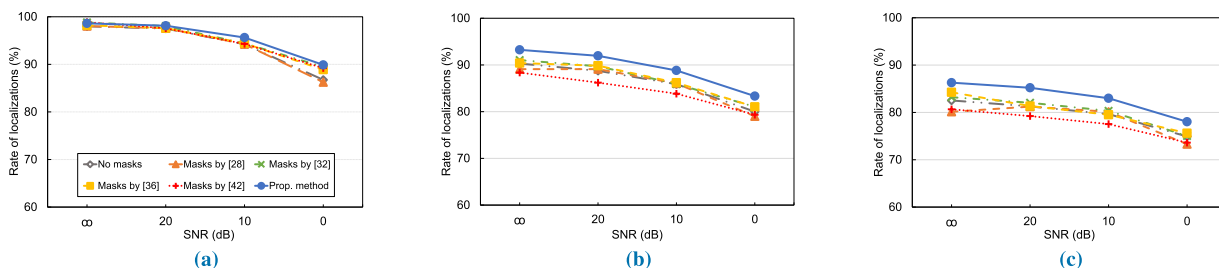
**FIGURE 5.** MAEs of estimated angles (in the upper row) and time delays (in the lower row) for the GCC-PHAT method with no masks, masks by [28], [32], [36], [42], and the proposed method on 30 signals uttered by three male and three female speakers at five different azimuthal angles with  $RT_{60}$ s of 0.2 s (in the left column), 0.4 s (in the center column), and 0.6 s (in the right column). The infinite SNR means that no noise was added. MAEs of estimated angles on data at  $RT_{60}$ s of (a) 0.2 s, (b) 0.4 s, and (c) 0.6 s, and MAEs of estimated time delays on data at  $RT_{60}$ s of (d) 0.2 s, (e) 0.4 s, and (f) 0.6 s.

method provided comparable or better performance than the others including the learning-based methods of [32] and [36]. Although the learning-based methods might achieve better performance with more various training data, it is worth noting that the proposed method does not require a learning process with training data in advance. Moreover, the results demonstrated that the proposed method successfully selected t-f components that were helpful for sound source localization and the localization using the selected t-f components achieved robustness against noise and reverberation.

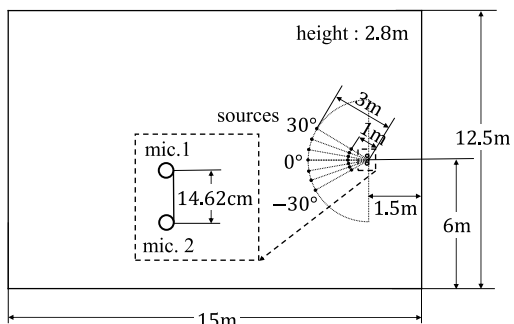
To evaluate the probability of successful localization estimates, Figs. 6 and 7 show the rates of localizations averaged over the same 30 concatenated sentences as above. The localization rate is defined as the ratio of the number of frames providing time delay estimates corresponding to successful localization, to the number of all frames, where errors of the time delay estimates (with the zero-padding) were less than or equal to three samples. Regardless of the used methods, the rates of localizations decreased as  $RT_{60}$  increased or the input SNR decreased because localization was disturbed by increased noisy or reverberant components.



**FIGURE 6.** Rates of localizations for the localization methods based on the conventional GCC function averaged over 30 signals uttered by three male and three female speakers at five different azimuthal angles with  $RT_{60}$ s of (a) 0.2 s, (b) 0.4 s, and (c) 0.6 s. The infinite SNR means that no noise was added.



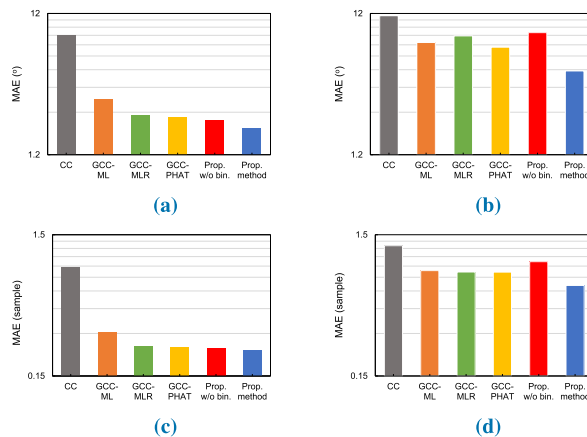
**FIGURE 7.** Rates of localizations for the GCC-PHAT method with no masks, masks by [28], [32], [36], [42], and the proposed method averaged over 30 signals uttered by three male and three female speakers at five different azimuthal angles with  $RT_{60}$ s of (a) 0.2 s, (b) 0.4 s, and (c) 0.6 s. The infinite SNR means that no noise was added.



**FIGURE 8.** Source and microphone positions for experiments on real-recorded data.

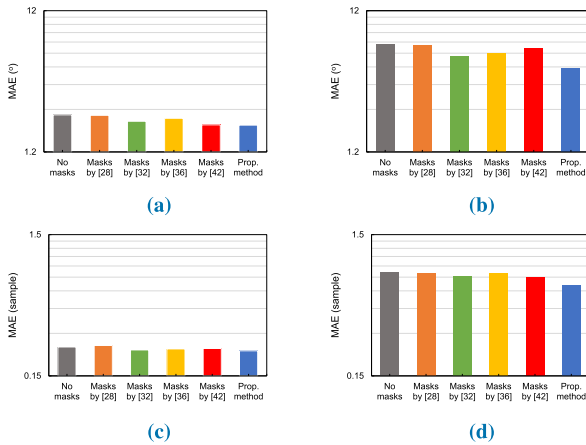
In particular, the proposed method showed comparable or better performance than the others, which demonstrated that the proposed method provided frame-wise localization estimates with a higher probability.

To conduct experiments for real-recorded data, we used four utterances uttered by two male and two female speakers from the TIMIT database [49]. As shown in Fig. 8, 2-s-long data (in the beginning part of each utterance) captured with two microphones at a sampling frequency of 16 kHz in a hall were considered for performing localization. A sound source placed at a distance of 1 m or 3 m from the center of the two microphones at an angle among azimuthal angles of every  $10^\circ$  from  $-30^\circ$  and  $30^\circ$ . The heights of the source and microphones were 1.4 m and 1.55 m, respectively. Figs. 9 and 10 show the MAEs on 28 signals uttered by two male and two female speakers at seven different angles for the proposed and other localization methods. In this experiment,

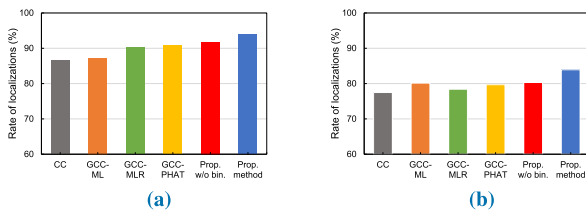


**FIGURE 9.** MAEs of estimated angles (in the upper row) and time delays (in the lower row) for the localization methods based on the conventional GCC function on 28 real-recorded signals uttered by two male and two female speakers at distances of 1 m (in the left column) and 3 m (in the right column) from the center of the two microphones at seven different azimuthal angles in a hall. MAEs of estimated angles on data at distances of (a) 1 m and (b) 3 m, and MAEs of estimated time delays on data at distances of (c) 1 m and (d) 3 m.

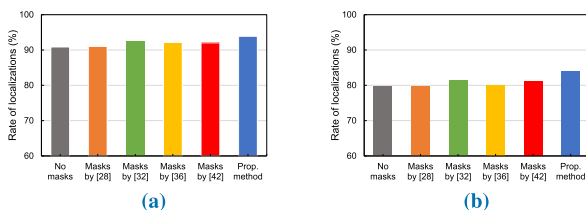
the parameters for [32] were optimized by 84 signals uttered by three male and three female speakers (disjoint from speakers for evaluation) at seven angles same as in Fig. 8 for two distances, and the parameters used in the previous experiment for [36] were finely tuned by the same data. Regardless of the used methods, the MAEs increased as the distance between the source and microphones increased because direct sound from the source that was helpful for localization became relatively diminished. Similar to the experiments on simu-



**FIGURE 10.** MAEs of estimated angles (in the upper row) and time delays (in the lower row) for the GCC-PHAT method with no masks, masks by [28], [32], [36], [42], and the proposed method on 28 real-recorded signals uttered by two male and two female speakers at distances of 1 m (in the left column) and 3 m (in the right column) from the center of the two microphones at seven different azimuthal angles in a hall. MAEs of estimated angles on data at distances of (a) 1 m and (b) 3 m, and MAEs of estimated time delays on data at distances of (c) 1 m and (d) 3 m.



**FIGURE 11.** Rates of localizations for the localization methods based on the conventional GCC function averaged over 28 real-recorded signals uttered by two male and two female speakers at distances of (a) 1 m and (b) 3 m from the center of the two microphones at seven different azimuthal angles in a hall.



**FIGURE 12.** Rates of localizations for the GCC-PHAT method with no masks, masks by [28], [32], [36], [42], and the proposed method averaged over 28 real-recorded signals uttered by two male and two female speakers at distances of (a) 1 m and (b) 3 m from the center of the two microphones at seven different azimuthal angles in a hall.

lated data, Figs. 11 and 12 show averaged rates of localizations. Although the rates of localizations decreased as the distance increased, the proposed method provided frame-wise localization estimates with a higher probability than the others. Above all, the proposed method consistently provided comparable or more accurate DOA estimates than the others, which indicated that the proposed method accomplished successful sound source localization even for the real-recorded data in a hall.

**V. CONCLUSION**

In this paper, we presented a robust sound source localization method based on GCC-PHAT in noisy and reverberant environments. To estimate the DOA robust against diffuse noise and reverberation, t-f components of observations directly emitted by a source were selected by the diffuseness that was computed from the CDR. In particular, the “inversed” diffuseness was binarized with a very rigorous threshold to choose highly reliable components for accurate DOA estimation even in noisy and reverberant environments. The experimental results for both simulated and real-recorded data consistently demonstrated the robustness of the presented method against diffuse noise and reverberation.

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