

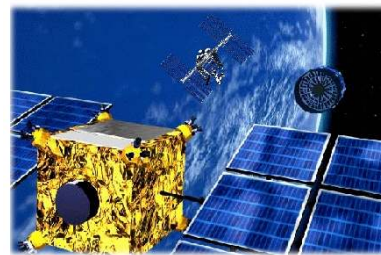
SQUID-based Readout Schemes for Microcalorimeter Arrays

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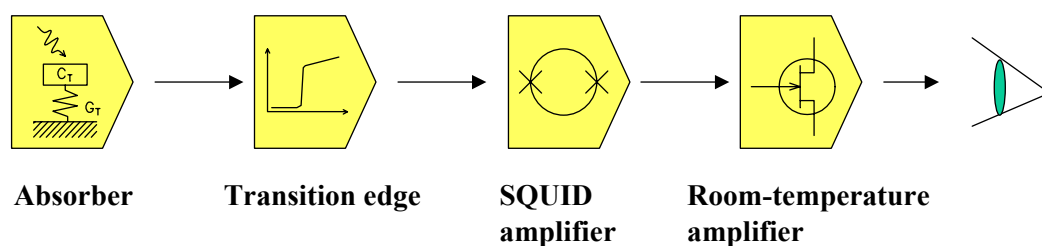
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Motivated by the XEUS mission by the ESA



Single-pixel signal path

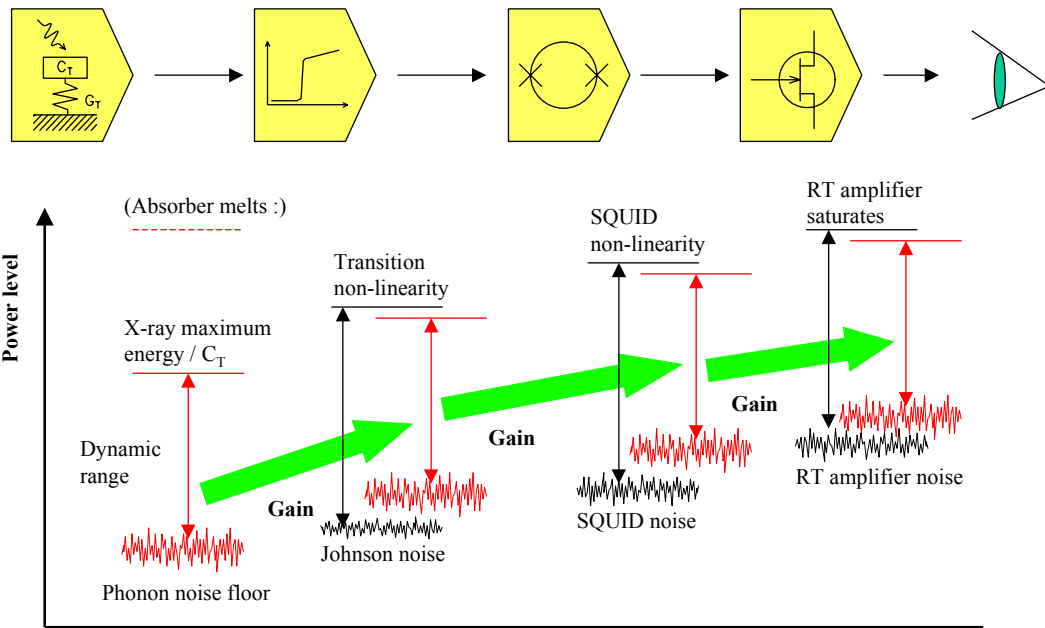


Non-feedback bare parameters:

Power gain	$\frac{1}{2}\alpha\left(1-\frac{T_{bath}}{T}\right)$	$(8\pi\omega^2 L_{SQ} C_j)^{-1}$	Can be very large
Bandwidth	$\frac{G_T}{C_T}$	Input coil resonance	Can be up to GHz's or more
Dynamic range	$\frac{\Delta T}{T} \sqrt{\frac{G_T}{4k_B}}$	$\frac{\Phi_0}{9.8 L_{SQ}^{3/4} C_j^{1/4} \sqrt{k_B T}}$	$\sim 10^9$ with standard analog circuits

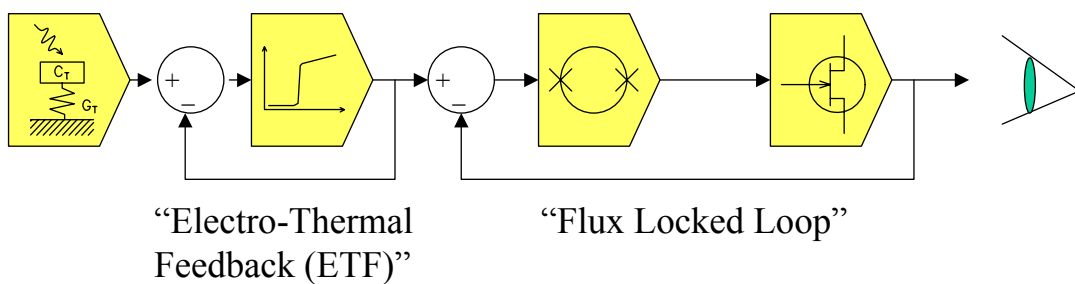
Use negative feedback to trade gain for bandwidth & dyn range
 Use positive feedback to trade BW & dyn range for gain

The designer's job

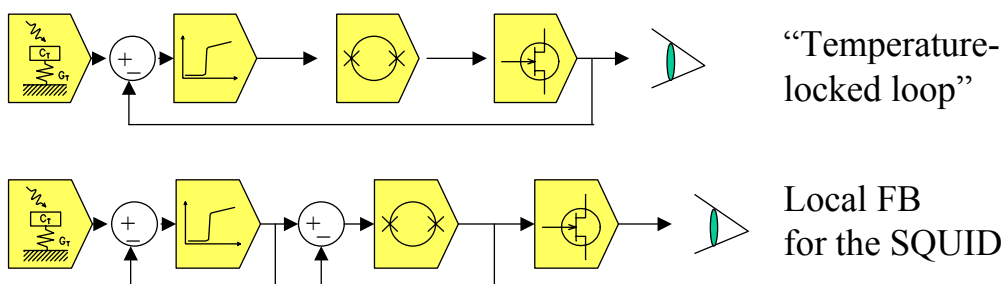


- Take care of the bandwidths, too.
- FB modifies input & output impedances (noise matching)

Standard arrangement for the feedback paths ...



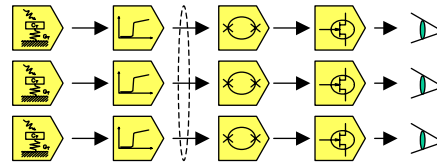
... but there's a number of other possibilities, eg. :



What if we have a large number of pixels?

Direct readout:

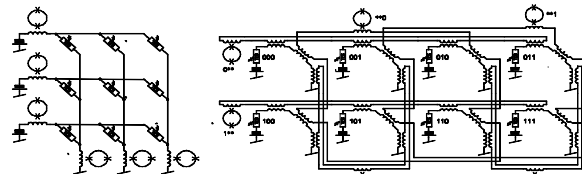
- Feasible (compare: MEG devices)
- Heat leak through the wires
- Complex and fragile



Wiring to 20 mK stage
(2.8 μ Wh cooling capacity [XEUS])

Correlation-based schemes:

- Noises are summed - *bad*
- Acceptable only when SNR can tolerate summation

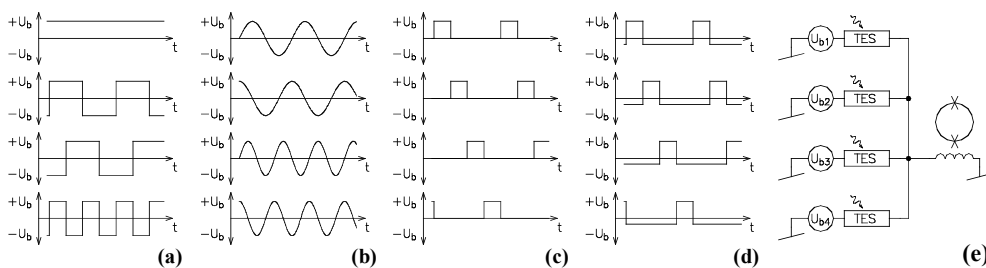


2D-array: 3 x 3 pixels

3D-array: 2 x 2 x 2 pixels

Multiplexing:

- Fingerprint signals by multiplying by an orthogonal set of functions $f_1(t), f_2(t) \dots$ (*sines & cosines; Hadamard functions; wavelets ...*)
- Sum to a single wire
- Detect the signals by multiplying with the same set $f_1(t), f_2(t) \dots$ and integrate over all times
- Multiplier: (i) TES, (ii) SQUID, (iii) some extra device

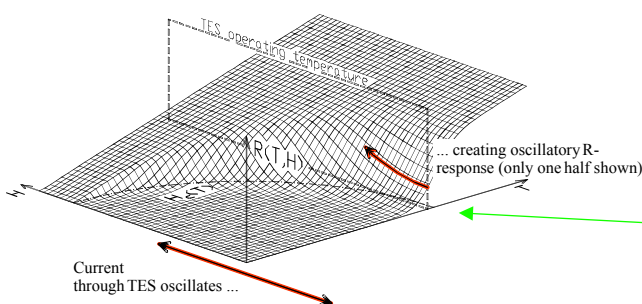


Hadamard codes
(Karasik & McGrath)

Sines & cosines
"frequency MUX"

Timeslot functions
"time domain MUX"

Modified timeslot
functions for enhanced
duty cycle (4ch versions
are symmetrically bipolar)

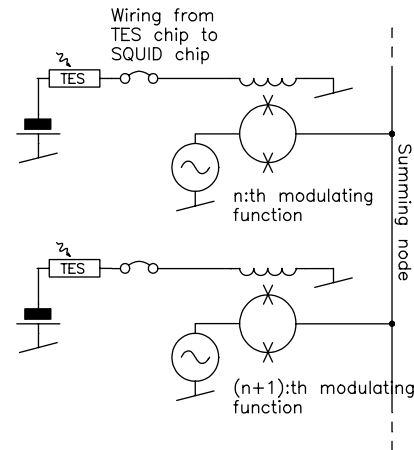


TESes as modulators

- $I(t) = G(t) \times U_b(t)$
- Conductance G carries the signal
- Bias voltage carries the modulating function
- No direct thermal response: average RMS heating
- Magnetic nonlinearity?
- Only N wires from TES chip to SQUID chip for $N \times M$ pixels
- Only N SQUIDS

SQUID as modulator

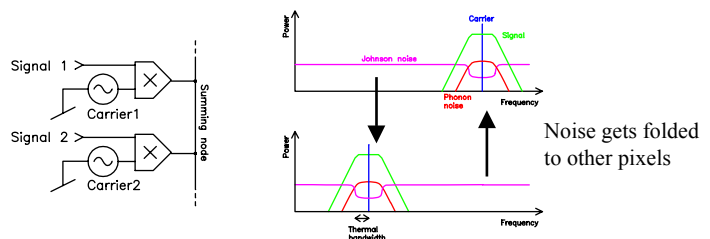
- Signal is multiplied by SQUID response function $I = MI_{TES} \times \partial I / \partial \Phi$.
- $\partial I / \partial \Phi$ is a non-linear function of U_b
- Works best with two-level mod-functions
- $m \times n$ wires from TES chip to SQUID chip, if cannot be integrated monolithically



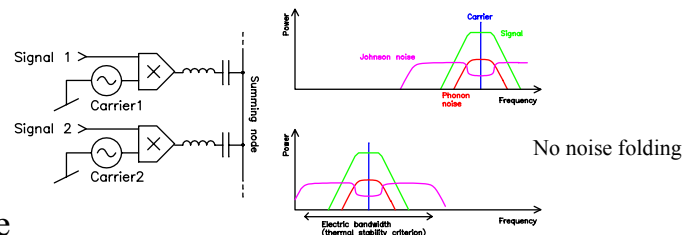
Noise folding

- Wideband noise is added after the modulator
- The noise from a given pixel aliases into *frequency bands / timeslots / codes* of other pixels
- **(i)** Provide gain so that noise summing can be tolerated.
- **(ii)** Use *frequency-preferring / timeslot-preferring / code-preferring* noise blocker.
- In case of freq. MUX, the blocker is just an LC resonator
- With other MUX schemes, active elements and external clock signal feeds are needed

Without noise blockers

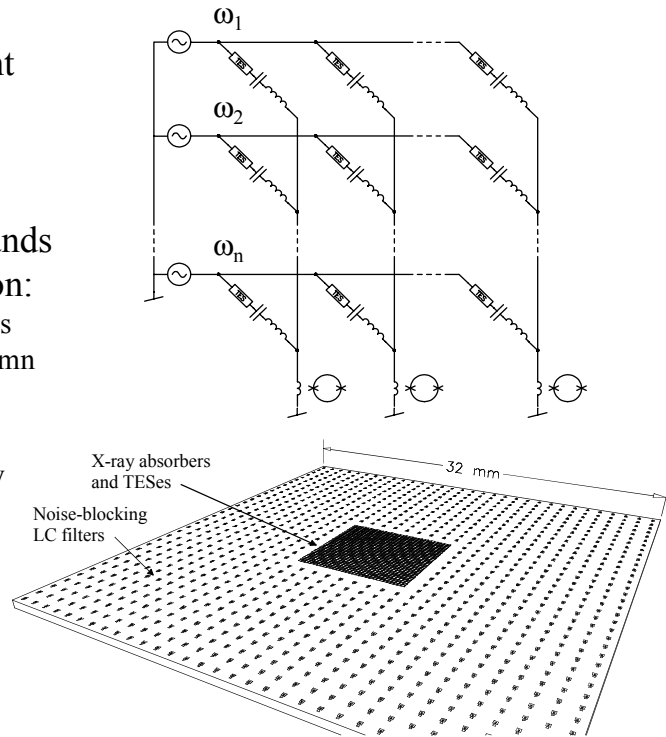


With noise blockers

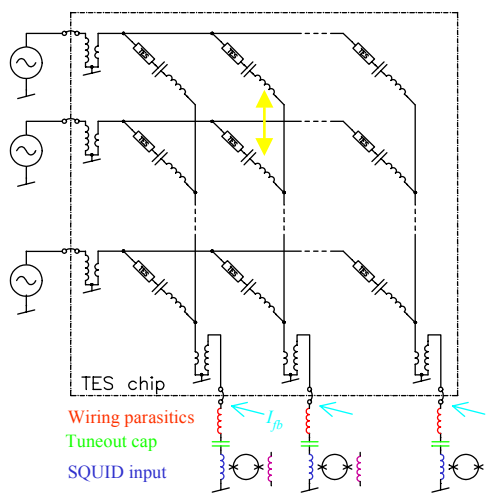


Filter implementation

- L is set by stability requirement
- 80 nH fits in $\sim 0.2 \times 0.2$ mm
- C implementability sets lower limit to $f \sim 25$ MHz
- Magnetic cross-coupling demands ~ 1 mm filter-to-filter separation:
 - (i) crosstalk between different columns
 - (ii) limits total BW available to a column
- Band separation
 - Only to avoid noise folding
 - Channel confusion: taken care by post-detection filters



Common inductance in a column

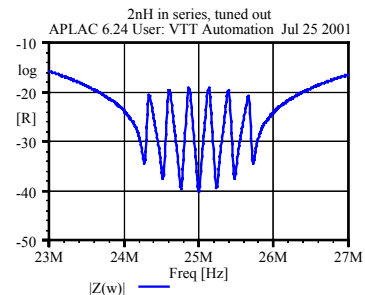
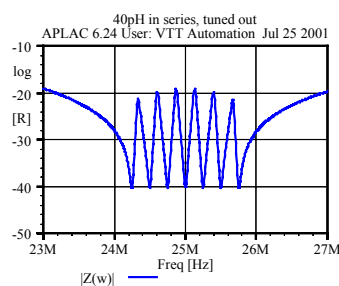
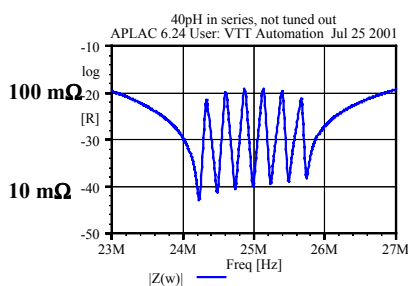


- Magnetic cross-coupling (example) appears as common series inductance, like L_p
- Parasitic inductance L_p in wiring: reactive part tuned out with C_c , L_p limits the bandwidth.
- Transformers ramp up the impedance level, to help with parasitic L
- SQUID input inductance L_{in} can be screened away with negative feedback
- Feedback by flux injection or current injection

Quantum-limited bandwidth:

$$\epsilon = \frac{1}{2} L_{in} I_n^2 = \frac{R I_n^2}{4\pi \Delta f}$$

XEUS: $R = 10$ m Ω
 24 hbar for 32 chans separated by 200 kHz



Dynamic range

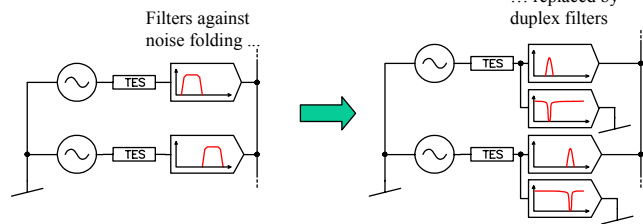
TES current:	$\frac{I_{pp}}{I_n} = \frac{2\sqrt{2} \times 2.36 \times E_{\max}}{\Delta E_{FWHM} \sqrt{\tau_i}}$	$\sim 5 \times 10^6$ for XEUS
SQUID: Limited by self-noise	$\frac{\Phi_0/2}{\Phi_n} = \frac{\Phi_0}{9.8 L_{SQ}^{3/4} C_j^{1/4} \sqrt{k_B T}}$	$\sim 2.4 \times 10^7$ for $T = 1$ K, $C_j = 0.5$ pF, $L_{SQ} = 4$ pH ($\epsilon \sim 2.2$ hbar)
SQUID: Limited by cable noise & RT amplifier	$\frac{\Phi_0/2}{\Phi_n} = \frac{\Phi_0}{5.3 L_{SQ}^{3/4} C_j^{1/4} \sqrt{k_B T_n}}$	$\sim 8 \times 10^6$, when $T_n = 10$ K + 20 K (for 30MHz RT amp + cables)

Need some more dynamic range for linearity ?

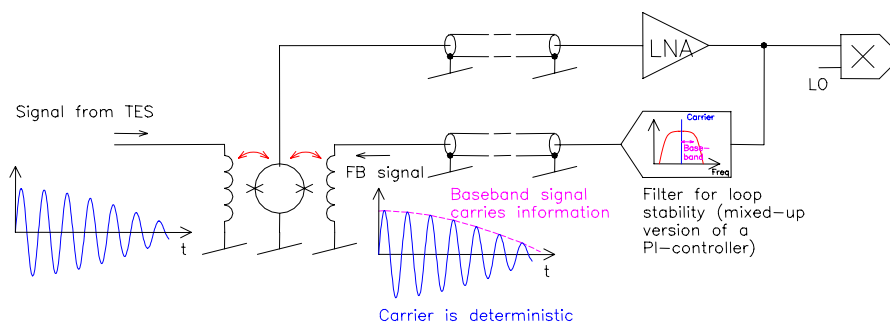
- Harmonic production by an event ? (No, falls above the signal band)
- Mixing between an event & imperfect idle current balancing ? (Probably not)
- Mixing between two coincident events ? (Not likely if pixels are scattered)
- Gain stability ? (Probably yes)

Dynamic range - how to improve ?

- Alleviate DR requirement?
Increase integration time (= filter settling time), still retaining thermal stability condition.



- Array SQUID for \sqrt{n} -fold DR improvement?
- Long negative feedback at carrier freq. through RT not feasible, but...
 - ... (i) FB through low-dissipation MOS amplifier at 20 K?
 - ... (ii) FB through RT at baseband rather than carrier frequency?



Total system: a scenario

