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# Sulfur poisoning recovery on a SOFC anode material through reversible segregation of nickel

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## Abstract

The perovskite-type mixed oxide  $\text{La}_{0.3}\text{Sr}_{0.55}\text{Ti}_{0.95}\text{Ni}_{0.05}\text{O}_{3-\delta}$  (LSTN) is demonstrated to exhibit the remarkable property of structural regeneration, where Ni can be reversibly exsolved from the host perovskite lattice resulting in a regenerable Ni catalyst for solid oxide fuel cell anode applications. Results of catalytic tests for the water gas shift reaction and electrochemical investigations on a button sized fuel cell demonstrate the redox stability of LSTN, its potential application in solid oxide fuel cells and its ability to recover catalytic activity completely after sulfur poisoning. Nickel segregation was characterized and quantified on powder samples by means of electron microscopy, X-ray diffraction, X-ray absorption spectroscopy as well as temperature programmed reduction – reoxidation cycles. Catalyst stability was much improved compared to impregnated  $\text{Ni}/\text{La}_{0.3}\text{Sr}_{0.55}\text{TiO}_{3-\delta}$  and  $\text{Ni}/\text{Y}_{0.08}\text{Zr}_{0.92}\text{O}_2$  anode materials. A full cell was tested under both open circuit voltage and polarized conditions showing a stable cell voltage over redox cycles as well as periods of reverse potential and current overload. The area specific resistance of the anode layer was as low as  $0.58 \Omega\text{cm}^2$  at  $850^\circ\text{C}$ . This allows LSTN to be applied in redox stable solid oxide fuel cell anodes and reversible segregation of Ni to be exploited for fast recovery from sulfur poisoning.

## Introduction

Modern society relies on the development of highly efficient and stable power sources ideally capable of using variable fuel sources to meet the ever increasing electricity demand.<sup>1-2</sup> Solid oxide fuel cells (SOFC) offer exceptionally high efficiency for chemical to electric power conversion with high fuel flexibility.<sup>3-5</sup> Unlike other types of fuel cells their high operating temperatures allow for hydrocarbon fuels from various sources to be directly used via internal reforming reactions<sup>6-7</sup> producing hydrogen and carbon monoxide mixture fuels. This is a major advantage over polymer electrolyte fuel cells (PEM), which rely on highly pure hydrogen as fuel gas.<sup>8</sup> Internal reforming occurs at the SOFC anode, Ni metal catalyzes this reaction as well as the important hydrogen oxidation reaction ( $\text{H}_2 + \frac{1}{2}\text{O}_2 \rightarrow \text{H}_2\text{O}$ , HOR) and the water gas shift reaction ( $\text{CO} + \text{H}_2\text{O} \rightarrow \text{CO}_2 + \text{H}_2$ , WGS), which produces additional  $\text{H}_2$  fuel from residual steam originating from reforming or water generated through HOR.<sup>9</sup> Besides catalytic activity, the anode material has to provide also both, high ionic and electronic conductivity for the electrochemical oxidation of the fuel gas and for current collection, respectively. For a long time Ni/ $\text{Y}_{0.08}\text{Zr}_{0.92}\text{O}_2$  (Ni/YSZ) cermets have been the state-of-the-art anode material offering both high catalytic activity (due to addition of a considerable amount of Ni, ca. 50 wt%) as well as good conductivity for both electrons and oxygen anions provided by the percolating Ni and YSZ phases, respectively.<sup>10-12</sup> However, their poor redox stability is regarded as a major disadvantage besides their susceptibility to poisoning by sulfur.<sup>13-14</sup> Sulfur contaminants are commonly present in fuel gas as they are used as odorants for natural gas or may be present in large quantities in biogenic fuels. At low concentrations sulfur species are known to strongly adsorb on the Ni surface thus deactivating the metal catalyst.<sup>15-18</sup> High sulfur concentrations may induce the formation of sulfur compounds (e.g. NiS,  $\text{Ni}_3\text{S}_2$  and  $\text{Ni}_7\text{S}_6$ ) that permanently degrade Ni containing SOFC anodes not only with respect to catalytic activity for hydrogen oxidation but especially for WGS.<sup>17-18</sup> Sulfur was also

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5 observed to promote the migration of Ni, thus decreasing the degree of Ni percolation within the anode  
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7 and reducing electronic conductivity.<sup>19</sup>  
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9 For these reasons much attention is currently drawn to the development of novel SOFC anode materials  
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11 capable to offer the required electrochemical performance and stability in sulfur containing feeds.  
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13 Other beneficial properties such as redox stability could be potentially exploited as it would allow  
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15 operating the cell in electrolysis mode but also regenerating a deactivated anode from sulfur poisoning  
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17 and/or coke deposits, which may have formed during internal reforming of hydrocarbons. Reduction of  
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19 overall Ni content is essential to achieve redox stability. Besides the coarsening of the Ni phase, the  
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21 oxidation of Ni and consequential volume expansion of the Ni phase may lead to electrode or  
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23 electrolyte cracking.<sup>13-14, 20-22</sup> Perovskite-type oxides ( $ABO_3$ ) are regarded as good candidates to replace  
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25 high Ni content anode cermets with the aim of increasing anode durability.<sup>23-25</sup> Their inherent structural  
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27 stability allows for a large number of elements to be incorporated at various stoichiometries within  
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29 their lattice and thus ultimately for the tailoring of both electronic and ionic conductivities besides  
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31 catalytic properties. Among others, lanthanum doped strontium titanates have attracted attention since  
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33 they are temperature and redox stable and offer the necessary conductivities required for SOFC  
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35 electrode applications.<sup>23</sup> Nickel can still be added for its catalytic activity and is deposited on the  
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37 perovskite backbone in the form of nanoparticles usually by impregnation.<sup>25-27</sup>  
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41 In more recent years direct Ni exsolution from the perovskite lattice through selective reduction has  
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43 been shown to produce particles with enhanced sintering and coking resistance.<sup>28-32</sup> Exsolution from  
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45 perovskite-type mixed oxides is achieved by partially substituting the B-site elements of a redox stable  
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47 perovskite host lattice by Ni and subjecting these materials to a reductive environment. This causes the  
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49 dispersed Ni within the perovskite to reduce and segregate forming well dispersed particles on the  
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51 perovskite surface, while the rest of the perovskite remains intact and structurally stable. Segregated Ni  
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53 particles show much higher particle-support interactions compared to Ni particles deposited through  
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5 conventional support impregnation methods, as they remain partially embedded in the surface of the  
6 perovskite material, which pins them in place.<sup>28</sup> Some perovskite-type oxides have also been shown to  
7 exhibit the remarkable property of structural self-regeneration, i.e. the reversible reincorporation of  
8 such particles into the perovskite lattice. This capability was shown to depend on both composition of  
9 the host perovskite as well as on the regeneration conditions (i.e. oxygen partial pressure and  
10 temperature) and has been demonstrated for a variety of Pt group metals for exhaust gas after treatment  
11 catalysts and recently for Fe and Co.<sup>33-37</sup> Ni has also been shown to segregate and reincorporate  
12 reversibly during simple redox cycles from  $\text{LaFe}_{1-x}\text{Ni}_x\text{O}_{3\pm\delta}$  perovskite-type oxides<sup>38-39</sup> and more  
13 recently  $\text{La}_{0.7}\text{Sr}_{0.3}\text{Cr}_{1-x}\text{Ni}_x\text{O}_{3-\delta}$ .<sup>40</sup> Exploitation of this effect produced highly redox stable catalysts,  
14 enabling the preservation of metal particle size and thus activity over repeated redox cycles.

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26 The objective of this work was to demonstrate that, if a material with such a property was applied as a  
27 SOFC anode, anode reoxidation at high temperatures could be utilized to remove poisoning (such as  
28  $\text{H}_2\text{S}$ ) from its surface through simple reoxidation as well as allowing the cell to be operated in  
29 electrolysis mode. We demonstrate that  $\text{La}_{0.3}\text{Sr}_{0.55}\text{Ti}_{0.95}\text{Ni}_{0.05}\text{O}_{3-\delta}$  exhibits all the properties required for  
30 operation as SOFC anode and verify the advantage of structural self-regeneration. This property can  
31 indeed be exploited on this perovskite-type host to restore the catalytic activity of Ni towards the water  
32 gas shift reaction after sulfur poisoning and to produce redox stable SOFCs.

## Experimental details

Mixed metal oxides with nominal composition  $\text{La}_{0.3}\text{Sr}_{0.55}\text{TiO}_{3-\delta}$  (LST) and  $\text{La}_{0.3}\text{Sr}_{0.55}\text{Ti}_{0.95}\text{Ni}_{0.05}\text{O}_{3-\delta}$  (LSTN) were synthesized using a citrate-gel method described including a final calcination step at  $960^\circ\text{C}$  for 6 h.<sup>30</sup> After calcination the powders are referred to as “calcined”. Nickel impregnated LST (Ni/LST) was prepared by wet impregnation of the as calcined LST perovskite with an aqueous solution of  $\text{Ni}(\text{NO}_3)_2 \cdot 6\text{H}_2\text{O}$  (pro analysis, Merck). Drying at  $90^\circ\text{C}$  overnight was followed by calcination in air at  $500^\circ\text{C}$  for 2 h. Furthermore,  $\text{Y}_{0.08}\text{Zr}_{0.92}\text{O}_2$  was impregnated with an aqueous solution of  $\text{Ni}(\text{NO}_3)_2 \cdot 6\text{H}_2\text{O}$  according to the same procedure to obtain 60 wt% NiO/YSZ (calculated 50 vol% Ni/YSZ) representing a standard solid oxide fuel cell anode material. In order to characterize the redox stability and the catalytic activity towards the water gas shift (WGS) reaction of these materials, aliquots of the powders received reductive and oxidative pretreatments or combinations thereof. If not otherwise stated all pretreatments were conducted at  $800^\circ\text{C}$ . Reduction was carried out in 10 vol%  $\text{H}_2/\text{Ar}$ , whereas oxidation was conducted in synthetic air (20 vol%  $\text{O}_2/\text{N}_2$ ) in a tubular quartz reactor.

The specific surface area (SSA) of the calcined powders was calculated from  $\text{N}_2$ -adsorption isotherms at  $-196^\circ\text{C}$  according to the Brunauer-Emmet-Teller (BET) model. Adsorption data was acquired using a Quantachrome Autosorb I instrument. Prior to SSA determination the samples were treated under vacuum at  $300^\circ\text{C}$  for 2 h.

The phase composition and crystal structure of calcined, reduced (10 vol%  $\text{H}_2$ ,  $800^\circ\text{C}$ , 15 h) and reoxidised powders (20 vol%  $\text{O}_2$ ,  $800^\circ\text{C}$ , 2 h) were analyzed by ex situ powder X-ray diffraction (XRD) using a Bruker D8 Advance diffractometer equipped with Ni-filtered Cu radiation, variable slits and an energy sensitive line detector (LynxEye). Diffractograms were collected between  $15^\circ$ - $80^\circ$   $2\theta$  with an acquisition time of 4 s and a step size of  $\Delta 2\theta = 0.03^\circ$ .



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5 Temperature programmed reduction (TPR) experiments were conducted using a bench top TPDRO-  
6 1100 (ThermoElectron) instrument equipped with mass flow controllers and a thermal conductivity  
7 detector. The samples (100 mg) were loaded into the quartz reactor tube and heated to 500°C under  
8 constant flow of 20 vol% O<sub>2</sub> before cooling to room temperature. TPRs were recorded in 10 vol%  
9 H<sub>2</sub>/Ar (20 mLmin<sup>-1</sup> at STP) and at a heating rate of 5°Cmin<sup>-1</sup>. The reoxidation temperature at which Ni  
10 is reversibly reincorporated into the perovskite lattice was estimated by TPR redox experiments. A  
11 TPR profile was recorded on the calcined sample up to 800°C followed by isothermal reduction for 1 h  
12 at the same temperature. The sample was then cooled in Ar to room temperature (25°C) before  
13 reoxidation at 700°C in 20 vol% O<sub>2</sub>/N<sub>2</sub> for 2 h. The sample was again cooled in Ar to 25°C before  
14 starting the second TPR on the now reoxidised material. Such TPR-reduction-reoxidation-TPR cycles  
15 were repeated five times with increasing reoxidation temperature (700°C, 750°C, 800°C, 850°C and  
16 900°C). The heating rate during reoxidation and cooling after all experiments was 10°Cmin<sup>-1</sup>.  
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31 Nickel K-edge (8.333 keV) X-ray absorption spectra were acquired ex situ on pelletized samples in  
32 fluorescence mode at the X10DA (SuperXAS) beamline of the Swiss Synchrotron Light Source (SLS,  
33 Villigen, Switzerland) using a 5 element SD detector. The required X-ray energies were scanned using  
34 a Si(111) monochromator. The Demeter software package (version 0.9.24)<sup>41</sup> was used to reduce and  
35 model all data. The radial distribution function (R) was obtained by Fourier transforming k<sup>3</sup>-weighted  
36 k-functions typically in the range of 3.0 - 12.0 Å<sup>-1</sup> using a Hanning window function. Fitting of bond  
37 distances was generally performed in the range of 1.0-4.0 Å. NiO (99.99% trace metals basis, Sigma)  
38 and Ni foil references were measured in transmission mode using ionization chamber detectors.  
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49 Linear combination fitting (LCF) of X-ray absorption near edge structure (XANES) spectra was  
50 performed in the spectral range -20 eV < E<sub>0</sub> < 30 eV around the absorption edge to quantify the  
51 fraction of each Ni species present in the samples. Reference compounds for each fit included Ni-foil,  
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5 NiO and calcined  $\text{La}_{0.3}\text{Sr}_{0.55}\text{Ti}_{0.95}\text{Ni}_{0.05}\text{O}_{3\pm\delta}$  representing  $\text{Ni}^{n+}_{\text{oct}}$  ( $n>2$ ) in the perovskite coordination  
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7 environment.

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10 X-ray fluorescence was collected ex situ on pretreated and pelletized samples at the Phoenix beamline  
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12 at SLS. A 4-element Si drift diode array was used to collect fluorescent radiation at an incident X-ray  
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14 energy of 2600 eV.

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17 Changes in the microstructure of the samples as a result of repeated redox cycles were studied using  
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19 scanning electron microscopy (field emission SEM, Zeiss ULTRA 55). The samples were analyzed  
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21 using a 5 keV electron beam and the in-lens secondary electron detector at a working distance of 1.8  
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23 mm. Typical magnifications in the range of 50'000-100,000 allowed the analysis of Ni particles of ca.  
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25 5-10 nm.

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28 Scanning transmission electron microscopy (STEM) images were acquired using an analytical TEM  
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30 (FEI Talos F200X) equipped with a Super-X EDX system (windowless) and a high angle annular dark  
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32 field (HAADF) detector. The accelerating voltage was set to 200 kV. EDX maps (512 x 512 pixels)  
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34 were acquired with a resolution of 7 nm.

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37 Catalytic activity tests towards the water gas shift reaction (WGS) were carried out with a homemade  
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39 test setup in a quartz reactor of plug flow geometry (6 mm ID). Mass flow controllers were used to  
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41 dose the reactant gases and a thermocouple placed in the middle of the catalyst bed was used to  
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43 determine catalyst bed temperature. To avoid back pressure all calcined powders were pelletized (4  
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45 MPa), crushed in an agate mortar and sieved to 100-150  $\mu\text{m}$  before use. The catalyst (100 mg) was  
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47 diluted with cordierite powder (100 mg, 75-100  $\mu\text{m}$ ) to achieve a thoroughly mixed catalyst bed of 10  
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49 mm in length. The reactant gas containing 15 vol% CO, 15 vol%  $\text{H}_2\text{O}$ , 7.5 vol%  $\text{H}_2$  (rest Ar) was fed at  
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51 a total flow rate of 50  $\text{mLmin}^{-1}$  at STP resulting in a weight hourly space velocity (WHGS) of 30,000  
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53  $\text{mLg}^{-1}\text{h}^{-1}$ . Catalytic tests were conducted on pre-reduced samples (20 vol%  $\text{H}_2$ , 800°C, 1 h). The  
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experiment was started at 800°C under reaction conditions after the catalyst was left to equilibrate for 10 min before cooling to 300°C at 5 °Cmin<sup>-1</sup>. All stainless steel gas lines were heated to 120°C to avoid condensation. Compositional analysis of the exhaust gas was performed using a quadrupole mass spectrometer (Pfeiffer OmniStar GSD 320) equipped with a heated stainless steel capillary. CO conversion ( $C_{CO}$ ) was determined according to eq. 1

$$C_{CO} [\%] = 100 \cdot \frac{[CO]_{in} - [CO]_{out}}{[CO]_{in}} \quad (1)$$

where  $[CO]_{in}$  and  $[CO]_{out}$  are the initial and final CO concentrations, respectively.

Equilibrium conversions were calculated from the following expression (eq. 2) for the WGS equilibrium constant  $K_{eq}$ <sup>42</sup>

$$\log K_{eq} = \frac{5693.5}{T} + 1.077 \ln T + 5.44 \cdot 10^{-4} T - 1.125 \cdot 10^{-7} T^2 - \left( \frac{49170}{T^2} \right) - 13.148 \quad (2)$$

and the relationship

$$K_{eq} \cong \frac{[CO_2] \cdot [H_2]}{[CO] \cdot [H_2O]} \quad (3)$$

where  $[CO_2]$ ,  $[H_2]$ ,  $[CO]$  and  $[H_2O]$  are the concentrations of the corresponding gases at equilibrium.

The effect of sulfur poisoning was assessed on pre-reduced LSTN (20 vol% H<sub>2</sub>/Ar, 800°C, 1 h) after eight redox cycles. The material was subjected to the water gas shift reaction mixture additionally containing 50 ppm H<sub>2</sub>S at 800°C for 2 h before cooling in Ar. The water gas shift activity of the poisoned catalyst was then obtained in identical tests to those on the non-poisoned material. Catalyst regeneration was conducted through two consecutive redox cycles at 800°C (1 h reduction followed by 2 h reoxidation).

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5 The preliminary tests of full solid oxide cells based on pure LSTN anodes exhibited a high polarization  
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7 resistance due to the low ionic conductivity of the LSTN anode layer because of the short length of  
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9 triple phase boundaries at the interphase with the electrolyte.<sup>43-44</sup> Hence, electrochemical tests were  
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11 conducted on composite electrodes with high LSTN content in a full cell design. LSTN powders were  
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13 mixed with ionically conductive gadolinium cerium oxide ( $\text{Ce}_{0.9}\text{Gd}_{0.1}\text{O}_2$ , CGO), dispersed in terpene  
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15 alcohol (mixture of isomers, anhydrous, Fluka) and homogenized by planetary milling as described  
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17 elsewhere.<sup>45</sup> Screen-printable inks with 60 vol% LSTN and 40 vol% CGO and  $\text{La}_{0.2}\text{Sr}_{0.8}\text{MnO}_3$ -  
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19  $\text{Y}_{0.15}\text{Zr}_{0.85}\text{O}_2$  (LSM-YSZ) cathodes (50:50 vol%) were printed onto sintered  $\text{Sc}_{0.12}\text{Zr}_{0.88}\text{O}_2$  electrolyte  
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21 (120  $\mu\text{m}$  thickness, non-reactive with titanates) and both electrodes were co-fired at 1150°C for 3 h.<sup>46</sup>  
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23 Nickel-free LST was printed on top of the active layer of the electrode for current collection and  
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25 contacted to measurement electrodes by Au and Ni meshes. The prepared cells (active electrode area =  
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27 1.44  $\text{cm}^2$ ) were inserted into the test setup, sealed with a ceramic gasket (Insufliz) and connected to the  
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29 measuring terminal (Zahner IM6ex). Electrochemical impedance spectroscopy (EIS) and voltammetry  
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31 were used for characterization. Cells were heated in oxidizing atmosphere at a rate of 3 °Cmin<sup>-1</sup> and  
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33 anodes reduced and operated in pure hydrogen (PanGas, 5.0) at a gas flow of 200 mLmin<sup>-1</sup> at STP. Air  
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35 was supplied to the cathode with a flow rate of 450 mLmin<sup>-1</sup> at STP. Cell temperature was measured  
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37 via the thermoelectric potential of an S-type thermocouple located close to the cell. Anode reoxidation  
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39 was conducted by 30 min fuel cut-offs at the working temperature of 850°C under open circuit voltage  
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41 (OCV). The cell was operated in electrolysis mode (-2.0 V) twice for 2 min and once for 2 min under  
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43 current overload (2.0  $\text{Acm}^{-2}$ ) to monitor the effects of these treatments on area specific resistance.  
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45 Impedance spectra were collected in the frequency range between 0.01 Hz and 1 MHz in galvanostatic  
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47 mode, both under OCV and under polarization when drawing 200  $\text{mAcm}^{-2}$ . Changes in the impedance  
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49 spectra were analyzed by Analysis of Differences in Impedance Spectra (ADIS), which shows  
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51 frequency dependent changes of impedance upon variation of operating conditions.<sup>47</sup>  
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The differential method (ADIS) is based on the analysis of real parts of impedance spectra:

$$\Delta\delta Z = \left| \left( \frac{\partial Z_{\text{Real}}^{P1}}{\partial \log f} \right) - \left( \frac{\partial Z_{\text{Real}}^{P2}}{\partial \log f} \right) \right| \quad (4)$$

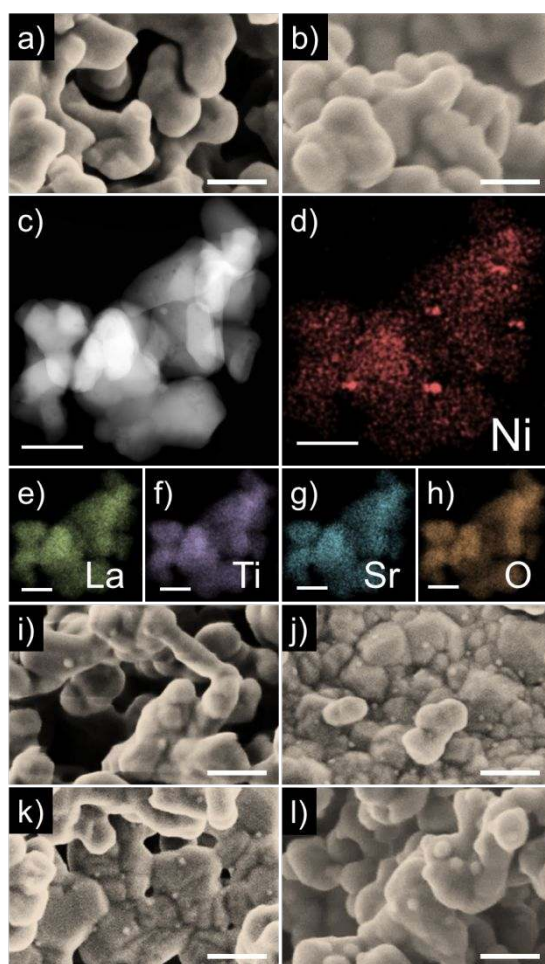
where  $\delta Z_{\text{Real}}^{P1}$  and  $\delta Z_{\text{Real}}^{P2}$  are differentials of the real impedance part upon the change of one experimental parameter (P1, P2 represent states before and after redox cycling).

### 3. Discussion

#### 3.1 Nickel reduction and segregation

The individual powder grains of calcined  $\text{La}_{0.3}\text{Sr}_{0.55}\text{Ti}_{0.95}\text{Ni}_{0.05}\text{O}_{3-\delta}$  (LSTN) were composed of individual crystallites forming a porous network as depicted in the scanning electron microscopy (SEM) image in Figure 1-a. All calcined perovskite-type oxide powders showed excellent phase purity and high crystallinity (Figure S1). Table S1 summarizes general powder characterization results including specific surface areas (SSA) and the analysis of X-ray diffraction (XRD) patterns. All sample abbreviations used throughout the discussion are also given in Table S1. The perovskite samples LSTN and LST contained a single cubic perovskite phase (Pm-3m), which was observed and reported also for undoped and stoichiometric  $\text{SrTiO}_{3\pm\delta}$ .<sup>48</sup> No indication of secondary phases (NiO) could be found by SEM on impregnated  $\text{Ni/La}_{0.3}\text{Sr}_{0.55}\text{TiO}_{3-\delta}$  (Ni/LST, Figure 1-b) even though NiO reflections (i.e. (200) at  $2\theta \approx 43.3^\circ$ ) could be observed by XRD. Reduction of both LSTN and Ni/LST at  $800^\circ\text{C}$  resulted in the display of metallic Ni particles on the surface of the materials. This is less surprising in the case of impregnated Ni/LST where NiO was simply reduced to  $\text{Ni}^0$  on the support surface. In LSTN however, formation of the observed particles must have occurred from reduction of Ni from the bulk of the material and segregation to the crystallite surface. The segregation of Ni and the formation of Ni

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5 particles on LSTN can be observed in the STEM image of the sample reduced at 800°C/15 h (Figure 1-  
6 c), after which few small particles in the size range of 10 – 30 nm were visible. These features overlap  
7 with the areas of increased Ni concentrations obtained from the elemental mapping of Ni (STEM EDX,  
8 Figure 1-d). All other elements remained uniformly distributed across the particles and likely remained  
9 inside the metal oxide crystallites. Therefore, we consider that segregation of other elements than Ni  
10 did not occur.  
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50 Figure 1. SEM images of a) LSTN and b) Ni/LST after calcination. c) High angle annular dark field  
51 TEM image of reduced LSTN (800°C, 10 vol% H<sub>2</sub>, 15 h); Elemental maps (STEM-EDX) of same  
52 sample region displaying Ni, (d) La, (e) Ti, (f) Sr (g) and O concentrations (h). Scale bars represent  
53 200 nm. SEM images of (i) LSTN and (j) Ni/LST after single reduction (800°C, 10 vol% H<sub>2</sub>, 1 h) as  
54 well as reduced after eight redox cycles (k) and (l), respectively. Scale bars on SEM images represent  
55 100 nm.  
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### 3.2 Self-regenerating property

Inherent material redox stability is decisive for application in a regenerable SOFC anode. Since the intended regeneration from sulfur poisoning involves anode redox cycling, additional catalyst deactivation due to Ni particle growth over the number of redox cycles may strongly limit its functionality. Figure 1 depicts a series of SEM images of LSTN (Figure 1-i and Figure 1-k) and Ni/LST (Figure 1-j and Figure 1-l) after a single reduction step at 800°C and reduced after eight redox cycles. Nickel particles are visible on all images. However, in the case of LSTN the size of these particles did not change significantly over eight redox cycles, whereas clear indications of Ni particle growth can be seen in the case of Ni/LST. After a single reduction step the material displayed numerous small Ni particles (mean size ca. 10 nm), whereas after eight redox cycles most particles had grown to 20-40 nm in size. Therefore, particle growth over redox cycles was indeed an issue on the impregnated Ni/LST, whereas the self-regenerating property of LSTN stabilized Ni particle size over the course of the treatment.

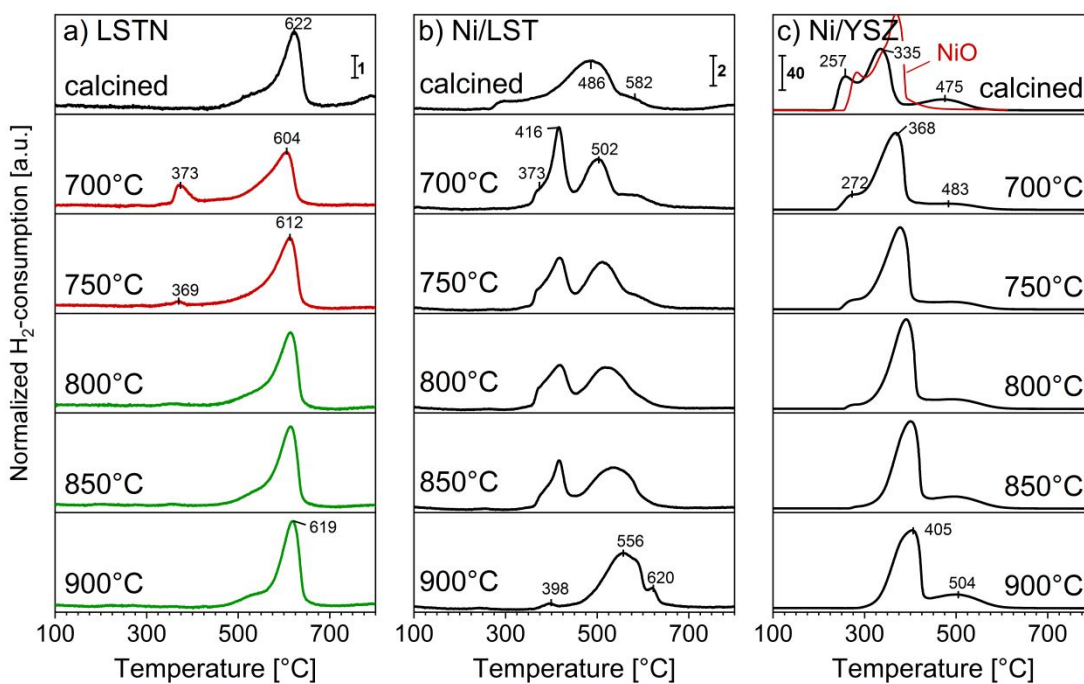


Figure 2. Temperature programmed reduction-reoxidation cycles for (a) LSTN, (b) Ni/LST and (c) Ni/YSZ. Hydrogen consumption values were normalized by the number of moles of sample used. Reoxidised samples were subjected to pre-reduction in 10 vol% H<sub>2</sub> at 800°C for 1 h before reoxidation at the given temperature (20 vol% O<sub>2</sub>, 2 h). Reduction profile of NiO reference is depicted in top row of c).

Metal segregation from and reincorporation back into perovskite-type oxide lattices is a temperature dependent process.<sup>49</sup> It is therefore of great interest for practical application to determine the reoxidation temperature at which Ni can be completely reincorporated into the perovskite lattice. This was achieved using a strategy previously applied to investigate Ni reincorporation into LaFe<sub>1-x</sub>Ni<sub>x</sub>O<sub>3±δ</sub> host lattices.<sup>38</sup> Figure 2 shows the results of H<sub>2</sub>-temperature programmed reduction (TPR) – reoxidation cycles on the three Ni catalysts. Similarities in the reduction profiles of calcined Ni/LST (Figure 2-b) and Ni/YSZ (Figure 2-c) were expected since XRD analysis (summarized in Table S1) already indicated the presence of a NiO phase dispersed on both materials. Reduction started below 250°C and appeared to be complete at 630°C. Reduction of calcined Ni/LST peaked at 486°C, whereas



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5 the highest hydrogen consumption of Ni/YSZ occurred at 335°C. In general, the shape and temperature  
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7 range of the reduction profile of Ni/YSZ was very similar to that obtained on pure NiO powder, which  
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9 showed maximum rate of reduction at 370°C (Figure 2-c). In marked contrast, H<sub>2</sub>-consumption during  
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11 the TPR of calcined LSTN started at 450°C and peaked at 622°C. The evident differences in the  
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13 reduction profiles of these materials are due to the different state of Ni - as determined by X-ray  
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15 absorption spectroscopy (XAS, vide infra in Figure 4) - and distinguish NiO from incorporated Ni  
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17 species (Ni<sup>n+</sup><sub>oct</sub>). Reduction profiles can therefore be used to determine the state of Ni and to estimate  
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19 the oxidation temperature necessary to reincorporate Ni into the perovskite lattice.  
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22 Figure 2 also shows a series of TPR profiles for each sample after pre-reduction (800°C, 10 vol%  
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24 H<sub>2</sub>/Ar, 1 h) and subsequent reoxidation (T=700, 750, 800, 850 and 900°C, 20 vol% O<sub>2</sub>/N<sub>2</sub>, 2 h). In the  
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26 case of LSTN, whenever the reoxidation temperature was not sufficient to reincorporate all Ni into the  
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28 lattice during the reoxidation a distinctive reduction peak of NiO appeared at ca. 370°C in the  
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30 subsequent TPR. After reoxidation at T ≥ 800°C this NiO feature disappeared, which indicated full Ni  
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32 reincorporation into the LSTN lattice.  
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35 Ni/LST and Ni/YSZ also showed changes in the reduction profiles from the calcined to the reoxidised  
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37 materials, which can be attributed predominantly to morphological changes of the NiO phase.<sup>50</sup> The  
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39 higher reduction temperature of NiO/LST compared to Ni/YSZ was attributed to the close contact  
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41 between the small amount of Ni and the oxygen providing perovskite surface in Ni/LST. In this case,  
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43 LST might have acted as an oxygen source to prevent NiO reduction at low temperatures.  
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45 Nevertheless, from the evolution of the reduction profile shape of the impregnated samples (Ni/LST  
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47 and Ni/YSZ) it can be assumed that Ni was always present as NiO species after each reoxidation cycle.  
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50 Similar TPR redox experiments involving multiple redox cycles at a constant reoxidation temperature  
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52 of 800°C were also conducted (Figure S2). This temperature is typical of SOFC operation<sup>51</sup> as well as  
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54 the temperature at which Ni was found to reincorporate into the perovskite lattice in LSTN. The  
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5 reduction profile of LSTN showed complete reversibility over all cycles and the temperature range of  
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7 H<sub>2</sub>-consumption remained between 450°C and 650°C with a maximum at 614-627°C. Reversible  
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9 reduction profiles were also found for Ni-free LST pointing to the intrinsic redox stability of the host  
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11 perovskite structure. The reduction feature observed for LST was assigned to the loss of oxygen and  
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13 partial reduction of Ti<sup>4+</sup> to Ti<sup>3+</sup>. The two impregnated samples Ni/LST and Ni/YSZ appeared to change  
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15 significantly after the first reoxidation. Changes were likely due to the low initial calcination  
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17 temperatures of 500°C after impregnation with the Ni precursor compared to the high reoxidation  
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19 temperature of 800°C used during the experiment. After the first high temperature reoxidation all  
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21 samples maintained their reduction profiles in the next redox cycles. Slight peak narrowing was  
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23 observed over the course of the redox cycles for the two impregnated samples, which has previously  
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25 been attributed to increased metal oxide crystallinity and can also be taken as an indication of NiO  
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27 particle growth, hence degeneration of the potential anode material.<sup>52</sup>  
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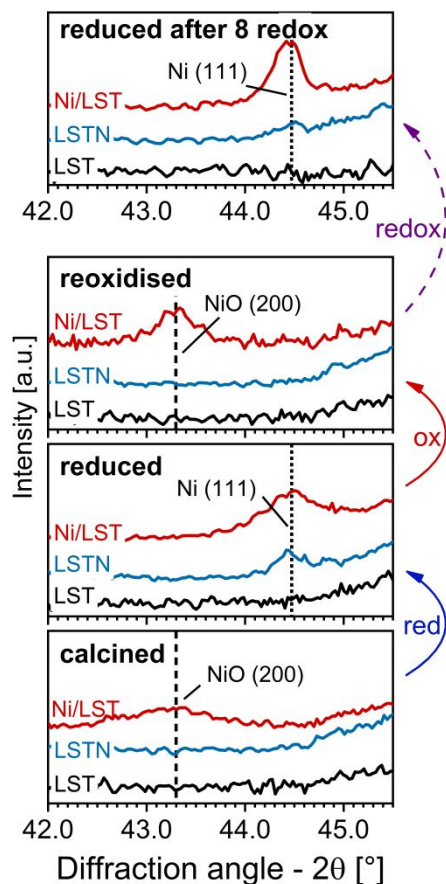


Figure 3. X-ray diffraction patterns of LST (black) LSTN (blue) and Ni/LST (red) in the angular range of  $42.0^\circ \leq 2\theta \leq 46.0^\circ$  in their calcined state, after reduction ( $800^\circ\text{C}$ , 10 vol%  $\text{H}_2$ , 1 h), after reoxidation ( $800^\circ\text{C}$ , 20 vol%  $\text{O}_2$ , 2 h) and reduced after eight redox cycles. The position of the NiO (200) reflection at  $43.299^\circ$  and the Ni (111) reflection at  $44.473^\circ$  are indicated with dashed and dotted lines, respectively.

The beneficial consequences of exploiting the smart material concept,<sup>30</sup> i.e. the absence of Ni particle growth on LSTN and the evidence of particle growth on impregnated Ni/LST, can also be visualized by XRD. Figure 3 shows the angular range in  $2\theta$  between  $42 - 45.5^\circ$  (including the main (200) reflection of NiO at  $43.3^\circ$  and the (111) reflection of Ni at  $44.5^\circ$ ) of LSTN, Ni/LST as well as plain LST for reference purposes over a similar series of redox cycles. Only a broad NiO reflection was

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5 observed on calcined Ni/LST, whereas no NiO reflection was present in LSTN and obviously LST  
6 (Figure 3-a). After reduction at 800°C the Ni (111) reflection appeared in both LSTN and Ni/LST  
7 (Figure 3-b). This reflection disappeared on LSTN after reoxidation at 800°C, whereas it changed into  
8 a strong NiO reflection in the case of Ni/LST. This indicates complete Ni reincorporation in the case of  
9 LSTN and the absence of this process in Ni/LST (Figure 3-c). However, XRD may not be sensitive  
10 enough to detect the presence of small and/or low concentrations of secondary phase crystallites.  
11 Nevertheless, after eight consecutive redox cycles (Figure 3-d) the Ni (111) reflection had significantly  
12 narrowed in the XRD of Ni/LST compared to the reflection after the initial reduction (Figure 3-b), thus  
13 indicating the undesired process of Ni crystallite growth. No significant peak narrowing was observed  
14 in the case of LSTN.

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26 The fact that Ni was changing oxidation states between that of NiO and of Ni<sup>0</sup> over the course of the  
27 redox cycle in the case of Ni/LST, whereas it was changing reversibly between Ni<sup>n+</sup><sub>oct</sub> inside the  
28 perovskite and Ni<sup>0</sup> in the case of LSTN, is reinforced by the Ni K-edge X-ray absorption near edge  
29 spectra (XANES) of LSTN (Figure 4-a) and Ni/LST (Figure 4-b). The spectrum of the reference Ni-  
30 foil showed a clear edge at 8333 eV and no whiteness was visible, which is typical for metallic samples.  
31 The absorption edge of NiO was shifted towards higher energies (8340 eV) due to the higher oxidation  
32 state of Ni<sup>2+</sup> and the spectrum included a clear single peak of the whiteness. The spectrum also  
33 contained a local minimum at 8361 eV, which can be used as a fingerprint feature of NiO in the Ni K-  
34 edge XANES region. The spectrum of calcined LSTN showed a more complex and intense whiteness  
35 including a shoulder at 8352 eV and no feature at 8361 eV.

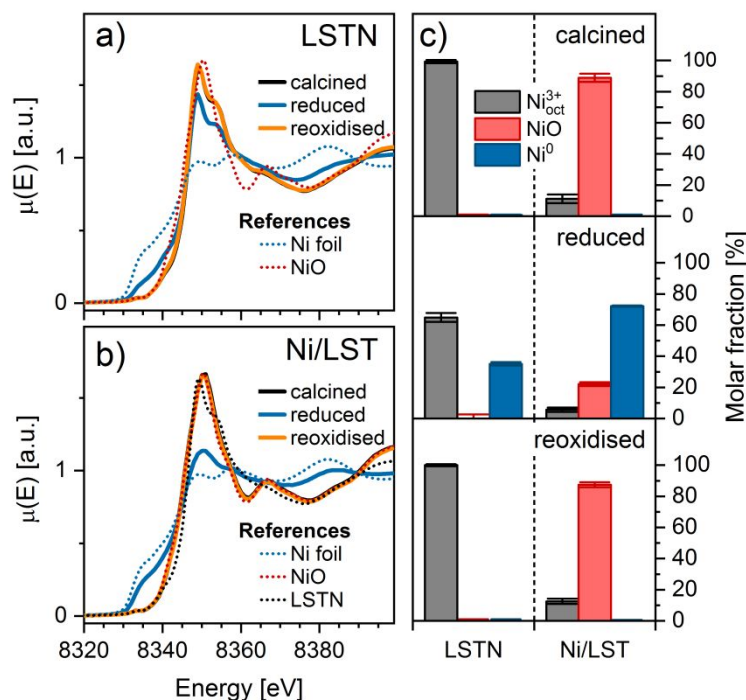


Figure 4. Normalized Ni K-edge (8333 eV) X-ray absorption near edge structure (XANES) data obtained for (a) LSTN and (b) Ni/LST calcined, reduced (10 vol%  $\text{H}_2$ , 800°C, 1 h) and reoxidised (20 vol%  $\text{O}_2$ , 800°C, 2 h). The spectra of Ni-foil and NiO reference materials are also shown. c) Ni speciation obtained from linear combination fitting of XANES data on LSTN and Ni/LST after calcination, after reduction and after reoxidation.

The spectra obtained after calcination and reoxidation completely overlapped in both materials. After reduction at 800°C, the spectra exhibited an intensified feature at 8335 eV and a whiteline of decreased intensity, thus resembling a linear combination of the spectra of the calcined material and the Ni-foil reference. Linear combination analysis was performed to determine the contribution of each Ni species ( $\text{NiO}$ ,  $\text{Ni}^0$  and  $\text{Ni}^{\text{n}+}_{\text{oct}}$ ) to the spectra of the reduced materials. The spectrum of LSTN was taken as representative of  $\text{Ni}^{\text{n}+}_{\text{oct}}$ . Results are presented in Figure 4-c and the full fits and residuals are provided in Figure S3. Nickel was predominantly present as NiO on Ni/LST (>85 %). The coordination of the remaining Ni resembled the one of  $\text{Ni}^{\text{n}+}_{\text{oct}}$ , which could indicate possible Ni incorporation into LST.

After reduction at 800°C, 35 % of the overall Ni was reduced to metallic Ni in the case of LSTN, whereas the extent of reduction was much higher (70 %) for impregnated Ni/LST. This behavior is explained with the fact that Ni in LSTN is evenly distributed within the bulk of the perovskite lattice and is not easily accessible to the reducing environment. In the case of Ni/LST, Ni is directly exposed to the gas environment. In both cases reoxidation restored the original Ni species. The observation of the reversible Ni segregation in the case of LSTN validates all observations and interpretations obtained by electron microscopy, XRD and TPR.

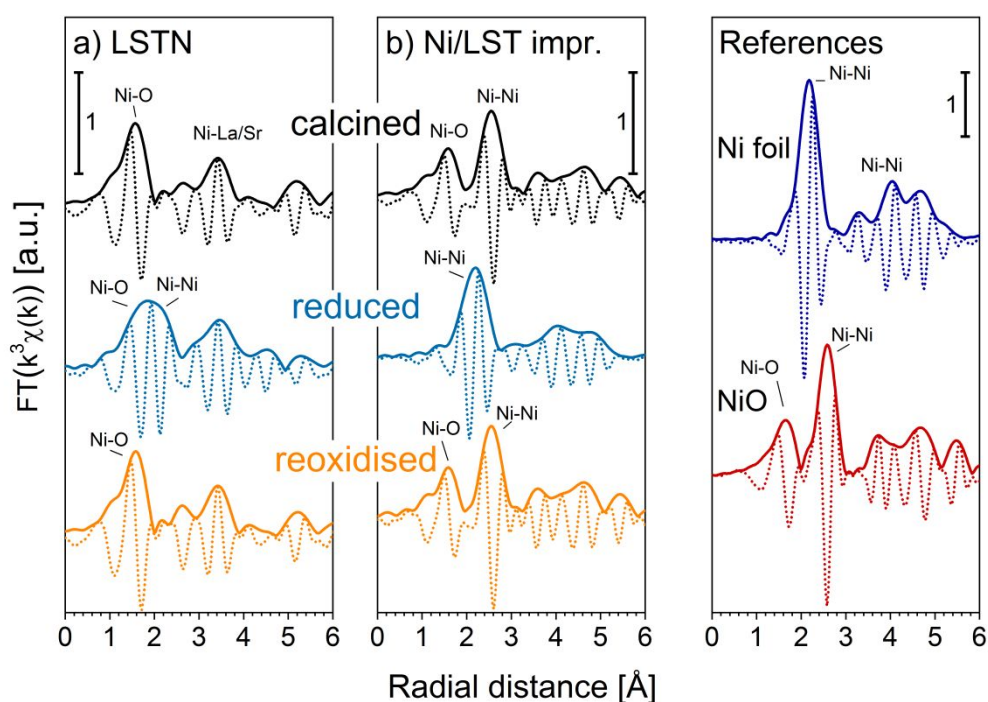


Figure 5. Fourier transformed  $k^3$ -weighted Ni K-edge EXAFS data obtained for (a) LSTN and (b) Ni/LST calcined, after reduction (800°C, 10 vol%  $H_2$ , 1 h) and reoxidation (800°C, 20 vol%  $O_2$ , 2 h). Features are labelled according to their underlying scattering paths. Reference compounds are shown for comparison.

Extended X-ray absorption fine structure (EXAFS) analysis and fitting consolidate our claim of reversible Ni segregation from LSTN. The radial distribution function obtained by Fourier

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5 transformation of the  $k^3$ -weighted EXAFS is shown in Figure 5. The signals of all reference materials  
6 displayed substantial differences (Figure 5-a). Nickel metal exhibits a characteristic first peak at 2.48 Å  
7 corresponding to the first Ni coordination shell, which consists of twelve neighboring Ni atoms in the  
8 fcc crystal structure. The first coordination shell of Ni in NiO contains six oxygen anions at a distance  
9 of 2.07 Å followed by a Ni coordination shell at 2.95 Å. In LSTN (Figure 5-b) the first oxygen  
10 coordination shell was found at a mean distance of 1.95 Å, which is shorter than in NiO due to the  
11 higher oxidation state of Ni in LSTN. The second coordination shell at around 3.3 Å is provided by the  
12 A-site cations ( $\text{La}^{3+}$  and  $\text{Sr}^{2+}$ ) while the Ni-Ni feature present in NiO was absent. The development of  
13 the feature at 2.5 Å corresponding to the Ni coordination shell in Ni metal was observed after reduction  
14 in both LSTN (Figure 5-a) and Ni/LST (Figure 5-b). Upon reoxidation the original coordination  
15 environment of Ni was completely restored in both samples, as revealed by the similarity of the radial  
16 distribution curves of the reoxidised and the calcined states. Similar conclusions can also be drawn  
17 directly from the  $k^3$ -weighted EXAFS functions ( $k^3 \cdot \chi(k)$ , Figure S4) as signature features of each Ni  
18 species and coordination state in the samples are clearly visible. The signature features included a  
19 distinct triple feature between 5.0 Å and 6.5 Å<sup>-1</sup> for  $\text{Ni}^{\text{n+}}_{\text{oct}}$  in LSTN, where the first two peaks were  
20 weak and followed by an intense third feature. The range in wavenumbers used for identification of  
21 NiO is somewhat narrower (5.8-6.8 Å<sup>-1</sup>) and included a distinctive double feature, of which the second  
22 peak was slightly more pronounced. The complete reversibility of  $k^3 \cdot \chi(k)$  profiles between calcined  
23 and reoxidised LSTN and Ni/LST can therefore already be appreciated prior to Fourier transformation.  
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### 46 3.3 Redox stability of water gas shift catalyst

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49 The ability of the anode material to catalyze water gas shift (WGS) is widely regarded to be critical for  
50 the efficiency of a SOFC operated on syngas feeds as readily oxidizable  $\text{H}_2$  fuel is produced.<sup>53</sup> This is  
51 also one of the main reasons for the use of high loadings of metallic Ni in Ni/oxide cermet anodes  
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besides excellent electronic conductivity of metallic Ni. It is clear that the dynamic conditions in the presence of electric current flow through a working SOFC anode cannot be easily replicated by the relatively simple experimental setup used for catalytic tests in plug flow reactors. Nevertheless, such tests provide important information on the intrinsic redox stability of the catalyst.

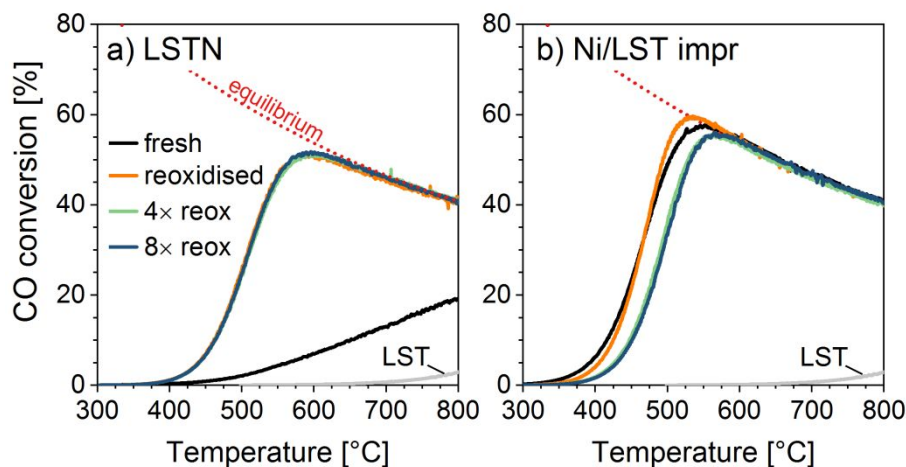


Figure 6. WGS activity profiles of reduced (a) LSTN and (b) Ni/LST over eight redox cycles. Feed gas composition: 15 vol% CO, 15 vol% H<sub>2</sub>O, 7.5 vol% H<sub>2</sub>, rest Ar; at 30,000 mLh<sup>-1</sup>g<sup>-1</sup> (at STP). The calculated theoretical conversion equilibrium is indicated by the dotted red curve.

Figure 6 displays typical CO conversions measured on LSTN (Figure 6-a) and Ni/LST (Figure 6-b) catalysts over eight redox cycles. Pre-reduced LSTN only showed very limited WGS activity and CO conversions did not exceed 20% even at high temperatures under the conditions used in this test. However, after a single oxidation-reduction cycle its catalytic activity improved significantly and equilibrium conversions were reached. It is assumed that this effect arises from increased amounts of Ni made available on the perovskite surface by high temperature reduction. It is obvious that conversion curves of LSTN after four and after eight redox cycles were identical to the one obtained after the first redox cycle. Comparison of the activity of LSTN and Ni/LST to the negligible conversion obtained for Ni-free LST indicated that the Ni metal surface area generated by reduction bestowed



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5 catalytic activity to the material (Figure S5). Stable WGS activity can be regarded as an indication of  
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7 constant Ni surface area and therefore negligible Ni particle growth over the number of redox cycles.  
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9 Ni/LST (Figure 6-b) showed maximal conversion already after a single reduction step. This was  
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11 expected since all Ni is at the surface of the material and available for WGS catalysis on impregnated  
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13 materials. Redox cycling shifted the conversion curves towards higher temperatures indicating catalytic  
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15 activity loss, which is likely due to an initial Ni particle growth over the number of redox cycles.  
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17 However, catalytic activity stabilized after four redox cycles (as documented by SEM in Figure 1).  
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19 This effect can be related to the decreased driving force of particle sintering as particle growth  
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21 progresses and/or to the stabilizing nature of the perovskite surface. The evolution of catalytic activity  
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23 over consecutive redox cycles in both samples demonstrated the particle size stabilizing function of  
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25 LSTN. Nevertheless, it is worth noticing that the final conversion curve of Ni/LST was still shifted to  
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27 lower temperatures by around 50°C compared to the one obtained for LSTN after eight redox cycles,  
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29 likely due to the larger amount of active Ni<sup>0</sup> available on the surface of Ni/LST compared to LSTN as  
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31 evident from XANES linear combination analysis (Figure 4-c). Since WGS activity is strongly  
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33 dependent on Ni content, it is not surprising that 60 wt% Ni/YSZ showed the highest activity of all  
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35 catalysts (Figure S5). Furthermore, redox cycling of Ni/YSZ did not affect catalytic activity towards  
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37 WGS, which is a consequence of the high Ni content in this sample. However, in a working cell  
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39 reoxidation of the Ni/YSZ anode can be fatal and leads to mechanical fracture and cell failure due to  
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41 the extreme volume expansion from Ni to NiO despite the fact that the material may preserve its high  
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43 catalytic activity.<sup>21</sup> Redox experiments on this material should therefore only be regarded as  
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45 complementary to the ones performed on the LST-type catalysts.  
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### 3.4 Redox stable SOFC anode

Fuel cell tests combined with detailed electrochemical analysis over a number of redox cycles were conducted on full button cells to investigate the performance and stability of LSTN during application as SOFC anode. Figure 7-a shows the current density and cell voltage under various operation conditions for 480 h. Anode reoxidation was carried out nine times, after 21, 24, 27, 45, 48, 51, 190, 194 h and 313 h, respectively, as indicated by vertical dashed time stamp lines. Reoxidation was carried out by a H<sub>2</sub> fuel supply cut-off simulating a gas delivery stop or severe sealing failure. First, the cell was aged for 213 h under open circuit voltage (OCV) conditions (including the first eight redox treatments) before drawing 200 mAcm<sup>-2</sup> current from the cell under polarization. The polarization resistance development of the cell with time and number of redox cycles was investigated using electrochemical impedance spectroscopy (EIS). In the initial 213 h of the experiment redox stability of the LSTN-CGO material pair was tested by subjecting the cell to eight redox cycles under OCV. The Nyquist plot in Figure 7-b depicts impedance spectra before and after selected redox cycles throughout the thermal aging of the cell. Nyquist plots could be described as “compressed” semicircles indicating the existence of several overlapping processes. In the higher frequency ranges only a minor resistance contribution could be identified. This is mainly attributed to the cathode material, which has an optimized microstructure and long-term stability as demonstrated elsewhere.<sup>54-56</sup> Because the cathode material exhibited a polarization resistance of 0.05 Ωcm<sup>2</sup> in symmetrical cell tests thus contributing only marginally to the overall resistance, all changes in polarization resistance were assigned to the electrochemical processes occurring at the anode. It is important to highlight that the measured ohmic resistance of the cell was very close to the theoretical resistance of the Sc<sub>0.12</sub>Zr<sub>0.88</sub>O<sub>2</sub> electrolyte and contributions from cell contacts and test rig itself did not affect the measurements. After the first two hours of aging at OCV a rather high area specific resistance (ASR) of 2.46 Ωcm<sup>2</sup> was measured. This high resistance value was attributed to an insufficient reduction and thus limited exsolution of the

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5 catalytically active Ni. Cell performance remarkably improved after 21 h and a first redox cycle, which  
6 suggested the exsolution of larger amounts of Ni from bulk LSTN. The redox treatment caused a  
7 decrease in ASR to  $0.82 \Omega\text{cm}^2$ . This behavior reflects the one observed during the catalytic tests on  
8 LSTN powders (Figure 6), where the first redox cycle also caused a large increase in catalytic activity  
9 indicating substantial increase in active Ni surface area over the first redox cycle.  
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16 A further decrease in ASR to  $0.71 \Omega\text{cm}^2$  was observed after the following two redox cycles. After 51 h  
17 of aging and six redox cycles, the ASR reached  $0.60 \Omega\text{cm}^2$ , which was four times lower than the initial  
18 value measured at the beginning of the experiment. Performance loss accompanied by an ASR increase  
19 to  $0.77 \Omega\text{cm}^2$  was observed during further aging without redox cycling (OCV, 136 h,  $850^\circ\text{C}$ ).  
20 However, the stimulus of two redox cycles again triggered the materials self-regeneration and led to a  
21 performance gain, which resulted in an ASR value of  $0.72 \Omega\text{cm}^2$  after 194 h at OCV and eight redox  
22 cycles. The analysis of differences in impedance spectra (ADIS), a data evaluation method in EIS,  
23 revealed information on the impact of redox cycling on electrochemical performance.<sup>57</sup> A low  
24 frequency process in the range of 1-10 Hz (Figure S6) was attributed to the chemical capacitance,  
25 which was kinetically limited by the catalytic processes occurring at the surface of the mixed electronic  
26 ionic conductor such as LSTN and CGO (i.e. hydrogen oxidation reaction, HOR). Redox cycling,  
27 reverse potential mode (-2.0 V), as well as degradation during aging only affected this low frequency  
28 domain at 10 Hz, which matches the previous observations. Long-term exposure of LSTN under OCV  
29 at  $850^\circ\text{C}$  is expected to cause thermal growth of the Ni particles and hence loss of catalytic activity. In  
30 combination with the data from EXAFS and catalytic measurements, it is likely that the redox cycles  
31 triggered Ni regeneration. Therefore, the observed variation in the EIS spectra rather reflect the  
32 properties of the Ni particles as catalytic active phase in LSTN and is not believed to be related to the  
33 additional CGO phase. This claim is supported by the increase in cell performance and decrease of  
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ASR with successive redox cycles and taking into account higher HOR activity of Ni compared to ceria.<sup>58</sup>

An alternative approach to carry out a redox cycle is to subject the cell to a negative polarization of about -2.0 V (electrolysis mode). The effect of electrolysis on the measured impedance is displayed in Figure 7-c and shows a narrowing of the Nyquist plot and decrease in ASR. ASR decreased to  $0.65 \Omega\text{cm}^2$  as oxygen is actively drawn from the anode towards the air electrode at this potential and an oxygen partial pressure of about  $10^{-30}$  Pa is typically reached.<sup>59</sup> This highly reducing atmosphere likely provoked stronger reduction and increased Ni exsolution resulting in larger active Ni surface area and higher performance.

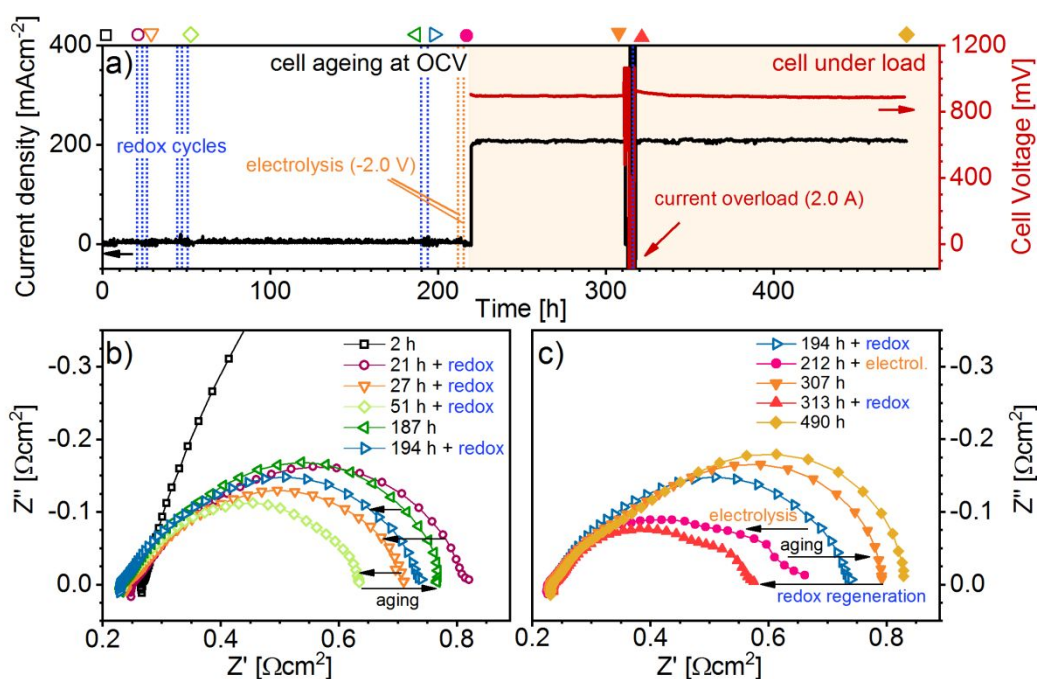


Figure 7. a) Current-Voltage characteristics and an overview of the conditions initiated during the long-term full cell test. White background - open circuit voltage (OCV) conditions, grey background - dynamic conditions with cell polarization. Symbols on top represent the times of EIS corresponding measurements in b) and c). b) Electrochemical impedance spectroscopy data of  $\text{La}_{0.3}\text{Sr}_{0.55}\text{Ti}_{0.095}\text{Ni}_{0.05}\text{O}_3 - \text{Ce}_{0.9}\text{Gd}_{0.1}\text{O}_2$  composite electrode operated under OCV conditions. c) Electrochemical impedance spectroscopy data measured for selected condition changes within the dynamic part of the experiment.

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5 After this aging procedure of the cell under OCV conditions, the cell performance was investigated  
6 under current load at a total current density of  $200 \text{ mA} \cdot \text{cm}^{-2}$ . The cell test included a period at 313 h  
7 (Figure 7-a), when the cell was subjected to severe current overload ( $2.0 \text{ Acm}^{-2}$ ). Current overload  
8 typically causes a rise in fuel utilization and oxygen partial pressure. It may cause irreversible damage  
9 to classical anodes with high Ni content, as Ni may be partially oxidized, similar to a fuel supply  
10 interruption.<sup>60</sup> Stability of the cell voltage, remaining practically constant at 890 mV over 255 h under  
11 polarization, regardless of the varying conditions, indicates excellent anode stability. Impedance results  
12 during this cell operation (Figure 7-c) confirm that anode aging also occurred under current load, as  
13 indicated by the increase of ASR from cell test start at 212 h to 307 h from  $0.67 \Omega\text{cm}^2$  to  $0.79 \Omega\text{cm}^2$   
14 during 90 h of operation at  $200 \text{ mA} \cdot \text{cm}^{-2}$ . However, the cell performance was fully restored by  
15 exploiting redox cycling, reversing degradation. Redox cycling was repeated again by interrupting the  
16 fuel supply, but also the short period of current overload may have additionally contributed to anode  
17 reoxidation. The lowest ASR ( $0.58 \Omega\text{cm}^2$ ) for this type of anode was measured after 313 h in  
18 combination with this redox cycle. The regeneration of the cell after aging under load demonstrated  
19 that the redox stability of the material was also valid under these circumstances.

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37 The electrochemical data clearly shows that LSTN is tolerant to a wide range of potentials and current  
38 overloads. It is also clear that redox cycling can be used as an operation strategy to regenerate such  
39 anodes and to increase performance characteristics after aging.  
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### 45 3.5 Recovery from sulfur poisoning

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47 Besides offering the possibility for cell operation in electrolysis mode, further potential benefits of the  
48 anode redox stability lie in the regeneration from sulfur poisoning, which is a severe problem for cells  
49 operated on  $\text{H}_2$  feeds.<sup>61</sup> Sulfur poisoning becomes detrimental when WGS catalysis is needed to  
50 efficiently convert CO containing fuels.<sup>61</sup> The effect of sulfur on the WGS activity of all catalyst  
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samples was analyzed by further catalytic tests (Figure 8 and Figure S7). The sulfur recovery was tested after the redox cycles displayed in Figure 6 and Figure S5. After these redox stability tests the sample was treated with 50 ppm of H<sub>2</sub>S at 800°C for 2 h under reaction conditions. Finally, CO conversion profiles were recorded after sulfur poisoning and after two further redox (regeneration) cycles. While the already poor activity of Ni-free LST was not affected by the addition of sulfur (Figure S7-b), CO conversions on LSTN and Ni/LST decreased significantly. The sulfur treatment was also sufficient to extinguish the WGS reaction over Ni/YSZ (Figure S7-a) in agreement with the behavior of this anode material in the presence of sulfur.<sup>61</sup> Even though both LSTN (Figure 8-a) and Ni/LST (Figure 8-b) suffered severely from sulfur poisoning, LSTN still retained some activity after poisoning, maintaining 25% CO conversion at 800°C. At this temperature CO conversion of poisoned Ni/LST was as low as 10% and 5% conversion was found on Ni/YSZ. LSTN does not display as much Ni on its surface as either Ni/LST or Ni/YSZ and the fact that it showed the highest activity of the three after poisoning indicates that other WGS active sites than plain Ni<sup>0</sup> may become important, likely as a result of the structural changes induced by Ni segregation.

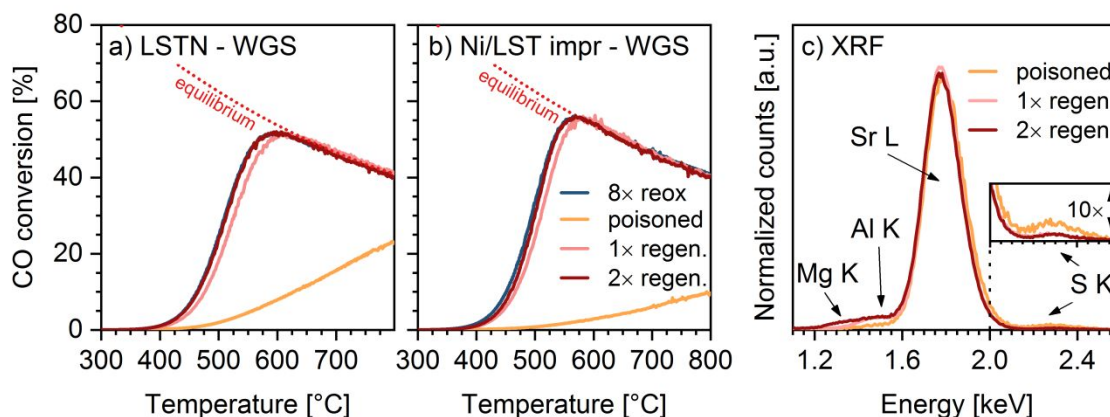


Figure 8. WGS activity profiles of (a) LSTN and (b) Ni/LST after eight redox cycles (prior to poisoning) as well as after H<sub>2</sub>S poisoning and two oxidative catalyst regeneration cycles at 800°C. Feed gas composition: 15 vol% CO, 15 vol% H<sub>2</sub>O, 7.5 vol% H<sub>2</sub>, rest Ar; at 30,000 mLh<sup>-1</sup>g<sup>-1</sup> (at STP). The calculated theoretical conversion equilibrium is indicated by the dotted red curve. c) X-ray

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5 fluorescence (1.1 keV – 2.6 keV) obtained on pellet samples of LSTN after H<sub>2</sub>S poisoning and after  
6 two subsequent oxidative catalyst regeneration cycles at 800°C (2 h oxidation, 1 h reduction). The inset  
7 depicts a 10 fold magnification in intensity of the energy range 2.0 keV – 2.6 keV.  
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11 Redox cycling of poisoned LSTN, identical to the redox cycling exploited to demonstrate structural  
12 reversibility, restored its initial activity. The first regeneration cycle already recovered catalytic activity  
13 substantially, whereas a subsequent second regeneration cycle restored the CO conversion to the  
14 original levels obtained prior to poisoning. Ni/LST could also be regenerated to a large extent by  
15 subjecting it to similar regeneration cycles (Figure 8-b). However, complete regeneration was not  
16 achieved. Besides the fact that Ni/YSZ anodes usually cannot be regenerated by redox cycling due to  
17 their insufficient redox stability,<sup>21</sup> it is also shown that regeneration of the material used as a catalyst  
18 was far from completion even after two regeneration cycles. Fresh Ni/YSZ showed significant activity  
19 below 400°C, whereas after sulfur poisoning and two regeneration cycles comparable CO conversion  
20 was achieved only at higher temperatures ( $\Delta T \sim 50^\circ\text{C}$ ).  
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24 Figure 8-c shows X-ray fluorescence (XRF) spectra of LSTN after sulfur poisoning and over two  
25 regeneration cycles used to regenerate completely LSTN. Beside Mg K and Al K signals due to the Al  
26 sample holder and the presence of traces of the cordierite used to dilute the catalyst bed during catalytic  
27 testing, two additional signals could be identified. The Sr L-edge fluorescence signal (1.8 keV) was by  
28 far the most prominent while a sulfur K-edge transition was clearly visible at 2.3 keV in the poisoned  
29 sample. Despite the intensity decrease already after a single regeneration cycle, sulfur remained  
30 detectable after two cycles. Due to the presence of sulfur after catalyst regeneration and the observed  
31 complete recovery of WGS activity, it is likely that sulfur traces are deposited on the perovskite surface  
32 rather than on the catalytically active Ni and therefore did not interfere with catalytic activity. The  
33 exact nature of these species remains unsettled. From the perspective of the Ni phase in the same  
34 samples, the Ni K-edge spectra of the poisoned sample, of the sample prior to poisoning (after eight  
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5 redox cycles) and after the complete regeneration cycles (reoxidation followed by reduction)  
6 overlapped completely (Figure S7). On the other hand, the spectrum of the reoxidised sample  
7 resembled the one of calcined LSTN. This clearly indicates that irrespective of sulfur poisoning Ni was  
8 able to reincorporate completely during the oxidative treatment of the redox cycle and segregated from  
9 the perovskite lattice upon the reductive treatment to restore the catalytically active Ni particles with a  
10 sulfur free surface and to regenerate catalytic activity.  
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#### 19 4. Conclusions

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21 A redox stable and active Ni based SOFC anode material is presented, which does not make use of  
22 precious metals to obtain sulfur tolerance. The cost efficient material exhibits the remarkable property  
23 of structural regeneration where Ni can be reversibly exsolved from the bulk of the perovskite-type  
24 mixed oxide through reduction and reincorporated back into the host lattice by reoxidation. The  
25 structural reversibility upon redox cycling was documented at microstructure scales as well as on the  
26 atomistic level by means of electron microscopy (SEM/TEM/EDX) and with various spectroscopy  
27 techniques (EXAFS, XANES, XRD). In addition, the associated reversibility of the catalytic activity  
28 was demonstrated by catalytic tests including e.g. WGS activity and TPR profiles. It is shown that Ni  
29 exsolution from the perovskite-type host oxide results in the formation of nano scale Ni particles active  
30 for the water gas shift reaction, which is important to achieve high efficiencies on fuel cells operated  
31 on syngas fuels. Structural reversibility (i.e. the reincorporation of Ni back into the host lattice) can be  
32 exploited to regenerate the anode layer after aging, which is known to cause deactivation of current  
33 SOFC anodes through Ni particle growth. Redox cycling even activated the  $\text{La}_{0.3}\text{Sr}_{0.55}\text{Ti}_{0.95}\text{Ni}_{0.05}\text{O}_{3-\delta}$   
34 anode material and it was demonstrated that catalytic activity of the material towards the water gas  
35 shift reaction could be completely restored after the catalyst had suffered from poisoning by sulfur. It is  
36 for the first time that a material with the properties required for SOFC anode applications was  
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5 demonstrated to also exhibit the remarkable structural regeneration after sulfur poisoning with the  
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7 result of a precious metal free, stable and regenerable SOFC anode layer.  
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## 10 11 5. Acknowledgements

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## 31 6. Supplementary information

32  
33 List of catalysts compositions and denotations including primary and secondary crystal phases. XRD  
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35 patterns of samples after calcination, reduction, reoxidization and reduction after 8 redox cycles. H<sub>2</sub>-  
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37 TPR profiles. Linear combination fit of XANES spectra. k<sup>3</sup>-weighted EXAFS spectra. CO conversion  
38  
39 profiles of Ni/YSZ and Ni free LST before and after H<sub>2</sub>S poisoning. Analysis of Differences in  
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41 Impedance Spectra (ADIS). Normalized Ni K-edge XANES spectra of LSTN after sulfur poisoning  
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43 and after regeneration.  
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