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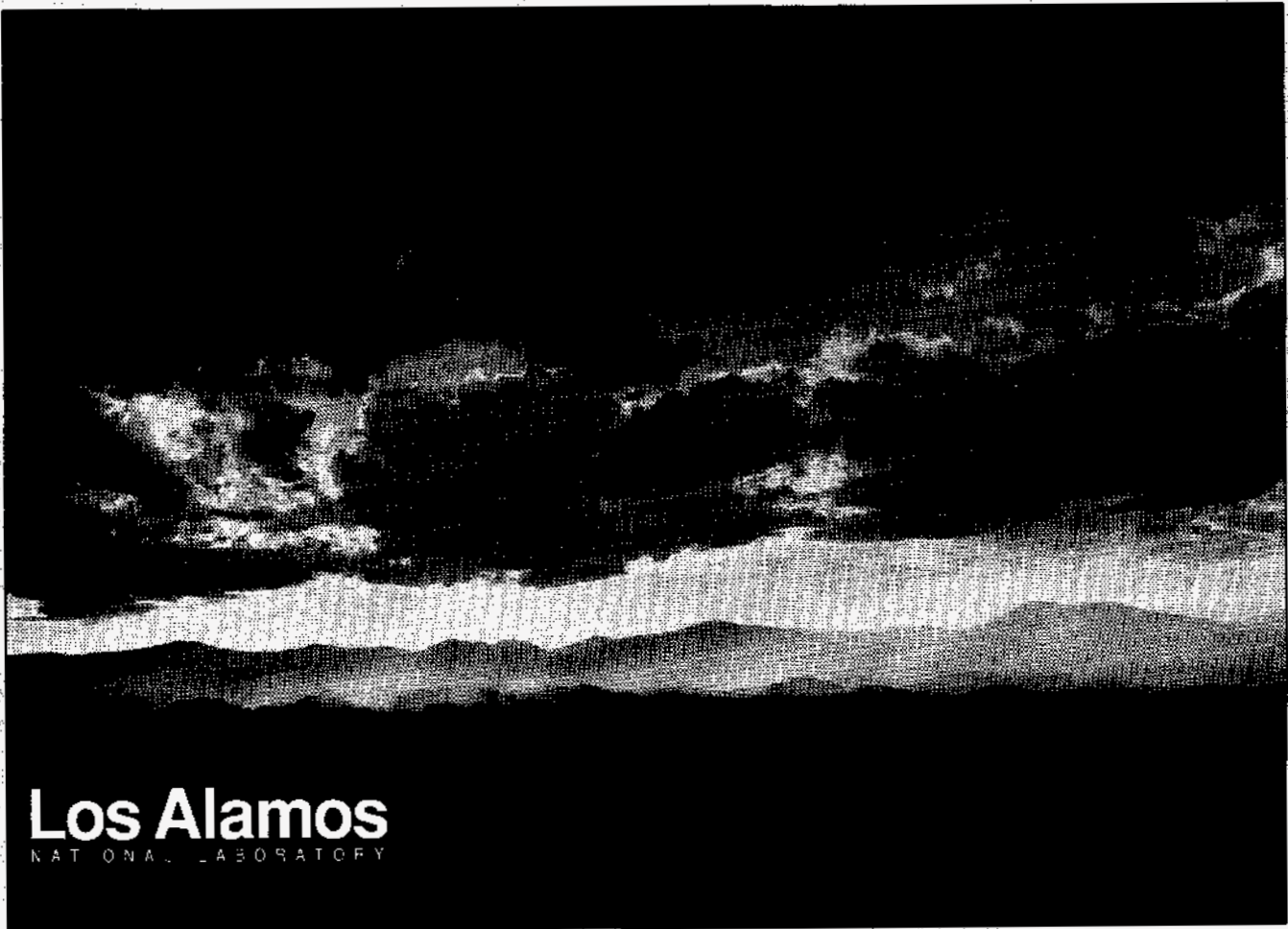
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SUPERCONDUCTING CAVITIES FOR THE APT ACCELERATOR

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Abstract

The design of an Accelerator Production of Tritium (APT) facility being investigated at Los Alamos includes a linear accelerator using superconducting rf-cavities for the acceleration of a high-current cw proton beam. For electron accelerators with particles moving at the speed of light ($\beta \approx 1.0$), resonators with a rounded shape, consisting of ellipsoidal and cylindrical sections, are well established. They are referred to as "elliptical" cavities. For the APT-design, this shape has been adapted for much slower proton beams with β ranging from 0.60 to 0.94. This is a new energy range, in which resonators of an elliptical type have never been used before. Simulations with the well-proven electromagnetic modeling tools MAFLA and SUPERFISH were performed. The structures have been optimized for their rf and mechanical properties as well as for beam dynamics requirements. The TRAK_RF simulation code is used to investigate potential multipacting in these structures. All the simulations will be put to a final test in experiments performed on single cell cavities that have started in our structures laboratory.

1 THE CAVITY SHAPE

Superconducting 5-cell cavities at a π -mode frequency of 700 MHz will be used for the major part of the APT facility. Due to the large velocity acceptance of these cavities only structures for two values of β (0.64 and 0.82) are needed [1]. For each value of β two different cross-sections have been determined, one for the mid-cells and one for the end-cells, where compensation for field penetration into the attached beam-pipe is required. The choice of cavity shape made use of previous design experience at other labs, including Cornell, KEK and DESY [2]. Figure 1 shows the shape description for the chosen geometries. The shape of both the medium- β (0.64) and the high- β (0.82) cavities uses elliptically shaped noses, straight side walls and a circular dome. The upright nose ellipses have an aspect ratio of 2:1.

In a first step the shapes of the resonators were determined to minimize electric and magnetic peak surface fields as far as possible. The resulting cavity shapes turned out to lack sufficient mechanical stability. The medium- β structure needed stiffer support to sustain the vacuum load without yielding the material. Encouraged by recent cavity tests at JAERI for a $\beta = 0.5$ superconducting cavity at 500 MHz [3], we revisited the proposed cavity shapes and came up with an improved design that had less steep straight walls while maintaining good performance in terms of rf properties. Table 1 gives the relevant geo-

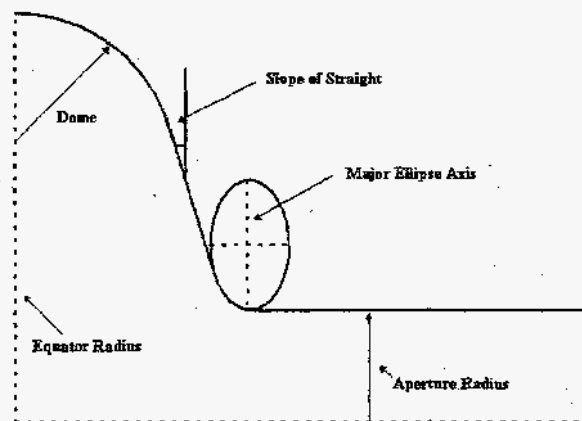


Figure 1: The describing parameters for the elliptical cavity shapes

metric parameters for all 4 shapes. The design procedure used fixed beam-pipe apertures based on beam-dynamics requirements, and fixed straight wall slopes (5 and 7 degrees in the first design and 10 degrees for both β values in the final design). The elliptical noses were varied to find shapes with good peak-fields. The equator radius has been used to tune the cavities to the proper frequency. All other parameters fell into place automatically, assuming smooth transitions between the different parts of the cavity shapes.

β	0.64	0.64	0.82	0.82
cell-type	mid	end	mid	end
aperture[cm]	6.5	6.5	8.0	8.0
equator[cm]	19.95	19.95	20.1	20.1
major axis[cm]	10.00	12.00	14.00	17.80
slope[degree]	10.00	10.00	10.00	10.00
dome[cm]	3.233	2.811	4.969	4.167
cell-length[cm]	13.71	13.71	17.56	17.56

The end-cell geometries use inner half-cells identical to the mid-cells. The outer half-cell uses an equator radius and a cell length identical to the mid-cells, and the elliptical nose and the circular dome radii have been used to retune the cell to the desired 700 MHz.

The simulations have been done on single cavity cells, using π -mode boundary conditions at iris positions where neighboring cells exist. This was sufficient and more efficient in optimizing the cells for the accelerating mode. An investigation of the higher order mode (HOM) spectrum has been done for the full 5-cell geometry. These results will be reported in a separate contribution [4].

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2 PERFORMANCE DATA

The electromagnetic design of the cavity-cells has been done with MAFIA [5] and SUPERFISH [6]. From the electromagnetic fields, a set of secondary quantities has been derived that describe the rf performance of these structures and their interaction with the beam. Table 2 gives the numbers for the most important quantities in a comparison of the mid-cells of the original design with the new shapes with larger side-wall slope.

β	0.64 new	0.64 old	0.82 new	0.82 old
Q_0 [10^{10}]	1.02	1.08	1.34	1.35
Geometry Factor	162	177	213	215
ZT^2/Q [Ω/m]	246	256	297	299
E_{pk}/E_a	2.94	2.96	2.48	2.50
H_{pk}/E_a [G/5MV/m]	355	340	305	303
P_{cav} [W]	8.13	7.32	9.25	9.16

The unloaded Q_0 assumes a surface resistance (R_s) of 15.9 $n\Omega$, ZT^2/Q is the ratio of effective shunt-impedance and Q_0 , E_{pk}/E_a and H_{pk}/E_a give the ratio of peak surface-fields over accelerating gradient ($E_a=E_0T$). P_{cav} is the power dissipated into the cavity by the accelerating mode. These power value reflect the dissipated power to achieve the average accelerating gradient (5.16 MV/m at $\beta=0.64$ and 5.92 MV/m at $\beta=0.82$) for the TM010 π -mode. The transit time factor (T) for a particle with the design- β is 0.78 for all mid-cells.

In terms of the rf-parameters there is only a small difference in performance between both designs. The major driver for switching to the new shapes is the potential gain in structural stability. The increase of power deposited into the medium- β cavities by 10 % does not have a significant effect, since most of the accelerator consists of high- β structures. The results for the end-cells are very similar, the only major difference being the transit time factors that are only 0.59 for the end-cells. This drop is partially compensated by a increase in E_0 , so that E_0T is only about 10 % smaller than for the mid-cells.

3 STRUCTURAL ANALYSIS

Some preliminary structural analysis has been done on 2D models of the cavity shapes [7]. The shapes with the 10 degree slopes in the side-walls seem to be structurally more stable. Both shapes can withstand the vacuum loads without stiffening. The other consideration in applying stiffeners has to do with raising the resonant frequencies of the cavity mechanical modes to decrease the microphonic detuning sensitivity in operation. These studies are continuing. Even if these studies indicate that stiffeners are needed, they can probably be less complex than the conical stiffeners used for our first single-cell test cavity with the original steeper-sloped side-walls.

The choice for a 10-degree slope came from the preliminary 2D structural analysis. The medium- β cavity showed

a clear minimum in von-Mises stresses for a shape with a straight wall slope around 10 degrees (with and without constrained iris). For the high- β cavity this minimum was not so clear, in fact even larger inclinations showed the same stresses as the 10 degree slope did. But, for these larger inclinations the rf performance deteriorated strongly. The peak surface magnetic fields also increased, so did the frequency sensitivity with radius variations.

4 MULTIPACTING

Another concern is the potential for multipacting in these elliptical structures. So far experimental results for cavities with $\beta \approx 0.85$ at Cornell and SACLAY[8], as well as the above mentioned result from JAERI, indicate that there should be no principal problem for such geometries. A final resolution of the multipacting aspect will come from the laboratory tests on single-cell structures that is presently under way in Los Alamos. To support the experimental work, there is a numerical study under way at the University of New Mexico [9]. The TRAK_RF code is being used to investigate the single-cell geometries of both cavity shapes for multipacting susceptibility. First simulations indicate possible multipacting for values of E_a between 2.8 and 4.5 MV/m.

5 SINGLE CELL CAVITY TEST

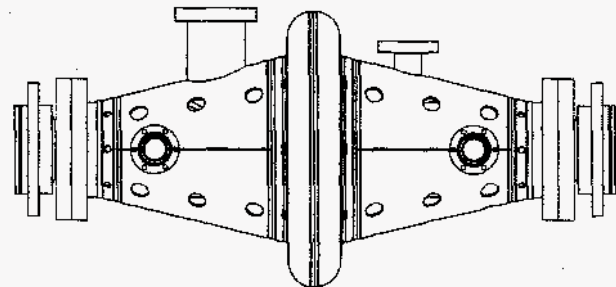


Figure 2: The tested $\beta=0.64$ single-cell cavity with stiffener

In the LANL superconducting structures laboratory we have completed assembly of the equipment for a vertical test of superconducting cavities at 700 MHz under moderate rf power without beam. We are presently testing a single cell cavity at $\beta = 0.64$ with the end-cell shape of the original choice of geometry. This is seen as a meaningful test of the operability of cavities as proposed for the APT facility, since it will provide data on the presence of multipacting in the medium- β structures and it will also provide some field performance data. The end-cell geometry of a multi-cell cavity is more critical in determining performance. This is due to a) the wider elliptical nose that brings the opposing cavity walls closer together than in the mid-cells, and b) the steeper sloped side-walls result in opposing walls that are closer to parallel walls, which increases the potential for two-point multipacting. The cavity uses niobium with a RRR=250 and material of a thickness of 1/8". These spec-

ifications are identical to the ones for the planned accelerator facility.

6 ACKNOWLEDGEMENTS

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7 REFERENCES

- [1] G. Lawrence, T. Wangler, "Integrated Normal-conducting/Superconducting High Power Proton Linac for APT", these proceedings
- [2] D. Proch, (Ed.), "Proceedings of the 5th Workshop on RF Superconductivity", August 19-23, 1991, DESY M-92-01
- [3] Nobuo Ouchi, JAERI, private communication
- [4] Frank L. Krawczyk, "Higher Order Mode Analysis of the APT Superconducting Cavities", these proceedings
- [5] M. Bartsch et al. "Solution of Maxwell's Equations", Computer Physics Comm. 72, 22-39 (1992)
- [6] J. H. Billen and L. M. Young, "POISSON/SUPERFISH on PC Compatibles," Proceedings of the 1993 Particle Accelerator Conference, Vol. 2, p. 790.
- [7] Dale Schrage, LANL, LANSCE-1, private communication
- [8] Henry Safa, SACLAY and Hassam Padamsee, Cornell, private communication
- [9] Stan Humphries, Daniel Rees, "TRAK_RF - Electromagnetic Field and Charged Particle Simulations in RF Devices", these proceedings

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