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# The Fleet Size and Mix Pollution-Routing Problem 

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#### Abstract

This paper introduces the fleet size and mix pollution-routing problem which extends the pollution-routing problem by considering a heterogeneous vehicle fleet. The main objective is to minimize the sum of vehicle fixed costs and routing cost, where the latter can be defined with respect to the cost of fuel and $\mathrm{CO}_{2}$ emissions, and driver cost. Solving this problem poses several methodological challenges. To this end, we have developed a powerful meta- heuristic which was successfully applied to a large pool of realistic benchmark instances. Several analyses have been conducted to shed light on the trade-offs between various performance indicators, including capacity utilization, fuel and emissions and costs pertaining to vehicle acquisition, fuel consumption and drivers. The analyses also quantify the benefits of using a heterogeneous fleet over a homogeneous one.


Keywords: Vehicle routing, fuel consumption, $\mathrm{Co}_{2}$ emissions, heterogeneous fleet, evolutionary metaheuristic.

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## 1. Introduction

Road freight transport is a primary source of greenhouse gases (GHGs) emissions such as carbon dioxide $\left(\mathrm{CO}_{2}\right)$, the amount of which is directly proportional to fuel consumption (Kirby et al., 2000). In the United Kingdom and in the United States, around a quarter of GHGs comes from freight transportation (DfT, 2012; EPA, 2012). Greenhouse gases mainly result from burning fossil fuel, and over $90 \%$ of the fuel used for freight transportation is petroleum-based, which includes gasoline and diesel. These sources account for over half of the emissions from the transportation sector (Kahn Ribeiro et al., 2007).

Demir et al. (2011) have analyzed several models for fuel consumption and greenhouse gas emissions in road freight transportation. Specifically, the authors have compared six models and have assessed their respective strengths and weaknesses. These models indicate that fuel consumption depends on a number of factors that can be grouped into four categories: vehicle, driver, environment and traffic. The pollution-routing problem (PRP), introduced by Bektaş and Laporte (2011), is an extension of the classical vehicle routing problem with time windows (VRPTW). It consists of routing vehicles to serve a set of customers, and of determining their speed on each route segment to minimize a function comprising fuel cost, emissions and driver costs. To estimate pollution, the authors apply a simplified version of the fuel use rate model proposed by Barth et al. (2005), Scora and Barth (2006) and Barth and Boriboonsomsin (2009). The simplified model assumes that in a vehicle trip all parameters will remain constant on a given arc, but load and speed may change from one arc to another. As such, the PRP model approximates the total amount of energy consumed on a given road segment, which directly translates into fuel consumption and further into GHG emissions. Demir et al. (2012) have developed an extended adaptive large neighbourhood search (ALNS) heuristic for the PRP. This heuristic operates in two stages: the first stage is an extension of the classical ALNS scheme to construct vehicle routes (Pisinger and Ropke, 2007; Ropke and Pisinger, 2006a,b) and the second stage applies a speed optimization algorithm (SOA) (Norstad et al., 2010; Hvattum et al., 2013) to compute the speed on each arc. In a later study, Demir et al. (2014a) have introduced the bi-objective PRP which jointly
minimizes fuel consumption and driving time. The authors have developed a bi-objective adaptation of their ALNS-SOA heuristic and compared four a posteriori methods, namely the weighting method, the weighting method with normalization, the epsilon-constraint method and a new hybrid method, using a scalarization of the two objective functions.

The trade-off between minimizing $\mathrm{CO}_{2}$ emissions and minimizing total travel times was studied by Jabali et al. (2012) in the context of the time-dependent vehicle routing problem. The planning horizon was partitioned into two phases: free flow traffic and congestion. The authors solved the problem via a tabu search and proposed efficient bounding procedures. Franceschetti et al. (2013) have later introduced the time-dependent pollution-routing problem where a two-stage planning horizon was used, as in Jabali et al. (2012). Such a treatment has allowed for an explicit modeling of congestion in addition to the PRP objectives. The authors developed an integer linear programming formulation in which vehicle speeds are optimally selected from a set of discrete values. Kopfer and Kopfer (2013) studied the emission minimization vehicle routing problem while considering a heterogeneous fleet. The authors described a mathematical formulation for the problem and computed the $\mathrm{CO}_{2}$ emissions based on the traveled distance. They have presented results of computational experiments performed on small size instances with up to 10 customers. Kwon et al. (2013) considered the heterogeneous fixed fleet vehicle routing problem with the objective of minimizing carbon emissions. They developed a mathematical model enabling them to perform a cost-benefit assessment of the value of purchasing or selling of carbon emission rights. The authors developed tabu search algorithms and suggested that the amount of carbon emission can be reduced without sacrificing the cost because of the benefit obtained from carbon trading. For other relevant references and a state-of-the-art coverage on green road freight transportation, the reader is referred to the survey of Demir et al. (2014b).

In most real-world distribution problems, customer demands are met with heterogeneous vehicle fleets (Hoff et al., 2010). Two major problems belonging to this category are the fleet size and mix vehicle routing problem introduced by Golden et al. (1984), which works with an unlimited heterogeneous fleet, and the heterogeneous fixed fleet vehicle routing problem proposed by Taillard (1999), which works with a known fleet. These two main problems are
reviewed by Baldacci et al. (2008) and Baldacci and Mingozzi (2009). To our knowledge, the fleet size and mix vehicle routing problem combining time windows with the PRP objectives, has not yet been investigated. We believe there is merit in analyzing and solving the fleet size and mix pollution-routing problem (FSMPRP), not only to quantify the benefits of using a flexible fleet with respect to fuel, emissions and the relevant costs, but also to overcome the necessary methodological challenges to solve the problem.

The contributions of this paper are threefold. First, we introduce the FSMPRP as a new PRP variant. The second contribution is to develop a new metaheuristic for the FSMPRP. Our third contribution is to perform analyses in order to provide managerial insights, using the FSMPRP model and several variants. These analyses shed light on the trade-offs between various method components and performance measures, such as distance, fuel and emissions, enroute time and vehicle types. They also highlight and quantify the benefits of using a heterogeneous fleet of vehicles over a homogeneous fleet.

The remainder of this paper is structured as follows. Section 2 presents a background on vehicle types and characteristics. Section 3 provides a formal description of the FSMPRP and the mathematical formulation. Section 4 contains a detailed description of the metaheuristic. Computational experiments and analyses are presented in Section 5, followed by conclusions in Section 6.

## 2. Background on vehicle types and characteristics

Available studies on emission models (e.g., Demir et al., 2011, 2014b) show the significant impact that the vehicle type has on fuel consumption. In a goods distribution context, using smaller capacity vehicles is likely to increase the total distance travelled and may increase $\mathrm{CO}_{2}$ emissions. According to Campbell (1995a,b), if large vehicles are replaced by a larger number of small vehicles, emissions are likely to increase, even though a heavy duty vehicle which has a larger engine consumes more fuel per km than a light duty vehicle. Vehicle type effects the engine friction factor, engine speed, engine displacement, aerodynamics drag, frontal surface area and vehicle drive train efficiency; vehicle curb-weight and payload, i.e., capacity, also play an important role in routing decisions.

In the United Kingdom, the Department of Environment, Food and Rural Affairs (DEFRA, 2007) considers that higher-power engines do not necessarily result in fuel savings, and although these types of engines usually have a larger residual value, they may not be financially advantageous. The effects of curb weight and payload on fuel consumption have been studied by some authors (Bektaş and Laporte, 2011; Demir et al., 2011). The payload of the vehicle has an impact on inertia force, rolling resistance and road slope force. Demir et al. (2011) point out that when compared with light and medium duty, heavy duty vehicles consume significantly more fuel, primarily due to their weight. From the perspective of payload reduction, a study by Caterpillar (2006) has shown that a $4.4 \%$ improvement in fuel savings can be reached through a 4500 kg reduction in payload and in gross weight with respect to an initial weight of 36 tonnes. The corresponding improvement is $8.8 \%$ for an initial weight of 27 tonnes. DEFRA (2012) states that a 17-tonne heavy duty vehicle emits $18 \%$ more $\mathrm{CO}_{2}$ per km when fully loaded, and $18 \%$ less $\mathrm{CO}_{2}$ per km when empty, relative to emissions at half-load.

The curb weight and payload constitute the Gross Vehicle Weight Rating (GVWR) of a vehicle. The United States Federal Highway Administration (FHWA, 2011) has categorized vehicles into three main types according to the GVWR: light duty, medium duty, and heavy duty. In practice, the prominent truck companies produce mainly three vehicle types for distribution (MAN, 2014; Mercedes-Benz, 2014; Renault, 2014; Volvo, 2014). We consider the same vehicle types in this study. Figure 1 shows the three types produced by MAN (2014).

Common parameters (Demir et al., 2012, 2014a; Franceschetti et al., 2013) for all vehicle types and specific parameters for each vehicle type (DfT, 2010; EPA, 2010; Scora and Barth, 2006) are given in Tables 1 and 2, respectively. The United States Environmental Protection Agency (EPA, 2010) provides a standardized set of parameters for several vehicle types indexed by $h$. These include the coefficient of aerodynamics drag $C_{d}^{h}$, the frontal surface area $A^{h}$, the curb weight $w^{h}$ and the maximum payload $Q^{h}$ for the three vehicle types. Values for the engine friction factor $k^{h}$ and the engine speed $N^{h}$ for several types of vehicles are taken from Scora and Barth (2006).


Figure 1: Three vehicle types (MAN, 2014)

Table 1: Vehicle common parameters

| Notation | Description | Typical values |
| :--- | :--- | :--- |
| $\xi$ | fuel-to-air mass ratio | 1 |
| $g$ | gravitational constant $\left(\mathrm{m} / \mathrm{s}^{2}\right)$ | 9.81 |
| $\rho$ | air density $\left(\mathrm{kg} / \mathrm{m}^{3}\right)$ | 1.2041 |
| $C_{r}$ | coefficient of rolling resistance | 0.01 |
| $\eta$ | efficiency parameter for diesel engines | 0.45 |
| $f_{c}$ | fuel and CO ${ }_{2}$ emissions cost $(£ /$ liter $)$ | 1.4 |
| $f_{d}$ | driver wage $(£ / \mathrm{s})$ | 0.0022 |
| $\kappa$ | heating value of a typical diesel fuel $(\mathrm{kj} / \mathrm{g})$ | 44 |
| $\psi$ | conversion factor $(\mathrm{g} / \mathrm{s}$ to $\mathrm{L} / \mathrm{s})$ | 737 |
| $v^{l}$ | lower speed limit $(\mathrm{m} / \mathrm{s})$ | $5.5($ or $20 \mathrm{~km} / \mathrm{h})$ |
| $v^{u}$ | upper speed limit $(\mathrm{m} / \mathrm{s})$ | $27.8($ or $100 \mathrm{~km} / \mathrm{h})$ |
| $\theta$ | road angle | 0 |
| $\tau$ | acceleration $\left(\mathrm{m} / \mathrm{s}^{2}\right)$ | 0 |

Table 2: Vehicle specific parameters (DfT, 2010; EPA, 2010; Scora and Barth, 2006)

| Notation | Description | Light duty (L) | Medium duty (M) | Heavy duty (H) |
| :--- | :--- | :--- | :--- | :--- |
| $w^{h}$ | curb weight (kg) | 4672 | 6328 | 13154 |
| $Q^{h}$ | maximum payload (kg) | 2585 | 5080 | 17236 |
| $f^{h}$ | vehicle fixed cost (£/day) | 41.68 | 59.90 | 93.92 |
| $k^{h}$ | engine friction factor (kj/rev/liter) | 0.25 | 0.20 | 0.15 |
| $N^{h}$ | engine speed (rev/s) | 39 | 33 | 30.2 |
| $V^{h}$ | engine displacement (liter) | 2.77 | 5.00 | 6.66 |
| $C_{d}^{h}$ | coefficient of aerodynamics drag | 0.6 | 0.6 | 0.7 |
| $A^{h}$ | frontal surface area $\left(\mathrm{m}^{2}\right)$ | 9.0 | 9.0 | 9.8 |
| $n_{t f}^{h}$ | vehicle drive train efficiency | 0.40 | 0.45 | 0.50 |

Daily vehicle fixed costs $f^{h}$ are determined according to the United Kingdom Department for Transport (DfT, 2010). These costs combine the capital cost and the annual fixed cost, which itself includes depreciation, repairs and maintenance, tires, insurance and vehicle excise duty. In this paper, we assume that each vehicle route can be completed in one day, so that we can transform the capital and annual cost values into daily costs.

We use the comprehensive emissions model of Barth et al. (2005), Scora and Barth (2006), and Barth and Boriboonsomsin (2008) to estimate fuel consumption and emissions for a given time instant. This model has been succesfully applied to the PRP by Bektaş and Laporte (2011), Demir et al. (2012, 2014a) and Franceschetti et al. (2013). In what follows, we adapt the comprehensive emissions model to account for the heterogeneous fleet case. The fuel consumption rate $F R^{h}$ (liter/s) of a vehicle of type $h$ is given by

$$
\begin{equation*}
F R^{h}=\xi\left(k^{h} N^{h} V^{h}+P^{h} / \eta\right) / \kappa, \tag{1}
\end{equation*}
$$

where the variable $P^{h}$ is the second-by-second engine power output (in kW ) of vehicle type $h$. It can be calculated as

$$
\begin{equation*}
P^{h}=P_{t r a c t}^{h} / n_{t f}^{h}+P_{a c c}, \tag{2}
\end{equation*}
$$

where the engine power demand $P_{a c c}$ is associated with the running losses of the engine and the operation of vehicle accessories such as air conditioning and electrical loads. We assume that $P_{\text {acc }}=0$. The total tractive power requirement $P_{\text {tract }}^{h}(\mathrm{in} \mathrm{kW})$ for a vehicle of type $h$ is

$$
\begin{equation*}
P_{\text {tract }}^{h}=\left(M^{h} \tau+M^{h} g \sin \theta+0.5 C_{d}^{h} \rho A v^{2}+M^{h} g C_{r} \cos \theta\right) v / 1000, \tag{3}
\end{equation*}
$$

where $M^{h}$ is the total vehicle weight (in kg ) and $v$ is the vehicle speed ( $\mathrm{m} / \mathrm{s}$ ). The fuel consumption $F^{h}$ (in liters) of vehicle type $h$ over a distance $d$, is calculated as

$$
\begin{equation*}
F^{h}=k^{h} N^{h} V^{h} \lambda d / v+P^{h} \lambda \gamma^{h} d / v \tag{4}
\end{equation*}
$$

where $\lambda=\xi / \kappa \psi, \gamma^{h}=1 / 1000 n_{t f}^{h} \eta$ and $\alpha=\tau+g \sin \theta+g C_{r} \cos \theta$ are constants. Let
$\beta^{h}=0.5 C_{d}^{h} \rho A^{h}$ be a vehicle-specific constant. Therefore, $F^{h}$ can be rewritten as

$$
\begin{equation*}
F^{h}=\lambda\left(k^{h} N^{h} V^{h} d / v+M^{h} \gamma^{h} \alpha d+\beta^{h} \gamma^{h} d v^{2}\right) . \tag{5}
\end{equation*}
$$

In this expression the first term $k^{h} N^{h} V^{h} d / v$ is called the engine module, which is linear in the travel time. The second term $M^{h} \gamma^{h} \alpha_{i j} d$ is referred to as the weight module, and the third term $\beta^{h} \gamma^{h} d v^{2}$ is the speed module, which is quadratic in speed. These functions will be used in the objective function of our model.

## 3. Mathematical model for the fleet size and mix pollution-routing problem

The FSMPRP is defined on a complete directed graph $\mathcal{G}=(\mathcal{N}, \mathcal{A})$ where $\mathcal{N}=\{0, \ldots, n\}$ is the set of nodes, $\mathcal{A}=\{(i, j): i, j \in \mathcal{N}, i \neq j\}$ is the set of arcs, and node 0 corresponds to the depot. The distance from $i$ to $j$ is denoted by $d_{i j}$. The customer set is $\mathcal{N}_{0}=\mathcal{N} \backslash\{0\}$, and each customer $i$ has a positive demand $q_{i}$. The index set of vehicle types is denoted by $\mathcal{H}$. If a vehicle arrives at customer $i$ before $a_{i}$, it waits until $a_{i}$ before servicing the node. Furthermore, $t_{i}$ corresponds to the service time of node $i \in N_{0}$, which must start within time window $\left[a_{i}, b_{i}\right]$.

The objective of the FSMPRP is to minimize a total cost function encompassing vehicle, driver, fuel and emissions costs. A feasible solution contains a set of routes for a heterogeneous fleet of vehicles that meet the demands of all customers within their respective predefined time windows. Each customer is visited once by a single vehicle, each vehicle must depart from and return to the depot, to serve a quantity of demand that does not exceed its capacity. Furthermore, the speed of each vehicle on each arc must be determined.

The binary variable $x_{i j}^{h}$ is equal to 1 if and only if a vehicle of type $h \in \mathcal{H}$ travels on arc $(i, j) \in \mathcal{A}$. The formulation works with a discretized speed function, proposed by Bektass and Laporte (2011), defined by $R$ non-decreasing speed levels $\bar{v}^{r}(r=1, \ldots, R)$. The binary variable $z_{i j}^{r h}$ is equal to 1 if and only if a vehicle of type $h \in \mathcal{H}$ travels on $\operatorname{arc}(i, j) \in A$ at speed level $r=1, \ldots, R, y_{j}$ is the service start time at $j \in \mathcal{N}_{1}$. The total time spent on a route in which $j \in \mathcal{N}_{0}$ is the last visited node before returning to the depot is defined by
$s_{j}$. Furthermore, let $f_{i j}^{h}$ be the amount of commodity flowing on $\operatorname{arc}(i, j) \in \mathcal{A}$ by a vehicle of type $h$. Therefore, the total load of vehicle of type $h$ on $\operatorname{arc}(i, j)$ is $w^{h}+f_{i j}^{h}$. We now present an integer linear programming formulation for the FSMPRP:

$$
\begin{align*}
\text { (FSMPRP) Minimize } & \sum_{h \in \mathcal{H}} \sum_{(i, j) \in \mathcal{A}} \lambda f_{c} k^{h} N^{h} V^{h} d_{i j} \sum_{r=1}^{R} z_{i j}^{r h} / \bar{v}^{r}  \tag{6}\\
& +\sum_{h \in \mathcal{H}} \sum_{(i, j) \in \mathcal{A}} \lambda f_{c} \gamma^{h} \alpha_{i j} d_{i j}\left(w^{h} x_{i j}^{h}+f_{i j}^{h}\right)  \tag{7}\\
& +\sum_{h \in \mathcal{H}} \sum_{(i, j) \in \mathcal{A}} \lambda f_{c} \beta^{h} \gamma^{h} d_{i j} \sum_{r=1}^{R}\left(\bar{v}^{r}\right)^{2} z_{i j}^{r h}  \tag{8}\\
& +\sum_{j \in \mathcal{N}_{0}} f_{d} s_{j}+\sum_{h \in \mathcal{H}} \sum_{j \in \mathcal{N}_{0}} f_{h} x_{0 j}^{h} \tag{9}
\end{align*}
$$

subject to

$$
\begin{align*}
\sum_{j \in \mathcal{N}_{0}} x_{0 j}^{h} \leq m_{h} & \forall h \in \mathcal{H}  \tag{10}\\
\sum_{h \in \mathcal{H}} \sum_{j \in \mathcal{N}} x_{i j}^{h}=1 & \forall i \in \mathcal{N}_{0}  \tag{11}\\
\sum_{h \in \mathcal{H}} \sum_{i \in \mathcal{N}} x_{i j}^{h}=1 & \forall j \in \mathcal{N}_{0}  \tag{12}\\
\sum_{h \in \mathcal{H}} \sum_{j \in \mathcal{N}} f_{j i}^{h}-\sum_{h \in \mathcal{H}} \sum_{j \in \mathcal{N}} f_{i j}^{h}=q_{i} & \forall i \in \mathcal{N}_{0}  \tag{13}\\
q_{j} x_{i j}^{h} \leq f_{i j}^{h} \leq\left(Q^{h}-q_{i}\right) x_{i j}^{h} & \forall(i, j) \in \mathcal{A}, \forall h \in \mathcal{H}  \tag{14}\\
y_{j}+y_{j}+t_{i}+\sum_{r=1}^{R} d_{i j} z_{i j}^{r h} / \bar{v}^{r} \leq M_{i j}\left(1-x_{i j}^{h}\right) & \forall i \in \mathcal{N}, j \in \mathcal{N}_{0}, i \neq j, \forall h \in \mathcal{H}  \tag{15}\\
\sum_{r=1}^{R} d_{j 0} z_{j 0}^{r h} / \bar{v}^{r} \leq L_{i j}\left(1-x_{j 0}^{h}\right) & \forall j \in \mathcal{N}_{0}  \tag{16}\\
a_{i} \leq y_{i} \leq b_{i} & \forall i \in \mathcal{N}_{0}  \tag{17}\\
\sum_{r=1}^{R} z_{i j}^{r h}=x_{i j}^{h} & \forall(i, j) \in \mathcal{A}, \forall h \in \mathcal{H}  \tag{18}\\
x_{i j}^{h} \in\{0,1\} & \forall(i, j) \in \mathcal{A}, \forall h \in \mathcal{H}  \tag{19}\\
z_{i j}^{r h} \in\{0,1\} & \forall(i, j) \in \mathcal{A}, r=1, \ldots, R, \forall h \in \mathcal{H}  \tag{20}\\
f_{i j}^{h} \geq 0 & \forall(i, j) \in \mathcal{A}, \forall h \in \mathcal{H}  \tag{21}\\
y_{i} \geq 0 & \forall i \in \mathcal{N}, \tag{22}
\end{align*}
$$

The first three terms of the objective function represent the cost of fuel consumption and of $\mathrm{CO}_{2}$ emissions. Term (6) computes the cost induced by the engine module, term (7) reflects the cost induced by the weight module and term (8) measures the cost induced by the speed module. Finally, term (9) computes the total driver wage and the sum of all vehicle fixed costs.

The maximum number of vehicles available for each type is imposed by constraints (10). We consider an unlimited number of vehicles for each vehicle type $h\left(m_{h}=\left|\mathcal{N}_{0}\right|\right)$. Constraints (11) and (12) ensure that each customer is visited exactly once. Constraints (13)
and (14) define the flows. Constraints (15)-(17) are time window constraints, where $M_{i j}=$ $\max \left\{0, b_{i}+s_{i}+d_{i j} / \bar{v}^{r}-a_{j}\right\}$ and $L_{i j}=\max \left\{0, b_{j}+t_{j}+\max _{i}\left\{d_{i j}\right\} / \bar{v}^{r}\right\}$. Constraints (18) impose that only one speed level is selected for each arc. Finally, constraints (19)-(22) enforce the integrality and nonnegativity restrictions on the variables.

## 4. Description of the hybrid evolutionary algorithm

This section describes the proposed hybrid evolutionary algorithm, called HEA++, for the FSMPRP. This algorithm builds on the HEA of Koç et al. (2014), which is itself based on the principles put forward by Vidal et al. (2014). We have developed the Heterogeneous Adaptive Large Neighborhood Search (HALNS) which is used as a main Higher EducaTION component in the HEA++. An adapted version of the speed optimization algorithm (SOA) (Norstad et al., 2010; Hvattum et al., 2013) is applied on a solution within the algorithm to optimize speeds between nodes. The combination of ALNS and SOA has provided good results for the PRP (Demir et al., 2012, 2014a).

The general framework of the HEA++ is sketched in Algorithm 1. The initial population is generated by using a modified version of the classical Clarke and Wright (1964) savings algorithm and the HALNS (line 1). A binary tournament process selects two parents from the population (line 3) and combines them into a new offspring $C$ via crossover (line 4), which then undergoes an improvement step through an advanced Split algorithm called Ssoa(line 5). In the Higher Education procedure, the HALNS with the SOA (line 6) are applied to offspring $C$. If $C$ is infeasible, this procedure is iteratively applied until a modified version of $C$ is feasible, which is then inserted into the population. The probabilities associated with the Higher Education procedure operators are updated by the adaptive weight adjustment procedure (AWAP) (line 7). The Intensification procedure is based on the HALNS and SOA (line 8), and is run on elite solutions. The population size $n_{a}$ is limited by $n_{p}+n_{o}$, where $n_{p}$ is a constant denoting the size of the initial population and $n_{o}$ is a constant showing the maximum allowable number of offsprings that can be inserted into the population. A survivor selection mechanism is applied (line 9) if the populations size $n_{a}$ reaches $n_{p}+n_{o}$ at any iteration. Mutation (line 10) is applied to a
randomly selected individual from the population with probability $p_{m}$ at each iteration of the algorithm. The entire population undergoes a Regeneration (line 11) procedure if there are no improvements in the best known solution for a given number of consecutive iterations $v$. When the number $\varpi$ of iterations without improvement in the incumbent solution is reached, the HEA++ terminates (line 11). For further implementation details on the initialization, parent selection, crossover, AWAP, survivor selection and diversification sections the reader is referred to Koç et al. (2014).

```
Algorithm 1 General framework of the HEA
    Initialization: initialize a population with size \(n_{p}\)
    while number of iterations without improvement \(<\varpi\) do
        Parent selection: select parent solutions \(P_{1}\) and \(P_{2}\)
        Crossover: generate offspring \(C\) from \(P_{1}\) and \(P_{2}\)
        Ssoa: partition \(C\) into routes
        Higher Education: educate \(C\) with HALNS and SOA and insert into population
        AWAP: update probabilities of the HALNS operators
        Intensification: intensify elite solution with HALNS and SOA
        Survivor selection: if the population size \(n_{a}\) reaches \(n_{p}+n_{o}\), then select survivors
        Mutation: diversify a random solution with probability \(p_{m}\)
        if number of iterations without improvement \(=v\) then
            Regeneration: diversify the population with Regeneration procedures
    end while
    Return best feasible solution
```

In what follows we detail the algorithmic features specifically developed for the FSMPRP. The expanded version of the SOA is presented in Section 4.1, SsoA is desribed in Section 4.2, and finally, the Higher Education and Intensification procedures are detailed in Section 4.3.

### 4.1. Speed optimization algorithm

The SOA optimizes the speed on each segment of a given route in order to minimize an objective function comprising fuel consumption costs and driver wages. Demir et al. (2012) adapted the arguments of Norstad et al. (2010) and Hvattum et al. (2013) to the PRP, which we describe here for the sake of completeness.

The SOA is defined on a feasible path $(0, \ldots, n+1)$ of nodes all served by a single vehicle, where 0 and $n+1$ are two copies of the depot. The speed $v_{i-1}$, represents the variable speed between nodes $i-1$ and $i, \underline{e}_{i}$ is the arrival time at node $i$ and $\bar{e}_{i}$ is the departure time from node $i$. The detailed pseude-code of the SOA is shown in Algorithm 2. The SOA starts with a feasible route with initial fixed speeds, it takes input parameters start node $s$ and end node $e, D$ and $T$ which are respectively the total distance and total service time, and returns speed-optimized routes. Initially, the speed $v_{i-1}$, for each link is calculated by considering the total distance of the route and the total trip duration without the total service time (line 4-7). The SOA runs in two stages where the main difference between these stages is the optimal speed $v_{i-1}^{*}$ calculation (line 8). In the first stage, optimal speeds are calculated as

$$
\begin{equation*}
v^{*}=\left(\frac{k^{h} N^{h} V^{h}}{2 \beta^{h} \gamma^{h}}+\frac{f_{d}}{2 \beta^{h} \lambda \gamma^{h} f_{c}}\right)^{1 / 3} \tag{23}
\end{equation*}
$$

which minimizes fuel consumption and driver wage. The first stage fixes the arrival time to the depot and uses this value as an input to the second stage where optimal speeds are calculated using

$$
\begin{equation*}
v^{*}=\left(\frac{k^{h} N^{h} V^{h}}{2 \beta^{h} \gamma^{h}}\right)^{1 / 3} \tag{24}
\end{equation*}
$$

which minimizes fuel consumption in the second stage. The speeds are updated (lines 912) if the vehicle arrives before $a_{i}$ and departs before $b_{i}$ or if the vehicle arrives before $b_{i}$ and departs after $b_{i}+t_{i}$. If node $i$ is the last customer before the depot, the speeds are recalculated to arrive at node $i$ at $a_{i}$ (lines 13-14). If $v_{i-1}$ is lower than $v^{l}$, then it is increased to $v^{l}$, or if it is greater than $v^{u}$, then it is decreased to $v^{u}$ (lines $15-18$ ). The optimal speed is then compared with $v_{i-1}$, if the optimal speed is greater, $v_{i-1}$ is then increased to the optimal speed (lines 19-20). The new arrival and departure times at node $i$ are then calculated (lines 21-23). If the departure time is less than $a_{i}+t_{i}$ or if the arrival time is greater than $b_{i}$, the violation is calculated; otherwise, it is set to zero (lines 24-27). At each iteration, the SOA selects the arc with largest time window violation and eliminates the violation.

```
Algorithm 2 Speed Optimization Algorithm ( \(s, e\) )
    Input: violation \(\leftarrow 0, p \leftarrow 0, D \leftarrow \sum_{i=s}^{e-1} d_{i}, T \leftarrow \sum_{i=s}^{e} t_{i}\)
    Output: Speed optimized routes
    for \(i=s+1\) to \(e\) do
        if \(\underline{e}_{s} \leq a_{s}\) then
            \(v_{i-1} \leftarrow D /\left(\bar{e}_{e}-a_{s}-T\right)\)
        else
            \(v_{i-1} \leftarrow D /\left(\bar{e}_{e}-\underline{e}_{s}-T\right)\)
        \(v_{i-1}^{*} \leftarrow\) Optimal speed by equation (23) or (24)
        if \(\bar{e}_{i-1}+d_{i-1} / v_{i-1}<a_{i}\) and \(\bar{e}_{i} \geq a_{i}+t_{i}\) and \(i \neq n\) then
            \(v_{i-1} \leftarrow d_{i-1} /\left(a_{i}-\bar{e}_{i-1}\right)\)
        else if \(\bar{e}_{i-1}+d_{i-1} / v_{i-1}<b_{i}\) and \(\bar{e}_{i} \geq b_{i}+t_{i}\) and \(i \neq n\) then
            \(v_{i-1} \leftarrow d_{i-1} /\left(b_{i}-\bar{e}_{i-1}\right)\)
        if \(i=n\) and \(\bar{e}_{i} \neq \underline{e}_{i}\) then
            \(v_{i-1} \leftarrow d_{i-1} /\left(a_{i}-\bar{e}_{i-1}\right)\)
        if \(v_{i-1}<v^{l}\) then
            \(v_{i-1} \leftarrow v^{l}\)
        else if \(v_{i-1}>v^{u}\) then
            \(v_{i-1} \leftarrow v^{u}\)
        if \(v_{i-1}^{*}>v_{i-1}\) then
            \(v_{i-1} \leftarrow v_{i-1}^{*}\)
        \(\underline{e}_{i} \leftarrow \bar{e}_{i-1}+d_{i-1} / v_{i-1}\)
        if \(i \neq n+1\) then
            \(\bar{e}_{i}=\underline{e}_{i}+t_{i}\)
        \(g_{i} \leftarrow \max \left\{0, \underline{e}_{i}-b_{i}, a_{i}+t_{i}-\bar{e}_{i}\right\}\)
        if \(g_{i}>\) violation then
            violation \(\leftarrow g_{i}\)
            \(p \leftarrow i\)
    end for
    if violation \(>0\) and \(\underline{e}_{p}>b_{p}\) then
        \(\bar{e}_{p} \leftarrow b_{p}+t_{p}\)
        Speed Optimization Algorithm ( \(s, p\) )
        Speed Optimization Algorithm ( \(p, e\) )
    if violation \(>0\) and \(\bar{e}_{p}<a_{p}+t_{p}\) then
        \(\bar{e}_{p} \leftarrow a_{p}+t_{p}\)
        Speed Optimization Algorithm ( \(s, p\) )
        Speed Optimization Algorithm ( \(p, e\) )
```


### 4.2. The Split algorithm with the speed optimization algorithm

The Split algorithm for heterogeneous vehicle routing problems Prins (2009), takes a giant tour as an input and optimally splits it into vehicle routes. The splitting procedure is based on solving the corresponding shortest path problem. Many extensions of the Split algorithm have been successfully applied in evolutionary based heuristics for several routing problems (Prins, 2009; Vidal et al., 2014; Koç et al., 2014). Koç et al. (2014) have developed an advanced Split algorithm for a heterogeneous fleet. This algorithm was embedded in the HEA to segment a giant tour and to determine the optimal fleet mix through a controlled exploration of infeasible solutions (Cordeau et al., 2001; Nagata et al., 2010). Time windows and capacity violations are penalized through a term in the objective function. Here we introduce a new algorithmic feature, the Split algorithm with the speed optimization algorithm (SSOA) in which we incorporate the SOA within the procedure for computing the cost of each arc in the shortest path problem.

### 4.3. Higher Education and Intensification

The classical ALNS scheme is based on the idea of gradually improving a starting solution by using both destroy and repair operators on a given fleet mix composition. The ALNS in Koç et al. (2014) uses nine removal and three insertion operators, selected from those employed by various authors (Ropke and Pisinger, 2006a,b; Pisinger and Ropke, 2007; Demir et al., 2012; Paraskevopoulos et al., 2008).

The ALNS is essentially a node improvement procedure and therefore does not explicitly account for the heterogenous fleet dimension. In this paper, we propose the HALNS which integrates fleet sizing within the removal and the insertion operators. If a node is removed, we check whether the resulting route can be served by a smaller vehicle and we update the solution accordingly. If inserting a node requires additional vehicle capacity, then we consider the option of using larger vehicles.

We redefine seven removal operators for the destroy phase of the HALNS procedure: worst distance, worst time, neighborhood, Shaw, proximity-based, time-based and demandbased. Furthermore, we redefine three insertion operators for the repair phase: greedy
insertion, greedy insertion with noise function and greedy insertion with en-route time. Each operator has its own specific cost calculation mechanism. Aside from the distance calculations, we account for the difference in the fixed vehicle cost within each operator.

The removal operators iteratively remove nodes, add them to the removal list $L_{r}$, and update the fleet mix composition. The latter operation checks whether a vehicle with a smaller capacity can serve the route after the node removal. The insertion operators iteratively find the least-cost insertion position for node in $L_{r}$, where the cost computation includes the potential use of larger vehicles due to increasing the total demand of the route. Therefore, the insertion operators insert the nodes in their best position while updating the fleet mix composition.

For each node $i \in \mathcal{N}_{0} \backslash L_{r}$, let $f^{h}$ be the current vehicle fixed cost associated with the vehicle serving $i$. Let $\Delta(i)$ be the saving obtained as a result of using a removal operator on node $i$, as defined in the ALNS. Let $f_{r}^{h *}$ be the vehicle fixed cost after removal of node $i$, i.e., $f_{r}^{h *}$ is modified only if the route containing node $i$ can be served by a smaller vehicle when removing node $i$. The saving in vehicle fixed cost can be expressed as $f^{h}-f_{r}^{h *}$. Thus, the total savings of removing node $i \in \mathcal{N}_{0} \backslash L_{r}$, denoted $R C(i)$, is calculated as follows for each removal operator:

$$
\begin{equation*}
R C(i)=\Delta(i)+\left(f^{h}-f_{r}^{h *}\right) \tag{25}
\end{equation*}
$$

Given a node $i \in \mathcal{N}_{0} \backslash L_{r}$ in the destroyed solution, we define the insertion cost of node $j \in L_{r}$ after node $i$ as $\Omega(i, j)$. Let $f_{a}^{h *}$ be the vehicle fixed cost after the insertion of node $i$, i.e., $f_{a}^{h *}$ is modified only if the route containing node $i$ necessitates the use of a larger capacity vehicle after inserting node $i$. The cost difference in vehicle fixed cost can be expressed as $f_{a}^{h *}-f^{h}$. Thus, the total insertion cost of node $i \in \mathcal{N}_{0} \backslash L_{r}$ is $I C(i)$, for each insertion operator is

$$
\begin{equation*}
I C(i)=\Omega(i, j)+\left(f_{a}^{h *}-f^{h}\right) . \tag{26}
\end{equation*}
$$

Figure 2 provides an example of the removal and insertion phases of the HALNS procedure.
Koç et al. (2014) developed a two-phase Intensification procedure whose main idea is to improve the quality of elite individuals through intensifying the search within promising


Figure 2: Illustration of the HALNS procedure
regions of the solutions space. Here we introduce an extended version of this procedure. We apply the HALNS by applying well-performing operators on the elite solutions. Furthermore, we apply the SOA on the intensified elite solutions.

## 5. Computational experiments and analyses

We now summarize the computational experiments performed in order to assess the performance of the HEA ++ . This algorithm was implemented in $\mathrm{C}++$ and run on a computer with one gigabyte of RAM and an Intel Xeon 2.6 GHz processor.

We have used the PRP library of Demir et al. (2012) as the test bed. These instances were derived from real geographical distances of United Kingdom cities and are available at http://www.apollo.management.soton.ac.uk/prplib.htm. From this library, we have selected the four largest sets containing 75, 100, 150 and 200 nodes. Each set includes 20 instances, resulting in a total of 80 instances. These PRP instances are coupled with the parameters listed in Tables 1 and 2 for the FSMPRP. All algorithmic parametric values were set as in Koç et al. (2014), where an extensive meta-calibration procedure was used to generate effective parameter values for the standard heterogeneous fleet vehicle routing problem with time windows.

The aim of the computational experiments is fourfold: (i) to analyse the effect of the
metaheuristic components (Section 5.1), (ii) to test the efficiency of the algorithm for the solution of the PRP and the FSMPRP (Section 5.2), (iii) to empirically calculate the savings that could be achieved by using a comprehensive objective function instead of separate objective functions (Section 5.3), and (iv) to quantify the benefits of using a heterogeneous fleet over a homogeneous one (Section 5.4).

### 5.1. Sensitivity analysis on method components

This section compares four versions of the HEA++. We present four sets of experiments on the 100-node instances, the details of which can be found in Table 3. A "No" for HALNS implies using the ALNS of Koç et al. (2014). Similarly, a "No" for SsoA corresponds to using the Split algorithm without SOA.

Table 3: Sensitivity analysis experiment setup

| Version | HALNS | Ssoa |
| :--- | :--- | :--- |
| $(1)$ | No | No |
| $(2)$ | No | Yes |
| $(3)$ | Yes | No |
| HEA ++ | Yes | Yes |

Table 4 presents the best results of ten runs on the instances for each of the four versions. The first column displays the instances and the other columns show the total cost (TC) in $£$, percentage deterioration in solution quality (Dev) with respect to the HEA++, and the total computational time in minutes (Time). The rows named Avg, Min and Max show the average results, as well as minimum and maximum deviations across all benchmark instances, respectively.

The results clearly indicate the benefits of including the SSOA and HALNS within the HEA++. The HEA++ algorithm is consistently superior to all other three versions on all 20 instances. Version (1) which uses the classical ALNS and Split corresponds to the HEA of Koç et al. (2014), performs worse than all other three versions. The superiority of version (3) over version (2) confirms the importance of the HALNS component in the algorithm. The computation times for all versions are of similar magnitude.

Table 4: Sensitivity analysis of the HEA++ components

| Instance | Version (1) |  |  | Version (2) |  |  | Version (3) |  |  | HEA++ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | TC | Dev | Time | TC | Dev | Time | TC | Dev | Time | TC | Time |
| UK100_01 | 1203.76 | 1.32 | 5.24 | 1197.18 | 0.78 | 5.39 | 1195.98 | 0.68 | 5.52 | 1187.89 | 5.71 |
| UK100_02 | 1151.04 | 1.00 | 4.01 | 1148.38 | 0.78 | 4.16 | 1144.01 | 0.40 | 4.35 | 1139.48 | 4.46 |
| UK100_03 | 1096.31 | 3.04 | 4.18 | 1087.14 | 2.22 | 4.29 | 1068.23 | 0.49 | 4.41 | 1062.96 | 4.48 |
| UK100_04 | 1156.92 | 0.92 | 4.21 | 1156.83 | 0.91 | 4.42 | 1148.18 | 0.17 | 4.71 | 1146.26 | 4.89 |
| UK100_05 | 1157.83 | 2.48 | 3.56 | 1143.93 | 1.29 | 3.67 | 1137.98 | 0.77 | 3.88 | 1129.16 | 4.12 |
| UK100_06 | 1225.73 | 1.44 | 4.59 | 1218.51 | 0.85 | 4.74 | 1210.76 | 0.22 | 5.03 | 1208.13 | 5.12 |
| UK100_07 | 1063.47 | 1.08 | 5.23 | 1060.97 | 0.85 | 5.53 | 1053.67 | 0.16 | 5.61 | 1051.96 | 5.74 |
| UK100_08 | 1138.96 | 3.85 | 3.91 | 1122.98 | 2.48 | 4.01 | 1103.89 | 0.79 | 4.11 | 1095.11 | 4.17 |
| UK100_09 | 1081.50 | 4.43 | 4.13 | 1053.44 | 1.88 | 4.22 | 1041.09 | 0.72 | 4.49 | 1033.63 | 4.65 |
| UK100_10 | 1120.52 | 1.87 | 3.87 | 1103.56 | 0.36 | 2.94 | 1100.91 | 0.12 | 3.06 | 1099.56 | 4.12 |
| UK100_11 | 1236.39 | 1.87 | 4.87 | 1227.01 | 1.12 | 4.01 | 1225.23 | 0.98 | 4.09 | 1213.27 | 5.13 |
| UK100_12 | 1055.21 | 3.38 | 4.13 | 1049.12 | 2.82 | 4.27 | 1049.61 | 2.87 | 4.52 | 1019.50 | 4.62 |
| UK100_13 | 1186.43 | 2.14 | 4.33 | 1183.65 | 1.91 | 4.49 | 1176.08 | 1.27 | 4.62 | 1161.09 | 4.77 |
| UK100_14 | 1248.48 | 1.63 | 4.62 | 1240.22 | 0.97 | 4.77 | 1233.70 | 0.45 | 4.91 | 1228.18 | 5.02 |
| UK100_15 | 1275.38 | 1.95 | 4.67 | 1258.77 | 0.66 | 4.82 | 1253.24 | 0.22 | 4.97 | 1250.50 | 5.09 |
| UK100_16 | 1077.71 | 0.95 | 4.27 | 1070.92 | 0.32 | 4.49 | 1073.02 | 0.51 | 4.55 | 1067.52 | 4.73 |
| UK100_17 | 1250.58 | 1.29 | 3.98 | 1253.00 | 1.48 | 4.11 | 1244.28 | 0.79 | 4.19 | 1234.49 | 4.24 |
| UK100_18 | 1127.36 | 3.52 | 4.34 | 1102.89 | 1.37 | 4.57 | 1089.05 | 0.12 | 4.68 | 1087.74 | 4.91 |
| UK100_19 | 1089.60 | 1.70 | 3.64 | 1086.31 | 1.40 | 3.81 | 1078.04 | 0.64 | 4.99 | 1071.09 | 5.13 |
| UK100_20 | 1241.16 | 3.18 | 3.79 | 1216.49 | 1.22 | 3.87 | 1207.02 | 0.44 | 4.11 | 1201.67 | 4.17 |
| Avg | 1159.22 | 2.15 | 4.28 | 1149.07 | 1.28 | 4.33 | 1141.7 | 0.64 | 4.54 | 1134.46 | 4.76 |
| Min |  | 0.92 |  |  | 0.32 |  |  | 0.12 |  |  |  |
| Max |  | 4.43 |  |  | 2.82 |  |  | 2.87 |  |  |  |

### 5.2. Results on the PRP and on the FSMPRP

To assess the quality of the HEA++, we have compared our algorithm with that of Demir et al. (2012), referred to as (DBL12), by using a homogenous fleet of vehicles with the corresponding vehicle parameters used in the PRP. In Tables 5 and 6, we present the computational results on the PRP instances with 100 and 200 nodes, respectively. The columns show the number of vehicles used in the solution (NV) and the total distance (TD). Ten separate runs were performed for each instance as done by DBL12, the best of which is reported. For each instance, a boldface entry with a "*" indicates a new best-known solution.

The results clearly show that HEA++ outperforms DBL12 on all instances in terms of solution quality. The average cost reduction is $1.60 \%$ for 100 -node instances, for which the minimum and maximum improvements are $0.32 \%$ and $2.33 \%$, respectively. For 200node instances, the corresponding values are $1.72 \%$ (average), $0.04 \%$ (minimum) and $3.88 \%$ (maximum). On average, the Demir et al. (2012) is faster on the 100 -node instances, however, this difference is less substantial on the 200-node instances.

Table 5: Computational results on the 100-node PRP instances

| Instance | DBL12 |  |  |  | HEA++ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | NV | TD | TC | Time | NV | TD | TC | Dev | Time |
| UK100_01 | 14 | 2914.40 | 1240.79 | 1.54 | 14 | 2795.08 | 1212.72* | -2.31 | 4.37 |
| UK100_02 | 13 | 2690.40 | 1168.17 | 1.64 | 13 | 2660.65 | 1149.16* | -1.65 | 4.67 |
| UK100_03 | 13 | 2531.80 | 1092.73 | 3.47 | 13 | 2487.25 | 1080.87* | -1.10 | 5.29 |
| UK100_04 | 14 | 2438.50 | 1106.48 | 2.49 | 14 | 2374.23 | 1085.66* | -1.92 | 5.13 |
| UK100_05 | 14 | 2328.50 | 1043.41 | 2.65 | 14 | 2256.48 | 1033.19* | -0.99 | 4.93 |
| UK100_06 | 14 | 2782.40 | 1213.61 | 2.23 | 14 | 2733.05 | 1192.67* | -1.76 | 4.83 |
| UK100_07 | 12 | 2463.90 | 1060.08 | 1.71 | 12 | 2412.54 | 1044.58* | -1.48 | 4.51 |
| UK100_08 | 13 | 2597.40 | 1106.78 | 3.49 | 12 | 2524.80 | 1092.67* | -1.29 | 5.67 |
| UK100_09 | 13 | 2219.20 | 1015.46 | 2.57 | 13 | 2204.89 | 992.36* | -2.33 | 4.97 |
| UK100_10 | 12 | 2510.10 | 1076.56 | 3.32 | 12 | 2432.26 | 1063.05* | -1.27 | 5.64 |
| UK100_11 | 15 | 2792.10 | 1210.25 | 1.79 | 14 | 2722.22 | 1200.53* | -0.81 | 4.11 |
| UK100_12 | 12 | 2427.30 | 1053.02 | 3.44 | 12 | 2336.10 | 1030.17* | -2.22 | 5.64 |
| UK100_13 | 13 | 2693.10 | 1154.83 | 1.47 | 13 | 2589.17 | 1132.02* | -2.01 | 3.49 |
| UK100_14 | 14 | 2975.30 | 1264.50 | 1.53 | 14 | 2892.45 | 1241.31* | -1.87 | 4.29 |
| UK100_15 | 15 | 3072.10 | 1315.50 | 1.85 | 15 | 3038.40 | 1311.36* | -0.32 | 3.87 |
| UK100_16 | 12 | 2219.70 | 1005.03 | 4.25 | 12 | 2203.99 | 986.57* | -1.87 | 5.97 |
| UK100_17 | 15 | 2960.40 | 1284.81 | 2.55 | 15 | 2860.97 | 1257.44* | -2.18 | 4.19 |
| UK100_18 | 13 | 2525.20 | 1106.00 | 1.54 | 13 | 2506.71 | 1088.89* | -1.57 | 4.21 |
| UK100_19 | 13 | 2332.60 | 1044.71 | 1.52 | 13 | 2288.50 | 1024.17* | -2.01 | 4.19 |
| UK100_20 | 14 | 2957.80 | 1263.06 | 3.41 | 14 | 2915.17 | 1249.84* | -1.06 | 5.17 |
| Avg | 13.4 | 2621.61 | 1141.29 | 2.42 | 13.3 | 2561.75 | 1123.46 | -1.60 | 4.76 |
| Min |  |  |  |  |  |  |  | -2.33 |  |
| Max |  |  |  |  |  |  |  | -0.32 |  |
| Processor | Xe 3.0 GHz |  |  |  | Xe 2.6 GHz |  |  |  |  |
| Runs | 10 |  |  |  | 10 |  |  |  |  |

Table 6: Computational results on the 200-node PRP instances

| Instance | DBL12 |  |  |  | HEA++ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | NV | TD | TC | Time | NV | TD | TC | Dev | Time |
| UK200_01 | 28 | 4609.60 | 2111.70 | 12.10 | 28 | 4545.77 | 2067.00* | -2.16 | 14.20 |
| UK200_02 | 24 | 4444.40 | 1988.64 | 17.00 | 25 | 4332.62 | 1953.35* | -1.81 | 15.80 |
| UK200_03 | 27 | 4439.90 | 2017.63 | 6.74 | 28 | 4365.82 | 1996.13* | -1.08 | 10.40 |
| UK200_04 | 26 | 4191.90 | 1934.13 | 6.86 | 26 | 4151.74 | 1905.88* | -1.48 | 9.47 |
| UK200_05 | 27 | 4861.90 | 2182.91 | 15.40 | 27 | 4848.28 | 2151.99* | -1.44 | 16.80 |
| UK200_06 | 27 | 3980.40 | 1883.22 | 7.51 | 27 | 3980.03 | 1859.40* | -1.28 | 11.50 |
| UK200_07 | 27 | 4415.30 | 2021.95 | 15.70 | 27 | 4276.06 | 1974.32* | -2.41 | 17.90 |
| UK200_08 | 27 | 4664.40 | 2116.76 | 7.17 | 27 | 4592.54 | 2088.12* | -1.37 | 9.17 |
| UK200_09 | 25 | 4031.10 | 1894.18 | 9.22 | 25 | 3932.44 | 1823.50* | -3.88 | 11.70 |
| UK200_10 | 28 | 4921.80 | 2199.95 | 8.33 | 27 | 4847.08 | 2166.59* | -1.54 | 9.78 |
| UK200_11 | 27 | 4099.50 | 1941.19 | 14.10 | 27 | 4126.44 | 1908.83* | $-1.70$ | 16.30 |
| UK200_12 | 25 | 4808.50 | 2105.14 | 11.90 | 26 | 4786.39 | 2104.40* | -0.04 | 12.80 |
| UK200_13 | 25 | 4760.30 | 2141.26 | 7.41 | 25 | 4734.21 | 2094.48* | -2.23 | 9.37 |
| UK200_14 | 27 | 4369.90 | 2011.35 | 7.51 | 27 | 4369.86 | 1994.49* | -0.85 | 10.30 |
| UK200_15 | 25 | 4723.90 | 2110.86 | 9.04 | 26 | 4642.58 | 2067.48* | -2.10 | 11.40 |
| UK200_16 | 27 | 4545.90 | 2075.83 | 7.59 | 27 | 4497.75 | 2023.55* | -2.58 | 9.71 |
| UK200_17 | 26 | 4972.80 | 2218.28 | 6.82 | 26 | 4915.18 | 2165.34* | -2.44 | 8.97 |
| UK200_18 | 27 | 4370.30 | 2004.68 | 13.20 | 27 | 4406.10 | 2003.75* | -0.05 | 14.00 |
| UK200_19 | 25 | 3995.40 | 1844.90 | 16.20 | 25 | 3946.49 | 1803.56* | -2.29 | 17.50 |
| UK200_20 | 27 | 4805.40 | 2150.57 | 8.85 | 26 | 4727.98 | 2114.31* | -1.71 | 11.30 |
| Avg | 26.35 | 4500.60 | 2047.76 | 10.40 | 26.45 | 4451.27 | 2013.32 | $-1.72$ | 12.40 |
| Min |  |  |  |  |  |  |  | $-3.88$ |  |
| Max |  |  |  |  |  |  |  | -0.04 |  |
| Processor | Xe 3.0 GHz10 |  |  |  | Xe 2.6 GHz |  |  |  |  |
| Runs |  |  |  |  | 10 |  |  |  |  |

Table 7 presents the average results obtained by HEA++ on the $75,100,150$ and 200node FSMPRP instances. For each instance set, the columns display the average fuel and $\mathrm{CO}_{2}$ emissions cost (FEC), driver cost (DC) and vehicle cost (VC). To evaluate the environmental impact of the solutions, we also report the average amount of $\mathrm{CO}_{2}$ emissions (in kg ) based on the assumption that one liter of gasoline contains 2.32 kg of $\mathrm{CO}_{2}$ (Coe, 2005). For detailed results, the reader is referred to Tables A.1-A. 4 in the appendix, where ten runs were performed for each instance and the best one is reported. We observe that on average, over all benchmark instances, the vehicle fixed cost accounts for $48.30 \%$ of the total cost, whereas the driver cost represents $31.85 \%$ of the total, and the fuel and emissions cost accounts for $19.85 \%$.

Table 7: Average results on the FSMPRP instances

| Instance | TD | $\mathrm{CO}_{2}$ | FEC | DC | VC | TC | Time |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 75-node | 1628.72 | 320.83 | 193.61 | 288.64 | 421.81 | 904.06 | 3.33 |
| 100-node | 1955.21 | 390.69 | 235.76 | 363.63 | 535.07 | 1134.46 | 4.76 |
| 150-node | 2563.83 | 536.59 | 323.80 | 523.65 | 798.55 | 1646.01 | 6.94 |
| 200-node | 3023.96 | 646.49 | 390.13 | 657.58 | 1026.56 | 2074.28 | 10.60 |

### 5.3. The effect of cost components

This section analyzes the implications of using different cost components on the performance measures. To this end, we have conducted experiments using four different objective functions, which are presented in the rows of Table 8. The experiments were conducted on a 100-node FSMPRP instance, and the best results collected over 10 runs are reported for each of four performance measures which we will now define. In min TD, we consider the objective of minimizing the total distance. In min FEC, we only consider fuel and emissions cost. This setting also implies minimizing $\mathrm{CO}_{2}$ since this is proportional to fuel consumption. In min DC , we account only for the driver cost. The min $\mathrm{TD}+\mathrm{VC}$ objective corresponds to the standard heterogeneous vehicle routing problems, which consists of minimizing distance and vehicle fixed costs. Finally we present the FSMPRP objective. Aside from the objective function values, we provide the main cost components in Table 8. In Table 9, we report the deviations from the smallest cost components shown in Table 8. For example, the minimum value for the total distance objective (min TD) is 2036.78 km , but the FEC objective yields
a solution with a total distance of 2241.20 km , corresponding to an increase of $10.04 \%$. It is clear that considering only distance in the objective results in a poor total cost performance, yielding a $8.35 \%$ increase. This increase is more substantial when looking only at the vehicle fixed cost where min TD is $14.71 \%$ higher in terms of VC. With respect to $\mathrm{CO}_{2}$ emissions, the closest objective value is min TD+VC. This result implies that a substantial gain in $\mathrm{CO}_{2}$ emissions can be achieved by using the TD+VC objective. However, minimizing $\mathrm{CO}_{2}$ emissions yields an average increase of $2.98 \%$ in TC. Similar to the TD objective, the DC objective performs poorly on all cost components, yielding an average increase of $11.04 \%$ in the $\mathrm{CO}_{2}$ emissions.

Table 8: The effect of cost components: objective function values

| Objective | TD | $\mathrm{CO}_{2}$ | FEC | DC | VC | TC |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Min TD (total distance) | $\mathbf{2 0 3 6 . 7 8}$ | 381.57 | 230.26 | 348.36 | 567.70 | 1146.32 |
| Min FEC (fuel and emissions cost) | 2241.20 | $\mathbf{3 4 9 . 6 3}$ | $\mathbf{2 1 0 . 9 8}$ | 391.14 | $\mathbf{4 9 4 . 8 9}$ | 1097.01 |
| Min DC (driver cost) | 2216.51 | 388.21 | 234.26 | $\mathbf{3 4 0 . 5 9}$ | 531.29 | 1106.14 |
| Min TD+VC (total distance+vehicle fixed cost) | 2121.02 | 356.14 | 214.91 | 363.37 | 501.92 | 1080.20 |
| Min TC (total cost) | 2153.69 | 424.61 | 256.23 | 384.42 | 547.24 | $\mathbf{1 0 6 5 . 2 5}$ |

Table 9: The effect of cost components: percent deviation from the minimum value

| Objective | TD | $\mathrm{CO}_{2}$ | FEC | DC | VC | TC |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Min TD (total distance) | $\mathbf{0 . 0 0}$ | 9.14 | 9.14 | 2.28 | 14.71 | 7.61 |
| Min FEC (fuel and emissions cost) | 10.04 | $\mathbf{0 . 0 0}$ | $\mathbf{0 . 0 0}$ | 14.84 | $\mathbf{0 . 0 0}$ | 2.98 |
| Min DC (driver cost) | 8.82 | 11.04 | 11.04 | $\mathbf{0 . 0 0}$ | 7.36 | 3.84 |
| Min TD+VC (total distance+ vehicle fixed cost) | 4.14 | 1.86 | 1.86 | 6.69 | 1.42 | 1.40 |
| Min TC (total cost) | 5.74 | 21.44 | 21.44 | 12.87 | 10.58 | $\mathbf{0 . 0 0}$ |

In order to quantify the added value of changing speeds, we have experimented with three other versions of the FSMPRP in which the speed on all arcs is fixed at 70,85 or 100 $\mathrm{km} / \mathrm{h}$. Table 10 presents the results of these experiments. The results suggest that while optimizing speeds with HEA++ yields the best results, using a fixed speed of $100 \mathrm{~km} / \mathrm{h}$ deteriorates the solution quality by only $1.11 \%$ on average. This makes sense since high driver costs will make it economical to drive fast. On the other hand, using a fixed speed of $70 \mathrm{~km} / \mathrm{h}$ deteriorates the solution value by an average value of $8.82 \%$.

### 5.4. The effect of the heterogeneous fleet

We now analyze the benefit of using a heterogeneous fleet of vehicles as opposed to using a homogenous fleet, coupled with using fixed versus variable speeds. To do so, we have

Table 10: The effect of the speed

| Instance | $70 \mathrm{~km} / \mathrm{h}$ |  |  | $85 \mathrm{~km} / \mathrm{h}$ | $100 \mathrm{~km} / \mathrm{h}$ |  | HEA++ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  | TC | Dev | TC | Dev | TC | Dev | TC |
| UK100_01 | 1290.76 | 8.73 | 1245.29 | 4.90 | 1220.61 | 2.82 | 1187.11 |
| UK100_02 | 1236.40 | 8.55 | 1187.68 | 4.27 | 1153.88 | 1.30 | 1139.02 |
| UK100_03 | 1180.39 | 11.05 | 1107.88 | 4.23 | 1085.54 | 2.12 | 1062.96 |
| UK100_04 | 1257.49 | 9.70 | 1196.63 | 4.39 | 1155.83 | 0.83 | 1146.26 |
| UK100_05 | 1223.57 | 8.36 | 1174.58 | 4.02 | 1148.46 | 1.71 | 1129.16 |
| UK100_06 | 1313.47 | 8.74 | 1245.18 | 3.09 | 1214.73 | 0.56 | 1207.91 |
| UK100_07 | 1148.42 | 9.26 | 1108.36 | 5.45 | 1058.25 | 0.68 | 1051.12 |
| UK100_08 | 1197.86 | 9.47 | 1124.08 | 2.72 | 1104.51 | 0.93 | 1094.28 |
| UK100_09 | 1115.25 | 7.90 | 1079.40 | 4.43 | 1062.79 | 2.82 | 1033.63 |
| UK100_10 | 1185.44 | 7.81 | 1121.09 | 1.96 | 1106.41 | 0.62 | 1099.56 |
| UK100_11 | 1332.62 | 9.84 | 1262.25 | 4.04 | 1221.69 | 0.69 | 1213.27 |
| UK100_12 | 1115.90 | 9.49 | 1048.67 | 2.90 | 1020.83 | 0.17 | 1019.14 |
| UK100_13 | 1249.36 | 7.60 | 1189.02 | 2.41 | 1166.52 | 0.47 | 1161.09 |
| UK100_14 | 1304.27 | 6.20 | 1251.53 | 1.90 | 1229.82 | 0.13 | 1228.18 |
| UK100_15 | 1383.67 | 10.70 | 1306.38 | 4.53 | 1280.94 | 2.49 | 1249.81 |
| UK100_16 | 1133.26 | 6.16 | 1093.13 | 2.40 | 1076.77 | 0.87 | 1067.52 |
| UK100_17 | 1341.49 | 8.67 | 1285.62 | 4.14 | 1247.79 | 1.08 | 1234.49 |
| UK100_18 | 1190.82 | 9.48 | 1109.74 | 2.02 | 1094.05 | 0.58 | 1087.73 |
| UK100_19 | 1172.41 | 9.49 | 1122.23 | 4.80 | 1080.92 | 0.94 | 1070.84 |
| UK100_20 | 1313.20 | 9.28 | 1263.24 | 5.12 | 1206.81 | 0.43 | 1201.67 |
|  |  |  |  |  |  |  |  |
| Average | 1234.30 | 8.82 | 1176.10 | 3.69 | 1146.86 | 1.11 | 1134.24 |
| Min |  | 6.16 |  | 1.91 |  | 0.13 |  |
| Max |  | 11.05 |  | 5.45 |  | 2.82 |  |

conducted three sets of experiments on the 100-node FSMPRP instances, each corresponding to using a unique vehicle type, i.e., only light duty, only medium duty and only heavy duty vehicles. This results in three sets of PRP instances which are solved with the HEA++. We have compared these results with those of the four experiments shown in Table 10. Table 11 provides a summary of this comparison. The columns $\operatorname{Dev}_{70}, \operatorname{Dev}_{85}$ and $\operatorname{Dev}_{100}$ respectively report the percentage increase in total cost as a result of using homogeneous vehicles as in Table 11 over the fixed-speed results shown in Table 10 for 70,85 and $100 \mathrm{~km} / \mathrm{h}$. Similarly, the colums entitled $\mathrm{Dev}_{V}$ show the deviation in total cost between the various homogeneous cases and the FSMPRP, i.e., with HEA++. Table 11 suggests that the total cost increases when using a light duty homogeneous fleet. Compared to the FSMPRP this increase ranges from $24.25 \%$ to $30.64 \%$. For the medium duty case, the total cost increase is on average $4.73 \%$ compared to the FSMPRP. With heavy duty vehicles, the average increase in total cost is $8.15 \%$ compared to the FSMPRP. These results imply that for the homogeneous case, it is preferable to use medium duty vehicles. It is clear that using a heterogeneous fleet of vehicles and optimizing their speeds is superior to using a homogeneous fleet of
vehicles and optimizing their speeds. Table 11 also indicates that using a heterogeneous fleet of vehicles with a fixed speed of $100 \mathrm{~km} / \mathrm{h}$ is better than using a homogeneous fleet of vehicles and optimizing their speeds with respect to the total cost. This implies that for our experimental setting heterogeneous fleet dimension is more important than speed optimization on each arc. The results of column $\operatorname{Dev}_{85}$ show that the FSMPRP with a fixed speed of $85 \mathrm{~km} / \mathrm{h}$ is better in 55 out of the 60 homogeneous cases.

Table 11: The effect of using a heterogeneous fleet

| Instance | Only light duty |  |  |  |  | Only medium duty |  |  |  |  | Only heavy duty |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | TC | $\mathrm{Dev}_{70}$ | $\mathrm{Dev}_{85}$ | $\mathrm{Dev}_{100}$ | $\mathrm{Dev}_{V}$ | TC | $\mathrm{Dev}_{70}$ | $\mathrm{Dev}_{85}$ | $\mathrm{Dev}_{100}$ | $\mathrm{Dev}_{V}$ | TC | $\mathrm{Dev}_{70}$ | $\mathrm{Dev}_{85}$ | $\mathrm{Dev}_{100}$ | $\mathrm{Dev}_{V}$ |
| UK100_01 | 1658.91 | 22.19 | 24.93 | 26.42 | 28.39 | 1260.87 | -2.37 | 1.24 | 3.19 | 5.79 | 1307.32 | 1.27 | 4.74 | 6.63 | 9.14 |
| UK100_02 | 1569.21 | 21.21 | 24.31 | 26.47 | 27.39 | 1163.37 | -6.28 | -2.09 | 0.82 | 2.05 | 1293.82 | 4.44 | 8.20 | 10.80 | 11.90 |
| UK100_03 | 1529.43 | 22.82 | 27.56 | 29.02 | 30.50 | 1132.33 | -4.24 | 2.16 | 4.13 | 6.13 | 1130.16 | -4.44 | 1.97 | 3.95 | 5.95 |
| UK100_04 | 1635.59 | 23.12 | 26.84 | 29.33 | 29.92 | 1220.95 | -2.99 | 1.99 | 5.33 | 6.12 | 1252.83 | -0.37 | 4.49 | 7.74 | 8.51 |
| UK100_05 | 1590.42 | 23.07 | 26.15 | 27.79 | 29.00 | 1210.89 | -1.05 | 3.00 | 5.16 | 6.75 | 1235.66 | 0.98 | 4.94 | 7.06 | 8.62 |
| UK100_06 | 1698.27 | 22.66 | 26.68 | 28.47 | 28.86 | 1255.71 | -4.60 | 0.84 | 3.26 | 3.79 | 1295.24 | -1.41 | 3.86 | 6.22 | 6.73 |
| UK100_07 | 1439.44 | 20.22 | 23.00 | 26.48 | 26.92 | 1114.21 | -3.07 | 0.53 | 5.02 | 5.59 | 1141.42 | -0.61 | 2.90 | 7.29 | 7.84 |
| UK100_08 | 1483.90 | 19.28 | 24.25 | 25.57 | 26.20 | 1141.55 | -4.93 | 1.53 | 3.24 | 4.07 | 1270.47 | 5.72 | 11.50 | 13.10 | 13.80 |
| UK100_09 | 1456.70 | 23.44 | 25.90 | 27.04 | 29.04 | 1104.46 | -0.98 | 2.27 | 3.77 | 6.41 | 1131.25 | 1.41 | 4.58 | 6.05 | 8.63 |
| UK100_10 | 1451.57 | 18.33 | 22.77 | 23.78 | 24.25 | 1134.85 | -4.46 | 1.21 | 2.51 | 3.11 | 1288.89 | 8.03 | 13.00 | 14.2 | 14.70 |
| UK100_11 | 1690.01 | 21.15 | 25.31 | 27.71 | 28.21 | 1256.92 | -6.02 | -0.42 | 2.80 | 3.47 | 1300.90 | -2.44 | 2.97 | 6.09 | 6.74 |
| UK100_12 | 1469.78 | 24.08 | 28.65 | 30.55 | 30.64 | 1104.37 | -1.04 | 5.04 | 7.56 | 7.69 | 1111.47 | -0.4 | 5.65 | 8.15 | 8.27 |
| UK100_13 | 1569.78 | 20.41 | 24.26 | 25.69 | 26.04 | 1168.26 | -6.94 | -1.78 | 0.15 | 0.61 | 1277.46 | 2.20 | 6.92 | 8.68 | 9.11 |
| UK100_14 | 1677.05 | 22.23 | 25.37 | 26.67 | 26.77 | 1270.47 | -2.66 | 1.49 | 3.20 | 3.33 | 1314.17 | 0.75 | 4.77 | 6.42 | 6.54 |
| UK100_15 | 1782.25 | 22.36 | 26.70 | 28.13 | 29.84 | 1305.88 | -5.96 | -0.04 | 1.91 | 4.24 | 1324.95 | -4.43 | 1.40 | 3.32 | 5.62 |
| UK100_16 | 1415.82 | 19.96 | 22.79 | 23.95 | 24.60 | 1109.24 | -2.17 | 1.45 | 2.93 | 3.76 | 1129.15 | -0.36 | 3.19 | 4.64 | 5.46 |
| UK100_17 | 1732.51 | 22.57 | 25.79 | 27.98 | 28.75 | 1336.98 | -0.34 | 3.84 | 6.67 | 7.67 | 1317.94 | -1.79 | 2.45 | 5.32 | 6.33 |
| UK100_18 | 1487.10 | 19.92 | 25.38 | 26.43 | 26.86 | 1137.43 | -4.69 | 2.43 | 3.81 | 4.37 | 1147.04 | -3.82 | 3.25 | 4.62 | 5.17 |
| UK100_19 | 1486.82 | 21.15 | 24.52 | 27.30 | 27.96 | 1115.84 | -5.07 | -0.57 | 3.13 | 4.01 | 1126.37 | -4.09 | 0.37 | 4.04 | 4.91 |
| UK100_20 | 1687.05 | 22.16 | 25.12 | 28.47 | 28.77 | 1272.90 | -3.17 | 0.76 | 5.19 | 5.60 | 1319.91 | 0.51 | 4.29 | 8.57 | 8.96 |
| Avg | 1575.58 | 21.62 | 25.31 | 27.16 | 27.94 | 1190.90 | -3.65 | 1.24 | 3.69 | 4.73 | 1235.82 | 0.06 | 4.78 | 7.14 | 8.15 |
| Min |  | 18.33 | 22.77 | 23.78 | 24.25 |  | -6.94 | -2.09 | 0.15 | 0.61 |  | -4.44 | 0.37 | 3.32 | 4.91 |
| Max |  | 24.08 | 28.65 | 30.55 | 30.64 |  | -0.34 | 5.04 | 7.56 | 7.69 |  | 8.03 | 13.00 | 14.20 | 14.70 |

The final set of experiments we now present aim at providing some insight into the capacity utilization of the vehicle fleet, for both homogenous and heterogeneous cases. In Table 12, we present the capacity utilizations for the three PRP settings of Table 11 as well as for the FSMPRP. The column CU displays the percentage of capacity utilization for the vehicle fleet. In contrast to the total cost, the capacity utilization reaches its maximum level ( $96.01 \%$ ) and a slightly worse level ( $94.89 \%$ ) when using only light duty or medium duty vehicles, respectively. Heavy duty vehicles have approximately six and three times more capacity than light duty and medium duty vehicles, respectively. The average capacity utilization for a heavy-duty only vehicle fleet is $37.47 \%$, but this is probably due to the
limitations imposed by the time window constraints. Using a heterogeneous fleet yields an average utilization of $68.80 \%$, which is a compromise between light and heavy duty vehicles.

Table 12: Capacity utilization rates

| Instance | Only light duty | Only medium duty | Only heavy duty | HEA++ |
| :--- | :--- | :--- | :--- | :--- |
|  | CU | CU | CU | CU |
| UK100_01 | 95.59 | 92.42 | 38.91 | 72.28 |
| UK100_02 | 94.18 | 95.85 | 36.32 | 83.01 |
| UK100_03 | 95.01 | 96.70 | 36.64 | 63.58 |
| UK100_04 | 95.20 | 96.88 | 40.79 | 58.46 |
| UK100_05 | 96.09 | 97.79 | 41.17 | 59.01 |
| UK100_06 | 95.14 | 96.83 | 35.67 | 63.79 |
| UK100_07 | 94.81 | 91.13 | 34.53 | 69.59 |
| UK100_08 | 97.06 | 93.29 | 35.35 | 61.34 |
| UK100_09 | 92.94 | 94.59 | 35.84 | 72.23 |
| UK100_10 | 94.92 | 91.24 | 34.57 | 79.01 |
| UK100_11 | 95.20 | 96.89 | 40.79 | 63.83 |
| UK100_12 | 96.90 | 93.15 | 41.18 | 71.13 |
| UK100_13 | 97.38 | 99.10 | 37.55 | 69.76 |
| UK100_14 | 96.74 | 93.53 | 39.38 | 61.62 |
| UK100_15 | 97.48 | 99.20 | 36.55 | 65.36 |
| UK100_16 | 95.89 | 92.16 | 34.92 | 79.81 |
| UK100_17 | 97.65 | 90.35 | 36.62 | 65.48 |
| UK100_18 | 98.05 | 94.25 | 35.71 | 81.61 |
| UK100_19 | 97.04 | 98.76 | 37.42 | 62.69 |
| UK100_20 | 96.78 | 93.57 | 39.40 | 73.18 |
|  |  |  |  |  |
| Avg | 96.01 | 94.88 | 37.47 | 68.84 |
| Min | 92.94 | 90.35 | 34.53 | 58.46 |
| Max | 98.05 | 99.20 | 41.18 | 83.01 |

## 6. Conclusions

We have presented a hybrid evolutionary metaheuristic for the fleet size and mix pollutionrouting problem (FSMPRP), which extends the pollution-routing problem (PRP) introduced by Bektas and Laporte (2011) and further studied by Demir et al. (2012), to allow for the use of a heterogeneous vehicle fleet. The effectiveness of the algorithm was demonstrated through extensive computational experiments on realistic PRP and FSMPRP instances. These tests have enabled us to assess the effects of several algorithmic components and to measure the trade-offs between various cost indicators such as vehicle fixed cost, distance, fuel and emissions, driver cost and total cost. We have demonstrated the benefit of using a heterogeneous fleet over a homogeneous one. An interesting insight derived from this study is that using a heterogeneous fleet without speed optimization allows for a further reduction in total cost than using a homogeneous fleet with speed optimization. Furthermore, we have shown that using an adequate fixed speed yields results that are only slightly worse than optimizing the speed on each arc. This has a practical implication since it is easier to instruct drivers to hold a constant speed for their entire trip rather than change their speed on each segment.

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## Appendix

Tables A. 1 to A. 4 present the detailed computational results on the FSMPRP instances. Columns TD, $\mathrm{CO}_{2}$, FEC, DC, VC, TC and Time are as explained in the main body of text. Column Mix shows the resulting fleet composition where $L, M$ and $H$ refer to light, medium and heavy vehicles and the subscripts denote the number of such vehicles used in the fleet.

Table A.1: Computational results on the 75 -node FSMPRP instances

| Instance | $\mathrm{HEA}++$ |  |  |  |  | DC | VC | Mix |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  |  | TD | $\mathrm{CO}_{2}$ | FEC | DC | TC | Time |  |
| UK75_01 | 1786.29 | 338.63 | 204.34 | 309.13 | 453.32 | $M^{6} H^{1}$ | 966.79 | 2.98 |
| UK75_02 | 1277.52 | 285.57 | 172.33 | 266.88 | 435.58 | $M^{1} H^{4}$ | 874.78 | 3.34 |
| UK75_03 | 1618.95 | 311.91 | 188.22 | 278.88 | 393.42 | $M^{5} H^{1}$ | 860.52 | 3.45 |
| UK75_04 | 1386.63 | 276.30 | 166.74 | 280.27 | 427.44 | $M^{4} H^{2}$ | 874.45 | 3.89 |
| UK75_05 | 1650.10 | 314.31 | 189.67 | 284.14 | 393.42 | $M^{5} H^{1}$ | 867.23 | 3.19 |
| UK75_06 | 1663.44 | 330.27 | 199.30 | 297.26 | 427.44 | $M^{4} H^{2}$ | 924.01 | 3.04 |
| UK75_07 | 1751.95 | 334.48 | 201.84 | 309.44 | 453.32 | $M^{6} H^{1}$ | 964.59 | 2.95 |
| UK75_08 | 1700.43 | 341.77 | 206.24 | 295.40 | 427.44 | $M^{4} H^{2}$ | 929.07 | 3.16 |
| UK75_09 | 1729.79 | 333.76 | 201.41 | 291.92 | 409.22 | $L^{1} M^{3} H^{2}$ | 902.54 | 3.38 |
| UK75_10 | 1717.70 | 343.15 | 207.08 | 293.39 | 427.44 | $M^{4} H^{2}$ | 927.91 | 3.71 |
| UK75_11 | 1157.88 | 241.64 | 145.82 | 247.30 | 401.56 | $M^{2} H^{3}$ | 794.68 | 3.35 |
| UK75_12 | 1620.67 | 307.32 | 185.45 | 275.90 | 393.42 | $M^{5} H^{1}$ | 854.77 | 3.71 |
| UK75_13 | 1886.06 | 344.59 | 207.94 | 309.79 | 419.30 | $M^{7}$ | 937.03 | 2.84 |
| UK75_14 | 1702.76 | 336.96 | 203.34 | 286.90 | 427.44 | $M^{4} H^{2}$ | 917.68 | 3.38 |
| UK75_15 | 1783.29 | 353.58 | 213.37 | 304.68 | 427.44 | $M^{4} H^{2}$ | 945.49 | 3.39 |
| UK75_16 | 1696.72 | 340.46 | 205.45 | 293.16 | 427.44 | $M^{4} H^{2}$ | 926.04 | 3.74 |
| UK75_17 | 1702.69 | 341.52 | 206.09 | 296.49 | 427.44 | $M^{4} H^{2}$ | 930.02 | 2.59 |
| UK75_18 | 1568.70 | 304.61 | 183.82 | 283.30 | 409.22 | $L^{1} M^{3} H^{2}$ | 876.34 | 3.39 |
| UK75_19 | 1529.44 | 308.81 | 186.35 | 276.51 | 427.44 | $M^{4} H^{2}$ | 890.30 | 3.69 |
| UK75_20 | 1643.34 | 327.00 | 197.33 | 292.08 | 427.44 | $M^{4} H^{2}$ | 916.84 | 3.43 |

Table A.2: Computational results on the 100 -node FSMPRP instances

| Instance | HEA++ |  |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  | TD | $\mathrm{CO}_{2}$ | FEC | DC | VC | Mix | TC | Time |
| UK100_01 | 2153.69 | 424.61 | 256.23 | 384.42 | 547.24 | $M^{6} H^{2}$ | 1187.89 | 5.71 |
| UK100_02 | 2167.57 | 412.24 | 248.76 | 377.49 | 513.22 | $M^{7} H^{1}$ | 1139.48 | 4.46 |
| UK100_03 | 1776.69 | 360.86 | 217.76 | 342.06 | 503.14 | $L^{1} M^{3} H^{3}$ | 1062.96 | 4.48 |
| UK100_04 | 1737.38 | 370.39 | 223.51 | 367.37 | 555.38 | $M^{3} H^{4}$ | 1146.26 | 4.89 |
| UK100_05 | 1695.43 | 360.62 | 217.62 | 356.17 | 555.38 | $M^{3} H^{4}$ | 1129.16 | 4.12 |
| UK100_06 | 1997.50 | 408.01 | 246.22 | 380.66 | 581.26 | $M^{5} H^{3}$ | 1208.13 | 5.12 |
| UK100_07 | 1892.01 | 374.81 | 226.18 | 338.44 | 487.34 | $M^{5} H^{2}$ | 1051.96 | 5.74 |
| UK100_08 | 1984.87 | 399.60 | 241.14 | 350.84 | 503.14 | $L^{1} M^{3} H^{3}$ | 1095.11 | 4.17 |
| UK100_09 | 1746.79 | 346.90 | 209.33 | 336.96 | 487.34 | $M^{5} H^{2}$ | 1033.63 | 4.65 |
| UK100_10 | 2045.48 | 390.15 | 235.43 | 350.91 | 513.22 | $M^{7} H^{1}$ | 1099.56 | 4.12 |
| UK100_11 | 2030.28 | 415.44 | 250.70 | 381.31 | 581.26 | $M^{5} H^{3}$ | 1213.27 | 5.13 |
| UK100_12 | 1699.67 | 340.89 | 205.71 | 326.45 | 487.34 | $M^{5} H^{2}$ | 1019.50 | 4.62 |
| UK100_13 | 2037.36 | 400.80 | 241.86 | 371.99 | 547.24 | $M^{6} H^{2}$ | 1161.09 | 4.77 |
| UK100_14 | 2140.28 | 435.28 | 262.67 | 384.25 | 581.26 | $M^{5} H^{3}$ | 1228.18 | 5.02 |
| UK100_15 | 2187.29 | 446.69 | 269.56 | 399.69 | 581.26 | $M^{5} H^{3}$ | 1250.50 | 5.09 |
| UK100_16 | 1843.10 | 350.41 | 211.46 | 342.84 | 513.22 | $M^{7} H^{1}$ | 1067.52 | 4.73 |
| UK100_17 | 2090.72 | 423.80 | 255.74 | 397.50 | 581.26 | $M^{5} H^{3}$ | 1234.49 | 4.24 |
| UK100_18 | 1966.68 | 370.19 | 223.39 | 351.12 | 513.22 | $M^{7} H^{1}$ | 1087.74 | 4.91 |
| UK100_19 | 1684.15 | 347.29 | 209.57 | 340.16 | 521.36 | $M^{4} H^{3}$ | 1071.09 | 5.13 |
| UK100_20 | 2227.17 | 434.98 | 262.49 | 391.95 | 547.24 | $M^{6} H^{2}$ | 1201.67 | 4.17 |

Table A.3: Computational results on the 150-node FSMPRP instances

| Instance | $\mathrm{HEA}++$ |  |  |  |  | VC | Mix | TC |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  | TD | $\mathrm{CO}_{2}$ | FEC | DC | Time |  |  |  |
| UK150_01 | 2254.43 | 484.03 | 292.09 | 498.34 | 803.12 | $M^{4} H^{6}$ | 1593.54 | 6.32 |
| UK150_02 | 2673.98 | 576.85 | 348.10 | 527.93 | 803.12 | $M^{4} H^{6}$ | 1679.15 | 6.78 |
| UK150_03 | 2257.26 | 478.13 | 288.52 | 487.13 | 769.10 | $M^{5} H^{5}$ | 1544.76 | 7.14 |
| UK150_04 | 2600.08 | 559.99 | 337.92 | 527.45 | 803.12 | $M^{4} H^{6}$ | 1668.50 | 7.27 |
| UK150_05 | 2414.48 | 500.73 | 302.16 | 503.90 | 769.10 | $M^{5} H^{5}$ | 1575.17 | 6.98 |
| UK150_06 | 2205.76 | 470.52 | 283.94 | 502.42 | 803.12 | $M^{4} H^{6}$ | 1589.47 | 7.17 |
| UK150_07 | 2557.91 | 559.32 | 337.52 | 533.68 | 837.14 | $M^{3} H^{7}$ | 1708.34 | 7.34 |
| UK150_08 | 2339.10 | 495.40 | 298.95 | 501.69 | 769.10 | $M^{5} H^{5}$ | 1569.74 | 7.98 |
| UK150_09 | 2945.39 | 574.78 | 346.85 | 555.34 | 820.86 | $M^{9} H^{3}$ | 1723.05 | 6.17 |
| UK150_10 | 2661.32 | 553.75 | 334.16 | 535.16 | 829.00 | $M^{6} H^{5}$ | 1698.33 | 6.93 |
| UK150_11 | 2791.87 | 547.00 | 330.09 | 542.57 | 820.86 | $M^{9} H^{3}$ | 1693.51 | 7.14 |
| UK150_12 | 2644.38 | 584.45 | 352.68 | 544.65 | 837.14 | $M^{3} H^{7}$ | 1734.48 | 7.73 |
| UK150_13 | 2625.97 | 554.80 | 334.79 | 512.67 | 769.10 | $M^{5} H^{5}$ | 1616.56 | 6.48 |
| UK150_14 | 2712.16 | 563.24 | 339.88 | 535.20 | 829.00 | $M^{6} H^{5}$ | 1704.09 | 6.67 |
| UK150_15 | 2258.80 | 460.52 | 277.90 | 492.74 | 735.08 | $M^{6} H^{4}$ | 1505.72 | 7.58 |
| UK150_16 | 2567.02 | 521.84 | 314.90 | 526.68 | 794.98 | $M^{7} H^{4}$ | 1636.56 | 7.07 |
| UK150_17 | 2577.35 | 549.59 | 331.65 | 531.52 | 784.90 | $L^{1} M^{3} H^{6}$ | 1648.07 | 7.09 |
| UK150_18 | 2561.09 | 537.98 | 324.64 | 516.52 | 769.10 | $M^{5} H^{5}$ | 1610.26 | 6.47 |
| UK150_19 | 2670.88 | 573.65 | 346.17 | 534.40 | 803.12 | $M^{4} H^{6}$ | 1683.68 | 6.37 |
| UK150_20 | 2957.40 | 585.24 | 353.17 | 563.05 | 820.86 | $M^{9} H^{3}$ | 1737.07 | 6.09 |

Table A.4: Computational results on the 200-node FSMPRP instances

| Instance | HEA ++ |  |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  | TD | $\mathrm{CO}_{2}$ | FEC | DC | VC | Mix | TC | Time |
| UK200_01 | 2967.79 | 637.11 | 384.46 | 671.73 | 1050.86 | $M^{5} H^{8}$ | 2107.05 | 9.95 |
| UK200_02 | 3005.63 | 618.48 | 373.22 | 633.16 | 982.82 | $M^{7} H^{6}$ | 1989.20 | 11.12 |
| UK200_03 | 2844.29 | 647.64 | 390.82 | 660.37 | 1059.00 | $M^{2} H^{10}$ | 2110.19 | 10.75 |
| UK200_04 | 2886.61 | 608.40 | 367.14 | 644.18 | 1016.84 | $M^{6} H^{7}$ | 2028.15 | 12.71 |
| UK200_05 | 3291.56 | 682.86 | 412.07 | 684.25 | 1042.72 | $M^{8} H^{6}$ | 2139.04 | 10.64 |
| UK200_06 | 2921.60 | 606.84 | 366.20 | 658.34 | 1042.72 | $M^{8} H^{6}$ | 2067.25 | 10.03 |
| UK200_07 | 3030.59 | 644.30 | 388.80 | 664.41 | 1050.86 | $M^{5} H^{8}$ | 2104.07 | 13.26 |
| UK200_08 | 2980.46 | 661.29 | 399.06 | 669.86 | 1024.98 | $M^{3} H^{9}$ | 2093.89 | 8.64 |
| UK200_09 | 2837.70 | 605.41 | 365.33 | 625.16 | 956.94 | $M^{5} H^{7}$ | 1947.43 | 9.19 |
| UK200_10 | 3133.90 | 702.37 | 423.85 | 679.35 | 1059.00 | $M^{2} H^{10}$ | 2162.20 | 11.18 |
| UK200_11 | 2917.55 | 622.01 | 375.35 | 655.46 | 1050.86 | $M^{5} H^{8}$ | 2081.67 | 9.49 |
| UK200_12 | 3220.46 | 679.53 | 410.06 | 655.53 | 1016.84 | $M^{6} H^{7}$ | 2082.43 | 10.83 |
| UK200_13 | 3215.42 | 676.23 | 408.07 | 656.75 | 1016.84 | $M^{6} H^{7}$ | 2081.67 | 9.73 |
| UK200_14 | 3022.87 | 636.42 | 384.05 | 670.17 | 1016.84 | $M^{6} H^{7}$ | 2071.05 | 9.55 |
| UK200_15 | 3212.95 | 663.70 | 400.51 | 659.43 | 982.82 | $M^{7} H^{6}$ | 2042.77 | 11.63 |
| UK200_16 | 2850.53 | 636.69 | 384.21 | 654.70 | 1024.98 | $M^{3} H^{9}$ | 2063.88 | 10.15 |
| UK200_17 | 3199.34 | 688.58 | 415.52 | 664.35 | 1050.86 | $M^{5} H^{8}$ | 2130.74 | 12.27 |
| UK200_18 | 3016.21 | 645.15 | 389.32 | 658.07 | 1050.86 | $M^{5} H^{8}$ | 2098.25 | 9.37 |
| UK200_19 | 2824.05 | 589.57 | 355.78 | 619.55 | 982.82 | $M^{7} H^{6}$ | 1958.15 | 9.79 |
| UK200_20 | 3099.77 | 677.40 | 408.78 | 666.86 | 1050.86 | $M^{5} H^{8}$ | 2126.49 | 11.28 |

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