







The Keck Cosmic Web Imager Integral Field Spectrograph

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Abstract

We report on the design and performance of the Keck Cosmic Web Imager (KCWI), a general purpose optical integral field spectrograph that has been installed at the Nasmyth port of the 10 m Keck II telescope on Maunakea, Hawaii. The novel design provides blue-optimized seeing-limited imaging from 350–560 nm with configurable spectral resolution from 1000–20,000 in a field of view up to $20'' \times 33''$. Selectable volume phase holographic (VPH) gratings and high-performance dielectric, multilayer silver, and enhanced-aluminum coatings provide end-to-end peak efficiency in excess of 45% while accommodating the future addition of a red channel that will extend wavelength coverage to 1 micron. KCWI takes full advantage of the excellent seeing and dark sky above Maunakea with an available nod-and-shuffle observing mode. The instrument is optimized for observations of faint, diffuse objects such as the intergalactic medium or cosmic web. In this paper, a detailed description of the instrument design is provided with measured performance results from the laboratory test program and 10 nights of on-sky commissioning during the spring of 2017. The KCWI team is lead by Caltech and JPL (project management, design, and implementation) in partnership with the University of California at Santa Cruz (camera optical and mechanical design) and the W. M. Keck Observatory (observatory interfaces).

Key words: galaxies: kinematics and dynamics – instrumentation: spectrographs – intergalactic medium – quasars: general – techniques: imaging spectroscopy – techniques: spectroscopic

1. Introduction

In recent years, integral field spectrographs have proliferated at major observatories around the world (Bacon et al. 2001, 2015; Allington-Smith et al. 2002; Larkin et al. 2006; Zurlo et al. 2014). These powerful new instruments produce three-dimensional images in which each image pixel contains full spectral information. They can be optimized for a diverse array of scientific applications from galactic surveys to exoplanet exploration but share common advantages over conventional slit spectrographs: high efficiency, uniform sampling, relaxed pointing, and unmatched survey capability. These features can be combined with a large telescope under dark skies to realize an instrument that is ideally suited for faint, diffuse light astronomical observations. We have conceived of such a spectrograph designed to probe the sky to extremely faint levels ($\sim 1\%$ sky) with minimal systematics by making use of reflective image slicers (Bowen 1938) of novel design combined with the nod-and-shuffle (N&S) technique (Glazebrook & Bland-Hawthorn 2001; Sembach & Tonry 1996) to study faint extended objects such as quasar halos (Martin et al. 2014a), circumgalactic medium

(Rubin et al. 2018), and ultimately, the cosmic web (Martin et al. 2014b) that weaves the universe together.

We are reporting on the design and performance of the Keck Cosmic Web Imager (KCWI), an integral field spectrograph at the 10 m Keck II telescope on Maunakea, Hawaii, that was commissioned on sky in spring 2017. It is a blue-sensitive instrument (350–560 nm) with unique features, including a selectable spectral resolution from $R = 1000$ –20,000 (achieved with three image slicers of different widths combined with a suite of gratings), a deployable N&S detector mask, and a design fully compatible with the future addition of a parallel red channel that will extend the wavelength sensitivity to 1 micron. KCWI was devised as a general purpose spectrograph based on a prototype that has been operating successfully on the Palomar Hale telescope since 2009 (Matuszewski et al. 2010; Martin et al. 2015). In order to generalize the Palomar implementation (Palomar Cosmic Web Imager, or PCWI) for facility use at Keck, we developed a set of top-level requirements to broaden its applicability to the needs of a wide range of likely observers while providing a competitive advantage over other available instruments in specific areas:

1. The instrument should provide broad optical spectral coverage, extending into the technically challenging blue region 350–400 nm while accommodating the phased implementation of a future red channel that would add coverage at higher redshifts.
2. The instrument should provide high spectral resolution in order to enable new science applications at high resolution on small scales, such as the search for globular cluster black holes and studies of the nuclei of active galaxies.
3. The instrument should provide moderate field survey capability, taking advantage of the excellent Maunakea site with a design that fully resolves the available seeing and minimizes background subtraction systematics
4. The instrument should be stable, easily configurable, and operationally straightforward to efficiently make use of the available observing time.
5. The instrument should draw from the technical heritage of the Palomar instrument both as a proof of concept and as a basis for development of the data pipeline.

With these in mind, we designed KCWI based on our Palomar design, but adding elements to improve the imaging capabilities and the range of spectral modes while still fitting into the allowed volume envelope at the observatory.

In this paper, we will describe the instrument design and its performance. In Section 2, we will describe the design of the optics, camera, and detector. In Section 3, we will describe the optical coatings. In Section 4, we describe the instrument pipeline and pipeline products. In Section 5, we describe the instrument performance measured in the laboratory and on sky during commissioning. In Section 6, we present some representative observing examples, and finally in Section 7, we provide a summary and basis for future work.

2. Instrument Design

KCWI is a highly configurable integral field spectrograph that is optimized for seeing-limited observations of faint, diffuse light through the use of the N&S technique in concert with a fixed-gravity bench-mounted structure that minimizes flexure. Its novel optical design includes selectable image slicers and gratings that can provide spectral resolution from 1000–20,000 in a field of regard $20'' \times 8''$ – $34''$ (the selectable field width is inverse to the spectral resolution). Simultaneous pixel-limited imaging and spectral resolution are achieved with the inclusion of a cylindrical wavefront-correcting mirror, while high throughput results from a combination of dielectric, multilayer silver and aluminum coatings, and a blue-optimized Teledyne-e2v (Chelmsford, UK) charge coupled detector (CCD). KCWI has been designed from the ground up as a dual channel instrument; a 530–1050 nm channel can be added by replacing a fold mirror with a dichroic to extend the current 350–560 nm sensitivity.

KCWI operates at the right Nasmyth port of the 10 m Keck II telescope. Figure 1 shows the KCWI instrument during installation at the Keck II telescope. The instrument is one of the largest at the observatory, comparable to DEIMOS (Faber et al. 2003) in volume ($3.0 \times 2.3 \times 3.9 \text{ m}^3$) and weighing approximately 4000 kg. Major mechanisms include a K-mirror field de-rotator, grating exchanger, and camera articulation stage allowing completely remote configuration. A large custom-made steel optical bench (Newport Corporation, Irvine, CA) supports all of the instrument’s components, and three

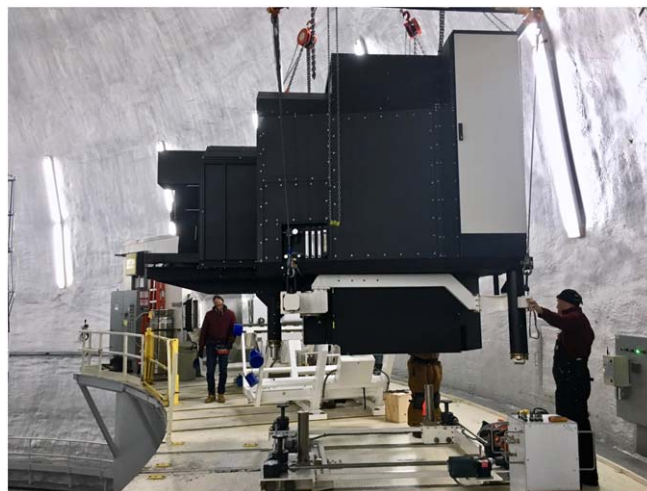


Figure 1. The KCWI instrument during installation at the Keck II telescope in 2017 January.

kinematic mounting points accurately position the instrument at the telescope focus. Transport rails on the Nasmyth platform and deck allow the instrument to be moved between the focal station and a storage location using an attached transport cart.

The instrument is housed in an enclosure and purged with filtered, dry air to protect the optical components (particularly the multilayer silver coatings) from humidity, dust, and other contaminants. Large panels are removable to provide service access. The camera and gratings are mounted on the bottom of the optical bench, while the K-mirror, IFU, and collimating optics are mounted on the top. The electronics are mounted in an electrically shielded, glycol-cooled equipment rack that provides service access to all of the electronics except for the CCD controller, which is mounted near the detector assembly.

The optical layout of KCWI is illustrated in Figure 2, with key design parameters summarized in Table 1. Converging light from the telescope tertiary ($f/13.7$ measured across the vertices of the hexagonal Keck primary) is directed through the instrument protective hatch, which is a $145 \times 135 \text{ mm}$ twin-blade shutter made by Bonn-Shutter UG (Bonn, Germany). The shutter is a spare identical to the one used in the camera and achieves linearity better than 1% for exposures as short as 0.1 s (c.f. Reif et al. 1999). Light continues through an AR-coated, fused silica meniscus entrance window that is designed to operate at its aplanatic conjugate, preserving the quality of the incoming converging beam (c.f. Morrissey 1994) while minimizing ghosting at the focal plane.

The converging beam continues through a K-mirror image de-rotator to deliver a stationary, on-axis, unvignetted $40''$ diameter science field to a selectable image slicer located at the telescope focus. The de-rotator contains three broadband (350–1050 nm) dielectric coated Zerodur (Schott AG, Germany) mirrors, each with an average reflectivity of over 99%. A diagram of the K-mirror assembly is shown in Figure 3. Its structure comprises a pair of weight-relieved steel plates bridged by cylindrical beams and kinematically mounted through three micrometer feet to a steel interface plate, which is in turn bolted to the optical bench. The mechanism is a gear-driven turret structure that is cantilevered off of the rear plate. The turret, which contains the three mirrors, is supported by a turntable bearing. Its motion is monitored by a four-head encoder and optical drum scale read by a Galil 4010 controller

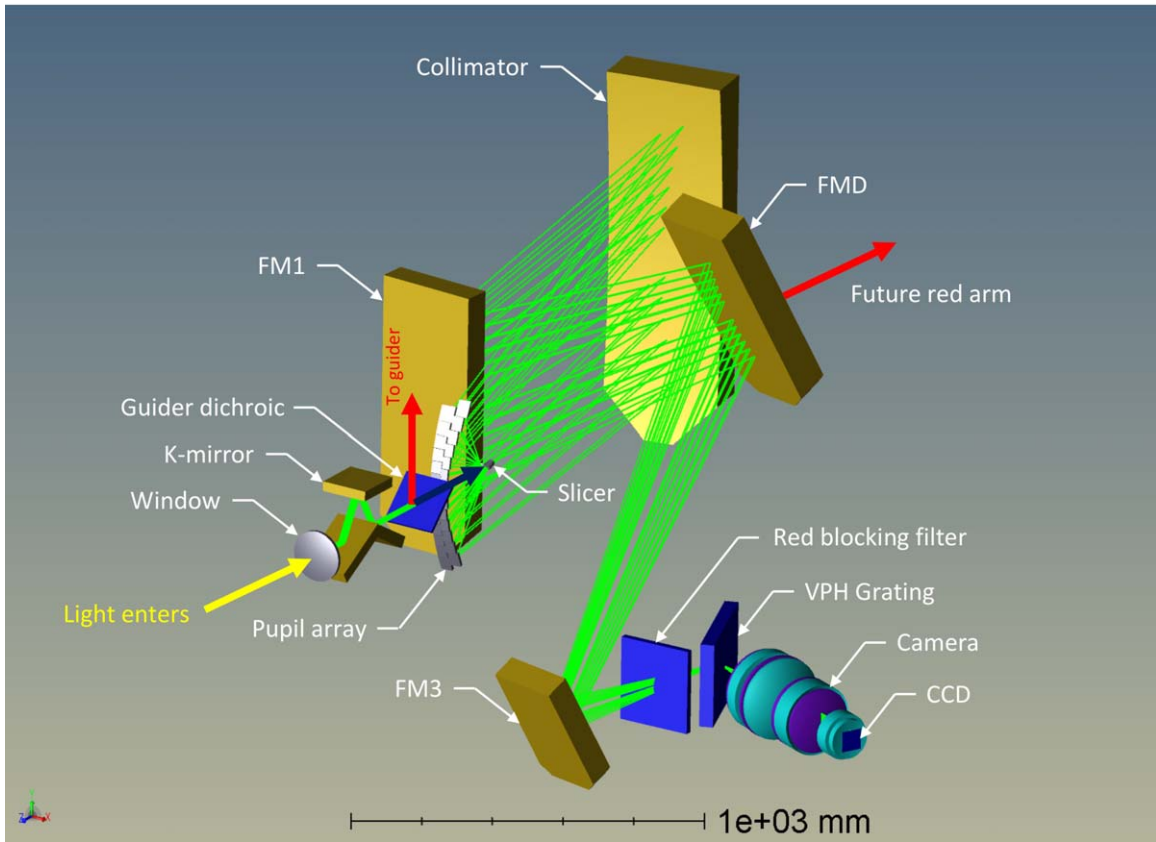


Figure 2. The optical layout of KCWI showing a subset of the optical rays for clarity. The primary mirror is 1.1 m tall for scale. The system forms a hexagonal compound pupil image at the grating that is 160 mm in diameter simultaneously with pixel-limited reimaging of the slicer focal plane at the detector. A parallel red arm can be accommodated by replacing the FMD fold mirror with a dichroic.

with custom firmware. The K-mirror has the property that it rotates the telescope field at twice the speed of its own rotation. An example is shown in Figure 4. A star on the rotational axis of an internally misaligned K-mirror will execute circular motions in the focal plane at the same speed as the mechanism, while a star off the axis (externally misaligned) of a correctly aligned K-mirror will execute circular rotations in the focal plane at twice the rate of the mechanism. Combinations of the two misalignments can produce complex nested circular image motions. Of chief concern in the KCWI implementation is not the image stability at the focal plane, which is corrected in real time by the downstream guider, but rather the residual pointing of the beam inside the instrument, or “beam walk,” which could result in vignetting inside the IFU pupil array.¹¹ In order to ensure that the KCWI K-mirror would be aligned with sufficient precision to avoid this ($\lesssim 30''$), a Monte Carlo simulation of optical ray traces was used to validate the alignment procedure. We determined that beam walk could be reduced to an acceptable level by aligning the three mirrors initially to the FARO-arm (Lake Mary, FL) tolerance ($\lesssim 100$ microns) and then using an On-Trak (Irvine, CA) laser alignment tool to null the image motion with final adjustments of only the KM2 mirror.

A 160 mm square dichroic beamsplitter (Asahi Spectra Co., Japan) with a 630 nm cutoff wavelength is mounted between the rear of the K-mirror and the focal plane. This element reflects red

¹¹ Clearances in the pupil array are as small as 125 microns between the beam footprints and their associated mirror edges. Vignetting in these areas would primarily affect the edges of the field of view.

Table 1
The KCWI Optical Prescription

Parameter	Value	Notes
Design band	350–560 nm	Blue channel
Design focal ratio	13.7	Keck telescope
Telescope Plate Scale	$1''.375 \text{ mm}^{-1}$	
Field of View	$(8.25, 16.5, \text{ or } 33)'' \times 20''$	Selectable
Slit width	$(0.34, 0.69, \text{ or } 1.38)'' \times 24$	Selectable
Window front radius	391.7 mm	Convex, spherical
Window rear radius	382.6 mm	Concave, spherical
IFU radius	225 mm	Focus to vertex
Slice radius	5206 mm	Convex, spherical
Pupil mirror radius	Infinity	
Collimator radius	4345 mm	Concave, spherical
FM1 radius ^a	675 m	Convex, cylindrical
Beam diameter	160 mm	Compound pupil
Camera focal length	304.4 mm	All spherical
Science detector ^b	4096×4112	15 micron pixels
Science detector plate scale	$0''.147 \text{ pixel}^{-1}$	1×1 bins
Focal plane camera	3296×2472	$24''9 \times 18''7$
Guider (Magiq) camera	1024×1024	$3'1 \times 3'1$

Notes.

^a The FM1 cylinder axis is vertical, along the long axis of the mirror.

^b The KCWI detector is a standard Teledyne-e2v CCD231-84 thin, back-illuminated, Astro-BB process CCD.

light to a standard platform-mounted MAGIQ guider (Adkins et al. 2008) with approximately a $2'$ diameter field of view, while blue light is transmitted to the science instrument. The coating performance is described in Section 3. This element would be

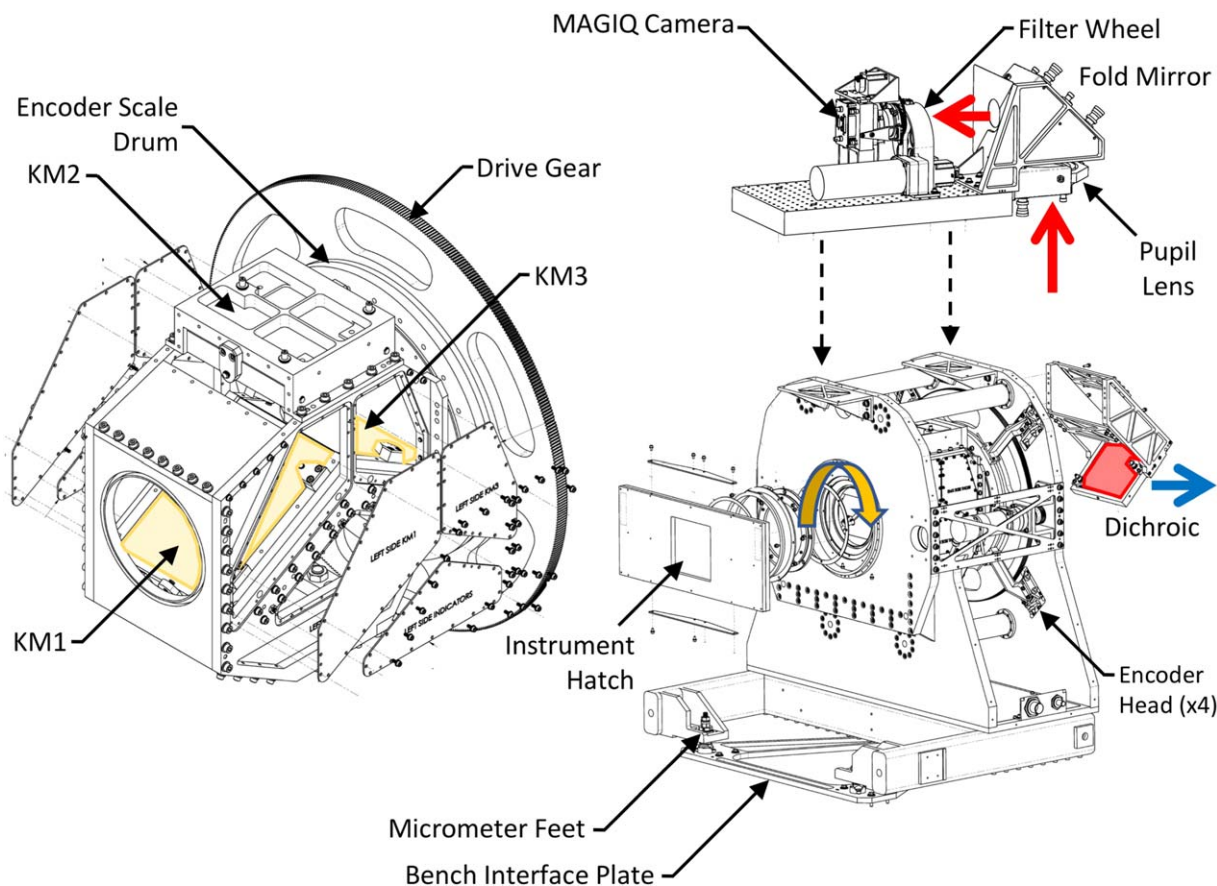


Figure 3. A line drawing of the K-mirror assembly, including the instrument hatch, guider dichroic, and MAGIQ guider. On the left, an expanded view of the rotating turret assembly is shown. Mirrors are kinematically mounted inside the turret and can be adjusted with locking spring plungers that rest on silicon carbide pucks bonded to each mirror surface. On the right, the turret is shown inside the K-mirror assembly. The assembly also supports the guider dichroic, which directs red light to a MAGIQ guider that is bench-mounted onto the top of the structure.

removed to accommodate the addition of a red channel. In the current implementation, the downstream guider location enabled by the dichroic permits measurements of the seasonal performance of the de-rotator necessary to inform any possible change to a guider location upstream of the K-mirror as part of the red channel implementation.

The instrument includes a calibration subsystem as shown in Figure 5. It utilizes a pair of deployable periscopes to inject light through (or after) the guider dichroic to the guider and the science focal planes. The unit employs a reflective Offner relay that reimages a set of movable targets at 1:1 magnification onto the science focal plane. The relay also simulates the hexagonal pupil of the telescope primary with a rotatable mask mounted over the relay secondary mirror. The calibration targets include an array of pinholes, bars, and flat-field elements. The calibration subsystem is illuminated through an integrating sphere by a selectable set of lamps including an LED continuum source, as well as ThAr and FeAr hollow cathode lamps.

The telescope focal plane is divided into 24 slitlets by one of three selectable image slicer elements of the KCWI Integral Field Unit (IFU), which was fabricated by Winlight Optics (Pertuis, France). The slicer mirror stacks provide $0''.35$, $0''.7$, or $1''.4$ spatial resolution (with a corresponding $8''.4$, $16''.8$, or $33''.6$ field of view in one axis and a $20''$ field of view for all configurations in the other axis).

A close-up view of the medium slicer is shown in Figure 6. A mechanical diagram of the IFU subassembly is shown in Figure 7. The image slicers sit on a linear stage that can position one of the three slicers or a focal plane camera (an Allied Vision Technologies Pro Silica GT3300 monochrome camera with an ON Semiconductor KAI-08050 CCD sensor) onto the spectrograph optical axis. The IFU structure comprises a Newport optical bench with Invar face sheets and an aluminum core flexure-mounted to a stainless steel weldment in such a way as to mimic a steel construction that thermally matches the K-mirror assembly.

The Zerodur slicers work in concert with a fixed array of 24 flat “pupil” mirrors to reconfigure the focal plane in reflection into a vertical long slit referred to as the “virtual slit” (Weitzel et al. 1996). The reformatted slicer array reflection, rather than being perfectly vertical, assumes a staircase pattern resulting from the geometry of the pupil array that is required to avoid overlap of the diverging beams of light from the slicer elements. The virtual slit pattern has also been tuned (lateral curvature added) to cancel long slit curvature in images taken with the high-resolution gratings, providing maximum bandwidth on the CCD (limited only by the staircase). This tuning was achieved by weighting the optical merit function to control the position of slice images on the detector in the high spectral resolution configuration. A consequence of this tuning is to add a “reverse” slit curvature in

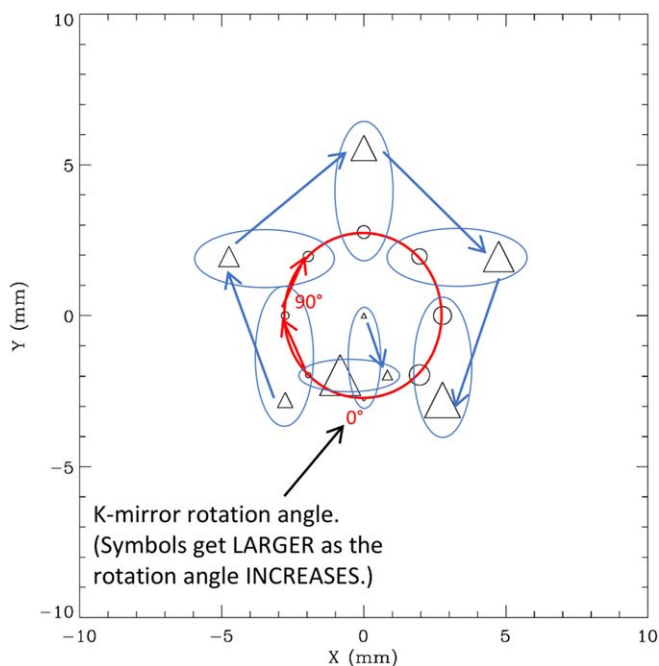


Figure 4. An example of focal plane image motions that result from a combination of internal and external K-mirror misalignments. The circular symbols show the path of a “planet” on the rotational axis of the K-mirror but deflected by an internal misalignment of one of its three mirrors. This planet executes a circle (depicted in red) in the focal plane at the same rate as the K-mirror. The triangular symbols show the path of a “moon” that is off the optical axis of the telescope. This triangular moon “orbits” the planet at twice the rate of the K-mirror. At a K-mirror rotation of 180°, the pattern of the “moon” and “planet” has rotated 360°, but is displaced in the focal plane. In this figure, the size of the symbol is proportional to the K-mirror rotation angle.

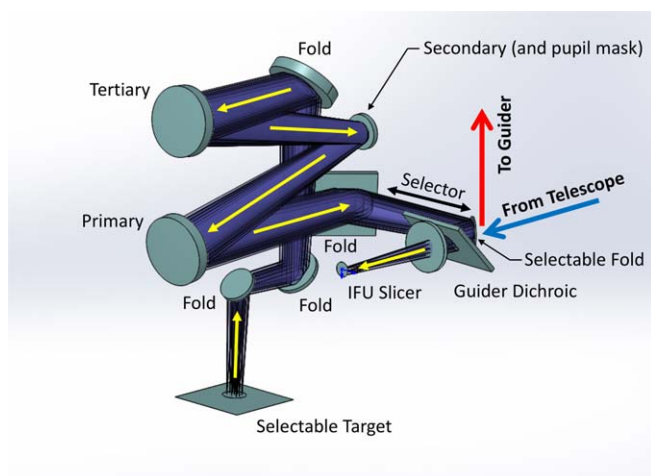


Figure 5. The optical layout of the KCWI Offner relay calibration system. The system reimages a target at 1:1 magnification onto the image slicer through the use of a selectable periscope mirror. The system can simultaneously illuminate the guider and the spectrograph to aid alignment. The relay also creates a hexagonal telescope pupil with a rotatable mask at the secondary mirror that is relayed onto the grating. The selectable calibration target is illuminated through an integrating sphere by either an LED continuum lamp, or by ThAr or FeAr hollow cathode arc lamps.

low-resolution configurations, although this was deemed to be acceptable given the larger bandwidth.

The individual slices are each spherically convex in order to reimagine the telescope pupil onto the grating. Each slice acts as a

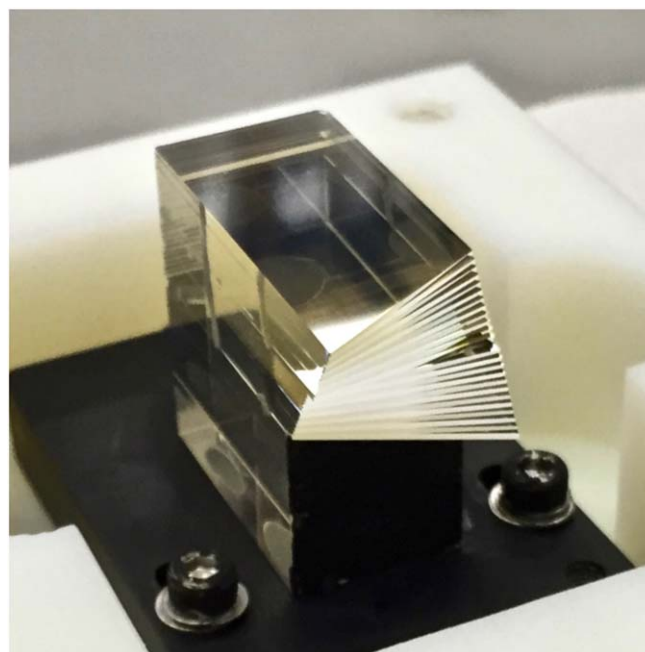


Figure 6. A close-up view of the medium slicer. As shown here, the element is on its side relative to its orientation inside the instrument. This element is made from optically contacted Zerodur. Each of the 24 slitlets is 0.5 mm thick and 14.8 mm tall. The reflective faces are convex with a radius of curvature of 5206 mm. The coating is multilayer enhanced silver.

field lens to form the pupil image, while the IFU works in concert to ensure the 24 individual pupil images are simultaneously co-aligned on the grating to form a compound pupil image. This configuration ensures that the minimum area of the grating–camera system is used, maximizing image quality while minimizing the required grating and camera sizes. The pupil relay system is illustrated in Figure 8. It can be interpreted as a Schmidt camera in reverse, with the “entrance” at the location of the compound pupil on the grating, which is formed at the radius of curvature of the spectrograph collimator. On the other side of the relay, the IFU virtual slit, which is curved reminiscent of a Schmidt camera focal plane, is formed at the collimator focal point. The virtual slit curvature is three dimensional as shown in Figure 9: a “C-”shaped track of 24 slitlets along the surface of a sphere roughly equal in radius to the collimator focal length. The diverging light from the virtual slit proceeds to a spherical collimator and then to a series of three fold mirrors.

The large rectangular Zerodur optical elements range in height from 1.1 m (COL) to 400 mm (FM3), decreasing as the collimated virtual slit converges to the compound pupil image located at the grating. The mirrors are each bonded to a set of three three-point semi-kinematic Invar whiffle trees (nine bonded locations) that are flexure-mounted to tubular steel weldments as shown in Figure 10. There are two similar optical mount designs to accommodate vertical (COL, FM1) and tilted (FMD, FM3) mirrors. Both designs provide weight relief to the heavy mirrors through sets of bonded gravity offloading suspension springs. One can think of the mirrors suspended from the springs and then clamped into position by a kinematic interface. Prior to bonding, the Zerodur and Invar surfaces were abraded with 220 grit silicon carbide and water until uniform in appearance. The parts were rinsed in water and flushed with acetone and alcohol prior to being coated with Dow Corning

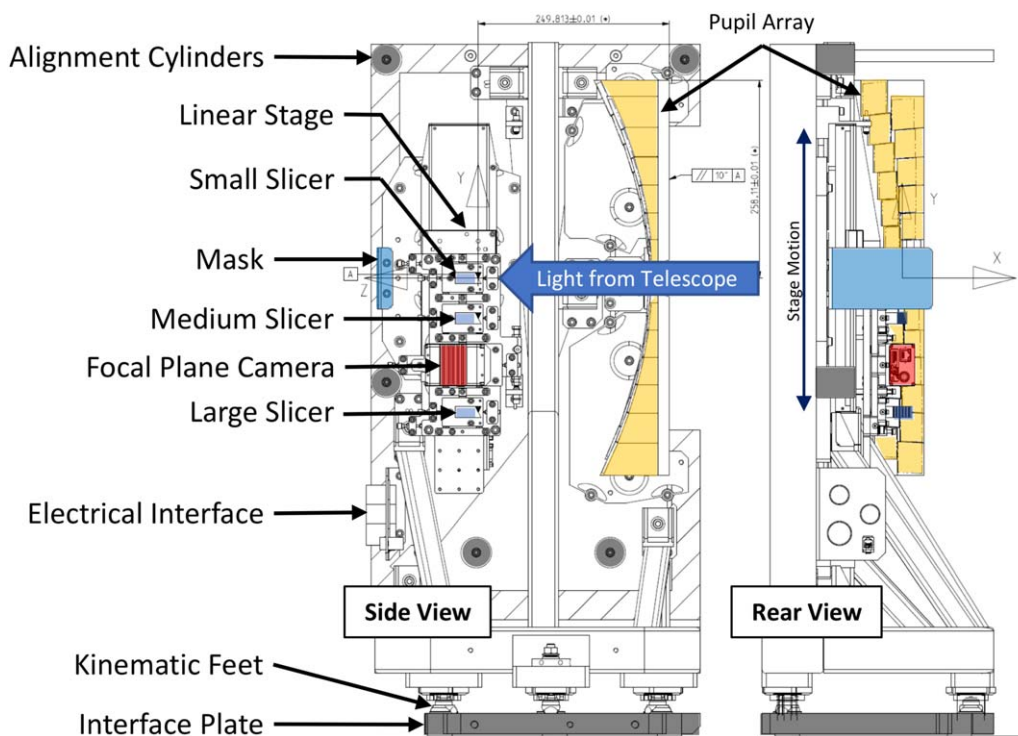


Figure 7. Side and rear views of the KCWI optomechanical integral field unit assembly. One of three image slicers or a direct imaging camera can be placed in the optical path by a linear stepper motor. The slicer elements are reconfigured in reflection behind the pupil array into a long virtual slit that is reimaged and dispersed by the spectrograph.

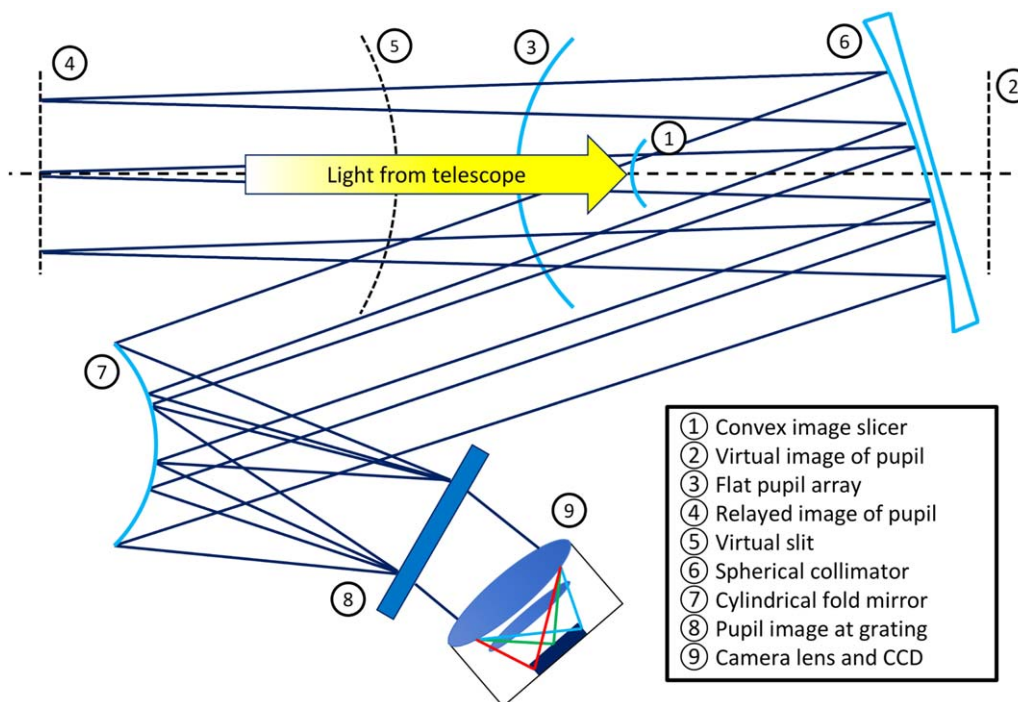


Figure 8. The KCWI pupil relay system, which images the telescope primary mirror onto the instrument grating surface in parallel with the spectrograph slit relay, which images the slicer elements onto the detector. 1: Light from the telescope arrives at the convex reflective slicer. 2: The virtual image of the telescope pupil is located behind the slicer. 3: The array of 24 flat pupil mirrors. 4: The virtual image of the telescope pupil as relayed by the pupil mirrors. 5: The virtual slit is formed by the pupil mirrors and located behind the pupil array. 6: The spherical spectrograph collimator. 7: The wavefront-correcting cylindrical fold mirror. 8: The compound pupil image is formed at the grating, which is located at the radius of the collimator. 9: The camera lens forms an image of the virtual slit on the detector.

(Auburn, MI) Z-6020 Silane primer (0.5% solution in ethanol). Approximately 30 minutes after priming, the parts were bonded with Armstrong A12 epoxy (Henkel Corporation, Westlake,

OH) mixed 1.5:1 with 1% 180 micron glass beads added by weight to set the bond line. Squeeze-out was carefully removed to eliminate the possibility of high-CTE epoxy fracturing the

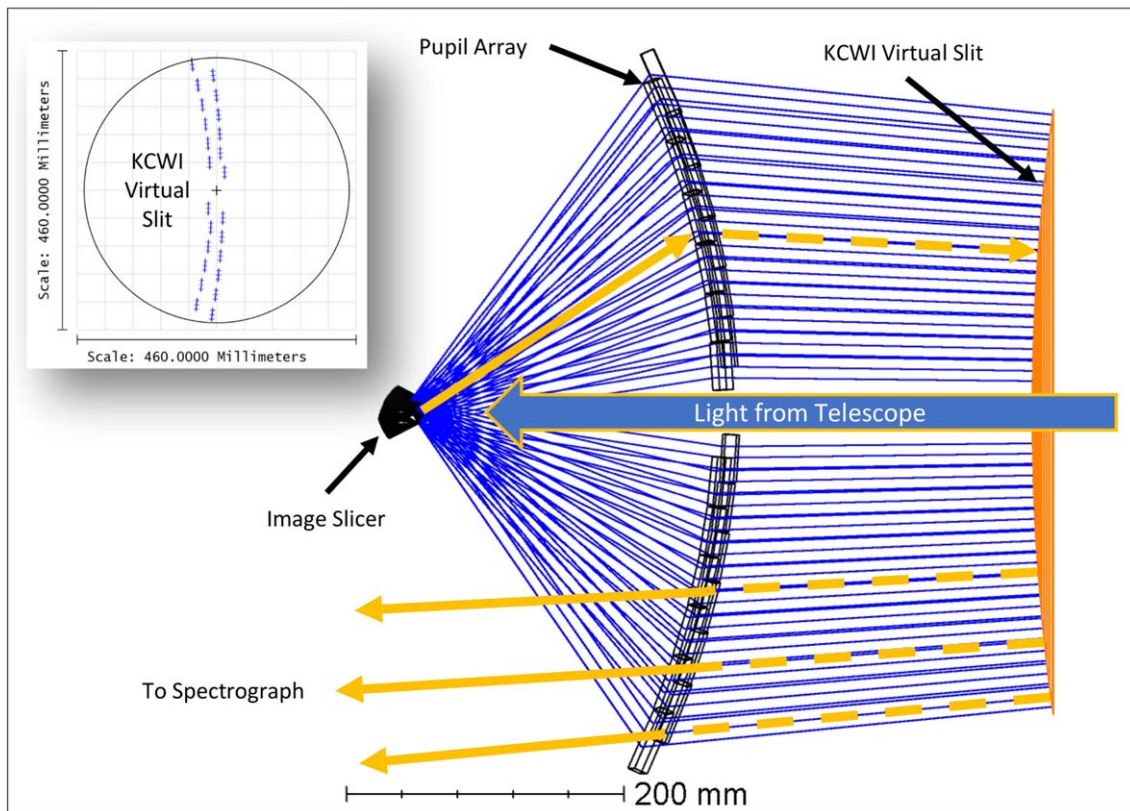


Figure 9. A ray trace of the KCWI IFU and virtual slit. Light enters from the right and is focused on the slicer at the telescope focal plane. Individual slices are tilted to redirect light toward the pupil array, which in turn forms the virtual slit (shown in orange) that is reimaged by the spectrograph onto the detector. The inset shows the footprint of the virtual slit on the spherical virtual slit surface.

glass under thermal stress. Bonded parts were clamped in place for seven days at room temperature to cure. This process was qualified to hold the 105 kg collimator mirror under a 4 g load through a temperature range from -20 to $+35$ °C.

The FM1 fold mirror is a 0.675 km radius convex cylinder (axis along the height of the mirror) providing wavefront correction to compensate for the collimator working angle, while FMD and FM3 are flat. The FMD fold mirror relays the light below the bench and is designed to be replaced with a dichroic to accommodate a future parallel red channel.

On the lower side of the bench, the FM3 fold mirror redirects the beam through a 248×220 mm red-light-blocking dielectric filter (Asahi Spectra Co., Tokyo, Japan) with a 570 nm 50% cutoff. The substrate is 20 mm thick Corning 7980 fused silica, tilted at an angle of 15° to the incoming beam to reduce ghost light between the detector and filter. The transmitted blue light forms a 160 mm diameter compound pupil image at the selected grating surface.

2.1. Gratings

KCWI accommodates a suite of five volume phase holographic (VPH) transmission gratings that are designed to maximize the flexibility and efficiency of the instrument. These gratings are three-dimensional structures that simultaneously obey the classical grating equation and exhibit a Bragg efficiency peak (Barden et al. 1998, 2000). The efficiency at a given wavelength can be optimized by rotating the grating between the collimator and camera. Design advantages include a reduction in ghosts and scattered light typically associated

with surface relief gratings, and complete encapsulation between two protective glass covers that are AR-coated to increase performance. The ability to tune the fringes within the volume of the grating allows the designer to optimize the polarization efficiency (Baldry et al. 2004). The VPH grating can be seen as combining the best features of both high-efficiency ruled gratings and low-scatter, polarization-insensitive holographic gratings.

Our suite of five gratings was purchased from Wasatch Photonics (Logan, UT) and is shown in Table 2 with typical incidence angles and spectral ranges across the CCD. The spectral range is reduced to about one-third the value shown when the N&S mask is deployed. The gratings are of “Dickson” design (Dickson 2003), which achieves simultaneous maximum efficiency for both *s*- and *p*-polarizations. The grating gelatin is sandwiched between a pair of $350 \times 250 \times 20$ mm thick, AR-coated Corning 7980 fused silica substrates ground and polished by Sydor Optical (Rochester, NY). The gratings are each designed to meet the instrument resolution requirements and when paired with the available image slicers provide spectral resolution in the range from 1000–20,000 as shown in Table 3. A “fringe tilt” of approximately 2° built into the design of each effectively places the grating at a small angle relative to the glass substrates (on the axis of dispersion) so that the Bragg angle of peak efficiency redirects a bright “Littrow” recombination ghost—a retro-reflection from the CCD to the grating and back (Burgh et al. 2007)—out of the wavelength range of interest, or at a minimum outside the area used for sensitive N&S observations.

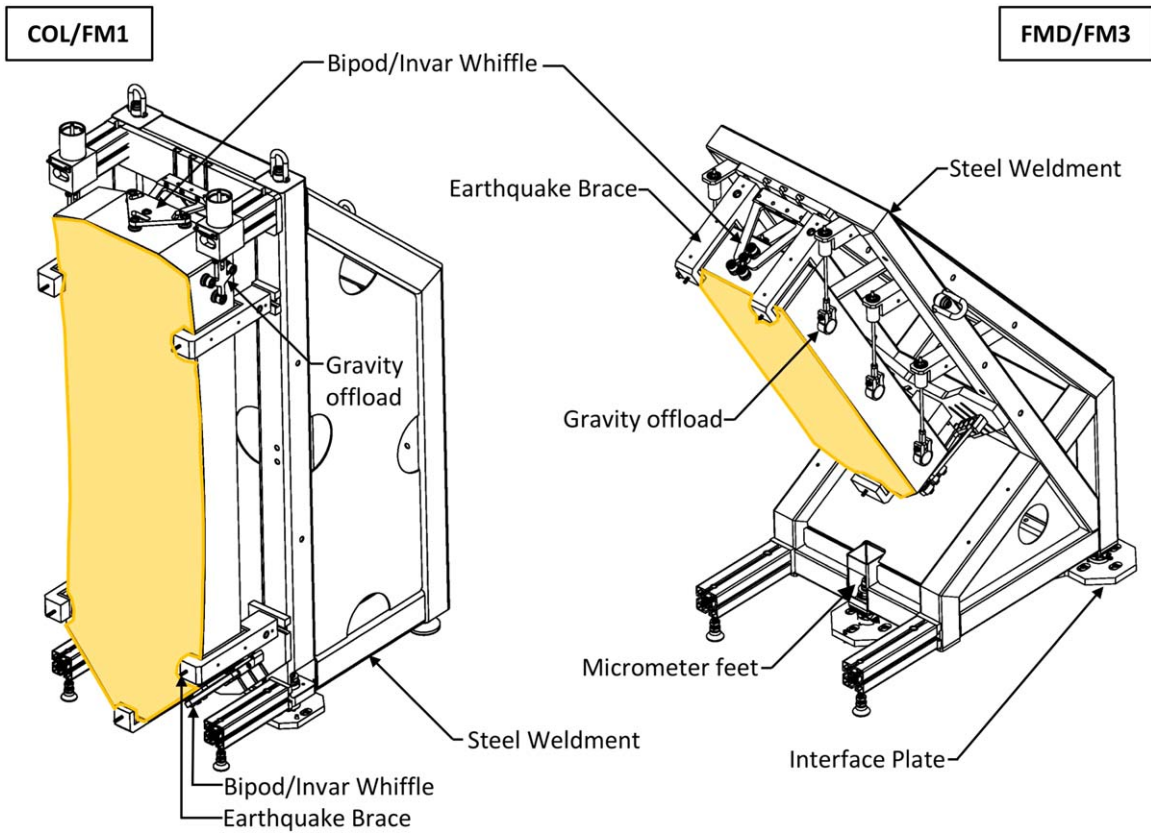


Figure 10. Line drawings of the two styles of KCWI large optics mounts. On the left is the design for the vertical mirrors, the COL and FM1 (similar but not identical). A tubular steel weldment structure provides stiffness and is CTE-matched to the K-mirror structure. The weldment is aligned with three micrometer feet and attached to the steel bench with a steel interface plate. In this design, the Zerodur mirror hangs from the weldment by a pair of suspension springs that are bonded to the mirror with Invar pads. The mirror is then held in position kinematically by three bipod-mounted whiffles, each with three Invar bond pads. The whiffles and pads are attached by spherical bearings. On the right, the design for the FMD relay mirror is shown. The FM3 mirror is conceptually similar (and is at the same angle) but is mounted from above rather than below. The tilted FMD and FM3 mounts use the same principle of offloading the mirror weight on suspension springs while constraining the position kinematically with three bipod-mounted whiffles. Each of the four mirrors are held in place by 15 bond pads, providing risk reduction in case of a bond failure during handling.

Table 2
The KCWI Suite of Gratings

Grating	Band (Å)	Rulings (lp mm ⁻¹)	α^a (°)	Dispersion (Å mm ⁻¹)	Range ^b (Å)
BH1 ^c	3500–4100	3800	55	6.0	360
BH2	4000–4800	3281	52	7.4	443
BH3	4700–5600	2801	50	8.6	516
BM	3500–5600	1900	30	16.1	965
BL	3500–5600	870	15	37.5	2250

Notes.

^a The typical incidence angle is shown for each grating design. Since the gratings design is tilted, the typical dispersion angle β is 9° less than α at the central wavelength.

^b The range shown is for the entire CCD and will be reduced to approximately one-third the value shown if the N&S mask is deployed.

^c The BH1 grating is in fabrication as of this writing. The example shown here is representative.

This tilt introduces an asymmetry in the incidence and diffracted angles of about 9°.

Each KCWI grating is flexure-mounted onto an aluminum cell that can be commanded in and out of an exchanger mechanism, which is shown in Figure 11. The commanded grating can be rotated 360° without interfering with the camera at any angle. Each grating has an oval-shaped pupil mask

Table 3
KCWI Slicer–Grating Spectral Resolution Table

Grating	Slicers		
	Small 8"25 × 20"	Medium 16"5 × 20"	Large 33" × 20"
BL	5000	2500	1250
BM	10,000	5000	2500
BHx	20,000	10,000	5000

on either side of the cell that baffles stray light from the instrument.

2.2. Camera

Dispersed light from the grating is reimaged with a 304.4 mm focal length, 250 mm diameter all-spherical refractive camera designed by Harland Epps and fabricated by the team at the University of California Observatories (UCO) and Lick Observatory led by Connie Rockosi (Rockosi et al. 2016). A ray trace of the nine-element air-spaced camera optics behind a high resolution grating is shown in Figure 12. The optical prescription for typical conditions at the summit of Maunakea is provided in Table 4 with the melt-sheet-derived Schott coefficients for the material indices of refraction provided in Table 5.

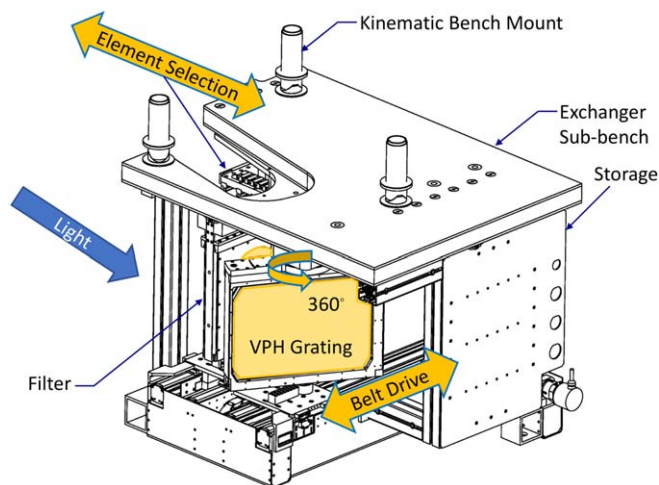


Figure 11. The KCWI blue filter and grating exchanger accommodates five gratings and five filters in a jukebox mechanism. Each element is flexure-mounted into an aluminum cell and covered on each side with a sheet metal baffle appropriate for its typical operating angle. A pair of belt-driven selectors allows any grating and filter combination to be inserted into the beam. The filter is placed at a fixed 15° angle to the beam, while the grating is rotatable to any angle. Coordinated motions of the exchanger are executed by a Galil motion controller which completes each sequence at a home position to minimize flexure.

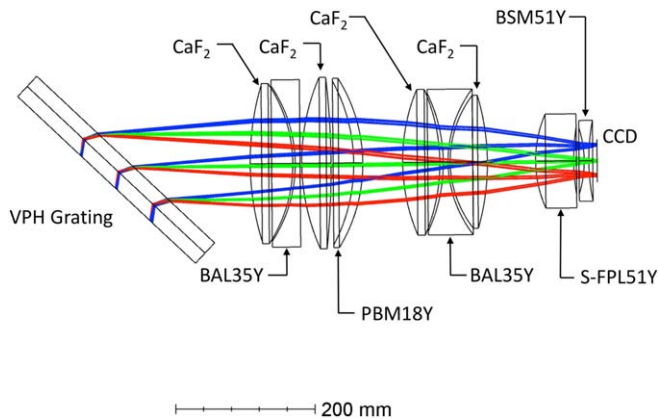


Figure 12. A ray trace of the KCWI camera with high-resolution grating. The nine spherical elements were designed, fabricated, and assembled at the University of California Lick Observatory in Santa Cruz. The ninth element (BSM51Y) is a field flattener and also the vacuum window for the CCD detector. The window and CCD move together on a linear stage to provide focus capability.

The quartet, triplet, doublet design shown produces pixel-limited imaging over the full 350 to 560 nm design wavelength range and across an 8.2° field radius (the CCD diagonal) without refocus, with acceptable performance to 700 nm in cases where the red-blocking filter is removed at the expense of increased ghosting. Lens materials were selected to provide high UV transmission. Four calcium fluoride elements generate most of the positive optical power, while Ohara (Kanagawa, Japan) i-line glasses are used for color correction. The last element, made of low-radioactivity Ohara BSM51Y, serves as both a field flattener and detector vacuum window. The design performance of this camera illuminated by a 158 mm diameter polychromatic pupil results in an average root-mean-square (rms) image diameter without refocus of $15.0 \pm 4.4 \mu\text{m}$. The maximum rms lateral color in direct imaging is $7.1 \mu\text{m}$, and distortion at the full diagonal field is 0.36%.

Table 4
KCWI Spherical Camera Prescription^a

Element	Material	R_1 (mm)	R_2 (mm)	Thickness (mm)	Spacing (mm)
1	CaF ₂	389.859	-208.667	61.065	3.500
2	BAL35Y	-200.674	∞	6.969	2.500
3	CaF ₂	306.107	-1145.486	42.023	32.649
4	PBM18Y	-247.324	-230.463	12.947	57.227
5	CaF ₂	270.853	-263.636	53.418	5.000
6	BAL35Y	-230.090	172.635	6.999	3.000
7	CaF ₂	156.636	-340.233	53.328	69.390
8	S-FPL51Y	167.551	311.824	54.784	15.000
9	BSM51Y	-155.177	300.975	6.589	11.995

Note.

^a The camera is designed to operate at 2°C and 456 mmHg and to accommodate a round 160 mm diameter entrance pupil located 200 mm ahead of the first lens element vertex.

The camera lenses were fabricated in the optical shop of the UC Lick Observatory by David Hilyard and AR-coated at ECI (Willow Grove, PA). Each is mounted in a machined metal cell and secured by a continuous bead of room-temperature vulcanizing silicone (Dow Corning RTV560; Fata & Fabricant 1998) designed to passively compensate and minimize stress on the lenses due to the temperature difference between the laboratory assembly conditions in Santa Cruz ($\sim 22^\circ\text{C}$, 760 mmHg) and the operating conditions on Maunakea ($\sim 2^\circ\text{C}$, 456 mmHg). A machined spacer between elements 7 and 8 is slotted to accommodate the camera shutter (the second of the two identical Bonn shutters in the instrument).

The principle of the mount design, similar to that used for the DEIMOS camera (Mast et al. 1998), requires the coefficient of thermal expansion (CTE) of the lens to be smaller than the CTE of its metal cell, and the CTE of the RTV to be larger than both the lens and cell material. When the camera is brought from lab temperature to operating temperature, the cell contracts more than the lens. The thickness of the RTV bond used to hold the lens into the cell is determined such that the thermal contraction of the RTV is the same as the difference between the contraction of the lens and cell. The cells are made from either 303 stainless steel (most of the glasses) or 7075 aluminum (CaF₂, S-FPL51Y) in cases for which the optical material has a large CTE.

Lenses were positioned in each cell on a rotating table with a series of gauges, and when the lens was centered adequately (the requirement is 15 microns for the finished cell), the RTV was injected into the gap and allowed to cure. The lenses were mounted into the front and rear stacks, with each cell shimmed into position to meet the alignment requirement. Element 5 was delivered last from the coating vendor and completed the assembly.

The camera was delivered to Caltech where it was installed onto a steel articulation stage that carries both the camera and the detector. A diagram of the assembly is shown in Figure 13. The traveler is articulated on curved rails that are centered around the grating axis of rotation and secured by a large custom stage that is kinematically mounted under the optical bench. Wavelength selection is accomplished by means of a rack-and-pinion mechanism. A servo motor mounted on the traveler provides station keeping during observations by means of a long magnetic strip encoder mounted on the perimeter of the stage.

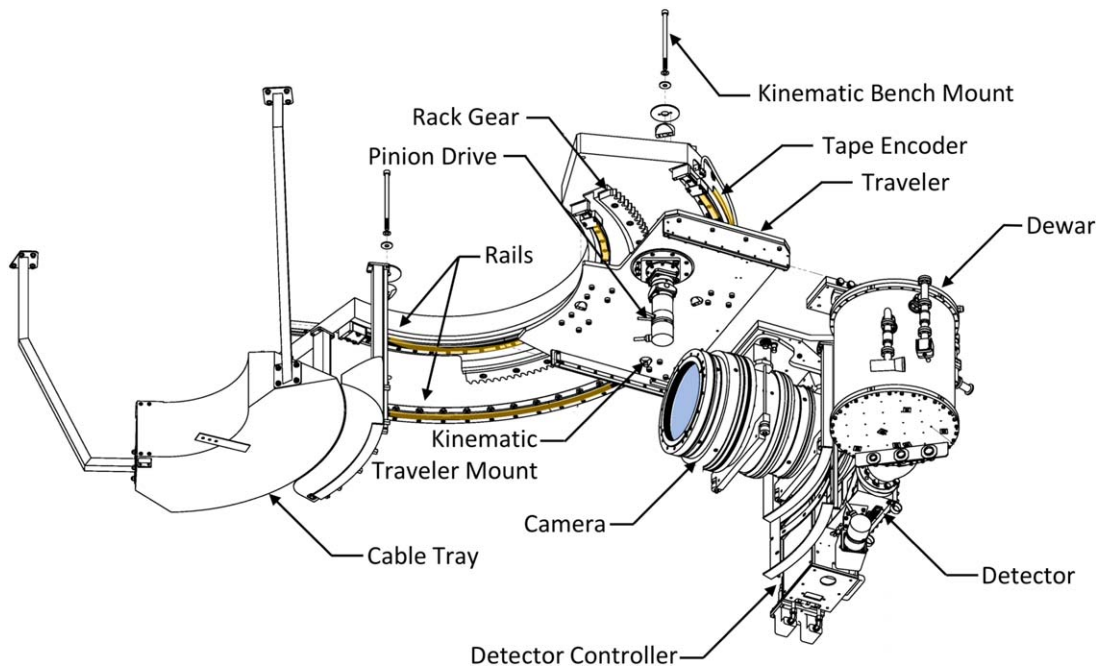


Figure 13. The KCWI articulation mechanism assembly, which includes the camera and detector. The stage is made from steel and is kinematically mounted to the underside of the optical bench. A rack-and-pinion drive with a magnetic tape encoder enables wavelength selection as well as access to a liquid nitrogen fill position. Station keeping is provided by a servo motor mounted on the traveler stage.

Table 5
Schott Coefficients for KCWI Camera Optical Glass^a

Material	a_0	a_1	a_2	a_3	a_4	a_5
BAL35Y	2.4882237	$-1.0433842 \times 10^{-2}$	1.3666718×10^{-2}	1.8847446×10^{-4}	9.7167343×10^{-7}	1.5430999×10^{-7}
BSM51Y	2.5315177	$-1.0613914 \times 10^{-2}$	1.4233791×10^{-2}	2.0023854×10^{-4}	1.3748829×10^{-6}	1.4992248×10^{-7}
CaF ₂	2.0397792	$-3.2198575 \times 10^{-3}$	6.1611382×10^{-3}	5.2037190×10^{-5}	4.2463262×10^{-7}	7.7562224×10^{-9}
PBM18Y	2.4854756	$-9.2258527 \times 10^{-3}$	1.9811993×10^{-2}	8.3005994×10^{-4}	$-3.5512051 \times 10^{-5}$	4.3642513×10^{-6}
S-FPL51Y	2.2192616	$-5.2736411 \times 10^{-3}$	8.4898019×10^{-3}	8.3761331×10^{-5}	6.0858203×10^{-7}	4.8911238×10^{-8}

Note.

^a The Schott formula for the index of refraction is $n^2 = a_0 + a_1\lambda^2 + a_2\lambda^{-2} + a_3\lambda^{-4} + a_4\lambda^{-6} + a_5\lambda^{-8}$, where n is the index of refraction and λ is the wavelength in micrometers. The coefficients are determined for operating conditions of 2 °C and 456 mmHg.

2.3. Detector

The camera is coupled to a liquid-nitrogen-cooled, AR-coated, back-illuminated CCD detector. The last lens of the camera serves as the vacuum window. The CCD is operated between -100 °C (lab) and -110 °C (observatory), with a measured hold time of 96 hr at the summit. The operating temperature is maintained by a Lakeshore 336 controller to within ~ 0.1 °C rms. The dewar is filled from a location at the end of the articulation stage travel that engages a fill port and vent with externally accessible plumbing. The vacuum is maintained by a charcoal getter located under the dewar and monitored by a 21 s^{-1} ion pump. Typical operating pressure when the dewar is cold is $< 10^{-6}$ Torr, enabling the system to operate continuously for up to one year. A focus mechanism provides precise (± 1 micron) piston control of the detector vacuum enclosure behind the camera barrel through a 6 mm design range with the liquid nitrogen dewar held fixed and connected through a flexible bellows. The CCD is a Teledyne-e2v CCD231-84 that has 4096×4112 pixels with $15\ \mu\text{m}$ pitch mounted on a SiC package with a pair of permanently attached and thermally

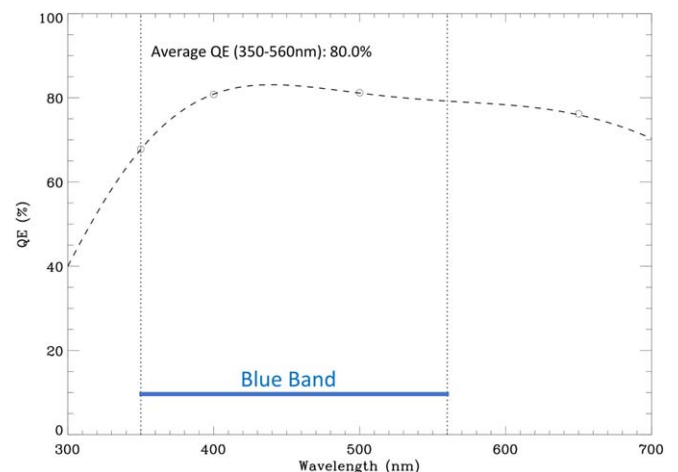


Figure 14. The QE of the KCWI CCD is shown for four points measured by the vendor. The dashed line is a fit to a standard Teledyne-e2v QE curve scaled to the measured values.

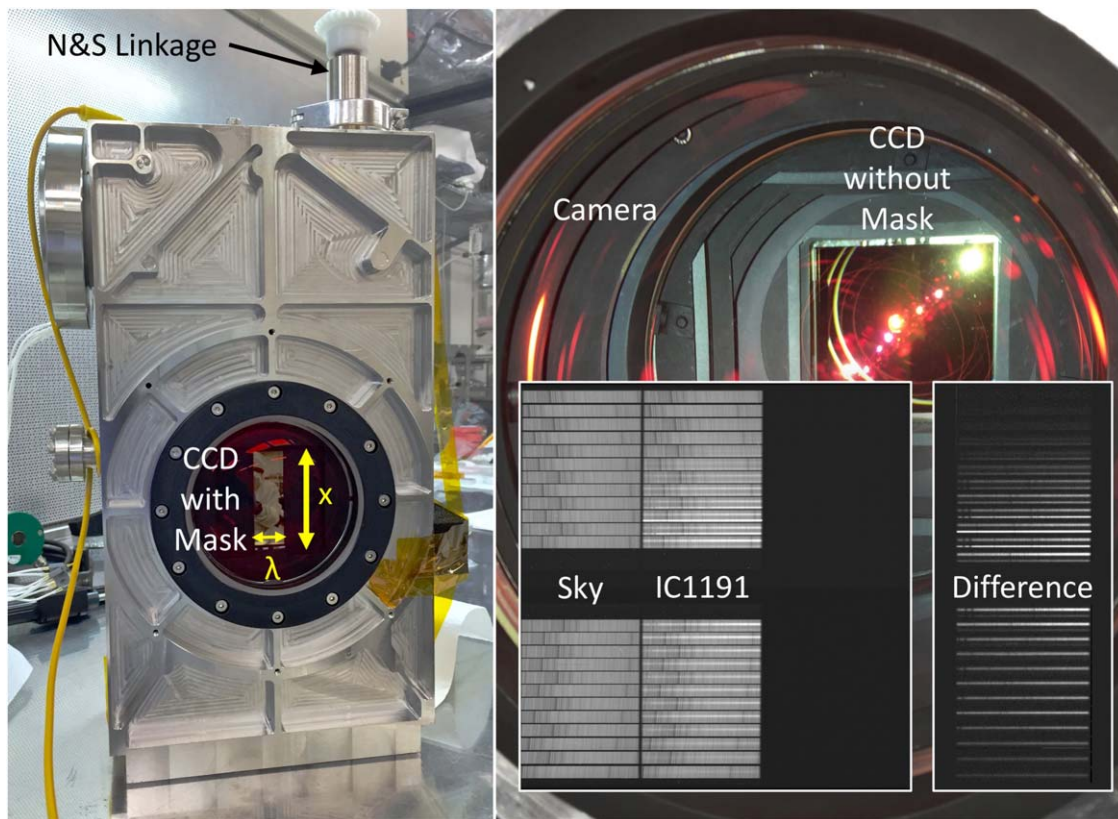


Figure 15. An illustration of the deployable N&S mask. In the benchtop image on the left, the mask is shown in the N&S position over the CCD. This is the mode used for the demonstration observation of IC 1191 from 2017 May 16–17 shown in the inset on the right. The night was moonlit, and the image shows considerable sky background filling the slicer in addition to the spectra of the galaxy. In the background on the right, the CCD is shown through the camera lens with the N&S mask in the OPEN position. Note the red reflections in the lens that are due to the high out-of-band reflectivity of the camera coatings. The red-blocking filter eliminates this out-of-band light during ordinary circumstances.

isolating flexible ribbon cables. The surface passivation and coating is the blue-optimized “astro broadband” process, which provides enhanced QE below 400 nm. The QE of the detector was measured at Teledyne-e2v and is shown in Figure 14. The average value is 80%.

A deployable N&S mask inside the vacuum provides enhanced observational capability to KCWI. The mask is made from stainless steel and is finished with black chrome. It is mounted approximately 1 mm above the CCD on a pair of linear bearings and is actuated by an external ground-isolated stepper motor linked to a lead screw through a ferro-fluidic vacuum feedthrough. The mask has three positions: open, dark, and N&S; its operation is illustrated in Figure 15. On the left side of the figure, the detector housing is shown with mask in the N&S position. In this mode, the middle third of the CCD is exposed, truncating two-thirds of the bandwidth but enabling nearly simultaneous target and sky measurements. During a typical observation, the telescope is “nodded” back and forth between a target and sky position for 2 minutes each. When the instrument is finished with one target, the shutter is closed and the image is “shuffled” under the mask. The telescope then points at the second field and repeats the process, typically for a total observation length of 1 hr (1/2 sky and 1/2 target). An example of a N&S spectrum of the galaxy IC 1191 is shown in the inset on the right side of the figure. The observation of the sky and the galaxy are both on a single CCD image (with only one readout noise penalty). This 20 minute demonstration was taken on the moonlit night of 2017 May 16–17 during KCWI commissioning with the large slicer and BL grating centered at

450 nm. While the N&S capability enables superior sky subtraction for extended objects, in cases where the sky can be adequately measured from within the field of view, the bandwidth can be extended by moving the mask to the OPEN position.

The detector controller is a standard Astronomical Research Cameras (San Diego, CA) Generation III controller designed by Robert Leach with quad channel, 16 bit readout, and correlated double sampling. The read noise is $\lesssim 3$ electrons with a controller gain of 0.16 electrons DN^{-1} (~ 4.5 electrons in fast mode) and essentially unchanged from the measured value in the laboratory at Caltech. We attribute this to our attention to ground isolation in the detector system. Care was taken throughout the design process to eliminate the possibility of ground loops by ensuring the CCD (including the package) is only grounded to the detector controller. We have measured the equilibrated dark current to be 1 electron $\text{pixel}^{-1} \text{hr}^{-1}$ at -110°C . Care should be taken that the dark current is elevated (a known charge trapping effect) for several hours after a controller restart (~ 4 electrons $\text{pixel}^{-1} \text{hr}^{-1}$ after 2 hr, ~ 2 electrons $\text{pixel}^{-1} \text{hr}^{-1}$ after 6 hr).

The controller is mounted next to the CCD vacuum housing in order to minimize the cable length from the CCD to the video input (estimated to be approximately 30 cm including the flex cable attached to the CCD itself). The controller is connected by optical fibers to a Linux host computer installed in the environmentally controlled data room at the observatory summit. The controller software supports readout from any of the four amplifiers, or from either serial register. Two readout

Table 6
KCWI Coating Overview

Element	Coating	Design Band (nm)	Vendor
Window	Dielectric	350–1050	ECI (Willow Grove, PA)
K-mirror	Dielectric	350–1050	ECI
Guider	Dielectric	350–630 ^a	Asahi (Japan)
Dichroic			
IFU	Multilayer-Ag	350–1050	Optics Balzers (Liechtenstein)
Collimator	Multilayer-Ag	350–1050	Zecoat (Torrance, CA)
FM1	Multilayer-Ag	350–1050	Zecoat
FMD	Enhanced-Al	350–560	Clausing (Skokie, IL)
FM3	Enhanced-Al	350–560	Clausing
Blocking	Dielectric	350–560	Asahi
Filter			
Camera	Dielectric	350–560	ECI

Note.

^a The guider dichroic is designed to permit HeNe laser light at 632.8 nm into the blue channel for alignment purposes.

speeds are also available, as is 2×2 binning. In order to optimize read noise performance, high gain (which limits the full well to the range of the A/D converter) is used. Readout times for the available modes range from 7 s (2×2 fast, quad amplifier) to 337 s (1×1 slow, single amplifier) with a typical science configuration (2×2 slow, single amplifier) reading out in 106 s.

3. Coatings

The KCWI design contains a meniscus window, nine mirrors, two filters, a grating and a nine-element camera lens. Careful attention to the design, performance, and stability of the coatings is clearly essential to achieve the instrument requirements. Throughout the design process, we made every effort to ensure that a high-performance red channel could be added without recoating existing elements. Table 6 shows the coatings and design bands used in KCWI, by element and by vendor.

3.1. Reflective Coatings

The common optics of the eventual red and blue channels include the window, three K-mirror reflections, two IFU reflections, the collimator, and the cylindrical FM1 mirror (the guider will be redesigned when the red channel is added). The existing FMD fold mirror will be replaced by a dichroic, and all existing elements in the blue arm from the FM3 mirror onward will not see light longer than 560 nm. We invested in broadband dielectric and multilayer silver coatings to boost red throughput for the common reflective elements, while the blue arm mirrors are coated with enhanced aluminum or multilayer dielectric.

The three elements of the K-mirrors represent a necessary addition to the mainframe optical design in order to accommodate the Nasmyth port location. Since this mechanism increases the number of required instrument reflections by 50%, it is important to minimize its impact on performance as much as possible. Furthermore, the alignment of the K-mirror is a precise and challenging operation that incentivizes the inclusion of robust coatings. As such, we elected to invest in broadband dielectrics from ECI, and each provides average

reflectivity $\gtrsim 99\%$ over the 350–1050 nm band. The K-mirror substrates are Zerodur with a diameter-to-thickness ratio of approximately 10. The mirrors were each back-side polished and stress-relieved with a compensating coating on the back to preserve the front side surface figure. We found that the finished mirrors exhibited a mainly spherical 0.5 wave peak-to-valley surface error due to residual coating stress as measured by an interferometer, well within the three-wave requirement and not severely degraded from the initial 0.1–0.2 wave fabrication quality.

The reflective dielectrics provide similarly high *s*- and *p*-polarization reflectivity; however, the complex interaction of light with the rotating K-mirror causes a phase shift of the incoming beam. We investigated this property by illuminating the instrument with linearly polarized light from a flat-field source in the laboratory. For each K-mirror angle, we analyzed the transmitted light using a selectable downstream polarizer that is part of the calibration unit. We find that as the K-mirror rotates, the transmitted beam polarization changes character from linear to circular and back to linear again, where the transmitted beam is linearly polarized at K-mirror rotation angles of 0° and 90° , but circularly polarized in between at 45° . Since this is a slowly varying effect, the N&S mode can be employed for demanding applications. Performance simulations with variable beam polarization were included in Morrissey et al. (2012).

The remaining blue and red common-path optics, the COL and FM1, are coated with multilayer-protected silver for enhanced broadband performance. Significant effort was expended in optimizing these specialty coatings for the KCWI application, taking advantage of the experience of the team at Lick Observatory and in industry (Sheikh et al. 2008; Phillips et al. 2012). Nontarnishing silver coating designs have been developed over the past 50 years with success. Denton Vacuum’s FS-99, protected by $\text{Al}_2\text{O}_3/\text{SiO}_2$, and Lawrence Livermore Laboratory’s nitride-based protective designs are noteworthy examples (Adams 1972; Wolf & Thomas 2000), and these coatings have been applied to many ground- and space-based mirrors. Recently, the desire to develop a silver reflector for the UV has led to new research (Sheikh 2016). These silver coatings are really dual designs in the sense that the multilayer protective coating is providing most of the reflectivity short of 400 nm, while the silver itself is an excellent coating for longer wavelengths (and far superior to aluminum in the *I* band). Nonetheless, unprotected silver is well known to be at risk of tarnishing on exposure to the elements. Since lifetime is an important consideration both to manage overall instrument cost and to accommodate the future red channel, we embarked on a rigorous test program for the KCWI silver coatings that included wiping with water and solvents as well as a 10 day accelerated lifetime test in a $80^\circ\text{C}/80\% \text{RH}$ salt atmosphere (Phillips et al. 2016). A variety of designs based on protective metal oxides, metal nitrides, and metal fluorides were tested and compared. We found that while no designs survived our abusive test without any damage at all, some fared substantially better than others. Of particular note, we found that a water drop (although not a solvent wipe) deposited on any coated mirror surface prior to the lifetime test would always reveal itself in the final results as a damaged area of the coating, pointing to the importance of a dry instrument purge at the observatory. The final design ZeCoat samples were among the best of all of those that were evaluated and revealed

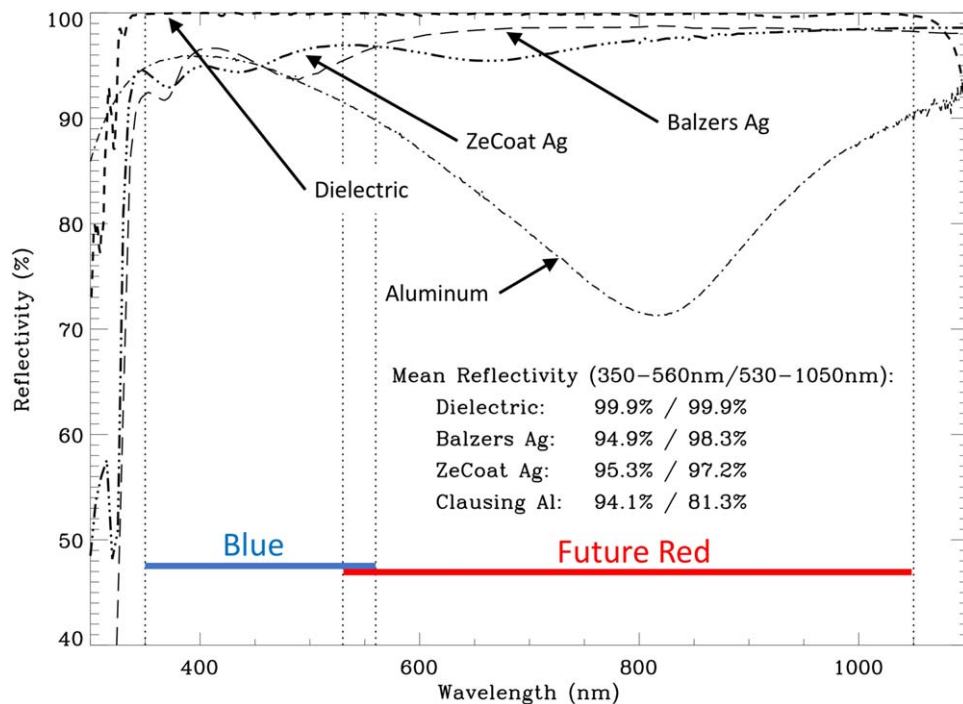


Figure 16. The measured reflectivity of the KCWI mirrors illustrating both current blue-band performance and the potential for high performance in the future red arm.

only minor degradation after environmental testing. In the end, we chose two proprietary designs for the protected silver in KCWI: the IFU was coated in Europe by Optics Balzers AG (Liechtenstein), while the two large mirrors were coated at ZeCoat Corporation (Torrance, CA). The average reflectivity of both designs is close to 95% in the blue band. The ZeCoat design received the most optimization and performed the best in the lifetime test with a salt atmosphere. The Optic Balzers coating passed a similar heat/high humidity test but without the salt. The project decided that the cost, export requirements, and transportation risk involved in coating the IFU in the U.S.A. outweighed the performance margin of the optimized coating, and we therefore accepted some increased risk on the IFU coating lifetime, judged to be reasonable in view of the fact that samples with similar Balzers coatings were remeasured with no degradation after five years in “desk drawer” conditions at Winlight.

Downstream of the FM1 cylinder, the FMD/FM3 pair of relay mirrors are coated with a proprietary enhanced-aluminum (“BB-100”) coating from Clousing (Skokie, IL) that has been optimized for the 350–560 nm band. The average reflectivity of these mirrors is 94% in the blue band. The measured results for all of the KCWI reflective optics are shown in Figure 16. It is apparent that the dielectric coatings are best of all, while aluminum is an excellent cost-effective option in the blue, and silver can effectively be used to coat large surfaces with enhanced red performance.

3.2. Windows and Filters

A fused silica meniscus window protects the entrance of the spectrograph in front of the K-mirror. It is coated with a standard commercial (ECI) broadband AR coating averaging 1.5% reflectivity per surface. Downstream of the K-mirror, the guider dichroic transmits 97% of the 350–630 nm blue-band light while reflecting 98.5% of the 650–900 nm red light to the

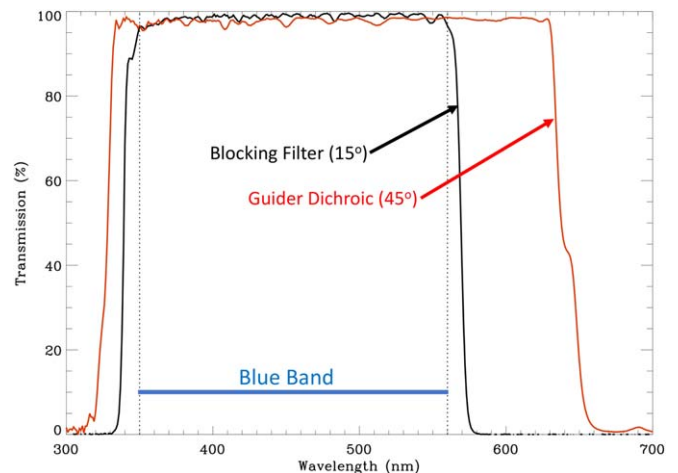


Figure 17. Black line: the measured throughput of the red-blocking filter. Red line: the measured throughput of the guider dichroic, which is designed to permit HeNe laser alignment tools. The overall instrument band can be broadened by removing the blocking filter at the expense of greatly increased ghosting in the camera.

MAGIQ guider. The intermediate choice of cutoff wavelength in the guider dichroic permits the use of HeNe laser alignment tools inside the spectrograph. A camera red-blocking filter ensures only blue-band light enters the grating and camera. It is coated with a dielectric filter from Asahi and tilted 15° to eliminate the possibility of ghost light from the camera return beam. It should be noted that the spectrograph can be used with wavelengths as red as the guider dichroic 630 nm cutoff by removing the red-blocking filter, although ghosts in the camera (discussed in the next section) would be expected to be relatively bright in this configuration. The measured throughput of the guider dichroic and camera red-blocking filter are shown in Figure 17.

3.3. Camera Coatings

The last element in the spectrograph, the nine-element camera, has demanding coating requirements. Eighteen surfaces plus the detector have the opportunity to scatter light and to redirect it in undesirable ways. We used the Zemax (Kirkland, WA) ghost focus generator to produce a Gaussian estimate of the expected ghosts resulting from double bounces through the camera system. The CCD is included as an element, and it produces some of the brightest ghosts because it is very reflective compared to any of the camera lens surfaces. For modeling purposes, we used 30% CCD reflectivity (worst case) and 0.5% lens reflectivity to make conservative estimates. There are two primary forms of ghosts: reflections that move with the source (forming a halo), and others that move in the opposite direction as the image is scanned across the field. Of the three brightest ghosts from the simulation, two involve the CCD and its nearest element, the field flattener, while the third is from a double bounce inside the field flattener (suppression due to the low coating reflectivity in this case is compensated by the close proximity to the CCD). These three bright ghosts are between 2 and 20 mm diameter (occupying 3%–30% of the detector field of view) with integrated intensities as bright as 0.1% of the source. Large extended ghosts are exacerbated by dispersion, which integrates them while simultaneously attenuating the original point source. The ghosts are quite faint, but must be evaluated relative to the sky continuum. For example, simulations indicate that a magnitude 20 star forms a broad, diffuse composite ghost at around the 10^{-3} of the sky level, depending on the dispersion. Observers should take care to avoid bright sources in regions for which the sky subtraction is required to work at the finest level (e.g., “light bucket mode,” for which a single spectrum is created from the entire slicer area).

In view of these results, we were careful to evaluate the performance of each coated element before integrating it into the camera. At the low reflectivity levels we were evaluating ($\sim 0.2\%$), we found that humidity and age could degrade performance (from a combination of coating porosity and deterioration of the black coating deposited on the rear surface of each witness sample). Adhesion was a challenge on some of the surfaces, particularly those made of CaF_2 . Several required multiple attempts (with associated repolishing) in order to meet the requirements. ECI chose two processes to deposit the AR coatings: electron beam (e-beam) and ion-beam sputtering (IBS). We found that the lowest reflectivity (due to the wider range of allowed materials) was achieved with the e-beam, but the IBS process yielded the best adhesion and repeatability, and was chosen for the most problematic elements.

The measured reflectivity results from our camera coating program are shown in Figure 18. The results for the worst ghost-generating surfaces are depicted in blue, revealing that on average we were able to hold their reflectivity to under 0.15%, while the overall camera surface reflectivity is under 0.2%. When combined, these result (with the addition of some predicted glass absorption below 400 nm) in an overall camera transmission of over 96% as shown in Figure 19.

3.4. Baffling and Stray Light

The control of ghosts and stray light is an important element of the design of a background-limited instrument such as KCWI. In the case of a reflective image slicer, a certain amount

of shadowing and stray light is unavoidable due to the close proximity of sharp reflective edges. Light incident close to the edge of one slice may collide with the wall formed by the adjacent slice and be misdirected. The KCWI design includes a range of slice angles spanning $\pm 27^\circ$ with a $\pm 4^\circ$ gap between the central two slices to allow room for light to enter from the telescope through the pupil array. While the two central slices have the largest angular discontinuity (8° versus a more typical 2°), they have the minimum shadowing because the central elements of the pupil array are designed along a diagonal (see Figure 9), and each accepts light from one of the two central slices in such a way that incident light is reflected away from the wall at the center.

We have performed a nonsequential analysis of the IFU with each image slicer design uniformly illuminated by a beam of light with a range of angles similar to the Keck telescope. Rays are considered to have been vignetted if they are eliminated at any point in the instrument path, but the effect is dominated by internal reflections in each slicer. We find that under these illumination conditions, the large slicer vignettes a maximum of 5% of the light from any location, while the medium and small slicers vignette a maximum of 9% and 25%, respectively. Results of this analysis are shown in Figure 20 and show that the vignetting is concentrated at specific slice edges particularly toward the corners of the field. The effect in the small slicer is mitigated by the fact that there are approximately two slices per seeing-limited PSF, and therefore is reduced by a factor of ~ 2 when the footprint on the slicer is taken into account.

A fraction of scattered rays from each slice will land on a pupil mirror and be transmitted though the system. The majority are eliminated by a series of baffles designed around the footprint of the virtual slit at each of the four large mirrors, the red-blocking filter, and (most effectively) on both sides of each grating. The remaining stray rays reach the detector and have the effect of broadening monochromatic spectral line images by approximately 1% with 0.5% of the total integrated flux. Spectral features that are broader will reduce the magnitude of the effect proportionately.

During the design phase, we identified the contribution of a “narcissistic ghost” that resulted from light reflecting off the detector and traveling backward through the optical system to reimage on the slicer. The return image is superimposed on the initial slicer input, and the majority of this light is redirected back out to space. However, the return image is not of the same quality as the input because it has traversed the spectrograph twice. The fuzzy return image can therefore straddle adjacent IFU slices and be redirected back into the spectrograph through the wrong channel. This ghost (which now has a peak contribution of a few parts in $\sim 10^{-3}$ in the central channels of the small slicer and much less in the others) was mitigated by adjusting the compound angle of the two central slices to move the two central pupil mirrors outboard approximately 1 cm as can be seen in Figure 9. The effect of this is to redirect the return light from the system that mixes the two central channels off the IFU pupil array and out of the optical path.

3.5. Predicted Optical Throughput

The overall instrument throughput, which is the product of the reflectivities of the nine KCWI mirrors and the transmission of the window, dichroic, and red-blocking filter, is shown in Figure 21. The rolloff shortward of 400 nm is primarily due to

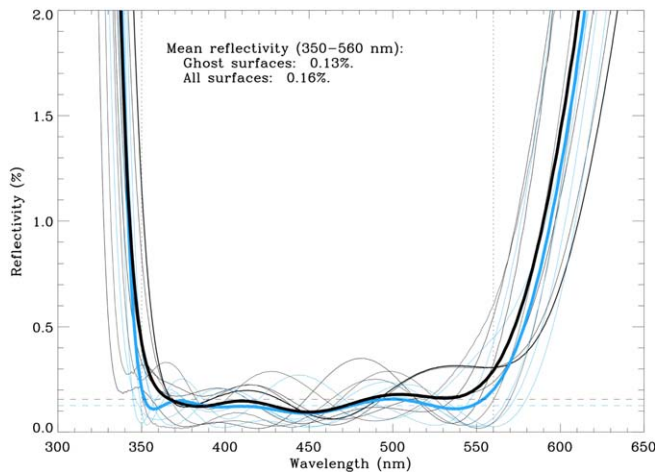


Figure 18. The measured reflectivity of the 18 camera lens surfaces. Surfaces with the potential to generate bright ghosts are highlighted in blue. The average reflectivity of all of the “ghost surfaces” is plotted in bold blue while the average reflectivity of all surfaces combined is plotted in bold black. The mean reflectivity is under 0.2%.

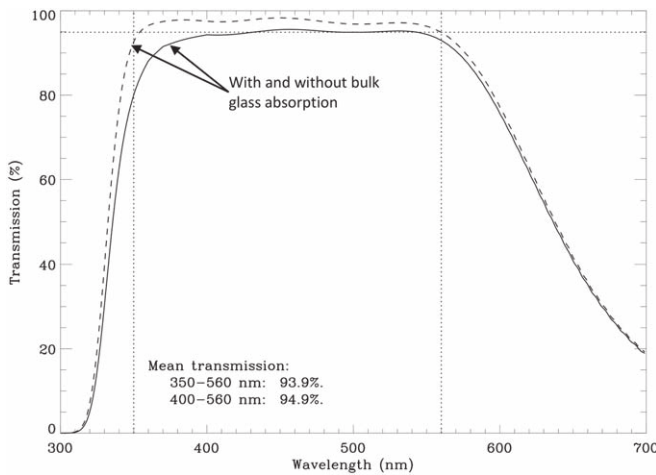


Figure 19. Solid line: the model transmission of the KCWI nine-element camera lens based on the measured reflectivity of all of the individual lens surfaces multiplied by a factor to account for bulk absorption in the glass. Dashed line: the estimated camera lens transmission in the absence of bulk glass absorption.

absorption in the camera glass. The average throughput from 350–560 nm is 65.5%. This figure does not include the effect of the grating or detector in order to isolate the performance of the coatings. We would anticipate similarly high throughput in the planned 530–1050 nm red channel based on witness sample measurements.

3.6. Predicted Optical Resolution

The KCWI design achieves pixel-sample-limited resolution without refocus as shown in Figure 22. The cylindrical FM1 corrector ensures that the performance of the system is completely dominated by the large 305 mm focal length camera lens. Good seeing at the summit of 0.5 corresponds to about 3.5 pixels at the detector, while the highest resolution small slicer slit image is nearly Nyquist sampled at 2.3 pixels. Optical imaging performance is comparable with all grating and filter combinations, but note that the small slicer

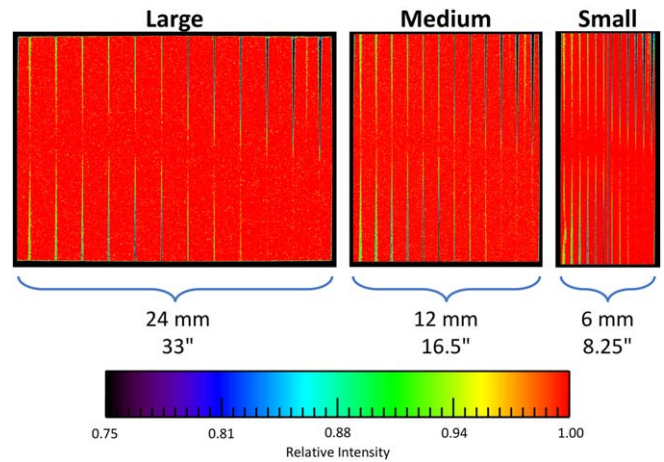


Figure 20. Reconstructed flat-field images of each slicer accounting for vignetting as determined with a nonsequential ray-trace simulation. Vignetting is correlated with slice edges as expected and ranges from a maximum of 5% for the large slicer up to 25% for the small slicer in isolated locations. The effect is reduced when considered with a convolved point source, typically >350 μm FWHM.

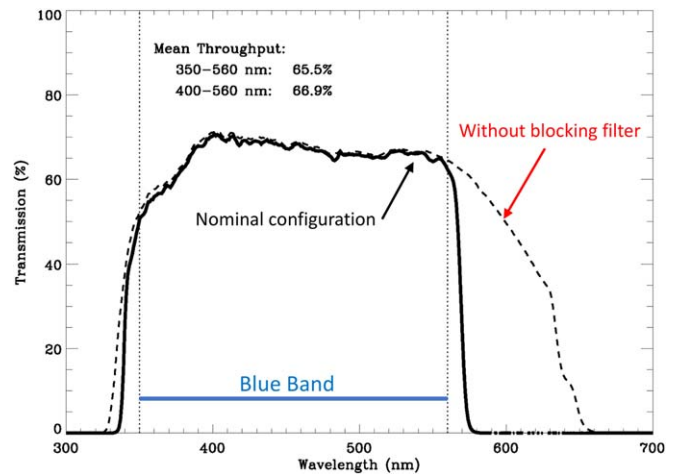


Figure 21. Black line: the model optical throughput of KCWI based on the measured reflectivity and transmission of the guider dichroic, nine mirrors, red-blocking filter, and camera. The detector and grating efficiencies are not included. Dashed line: the model throughput with the blocking filter removed (at a cost of increased camera ghosting).

oversamples the seeing-limited point-spread function at the focal plane.

4. Data Reduction Pipeline

The data reduction pipeline (DRP) was developed using data from the PCWI, which is optically similar to the large slicer configuration of KCWI. Here we will provide the basic outline of the KCWI DRP; a more detailed description of the algorithms used will be presented in J. D. Neill et al. (2018, in preparation).

The DRP is written in the Interactive Data Language (IDL).¹² Versioning and distribution are handled through an online repository (Neill & Matuszewski 2018). Key features include

¹² Harris Geospatial Solutions, Herndon, VA.

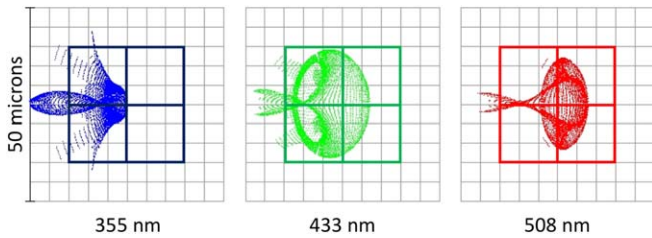


Figure 22. Model end-to-end spatial resolution of KCWI with a BL grating at three wavelengths for a point source input. The 2×2 grid in the center of each image depicts the pixel sampling with 1×1 binning.

1. Modular processing stages with minimum resampling for wavelength calibration, flat fielding, etc.
2. User-editable files for control of how the DRP operates
3. Detailed observation and configuration information stored in each image header.
4. Capability to process an entire night of data and to select sets of calibration images for each science observation

4.1. Pipeline Overview

The pipeline is divided into nine modular stages as shown in Table 7. Each of these stages produces a detailed log file and complementary ancillary diagnostic outputs.

Table 8 lists the primary image products for each stage of the DRP. The file names are constructed as follows: `kbYYMMDD_NNNNN_sfx.fits`, where `YYMMDD` is replaced by the UT date of observation, `NNNNN` is replaced by the zero-padded image sequence number, and `sfx` is replaced by the file suffix listed in the Table 8.

Figure 23 provides a composite of several of the science and calibration images typically associated with the data reduction. Panel (A) shows a 10 minute observation of the star-forming region HH 32 taken during commissioning (small slicer with BM grating centered at 470 nm) that has been processed through Stage 4 (flat field) of the pipeline. Panel (B) shows an expanded view of two prominent emission features. The image is overlaid (Panels (C) and (D)) with insets showing a calibration continuum lamp bar image used for spatial alignment of each spectrum and a ThAr arc lamp image used for the wavelength alignment. Fraunhofer lines are visible across the log-stretch image. The lower-right panel shows a pipeline reconstruction of the image on the slicer at one wavelength.

Figure 24 shows four reconstructed HH 32 emission-line images from the pipeline generated `_icubes` files based partly on the data shown in Figure 23, part of a series of spectra with different grating configurations from the same night. Since the cube contains several different atomic emission lines, it can be used to reconstruct the emission of different gases, or alternately, the kinematic distribution of gas from one species.

4.2. Pipeline Preparation

Stage 0 of the pipeline reads all of the image headers from a given night to associate the instrument configurations and their calibration sets. Two files are written that determine the way in which subsequent stages are executed: `kcwi.ppar`, which sets pipeline parameters, and `kcwi.proc`, which lists the default associations of object files with their required

Table 7
KCWI DRP Stages

Stage	Program	Description
0	<code>kcwi_prep</code>	Association of science and calibration files
1	<code>kcwi_stage1</code>	Basic CCD-level reduction, N&S panel subtraction
2	<code>kcwi_stage2dark</code>	Master dark frame creation and subtraction
3	<code>kcwi_stage3geom</code>	Geometry solution and creation of pixel maps
4	<code>kcwi_stage4flat</code>	Illumination correction using b-splines
5	<code>kcwi_stage5sky</code>	Sky subtraction using b-splines
6	<code>kcwi_stage6cube</code>	Image cube creation
7	<code>kcwi_stage7dar</code>	Differential atmospheric refraction correction
8	<code>kcwi_stage8std</code>	Standard star measurement and flux calibration

calibration files. Additional files written out in this step include the pipeline parameter files required to reduce the master calibration images and an image summary file (`kcwi.imlog`).

4.3. Basic CCD Reduction

Stage 1 performs detector-specific processing such as bias subtraction, overscan trimming, gain correction, cosmic-ray rejection, cosmetic defect correction, error image creation, and scattered light subtraction. If the image was taken in N&S mode, this stage also handles the repackaging and subtraction of the sky panel from the object panel. The output of this stage is a two-dimensional image with intensities in electrons.

Stage 2 creates and subtracts a master dark frame and then scales and subtracts it from all object frames whose CCD configuration matches the master dark.

4.4. Geometry Solution and Map Generation

Stage 3 solves the geometry of the three-dimensional data cube using continuum bars and arc lamp images to define both the spatial and the spectral mapping (see Figure 23). The bar target is projected across the slices in continuum light such that each one has five bars that define the spatial scale along the slit height. The arc lamp spectra are solved in wavelength by comparing with an atlas (either FeAr or ThAr). These wavelength solutions, combined with the known spatial separation of the bars, produce the mapping required to assemble the three-dimensional data cube.

The pipeline outputs the coefficients of the transformation for each slice along with ancillary geometry information into a FITS table that will be used to generate 3D data cubes in stage 6. It also outputs three maps that give the 3D data cube position for each 2D pixel: a slice map, corresponding to the X axis in the 3D cube; a slice position map, corresponding to the Y axis; and a wavelength map, corresponding to the Z axis.

4.5. Illumination Correction

Stage 4 corrects the profile of each slice image that results from vignetting, pixel response, and other factors.

Continuum flats are used to generate a master correction image that removes the illumination and pixel-to-pixel variations in one step. A set of six continuum flat images are stacked and averaged with outlier rejection to reduce the effect

Table 8
KCWI DRP Primary Output Products

Stage	File Suffix	Units	Notes
1	int	electrons	reduced output intensity
	var	electrons ²	intensity variance
	msk	flag	cosmic rays, defects flagged
	sky	electrons	sky panel for N&S
	obj	electrons	object panel for N&S
2	intd	electrons	dark-current-subtracted intensity
	vard	electrons ²	variance + dark image variance
	mskd	flag	combination of dark and object flags
3	geom	struct	IDL structure with geometry solution
	wavemap	angstroms	Map of wavelengths at each pixel
	posmap	pixel	Map of slice position at each pixel
	slicemap	slice	Map of slice number at each pixel
4	intf	electrons	flat-fielded intensity
	varf	electrons ²	variance + master flat variance
	mskf	flag	no change
5	intk	electrons	sky-subtracted intensity
	vark	electrons ²	variance + master sky variance
	mskk	flag	no change
6	icube	electrons	3D intensity data cube
	vcube	electrons ²	3D variance cube
	mcube	flag	3D mask cube (padded pixels masked)
	scube	electrons	3D sky panel intensity cube
	ocube	electrons	3D object panel intensity cube
7	icubed	electrons	DAR-corrected 3D data cube
	vcubed	electrons ²	DAR-corrected 3D variance cube
	mcubed	flag	DAR-corrected 3D flag cube (padded pixels masked)
8	icubes	$10^{16} \text{ erg s}^{-1} \text{ cm}^{-2} \text{ \AA}^{-1}$	Flux: $F_\lambda \times 10^{16}$
	vcubes	$(F_\lambda \times 10^{16})^2$	Flux variance
	mcubes	flag	no change

of cosmic rays. A reference region on a single slice is used to normalize the illumination of all other slices. This reference region is fit using b-splines with sufficient tension to detect pixel-to-pixel variations within each individual slice.

The output of this stage is a master flat image for each configuration and the illumination-corrected images for all continuum flat and object images.

4.6. Sky Subtraction

Stage 5 uses the illumination-corrected images, along with the geometry maps produced in stage 3, to produce a model of the sky spectrum using b-splines. Object flux is rejected with a statistical cutoff. For compact objects, this sky subtraction is effective. If the object fills the IFU, then a separate sky observation should be used with appropriate scaling to account for sky brightness variations. The N&S technique is also available for the most critical background subtraction applications.

Stage 5 produces a sky model 2D image and the sky-subtracted 2D object image.

4.7. Data Cube Generation

Stage 6 generates the 3D data cube. This stage uses the geometry mapping previously determined in stage 3 to

transform each 2D image into a geometry-corrected 3D data cube that reconstructs the focal plane at each wavelength bin.

4.8. Differential Atmospheric Refraction Correction

Stage 7 corrects differential refraction. The atmosphere refracts light as a function of wavelength with the result that at high airmass, objects are pre-dispersed on the image slicer. This has the effect of tilting spectra in the raw images, which can be accounted for in the data cubes. Using the known properties of the atmosphere combined with the airmass, wavelength band, and orientation of the input observation, the spatial shift at each wavelength can be calculated. Each wavelength slice of the data cube is shifted with a fractional pixel shift to remove the differential shifts due to the atmosphere.

4.9. Flux Calibration

Stage 8 uses standard star observations to measure the instrumental response and scale science observations to flux units. Reference standard star spectra are from the CALSPEC¹³ database hosted by the Space Telescope Science Institute (Baltimore, MD). The light from the observed standard, which

¹³ <http://www.stsci.edu/hst/observatory/crds/calspec.html>

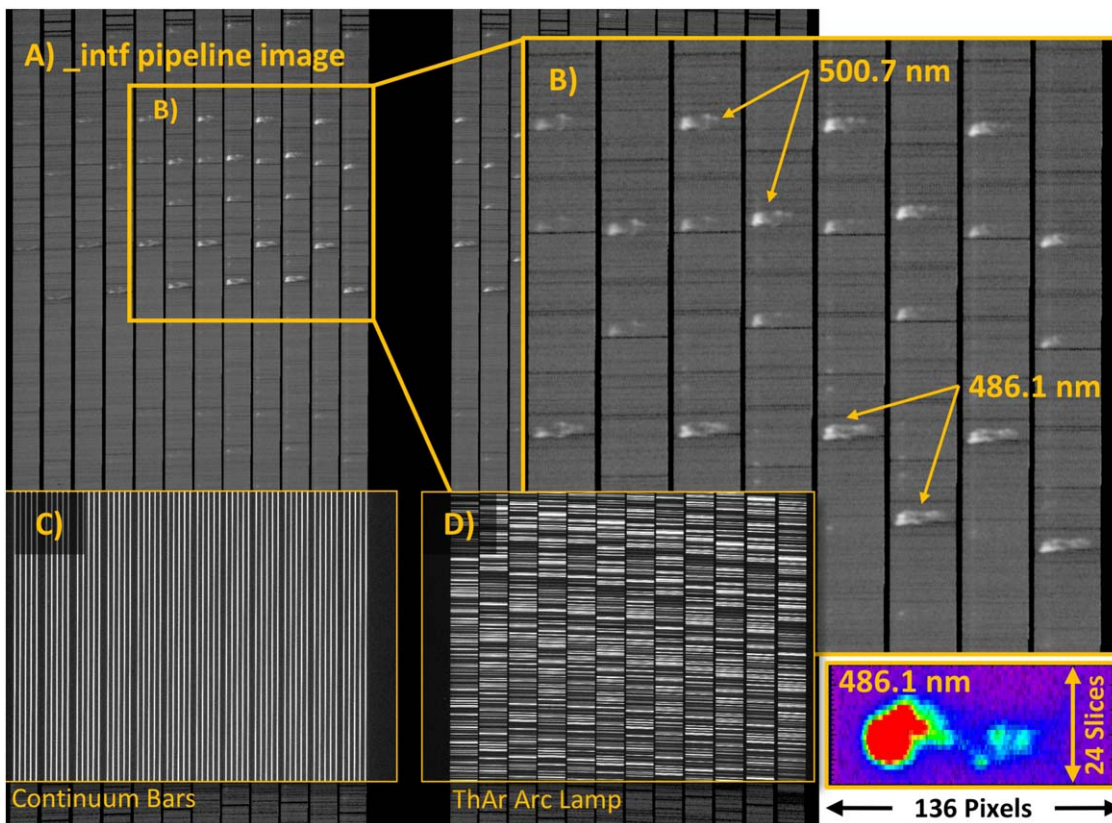


Figure 23. A sample of pipeline image reconstruction. Panel (A): a log-stretch flat-fielded image (`_intf`) of HH 32 taken with the small slicer and BM grating centered at 470 nm. Panel (B): a magnified view of some emission lines revealing the distribution of different species. Panel (C): an LED-illuminated “continuum bars” calibration image. Panel (D): a ThAr arc lamp flat-field calibration image. Lower-right panel: a pipeline-reconstructed image of the small slicer at a single wavelength.

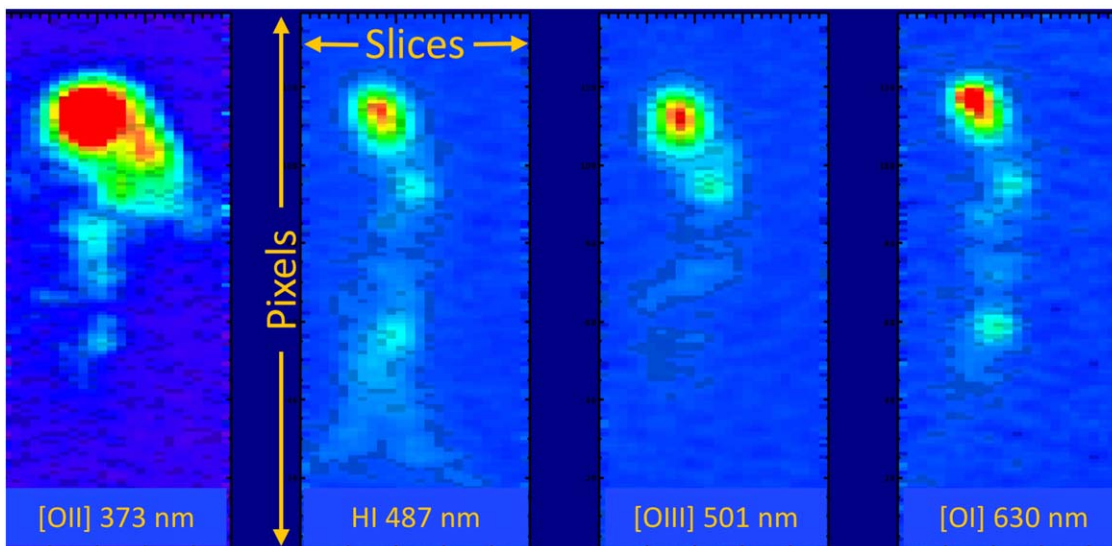


Figure 24. Emission-line reconstructions of HH 32 extracted from the pipeline-produced `_icubes` files. Pixels in the reconstruction are not square in order to show the image with the correct aspect ratio.

is usually the brightest source in the field, is integrated. The reference spectrum is resampled onto the observed wavelength scale and compared with the observed spectrum to produce an inverse-sensitivity curve that is used to scale engineering units to flux-calibrated units. The calibrated cubes are scaled by 10^{16} and give the brightness units in the header as FLAM16.

5. System Verification

5.1. Laboratory Calibration

The end-to-end optical performance of the fully assembled instrument was measured at 25 °C in the laboratory at Caltech prior to shipment. We projected a 0.5 mm diameter pinhole

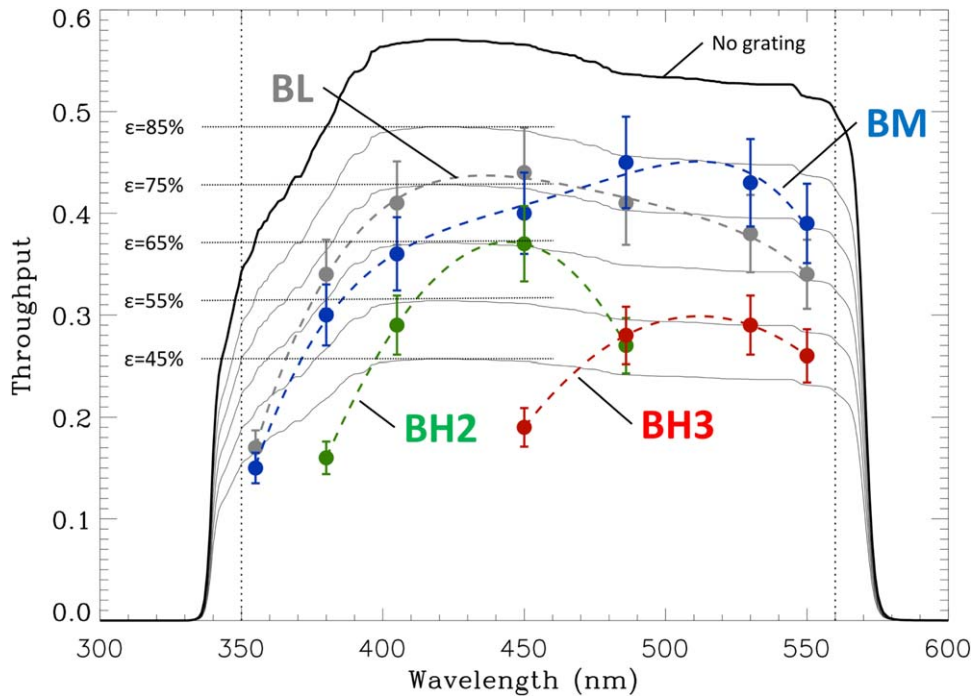


Figure 25. The laboratory-measured end-to-end KCWI throughput is shown with filled circles for the large slicer configurations shown in the indicated colors. Polynomial fits to the laboratory data are overplotted with dashed lines. The model instrument throughput without a grating (but with the CCD) is shown with a solid black line, while a family of curves are scaled in light gray, representing the system efficiency that would be achieved with grating throughput (ϵ) as labeled.

image onto the focal plane using the calibration system. A series of 10 nm FWHM filters centered at 380 nm, 405 nm, 450 nm, 486 nm, and 530 nm defined the bandpass for five measurements in each grating configuration. Each was referenced to the KCWI focal plane camera CCD sensor using the quantum efficiency from the manufacturer’s data sheet. The focal plane camera read noise (16 electrons) and gain (1.26 electrons DN^{-1}) were measured with the photon transfer technique (Janesick et al. 1987). The large slicer was then inserted into the focal plane position (spot centered) with the grating rotation optimized for the wavelength under test. Results are plotted in Figure 25 using filled circles. They are corrected (reduced by a few percent) for the throughput of the guider dichroic, K-mirror assembly, and window since these elements were not included in the beam path for our lab measurements. We estimate the uncertainty to be about 10%, including errors in the focal plane and science camera calibrations, variations in the LED source intensity, and scattering in the bandpass filters. We show the model system efficiency as a solid line, which is the product of the instrument throughput (Figure 21) and the science camera QE (Figure 14). We have overplotted a family of curves with 45% to 85% grating throughput to indicate the grating performance implied by the end-to-end measurements for each configuration as a function of wavelength. The implied peak throughput of the BL, BM, and BH2 gratings, which includes the gelatin diffraction efficiency, absorption, and any reflection losses, meets our expectations while the BH3 grating has a peak efficiency around 55% and could likely be improved. Absorption in the grating gelatin and bonding agent probably accounts for a rolloff below 400 nm. The reason for the reduced BH3 performance is not clear, but the most likely explanations are some combination of a misalignment in the peak for each polarization and scattering in the gelatin. This grating has a

slightly hazy appearance compared to the others, and the vendor is working on a replacement to be delivered with BH1.

We also measured the spectral resolution with the calibration unit FeAr hollow cathode lamp at Caltech prior to delivery. The instrument was configured with the small slicer and each of the four available gratings. The camera and grating rotations were configured optimally to span the efficient range of each grating. The data were processed in “light bucket” mode, for which a single spectrum is generated for the entire slicer. We subsequently evaluated the widths of isolated arc lamp lines to compute the spectral resolution. The results are presented in Figure 26 and demonstrate the widely configurable range of KCWI with spectral resolution achieved in excess of 20,000. The spectral resolution varies with wavelength, increasing as expected with the tangent of the grating angle. An example small slicer slit image (similar for all gratings) is shown with 1×1 detector binning for samples of calibration arc data taken in operating conditions at Keck observatory. The measured resolution is slit-limited for all medium and large slicer configurations, which would scale the results in the figure by factors of 0.5 and 0.25 respectively.

5.2. Commissioning

KCWI was commissioned on the Keck II telescope during three observing runs over 10 nights in 2017 as shown in Table 9. Only two of the nights were mainly clear, but many of the required tasks (pointing, de-rotator alignment, N&S testing) could be adequately evaluated with relatively bright stars. During the program, the observatory also commissioned its telescope control system upgrade (Kwok et al. 2016) for KCWI, and an immediate improvement in the blind pointing precision from $\sim 30''$ to $\sim 3''$ was noted, well within the required precision to support N&S observations even with the

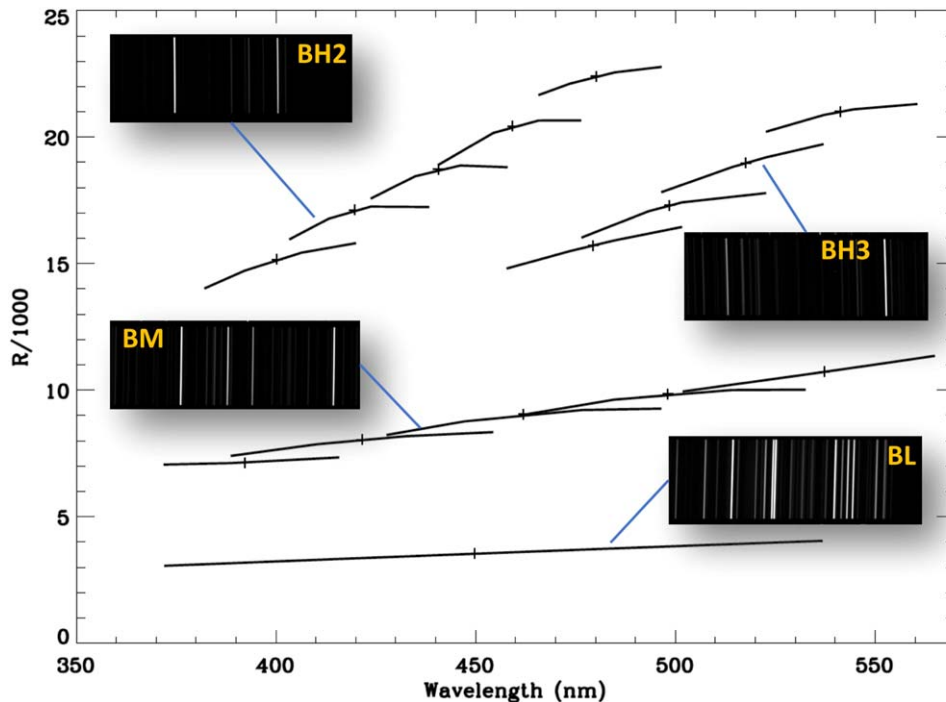


Figure 26. Laboratory-measured spectral resolution of KCWI using the small slicer and each of the available gratings. Points marked with a “+” indicate wavelengths for which the camera and grating were configured. The inset calibration arc images were taken during commissioning using the small slicer and show sample imaging performance for each grating configuration.

Table 9
Commissioning Conditions and Schedule

Date	Lunar Phase	Conditions
Apr 11	15d	Partly cloudy
Apr 13	17d	Partly cloudy
Apr 14	18d	Partly cloudy
May 13	17d	Clear
May 15	19d	Cloudy
May 16	20d	Partly cloudy
Jun 15	20d	Partly cloudy
Jun 18	23d	Partly cloudy
Jun 19	24d	Partly cloudy
Jun 20	25d	Clear

Table 10
KCWI CALSPEC Standards

Star	m_V	R.A.	Decl.
BD +02 3375	9.93	17 39 45.596	+02 24 59.60
BD +25 4655	9.69	21 59 41.975	+26 25 57.40
BD +28 4211	10.51	21 51 11.021	+28 51 50.36
BD +33 2642	10.83	15 51 59.886	+32 56 54.33
Feige 67	11.82	12 41 51.791	+17 31 19.76
G191B2B	11.78	5 05 30.613	+52 49 51.96
HZ 4	14.51	03 55 21.990	+09 47 18.00
HZ 44	11.67	13 23 35.258	+36 07 59.51

8.25 × 20” small slicer. In this section, the key performance verifications for spatial and spectral resolution are described.

Throughput was measured for the white dwarf standards listed in Table 10, all of which are included in the CALSPEC database (e.g., Turnshek et al. 1990; Bohlin et al. 2014). We measured the standards periodically over the course of commissioning with a range of grating, filter, and slicer

combinations, although a large fraction are from the night of June 15.

The analysis was performed on bias-subtracted KCWI raw data, using the pipeline-produced “wavemap” files (created from sets of associated calibration lamp spectra) to identify the wavelength associated with each pixel. The selected standards are the dominant sources in each field. In order to estimate the signal, the columns of each image were sorted according to total integrated brightness including all wavelengths. The brightest 10% of columns (approximately equivalent to two complete slices) were integrated to form the target signal, while the next 10% of columns were integrated to form the sky signal, thus ensuring that the sky was measured in the vicinity of the source. We also estimated the fractional contribution of each sky measurement and rejected those with a contribution greater than 5%. The typical sky brightness measured in this way ranges from 1%–3% of the signal.

The end-to-end throughput of KCWI corrected for telescope and atmosphere for 74 large slicer spectra is presented in Figure 27. Measurements for each configuration are shown with “+” symbols, while the envelope of each set of measurements for a given grating is shown with a thick solid line. Colors are used to identify measurements for each of the four gratings, including an indication of the design band of the BH1 grating currently in fabrication. Pre-ship laboratory measurements of the throughput from Figure 25 are overplotted with filled circles. The raw throughput measured with telescope and atmosphere included is shown with a black dashed line for scale. The losses due to the reflectivity of the three aluminum-coated Keck telescope mirrors cannot be independently measured. We have assumed a measured reflectivity curve for fresh coatings provided by the observatory (typically about 90% in the KCWI band) with approximately 1.5% reflectivity loss for each Keck mirror based on the average 1 year age of

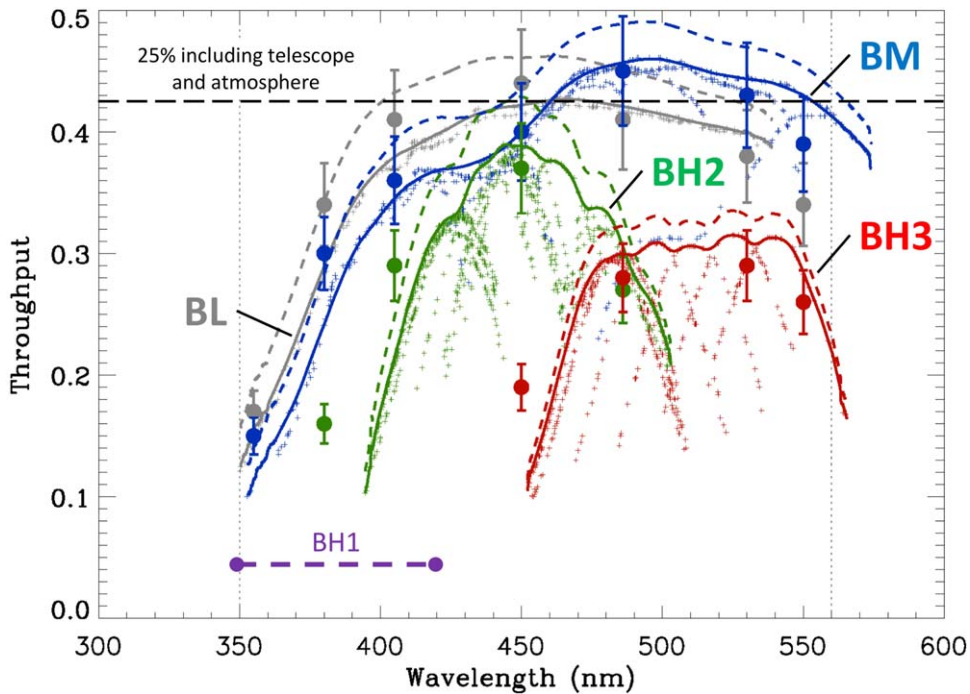


Figure 27. A composite of CALSPEC standard star throughput measurements for the large slicer and four available KCWI gratings, corrected for the telescope and atmosphere. Each grating is shown with a different color, including a placeholder for the BH1 grating. Individual configuration data is shown with “+” symbols, while the envelope of measurements for all on-sky configurations for a given grating is shown with a solid line. In order to indicate the uncertainty in the measurements, a colored dashed line is also shown with extinction $1.5\times$ worse than photometric. Laboratory-measured data points are shown with filled circles. The black dashed line indicates the throughput that would be measured with the telescope and atmosphere included.

the coatings at the time of the KCWI commissioning (K. Tai 2018, private communication). We have also made a correction for atmospheric extinction based on Buton et al. (2013) and the airmass of the standard star at the time of the observation. Since we do not have a large number of measurements on different days, and since the weather was not perfect, we also show the instrument response that would be derived under less than ideal conditions as an estimate for the uncertainty with solid dashed lines. These latter models use the Buton extinction scaled by a factor of 1.5.

The agreement between the pre-ship end-to-end measurements and the on-sky measurements is excellent, especially given the uncertainties. Measurements with the medium slicer are similar, and measurements with the small slicer are a few percent lower. On a bright note, the coating program for KCWI was quite successful, and the complete system exhibits an end-to-end throughput $1.5\times$ – $2.5\times$ higher than PCWI before accounting for the large increase in telescope aperture. With telescope and atmosphere included, the Keck II+KCWI system achieves a peak throughput of over 25%.

5.3. Spectral Resolution

We remeasured the spectral resolution on sky during the first commissioning run. We observed the galaxy NGC 5886 for 3 minutes using the small slicer and BH3 grating centered at 545.5 nm. In this setting, we capture the very bright [O I] atmospheric line at 557.7 nm. We analyzed the line in the same way as the arc spectra in the laboratory (which provides a dithered spectral line measurement as the different slices image the line with different phasing across the detector). We found a spectral resolution $R \sim 19,500$, comparable but slightly below the pre-ship value. Figure 28 shows the “light bucket mode” sky line and our fit to it. We also observed a $\sim 5\%$ variation in

spectral resolution across the 24 slices primarily due to residual focus non-uniformity across the CCD and slit rotation effects. The system is only optically limited for the high-resolution gratings and small slicer. Other configurations are slit limited.

6. Observing Examples

In this section, we present a sample of observations made with KCWI during commissioning. The examples are selected to show a range of KCWI applications and to familiarize the reader with KCWI data and pipeline reconstructions for likely categories of targets.

6.1. First-light Image of M3 with KCWI

Our first example illustrates the high spatial and spectral resolution capability of KCWI pairing the small slicer with the BH2 grating. In panel (A) of Figure 29, we show a spectrum of the core of the globular cluster Messier 3 centered near the $H\beta$ line at 486.1 nm. Panel (B) in the upper right shows the reconstructed image on the small slicer. The reconstructed image is oriented so that the 24 slice images are horizontal (the same as in panel (A)). Blue arrows indicate how slice images are aligned to form representative parts of the image. Full spectral information is contained in the reconstructed image cube. A rich example spectrum of one star with many absorption lines is shown in panel (C). A wide-field image (courtesy Adam Block/Mount Lemmon SkyCenter/University of Arizona) showing the full $18'$ extent of the cluster is shown in panel (D). The high spectral resolution ($R \sim 20,000$) allows us to measure star velocities with a precision of $\leq 15 \text{ km s}^{-1}$ and high sensitivity to many elemental spectral lines. This data cube was obtained with a single 10 minute exposure, with a

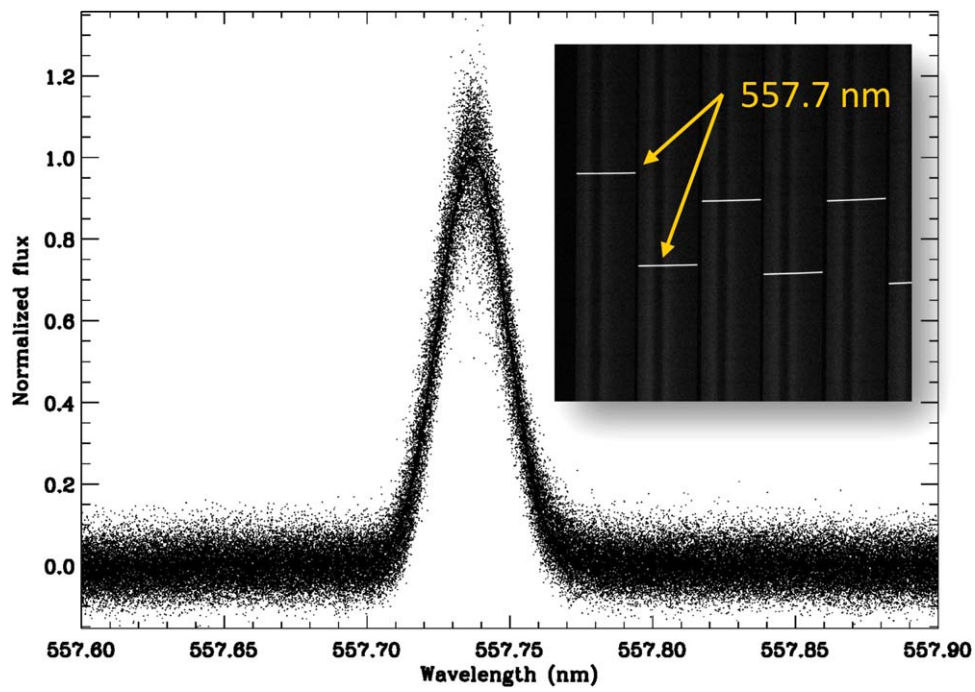


Figure 28. A light bucket mode sky emission-line extraction showing on-sky spectral resolution close to 20,000 with the small slicer and the BH3 grating. The inset shows the bright sky line at 557.7 nm used to generate the curve.

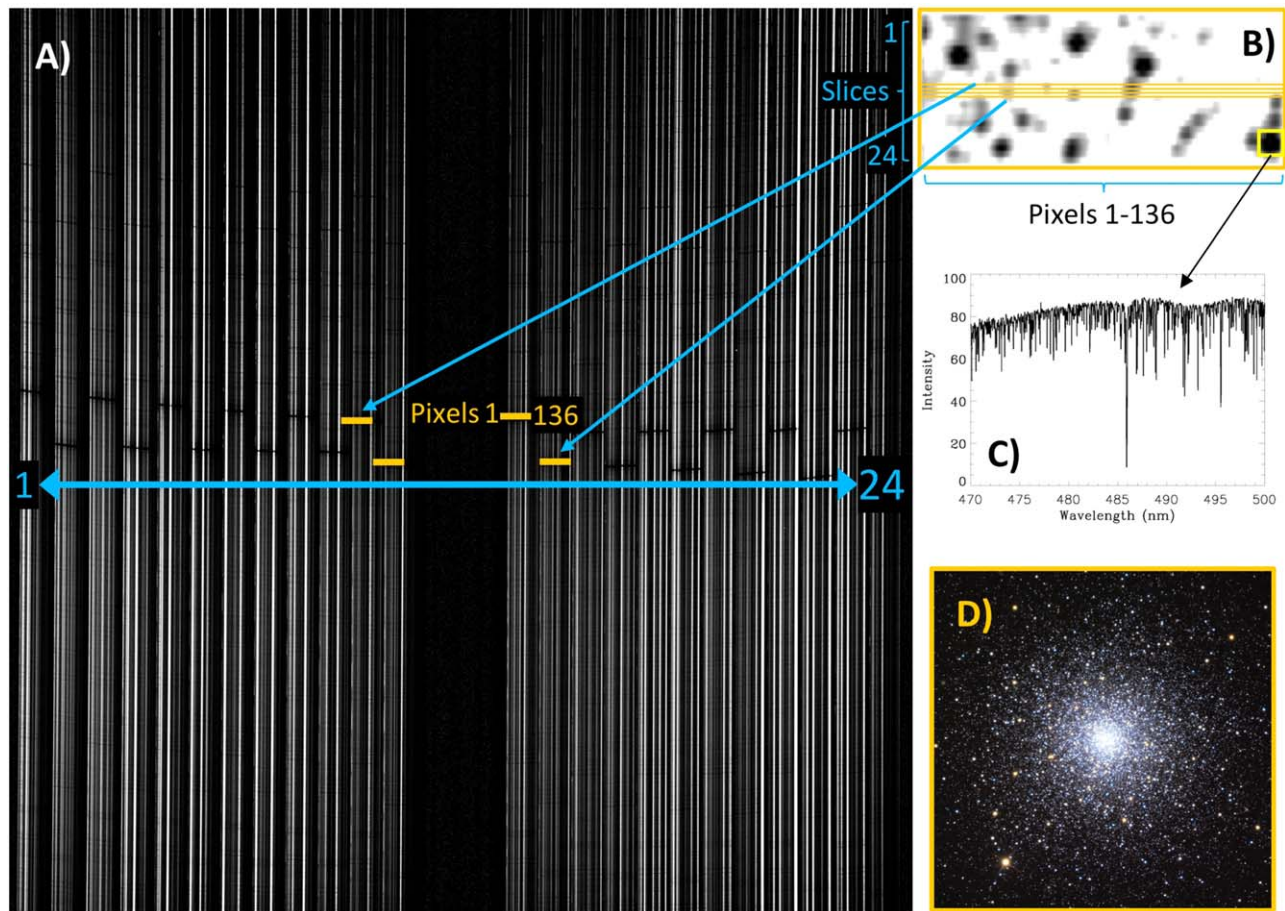


Figure 29. KCWI first-light image of M3. Panel (A) shows the pipeline-reduced `_intf` spectral image. Panel (B) shows the reconstructed $20'' \times 8''/25$ image of the cluster core. Panel (C) shows a representative $R \sim 20,000$ stellar spectrum, and panel (D) shows the full $18'$ extent of the cluster (credit for M3 image: Adam Block/Mount Lemmon SkyCenter/University of Arizona).

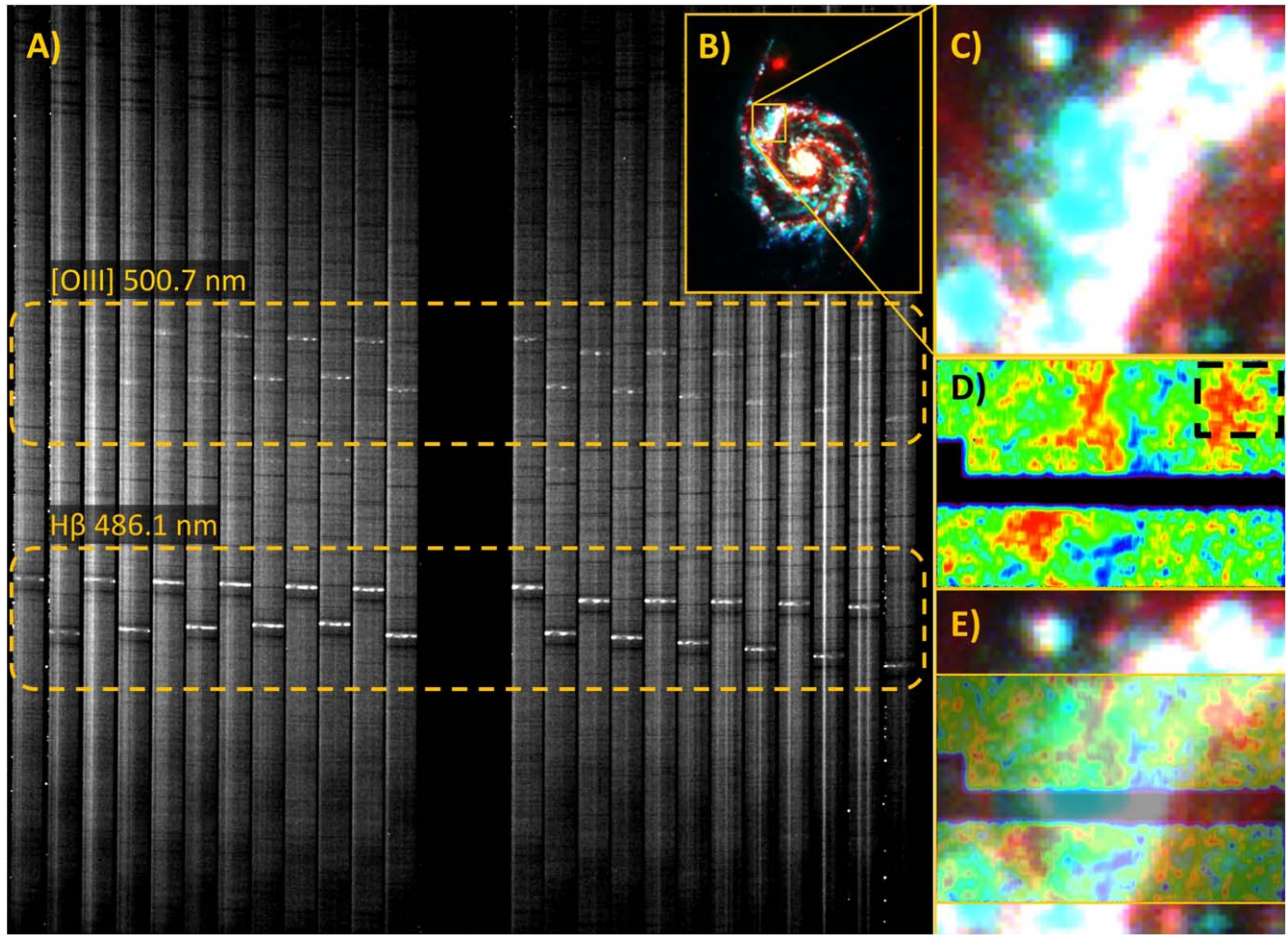


Figure 30. KCWI reveals the direct connection between feedback from massive star formation and the regulation of that star formation. Panel (A): a 300 s KCWI spectrum of M51 with the medium slicer and BH3 grating. Panel (B): a *GALEX*+*Spitzer* image of the Whirlpool Galaxy M51. Panel (C): a blowup of a spiral arm imaged by *GALEX*+*Spitzer* that is the subject of the current KCWI study. Panel (D): a mosaic of KCWI [O III] 500.7 nm images of M51. The footprint of the medium slicer is shown with a black dashed rectangle. Panel (E): the KCWI mosaic overlaid on the *GALEX*+*Spitzer* image showing excellent correlation between the KCWI emission and the *GALEX* UV emission.

total field size of $20'' \times 8.25''$. The seeing-limited stellar images are approximately $0''.7$ wide.

6.2. Feedback from Star Formation in a Spiral Arm

One of the most important problems in understanding star formation and galaxy evolution is how feedback from massive stars regulates star formation. KCWI can directly measure gas that has been shocked by massive star winds and supernova explosions. In the image montage shown in Figure 30, we focus on a spiral arm of the Whirlpool Galaxy, Messier 51. The spiral arm is created by a spiral density wave that triggers a burst of star formation.

This example shows a mosaic of 300 s images collected with the medium slicer and the high-dispersion BH3 grating demonstrating excellent spatial ($\sim 0''.7$) and spectral ($R \sim 10,000$) resolution. The set of observations is comprised of 11 tiles. An example tile is shown in panel (A) of Figure 30, in which the emission from H β and O III is identified. In panel (B), we show a $7' \times 11'$ *GALEX* UV (blue) and *Spitzer* IR (red) overlaid image of M51. A box superimposed on the image shows the region tiled by KCWI and is expanded in panel (C). In this blowup, we can see the time sequence of events after the wave passes as stars move from lower

right to upper left. Massive stars are traced by *GALEX* UV, and gas and dust are traced by *Spitzer* IR. Star formation is triggered by the spiral wave shock, creating a region of high-density gas and dust and dust-obscured young stars (red = high IR to UV). The stars begin to feedback against the gas and dust, allowing more UV to escape (yellow = intermediate IR to UV). Finally, the stars begin to explode in supernovae after 10–20 million years and clear out the dust and gas (blue = high UV to IR).

In panel (D), we show a mosaic of 11 KCWI pointings (a region approximately $68'' \times 44''$ in size) with a gap that will be filled in at a later time. KCWI traces the shocked, high-velocity gas energized by these supernovae. Red regions are high-velocity shocked gas. These are correlated with the UV-bright regions as shown in panel (E), forming a web of shocked gas walls as the supernova shock waves push the gas away from the star-forming regions and up and away from the galaxy's disk. As the gas is disrupted, star formation stops (the arm peters out). This is the fundamental process that regulates star formation efficiency, and with this new KCWI result, this process is now revealed and provides missing input to galaxy formation models.

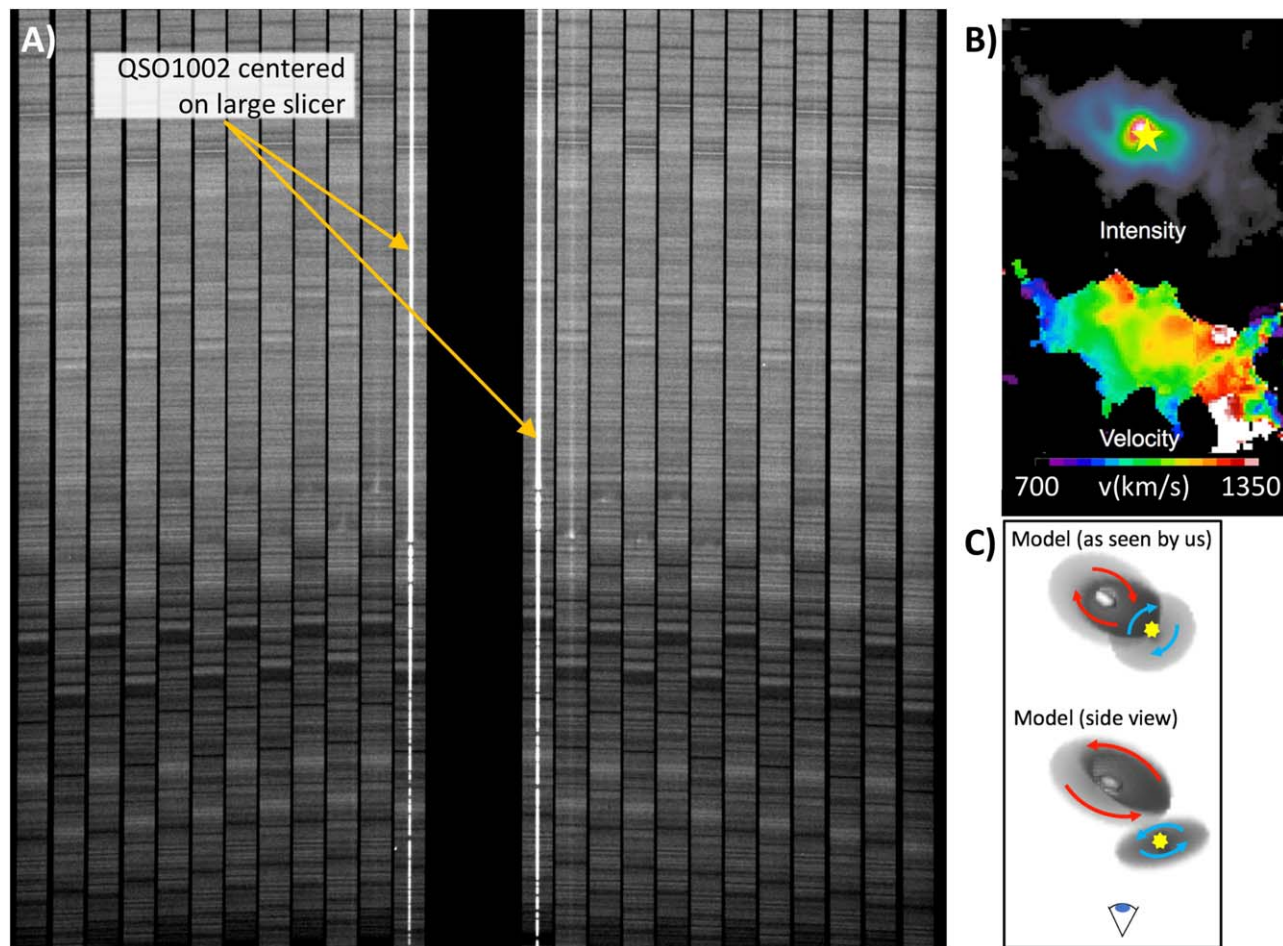


Figure 31. Two giant disks illuminated by QSO 1002. Panel (A) shows a 1200 s $_intf$ spectral image with the bright quasar spectrum centered on the large slicer with the BM grating configured for the spectral band near 449 nm. Panel (B) shows the reconstructed image on the slicer (top) and velocity map (bottom), which was determined by the velocity associated with the $H\beta$ 486.1 nm emission line. Panel (C) shows a model that explains the emission as seen from our vantage point.

6.3. QSO-illuminated Interacting Disks

Our third example shows the large slicer with BM grating to illustrate the low surface brightness capability of KCWI. Two giant disks illuminated by the quasi-stellar object QSO 1002 are revealed in a single hour of exposure. KCWI observes the hydrogen $H\beta$ line emission from this distant object, and the redshift of the emission line probes the velocity of the gas in the system. A 20 m spectrum of the centered quasar and environs is shown in panel (A) of Figure 31. A narrowband reconstructed intensity image (top, with the QSO position marked by a yellow star) and the gas velocity (bottom) are shown in panel (B) of the figure. The bright QSO is model-subtracted and the background removed using a portion of the field known (from previous PCWI measurements) to be free from emission. Red indicates gas moving away from us (redshifted), while blue/green indicates gas moving toward us. The image and velocity maps are consistent with the model shown in panel (C). The model consists of two giant (60 kpc and 80 kpc) disks, rotating approximately with the same spin direction, and orbiting each other also with the same spin sense. The lower disk has the QSO in its center. The interaction of the two disks produces large torques, and gas flows into the disk centers. The gas flow into the center of the lower disk is feeding the QSO. The light from the QSO exits in conical beams, which only illuminate part of the companion disk (darker area of the

model and brighter area of the image). KCWI can measure the disk size, rotation speed, gas inflow speed, and approximate separation. This detection reveals both the presence of large gaseous rotating disks in the distant universe and their role in generating the most luminous objects in the universe.

7. Discussion

KCWI has been successfully constructed and installed on Maunakea at the 10 m Keck II telescope. The instrument is performing very well and is poised with its unique configurability and available N&S mode to open a new window to the low surface brightness universe. Spectral resolution is excellent, and the spatial resolution is pixel-limited, taking full advantage of the excellent seeing available on the mountain. The peak throughput is quite high for the BL, BM, and BH2 gratings, and plans are underway to complete the grating suite with the BH1 installation and a BH3 upgrade. The recent control system upgrade at the Observatory will enable the instrument to efficiently employ its N&S observing mode for the most challenging faint targets.

A conceptual design of the red arm was presented at the KCWI Preliminary Design Review in 2011. Now that the phased delivery of the blue channel is successfully in place, work on the detailed design of the funded red channel is underway. The new arm will include a large dichroic to replace

the FMD fold mirror as well as an updated guider design that is compatible with red and blue science from 350–1050 nm. A second camera, detector, and red-optimized grating suite are planned for the available volume on the top of the bench behind the FMD fold mirror.

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Facilities: GALEX, Hale, Keck:II (KCWI), *Spitzer*.

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