

The key management of direct/external modulation semiconductor laser response systems for relative intensity noise control

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ABSTRACT

This study outlines the management of either direct or external modulation semiconductor laser systems for the key solution of bit rate up to 25 Gb/s under relative intensity noise (RIN) control. The bias and modulation peak currents based laser rate equations are optimized to achieve max Q factor and min bit error rate (BER) using first proposed model and optical/electrical signal power, optical/electrical signal to noise ratio are also enhanced using second proposed model. The percentage enhancement ratio in max. Q-factor and min. BER using first proposed model ranges from 53.25 % to 71.63 % in compared to the previous model. In the same way, by using second proposed model, the electrical signal power at optical receiver is enhanced within the range of 48.66 % to 68.88 % in compared to the previous model. Optical signal/noise ratio (OSNR) after optical fiber cable (OFC), signal/noise ratio (SNR) after electrical filter are measured with using different electrical pulse generators and electrical modulators at the optimization stage.

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1. INTRODUCTION

They have analyzed the dynamics and noise of semiconductor laser communication systems for optical access television communication systems [1-7]. The typical frequency spectra of relative intensity noise are studied with modulation. When the modulation index is over 50%, the modulated signal is clipped and the noise levels will increase. Relative intensity noise and modulation index equations are modeled mathematically. As well as small signal modulation transfer function is covered [8-17]. The modulated signal response of the laser is also characterized. The variations between modulation index and modulation channel frequency are reviewed. The relation between RIN frequency spectra and different modulation types are studied [1, 18-22]. They have presented the optimum parameters for the control of noise and distortion in semiconductor laser under analog modulation. The laser rate equations are modeled and integrated numerically. The relation between modulation index/channel, number of loaded channels and fiber length are reviewed mathematically [23-28]. The increase of fiber length limits the modulation index per channel and

number of loaded channels. The total of carrier to noise ratio of semiconductor laser is estimated for fiber access communication television. Optimum noise and distortion of semiconductor laser are covered [2, 3].

They have proposed the modulation semiconductor laser amplifier response by using optiwave simulation. The resonance frequency of laser is estimated for known threshold current, modulation peak current, and carrier lifetime based on laser rate equations [29-38]. The effect of increase modulation frequency above resonance at data rate of 10 Gb/s is reviewed [4-6].

2. MODEL DESCRIPTION AND RESEARCH METHOD

The view of external laser system modulation is shown in Figure 1 (external modulation), where the user sequence generator is responsible for generating a series of bit sequence. The series of bits is represented by electrical pulse generators and then directed to low pass Gaussian filter to remove the ripple from the original signal. The filtered signal is routed to laser rate equations in order to convert the electrical signal to optical signal under the control of both modulation peak current and bias current. The Mach Zehnder modulators combine both the optical signal from laser and electrical signal from electrical pulse generator. The modulated signal is then directed to the optical fiber cable channel and then to optical attenuator which increases the signal losses level. The signal is then directed to optical receiver to convert the light signal to electrical signal.

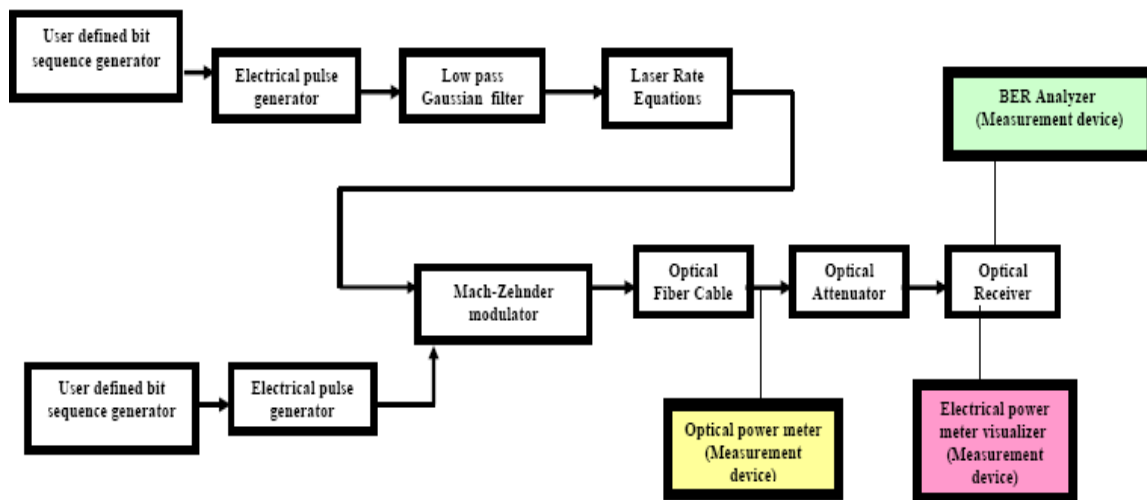


Figure 1. First proposed simulation model (external modulation)

Optical power meter measures the optical signal power through the optical fiber communication channel. Electrical power meter visualizer tests the electrical signal power at the receiving side. BER analyzer tests the max. Q-factor and minimum BER values at the optical receiver side. Figure 2 shows the direct modulation method of laser systems. The pseudo random bit sequence generator generates a random bit sequence and is directed to both electrical pulse generator and electrical modulators to be reshaped. The reshaped signal is directed to laser rate equations which converts the electrical signal to optical signal under the control of bias and maximum peak currents. The optical signal is then routed to optical fiber cable channel and then to PIN photo-detector which converts the optical signal to electrical signal. The converted signal is directed to band pass Gaussian filter in order to remove the unwanted signal (noise signal) for the original signal and then directed to 3R regenerator in order to achieve retiming, reshaping, regeneration for the filtered signal. WDM analyzer tests the optical signal to noise ratio through the optical fiber cable channel and noise power through optical fiber. Optical power meter tests the optical signal power at optical fiber cable channel. BER analyzer test the max. Q-factor and min BER values. Electrical carrier analyzer after band pass Gaussian filter measures the signal to noise ratio (signal power/noise power). Oscilloscope visualizer after both PIN photodetector and band pass Gaussian filter tests maximum signal amplitude variations against bit period time variations. As well as electrical power meter visualizer after PIN photodetector measures electrical signal power.

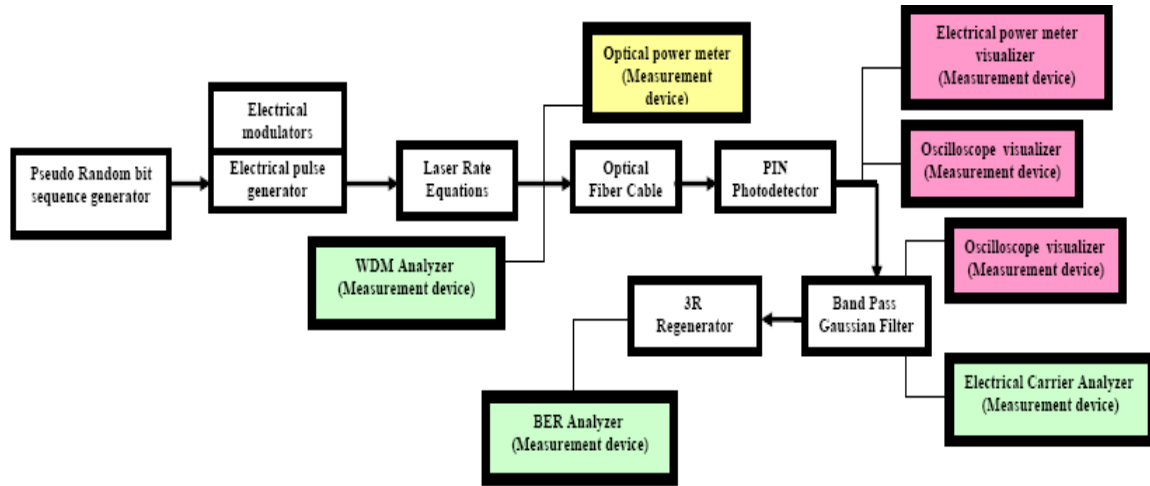


Figure 2. Second proposed simulation model (direct modulation)

3. PERFORMANCE ANALYSIS WITH DISCUSSIONS

We have simulated the direct/external modulation laser rate equation systems for the management of relative intensity noise (RIN) by the control of bias current and modulation peak current. Different electrical signal pulse generators and modulators are used in order to measure the signal power level with respect to noise power level. Optical signal to noise ratio after optical fiber cable channel, max. Q-factor, Min. BER, signal to noise ratio after receiver side, signal amplitude and power are also measured under the controlling parameters in Table 1. The important performance parameter for direct/external modulation systems are measured at the optimization stage of laser rate equations by setting the bias current and modulation peak current at the values of ($I_{bias}=100$ mA, $I_m=20$ mA).

Table 1. List of variables used in the proposed model [7-10].

Components	Parameters	Values/units
Laser rate equations	Frequency	193.1 THz
	Power	0 dBm
	Power at bias current	-30 dBm
	Bias current (I_b)	50 mA-150 mA
	Modulation Peak current (I_m)	20 mA-100 mA
	Threshold current	33.45 mA
	Threshold power	0.035 mW
	Quantum efficiency	0.9
PAM modulator, QAM modulator, PSK modulator, DPSK modulator, FSK modulator, CPFSK modulator, OQPSK modulator, MSK modulator	Frequency	500 MHz
	Amplitude	1 a.u.
	Bias	0 a.u.
	Width	0.5 bit
	Extinction ratio	30 dB
Mach Zehnder Modulator	Symmetry factor	-1
	Depth	100 dB
Optical fiber cable	Fiber length	20 Km
	Channel bit rate	25 Gb/s
	Attenuation at 1550 nm	0.2 dB/Km
	Dispersion at 1550 nm	16.75 ps/nm/Km
	Dispersion slope at 1550 nm	0.075 ps/nm ² /Km
	Effective area at 1550 nm	80 μm^2
	Dark current	0 nA
PIN photodetector	Responsivity	1 A/W
	Frequency	500 MHz
Band Pass Gaussian Filter	Bandwidth	100 MHz
	Insertion loss	0 dB
	Depth	100 dB
	Order	1
	Attenuation	27 dB
Optical attenuator	Insertion loss	0 dB
	Depth	100 dB
Low pass Gaussian filter	Depth	100 dB
	Order	1

The results are approved as clarified in Figure. 3-14 based on variables in Table 1. Figure 3 covered the max Q-factor values for different electrical signal pulse generators at the transmitter side based previous model and first proposed model with external modulation. It is observed that raised cosine pulse generator gives better max. Q-factor than other electrical signal generators at the optimization current stage of laser rate equations. Figures 4 and 5 have presented the max Q-factor and min BER values by using eye diagram analyzer with raised cosine pulse generator. Where the max. Q-factor value reaches to 10.53 and min BER value reaches to 9.45×10^{-26} .

Figure 6 outlines the electrical signal power variations after optical receiver against different electrical signal pulse generators for both previous and second proposed models (direct modulation) at the optimization values of bias current (100 mA), and modulation peak current (20 mA). NRZ pulse signal generator presented better performance in maximum electric signal power than other pulse generators whose it value reaches to 485.76. Enhancement percentage ratio in electrical signal power by using NRZ pulse generator is reached to 60.78 % in compared to previous model. In addition to optical signal power after optical fiber cable in relation to both modulation peak current and bias current based laser rate equations (second proposed model) is shown in Figure. 7. It is found that by increasing bias current and modulation peak current parameters of laser rate equations, this results in increasing optical signal power at optical fiber cable channel.

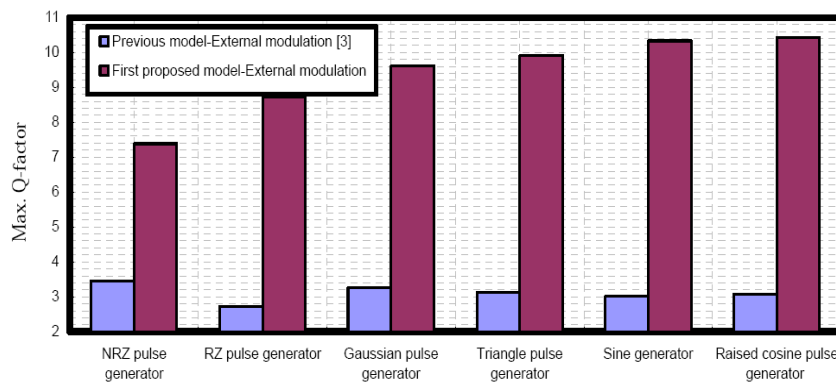


Figure 3. Max Q-factor with different electrical signal pulse generators for both previous and first proposed model with external modulation at the optimization values

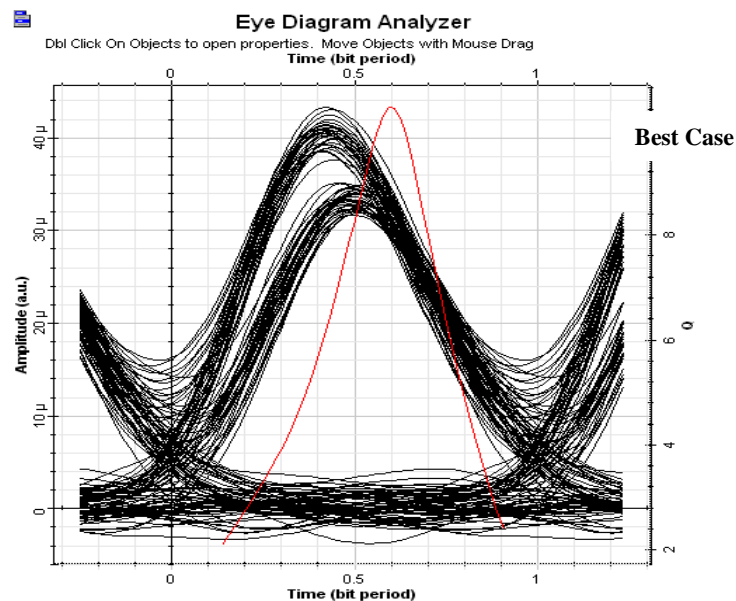


Figure 4. Maximum Q- factor with Raised cosine pulse generator based external modulation using eye diagram analyzer at the optimization stage (First proposed model)

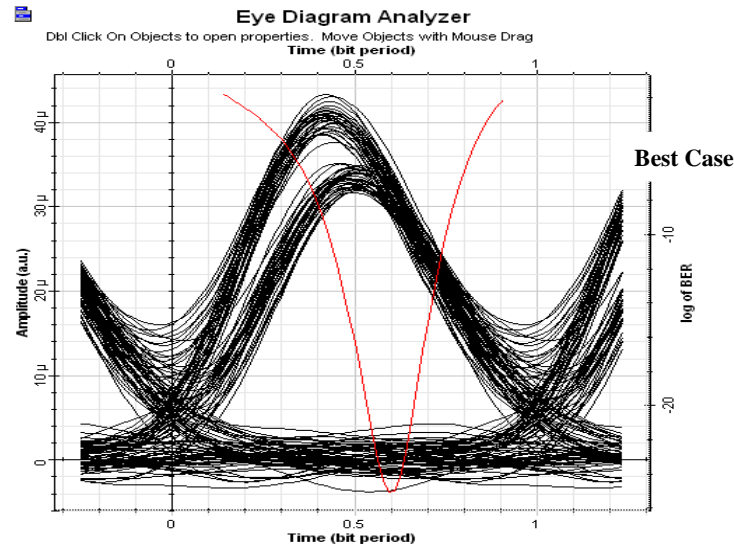


Figure 5. Minimum BER with Raised cosine pulse generator based external modulation using eye diagram analyzer at the optimization stage (First proposed model)

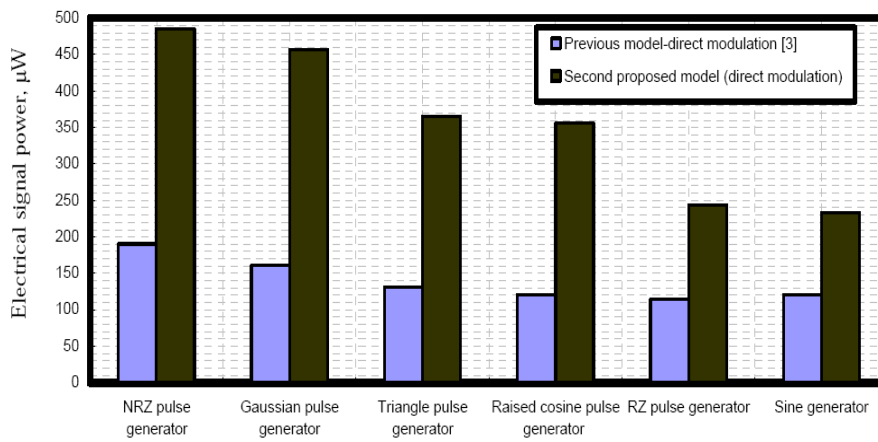


Figure 6. Electrical signal power variations after optical receiver versus different electrical signal pulse generators for both previous and second proposed models (direct modulation) at the optimization values

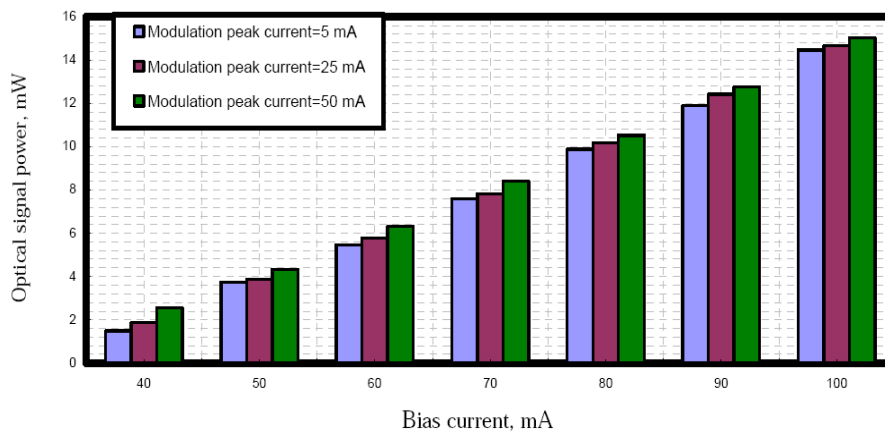


Figure 7. Optical signal power after optical fiber cable in relation to both modulation peak current and bias current based laser rate equations (Second proposed model)

Figure 8 shows the relation between optical signal to noise ratio after optical fiber cable channel and modulation peak, bias current variations. It is clear that by increasing modulation peak current, this leads to decrease in optical signal to noise ratio for low bias current values (50 mA, 100 mA) but for bias current at a value of 150 mA, the relation is inversely condition. So we recommend for the choice bias current with a value of 100 mA at the optimization stage. Figure. 9 covered the signal to noise ratio after band pass Gaussian filter (BPGF) in relation to both modulation peak current and bias current based laser rate equations by using second proposed model. Signal to noise ratio after band pass Gaussian filter is enhanced with maximum modulation peak current of 50 mA at a constant bias current. Signal to noise ratio is enhanced also with increasing bias current expect for modulation peak current value of 5 mA, the relation is inversely condition.

Figures 10 and 11 show the variation of maximum signal amplitude after PIN photodetector, maximum signal amplitude after BPGF against the variations of both modulation peak current and bias current based laser rate equations by using second proposed model. It is clear that the increase in bias current, this results in increasing of maximum signal amplitude after PIN photodetector at constant modulation peak current. It is preferred to choose minimum modulation peak current value of 50 mA in this case in order to achieve maximum signal amplitude after receiver side. Figure 12 outlines the variation of electrical signal power after PIN photodetector against the variations of both modulation peak current and bias current based laser rate equations by using second proposed model. It is observed that the best choice of bias current value at 100 mA and modulation peak current of 50 mA in order to achieve maximum electrical signal power at receiver side. But we recommend to choose modulation peak current less than 50 mA, because the higher modulation peak current, the higher noise power is presented. Figures 13 and 14 covered the optical signal/noise ratio at optical fiber cable and signal/noise ratio after band pass Gaussian filter in relation to different electrical signal pulse generators/electrical signal modulators integrated with laser rate equations at the optimization values by using second proposed model. Both optical signal/noise ratio at fiber cable channel and signal/noise ratio are enhanced better percentage performance by using electrical signal modulators than electrical signal modulators by about 15.88 %.

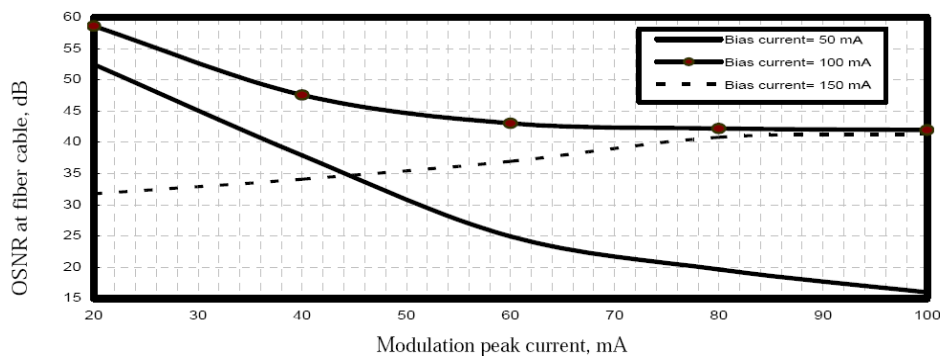


Figure 8. Variations of optical signal to noise ratio at optical fiber cable against variations of both bias current and modulation peak current based laser rate equations (Second proposed model)

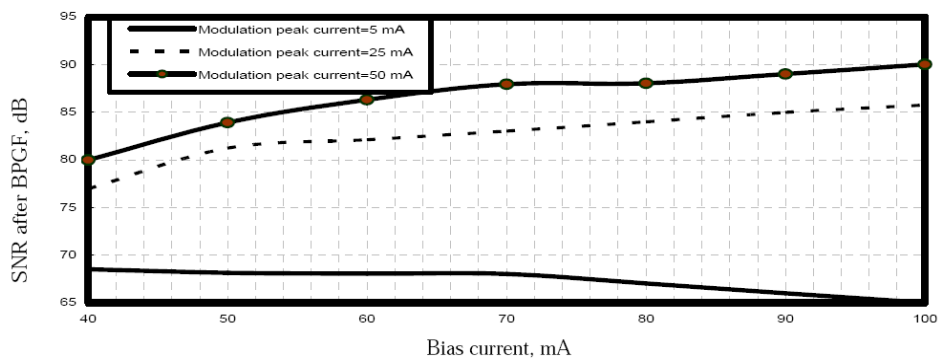


Figure 9. Signal to noise ratio after band pass Gaussian filter (BPGF) in relation to both modulation peak current and bias current based laser rate equations (Second proposed model)

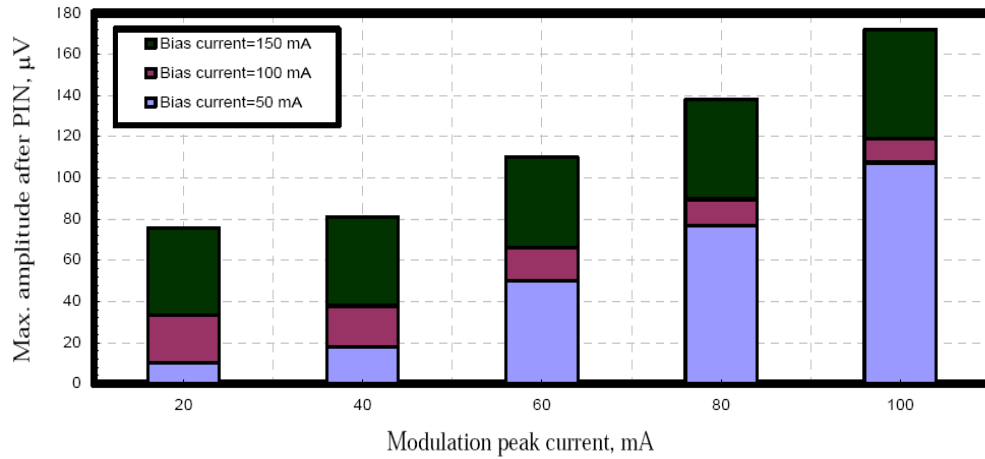


Figure 10. Variation of maximum signal amplitude after PIN photodetector versus the variations of both modulation peak current and bias current based laser rate equations (Second proposed model)

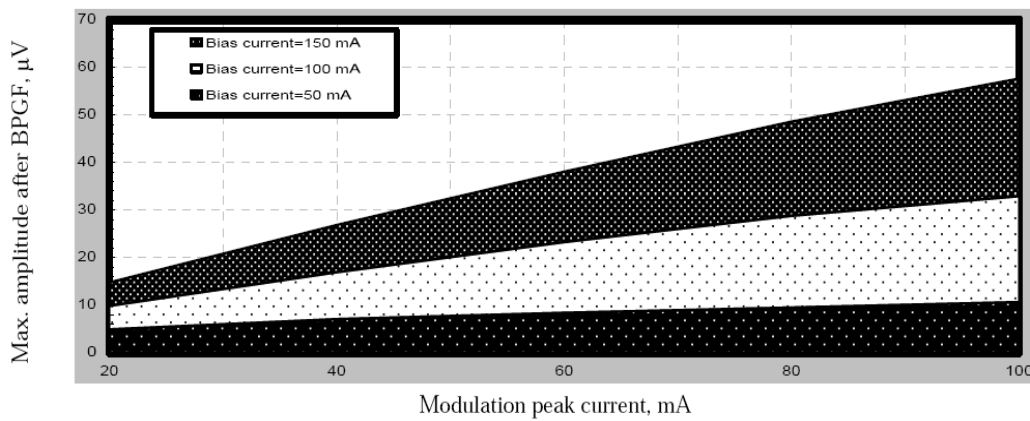


Figure 11. Variation of maximum signal amplitude after BPGF versus the variations of both modulation peak current and bias current based laser rate equations (Second proposed model)

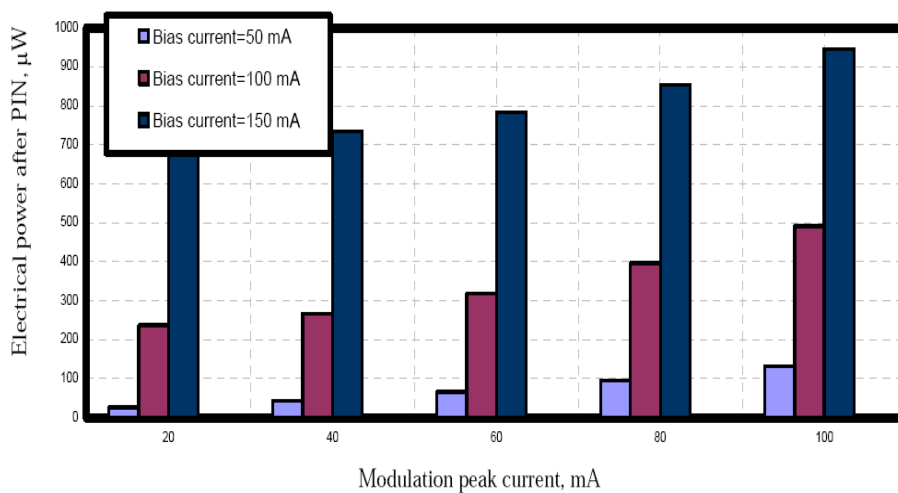


Figure 12. Variation of electrical signal power after PIN photodetector versus the variations of both modulation peak current and bias current based laser rate equations (Second proposed model)

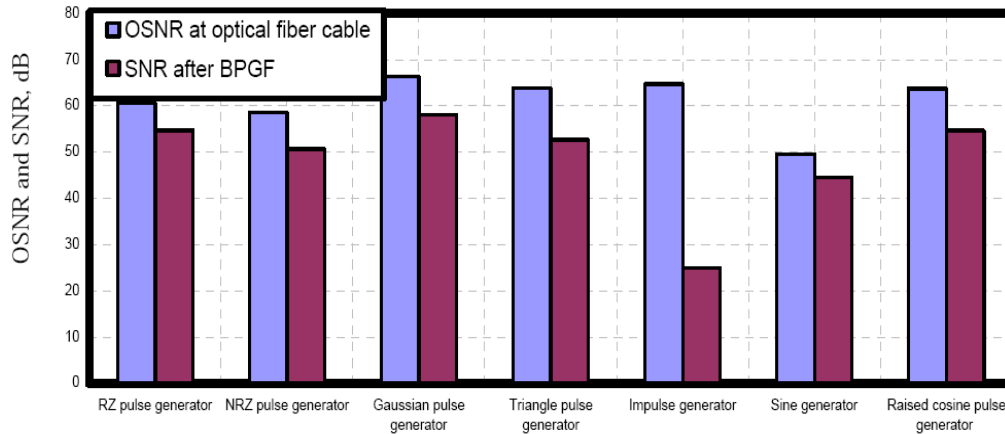


Figure 13. Optical signal/noise ratio at optical fiber cable and signal/noise ratio after band pass Gaussian filter in relation to different electrical signal pulse generators integrated with laser rate equations at the optimization values

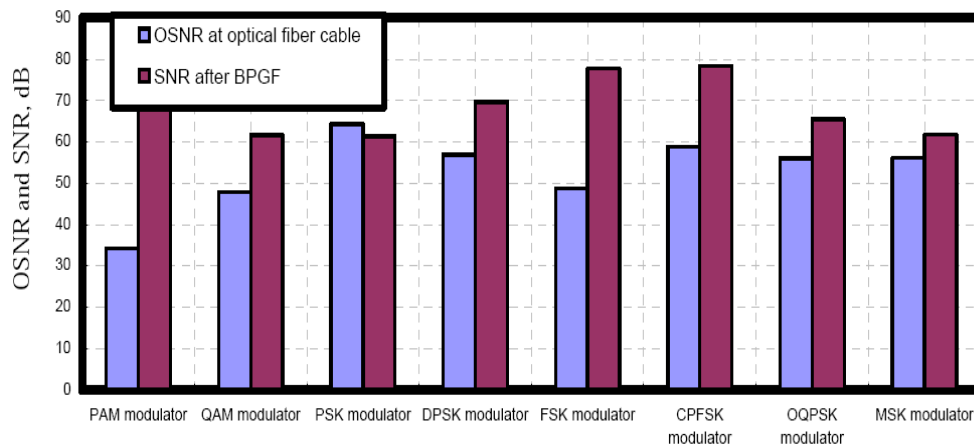


Figure 14. Variations of optical signal to noise ratio at optical fiber cable and signal to noise ratio after band pass Gaussian filter against different electrical modulators integrated with laser rate equations at the optimization values

4. CONCLUSION

We have modeled and developed two proposed direct/external modulation laser systems for the key management of relative intensity noise control for the bit rates up to 25 Gb/s. The laser rate equations operating parameters are optimized through bias current of 100 mA and modulation peak current of 20 mA. The first proposed model (external modulation) has presented better max. Q-factor and min. BER than previous model (external modulation) at the same simulation parameters for different signal pulse generators. Enhancement percentage ratio in max. Q-factor and min. BER values ranges from 53.25 % to 71.63 % by using first proposed model over the previous model. In addition to electrical signal power is enhanced by using second proposed model (direct modulation) with the previous model. Enhancement percentage ratio in electrical signal power ranges from 48.66 % to 68.88 % by using second proposed model over the previous model. Raised cosine pulse generator is employed efficiently in both proposed models for the percentage enhancement ratio of max. Q-factor, min. BER, and electrical signal power over the previous models (either direct or external modulation). OSNR at optical fiber cable and SNR at optical receiver are enhanced by using electrical modulators (external modulation) than pulse generators (direct modulation) at the optimization case. It is evident that noise power reduction percentage ratio is reached to 37.34 % by using raised cosine pulse generator integrated with optical modulator (external modulation).

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