The Seismic Category I Structures Program Results for FY 1987

Prepared by
C. R. Farrar, J. G. Bennett, W. E. Dunwoody, W. E. Baker*

Los Alamos National Laboratory
Los Alamos, NM 87545

*University of New Mexico
Albuquerque, NM 87131

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E. G. Endebrock, R. C. Dove, and W. E. Dunwoody, "Analysis and Tests on Small-Scale Shear Walls—FY 82 Final Report," Los Alamos National Laboratory report LA-10443-MS, NUREG/CR-4274 (September 1985).

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C. R. Farrar, J. G. Bennett, W. E. Dunwoody, and W. E. Baker, "Static Load Cycle Testing of a Low-Aspect-Ratio Six-Inch Wall TRG-Type Structure TRG-4-6 (1.0, 0.25)," Los Alamos National Laboratory report LA-11422-MS, NUREG/CR-5222 (June 1989).

ABSTRACT

The accomplishments of the Seismic Category I Structures
Program for FY 1987 are summarized. These accomplish-
ments include the quasi-static load cycle testing of large
shear wall elements, an extensive analysis of previous data
to determine if equivalent linear analytical models can
predict the response of damaged shear wall structures, and
code committee activities. In addition, previous testing
and results that led to the FY 1987 program plan are dis-
cussed and all previous data relating to shear wall stiff-
ness are summarized. Because separate reports have already
summarized the experimental and analytical work in FY 1987,
this report will briefly highlight this work and the
appropriate reports will be referenced for a more detailed
discussion.

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THE SEISMIC CATEGORY I STRUCTURES PROGRAM
RESULTS FOR FY 1987

by

Charles R. Farrar
Joel G. Bennett
Wade E. Dunwoody
and William E. Baker

I.   INTRODUCTION

The Seismic Category I Structures Program is being carried out at the
Los Alamos National Laboratory under sponsorship of the U.S. Nuclear Regulatory
Commission (NRC), Office of Nuclear Regulatory Research. Its objective is to
investigate the dynamic response of Seismic Category I reinforced concrete
structures (exclusive of containment) that are subjected to seismic loads
beyond their design basis. The program, as originally conceived, is a
combined experimental/analytical investigation with heavy emphasis on the
experiment component to establish a good data base. A number of meetings and
interactions with the NRC staff have led to a set of specific program objec-
tives, which are as follows:

1.   Address the seismic response of reinforced concrete Category I
     structures other than containments;

2.   Develop experimental data for determining the sensitivity of struc-
     tural behavior in the elastic and inelastic response range of
     Category I structures to variations in configuration, design prac-
     tices, and earthquake loading;

3.   Develop experimental data to enable validation of computer pro-
     grams used to predict the behavior of Category I structures during
     earthquake motions that cause elastic and inelastic responses;

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4. Identify floor response spectra changes that occur during earthquake
    motions that cause elastic and inelastic structural responses; and

5. Develop a method for representing damping in the inelastic range,
    and demonstrate how damping changes when structural response goes
    from the elastic to the inelastic ranges.

The prevailing feature of the typical structure under investigation is
that shear rather than flexure is dominant, that is the ratio of displacement
values calculated from terms identified with shear deformation to the values
contributed from bending deformation is one or greater. These buildings are
therefore called "shear wall" structures. The background of the program and
its status leading to the work reported here will briefly be summarized below.

II. FY 1980 TO FY 1986 ACTIVITIES

The Seismic Category I Structures Program began in FY 1980 with an inves-
tigation that identified the typical nuclear shear wall structure and its
characteristics (stiffnesses, frequencies, etc.) as being the most important
and least understood seismic resisting structure. A combined experimental/
analytical plan for investigation of the dynamic behavior of these structures
was laid out as described in Ref. 1. During the first phase, the program
concentrated on investigating isolated shear wall behavior using small models
(1/30 scale, 1-in. wall thickness, see Fig. 1) that could be economically con-
structed and tested both statically and dynamically. This work is reported on
in Ref. 2. During this early phase of the program, a Technical Review Group
(TRG), consisting of nationally recognized seismic and concrete experts on nu-
clear civil structures, was established to both review the progress and make
recommendations regarding the technical direction of the program. The recom-
mendations of this group have been evaluated in light of the needs of the NRC
and, where possible, have been carefully integrated into the program.

Following the isolated shear wall phase, the program began testing and
evaluating three-dimensional (3-D) box-like structures that represented
idealized diesel generator buildings (see Fig. 2). It was recognized from the
outset that scale model testing of concrete structures is a controversial
issue in the U.S. civil engineering community. Thus, two sizes of structures
were tested in an effort to demonstrate scalability of results. This work is
reported on in Refs. 3-5. Other variables of interest, especially the effect

a. ONE-STORY STRUCTURE

b. TWO-STORY STRUCTURE
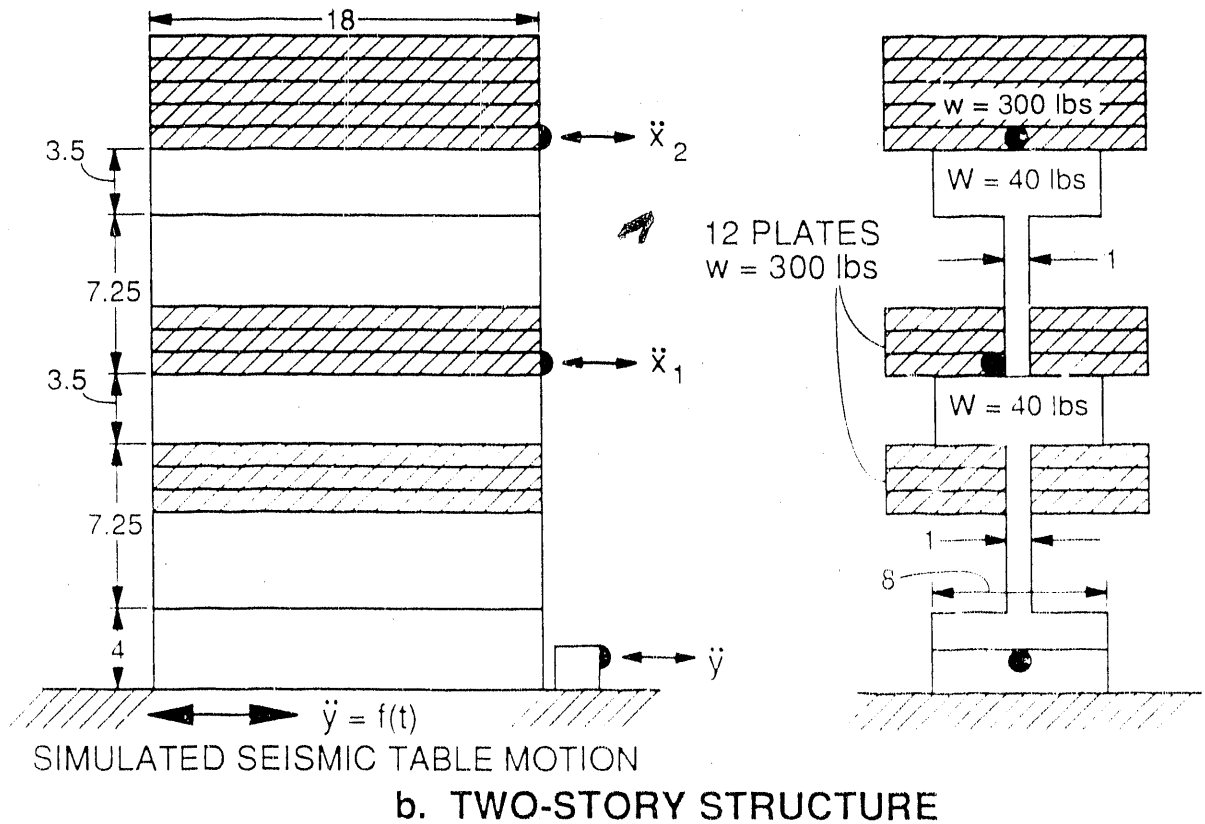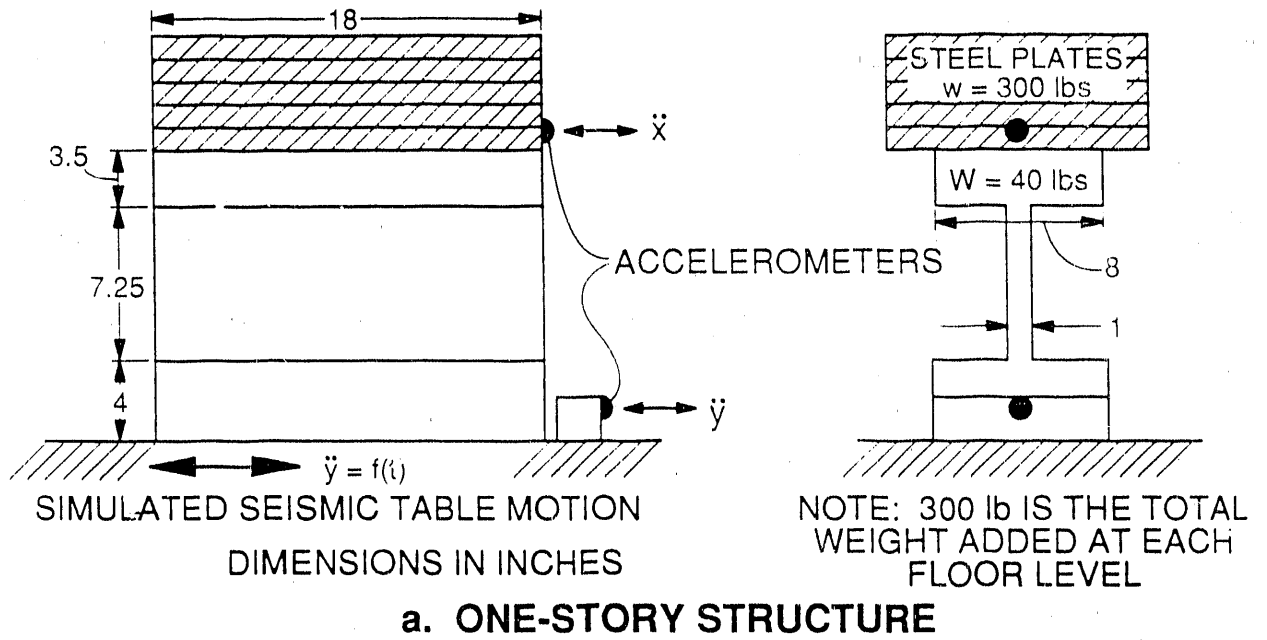
Fig. 1. Isolated shear wall structure.

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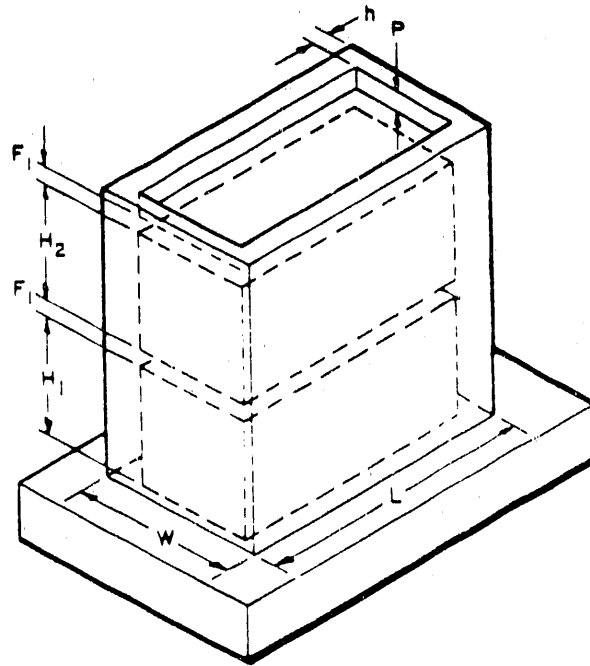
	h, F_1, F_2	W	L	H_1 & H_2	P	W/STORY*(lb)
1/30 SCALE	1 in.	10 in.	18 in.	7.25 in.	1 in.	47.7
1/10 SCALE	3 in.	30 in.	54 in.	21.75 in.	3 in.	1286
PROTOTYPE	30 in.	25 ft	45 ft	18 ft, 1.5 in.	30 in.	1,286,000

*BASE NOT INCLUDED
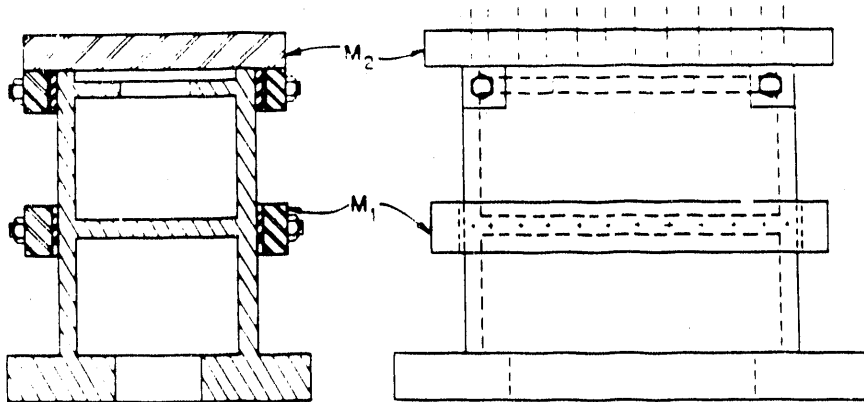
STRUCTURE	SCALE	M_1 (lbs)	M_2 (lbs)
3D-10-2	1/30	228	231
3D-11-2	1/30	228	231
3D-12-2	1/30	236	166
CERL 1	1/10	1285	1330
CERL 2	1/10	1285	906

Fig. 2. Diesel generator building model.

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of the number of stories, were investigated by constructing, analyzing, and testing small-scale structures representative of a typical three-story auxiliary building shown in Fig. 3. The results obtained from the tests of these structures are given in Ref. 6.

Although a number of results on items such as aging (cure time), effect of increasing seismic magnitude, etc., have already been reported, the two most important and consistent conclusions coming out of the data from this program are (1) the scalability of the results between microconcrete models of different sizes was illustrated both in the elastic and inelastic range and (2), the so-called "working load" secant stiffness of the models was lower than the computed uncracked cross-sectional values by a factor of about 4. The term "working load" is meant as loads that produce stress levels equivalent to at least the operating basis earthquake and up to the safe shutdown earthquake.

During their review of this program, the TRG pointed out the following:

1. Design of prototype nuclear plant structures is normally based on an uncracked cross-section strength-of-materials approach that may or may not use a "stiffness reduction factor" for the concrete, but, if it does, then that factor is never as large as 4.

	h, F_1, F_2, F_3	W	H_1, H_2, H_3	Wt/STORY* (lb)
1/42 SCALE	1 in.	26 in.	10 in.	140
1/14 SCALE	3 in.	78 in.	30 in.	3780
PROTOTYPE	42 in.	1092 in.	42 in.	10,372,000

*BASE NOT INCLUDED

STRUCTURE	M_1 (lbs)	M_2 (lbs)	M_3 (lbs)
1/42-SCALE	500	460	395
1/14-SCALE	3334	3060	2631
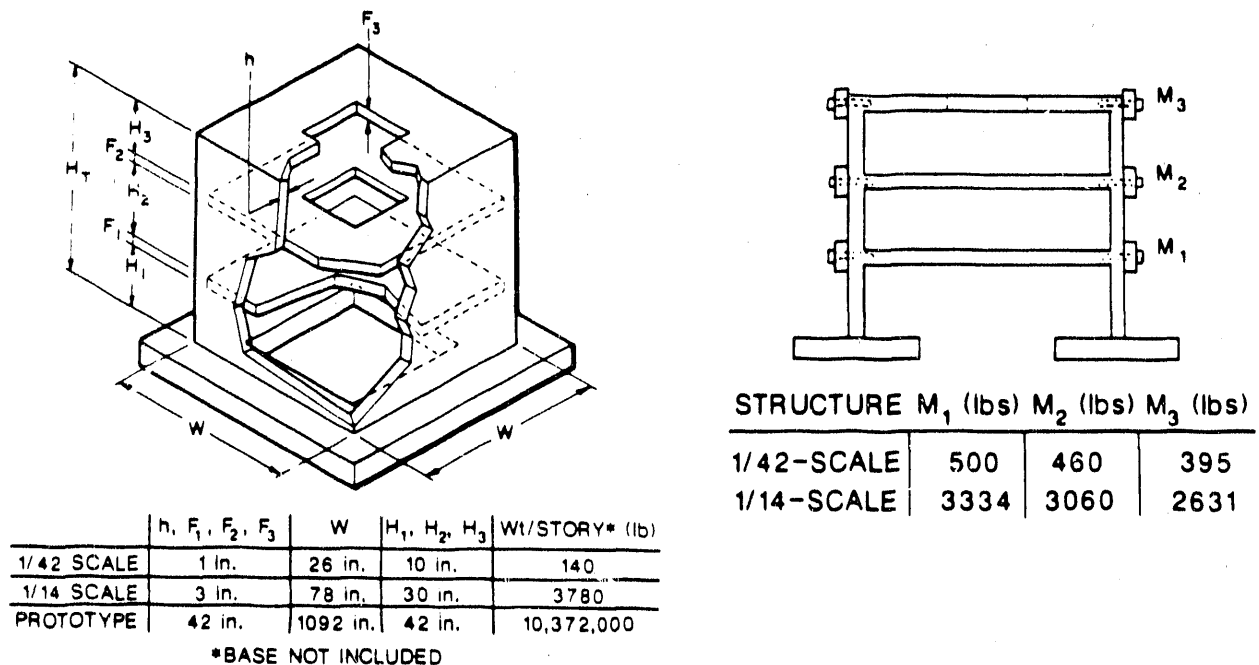
Fig. 3. Three-story auxiliary building model.

2. Although the structures themselves appear to have adequate reserve margin (even if the stiffness is only 25% of the theoretical), any piping and attached equipment will have been designed using inappropriate floor response spectra.

3. Given that a nuclear plant structure designed to have a natural response of about 15 Hz may have a natural frequency of 7.5 Hz (corresponding to a reduction in stiffness of 4), and allowing further that the natural frequency may further decrease because of degrading stiffness, the response of the structure will shift well down into the frequency range for which an earthquake's energy content is the largest. This shift will result in increased amplification in the floor response spectra at lower frequencies, and this fact potentially has impact on the equipment and piping design response spectra and their margins of safety.

Note that all three points are related to the difference between measured and calculated stiffnesses of these structures.

Having made these observations, one can think of several questions. Can the previous experimental data taken on microconcrete models be observed on prototype structures as well? What is the appropriate value of the stiffness that should be used in the design and for component response spectra computations of these structures? Should it be a function of load level? Have the equipment and piping in existing buildings been designed to inappropriate response spectra? What steps should be taken to evaluate the reduced stiffness for existing structures?

Thus, starting in FY 1985, the primary Program emphasis was to assure credibility of previous experimental work by beginning to resolve the difference between the analytical and theoretical stiffness that came to be called "stiffness difference" issue. The TRG for this program believed that this important issue should be addressed before other program objectives could be accomplished.

For these stiffness-related concerns, it was agreed that a series of credibility experiments would be carried out using both large- and small-scale structures. For the large-scale structure, the TRG set limitations on the design parameters. Their recommended "ideal" structure characteristics, in order of decreasing priority, were as follows:

1. Maximum predicted bending and shear mode natural frequency ≤ 30 Hz,
2. minimum wall thickness = 4 in.,
3. Height-to-depth ratio of shear wall ≤ 1,
4. Actual No. 3 rebar to be used for reinforcing,
5. Realistic material to be used for aggregate,
6. 0.1 to 1% steel (0.3% each face, each direction ideally) to be used, and
7. Water-blasted construction joints will ensure good aggregate frictional interlock.

The TRG structure shown in Fig. 4 was specifically designed to meet these requirements. The computed characteristics of this structure are given in Table I. However, it was decided that, before constructing this relatively large and expensive (both to build and especially to test) structure, a smaller, 1/4-scale model of the proposed structure should be designed, constructed, and tested.

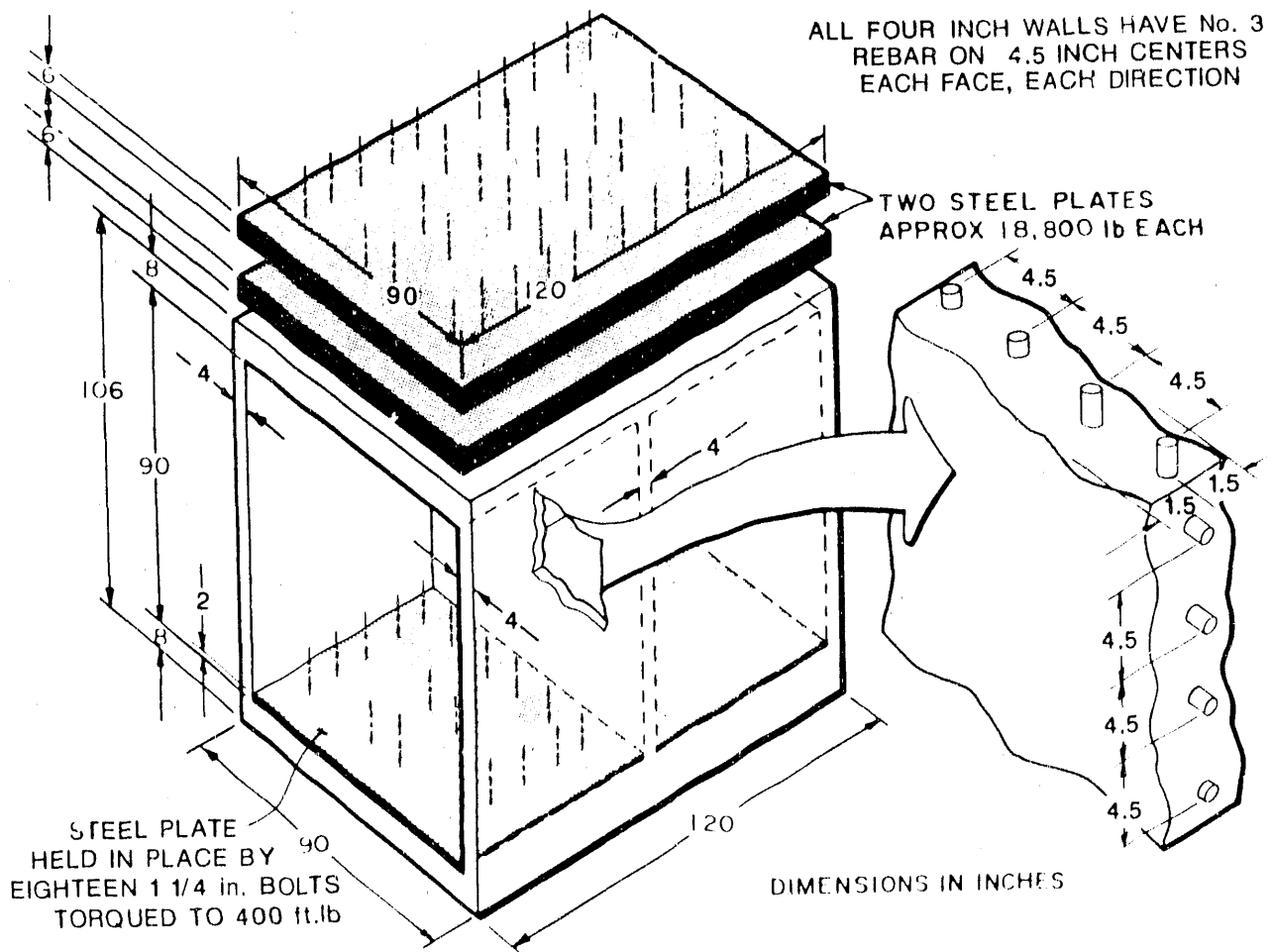ALL FOUR INCH WALLS HAVE No. 3 REBAR ON 4.5 INCH CENTERS EACH FACE, EACH DIRECTION

TWO STEEL PLATES APPROX 18,800 lb EACH

STEEL PLATE HELD IN PLACE BY EIGHTEEN 1 1/4 in. BOLTS TORQUED TO 400 ft.lb

DIMENSIONS IN INCHES

Fig. 4.   TRG-3-4 (1.0, 0.60) and TRG-5-4 (1.0, 0.60).

TABLE I
COMPUTED CHARACTERISTICS OF THE TRG STRUCTURE

Wall thickness	= 4 in.
Cross-section moment of inertia	= 2.06×10^6 in.^{4}
Effective shear area	= 379 in.^{2}
Area total (plan view)	= 1288 in.^{2}
Bending stiffness	= 2.5×10^7 lb/in.
Shear stiffness	= 5.3×10^6 lb/in.
Total stiffness	= 4.2×10^6 lb/in.
Max dead weight normal stress	= 42 psi
Total concrete volume	= 6 cubic yards
Total added weight	= 37,000 lb
Total weight	= 61,000 lb

The purposes of this 1/4-scale microconcrete model were as follows: (1) by applying the same principles of analysis and design, and the same construction practices as were used in the previous work, the scalability of the results of a microconcrete model to a prototype structure of "real" concrete could be investigated; (2) conclusions (based on calculations) concerning the model and prototype torsional response, individual wall frequencies, out-of-plane bending, and other features that affect the response of the large TRG structure can be confirmed on a less expensive test structure; and (3), instrumentation and other data acquisition requirements could be worked out before the larger-scale tests. The construction, analysis, testing, (low level static and random base excitation followed by seismic testing to failure) and results from the investigation of the 1/4-scale microconcrete model of the TRG structure are discussed in Ref. 7. Results for the prototype TRG structure using comparable testing procedures are discussed in Ref. 8. Form these results it tentatively appeared that

1. If either microconcrete or real concrete structures are carefully constructed and tested, their effective initial low-load level stiffness can be in the neighborhood of 50% of the value predicted by a mechanics of material calculation using a concrete modulus of 57,000 $\sqrt{f_c}$. At working loads, the stiffness values can be as low as 25% of the mechanics of material value.

2. At the low-load level, a microconcrete structure can serve as an adequate model for a real concrete structure.

3. The way in which real concrete structure's stiffness degrades at higher load-levels cannot be established from the tests reported in Ref. 8.

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However, during these tests, the real concrete structure appears to have suffered _more_ stiffness loss than would be predicted by the microconcrete model.

The authors feel strongly that any further tests to establish the dynamic scalability between "micro" and "real" concrete at higher-load levels should not be conducted using large complete structures because of the inadequacy (in capacity and control) of available dynamic test facilities.

New experimental and analytical activities were initiated in FY 1987 to further address the reduced stiffness issue and to address program objectives in general. Also, the investigators for this program have worked closely with several code committees in FY 1987 to incorporate the results of this program into current industry standard design and analysis codes. The following sections of this report will summarize these activities. Appendix A summarizes all the data related to shear wall stiffness that has been obtained in this program.

III. FY 1987 EXPERIMENTAL ACTIVITIES

Because of findings from previous tests and the continued skepticism of certain members of the TRG concerning the reduced stiffness measured during these tests, a new series of tests was suggested by the TRG to further investigate the reduced stiffness issue. This series consisted of quasi-static load cycle tests on structures with a cross-sectional geometry similar to the prototype TRG structure previously mentioned. The nomenclature used to distinguish these structures is as follows:

TRG-No.-Wt (AR,%R), sometimes abbreviated TRG-No.,

where   TRG is the designation for the series of structures designed and tested using guidance from the Program's Technical Review Group, a group of nationally recognized nuclear structural experts,

No. is the sequence number in the series,

Wt is the shear wall thickness,

AR is the height-to-length aspect ratio of the shear wall, and

%R is total percentage by area of steel reinforcing in both directions.

Thus the prototype TRG structure reported in Ref. 8 would be referred to as TRG-3-4 (1.0, 0.6). The test structures for FY 1987 were to be constructed with different aspect ratios and reinforcement percentages so that variations in these parameters that exist in actual Category I structures could be taken into account in the experiments, and the sensitivity to these variables could be identified. These structures were TRG-4-6 (1.0, 0.25), TRG-5-4 (1.0, 0.6) and TRG-6-6 (0.27, 0.50) and are shown in Figs. 5, 4, 6 respectively. Note that TRG-5 was identical in geometry and reinforcement to TRG-3. A detailed summary of these structures' construction, testing, and results can be found in Ref. 9 and subsequent reports to be issued by Los Alamos.

One of the purposes of these tests was to determine if, at equivalent stress levels, a reduction in stiffness occurs during static testing that is similar to that observed during dynamic testing. In addition, the structures

Fig. 5. TRG-4-6 (1.0, 0.25).

ALL SIX INCH WALLS HAVE No. 3
REBAR ON 7.25 INCH CENTERS
EACH FACE, EACH DIRECTION

TWO STEEL PLATES
APPROX 18,800 lb EACH

2 in. STEEL PLATE
HELD IN PLACE BY
EIGHTEEN 1 1/4 in. BOLTS
TORQUED TO 400 ft.lb

DIMENSIONS IN INCHES
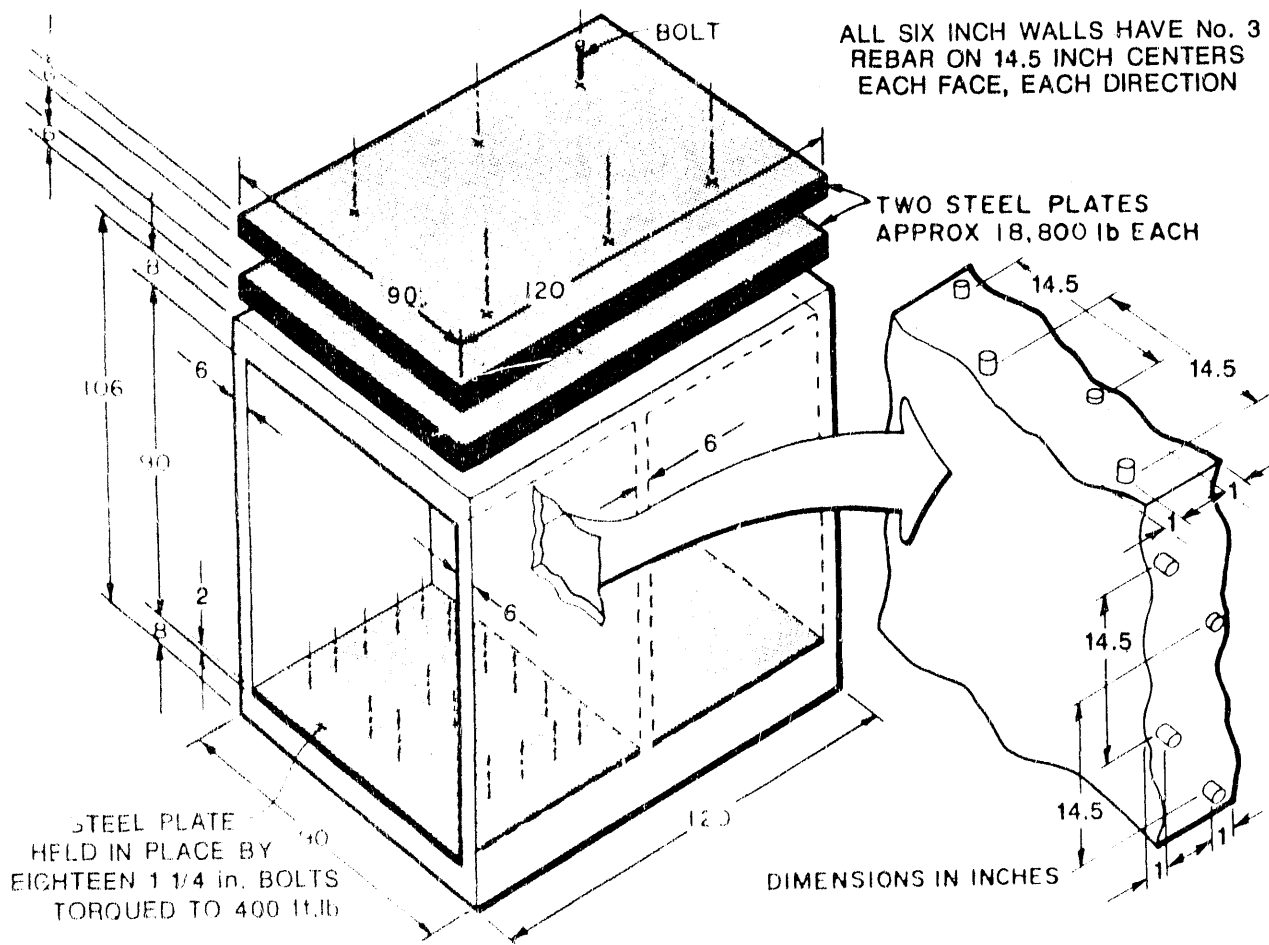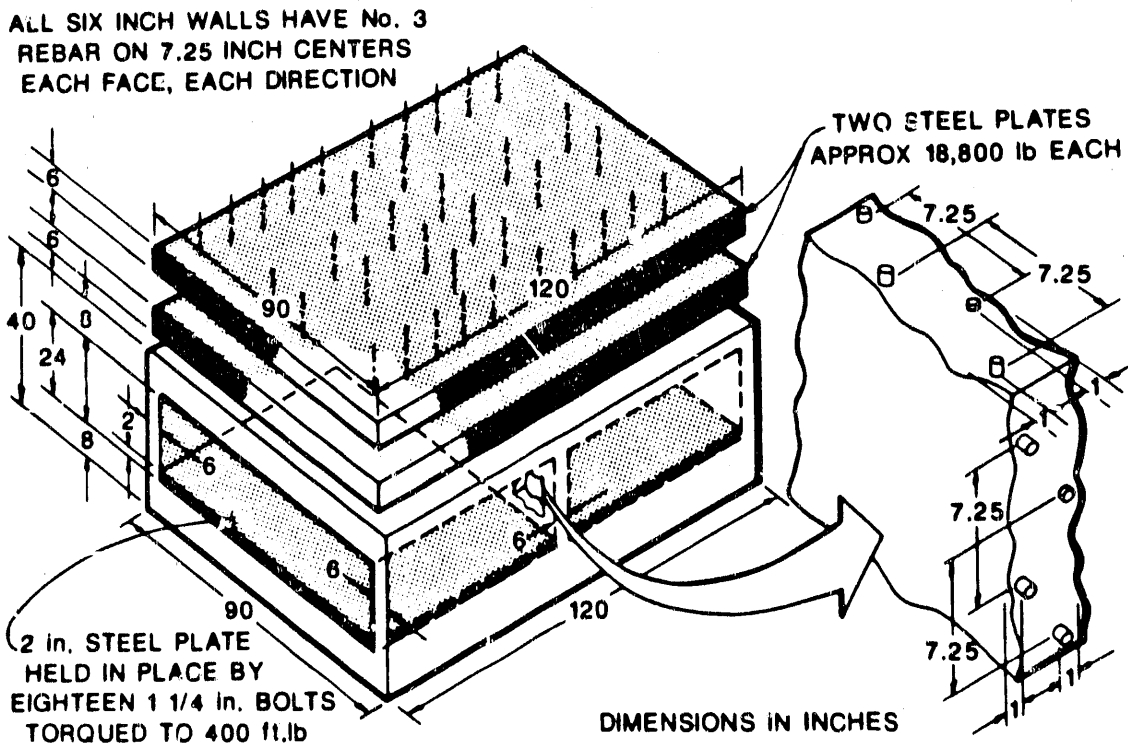
Fig. 6.   TRG-6-6 (0.27, 0.50).

were to be instrumented so that the contribution to bending stiffness of the flexural boundary elements (shear walls in orthogonal planes) could be assessed. The structures were also instrumented so that the shear and bending contributions to the total stiffness could be measured separately. The separation of shear and bending components of stiffness was intended to provide additional information concerning the mechanism for the reduction in stiffness. Also, these structures were to be constructed and tested in the same facility so that a minimal amount of handling would be required. The minimal handling criteria was to ensure that the reductions in stiffness, if any, were not caused by damage incurred during the shipping process to a remote testing facility.

Before the concrete was placed, weldable strain gages had been attached at various locations on the reinforcement. After the test structures had been placed and had cured for a minimum of 28 days, an ultrasonic inspection was made to determine if voids existed. When voids were found, they were repaired with a cement-sand filler. Figure 7 shows the completed TRG-4-6 (1.0, 0.25) structure mounted on the load frame.

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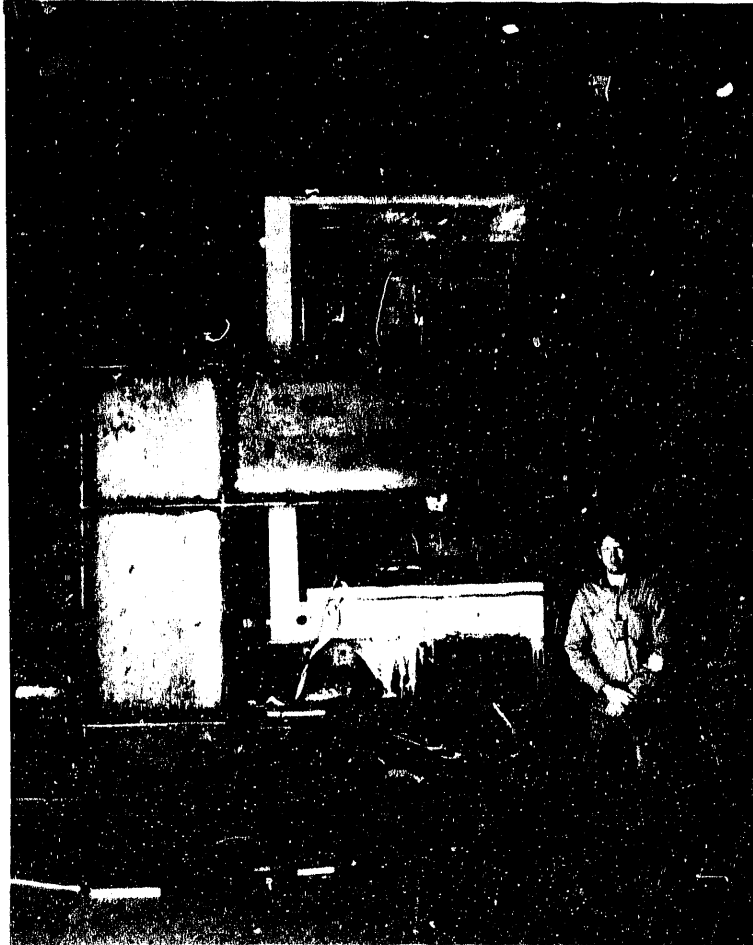
Fig. 7. TRG-4 mounted on the load frame.

Before the quasi-static load cycling was performed, an experimental modal analysis was performed to characterize the dynamic properties (mode shapes, resonant frequencies) of the structures. These properties were then compared with similar properties determined from a linear (uncracked) finite element analysis of the structures. This comparison provided an indirect method to assess the as-built stiffness of the structures while introducing a minimum amount of damage into the structure. Figures 8 and 9 show a typical modal test setup. The air bearings used to simulate free-boundary conditions are
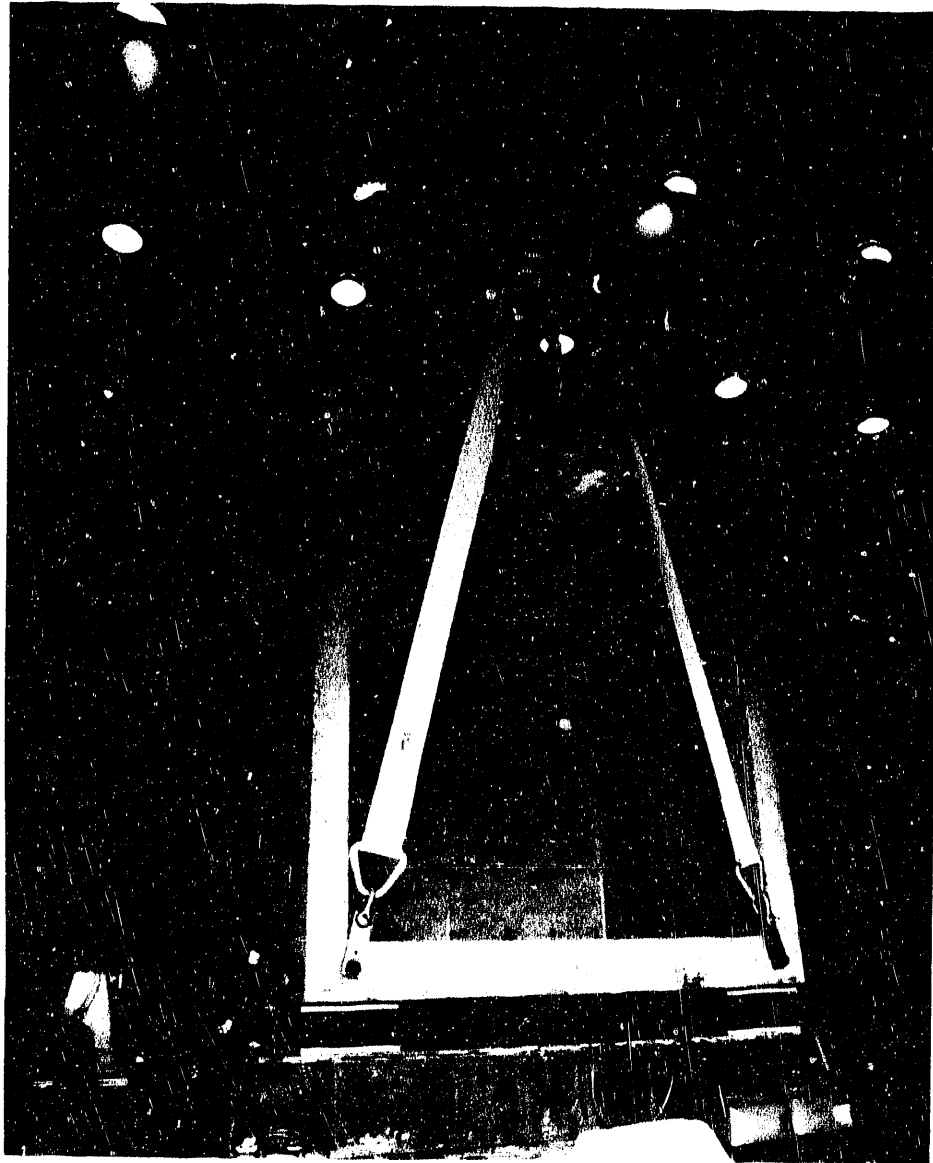
Fig. 8. TRG-4 mounted on air-bearings
for experimental modal analysis.

shown in Fig. 8 and the electrodynamic shaker used to excite the structure is
shown in Fig. 9. A typical comparison between an experimentally measured mode
shape and the corresponding mode determined by finite element analysis is shown
in Fig. 10 for TRG-4-6 (1.0, 0.25). Table II compares the measured and anal-
ytical resonant frequencies determined for TRG-4, 5, and 6.
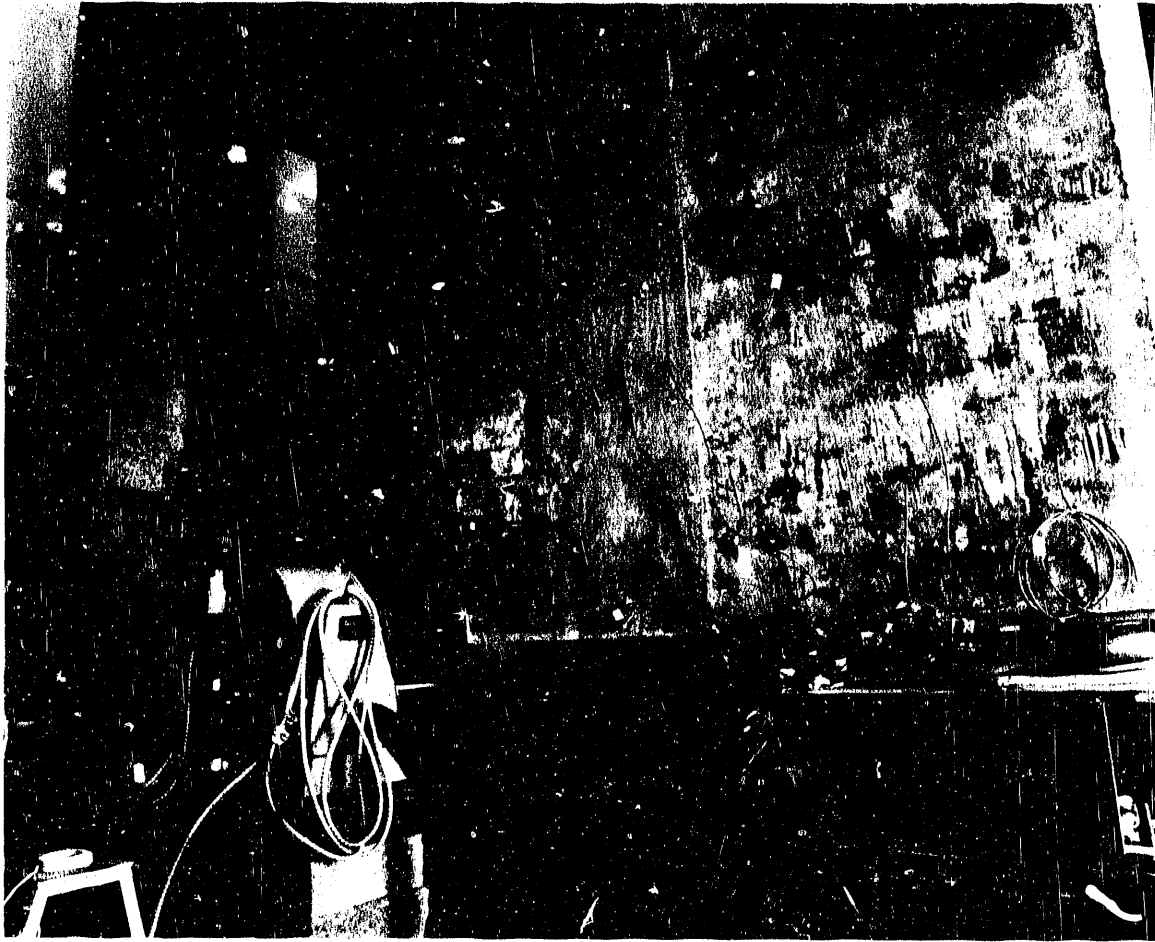
Fig. 9.   Electrodynamic shaker used to excite the struc-
          tures during the experimental modal analysis.
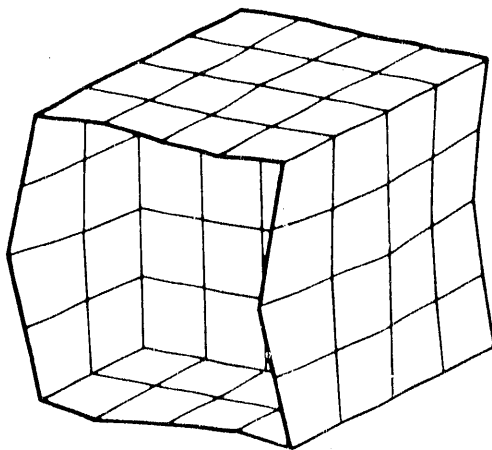
MODE No. 5
EXPERIMENTALLY DETERMINED
Freq = 111 Hz
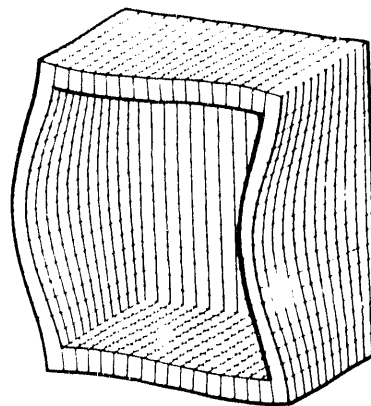
MODE No. 5
DETERMINED WITH ABAQUS
F.E. PROGRAM
Freq = 111 Hz

Fig. 10.   Comparison of a mode shape identified during
           the experimental modal analysis with a mode
           shape determined by finite element analysis.

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TABLE II

A COMPARISON OF RESONANT FREQUENCIES IDENTIFIED FROM THE EXPERIMENTAL
MODAL ANALYSIS AND THE RESONANT FREQUENCIES IDENTIFIED FROM THE
ANALYTICAL MODAL ANALYSIS FOR THE LARGE TRG-STRUCTURES

| Mode	Experimental Before Cracking (Hz)			Linear Finite Element Analysis (Hz)		
	TRG-4	TRG-5	TRG-6	TRG-4	TRG-5	TRG-6
1	37.1	31.9	92.9	36.3	31.9	91.8
2	79.2	67.0	123.4	77.8	72.3	125.1
3	88.3	73.9	136.4	86.0	79.7	134.9
4	100.0	77.8	179.2	102.0	88.4	172.6
5	111.0	84.4	208.8	111.0	95.2	196.2
6	122.0	*	*	120.0	112.0	206.1
7	*	117.0	*	130.0	113.0	—
8	141.0	126.0	*	136.0	129.0	—
9	*	*	*	143.0	133.0	—
10	172.0	*	*	154.0	135.0	—
11	*	159.0	*	162.0	152.0	—
12	*	170.0	*	—	196.0	—
13	*	198.0	*	—	230.0	—

* Not identified.

The actual quasi-static load cycle testing was similar for each structure.
Displacement transducer locations for a typical test are shown in Fig. 11. The
load histories for the three structures are shown in Figs. 12-14. As can be
seen in Fig. 14, TRG-6-6 (0.27, 0.50) was cycled numerous times at different
load levels to see if stiffness would reduce with the number of load cycles.
A typical load-displacement response curve is shown for TRG-5-4 (1.0, 0.6) in
Fig. 15 and the final crack patterns for this structure are shown in Fig. 16.
In general, the relative displacement interior gages gave the best results,
but on TRG-6-6 (0.27, 0.50) the instrumentation system was at its limits
because of the low aspect ratio of this structure and its very stiff nature.

Hysteretic energy losses were measured during the static cyclic testing
and these losses were used to evaluate equivalent viscous damping ratios.
Tables III and IV summarize the damping ratios obtained for TRG-4 and -5.
Because the TRG-6 structure was so stiff, the results from the displacement
transducers showed evidence of "lost motion." That is why no hysteresis
evaluation was possible for this model.
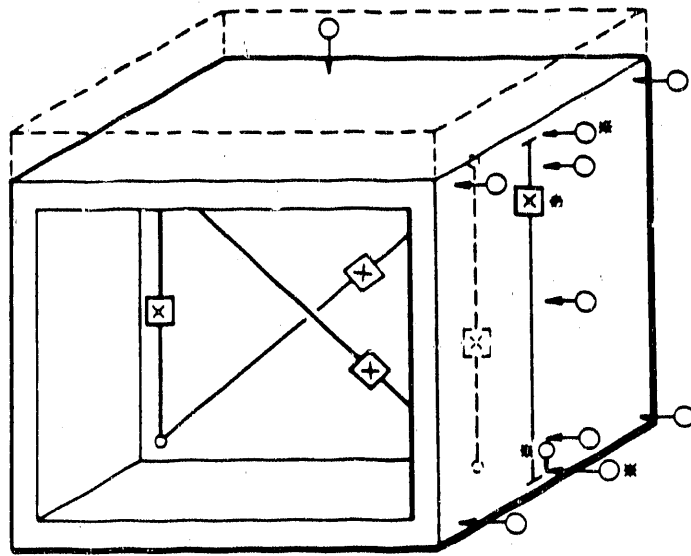
```
o———☐—   RELATIVE DISPLACEMENT
———O     DISPLACEMENT, FIXED REFERENCE
  ✳      FOUR GAGES CORRESPONDING
         TO THESE ON THE OTHER END
  ✕      FOUR GAGES CORRESPONDING
         TO THESE ON THE OTHER SIDE
         OF THE SHEAR WALL
```

Fig. 11.   Location of displacement transducers
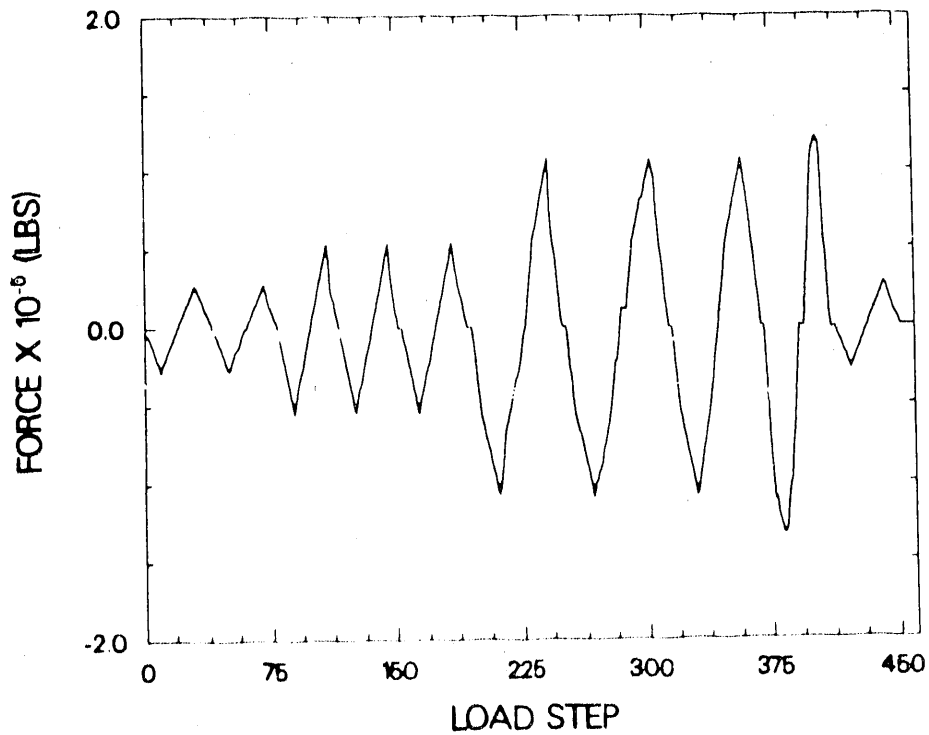   used during static cyclic testing.

Fig. 12.   Load history for TRG-4.

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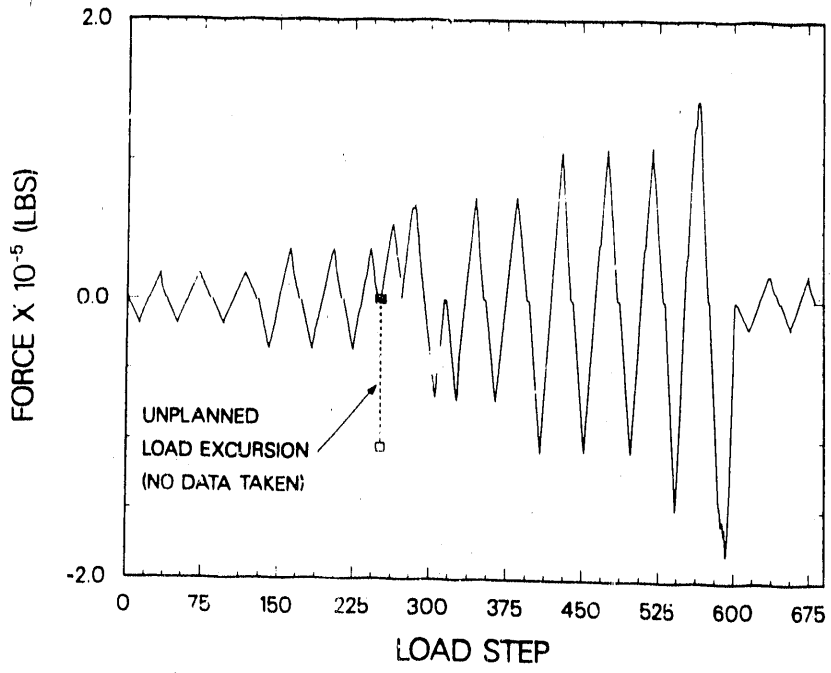
Fig. 13. Load history for TRG-5.
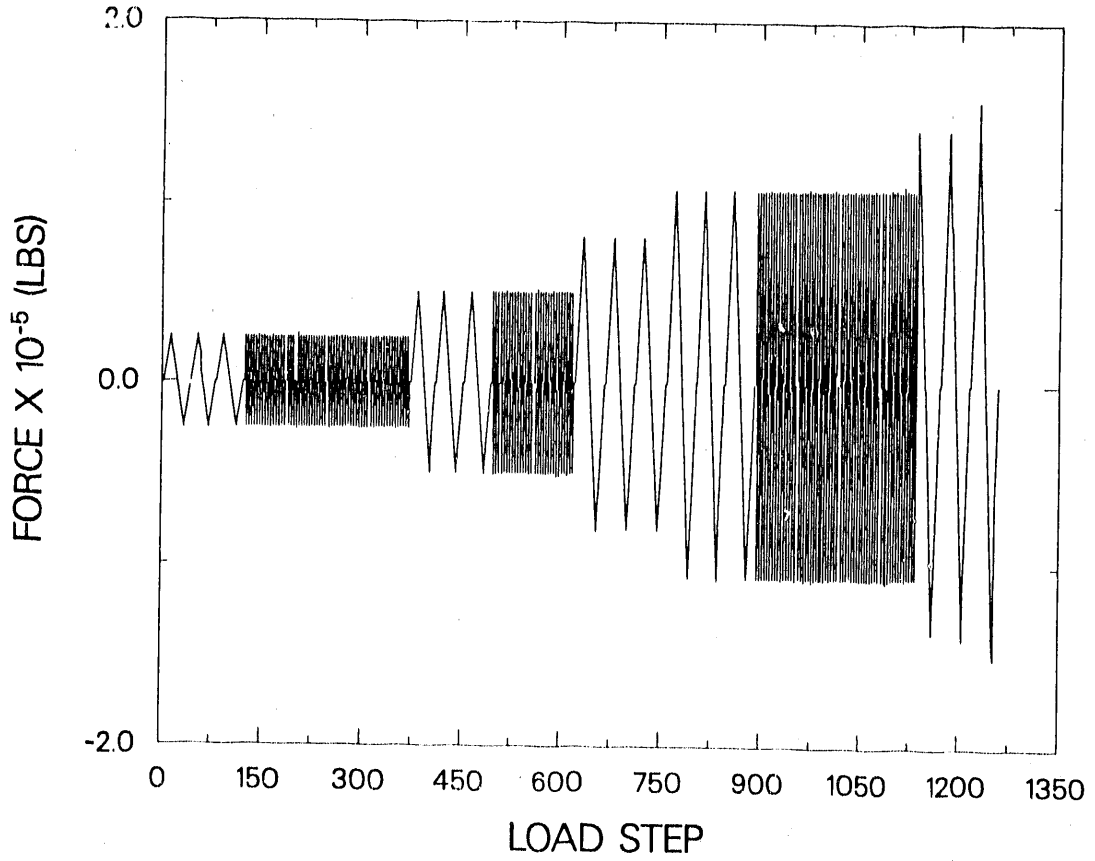
Fig. 14. Load history for TRG-6.
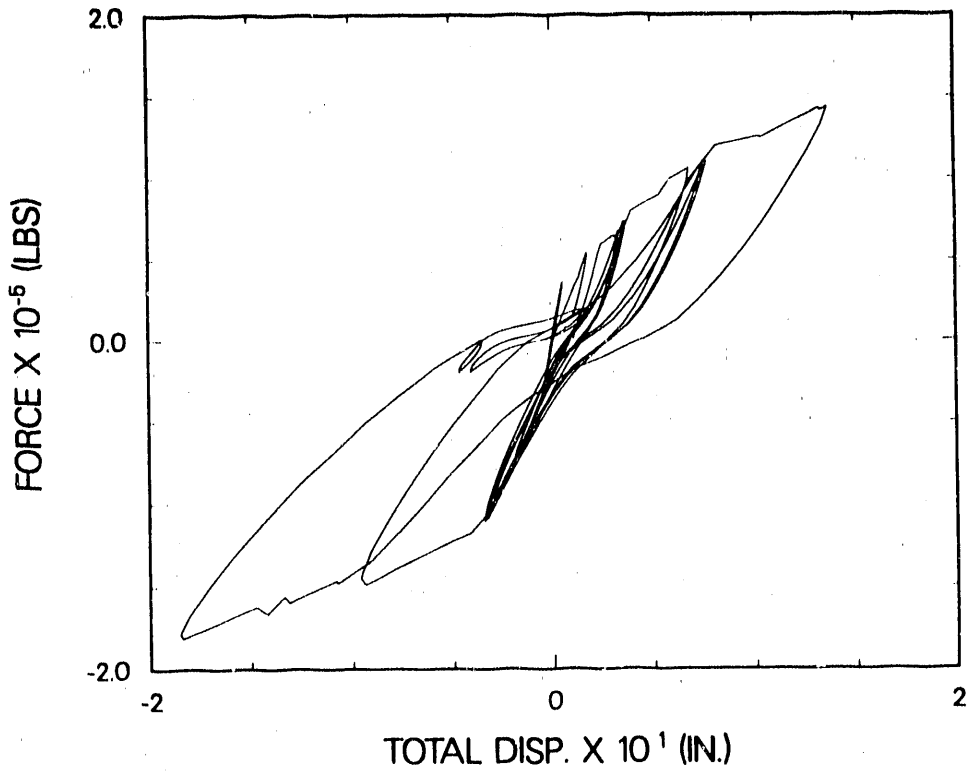
Fig. 15. Load displacement re-
sponse of TRG-5.
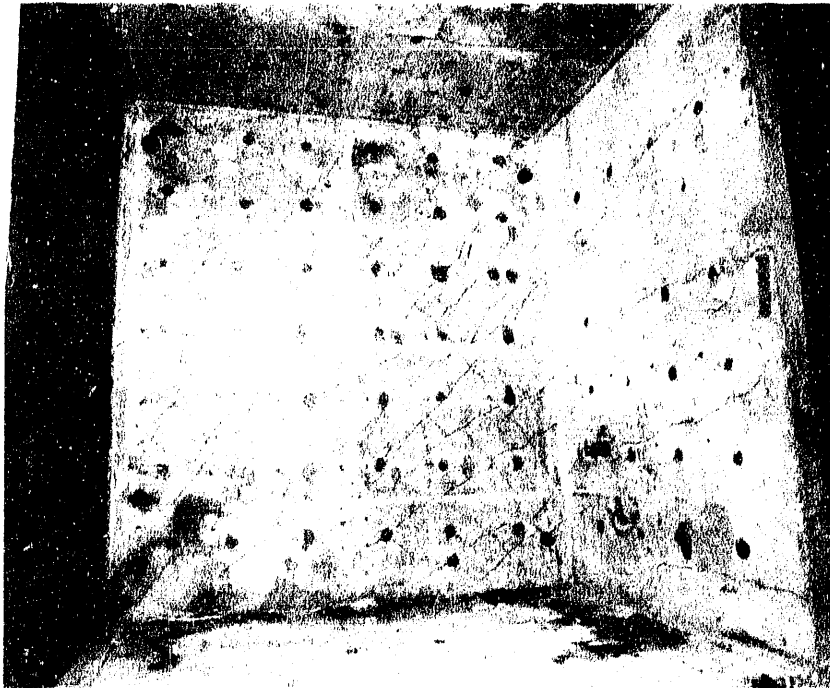
Fig. 16. Final crack patterns in TRG-5.

TABLE III

HYSTERETIC ENERGY LOSSES MEASURED ON TRG-4

Load Cycle	Peak Average Base Shear Stress (psi)	Peak Force (lbs)	Hysteretic Energy Loss (in. - lbs)	Equivalent Viscous Damping (% of critical)
1	50	27,000	29.5	5.9
2	50	27,000	35.4	7.0
3	100	54,000	113	5.2
4	100	54,000	81.2	3.7
5	100	54,000	77.4	3.5
6	200	108,000	1560	*
7	200	108,000	940	5.7
8	200	108,000	888	4.9
9	260	140,000	16400	*
10	50	27,000	582	6.3

* Cycles that exhibited nonlinear response.

TABLE IV

HYSTERETIC ENERGY LOSSES MEASURED ON TRG-5

Load Cycle	Peak Average Base Shear Stress (psi)	Peak Force (lbs)	Hysteretic Energy Loss (in.-lb)	Equivalent Viscous Damping (% of Critical)
1	50	18000	10	3.5
2	50	18000	10	3.4
3	50	18000	11	4.0
4	100	36000	39	3.3
5	100	36000	33	2.7
6	100	36000	32	2.8
7	150	54000	156	*
8	200	72000	786	*
9	200	72000	475	3.8
10	200	72000	449	3.5
11	300	108000	2630	*
12	300	108000	1690	4.6
13	300	108000	1300	3.4
14	400	144000	12000	*
15	500	180000	11300	*
16	50	18000	434	*
17	50	18000	293	8.0

*Cycles that exhibited nonlinear response. Stiffness was not well defined during these cycles.

To briefly summarize the results of these tests, it was found that before the structure cracked, the stiffness of the structure had accurately been predicted by strength-of-materials analysis. After the structure had cracked, stiffness was found to be a function of the amount of reinforcement, prior load history, and current load level. Because of the structure's geometry, the entire end walls were effective in resisting bending deformations. No effects from repeated load cycling to a constant load level were noticed for TRG-6. Shear and bending components of stiffness degraded equally in terms of percentage as can be seen in Table V. The reader is reminded that a detailed summary of these tests can be found in Ref. 9 and subsequent reports to be issued by Los Alamos.

IV. FY 1987 ANALYTICAL ACTIVITES

Concurrent with this experimental effort, an analytical investigation was conducted to match floor response spectra (FRS) determined from measured acceleration-time histories during simulated seismic tests (herein referred to as measured FRS) with FRS determined from linear analytical models of the test structures subjected to the same base excitation (herein referred to as analytical FRS).

TABLE V

TRG-4 MEASURED STIFFNESS VALUES

Load Cycle	Total Stiffness lbs/in. x 10^{-6}	Bending Stiffness lbs/in. x 10^{-6}	Shear Stiffness lbs/in. x 10^{-6}	Ratio Shear Stiffness Bending Stiffness
1-5 (50 & 100 psi cycles)	8.5	52.6	10.2	0.19
7-8 (200 psi cycles after 1st cracking)	4.05	23.0	4.91	0.21
10 (post failure 50 psi cycle)	0.54	4.8	0.61	0.13

The response spectra matching was attempted on a variety of test structure geometries including TRG-1-1 (1.0, 0.56), TRG-3-4 (1.0, 0.60), a two-story 1/10-scale diesel generator building model, and the three-story 1/42-scale auxiliary building. These structures are shown in Figs. 17, 4, 2, and 3, respectively. Matching was to be accomplished by adjusting the stiffness and damping in the analytical model. The motivation for this investigation was based on the TRG's feeling that more emphasis should be placed on the analysis of data already obtained. In particular, the TRG felt that it was pertinent to determine if the Seismic Category I structures can continue to be analyzed with corrected linear models despite the reductions in stiffness associated with the seismic loading. Also, comparisons of measured and analytical response spectra quantify the differences between the predicted response of these structures based on current design practices and the experimentally observed response as they would actually be used by the engineer in plant and equipment design. A detailed summary of the response spectra matching calculations can be found in Ref. 10.
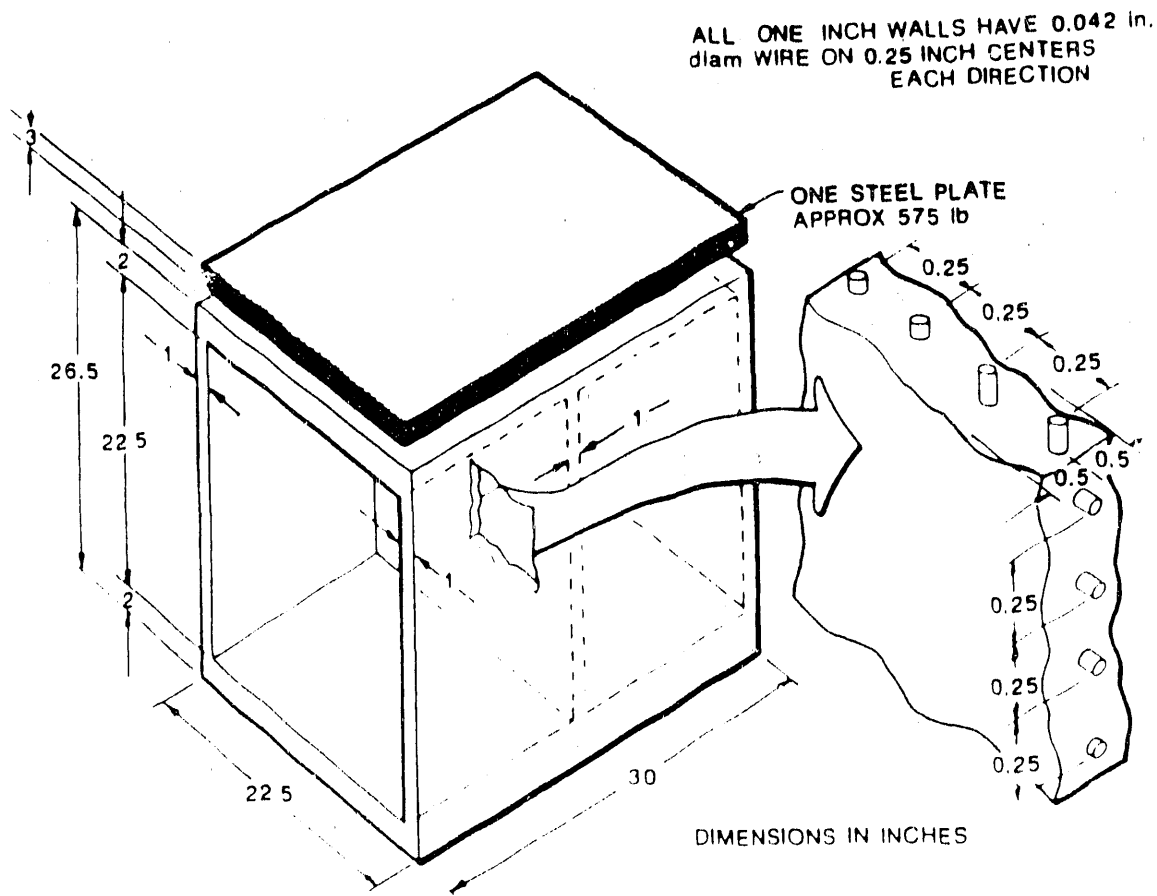
Fig. 17. TRG-1-1 (1.0, 0.56).

For each structure, three different levels of simulated seismic base excitation were analyzed. An example of a base excitation response spectrum is shown in Fig. 18 for the diesel generator building model. This spectrum was generated from a time-scaled version of the North-South component of the 1940 El Centro earthquake normalized to 1.88 g's peak acceleration. Two and ten
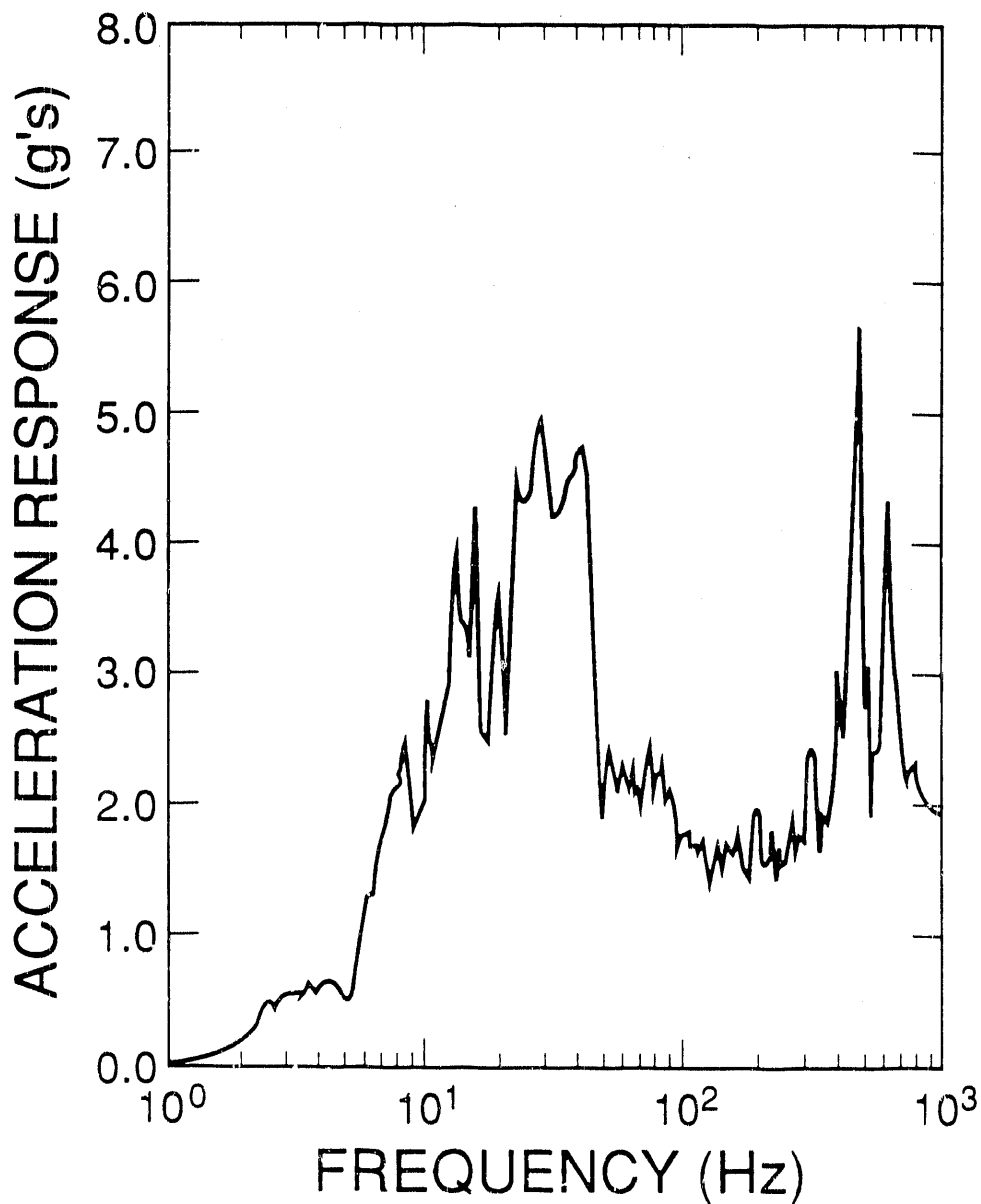
Fig. 18. Base input response spectrum generated from the 1.88 g's peak acceleration seismic input used on the 1/10-scale diesel generator building.

percent equipment damping was used in the FRS calculations. The initial values of stiffness in the analytical model were taken from the reduced stiffness plot in Fig. 19 and damping was initially estimated at 7% of critical based on previous test results. Stiffness was adjusted to match the frequency of peaks in the analytical response spectrum while damping was adjusted to match the amplitudes in the spectrum. All damping values refer to viscous damping, percent of critical.
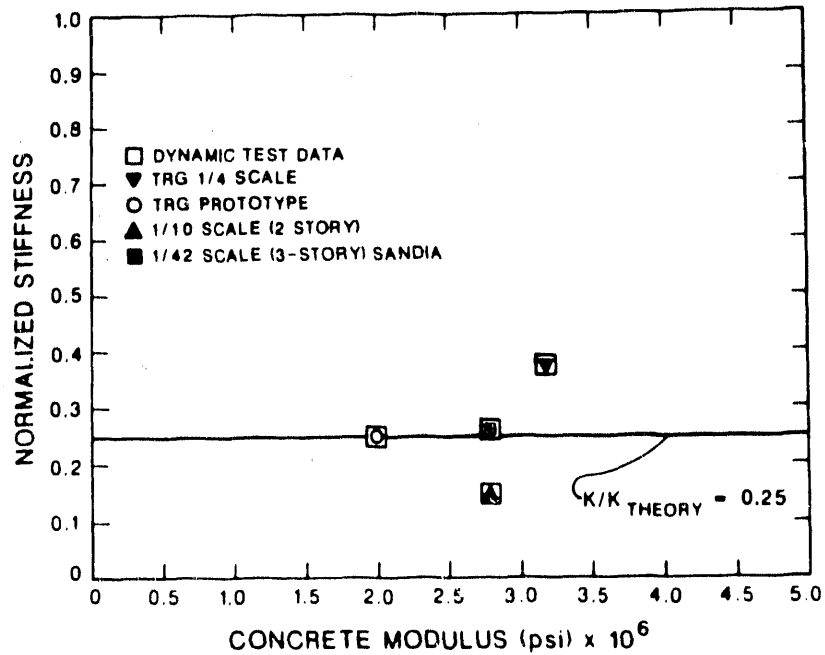
Fig. 19. Reduced stiffness measured during initial low-
level seismic tests of the structures analyzed
in the response spectra matching exercise.

A summary of the steps used to match the response spectra is given below.

1. Calculate base input response spectra using 2% and 10% damping, filter the signal for 60 Hz noise, and baseline correct for dc offset before the calculation.

2. Calculate measured floor response spectra for 2% equipment damping, filter the signals for 60 Hz noise, and baseline correct for dc offset before the calculation.

3. Develop a lumped mass model of the test structure and subject it to the measured base input.

4. Calculate floor response spectra based on response of model in step 3 for 2% equipment damping.

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5. Repeat steps 3 and 4 adjusting stiffness in the model to match response spectra peaks in terms of frequency (often requiring several iterations).

6. Repeat steps 3 and 4 adjusting damping in the model to match the amplitude of the peaks in the response spectra (often requiring several iterations).

7. Repeat steps 2-6 for 10% equipment damping.

Figure 20 shows the lumped mass model of the 1/10-scale diesel generator building model and Figs 21 and 22 compare the measured FRS for each floor of the diesel generator building with the reduced stiffness analytical FRS that best match the measured response for this structure when subjected to the input whose response spectrum is shown in Fig. 18. Also included on this plot is an analytical FRS based on the "current design practice." These plots are typical of the reduced stiffness, linear analytical model's ability to predict the measured reduced stiffness response.

For the 1/42-scale auxiliary building, three additional calculated response spectra were generated. The first referred to as the "current design practice" used a strength-of-materials stiffness value assuming the entire end walls contribute to the bending stiffness. The second
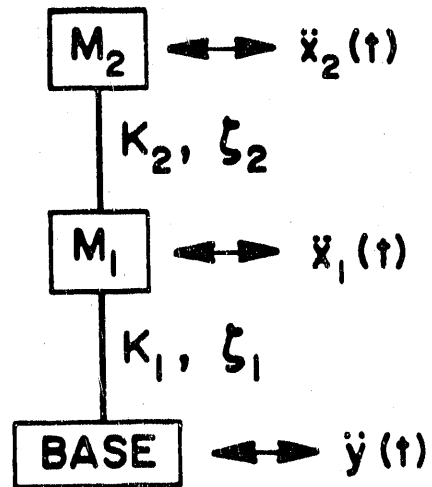
Fig. 20. Lumped mass model of the 1/10-scale diesel generator building.
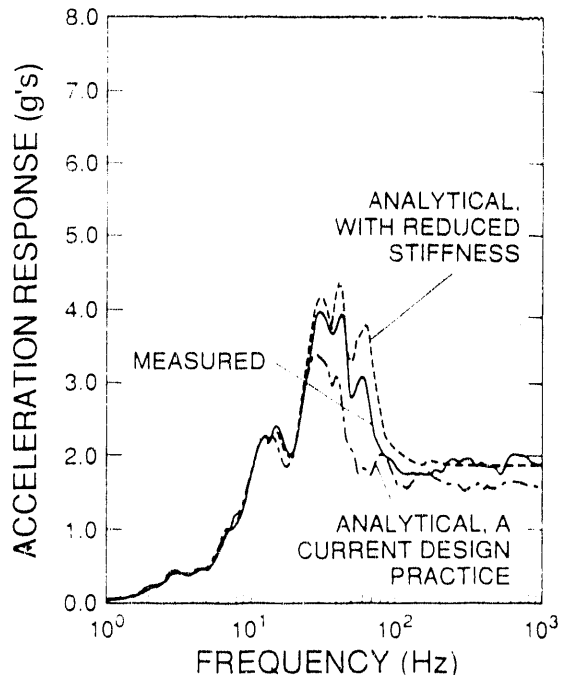
Fig. 21. Comparison of the measured and analytical response spectra for the first floor of the 1/10-scale diesel generator building.
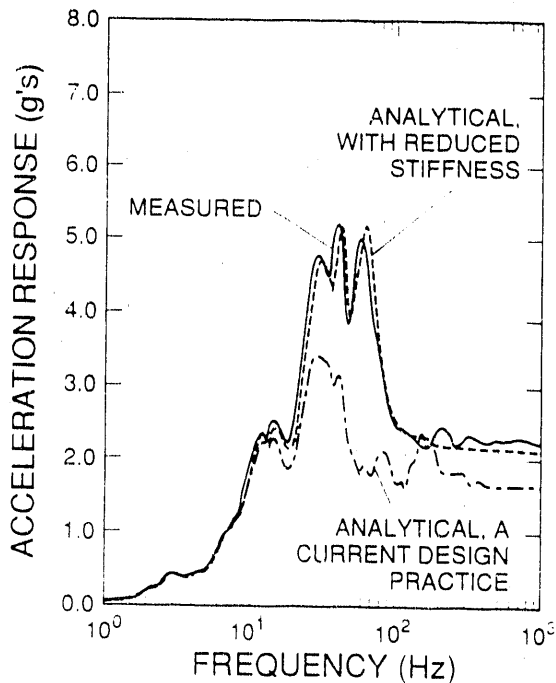
Fig. 22. Comparison of the measured and analytical response spectra for the second floor of the 1/10-scale diesel generator building.

used ACI 349-85 (Ref. 11) T-beam criteria to determine the end walls contribution and the third neglected the end walls altogether. These additional response spectra correspond to the alternate stiffness values that were calculated and reported in Ref. 10. Current design practice plots were included in Ref. 10 for the other structures as well. All analytical stiffness values were calculated with measured modulus of elasticity values as opposed to using the empirical formulas in ACI 349-85.[11]

The TRG also requested that the analytical values of stiffness for several different test structure geometries be recomputed using various design assumptions. These alternate values of stiffness were then to be compared with the measured stiffness values. Table VI summarizes the results of these alternate stiffness calculations. These results are discussed in detail in Ref. 10.

V. FY 1987 TECHNICAL REVIEW GROUP ACTIVITIES

In addition to providing input with regard to the experimental and analytical efforts for FY 1987, the members of the TRG were requested to respond in writing to a series of questions that addressed the general issue of whether the results obtained for tests in this program were credible and whether these results were addressing the program objectives. Replies to these questions were solicited for the purpose of providing members of the Nuclear Regulatory Research (NRR) Branch of the NRC with all the input possible to

TABLE VI

ANALYTICAL STIFFNESS VALUES COMPARED WITH MEASURED STIFFNESS VALUES

	Stiffness Determined from Static Tests	Stiffness Determined from Seismic Response[d]	Stiffness Determined from Response Spectra Matching	Analytical Stiffness Values			
				End Walls Fully Effective	ASCE Criteria (Ref. 12)	ACI T-Beam Criteria (Ref. 11)	Neglect End Walls
	lb/in. x 10⁻⁶	lb/in. x 10⁻⁶	lb/in. x 10⁻⁶		lb/in. x 10⁻⁶		
TRG-1 (1 story)[a]	.92	0.41	0.44	1.07	0.93	0.61	0.44
TRG-1 (1 story)[b]	.92	0.41	0.44	1.17	1.02	0.66	0.48
TRG-3 (1 story)[a]	2.0	0.67	0.45	2.67	2.33	1.54	1.11
TRG-3 (1 story)[b]	2.0	0.67	0.45	4.67	4.07	2.70	1.94
1/10-scale diesel[a,c] generator building model	--	1.31	1.4	8.21	6.88	2.00	1.94
1/10-scale diesel[b,c] generator building model	--	1.31	1.4	9.38	7.86	2.29	2.22
1/42-scale auxiliary[a,c] building model	--	1.39	1.37	5.45	5.11	4.82	4.68
1/42-scale auxiliary[b,c] building model	--	1.39	1.37	6.26	5.86	5.53	5.37
TRG-4 (1 story)[a]	8.5[e]	--	--	8.42	7.70	5.81	4.02
TRG-4 (1 story)[b]	8.5[e]	--	--	9.60	8.78	6.62	4.58

a Theoretical values calculated using measured modulus of elasticity

b Theoretical values calculated using $E_c = 57,000 \sqrt{f'_c}$

c These stiffness values are for an individual story assuming cantilever deformation

d These stiffness values were determined from

$$K = \left(\frac{f_{meas.}}{f_{Theory}}\right)^2 K_{Theory}$$

e Based on the interior relative displacement measurements.

make decisions about both the applicability and regulatory impact of this research program. The questions posed to the TRG were

    1. Are the tests in this program valid for addressing the program objectives?

    2. In light of the program objectives, are the model test data obtained applicable to nuclear power plant structures?

    3. Have the technical issues of scaling, instrumentation, and model fabrication effects been resolved?

    4. Should there be another "carefully handled" dynamic test to address the possible "dynamic effects" issue? If so, what configuration should be used?

    5. Have we obtained enough data and have we tested the correct configurations to meet the program objectives?

    6. Would the variability in stiffness observed in the models be observed in real nuclear plant structures at comparable load levels?

The TRG's responses to these questions can be found in Appendix B. A summary of the responses, as interpreted by the authors, is given in Table VII.

VI. FY 1987 CODE COMMITTEE ACTIVITIES

Finally, results from this program were presented to both American Society of Civil Engineers (ASCE) and American Concrete Institute (ACI) code committees during FY 1987. This interaction with the code committees has led to investigators from Los Alamos being added to the committees and the results that have been presented, will, most likely, be reflected in future revisions of these committees' current analysis and design standards.

This program has generated considerable interest among members of national code committees addressing reinforced concrete analysis and design. Presentations of the findings and issues with regard to the reduced stiffness implications on seismic response of equipment and piping were given in November 1986 to an ACI Committee, and the ASCE Dynamic Analysis Committee.

Dr. John Stevenson, a member of the Program's TRG is chairman of the ASCE Nuclear Standards Committee. Dr. Joel Bennett, principal investigator for this program, is a member of the ASCE Nuclear Standards Committee. This committee has just approved an ASCE Standard for the Seismic Analysis of Safety-Related Nuclear Structures.[12] The new standard does not include results from this

TABLE VII

RESPONSE OF THE TRG MEMBERS TO QUESTIONS CONCERNING PROGRAM OBJECTIVES

Question	Dr. J. D. Stevenson	Prof. M. A. Sozen	Dr. R. P. Kennedy	Dr. W. Baker	Mr. D. R. Denton	Dr. K. Buchert
1	Yes, unless you wish to evaluate difference in stiffness between cracked & uncracked walls. Buildings are more susceptible to damage than equipment.	Yes	Yes for determining stiffness degradation. The program has not been valid for determining initial stiffness.	Yes	Yes	No
2	Qualified yes. Stiff data applied to un-cracked walls at low-level earthquake; fewer stiff data relate to damaging earthquakes.	Yes	partially - no instruments to directly obtain stiffness in dynamic test, thin walls, model shipment are concerns. Real answer bound by test data.	Yes	Qualified yes. Magnitude of stiff-loss may not be accurate. He questions reduction of precracked stiff-ness.	No
3	Qualified yes. He does not know when models cracked.	Yes, with respect to overall impact of results.	No - base rotation and wall thickness are open issues. Scaling has been resolved.	Qualified yes. Why was stiffness of last 2 models so close to theory?	No, as it relates to scaling response in full-size structures.	No
4	No, do more analytical work to model real nuclear plant shear walls.	Make this decision after risk significance studies have been completed	Yes	No strong endorsement.	No recommendation.	No
5	Yes	No. Need to re-evaluate state-of-the-art floor spectra calculations and their impact on equipment design.	Yes	Enough data have been obtained, defer decision on correct configuration to other TRG members.	Cannot quantitatively determine what stiffness reduction should be used in design.	No opinion.
6	Even more variability would be observed.	Yes	Substantial variability in real nuclear plants but not as great as reported here.	Test actual plants and find out.	Yes	To some extent.
Comments		Expects stiffness at low-level excitation to be less than 3/4 of predicted about 1/2 of the time. Time to investigate the impact of stiffness reduction on design decisions, e.g., equipment.	Study consequences of stiffness reduction on equipment design.			

Program. Committee members are aware that a portion of the Standard may have to be revised depending upon the outcome of future tests.

Dr. Robert P. Kennedy, a member of the Program's TRG, is immediate past chairman of the ASCE Dynamic Analysis Committee. Dr. Kennedy's committee was responsible for developing the Standard for Seismic Analysis of Safety-Related Nuclear Structures. Dr. Kennedy has advised the subcommittee of the Seismic Category I Structures Program results, particularly with regard to the reduced stiffness issue and its implication on floor response spectra. Based on program results, Dr. Kennedy has reconstituted the Working Group on Stiffness of Concrete Shear Wall Structures. The Working Group, chaired by Dr. Robert Murray, Lawrence Livermore National Laboratory, will meet biannually.

Dr. Bennett is a member of the working group as is Dr. Charles Farrar. During FY 1987, this Working Group has undertaken the task of writing a position paper on the proper stiffness to be used in calculating the dynamic response of low aspect ratio shear wall structures. The investigators from the Seismic Category I Structures Program have provided the Working Group with a review of previous investigations into the stiffness of low aspect ratio shear walls and detailed information concerning results obtained by this Program. Appendix A contains a summary of the shear wall test data provided to the Working Group.

VII. CONCLUSIONS

One of the primary purposes of the tests performed in FY 1987 was to determine if, during a carefully monitored static load cycle test, a stiffness reduction of 4 would occur at similar load levels as have been observed in dynamic tests. The models tested in FY 1987 were constructed with prototypical materials; with one exception, TRG-3, the previous dynamic test specimens were constructed with microconcrete. During the precracking load cycles and the low-level modal analysis, no stiffness reduction was observed, and in the case of TRG-6, the measurements indicated a stiffness slightly higher than theory would predict. The precracking response of these structures was accurately predicted with currently used linear analysis techniques based on strength of materials theory. These same techniques would not have adequately predicted the dynamic response of structures previously tested in this program, even though

stress levels during the dynamic tests were well below those predicted to crack the structure.

The boundary elements or end walls were found to be fully effective in resisting bending deformation, but it is felt that the geometry of the test structure constrained these elements to be effective. In terms of percentage, the stiffness components were found to degrade equally implying that the reduction in stiffness is not caused by a loss of one of the stiffness components.

Based upon the quasi-static, cyclic testing of TRG structures 4, 5, and 6, it is readily apparent that carefully handled structures tested fairly "green" (i.e., unaged), are uncracked, and the stiffness can be accurately predicted by strength-of-materials theory.

The most likely cause of the reduced stiffness that has been measured in this Program is concrete cracking. The source of this cracking has probably been (in our tests), a combination of several causes that include handling and transportation, aging (curing), shrinkage, and other time effects, and the construction imperfections and material variability that exist in all fabricated structures. However, we generally believe that the same cracking effects exist in real reinforced concrete structures because of many of the same reasons (handling and transportation loadings can be replaced by "differential settlement").

The current method of treating these structures, namely, using an uncracked cross-section for determining the structural element parameters and resulting floor response spectra should be re-examined and more realistic guidelines established to cover the effects. Los Alamos is working with the professional society committees in this re-examination.

The following conclusions were made based on the results of the floor response spectra matching for the various structures:

1. Linear response spectra techniques applied to the analytical responses generated with lumped mass models of the structures did an adequate job of predicting the experimentally measured response spectra. These predictions required modifications in the stiffness and damping from currently used design practice. The linear response spectra techniques continued to work well even after the structure was known to have sustained significant damage in previous tests.

2. The stiffness values that provide the best match are significantly less than current design criteria would predict even if end walls were neglected.

3. At higher input levels, stiffness must be further reduced to obtain an accurate match.

4. In order to obtain an accurate match for these particular tests, damping values must be in the 6% to 10% range at the low-level excitations and must be increased to as high as 35% when the damaged structure receives severe seismic loading.

5. Damping has a greater effect on peaks in the response spectra because of resonance than it does on peaks caused by a surge in the energy content of the input signal.

6. For multi-degree-of-freedom (MDOF) systems, a good match with the measured response spectra was obtained by progressively increasing the damping in the lower floor. This fact suggests a frictional damping mechanism.

7. For MDOF systems, the damping in the bottom floor plays a major role in controlling the system response. The structures seem relatively insensitive to the damping values associated with the upper floors.

8. For MDOF systems, it is not clear that there is a unique set of damping values that provide the best match to the measured response spectra. In general, the analytical model that gives the best overall match tends to overestimate the bottom floor response and underestimate the top floor response.

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APPENDIX A

SUMMARY OF MEASURED STIFFNESS VALUES

APPENDIX A
SUMMARY OF MEASURED STIFFNESS VALUES

Because the experimental effort of FY 1987 was primarily intent upon resolving discrepancies between measured and calculated stiffness values, it is appropriate to review all the experimentally determined stiffness values obtained during this Program. Table VIII summarizes the geometry of all previous test structures.

Initially in this Program, measured stiffness values from static and dynamic tests[2,3,6] were compared with theoretical values that were determined using a modulus of elasticity calculated from the empirical formula in ACI 349-85.[11] The empirical formula generally gave a higher value for the concrete's modulus than the values measured from test specimens. It is the opinion of a member of the TRG that this formula does not apply to micro-concrete. In addition, theoretical stiffness values were determined using measured moduli from the ASTM standard test. Because this investigation is concerned with determining the proper values of stiffness to be used in the analysis of Seismic Category I Structures, it is felt that the best estimate of actual material properties should be used when experimental results are compared with theory. The comparisons between measured and theoretical stiff-nesses that were calculated with the empirical modulus do, however, provide information concerning analytical differences that could occur during the design process, when material properties have yet to be measured. These comparisons have been reported in all subsequent investigations.[7-9]

A. Review of Previous Static Test Results Obtained In the Seismic Category I Structure Program

Table IX summarizes the previous static test results using both the meas-ured and design values for the concrete's modulus. These results are discussed in the following paragraphs.

  1. Isolated Shear Walls. The first static tests were performed on single-story isolated shear walls and were reported in Ref. 2. These walls are shown in Fig. 1. Five walls were tested, two monotonically and three cyc-lically. These specimens were made with microconcrete and with wire mesh rein-forcement. The amount of reinforcement at the shear wall base and shear wall

TABLE VIII
SUMMARY OF LOS ALAMOS TEST STRUCTURE GEOMETRY

Type of[a] Structure	Wall Thickness (in.)	Aspect[b] Ratio (h/L)	Number Tested Static	Number Tested Dynamic	Reinforcement[d] %, each direction	Max[e] Normal Stress (psi)
Isolated Shear Walls, 1-story	1.0	0.42	5	6	0.56 Hardware cloth	D = 19.5 S = 0.625
Isolated Shear Walls, 2-story	1.0	0.42	0	1	0.56 Hardware cloth	39.0
Diesel Generator Building, 1-story, 1/30-scale	1.0	0.40 0.73	11	2	0.56 Hardware cloth	5.3
Diesel Generator Building, 2-story 1/30-scale	1.0	0.73	0	3	0.56 Hardware cloth	10.6
Diesel Generator Building, 2-story 1/10-scale	3.0	0.73	0	2	0.56 Model rebar	10.8
Auxiliary Bldg. 3-story, 1/42-scale	1.0	0.38	0	1	0.56 Hardware cloth	17.6
Auxiliary Bldg. 3-story 1/14-scale	3.0	0.38	0	1	0.56 Model Rebar	10.8
TRG-1	1.0	1	(c)	1	0.56 Hardware cloth	10.4
TRG-3	4.0	1	(c)	1	0.61 #3 Rebar	42.3
TRG-4	6.0	1	1	0	0.25 #3 Rebar	31.0
TRG-5	4.0	1	1	0	0.61 #3 Rebar	42.3
TRG-6	6.0	0.27	1	0	0.5 #3 Rebar	25.7

a   All structures were made with microconcrete except TRG-3 through TRG-6; these were made with 3/4-in. aggregate concrete.

b   For multi-story structures, the aspect ratio reported is for an individual floor.

c   TRG-1 and TRG-3 were statically tested to low-stress levels before the dynamic tests.

d   Hardware cloth is 0.042-in.-dia. welded wire fabric; model rebar is deformed model reinforcing rods obtained from the Portland Cement Association (0.113 in. dia).

e   With added mass used during dynamic tests. Static testing of the isolated shear walls was performed without added mass.

TABLE IX

PREVIOUS STATIC TEST RESULTS

	Measured Stiffness Before Cracking (lb/in.) 1	Ultimate* Compressive Strength f_c' (ksi)	Theoretical** Stiffness Using Measured Modulus (lb/in.) 2	Theoretical* Using ACI Empirical Modulus (lb/in.) 3	The Ratio of Columns		
					$\frac{2}{1}$	$\frac{3}{1}$	$\frac{2}{3}$
Isolated Shear Walls:							
1	0.78 x 10⁶	4.34	1.60 x 10⁶	2.33 x 10⁶	2.05	2.99	0.69
2	0.79 x 10⁶	5.89	–	2.71 x 10⁶	–	3.43	–
3	1.0 x 10⁶	7.35	1.90 x 10⁶	3.03 x 10⁶	1.90	3.03	0.63
4	1.06 x 10⁶	6.86	–	2.92 x 10⁶	–	2.75	–
5	0.87 x 10⁶	6.31	1.75 x 10⁶	2.80 x 10⁶	2.02	3.22	0.63
1/30-scale, 1-story, Diesel Generator Buildings:							
3D-2	0.76 x 10⁶	2.70	2.25 x 10⁶	2.90 x 10⁶	2.96	3.82	0.78
3D-4	1.74 x 10⁶	3.32	4.82 x 10⁶	6.08 x 10⁶	2.77	3.49	0.79
3D-7	0.92 x 10⁶	2.35	2.45 x 10⁶	2.71 x 10⁶	2.66	2.95	0.90
3D-8	0.80 x 10⁶	2.30	2.36 x 10⁶	2.68 x 10⁶	2.95	3.35	0.88
3D-9	1.67 x 10⁶	2.69	4.62 x 10⁶	5.47 x 10⁶	2.77	3.27	0.84
3D-10	1.14 x 10⁶	3.27	–	3.19 x 10⁶	–	2.80	–
3D-11	0.92 x 10⁶	3.09	–	3.11 x 10⁶	–	3.38	–
3D-12	1.23 x 10⁶	2.05	–	2.53 x 10⁶	–	2.06	–
3D-13	0.88 x 10⁶	2.04	–	2.52 x 10⁶	–	2.86	–
3D-19	0.80 x 10⁶	4.70	–	3.83 x 10⁶	–	4.79	–
3D-20	1.08 x 10⁶	4.30	3.22 x 10⁶	3.65 x 10⁶	2.98	3.38	0.88
TRG1	0.75 x 10⁶	3.77	1.2 x 10⁶	1.3 x 10⁶	1.60	1.73	0.92
TRG3	4.4 x 10⁶	3.81	3.0 x 10⁶	5.0 x 10⁶	0.68	1.13	0.60
TRG4	8.5 x 10⁶	4.15	8.4 x 10⁶	9.6 x 10⁶	0.99	1.13	0.88
TRG5	6.9 x 10⁶	5.03	6.8 x 10⁶	7.1 x 10⁶	0.99	1.03	0.96
TRG6	58.2 x 10⁶	4.69	48.5 x 10⁶	54.8 x 10⁶	0.83	0.94	0.89

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* The empirical modulus, $E_{c_{ACI}}$, is $57{,}000 \sqrt{f_c'}$, and the measured modulus, E_{c_m}, can be computed by the following formula:

$$E_{c_m} = 57{,}000 \sqrt{f_c'} \left\{ \frac{\text{Stiffness Col. 2}}{\text{Stiffness Col. 3}} \right\} .$$

** Based on the gross section.

top plate interface was varied along with the amount of moment reinforcement in the form of threaded steel rods located at the ends of the shear wall.

All specimens remained essentially linear up to a load producing a nominal-base shear stress (NBSS) of 200 psi and a principal tensile stress (PTS) of 600 psi or more. The load at first cracking, as predicted from a strength-of-materials approach, agreed very well with the measured cracking strength of the walls and the average split-cylinder tensile strength of 670 psi. Also, when the walls were subjected to repeated load cycles below the first-cracking load, there was no evidence of stiffness degradation or increase in the area of the hysteresis loop for a given load level. Above the first-cracking load, stiffness degraded and the area of the hysteresis loop increased with increased load and increased cycles at a constant load. The ultimate strength of the walls exceeds the provisions for shear capacity, as determined by ACI 349-85, 11.10. The measured stiffnesses in the linear region were down by a factor of 1.90 to 2.05 from the calculated uncracked cross-section stiffness using a measured modulus.

2. 1/30-Scale, Single-Story, Diesel Generator Buildings. Eleven 1/30-scale, single-story, diesel generator buildings were statically tested to failure and are reported in Ref. 3. These structures had a geometry identical to that of the second floor of the 1/30-scale, two-story diesel generator buildings (Fig. 2). Nine models were tested monotonically, eight in the transverse direction and one in the longitudinal direction. Two models were tested cyclically, one each in the transverse and longitudinal directions. All these specimens were made with microconcrete and with wire mesh reinforcement. Other than the direction of applied load, the only parameters that were varied in these tests were the amount of cure time each model experienced before testing and the embedment length of the reinforcement into the base of the structure.

As with the isolated shear walls, all specimens remained linear up to the load that produced cracking. This load produced an NBSS on the order of 200 psi and a PTS on the order of 340 psi, assuming the end walls were fully effective in bending. At a given load level below the first-cracking load, the area under the hysteresis loop remained constant when the load was cycled and the stiffness remained constant. Above the cracking load, stiffness again was observed to degrade and the area of the hysteresis loop increased with either increases in load level or increases in the number of load cycles. The load at

first cracking was in good agreement with the value predicted from strength-of-materials analysis and the measured tensile stress of the concrete. Provisions for the shear capacity of the walls from ACI 349-85 were exceeded. Stiffness based on a secant from the origin to half the ultimate load were down by factors ranging from 2.7 to 3.0, when compared with the calculated stiffness based on an uncracked cross section and measured modulus.

It should be noted that the moment of inertia used in the calculated stiffness value and principal stress calculations considered the entire end wall to contribute to the flexural stiffness of the shear wall, and the modulus of elasticity was based on the measured values. No effect from cure time or embedment length was observed.

3. TRG-Type Structures. TRG-3 and the two 1/4-scale models of it, TRG-1 and -2, were tested statically and monotonically at low-load levels that produced a NBSS of 28 psi and a PTS of 40 psi on TRG-3 and a NBSS of 53 psi and a PTS of 80 psi on TRG-1 and TRG-2. TRG-1 and -2 are shown in Fig. 17 and TRG-3 is shown in Fig. 4.

These tests were repeated several times and were intended to identify the initial stiffness condition of each model while introducing a minimum amount of damage into the test structure. TRG-3 was constructed with conventional concrete and No. 3 rebar, and TRG-1 and -2 were made with microconcrete and wire mesh reinforcement.

During these low-level tests, TRG-3 showed a measured stiffness up by a factor of 1.47 from the uncracked cross-section stiffness, and TRG-1 showed a reduction of 1.60 from the theoretical stiffness. In both cases, the theoretical stiffness was computed with a measured value of E_c and the end walls were considered fully effective in bending. However, the measured modulus for TRG-3 was considerably less than the empirical modulus (2.1×10^6 psi compared to 3.5×10^6 psi). TRG-2 was found to have significant shrinkage cracks; results from this model were not considered to be accurate. When properly scaled, the static stiffness values for the two models were in good agreement, showing that stiffness can be scaled from microconcrete to conventional concrete in this low-load level region.

TRG-4 and TRG-5 were tested statically to failure in a cyclic manner and TRG-6 was tested statically to first cracking. TRG-4 is shown in Fig. 5, TRG-5 was identical to TRG-3, and TRG-6 is shown in Fig. 6. TRG-4 and TRG-5 exhibited repeatable linear response with stiffnesses that were almost identical to theory

until first cracking. TRG-6 exhibited stiffness values that were 20% above theory until first cracking. This increased stiffness was assumed to result from errors in the deformation readings caused by limitations in the resolution of the instrumentation. For TRG-4, first cracking occurred when a NBSS of 131 psi and a PTS of 171 psi were reached. For TRG-5, this occurred approximately at a NBSS of 167 psi and a PTS of 227 psi. For TRG-6, first cracking occurred at a NBSS of 150 psi and a PTS of 169 psi. "Approximately" is used with the TRG-5 value because an unplanned load excursion prevented the actual value from being recorded. For TRG-4 and TRG-5, the components of stiffness caused by shear and bending were separated, and these components also agreed with their respective theoretical values. Because of the low aspect ratio of TRG-6, bending deformations could not be accurately measured and, hence, the individual components of stiffness could not be assessed. After cracking, the structures behaved once again in a linear manner when loaded to levels that did not exceed the peak load during the first-cracking cycle. During these cycles, the stiffness in TRG-4 and TRG-5 was down by a factor of 2, with the loss occurring equally in each component of the stiffness. The stiffness in TRG-6 did not degrade as much after cracking as it did with TRG-4 and TRG-5. Only a 25% reduction in stiffness was observed in TRG-6 after cracking. Figure 23 shows the degradation in stiffness as a function of the NBSS caused by the applied load.
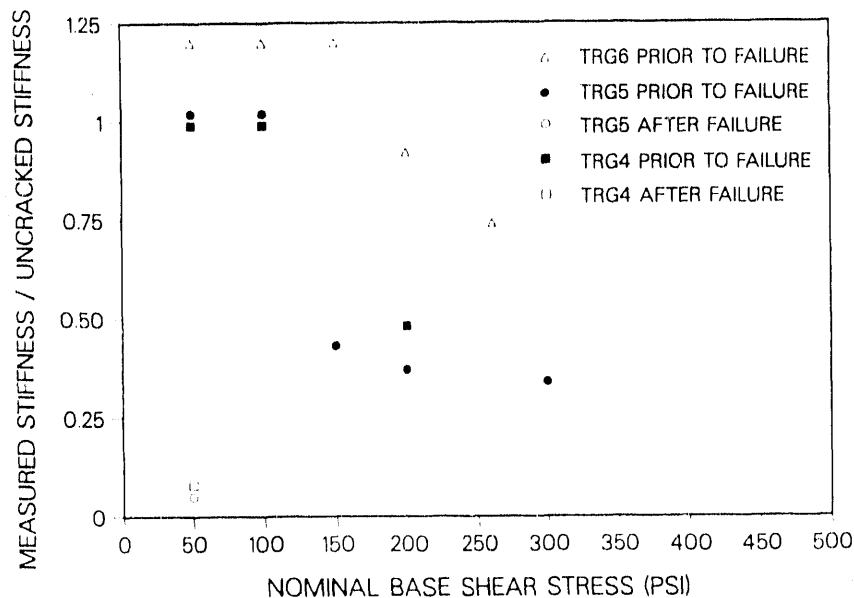

Fig. 23. Reduction in stiffness as a function of the NBSS for the structures that were quasi-statically cycled.

The testing of TRG-1 is discussed in detail in Ref. 7. TRG-3 testing is discussed in Ref. 8, and the tests on TRG-4 through -6 are reported in Ref. 9 and subsequent reports to be issued by Los Alamos.

B. Review of Previous Dynamic Test Results Obtained in the Seismic Category I Structures Program

Table X summarizes the measured material properties for all the dynamic test specimens except TRG-1 and TRG-3. The properties for TRG-1 and TRG-3 can be found in Table IX.

TABLE X

MEASURED PROPERTIES FOR DYNAMIC TEST SPECIMENS

Isolated Shear Walls	f'_c (ksi)	E_{c_m} (psi)	$57,000 \sqrt{f'_c}$ (psi)
10	7.48	3.5×10^6	4.93×10^6
11	6.27	3.4×10^6	4.51×10^6
12	5.74	3.0×10^6	4.32×10^6
13	6.85	3.4×10^6	4.72×10^6
21	7.18	3.9×10^6	4.83×10^6
23	5.32	3.1×10^6	4.16×10^6
2-2	7.45	3.1×10^6	4.92×10^6

$1/30$-Scale, Single-Story Diesel Generator Building	f'_c (ksi)	E_{c_m} (psi)	$57,000 \sqrt{f'_c}$ (psi)
3D-5	2.62	2.4×10^6	2.92×10^6
3D-6	2.50	2.4×10^6	2.85×10^6

Two-Story Diesel Generator Building	f'_c (ksi)	E_{c_m} (psi)	$57,000 \sqrt{f'_c}$ (psi)
3D-10-2 (1/30-Scale)	2.60	2.5×10^6	2.91×10^6
3D-11-2 (1/30-Scale)	2.89	-	3.06×10^6
3D-12-2 (1/30-Scale)	2.78	2.8×10^6	3.01×10^6
CERL 1 (1/10-Scale)	3.18	2.8×10^6	3.21×10^6
CERL 2 (1/10-Scale)	3.33	2.6×10^6	3.29×10^6

Three-Story Auxiliary Building	f'_c (ksi)	E_{c_m} (psi)	$57,000 \sqrt{f'_c}$ (psi)
1/42-Scale	2.90	2.7×10^6	3.07×10^6
1/14-Scale	3.32	2.8×10^6	3.28×10^6

1. Isolated Shear Walls. Four single-story, isolated shear wall structures were subjected to sine-sweep vibration tests. During these tests, the structures had added mass attached, as shown in Fig. 1. The results from these tests are summarized in Table XI. For all dynamic testing, the equivalent stiffness was determined indirectly from the resonant frequency measurements. Initially, these stiffness values were between a factor of 3.6 to 14.3 below the theoretical values, using the measured modulus, and between a factor of 5.0 and 18.1 below the theoretical values, using the ACI empirical modulus.

Two additional tests were performed on single-story isolated shear walls using simulated seismic inputs and random inputs. The results from these tests are summarized in Tables XII and XIII. Initially, stiffnesses were down by factors ranging from 4.2 to 5.7, when the measured modulus was used in the theoretical stiffness calculation; the stiffnesses were down by a factor ranging from 5.7 to 7.1, when the ACI empirical modulus was used.

Finally, a two-story isolated shear wall structure was tested with simulated seismic and random inputs. The results from this test are summarized in Table XIV. During all the dynamic tests, reductions in the resonant frequencies occurred before there were any visible signs of damage in the structures, and the reductions were greater during the sine-sweep testing than during the simulated-seismic or random testing. A detailed discussion of this testing can be found in Ref. 2.

2. Diesel Generator Buildings. Two 1/30-scale, single-story diesel generator building models were tested with random inputs. The results of these tests are summarized in Table XV. This table shows the indirectly determined stiffness compared with the theoretical stiffness obtained with an empirical modulus that assumes the entire end wall to be effective in resisting bending.

Five two-story diesel generator models (three 1/30-scale and two 1/10-scale), shown in Fig. 2, were tested with simulated seismic and random inputs. The results of these tests are summarized in Table XVI. These tests demonstrated scalability among different-size microconcrete models. Again, the measured resonant frequencies were down by a factor of 1.74 or more; this result suggests that stiffnesses were down by a factor of 3.0 or more. The details of all the diesel generator building tests are summarized in Ref. 3.

3. Auxiliary Building. Two different scale models (1/14- and 1/42-scale) of an auxiliary building were tested with both simulated seismic and random inputs. These structures are shown in Fig. 3 and the results from the 1/42-

TABLE XI

RESULTS OF SINE-SWEEP TESTS ON ISOLATED SHEAR WALLS

Structure	Test	Peak Response (g's)	Measured First Mode Frequency (Hz)	Theoretical First[a] Mode Frequency (Hz)	Theoretical First[b] Mode Frequency (Hz)	Measured First Mode Freq. / Calculated First Mode Freq. $E_{c_{ACI}}$	E_{c_m}	Measured Stiffness[c] / Computed Stiffness $E_{c_{ACI}}$	E_{c_m}	NBSS[d] psi
10	1	0.94	132	298	251	0.44	0.53	0.20	0.28	18
	2	1.57	125			0.42	0.51	0.18	0.26	30
	3	5.44								103
	4	5.38	72			0.24	0.29	0.06	0.08	102
11	1	0.97	67	285	247	0.24	0.27	0.06	0.07	18
	2	1.93	56			0.20	0.23	0.04	0.05	36
	3	3.03	50			0.18	0.20	0.03	0.04	57
	4	4.26	42			0.15	0.17	0.02	0.03	79
12	1	1.19	86	279	232	0.31	0.37	0.10	0.14	22
	2	2.41	72			0.26	0.31	0.07	0.10	46
	3	3.55	56			0.20	0.24	0.04	0.06	67
	4	4.59	53			0.19	0.23	0.04	0.05	87
	5	2.33	50			0.18	0.22	0.03	0.05	44
13	1	1.21	75	292	247	0.26	0.30	0.07	0.09	23
	2	2.14	66			0.23	0.27	0.05	0.07	40
	3	3.37	59			0.20	0.24	0.04	0.06	64
	4	4.21	48			0.16	0.19	0.03	0.04	80
	5	5.55	42			0.14	0.17	0.02	0.03	105

[a] Calculated using the ACI empirical modulus, $E_{c_{ACI}}$

[b] Calculated using the measured modulus, E_{c_m}

[c] $\dfrac{K_{meas}}{K_{comp}} = \left(\dfrac{f_{meas}}{f_{comp}}\right)^2$

[d] $NBSS = \dfrac{(340\ lb/g)\ (Peak\ Response\ Acc.)}{18\ in.^2}$

TABLE XII

ISOLATED SHEAR WALL MODEL 21 SIMULATED SEISMIC TEST RESULTS

Test	Peak Input Level (g's)	Peak Response (g's)	Measured First Mode Frequency (Hz)	Theoretical First[a] Mode Frequency (Hz)	Theoretical First[b] Mode Frequency (Hz)	Measured First Mode Freq. / Calculated First Mode Freq. $E_{C_{ACI}}$	Measured First Mode Freq. / Calculated First Mode Freq. E_{C_m}	Measured Stiffness[c] / Computed Stiffness $E_{C_{ACI}}$	Measured Stiffness[c] / Computed Stiffness E_{C_m}	NBSS[d] (psi)
EE1 x 5	0.35	0.60	111	295	265	0.38	0.42	0.14	0.18	11
EE1 x 10	0.55	0.94	106			0.36	0.40	0.13	0.16	18
EE1 x 10	1.19	1.78	105	295	265	0.36	0.40	0.13	0.16	34
EE1 x 10	2.48	3.97	99			0.34	0.37	0.11	0.14	75
EE1 x 20	0.53	0.90	106			0.36	0.40	0.13	0.16	17
EE1 x 20	0.88	1.67	105	295	265	0.36	0.40	0.13	0.16	32
EE1 x 20	2.16	4.32	93			0.32	0.35	0.10	1.12	82
EE1 x 50	0.63	1.13	105	295	265	0.36	0.40	0.13	0.16	21
EE1 x 50	1.28	2.56	99			0.34	0.37	0.11	0.14	48
EE1 x 50	3.42	5.81	88			0.30	0.33	0.09	0.11	110
EE1 x 50	3.83	6.13	88			0.30	0.33	0.09	0.11	116
EE1 x 50	6.02	8.43	85			0.29	0.32	0.08	0.10	159

a Calculated using the ACI empirical modulus, $E_{C_{ACI}}$

b Calculated using the measured modulus, E_{C_m}

c $\dfrac{K_{meas}}{K_{comp}} = \left(\dfrac{f_{meas}}{f_{comp}}\right)^2$

d $NBSS = \dfrac{(340\ \text{lb/g})(\text{Peak Response Acc.})}{18\ \text{in.}^2}$

TABLE XIII

ISOLATED SHEAR WALL MODEL 23 SIMULATED SEISMIC TEST RESULTS

Test	Peak Input Level (g's)	Peak Response (g's)	Measured First Mode Frequency (Hz)	Theoretical First Mode Frequency (Hz) [a]	Theoretical First[b] Mode Frequency (Hz)	Measured First Mode Freq. / Calculated First Mode Freq. $E_{c_{ACI}}$	E_{c_m}	Measured Stiffness[c] / Computed Stiffness $E_{c_{ACI}}$	E_{c_m}	NBSS[d] (psi)
EE1 x 5	0.34	0.51	115	274	236	0.42	0.49	0.18	0.24	9.6
EE1 x 10	0.69	0.95	115			0.42	0.49	0.18	0.24	18
EE1 x 10	1.21	1.54	112			0.41	0.48	0.17	0.23	29
EE1 x 10	3.46	4.36	110			0.40	0.47	0.16	0.22	82
EE1 x 20	0.95	1.54	108	274	236	0.39	0.46	0.16	0.21	29
EE1 x 20	1.88	3.46	106			0.39	0.45	0.15	0.20	65
EE1 x 20	2.70	5.00	99			0.36	0.42	0.13	0.18	94
EE1 x 20	4.10	6.56	93			0.34	0.40	0.12	0.16	124
EE1 x 50	0.46	1.04	115	274	236	0.42	0.49	0.18	0.24	20
EE1 x 50	0.54	1.04	115			0.42	0.49	0.18	0.24	20
EE1 x 50	0.94	1.54	108			0.39	0.46	0.16	0.21	29
EE1 x 50	2.34	4.42	107			0.39	0.46	0.16	0.21	83
EE1 x 50	4.77	6.96	96			0.35	0.41	0.13	0.17	131
EE1 x 50	10.70	12.5	73			0.27	0.31	0.07	0.10	236
EE1 x 50	13.80	11.9	58			0.21	0.25	0.05	0.06	225
EE1 x 50	20.80	13.3	58			0.21	0.25	0.05	0.06	251

a   Calculated using the ACI empirical modulus, $E_{c_{ACI}}$

b   Calculated using the measured modulus, E_{c_m}

c $\dfrac{K_{meas}}{K_{comp}} = \left(\dfrac{f_{meas}}{f_{comp}}\right)^2$

d $NBSS = \dfrac{(340 \text{ lb/g})(\text{Peak Response Acc.})}{18 \text{ in.}^2}$

TABLE XIV

ISOLATED SHEAR WALL MODEL 2-2 SIMULATED SEISMIC TEST RESULTS

Test	Peak Input Level (g's)	Peak Response Level (g's) 1st Floor	2nd Floor	Measured First Mode Frequency (Hz)	Theoretical First[a] (Hz)	Theoretical First[b] Mode Frequency	Measured First Mode Freq./Calculated First Mode Freq. $E_{c_{ACI}}$	E_{c_m}	Measured Stiffness[c]/Computed Stiffness $E_{c_{ACI}}$	E_{c_m}	NBSS[d] psi
EE1 x 5	0.37	0.40	0.54	55	184	146	0.30	0.38	0.09	0.14	18
EE1 x 10	0.66	0.92	1.47	54			0.30	0.37	0.09	0.14	43
EE1 x 20	0.55	0.65	0.94	53	184	146	0.29	0.37	0.08	0.13	29
EE1 x 50	0.46	0.55	1.05	55	184	146	0.30	0.38	0.09	0.14	29
EE1 x 50	1.97	2.68	3.55	32			0.17	0.22	0.03	0.05	112
EE1 x 50	4.26	7.20	5.33	27			0.15	0.19	0.02	0.03	226
EE1 x 50	7.62	9.98	8.99	27			0.15	0.19	0.02	0.03	341

a Calculated using the ACI empirical modulus, $E_{c_{ACI}}$

b Calculated using the measured modulus, E_{c_m}

c $\dfrac{K_{meas}}{K_{comp}} = \left(\dfrac{f_{meas}}{f_{comp}}\right)^2$

d NBSS = $\dfrac{(340 \text{ lb/g})(\text{1st Floor Peak Response Acc.}) + (340 \text{ lb/g})(\text{2nd Floor Peak Response Acc.})}{18 \text{ in.}^2}$

TABLE XV

1/30-SCALE DIESEL GENERATOR BUILDING MODELS DYNAMIC TEST RESULTS

Structure	Test[a]		Input level (g's)	Measured First Mode Frequency (Hz)	Theoretical First[b] Mode Frequency (Hz)	Theoretical First[c] Mode Frequency (Hz)	Measured First Mode Freq. / Calculated First Mode Freq.		Measured Stiffness[d] / Computed Stiffness	
							$E_{c_{ACI}}$	E_{c_m}	$E_{c_{ACI}}$	E_{c_m}
30 5	1.	No Mass L	0.5	960	1590	1440	0.60	0.67	0.36	0.44
	2.	130 lb. L	0.5	325	569	516	0.57	0.63	0.33	0.40
	3.	230 lb. L	0.5	247	441	400	0.56	0.62	0.31	0.38
	4.	No Mass T	0.5	560	1150	1040	0.49	0.54	0.24	0.29
	5.	130 lb. T	0.5	212	413	374	0.51	0.57	0.26	0.32
	6.	230 lb. T	0.5	155	320	290	0.48	0.53	0.23	0.29
30 6	1.	No Mass T	0.5	560	1133	1040	0.49	0.54	0.24	0.29
	2.	230 lb. T	0.5	167	316	290	0.57	0.58	0.28	0.33

a The weights indicate steel plates that were added to the top of the structure. L - model was tested in the longitudinal direction. T - model was tested in the transverse direction.

b Calculated using the ACI empirical modulus, $E_{c_{ACI}}$

c Calculated using the measured modulus, E_{c_m}

d $\dfrac{K_{meas}}{K_{comp}} = \left(\dfrac{f_{meas}}{f_{comp}}\right)^2$

TABLE XVI

TWO-STORY DIESEL GENERATOR BUILDING SIMULATED SEISMIC TEST RESULTS

Structure	Test	Peak Input Level (g)	Measured First Mode Frequency (Hz)	Theoretical First Mode Frequency (Hz) [a]	Theoretical First Mode Frequency (Hz) [b]	Measured First Mode Freq / Calculated First Mode Freq $E_{c_{ACI}}$	E_{c_m}	Measured Stiffness / Computed Stiffness [c] $E_{c_{ACI}}$	E_{c_m}
3D 10 2 1/30 Scale	1	1.5	104	197	181	0.53	0.57	0.28	0.33
	2	5.3	80	--	--	0.41	0.44	0.16	0.20
3D-11 2 1/30 Scale	1	0.5	94	224	--	0.42	--	0.18	--
	2	0.8	93	--	--	0.42	--	0.18	--
	3	1.0	92	--	--	0.41	--	0.17	--
	4	1.5	90	--	--	0.40	--	0.16	--
	5	8.2	63	--	--	0.28	--	0.08	--
3D 12 2 1/30 Scale	1	0.4	94	216	202	0.44	0.47	0.19	0.22
	2	0.8	93	--	--	0.43	0.46	0.19	0.21
	3	1.4	91	--	--	0.42	0.45	0.18	0.20
	4	3.2	91	--	--	0.42	0.45	0.18	0.20
	5	4.1	90	--	--	0.42	0.44	0.17	0.20
CERL #1 1/10 Scale	1	0.7	54	152	142	0.35	0.38	0.12	0.14
	2	1.2	54	--	--	0.35	0.38	0.12	0.14
	3	2.0	51	--	--	0.34	0.36	0.11	0.13
	4	2.7	50	--	--	0.33	0.35	0.11	0.12
	5	3.5	49	--	--	0.32	0.35	0.10	0.12
CERL #2 1/10 Scale	1	0.8	53	145	129	0.37	0.41	0.14	0.17
	2	0.7	53	--	--	0.37	0.41	0.14	0.17
	3	1.8	50	--	--	0.34	0.39	0.12	0.15
	4	3.9	48	--	--	0.33	0.37	0.11	0.14
	5	5.4	46	--	--	0.32	0.36	0.10	0.13

[a] Calculated using the ACI empirical modulus, $E_{c_{ACI}}$

[b] Calculated using the measured modulus, E_{c_m}

[c] $\dfrac{K_{meas}}{K_{comp}} = \left(\dfrac{f_{meas}}{f_{comp}}\right)^2$

scale models are summarized in Table XVII. The reductions in stiffness shown
in Table XVII are consistent with the reductions observed in the two-story
diesel generator buildings. An unplanned load excursion occurred while the
1/14-scale model was on the shake table and it produced visible cracking into
the structure. Therefore, no data were obtained on this structure in its
initial condition. The details of these tests are summarized in Ref. 6.

   4. TRG-Type Structures. TRG-1 and -3 were both tested with simulated
seismic inputs. In addition, random inputs were applied to TRG-1 and haversine
pulses were applied to TRG-3. Again, stiffnesses determined indirectly from
resonant frequency measurements were found to be a factor of 2.6 to 4.0 below
the theoretical stiffness values using the measured modulus and assuming the
entire end walls were effective in their contribution to the bending stiffness.

   When TRG-1 was subjected to a 0.5-g peak acceleration random input, it re-
sponded with a stiffness that was down by a factor of 2.6 from theory (as
inferred from a resonant frequency that was a factor of 1.6 below theory),
even though this excitation produced only 16.3 psi NBSS and 16.6 PTS. Similar
stiffness values were obtained during a 0.5-g seismic test. TRG-3 responded to
a 0.73-g seismic test with a stiffness that was down by a factor of 4.0 from
theory at an NBSS of 91 psi and a PTS of 92 psi.

   Experimental modal analyses were performed on all the TRG type structures.
During these tests, free boundary conditions were simulated by supporting the
structures on air-bearings or, in the case of TRG-1, a foam pad. Results of
these tests were compared to the results from finite element modal analyses of
the structures. In general, the experimental and analytical modal analyses
agreed implying that when the structures were subjected to the low level random
excitations used during experimental tests, they responded with a stiffness
that finite element analyses would have predicted. Table XVIII summarizes the
experimental modal analysis results. Dynamic tests and results for TRG-1 are
discussed in Ref. 7, TRG-3 results are discussed in Ref. 8, TRG-4 modal analy-
sis results are discussed in Ref. 9 and modal analysis results for TRG-5 and
-6 will appear in subsequent Los Alamos reports.

C. Comparison of Stiffnesses Measured From Static and Dyanmic Test Results
   1. Isolated Shear Walls. When normalized to a common modulus of elas-
ticity, the static stiffness values can be compared with those measured

TABLE XVII

1/42-SCALE AUXILIARY BUILDING MODEL SIMULATED SEISMIC TEST RESULTS

Test	Peak Input Level (g's)	Measured First Mode Frequency (Hz)	Theoretical First[a] Mode Frequency (Hz)	Theoretical First[b] Mode Frequency (Hz)	Measured First Mode Freq. / Calculated First Mode Freq. $E_{c_{ACI}}$	E_{c_m}	Measured Stiffness[c] / Computed Stiffness $E_{c_{ACI}}$	E_{c_m}
Bare model Random	1.0	187	435	400	0.43	0.47	0.18	0.22
Mass added Random	0.17	80	156	144	0.51	0.55	0.26	0.31
Mass added Seismic	0.5	79	156	144	0.51	0.55	0.26	0.31
	1.0	78	--		0.50	0.54	0.25	0.29
	2.0	73	--		0.47	0.51	0.22	0.26
	2.9	69	--		0.44	0.48	0.20	0.23
	6.2	60	--					
	6.7	47	--		0.30	0.33	0.09	0.11
	10.7	30	--		0.19	0.21	0.04	0.04

[a] Calculated using the ACI empirical modulus, $E_{c_{ACI}}$

[b] Calculated using the measured modulus, E_{c_m}

[c]
$$\frac{K_{meas}}{K_{comp}} = \left(\frac{f_{meas}}{f_{comp}}\right)^2$$

TABLE XVIII

A COMPARISON OF RESONANT FREQUENCIES IDENTIFIED FROM THE EXPERIMENTAL MODAL ANALYSIS AND THE RESONANT FREQUENCIES IDENTIFIED FROM THE ANALYTICAL MODAL ANALYSIS OF ALL THE TRG-5 STRUCTURES

Mode	Experimental Before Cracking** (Hz)					Linear Finite Element Analysis*** (Hz)				
	TRG-1	TRG-3	TRG-4	TRG-5	TRG-6	TRG-1	TRG-3	TRG-4	TRG-5	TRG-6
1	112	29	37.1	31.9	92.9	106.	21.	36.3	31.9	91.8
2			79.2	67.0	123			77.8	72.3	125.1
3			88.3	73.9	136			86.	79.7	134.9
4			100.	77.8	179			102.	88.4	172.6
5	307	75	111.	84.4	208	290.	57.	111.	95.2	197.2
6			122.	*	*			120.	112.	206.1
7			*	117.	*			130.	113.	–
8			141.	126.	*			136.	129.	–
9			*	*	*			143.	133.	–
10			172.	*	*			154.	135.	–
11			*	159.	*			162.	152.	–
12				170.	*			–	196.	–
13				198	*			–	230	–

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* These modes were not identified.

** Free boundary conditions were simulated with air-bearings or foam pads under the structures.

*** Calculated with the measured modulus, E_{C_m}, and free boundary conditions.

After TRG-3 had been shipped to the shake table facility in Champaign, IL, cracks became visible in the base of the structure; this suggested that the model had been damaged in shipping.

dynamically during sine-sweep and with simulated seismic tests of similar isolated shear wall models. At force levels that were 10% of the load required to produce first cracking (200 psi NBSS, 600 psi PTS) in the static test, stiffnesses measured during the sine-sweep and simulated seismic tests were considerably lower than those obtained during static tests. They were even lower than those calculated by using an uncracked cross-section stiffness value with a measured modulus. The sine-sweep and seismic resonant frequency values were down, on the average, by a factor of 2.6 and 2.2 from the calculated uncracked value, respectively. This result suggests that stiffness values were down by an average factor of 6.7 and 4.8 from the calculated uncracked value. In turn, the calculated uncracked values are down by an average factor of 2.9 and 1.9 from the average measured static value.

2. 1/30-Scale, Single-Story Diesel Generator Buildings. When these models were tested dynamically with a 0.5-g's is peak acceleration random input producing an NBSS of 6.3 psi and a PTS of 10.6 psi, the models indicated resonant frequencies that were a factor of 1.7 to 1.95 below theory, suggesting that stiffnesses were down by a factor of 2.9 to 3.8 from the strength-of-materials prediction using a measured modulus. These results can be compared with the static results that showed reductions in stiffness between 2.7 and 3.0 from the strength-of-materials prediction using a measured modulus. When normalized to a common modulus of elasticity, the dynamic stiffnesses were, on the average, down by a factor of 1.15 from the static stiffness values. It should be reiterated that the static stiffnesses were determined by a secant from the origin to half the ultimate load, when the NBSS was on the order of 200 psi and the PTS was on the order of 300 psi. These stress levels are significantly higher than the ones induced by the dynamic excitations.

3. TRG-1 and TRG-3. TRG-4 exhibited a stiffness that was a factor of 1.60 below theory when tested to a maximum NBSS of 53 psi and a maximum PTS of 28 psi. During the first 0.5-g's peak acceleration random input, the stiffness was down by a factor of 2.6 at excitation levels that produced an NBSS of 16.3 psi and a PTS of 16.3 psi.

TRG-3's static stiffness was a factor of 1.47 above theory when the loads produced a maximum NBSS of 28 psi and a maximum PTS of 40 psi. When TRG-3 was subjected to a 0.73-g's seismic test that produced an NBSS of 91 psi and a PTS of 92 psi, the stiffness was down by a factor of 4.0.

APPENDIX B

THE TECHNICAL REVIEW GROUP'S RESPONSE

TO QUESTIONS CONCERNING THE VALIDITY OF THIS PROGRAM'S RESULTS

January 4, 1988

REVIEW OF TESTS ON MODEL SHEAR WALLS

Appendix I through Appendix XVII give details of a brief review of the literature on tests on shear walls and information on aggregate used on nuclear power plants in the US.

Based upon these and other tests and on the writer's "hands on" experience on the design and field construction of many plants around the world, it is recommended that the results of the Los Alamos tests not be used on the analysis of US nuclear power plants.

Ken Buchert

NOTE FROM THE AUTHORS

Ken Buchert did not respond directly to the questions that were posed to the TRG. Instead, he sent the above note and appendices. When asked to specifically address the questions over the phone he gave the following answers:

1. Are the tests in this program valid for addressing the program objectives?
   Ken Buchert's response: No

2. In the light of the program objectives, are the model test data obtained applicable to nuclear power plant structures?
   Ken Buchert's response: No

3. Have the technical issues of scaling, instrumentation, and model fabrication effects been resolved?
   Ken Buchert's response: No

4. Should there be another "carefully handled" dynamic test to address the possible "dynamic effects" issue? If so, what configuration?
   Ken Buchert's response: No

5. Have we obtained enough data and have we tested the correct configurations to meet the program objectives?
   Ken Buchert's response: No opinion

6. Would the variability in stiffness observed in the models be observed in real nuclear plant structures at comparable load levels?
   Ken Buchert's response: To some extent

In the interest of brevity only a list of the appendices that Ken Buchert sent to Los Alamos is supplied.

LIST OF APPENDICES SENT BY KEN BUCHERT

8103 Broadway, Suite 102 • P.O. Box 6477 • San Antonio, Texas 78209
(512) 824-5960

December 30, 1987

Mr. Joel G. Bennett
Mail Stop J576
Los Alamos National Laboratory
Los Alamos, NM 87545

Dear Joel:

I have read (or reread) the reports and papers you sent with your letter of November 16, and have thought at some length about the questions you pose in your letter. Sorry that I couldn't respond in writing before now, but we seem to be having a pre-Christmas rush in our small business. I will now try to follow up my earlier phone call with this written response. I will take your questions in order:

1.   Are the tests in this program valid for addressing the program objectives?

I feel that the tests in this program are indeed valid for addressing the program objectives (if not, then we all ought to turn in our union cards).

2.   In light of the program objectives, are the model test data obtained applicable to nuclear power plant structures?

I believe that the model test data most certainly should apply to the classes of nuclear power plant structures they were intended to represent. I probably have fewer reservations on the applicability of model test data to larger structures than many of the TRG.

3.   Have the technical issues of scaling, instrumentation and model fabrication effects been resolved?

The model analysis has been done carefully and correctly. Instrumentation has, in my opinion, been excellent to superior throughout the parts of the program I have followed in detail. I also believe that model fabrication effects have been largely resolved, and that the issue Ken Buchert raises regarding lack of very detailed testing or characterization of the aggregate for the latest models is a minor issue, having little effect on test results. But, one key issue certainly appears to be unresolved. That is, "Why are the stiffnesses of the last two TRG models the **only** measured stiffnesses in the entire program which reach the full values calculated using strength of materials methods for uncracked concrete?"

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4.   **Should there be another "carefully handled" dynamic test to address the possible "dynamic effects" issue? If so, what configuration?**

It is possible that another dynamic test or tests on carefully handled models could address this issue. I will defer to other TRG members in choosing a configuration, but the size and configuration **must** be well within the testing capabilities of the test facility.

5.   **Have we obtained enough data and have we tested the correct configurations to meet the program objectives?**

I feel that you certainly have enough data on the configurations tested. As to whether the current configurations are the correct ones, I will defer to other members of the TRG.

6.   **Would the variability in stiffness observed in the models be observed in real nuclear plant structures at comparable load levels?**

In response to this question, I have a reply which the NRC and other members of the TRG may feel is impractical. My reply is, "Why don't you find out?" At least, find out what the **stiffnesses** are for shear walls in existing plant structures by "thumping" them and measuring their response frequencies together with as-built drawings. This should allow stiffness calculations to be easily made. The "thumper" could be an air impulser, of a type developed primarily by SwRI to impulse-load a large submarine hull model. It utilizes a compressed gas bottle with an expansion nozzle, opened rapidly by a rupture disc at the nozzle throat. A very fast rising reaction force occurs, with exponential decay as the vessel exhausts.

In-service buildings could be tested with no damage, or out-of-service buildings could perhaps be subjected to larger impulses.

Perhaps this idea is unreasonable or too expensive to field, but I feel it would perhaps give us more useful information than building and dynamically testing one or more new structural models.

Joel, I hope that this letter and my suggestions are of some use to you and Roger Keanneally.

Sincerely,

Dr. Wilfred E. Baker
President

/tme

December 11, 1987

Dr. Joel G. Bennett
Mail Stop J576
Advanced Engineering Technology
LOS ALAMOS NATIONAL LABORATORY
Los Alamos, NM 87545

RE: STIFFNESS OF CONCRETE LOW-RISE SHEAR WALL STRUCTURES TEST PROGRAM

Dear Joel:

This letter is being written in response to your request for written comments
from the Technical Review Group (TRG) on the subject test program.

Background Comments

In 1982, a whole series of small-scale shear wall structures were tested both
cyclic statically and dynamically, using a simulated seismic time history.
These test structures were made of microconcrete and model rebar. Such model
test structures contained both 1" thick walls (called 1/30- and 1/42-scale
tests) and 3" thick walls (called 1/10- and 1/14-scale tests). One of the
purposes of these tests was to better understand the stiffness of concrete
low-rise shear wall structures under SSE and lesser levels of seismic shaking.
Another purpose was to better understand the influence of stiffness degrada-
tion at higher levels of shaking on in-structure (floor) spectra to which
equipment are subjected.

It is my understanding that all of these tests (both cyclic static and
dynamic) exhibited substantial reduction in overall stiffness or natural
frequency below values computed using uncracked-strength-of-materials
approaches at low input load levels (less than 100 psi average shear stress).
The reduction of stiffness below that computed from uncracked-strength-of-
materials approaches tended to average about a factor of 4 at shear stress
levels corresponding to about OBE seismic input. At higher shaking levels,
the stiffness continued to degrade to factors substantially greater than 4
below the computed uncracked stiffness.

Frankly, I was very surprised at the fairly consistent reduction of stiffness
of about a factor of 4 below the computed uncracked stiffness at input levels
resulting in average shear stresses less than 100 psi and sometimes even less
than 50 psi. The further reduction of stiffness at higher stress levels
beyond concrete-cracking stress levels was expected and is consistent with
theoretical models. Because of several open issues concerning these tests of

microconcrete models, I could not fully support that these tests demonstrated that real concrete low-rise shear wall structures were likely to have reduced stiffness of about a factor of 4 below the computed uncracked stiffness when at low average shear stress levels of less than about 100 psi. I judged that these tests exaggerated the effect, but that they did demonstrate that significant reduction at low stress levels was certainly possible. The open issues with these tests were all related to the small scale of the models and the use of microconcrete. Because of the small scale, about anything could reduce stiffness.

In my judgment:

1. Trivial amounts of base rotation or base attachment flexibility could easily account for a factor of 4 stiffness reduction in these small models.

2. Thin walls (1" and 3" thick walls) can more easily be cracked by shrinkage, aging, and handling effects than could actual walls which are generally 12" and greater thickness. Furthermore, any existing non-visible cracks of such small-scale models could have more influence on their stiffness than could small, only slightly visible or non-visible cracks on real-scale prototype walls.

3. There is likely to be less aggregate interlock in small-scale models with microconcrete than in full-scale walls. With less aggregate interlock, cracks could result in a greater reduction of stiffness. Thus, small-scale models of microconcrete with cracks could seriously underestimate the stiffness of full-scale models with cracks.

4. Normal stresses were very low in these small-scale models (generally less than 20 psi, if I recall correctly). Normal stresses should help to hold cracks closed and, together with aggregate interlock, should help to lessen the reduction of stiffness at low shear stress levels.

Because of these open issues, the TRG (including myself) recommended testing of a larger-scale structure. This structure was to be of normal concrete with actual rebar. Wall thickness was to be at least 4", and the uncracked natural frequency was to be less than 30 Hz. Substantial top mass was to be added by steel plates to lower the natural frequency and to provide a more realistic and higher normal stress of about 40 psi, which unfortunately is still low compared to most prototype structures. To meet these requirements, TRG-3 was constructed and tested dynamically by simulated seismic shaking on a shake table. Stiffnesses back-calculated from the natural frequency of this test structure at low shaking levels (less than 50 psi average shear stress) also

showed about a factor of 4 reduction from the computed uncracked stiffness. Thus, this dynamic testing of TRG-3 seemed to support the tentative conclusions drawn from the small-scale testing.

Unfortunately, TRG-3 seems to contain most of the same open issues as listed previously for the smaller-scale tests, but to a lesser extent. These issues cloud the results of TRG-3:

1. No direct measurements of structure relative deformation were made. Therefore, estimates of stiffness had to be back-calculated from natural frequencies. These natural frequencies could be heavily influenced by base rotation; and such rotations, if present, would cloud the estimates of stiffness. From the limited data I have seen, it still seems probable to me that substantial base rotation effects did occur. For example, the results shown in Figures 16 and 17 of the FY 1986 Rough Draft Final Report for TRG-3 subjected to a haver-sine pulse are completely consistent with this assumption of sub-stantial base rotation effects. The base slab and the top of the structure are both oscillating at about 8 Hz, as seen in Figure 16. This result, together with the transfer function of Figure 17, indi-cates to me a predominant base rotational mode at 8 Hz rotating about a point located below the base slab.

2. The walls are still thin and the normal stresses are still somewhat low relative to a prototype full-scale structure. These two condi-tions might result in more cracking and might result in greater reduction in stiffness due to cracking than would occur in a full-scale structure.

3. TRG-3 was built at Los Alamos and shipped to the shake table at CERL in Illinois. This handling and transportation could have resulted in more cracking of TRG-3 prior to the low-level shake-table test than would exist in an aged prototype structure. However, visible cracking did not appear to be present prior to testing.

Because of concern over issues 1 and 3, two additional tests (TRG-4 and TRG-5) were performed. Both structures were constructed of normal concrete with actual rebar. TRG-4 had 6" thick walls, and TRG-5 had 4" thick walls. Both models were subjected to cyclic static tests, and both models were handled very carefully prior to being tested to low shear stress levels so that they represented "virgin" uncracked concrete models to the greatest extent practi-cal prior to testing. An internal relative deformation instrumentation system was used so that direct measurements of relative deformations could be taken. This enabled shear and bending deformations to be separately estimated. Also any deformations due to base rotation or base flexibility effects were not included in these measurements, so that base effects could not "cloud" the

data. Because of the impracticality of adding additional top weight, normal stresses were still low (about 20 psi for TRG-4 and 40 psi for TRG-5, I believe).

Low-level cyclic static tests on these "virgin" uncracked concrete models produced relative deformations in "essentially exact" agreement with those predicted by uncracked concrete stiffness models. Thus, these two tests produced results contradictory to those obtained from all previous tests within this program. The results were exactly as I would expect for "virgin" uncracked concrete models. As the cyclic average shear stress levels were increased to beyond the cracking stress level, stiffness of these models did degrade as one would expect. Prior to reaching their ultimate cyclic load-carrying capacity (at roughly expected levels), the secant stiffness of these models appears to have degraded to less than 10% of their uncracked stiffness. I can fully support all test results which I have seen for these well-instrumented, carefully handled TRG-4 and TRG-5 "virgin" uncracked concrete models. These results will be very useful in defining stiffness degradation of uncracked concrete structures when subjected to high average shear stress cyclic loading from seismic input. Although these tests were cyclic static tests, the measured hysteretic behavior with stiffness degradation can be used analytically to study the effect in floor spectra from increased seismic shaking levels.

However, the results of TRG-4 and TRG-5 tests cannot be used to conclusively demonstrate that uncracked stiffness estimates can be used for estimating the stiffness of actual structures at low cyclic shaking stress levels less than about 100 psi. These test models were so carefully handled that they are not likely to be representative of actual structures after 20 or more years of life. Actual concrete shear walls crack due to shrinkage, aging, thermal loadings, vibration loadings, and soil settlement over time. Such cracking will undoubtedly be greater than that contained in TRG-4 and TRG-5 prior to testing.

Observations

This test program has not provided conclusive results concerning the stiffness of low-rise concrete shear wall structures at lower OBE-type stress levels. A number of issues "cloud" all of the smaller-scale test results, as well as the results of TRG-3. Severe doubt can likely be cast on results of all of these tests which show a substantial reduction (about a factor of 4) in stiffness below the computed uncracked stiffness at low shear stress levels, because of these "clouding" issues by those who do not believe these results. The results of TRG-4 and TRG-5, which were better-instrumented and better-handled, can be used to support these doubts. However, real structures are likely to be cracked to some extent, and the use of uncracked stiffness estimates may

not be appropriate for such structures, even though uncracked stiffness estimates worked well for the "virgin" uncracked TRG-4 and TRG-5 models. In my opinion, the results of this test program have simply added "fuel" to the controversy rather than resolving the issue. This conclusion is not meant as a criticism of the test program; I am not sure any model structure test program could resolve this controversy. Certainly this test program provided a substantial quantity of very interesting data.

In my opinion, the stiffness of low-rise concrete shear wall structures at low shear stress levels is highly uncertain at this time. I suspect it is unlikely that real structures with substantial normal stress (40 to 100 psi) on the shear walls have stiffnesses at low shear stress levels (50 to 100 psi) reduced by as much as a factor of 4 below those estimated from uncracked models. On the other hand, I suspect that a substantial number of such structures, after time, have stiffnesses well below their uncracked stiffness, even at low shear stress levels. Because of this strong possibility, I believe we should be studying the consequences of such stiffness reduction for equipment mounted in structures which are currently estimated to have stiffnesses estimated to exceed about 9 Hz using uncracked stiffness models. Design earthquakes tend to have their power concentrated at frequencies below about 7 Hz, so that structure models with frequencies in excess of about 9 Hz tend to escape this power; thus the input to equipment is likely to be increased if the actual stiffness is substantially less than that used in the structure analysis.

This test program has done an excellent job of demonstrating the stiffness degradation that occurs at higher shear stress levels between the cracking stress and the ultimate strength. All of the tests (both the small models and TRG-4 and TRG-5) demonstrate this reduction, and it seems to be reasonably consistent from test to test. I believe that each of the tests showed at least a factor of 10 reduction in stiffness below the uncracked stiffness before the ultimate cyclic capacity was reached. Particularly, TRG-4 and TRG-5 provide excellent data on the cyclic hysteretic behavior with stiffness degradation of these low-rise shear walls because of the excellent instrumentation available on these tests.

This test program has also provided excellent data on how floor spectra shift as shaking levels are increased. This shift in floor spectra is observed in the dynamic small-scale tests and can be studied analytically from the TRG-4 and TRG-5 hysteretic data. This test data is also available for studying the necessary characteristics of simplified mathematical models used to estimate floor spectra. For instance, preliminary investigations have indicated that even with substantial frequency shift, pseudo-linear-elastic models with reduced frequency and damping in the 7% to 10% range and sometimes higher can be used to estimate the measured floor spectra at high shaking levels.

Thus, although this test program has not conclusively resolved the question of low-rise concrete shear wall stiffness at low shear stress levels, it has conclusively demonstrated the further reduction of these stiffnesses to values much below the uncracked stiffness as shear stress levels are increased to values approaching the shear wall capacity. This test program has provided the necessary data to study the effects of such stiffness shifts on floor spectra.

Recommendations for Additional Testing

I believe it would be very useful to conduct one larger-scale dynamic shake table test on a carefully handled, well-instrumented "virgin" uncracked model made of normal concrete and actual rebar. To date we have no such test in this program. This model could look very much like TRG-3. However, it should be built at the shake table site and carefully handled so as to avoid the handling and transportation questions associated with TRG-3. Normal stresses should be at least 40 psi. This model should have instrumentation capable of reliably measuring internal relative deformations during dynamic shaking simi-lar to the measurements taken on TRG-4 and TRG-5. This instrumentation is absolutely necessary so as to directly obtain dynamic stiffness information "unclouded" by base rotation or base flexibility effects. It is not clear to me whether such measurements can be reliably made during a dynamic shake table test. Unless such measurements can be reliably obtained, I see very little purpose to this test.

I expect that a carefully handled, well-instrumented "virgin" uncracked TRG-3 model subjected to a dynamic shake table test will produce stiffness results in agreement with TRG-4 and TRG-5; in other words, that an uncracked stiffness model adequately models its stiffness at low stress levels. If this proves to be the case, then this test can produce data for several comparison studies.

    1.   Is the degradation of stiffness during the dynamic test at higher shaking levels, similar to that observed in the cyclic static tests of TRG-4 and TRG-5?

    2.   Can floor spectra measured at the top of this structure during dynamic tests be adequately estimated using the hysteretic and degrading stiffness properties observed during the cyclic static tests?

These studies are very important to confirm our ability to predict dynamic behavior from mathematic models based on cyclic static test data.

If the unexpected occurs and the carefully handled, well-instrumented "virgin" uncracked TRG-3 model during low-level dynamic tests exhibits substantially

less than the uncracked stiffness, this result would indicate a serious dif-
ference between the dynamic and the cyclic static behavior of TRG-4 and TRG-5.
This result would provide more credence to the small-scale test results and
the current TRG-3 results. Either way, this test should provide important
additional data, so long as the model is a large-scale "virgin" uncracked
model and internal relative deformations are reliably measured.

However, this test will not resolve the question of the stiffness of low-rise
concrete shear wall structures under OBE and SSE shaking levels. After time,
real structures are likely to be cracked. This new model should be a "virgin"
uncracked model, and in this regard it is likely to underestimate the
stiffness reduction below the uncracked stiffness at low shaking levels.
Furthermore, the model wall is still thin (4" or 6") relative to actual walls,
and thus might overestimate the stiffness reduction due to cracking for actual
thicker walls. Lastly, the normal stress on the model wall will still be low
(probably cannot get much above 40 psi) because of the difficulty of adding
sufficient top weight or vertical preload. Thus, the model wall might over-
estimate the stiffness reduction of cracked actual walls because of the lesser
normal stress. Therefore, no matter what this test produces, I do not expect
it to resolve the question of the stiffness of low-rise concrete shear wall
structures at low average shear stress levels.

The most convincing (but very costly) way to resolve the question of the
stiffness of actual low-rise concrete shear wall structures is to test several
structures. Ideally, such tests should use a very large eccentric mass oscil-
latory, such as that used on the HDR structure in Germany. Furthermore,
internal relative deformations need to be measured to avoid "clouding" the
results with base flexibility effects. Short of these tests, I am not sure
the issue of stiffness of actual structures will be resolved.

Some people have suggested using the large-scale reactor building test struc-
ture built by Niagara Mohawk and EPRI at Nine-Mile Point. However, being a
model, this structure will not have adequate normal stress to be representa-
tive of actual walls, and there will be base rotation effects, again neces-
sitating the measurement of internal relative deformations during dynamic
testing. I think tests of this structure would be useful, but not conclusive.

Summary Responses to Specific Questions

Although I believe that I have provided my response to each of your questions
in the preceding write-up, to be sure I am responsive I will summarize my
response to each question:

1. Are the tests in this program valid for addressing the program objectives?

    These tests are valid for addressing the question of stiffness degrada-
    tion with increasing levels of shaking input and the influence of this
    degradation on floor spectra and equipment input. The test program has
    not been particularly valid or conclusive for addressing the stiffness
    of low-rise concrete shear wall structures at low shear stress levels
    (less than about 100 psi). The important issues are: How cracked are
    actual structures; and how much do these cracks reduce the stiffness of
    these structures? The small model test results probably overemphasize
    these issues and TRG-4 and TRG-5 being "virgin" uncracked models should
    underestimate the influence of cracking.

2. In light of the program objectives, are the model test data obtained
    applicable to nuclear power plant structures?

    Open issues discussed in the Background Comments and Observations
    sections "cloud" each of the sets of test data. Therefore, none of the
    test data is totally applicable to nuclear power plant structures.
    However, the stiffness degradation below the uncracked stiffness of
    nuclear power plant structures is likely to be bounded between the
    small scale model and TRG-3 results on one side and TRG-4 and TRG-5
    results on the other. This comment is expanded upon in my Observations
    section.

3. Have the technical issues of scaling, instrumentation, and model
    fabrication effects been resolved?

    The technical issue of scaling has been resolved. However, the open
    issues of base flexibility and rotation effects, and the influence of
    wall thickness, normal stress, and aggregate interlock on cracking and
    stiffness reduction has not been resolved. Except for the above, model
    fabrication effects have been resolved, in my opinion. TRG-4 and TRG-5
    had adequate instrumentation. The other tests either did not have
    adequate instrumentation or else the data has not been adequately
    processed to fully resolve the issue of base rotation and flexibility
    effects, at least in my mind.

4. Should there be another "carefully handled" dynamic test to address the
    possible "dynamic effects" issue? If so, what configuration?

    Yes. My recommendations for this test are contained in the
    Recommendations for Additional Testing section.
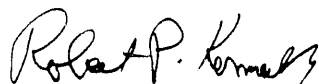
5. Have we obtained enough data and have we tested the correct configurations
    to meet the program objectives?

    With one more dynamic test as discussed in my Recommendations for
    Additional Testing section, I believe we have obtained the data we are
    going to obtain from model testing, and have tested correct and suffi-
    cient configurations. I cannot recommend any more such tests beyond
    one more dynamic test.

6. Would the variability in stiffness observed in the models be observed in
    real nuclear plant structures at comparable load levels?

    I doubt that the variability in stiffness relative to the uncracked
    stiffness in real nuclear power plants will be as great as that
    observed in the full range of these model tests, including TRG-4 and
    TRG-5. However, I expect the variability in real nuclear plant stiff-
    nesses will be substantial, and stiffnesses significantly less than the
    uncracked stiffness should be considered possible. My comments on this
    question are expanded upon in the Observations section.

Very truly yours,

Robert P. Kennedy

RPK:lms

TENNESSEE VALLEY AUTHORITY

KNOXVILLE, TENNESSEE 37902

400 West Summit Hill Drive, W9 D191

Los Alamos National Laboratory
Los Alamos, New Mexico 87545

Attention: Mr. Joel G. Bennett

Gentlemen:

REVIEW OF OBJECTIVES AND PROGRESS OF THE SEISMIC CATEGORY I STRUCTURES PROGRAM

Reference: Your letter to me dated November 16, 1987, MEE-13:87:567

I have reviewed the materials cited in the referenced letter with the purpose
of answering the six questions that were asked of the Technical Review Group.
I have given below my "bottom line" answers to the six questions without, for
the most part, the basis or rationale for the answers.

1. Yes. The progression of the models used (one-story shear walls, two-story
    shear walls, box structure and TGR structure), tests performed (static
    tests, cyclic tests, dynamic tests) and analysis is a logical and
    purposeful approach.

2. Yes, with this qualification--the model tests clearly show that the
    stiffness of reinforced concrete structures are degraded by cyclic
    loadings, and consequently, the stiffness of nuclear power plant
    structures will be degraded under repeated cycles of strong motion
    earthquake. The model tests probably do not predict accurately the
    magnitude of the loss of stiffness. Furthermore, it is not clear that the
    reduction of the precracked stiffness shown by the model tests, based on
    strength of materials (SOM) analysis, are true indications.

3. No, as it relates to scaling of the responses to full size nuclear power
    plant structures.

4. I do not have a recommendation at this time. I would want to study the
    previous tests results some more.

5. Yes and no. Simply stated that tests performed answer a basic question
    that the response of nuclear power plant structures when subjected to
    several cycles of strong earthquake ground motion will not be as predicted
    by linear, SOM analyses based on gross section properties.

    The test available to date, in my opinion, is not sufficient to answer,
    quantitively, what reduction in stiffness should be considered in design
    or evaluation of structures.

Mr. Joel G. Bennett
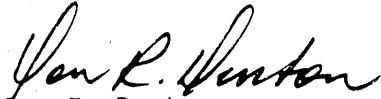
The response of structures to low (OBE level) earthquakes falls into a "grey zone" between mostly the precracked state and where opening of the microcracks have clearly reduced the structural stiffness.

6. Yes, in my opinion, because of the variables that exist in construction.

I apologize for being late in responding. I will be glad to discuss further the basis for my response.

Very truly yours,

TENNESSEE VALLEY AUTHORITY

Don R. Denton
Senior Civil Engineer

NEWMARK LABORATORY

15 January 1988

TO : Dr. Joel G. Bennett

FROM : Mete A. Sozen

RE: Objectives and Progress of the "Seismic Category I Structures Program"

It would have been a time-saver for both of us for me to be able to answer your questions with curt yeas and nays. But your six questions in the context of the six objectives listed in the draft FY 1986 report cover a lot of fertile ground. Before I attempt brief answers I should make an attempt to expose the roots of my prejudgments.

I should also record my appreciation of the effort you and your co-workers have put into the documents you sent me. The documents show both the breadth and depth of the project clearly. I think they are very well done and deserve detailed if not always positive comment. I shall do that informally and in bits and pieces after I finish this note and the one on aggregate. I wish you could locate me on the computer network (my address is sozen@cevax.ce.uiuc.edu) because that medium does encourage quick written exchange.

To start, let me quote from the engineering market place. It is stated in the Commentary to the ACI Building Code 318-83 (Section A.2.1, p.318R-134) that

"As a properly detailed reinforced concrete structure responds to strong ground motion, its effective stiffness decreases and its capability to dissipate energy increases. These developments tend to reduce the response acceleration or lateral inertia forces with respect to those forces calculated for a linearly elastic model of the uncracked and lightly damped structure."

That the effective stiffness of a reinforced concrete structure is likely to decrease from its initial value at the beginning of strong ground motion is a generally held belief from observation. There is no contrary evidence. The reasons for the reduction in stiffness are explicit. Concrete cracks. Reinforcing bars yield and slip. Surfaces bounding cracks slide with respect to one another.

Initial stiffness of the reinforced concrete structure is another question. For building structures, initial stiffness is often polluted by effects of base fixity and nonstructural components. The stiffness of the structural system on rigid base could be estimated closely by calculations based on uncracked sections.

Within my experience, I expect the effective stiffness of structural building models in very-low amplitude vibration to be less than three quarters of the calculated stiffness (based on gross section) about half the time. For simple one-element models, the ratio of measured initial to calculated stifness based on gross section is likely to be closer unless, of course, the model was mishandled.

The initial stiffness of an actual building (stiffness of the elements above the foundation) could also be close to that based on uncracked section. But we cannot assert that to be correct in every case. Volume-change cracking (caused by effects such as temperature, shrinkage, creep, and corrosion of reinforcement) is likely to reduce the effective stiffness even if the structure has not been loaded or deformed by external effects before the occurrence of the strong ground motion.

If energy transmission through the structure at different frequencies is a critical design factor, it is proper to estimate the "floor spectra" for a credible range of effective stiffnesses. In my opinion, the "Seismic Category I Structures program" has established the magnitude of the stiffness-change problem for very stiff reinforced concrete structures (for which the available information in the dynamic domain is, at best, meager). It seems now to be time for projecting these results to the target structures and assess the possible ranges of effects on design calculations. If design calculations indicate problems, then we could go back and refine the input (coming out of this investigation) and/or re-evaluate the design calculations. As an engineer, I am resigned to making design decisions without knowing everything. I think the time has come to investigate systematically the impact of the stiffness-reduction factor on design decisions. It would be very useful to have an estimate of whether equipment design will be affected by the acknowledgment of stiffness change and , if so, what (in terms of dollars) its impact is likely to be.

I indulge in the obvious only to expose my low-brow approach to the problem. I am willing to turn to practice from the laboratory without having methods to give me one hundred percent of the truth. Your experiments have confirmed that stiff box-like structures soften and that their initial stiffness may not be exactly that which is indicated by calculations based on observations on undisturbed samples. The same experiments also show that the equivalent viscous damping factor may be in the range from 0.05 to 0.1. I concede that available information does not enable us to specify the exact value of the initial stiffness for every structure in the field, but we do have a handle on the credible range. It is time to probe the effects on design.

(1) Are the tests in this program valid for addressing the program objectives?

Yes. The tests do provide information on changes in stiffness of stiff reinforced concrete structures and their ability to dissipate energy at various levels of applied stress. Consequently, they provide useful information related to "floor response spectra."

A simple point needs reinforcement here in relation to validation of computer programs (objective 3). The most optimistic result to expect from such an enterprise is that the test data will not invalidate a computer program in the range of the test parameters. The likely result is that the experimental results will help calibrate the numerical model over a given range of the parameters. To refer to "validation of computer programs" sets up unfulfillable expectations.

(2) In light of the program objectives, are the model test data obtained applicable to nuclear power plant structures?

Yes.

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(3) Have the technical issues of scaling, instrumentation and model fabrication issues been resolved?

With respect to overall impact of the results, yes. Details remain to be resolved, but it would be inefficient to focus on detail when there are some important implications to be studied.

(4) Should there be another "carefully handled" dynamic test to address the possible "dynamic effects" issue? If so, what configuration?

It would be preferable to decide on the use of resources for experimental analysis after the design impact studies have been carried out and evaluated.

(5) Have we obtained enough data and have we tested the correct configurations to meet the program objectives?

No. Sufficient data have been obtained to confirm the need for re-evaluating state-of-the-art floor response calculations and their impact on design of equipment.

(6) Would the variability in stiffness observed in the models be observed in real nuclear plant structures at comparable load levels?

Yes, if the structure in question is reinforced concrete.

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December 17, 1987

Dr. Joel Bennett
Advanced Engineering Technology
Los Alamos National Laboratory
Los Alamos NM 87545

Dear Joel:

My apologies for not responding to MEE-13: 87:567 by 4 December 1987 but
apparently your letter to me got lost in the mail. I was at the NRC research
Offices in Rocksville on 14 December 1987 and ran into Roger Kenneally who
asked me about my response to your letter. He gave me the package and asked
that I respond to your six questions ASAP.

Question #1- Are the tests in this program valid for addressing program
              objectives?

Yes, unless you really wish to evaluate the difference in stiffness between
cracked and uncracked shear walls which I do not recommend. In the limit, in
response to a damaging strong motion earthquake, it should be assumed that
concrete shear walls of the nuclear plant building structures will be
cracked. The literature on behavior of heavy industrial equipment and
building structures in damaging strong motion earthquake supports the belief
that building structures are more susceptible to earthquake damage than the
equipment they contain. This suggests that nuclear power plant structures
would at least be cracked before the safety related equipment contained
therein would be susceptible to damage.

Question #2   Are the model test data obtained applicable to nuclear power
              plant structures?

A qualified yes. In my opinion the "stiff" shear wall data is from uncracked
specimens. The less stiff data would be applicable to "cracked" specimens. I
also believe the data developed for the uncracked specimen would be applicable
to earthquakes well below the damage threshold for safety related equipment in
the plant hence of little practical use. The more limited "cracked" data is
applicable to seismic evaluation of shear walls and equipment at response
levels nearer those levels which could course damage to the structure itself
and the safety related equipment contained therein.

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Question #3   Have the technical issues of scaling, instrumentation and model
fabrication effects been resolved?

Except for the question of whether or not the seismic tests models were
cracked prior to testing, I believe scaling, instrument and model fabrication
effects have been resolved. However, this is not my area of special
expertise. I would defer to the opinion of others such as Meta Sozen on this
question.

Question #4   Should there be another "carefully handled" dynamic test to
address the possible "dynamic effects" issue?

No. I believe the money would be better spent in developing a consenses
method of analytically modeling real nuclear plant shear wall structures which
probably should consider the concrete cracked.

Question #5   Have we obtained enough test data?

In my opinion, yes.

Question #6   Would the variability in stiffness observed in the models be
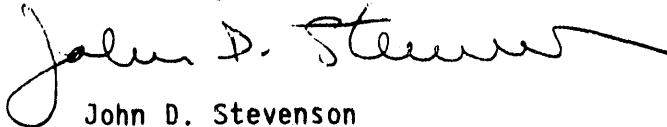observed in real nuclear plant structures?

Even more variability in stiffness would be observed in real nuclear plant
structures. This is due primarily to soil-structure interaction effects which
includes both gaps between the structure and the support media as well as the
non-linear behavior of the support media as a function of media strain
levels. Also effecting real nuclear plant structures, would be cracking due
to differential settlement, shrinkage and differential temperature effects. I
believe it is imperative that we educate structure engineers to understand
that linear elastic dynamic analysis of structure at best is an indice of
seismic loads and it does not with any degree of accuracy predict the seismic
stresses in real structure or equipment. We broaden our design response
spectra which has the effect of adding significantly more energy than any one
earthquake's time history would generate. This conservatism in my opinion
more than compensates for any frequency shift that may exist as a result of

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actual and variable versus computed constant structural stiffness. This is true also for design of equipment in the building as well as the building itself.

I hope this letter reaches you in time to be of some use. Please advise if you require any clarification of this letter.

Sincerely,

John D. Stevenson
President

JDS:mm

cc: R. Kenneally-NRC

Ref. (1)   Draft Report "Development of Criterion for Determining OBE Exceedance" in preparation for EPRI

U.S. NUCLEAR REGULATORY COMMISSION

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Washington, DC 20555

10. SUPPLEMENTARY NOTES *Consultant at Los Alamos. Mechanical Engineering Department,
University of New Mexico, Albuquerque, NM 87131

11. ABSTRACT *(200 words or less)*

The accomplishments of the Seismic Category I Structures
Program for FY 1987 are summarized. These accomplishments
include the quasi-static load cycle testing of large shear
wall elements, an extensive analysis of previous data to
determine if equivalent linear analytical models can predict
the response of damaged shear wall structures, and code
committee activities. In addition, previous testing and
results that led to the FY 1987 program plan are discussed and
all previous data relating to shear wall stiffness are
summarized. Because separate reports have already summarized
the experimental and analytical work in FY 1987, this report
will briefly highlight this work and the appropriate reports
will be referenced for a more detailed discussion.

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