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# The Sloan Digital Sky Survey Reverberation Mapping Project: Initial CIV Lag Results from Four Years of Data

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C. J. Grier<sup>1,2,3</sup>, Yue Shen<sup>4,5,28</sup>, Keith Horne<sup>6</sup>, W. N. Brandt<sup>1,2,7</sup>, J. R. Trump<sup>8</sup>, P. B. Hall<sup>9</sup>, K. Kinemuchi<sup>10</sup>, David Starkey<sup>4,6</sup>, D. P. Schneider<sup>1,2</sup>, Luis C. Ho<sup>11,12</sup>, Y. Homayouni<sup>8</sup>, Jennifer I-Hsiu Li<sup>4</sup>, Ian D. McGreer<sup>3</sup>, B. M. Peterson<sup>13,14,15</sup>, Dmitry Bizyaev<sup>10,16</sup>, Yuguang Chen<sup>17</sup>, K. S. Dawson<sup>18</sup>, Sarah Eftekharzadeh<sup>18</sup>, Yucheng Guo<sup>12</sup>, Siyao Jia<sup>19</sup>, Linhua Jiang<sup>11</sup>, Jean-Paul Kneib<sup>20,21</sup>, Feng Li<sup>22</sup>, Zefeng Li<sup>12</sup>, Jundan Nie<sup>23</sup>, Audrey Oravetz<sup>10</sup>, Daniel Oravetz<sup>10</sup>, Kaike Pan<sup>10</sup>, Patrick Petitjean<sup>24</sup>, Kara A. Ponder<sup>25</sup>, Jesse Rogerson<sup>9,26</sup>, M. Vivek<sup>1,2</sup>, Tianmeng Zhang<sup>23,27</sup>, and
                                                                                                                 Hu Zou<sup>23</sup> (
      <sup>1</sup> Department of Astronomy and Astrophysics, Eberly College of Science, The Pennsylvania State University, 525 Davey Laboratory, University Park, PA
                                                                                                                    16802, USA
                                        <sup>2</sup> Institute for Gravitation & the Cosmos, The Pennsylvania State University, University Park, PA 16802, USA
                                               Steward Observatory, The University of Arizona, 933 North Cherry Avenue, Tucson, AZ 85721, USA
                                                    Department of Astronomy, University of Illinois at Urbana-Champaign, Urbana, IL 61801, USA
                                <sup>5</sup> National Center for Supercomputing Applications, University of Illinois at Urbana-Champaign, Urbana, IL 61801, USA
                                                                SUPA Physics and Astronomy, University of St. Andrews, Fife, KY16 9SS, UK
                                                    <sup>7</sup> Department of Physics, The Pennsylvania State University, University Park, PA 16802, USA
                                          <sup>8</sup> Department of Physics, University of Connecticut, 2152 Hillside Road, Unit 3046, Storrs, CT 06269, USA

    Department of Physics and Astronomy, York University, Toronto, ON M3J 1P3, Canada
    Apache Point Observatory and New Mexico State University, P.O. Box 59, sunspot, NM 88349-0059, USA

                                     Kavli Institute for Astronomy and Astrophysics, Peking University, Beijing 100871, People's Republic of China

    Department of Astronomy, School of Physics, Peking University, Beijing 100871, People's Republic of China
    Department of Astronomy, The Ohio State University, 140 W 18th Avenue, Columbus, OH 43210, USA

                  Center for Cosmology and AstroParticle Physics, The Ohio State University, 191 West Woodruff Avenue, Columbus, OH 43210, USA
                                                           Space Telescope Science Institute, 3700 San Martin Drive, Baltimore, MD 21218, USA <sup>16</sup> Sternberg Astronomical Institute, Moscow State University, Moscow, Russia
                                             <sup>17</sup> California Institute of Technology, 1200 E California Blvd., MC 249-17, Pasadena, CA 91125, USA
                                       Department of Physics and Astronomy, University of Utah, 115 S. 1400 E., Salt Lake City, UT 84112, USA
                                                                  Department of Astronomy, University of California, Berkeley, CA 94720, USA
   <sup>20</sup> Institute of Physics, Laboratory of Astrophysics, Ecole Polytechnique Fédérale de Lausanne (EPFL), Observatoire de Sauverny, 1290 Versoix, Switzerland
    21 Aix Marseille Université, CNRS, LAM (Laboratoire d'Astrophysique de Marseille) UMR 7326, F-13388, Marseille, France

22 School of Mathematics and Physics, Changzhou University, Changzhou 213164, People's Republic of China

23 Key Laboratory of Optical Astronomy, National Astronomical Observatories, Chinese Academy of Sciences, Beijing 100012, People's Republic of China

24 Institut d'Astrophysique de Paris, Sorbonne Université and CNRS, 98bis Boulevard Arago, F-75014, Paris, France
                          25 Berkeley Center for Cosmological Physics, University of California Berkeley, 341 Campbell Hall, Berkeley, CA 94720, USA

26 Canada Aviation and Space Museum, 11 Aviation Parkway, Ottawa, ON, K1K 4Y5, Canada
                                  <sup>27</sup> School of Astronomy and Space Science, University of Chinese Academy of Sciences, People's Republic of China
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## Abstract

We present reverberation-mapping (RM) lags and black hole mass measurements using the C IV  $\lambda$ 1549 broad emission line from a sample of 348 quasars monitored as a part of the Sloan Digital Sky Survey RM Project. Our data span four years of spectroscopic and photometric monitoring for a total baseline of 1300 days, allowing us to measure lags up to  $\sim$ 750 days in the observed frame (this corresponds to a rest-frame lag of  $\sim$ 300 days in a quasar at z=1.5 and  $\sim$ 190 days at z=3). We report significant time delays between the continuum and the C IV  $\lambda$ 1549 emission line in 48 quasars, with an estimated false-positive detection rate of 10%. Our analysis of marginal lag measurements indicates that there are on the order of  $\sim$ 100 additional lags that should be recoverable by adding more years of data from the program. We use our measurements to calculate black hole masses and fit an updated C IV radius-luminosity relationship. Our results significantly increase the sample of quasars with C IV RM results, with the quasars spanning two orders of magnitude in luminosity toward the high-luminosity end of the C IV radius-luminosity relation. In addition, these quasars are located at some of the highest redshifts ( $z\approx1.4-2.8$ ) of quasars with black hole masses measured with RM. This work constitutes the first large sample of C IV RM measurements in more than a dozen quasars, demonstrating the utility of multiobject RM campaigns.

*Unified Astronomy Thesaurus concepts:* Reverberation mapping (2019); Quasars (1319); Active galactic nuclei (16); Supermassive black holes (1663)

Supporting material: figure sets, machine-readable tables

#### 1. Introduction

Supermassive black holes (SMBHs) are nearly ubiquitous in massive galaxies across the universe, and their masses have been

shown to be correlated with a variety of properties of the galaxies in which they reside (e.g., Kormendy & Richstone 1995; Magorrian et al. 1998; Ferrarese & Merritt 2000; Gebhardt et al. 2000; Gültekin et al. 2009). As a consequence, theories and simulations regarding the evolution of galaxies must include SMBHs; explaining how SMBHs grew to their observed masses

<sup>&</sup>lt;sup>28</sup> Alfred P. Sloan Research Fellow.

and how they are connected to their host galaxies is a critical component of galaxy evolution models. Accurate measurements of SMBH masses are therefore of paramount importance to successfully explaining the connection between galaxies and their SMBHs across the observable universe.

In nearby galaxies, black hole mass  $(M_{\rm BH})$  measurements can be obtained from observations of stellar and gas dynamics near the center of the galaxy (e.g., McConnell & Ma 2013). However, this approach is currently infeasible for distant galaxies; to determine  $M_{\rm BH}$  in galaxies beyond the local universe, we use active galactic nucleis (AGNs). Assuming that the broad emission lines observed in Type 1 AGNs are emitted by gas with motion that is dominated by the gravitational potential of the central SMBH, one can use this gas to obtain  $M_{\rm BH}$  measurements. However, as the broad lineemitting regions (BLR) in most AGNs are too small to directly resolve with current technology (see Gravity Collaboration et al. (2018) for the only exception thus far), there are limited opportunities to learn about the size and structure of the BLR. Reverberation mapping (RM) is the primary technique employed for this (the other being gravitational microlensing; e.g., Morgan et al. 2010 and Mosquera et al. 2013).

RM uses the variability of AGNs to obtain BLR information: variations in the continuum flux (generally assumed to be emitted close to the SMBH) are echoed by gas in the BLR, with the signal from the BLR delayed by the light-travel time between the continuum-emitting source and the BLR gas (e.g., Blandford & McKee 1982; Peterson et al. 2004). Measuring this time delay determines the distance between these two regions, which yields a characteristic radius for the BLR,  $R_{\rm BLR}$ . This measurement can be combined with a characterization of the virial velocity of the gas,  $\Delta V$ , which is assumed to be related to the width of the emission line, to yield a black hole mass:

$$M_{\rm BH} = \frac{fR_{\rm BLR} \,\Delta V^2}{G},\tag{1}$$

where f is a dimensionless factor that accounts for the geometry, orientation, and kinematics of the BLR.

In theory, RM measurements can be made using any suitably strong broad emission lines arising from gas that reverberates in response to the continuum and is in virial motion around the SMBH. Thus far, most ground-based efforts have been focused on the H $\beta$  emission line, which falls in the optical range in local AGNs, and additional strong optical lines such as H $\alpha$ , H $\gamma$ , and He II $\lambda$ 4686. Attention has also been given to the C IV $\lambda$ 1549 and Mg II $\lambda$ 2798 emission lines, which are often quite strong and lie within the optical range of many ground-based spectrographs for higher-redshift quasars. To date, on the order of 100 AGNs have RM measurements (e.g., Kaspi et al. 2000, 2005; Peterson et al. 2004; Bentz et al. 2009, 2010; Denney et al. 2010; Grier et al. 2012; Du et al. 2014, 2016a, 2016b; Barth et al. 2015; Hu et al. 2015; Grier et al. 2017; Lira et al. 2018).

RM measurements of local AGNs have established a tight correlation between  $R_{\rm BLR}$  and the luminosity of the AGN (e.g., Kaspi et al. 2000, 2005; Bentz et al. 2013), with  $R \propto \sqrt{L}$ , consistent with basic photoionization expectations. This relation allows the estimation of  $R_{\rm BLR}$  from a single spectrum, enabling  $M_{\rm BH}$  estimates (hereafter referred to as single-epoch, or SE,

masses) for a large number of quasars for which RM campaigns are impractical (e.g., Shen et al. 2011). The current H $\beta$   $R_{\rm BLR}-L$  relationship is calibrated fairly well (Bentz et al. 2013), although there is a dearth of measurements at the high-luminosity end of the relation. The sample included in the most recent calibration of this relation is composed of ~40 nearby (z < 0.3), low-luminosity AGNs that may not be representative of the general AGN/quasar population. Recent studies by Du et al. (2016a) and Grier et al. (2017) find many objects below the measured relation, although the origin of this phenomenon is still currently under investigation and selection effects are likely relevant in some cases (e.g., Li et al. 2019; Fonseca Alvarez et al. 2019).

Many studies have focused on the C IV $\lambda$ 1549 emission line because it is one of the few strong lines in the ultraviolet (UV), making  $M_{\rm BH}$  measurements in higher-redshift quasars feasible from the ground. The status of the CIV emission line with regards to measuring  $M_{\rm BH}$  is complex: C IV frequently exhibits a blueshifted component reminiscent of outflows, and has been found to have significant nonreverberating components (e.g., Gaskell 1982; Korista et al. 1995; Richards et al. 2011; Denney 2012), though it has been suggested that many of the reported blueshifts are affected by incorrect redshift measurements (Denney et al. 2016a). In addition, these properties depend on luminosity—i.e., the blueshift is observed primarily in higher-luminosity quasars—and recent velocity-resolved RM results of the local Seyfert galaxy NGC 5548 (De Rosa et al. 2015; Horne et al. 2019, in preparation) show signatures indicative of a Keplerian disk with gas in virial motion, rather than evidence for outflowing gas. Possibly as a consequence of the above issue, differences have been reported between the full width at half maximum (FWHM) of C IV and the FWHM of H $\beta$  (Baskin & Laor 2005; Netzer et al. 2007; Shang et al. 2007; Shen & Kelly 2012; Trakhtenbrot & Netzer 2012; Shen 2013), with C IV sometimes showing narrower widths than H $\beta$ . This has been interpreted as possible evidence against a simple radially stratified BLR that RM studies generally support (e.g., Peterson 1993; Korista et al. 1995). These issues have raised concerns over the suitability of CIV for SE  $M_{\rm BH}$  estimates—though some studies suggest that data quality is the major issue, rather than C IV itself (e.g., Vestergaard & Peterson 2006; Denney 2012). Several corrections have been proposed to address these various issues and allow CIV to continue be used as an SE estimator (e.g., Assef et al. 2011; Denney 2012; Runnoe et al. 2013; Brotherton et al. 2015; Coatman et al. 2017). With or without these corrections, C IV has continued to be used to estimate  $M_{\rm BH}$  in large numbers of sources (e.g., Shen et al. 2011).

Despite all of these potential issues, C IV can still be used for RM  $M_{\rm BH}$  measurements, as RM methods make use of the root-mean-square (rms) line profile, which includes only the part of the C IV line that does reverberate. However, RM measurements of the C IV emission line are difficult to obtain. First, measurements in local galaxies require the use of space telescopes, as rest-frame C IV lies in the UV and is not accessible from the ground. Second, in higher-redshift, more luminous quasars, the expected observed lags are on the order of years (due to cosmological time dilation), making them impossible to measure in a single observing season and requiring long-term, logistically difficult observing campaigns. It is for these reasons that C IV RM measurements are far more scarce than H $\beta$  RM measurements. Thus far, there have

been only  $\sim$ 15–18 C IV robust RM lag measurements that are used to calibrate the C IV  $R_{\rm BLR}-L$  relation (Peterson et al. 2004 and references therein; Peterson et al. 2005; Kaspi et al. 2007; Trevese et al. 2014; De Rosa et al. 2015; Lira et al. 2018; Hoormann et al. 2019), though there were some earlier reports of C IV lag detections of varying quality (e.g., Gaskell & Sparke 1986; Clavel et al. 1989; Koratkar & Gaskell 1989, 1991). The most recently measured  $R_{\rm BLR}-L$  relations for the C IV emission line (Lira et al. 2018; Hoormann et al. 2019) still contain relatively few measurements compared to the H $\beta$  relation, and there are large ranges of luminosities along that relation for which there are no published measurements.

We have embarked on a large-scale, multiobject RM campaign called the Sloan Digital Sky Survey RM Project (SDSS-RM; Shen et al. 2015a), one of the major goals of which is to measure C IV lags in a large sample of quasars over a range of luminosities and redshifts. SDSS-RM began in 2014 as an ancillary program within the SDSS-III Baryon Oscillation Spectroscopic Survey (BOSS; Eisenstein et al. 2011; Dawson et al. 2013), and has continued to acquire spectra thereafter as a part of the SDSS-IV eBOSS program (Dawson et al. 2016; Blanton et al. 2017). Spectra of 849 quasars are obtained each observing season between January and July with the SDSS 2.5 m telescope (Gunn et al. 2006), and accompanying photometric data are acquired with the 3.6 m Canada-France-Hawaii Telescope (CFHT) and the Steward Observatory 2.3 m Bok telescope. Observations will continue to be taken through 2020. The main goals of the program are to obtain RM measurements using the H $\beta$ , Mg II, and C IV emission lines for quasars over a wide range of redshifts; however, a wide variety of science topics can be (and have been) addressed with the rich data set provided by the SDSS-RM program, ranging from studies of quasar host galaxies, to broad absorption line (BAL) variability, to emission-line properties, to general quasar variability (e.g., Grier et al. 2015; Matsuoka et al. 2015; Shen et al. 2015b, 2016; Sun et al. 2015; Denney et al. 2016b; Yue et al. 2018; Hemler et al. 2019; Homayouni et al. 2019).

We here present C IV RM results from the SDSS-RM quasar sample using data taken during the first four years of the program (2014–2017). We present our quasar sample and the data used in our study in Section 2. In Section 3, we describe the methodology used for the various measurements. In Section 4, we discuss our results and their implications. We conclude in Section 5, with a summary of our main results. Throughout this article, we adopt a  $\Lambda$ CDM cosmology with  $\Omega_{\Lambda}=0.7$ ,  $\Omega_{M}=0.3$ , and h=0.7.

# 2. Data and Data Processing

# 2.1. The Quasar Sample

The parent sample of quasars consists of the 849 quasars monitored in the SDSS-RM field; details of this sample are provided by Shen et al. (2019b). We first restrict our sample to the 492 quasars with z > 1.3, i.e., quasars with observed-frame wavelength coverage of the C IV emission line in the BOSS spectra.

In many sources, however, the C IV emission line was not sufficiently variable to obtain RM measurements. Before performing our analysis, we thus first excluded sources whose C IV emission lines did not show significant variability over the span of our observations. To characterize the variability, we measured the C IV light curve variability signal-to-noise ratio (S/N) using the quantity S/N2, which is an output from the PrepSpec software (see Section 2.2 for a discussion of

PrepSpec). S/N2 is defined as  $\sqrt{\chi^2 - \text{DOF}}$ , where  $\chi^2$  is calculated against the average of the light curve flux (using the measurement uncertainties of the light curves  $\sigma_i$ ), and DOF is the degrees of freedom, which is equal to the number of points in the light curve -1. Larger values of S/N2 indicate that the null-hypothesis model of no variability is a poor description of the emission-line light curve, while smaller values indicate that the light curve is consistent with zero variability. We require that the S/N2 of the C IV emission line is greater than 20 for a quasar to be included in our sample (this number was chosen based on visual inspection of the PrepSpec fits, light curves, and rms residual line profiles). This criterion produced a final sample of 348 quasars, with redshifts ranging from 1.35 to 4.32. Basic information on these quasars is provided in Table 1, and Figure 1 displays the distributions of redshift, i-mag, and luminosity of the quasars in our final sample.

#### 2.2. Spectroscopic Data

We obtained the spectra used in this study during the first four years of observations for the SDSS-RM campaign (e.g., Shen et al. 2015a), which monitors 849 quasars with i < 21.7 at redshifts ranging from 0.1 to 4.5. The spectra were acquired with the BOSS spectrograph (Dawson et al. 2013; Smee et al. 2013), which covers a wavelength range of  $\sim 3560-10400$  Å. The spectrograph has a spectral resolution of  $R \sim 2000$  and the data are binned to 69 km s<sup>-1</sup> per pixel. We obtained a total of 68 epochs between 2014 January and 2017 July, with observations taken between January and July in each year only, leaving a gap of six months between observing seasons. The first year of SDSS-RM monitoring yielded 32 spectroscopic epochs and the additional three years of monitoring yielded 12 epochs each. Figure 2 displays the observing cadence for the observations.

The 2014 spectra were processed using the standard SDSS-III pipeline (version 5\_7\_1); data from the subsequent years were processed using the updated SDSS-IV eBOSS reduction pipeline (version 5\_10\_1). We then further processed all spectra using a custom flux-calibration scheme described by Shen et al. (2015a), which improves the spectrophotometric calibrations by using additional standard stars observed on the plate.

To further enhance the relative flux calibration of the data, we employed a custom procedure using software referred to as PrepSpec<sup>29</sup> (this code is described in detail by Shen et al. (2015a, 2016) and Horne et al. (2019, in preparation)). PrepSpec models the spectra using a variety of different components, and applies a time-dependent flux correction that is calculated by using the narrow emission lines (when present) as a calibrator. The correction assumes that there is no intrinsic variability in the fluxes of the narrow emission lines over the course of the campaign—some observations of long-term changes in narrow-line flux in local, low-luminosity sources have been reported (e.g., NGC 5548; Peterson et al. 2013), but simple luminosity scaling from NGC 5548 predicts narrow-line variability timescales of >30 rest-frame years in our quasars.

The PrepSpec model includes intrinsic variations in the continuum and broad emission lines, and the model is optimized to simultaneously fit all of the spectra of an object. In addition to the intrinsic variability of the continuum and emission lines,

<sup>&</sup>lt;sup>29</sup> PrepSpec can be downloaded at http://star-www.st-andrews.ac.uk/~kdh1/lib/prepspec/prepspec.tar.gz.

**Table 1**Quasar Sample Information

|            |  |                                       | Quasar                           | Sample Inform  | nation             |  |   |                   |
|------------|--|---------------------------------------|----------------------------------|----------------|--------------------|--|---|-------------------|
| RMID       | SDSS<br>Identifier                         | R.A. <sup>a</sup><br>(deg)<br>(J2000) | Decl. <sup>a</sup> (deg) (J2000) | z <sup>b</sup> | i mag <sup>b</sup> | $\log \lambda L_{\lambda 1350}^{\text{b}}$ $(\text{erg s}^{-1})$ | $\log M_{ m BH,SE}^{ m b,c} \ (M_{\odot})$                | S/N2 <sup>d</sup> |
| 000        | J141437.04+530422.7                        | 213.6543                              | 53.0730                          | 1.464          | 20.837             | $44.847 \pm 0.004^*$   |   | 20.9              |
| 004        | J141508.57+530019.7                        | 213.7857                              | 53.0055                          | 2.767          | 21.254             | $45.377 \pm 0.004$<br>$45.377 \pm 0.003$                         | $8.47 \pm 0.02$   | 20.9              |
| 006        | J141401.85+530058.5                        | 213.5077                              | 53.0163                          | 1.517          | 21.134             | $44.996 \pm 0.002^*$   | 0.47 ± 0.02   | 29.8              |
| 011        | J141534.20+525743.2                        | 213.8925                              | 52.9620                          | 2.053          | 20.174             | $45.649 \pm 0.001$   | $9.09 \pm 0.01$   | 42.4              |
| 012        | J141355.72+531202.3                        | 213.4822                              | 53.2006                          | 1.585          | 21.499             | $44.740 \pm 0.004^*$   |   | 30.7              |
| 013        | J141502.82+525401.2                        | 213.7618                              | 52.9003                          | 1.850          | 21.201             | $44.915 \pm 0.005$   | $8.15 \pm 0.02$   | 20.6              |
| 019        | J141529.69+525205.4                        | 213.8737                              | 52.8682                          | 1.918          | 20.117             | $45.422 \pm 0.001$   | $8.68 \pm 0.03$   | 26.4              |
| 024        | J141526.06+531941.7                        | 213.8586                              | 53.3283                          | 1.552          | 21.483             | $44.903 \pm 0.002^*$   |   | 22.7              |
| 025        | J141607.83+531535.0                        | 214.0327                              | 53.2597                          | 1.816          | 21.365             | $45.234\pm0.002$   | $8.93 \pm 0.01$   | 50.4              |
| 028        | J141543.08+525056.9                        | 213.9295                              | 52.8491                          | 1.392          | 19.087             | $45.786 \pm 0.001^*$   | •••   | 48.6              |
| 031        | J141640.89+530657.4                        | 214.1704                              | 53.1160                          | 1.907          | 19.675             | $45.967\pm0.001$   | $9.04 \pm 0.01$   | 53.9              |
| 032        | J141313.52+525550.2                        | 213.3064                              | 52.9306                          | 1.715          | 20.341             | $44.492 \pm 0.021$   | $7.60 \pm 0.03$   | 79.5              |
| 034        | J141254.00+530814.6                        | 213.2250                              | 53.1374                          | 1.825          | 19.847             | $45.589 \pm 0.001$   | $8.71 \pm 0.02$   | 30.2              |
| 035        | J141549.95+532005.5                        | 213.9581                              | 53.3349                          | 1.803          | 20.310             | $45.502 \pm 0.002$   | $8.76 \pm 0.02$   | 42.7              |
| 036        | J141420.55+532216.6                        | 213.5856                              | 53.3713                          | 2.216          | 19.447             | $45.909 \pm 0.001$   | $9.11 \pm 0.01$   | 28.7              |
| 038        | J141635.77+525649.3<br>J141607.12+531904.8 | 214.1491                              | 52.9470                          | 1.383          | 18.757             | $45.789 \pm 0.001^*$   | 0.49   0.07   | 23.3              |
| 039<br>041 | J141607.12+531904.8<br>J141643.78+525823.9 | 214.0297<br>214.1824                  | 53.3180<br>52.9733               | 3.041<br>1.852 | 19.769<br>19.097   | $45.619 \pm 0.003 45.396 \pm 0.002$                              | $\begin{array}{c} 8.48\pm0.07 \\ 9.05\pm0.01 \end{array}$ | 71.9<br>57.5      |
| 045        | J141501.31+532438.5                        | 213.7555                              | 53.4107                          | 3.060          | 20.295             | $45.974 \pm 0.002$   | $8.68 \pm 0.02$   | 22.0              |
| 049        | J141301.31+332438.3<br>J141416.10+524435.2 | 213.5671                              | 52.7431                          | 1.652          | 21.019             | $45.285 \pm 0.001^*$   | 6.06 ± 0.02<br>   | 20.2              |
| 051        | J141352.16+532434.8                        | 213.4673                              | 53.4097                          | 2.017          | 19.788             | $45.709 \pm 0.001$   | $9.00 \pm 0.01$   | 56.4              |
| 052        | J141250.39+531719.6                        | 213.2100                              | 53.2888                          | 2.305          | 20.701             | $45.499 \pm 0.002$   | $8.30 \pm 0.02$   | 26.9              |
| 055        | J141627.75+524813.9                        | 214.1157                              | 52.8039                          | 1.534          | 21.396             | $44.895 \pm 0.002^*$   |   | 36.6              |
| 057        | J141721.81+530454.3                        | 214.3409                              | 53.0818                          | 1.930          | 20.486             | $45.393 \pm 0.003$   | $8.33 \pm 0.02$   | 59.8              |
| 058        | J141229.66+531431.7                        | 213.1236                              | 53.2422                          | 2.300          | 21.381             | $45.353 \pm 0.002$   | $8.63 \pm 0.01$   | 30.5              |
| 059        | J141721.28+530210.5                        | 214.3387                              | 53.0363                          | 1.891          | 19.269             | $45.887 \pm 0.001$   | $8.90 \pm 0.01$   | 47.3              |
| 063        | J141233.79+525240.0                        | 213.1408                              | 52.8778                          | 1.537          | 20.899             | $44.631 \pm 0.004^*$   |   | 22.1              |
| 064        | J141641.41+532147.1                        | 214.1726                              | 53.3631                          | 2.216          | 20.768             | $45.390\pm0.001$   | $8.42\pm0.05$   | 36.4              |
| 065        | J141357.11+524229.9                        | 213.4880                              | 52.7083                          | 2.785          | 21.472             | $45.431 \pm 0.003$   | $8.65 \pm 0.04$   | 21.9              |
| 066        | J141524.43+532832.7                        | 213.8518                              | 53.4758                          | 2.148          | 21.295             | $45.173 \pm 0.003$   | $8.63 \pm 0.04$   | 49.8              |
| 069        | J141408.56+524038.7                        | 213.5357                              | 52.6774                          | 2.793          | 20.458             | $45.726 \pm 0.001$   | $8.53 \pm 0.02$   | 29.6              |
| 071        | J141551.33+524119.9                        | 213.9639                              | 52.6889                          | 1.693          | 20.721             | $45.354 \pm 0.002$   | $8.73 \pm 0.01$   | 34.8              |
| 072        | J141658.42+524806.3                        | 214.2434                              | 52.8018                          | 1.962          | 20.615             | $45.469 \pm 0.001$   | $8.99 \pm 0.02$   | 22.2              |
| 075        | J141217.02+525127.4                        | 213.0710                              | 52.8576                          | 2.655          | 19.596             | $46.059 \pm 0.001$   | $9.60 \pm 0.01$   | 23.7              |
| 076<br>079 | J141331.06+532858.6                        | 213.3794                              | 53.4830                          | 1.745          | 20.537             | $45.281 \pm 0.002$   | $8.75 \pm 0.01$   | 45.2              |
| 080        | J141743.33+531145.6<br>J141224.60+532150.3 | 214.4305<br>213.1025                  | 53.1960<br>53.3640               | 2.059<br>1.503 | 20.851<br>21.434   | $45.384 \pm 0.002 44.720 \pm 0.005^*$                            | 8.41 ± 0.02   | 21.6<br>33.6      |
| 081        | J141527.96+523746.9                        | 213.8665                              | 52.6297                          | 1.586          | 19.786             | $45.557 \pm 0.003$   | •••   | 39.4              |
| 086        | J141756.95+525956.7                        | 214.4873                              | 52.9991                          | 1.542          | 21.035             | $44.893 \pm 0.003^*$   | •••   | 21.1              |
| 087        | J141327.46+523851.8                        | 213.3645                              | 52.6477                          | 3.157          | 19.862             | $46.083 \pm 0.003$   | $8.76 \pm 0.01$   | 22.7              |
| 092        | J141134.18+530005.1                        | 212.8924                              | 53.0014                          | 1.357          | 20.155             | $45.131 \pm 0.002^*$   |   | 23.5              |
| 095        | J141219.47+532457.4                        | 213.0811                              | 53.4160                          | 2.316          | 21.457             | $45.202 \pm 0.003$   | $8.18 \pm 0.01$   | 24.5              |
| 097        | J141340.50+523618.4                        | 213.4188                              | 52.6051                          | 2.434          | 21.315             | $45.130 \pm 0.003$   | $8.21 \pm 0.01$   | 44.3              |
| 098        | J141416.34+533508.3                        | 213.5681                              | 53.5857                          | 2.454          | 21.254             | $44.816 \pm 0.008$   | $8.06 \pm 0.02$   | 60.8              |
| 107        | J141817.46+531116.8                        | 214.5728                              | 53.1880                          | 2.234          | 20.436             | $45.437 \pm 0.002$   | $8.48 \pm 0.01$   | 45.3              |
| 108        | J141226.77+524120.3                        | 213.1116                              | 52.6890                          | 2.193          | 21.013             | $45.375\pm0.002$   | $8.70 \pm 0.02$   | 22.7              |
| 110        | J141807.73+531754.0                        | 214.5322                              | 53.2983                          | 2.281          | 20.671             | $45.439\pm0.002$   | $8.90 \pm 0.01$   | 23.4              |
| 112        | J141132.56+525111.5                        | 212.8857                              | 52.8532                          | 1.397          | 19.793             | $44.956 \pm 0.003^*$   | •••   | 40.1              |
| 116        | J141432.46+523154.5                        | 213.6353                              | 52.5318                          | 1.878          | 19.681             | $45.652 \pm 0.001$   | $8.90 \pm 0.03$   | 34.5              |
| 117        | J141829.50+530207.8                        | 214.6229                              | 53.0355                          | 2.007          | 20.227             | $45.714 \pm 0.001$   | $9.15 \pm 0.01$   | 27.3              |
| 119        | J141135.55+524814.4                        | 212.8982                              | 52.8040                          | 2.729          | 20.048             | $46.060 \pm 0.001$   | $8.53 \pm 0.01$   | 39.6              |
| 124        | J141708.46+533253.6                        | 214.2853                              | 53.5482                          | 2.015          | 19.854             | $45.653 \pm 0.001$   | $8.86 \pm 0.01$   | 30.6              |
| 128        | J141103.17+531551.3                        | 212.7632                              | 53.2643                          | 1.862          | 20.012             | $45.359 \pm 0.002$   | $8.68 \pm 0.05$   | 24.2              |
| 130        | J141735.33+523851.4                        | 214.3972                              | 52.6476                          | 1.960          | 20.036             | $45.534 \pm 0.001$   | $8.39 \pm 0.03$   | 39.6              |
| 137        | J141112.59+532254.5                        | 212.8025                              | 53.3818                          | 3.266          | 21.129             | $45.709 \pm 0.003$   | $8.46 \pm 0.02$   | 24.8              |
| 142        | J141803.36+524127.7                        | 214.5140                              | 52.6910                          | 1.685          | 20.024             | $45.480 \pm 0.003$   | $8.96 \pm 0.01$   | 69.2              |
| 144        | J141843.30+531920.8                        | 214.6804                              | 53.3225<br>52.7322               | 2.300<br>2.137 | 20.685<br>21.592   | $45.516 \pm 0.001$   | $8.90 \pm 0.01$   | 38.9              |
| 145        | J141818.45+524356.0                        | 214.5769                              |                                  | 1.623          | 21.392             | $45.113 \pm 0.004 44.796 \pm 0.003^*$                            | 8.76 ± 0.03   | 63.2              |
| 149<br>150 | J141903.89+530855.4<br>J141252.32+523046.1 | 214.7662<br>213.2180                  | 53.1487<br>52.5128               | 1.623          | 20.765             | $45.057 \pm 0.003$   |   | 28.5<br>22.4      |
| 153        | J141232.32+323040.1<br>J141101.15+532327.7 | 212.7548                              | 53.3910                          | 2.753          | 19.761             | $45.831 \pm 0.002$   | $9.01 \pm 0.01$   | 28.9              |
| 154        | J141704.00+533807.4                        | 214.2667                              | 53.6354                          | 2.499          | 21.613             | $45.205 \pm 0.004$   | $8.79 \pm 0.01$   | 51.5              |
|            | 11.1.1.1.00   000007.1                     | =12007                                | 20.0001                          | /              | 21.010             | 0.001  | 2 / _ 0.01  | 01.0              |

Table 1 (Continued)

|            |  |                                       |  | (Continued)    |                    |  |  |                   |
|------------|--|---------------------------------------|--|----------------|--------------------|--|--|-------------------|
| RMID       | SDSS<br>Identifier                         | R.A. <sup>a</sup><br>(deg)<br>(J2000) | Decl. <sup>a</sup><br>(deg)<br>(J2000) | z <sup>b</sup> | i mag <sup>b</sup> | $\log \lambda L_{\lambda 1350}^{\text{b}}$ $(\text{erg s}^{-1})$ | $\log M_{\mathrm{BH,SE}}^{\mathrm{b,c}}$ $(M_{\odot})$ | S/N2 <sup>d</sup> |
| 155        | J141123.68+532845.7                        | 212.8487                              | 53.4794                                | 1.657          | 19.650             | $45.364 \pm 0.001^*$   |  | 46.8              |
| 156        | J141123.08+332843.7<br>J141334.20+534222.0 | 213.3925                              | 53.7061                                | 1.660          | 20.388             | $45.364 \pm 0.001$<br>$45.148 \pm 0.002^*$                       | •••  | 25.5              |
| 157        | J141045.53+531943.5                        | 212.6897                              | 53.3288                                | 1.383          | 19.958             | $45.148 \pm 0.002$<br>$45.125 \pm 0.002^*$                       |  | 37.5              |
| 158        | J141754.72+533254.8                        | 214.4780                              | 53.5486                                | 1.478          | 20.378             | $44.999 \pm 0.004^*$   | •••  | 31.9              |
| 159        | J141446.74+522523.7                        | 213.6948                              | 52.4233                                | 1.587          | 19.451             | $45.740 \pm 0.001^*$   | •••  | 50.7              |
| 161        | J141048.88+524839.8                        | 212.7037                              | 52.8111                                | 2.067          | 20.669             | $45.491 \pm 0.001$   | $8.32 \pm 0.04$  | 54.2              |
| 164        | J141655.72+534012.1                        | 214.2322                              | 53.6700                                | 1.907          | 21.658             | $44.985 \pm 0.005$   | $7.65 \pm 0.02$  | 38.4              |
| 172        | J141020.78+531316.8                        | 212.5866                              | 53.2213                                | 3.207          | 18.193             | $46.792 \pm 0.000$   | $9.54 \pm 0.00$  | 33.0              |
| 176        | J141801.94+523514.9                        | 214.5081                              | 52.5875                                | 1.497          | 19.425             | $45.473 \pm 0.001^*$   |  | 26.2              |
| 178        | J141852.89+532533.4                        | 214.7204                              | 53.4260                                | 1.947          | 20.614             | $45.585\pm0.001$   | $8.75\pm0.02$  | 35.1              |
| 179        | J141357.48+534612.8                        | 213.4895                              | 53.7702                                | 2.265          | 21.155             | $45.152\pm0.003$   | $8.37 \pm 0.07$  | 23.6              |
| 180        | J141007.73+530719.4                        | 212.5322                              | 53.1221                                | 3.101          | 19.815             | $46.166 \pm 0.001$   | $9.23 \pm 0.03$  | 28.1              |
| 181        | J141040.30+524523.1                        | 212.6679                              | 52.7564                                | 1.675          | 21.392             | $44.545 \pm 0.015$   | $7.79 \pm 0.04$  | 35.6              |
| 182        | J141121.05+523634.6                        | 212.8377                              | 52.6096                                | 1.571          | 20.430             | $45.253 \pm 0.001^*$   | •••  | 39.0              |
| 186        | J141022.58+532034.5                        | 212.5941                              | 53.3429                                | 1.393          | 21.589             | $45.168 \pm 0.002^*$   |  | 40.5              |
| 190        | J141005.94+531333.7                        | 212.5248                              | 53.2260                                | 1.992          | 21.013             | $45.284 \pm 0.003$   | $8.30 \pm 0.02$  | 53.0              |
| 194        | J141231.13+522632.0                        | 213.1297                              | 52.4422                                | 1.560          | 20.778             | $44.700 \pm 0.004^*$   | •••  | 27.4              |
| 196        | J140957.62+530959.6                        | 212.4901                              | 53.1666                                | 1.595          | 21.378             | $44.775 \pm 0.004^*$   | 0.40   0.01  | 25.4              |
| 201        | J141215.24+534312.1                        | 213.0635                              | 53.7200                                | 1.812          | 18.375             | $46.240 \pm 0.001$   | $9.40 \pm 0.01$  | 61.2              |
| 202<br>205 | J140958.54+525516.6<br>J141924.44+532315.5 | 212.4940<br>214.8519                  | 52.9213<br>53.3877                     | 2.635<br>2.940 | 19.803<br>19.318   | $45.927 \pm 0.001$ $46.002 \pm 0.001$                            | $8.61 \pm 0.01$<br>$9.00 \pm 0.02$                     | 58.9<br>51.1      |
| 207        | J141738.54+534251.0                        | 214.4106                              | 53.7142                                | 2.620          | 18.784             | $46.361 \pm 1.000$   | 9.00 ± 0.02<br>  | 33.0              |
| 208        | J141943.58+525431.3                        | 214.9316                              | 52.9087                                | 3.440          | 21.265             | $45.587 \pm 0.003$   | $8.18 \pm 0.03$  | 21.7              |
| 210        | J141952.79+530204.2                        | 214.9700                              | 53.0345                                | 1.903          | 20.922             | $45.346 \pm 0.002$   | $8.50 \pm 0.03$  | 25.9              |
| 213        | J141418.23+535046.8                        | 213.5760                              | 53.8463                                | 2.716          | 21.034             | $45.419 \pm 0.002$   | $8.65 \pm 0.02$  | 28.7              |
| 216        | J141541.99+521921.7                        | 213.9250                              | 52.3227                                | 2.036          | 21.615             | $45.396 \pm 0.002$   | $8.97 \pm 0.01$  | 28.0              |
| 217        | J141000.68+532156.1                        | 212.5029                              | 53.3656                                | 1.817          | 20.388             | $45.382 \pm 0.002$   | $8.67 \pm 0.02$  | 31.4              |
| 218        | J141229.98+522323.6                        | 213.1249                              | 52.3899                                | 2.102          | 20.900             | $45.402 \pm 0.002$   | $8.12 \pm 0.06$  | 26.9              |
| 220        | J141918.07+524158.4                        | 214.8253                              | 52.6996                                | 2.038          | 20.412             | $45.669\pm0.001$   | $8.81 \pm 0.02$  | 28.0              |
| 222        | J141044.47+533407.0                        | 212.6853                              | 53.5686                                | 2.009          | 21.355             | $45.081\pm0.004$   | $8.40 \pm 0.01$  | 59.8              |
| 225        | J141920.23+532838.9                        | 214.8343                              | 53.4775                                | 1.838          | 21.392             | $45.059\pm0.004$   | $8.10 \pm 0.03$  | 38.1              |
| 226        | J141431.50+535154.6                        | 213.6313                              | 53.8652                                | 2.915          | 20.804             | $45.396 \pm 0.003$   | $9.44 \pm 0.44$  | 26.4              |
| 227        | J141816.24+522940.6                        | 214.5677                              | 52.4946                                | 1.608          | 19.906             | $45.541 \pm 0.001^*$   |  | 26.0              |
| 230        | J141005.73+524342.2                        | 212.5239                              | 52.7284                                | 2.003          | 18.776             | $45.732 \pm 0.001$   | $9.17 \pm 0.04$  | 30.1              |
| 231        | J142005.59+530036.7                        | 215.0233                              | 53.0102                                | 1.645          | 19.794             | $45.736 \pm 0.001^*$   |  | 59.5              |
| 237<br>238 | J141021.95+523813.2<br>J141750.37+534517.7 | 212.5915<br>214.4599                  | 52.6370<br>53.7549                     | 2.392<br>2.189 | 19.600<br>20.115   | $45.866 \pm 0.001$ $45.831 \pm 0.001$                            | $9.20 \pm 0.01$<br>$8.92 \pm 0.03$                     | 51.6<br>32.3      |
| 236        | J141738.83+522333.0                        | 214.4399                              | 52.3925                                | 2.189          | 20.113             | $45.831 \pm 0.001$<br>$45.271 \pm 0.003$                         | $8.92 \pm 0.03$<br>$8.14 \pm 0.03$                     | 55.0              |
| 242        | J142010.48+531223.8                        | 215.0437                              | 53.2066                                | 2.591          | 20.050             | $45.652 \pm 0.002$   | $9.16 \pm 0.02$  | 24.7              |
| 244        | J140942.79+532219.3                        | 212.4283                              | 53.3720                                | 1.759          | 20.575             | $44.627 \pm 0.002$   | $8.95 \pm 0.12$  | 33.1              |
| 245        | J141347.68+521646.2                        | 213.4487                              | 52.2795                                | 1.670          | 20.903             | $45.351 \pm 0.004$   | $9.22 \pm 0.01$  | 23.1              |
| 249        | J141956.29+532402.6                        | 214.9846                              | 53.4007                                | 1.717          | 21.002             | $44.984 \pm 0.010$   | $7.89 \pm 0.06$  | 45.6              |
| 251        | J141554.32+535357.0                        | 213.9763                              | 53.8992                                | 2.196          | 20.862             | $45.324\pm0.002$   | $8.43 \pm 0.09$  | 31.0              |
| 253        | J141918.12+533453.3                        | 214.8255                              | 53.5815                                | 1.817          | 19.903             | $45.470\pm0.001$   | $8.79 \pm 0.01$  | 27.2              |
| 256        | J141334.12+535430.3                        | 213.3922                              | 53.9084                                | 2.244          | 21.640             | $45.089\pm0.003$   | $8.27\pm0.03$  | 32.5              |
| 257        | J140931.90+532302.2                        | 212.3830                              | 53.3840                                | 2.419          | 19.541             | $45.782\pm0.005$   | $9.19 \pm 0.04$  | 20.6              |
| 259        | J142025.58+531105.2                        | 215.1066                              | 53.1848                                | 1.845          | 21.401             | $44.777 \pm 0.010$   | $8.74 \pm 0.06$  | 27.5              |
| 262        | J141325.87+535440.6                        | 213.3578                              | 53.9113                                | 3.170          | 20.826             | $46.007 \pm 0.004$   | $8.90 \pm 0.01$  | 23.9              |
| 264        | J141214.19+535055.2                        | 213.0591                              | 53.8487                                | 2.120          | 21.513             | $45.434 \pm 0.002$   | $8.72 \pm 0.01$  | 67.5              |
| 266        | J141002.92+533334.4                        | 212.5122                              | 53.5596                                | 2.392          | 21.277             | $45.582 \pm 0.002$   | $8.47 \pm 0.01$  | 25.2              |
| 269        | J141929.90+533501.4                        | 214.8746                              | 53.5837                                | 2.393          | 21.269             | $45.193 \pm 0.003$   | $8.13 \pm 0.03$  | 20.4              |
| 275        | J140951.81+533133.7                        | 212.4659                              | 53.5260                                | 1.577          | 20.154             | $45.611 \pm 0.001^*$   | <br>9.61 ± 0.02  | 118.5             |
| 279<br>280 | J140945.82+523950.4                        | 212.4409                              | 52.6640<br>53.5355                     | 2.398          | 21.297             | $45.627 \pm 0.001$<br>$45.711 \pm 0.001^*$                       | 8.61 ± 0.03  | 30.6              |
| 280        | J141949.19+533207.7<br>J141938.71+523537.7 | 214.9550<br>214.9113                  | 53.5355<br>52.5938                     | 1.366<br>3.353 | 19.494<br>21.525   | $45.711 \pm 0.001^{*}  45.052 \pm 0.008$                         | $8.40 \pm 0.04$  | 40.5<br>24.8      |
| 282        | J141712.26+521655.8                        | 214.3011                              | 52.3938                                | 3.333<br>1.847 | 20.524             | $45.032 \pm 0.008$<br>$45.715 \pm 0.001$                         | $8.40 \pm 0.04$<br>$8.53 \pm 0.02$                     | 32.6              |
| 284        | J141927.35+533727.7                        | 214.8640                              | 53.6244                                | 2.386          | 20.324             | $45.642 \pm 0.001$   | $9.05 \pm 0.02$  | 53.0              |
| 286        | J142040.56+530740.7                        | 215.1690                              | 53.1280                                | 1.751          | 20.210             | $44.904 \pm 0.005$   | $8.50 \pm 0.03$  | 30.1              |
| 293        | J141923.06+533936.5                        | 214.8461                              | 53.6601                                | 1.849          | 21.133             | $45.201 \pm 0.002$   | $8.59 \pm 0.02$  | 21.6              |
| 295        | J141347.87+521204.9                        | 213.4495                              | 52.2014                                | 2.352          | 20.800             | $45.605 \pm 0.001$   | $8.87 \pm 0.02$  | 47.7              |
| 298        | J141155.56+521802.9                        | 212.9815                              | 52.3008                                | 1.635          | 19.997             | $45.596 \pm 0.001^*$   |  | 27.0              |
| 304        | J140847.22+530235.2                        | 212.1968                              | 53.0431                                | 1.492          | 20.606             | $45.414 \pm 0.001^*$   |  | 36.9              |
|            |  |                                       |  |                |                    |  |  |                   |

Table 1 (Continued)

|            |  |                            |                          | (Continued)      |                    |                                       |  |                   |
|------------|--|----------------------------|--------------------------|------------------|--------------------|---------------------------------------|--|-------------------|
|            | SDSS                                       | R.A. <sup>a</sup><br>(deg) | Decl. <sup>a</sup> (deg) |                  |                    | $\log \lambda L_{\lambda 1350}^{b}$   | $\log M_{\mathrm{BH,SE}}^{\mathrm{b,c}}$ |                   |
| RMID       | Identifier                                 | (J2000)                    | (J2000)                  | $z^{\mathbf{b}}$ | i mag <sup>b</sup> | $(erg s^{-1})$                        | $(M_{\odot})$                            | S/N2 <sup>d</sup> |
| 310        | J141220.09+535513.2                        | 213.0837                   | 53.9204                  | 2.770            | 20.561             | $45.717 \pm 0.002$                    | $9.34 \pm 0.02$                          | 28.8              |
| 312        | J140942.41+523516.7                        | 212.4267                   | 52.5880                  | 1.924            | 21.441             | $45.077\pm0.004$                      | $8.86\pm0.02$                            | 47.8              |
| 317        | J141905.16+522527.6                        | 214.7715                   | 52.4244                  | 1.602            | 19.677             | $45.520 \pm 0.001^*$                  | •••                                      | 45.1              |
| 318        | J141248.18+521243.6                        | 213.2008                   | 52.2121                  | 1.515            | 19.416             | $45.714 \pm 0.001^*$                  |  | 30.6              |
| 319        | J141842.55+534828.8                        | 214.6773                   | 53.8080                  | 2.337            | 21.345             | $45.296 \pm 0.002$                    | $8.64 \pm 0.02$                          | 22.0              |
| 321<br>322 | J142043.67+532206.3<br>J141851.53+534748.0 | 215.1820<br>214.7147       | 53.3684<br>53.7967       | 1.720<br>2.028   | 19.013<br>21.629   | $45.703 \pm 0.001 44.780 \pm 0.005$   | $8.55 \pm 0.01$<br>$8.10 \pm 0.03$       | 41.4<br>30.8      |
| 327        | J141831.33+334748.0<br>J142015.64+523718.8 | 215.0652                   | 52.6219                  | 1.675            | 19.101             | $45.821 \pm 0.003$                    | $8.88 \pm 0.01$                          | 55.0              |
| 330        | J141647.20+521115.2                        | 214.1967                   | 52.1876                  | 2.156            | 18.497             | $46.453 \pm 0.000$                    | $9.51 \pm 0.00$                          | 55.1              |
| 332        | J140843.68+524941.0                        | 212.1820                   | 52.8281                  | 2.581            | 21.203             | $45.551 \pm 0.002$                    | $8.15 \pm 0.02$                          | 51.7              |
| 334        | J141910.22+534707.1                        | 214.7926                   | 53.7853                  | 2.375            | 20.323             | $45.716 \pm 0.001$                    | $8.53 \pm 0.03$                          | 58.2              |
| 335        | J141932.07+522639.4                        | 214.8837                   | 52.4443                  | 2.167            | 21.087             | $45.491\pm0.002$                      | $8.56\pm0.03$                            | 37.1              |
| 339        | J142014.84+533609.0                        | 215.0618                   | 53.6025                  | 2.010            | 20.004             | $45.743\pm0.001$                      | $8.94 \pm 0.01$                          | 24.0              |
| 342        | J140822.40+530451.8                        | 212.0934                   | 53.0811                  | 1.696            | 19.474             | $45.834\pm0.001$                      | $9.11 \pm 0.01$                          | 54.9              |
| 343        | J141104.13+521755.4                        | 212.7672                   | 52.2987                  | 2.895            | 19.148             | $46.253 \pm 0.001$                    | $8.69 \pm 0.01$                          | 45.4              |
| 344        | J142113.25+531218.5                        | 215.3052                   | 53.2052                  | 1.948            | 20.777             | $45.161 \pm 0.003$                    | $8.66 \pm 0.01$                          | 46.8              |
| 345        | J141041.89+522020.4                        | 212.6746                   | 52.3390                  | 3.550            | 21.279             | $45.647 \pm 0.003$                    | $8.30 \pm 0.04$                          | 26.1              |
| 346        | J141843.67+535138.5                        | 214.6820                   | 53.8607                  | 1.589            | 20.672             | $44.905 \pm 0.003^*$                  | $7.95 \pm 0.08$                          | 35.0              |
| 348<br>349 | J142039.95+524014.9<br>J142005.04+533937.3 | 215.1665<br>215.0210       | 52.6708<br>53.6604       | 1.676<br>3.614   | 19.756<br>21.291   | $45.367 \pm 0.003 45.788 \pm 0.002$   | $7.93 \pm 0.08$<br>$8.52 \pm 0.02$       | 31.6<br>26.1      |
| 351        | J142003.04+333937.3<br>J141114.52+521611.0 | 212.8105                   | 52.2697                  | 1.717            | 20.790             | $43.788 \pm 0.002$ $44.788 \pm 0.009$ | $8.03 \pm 0.02$<br>$8.03 \pm 0.04$       | 44.2              |
| 353        | J140851.64+524134.2                        | 212.2152                   | 52.6928                  | 2.191            | 20.790             | $45.598 \pm 0.001$                    | $8.69 \pm 0.02$                          | 42.9              |
| 358        | J140954.32+522528.5                        | 212.4764                   | 52.4246                  | 1.906            | 20.159             | $45.268 \pm 0.003$                    | $8.54 \pm 0.04$                          | 86.1              |
| 359        | J142117.99+525346.0                        | 215.3250                   | 52.8961                  | 2.309            | 20.051             | $45.838 \pm 0.001$                    | $9.02 \pm 0.01$                          | 32.9              |
| 361        | J142100.22+524342.3                        | 215.2509                   | 52.7284                  | 1.617            | 19.459             | $45.576 \pm 0.001^*$                  |  | 42.9              |
| 362        | J141730.52+521019.4                        | 214.3772                   | 52.1721                  | 1.860            | 20.906             | $45.301\pm0.003$                      | $8.91 \pm 0.02$                          | 25.6              |
| 363        | J142113.29+524929.9                        | 215.3054                   | 52.8250                  | 2.635            | 19.000             | $46.497\pm0.001$                      | $9.68 \pm 0.01$                          | 24.6              |
| 366        | J142041.26+533355.3                        | 215.1719                   | 53.5654                  | 2.420            | 20.843             | $45.626\pm0.001$                      | $8.95\pm0.02$                            | 25.9              |
| 372        | J141236.48+540152.1                        | 213.1520                   | 54.0311                  | 1.745            | 20.246             | $45.616 \pm 0.001$                    | $9.09 \pm 0.01$                          | 63.0              |
| 379        | J141138.20+535906.2                        | 212.9092                   | 53.9851                  | 2.321            | 19.972             | $45.921 \pm 0.001$                    | $8.66 \pm 0.01$                          | 71.1              |
| 380<br>381 | J140801.53+530500.7                        | 212.0064<br>212.1142       | 53.0836                  | 1.969<br>2.538   | 20.415<br>20.058   | $45.527 \pm 0.001$ $46.152 \pm 0.001$ | $8.90 \pm 0.02$<br>$8.77 \pm 0.01$       | 29.7<br>64.7      |
| 383        | J140827.41+532710.2<br>J142136.28+530113.7 | 215.4012                   | 53.4528<br>53.0205       | 4.288            | 20.038             | $45.853 \pm 0.001$                    | $8.34 \pm 0.03$                          | 22.1              |
| 386        | J142050.74+533514.9                        | 215.2114                   | 53.5875                  | 1.865            | 20.803             | $45.279 \pm 0.002$                    | $8.39 \pm 0.03$                          | 22.4              |
| 387        | J141905.24+535354.1                        | 214.7719                   | 53.8984                  | 2.426            | 19.977             | $45.687 \pm 0.002$                    | $8.83 \pm 0.02$                          | 51.9              |
| 389        | J141839.03+521333.0                        | 214.6627                   | 52.2259                  | 1.850            | 19.656             | $45.564 \pm 0.002$                    | $8.97 \pm 0.01$                          | 59.2              |
| 394        | J140846.62+533613.5                        | 212.1943                   | 53.6038                  | 1.966            | 21.160             | $44.905 \pm 0.007$                    | $8.04 \pm 0.04$                          | 25.6              |
| 396        | J140751.37+531024.5                        | 211.9641                   | 53.1735                  | 1.836            | 21.072             | $44.911\pm0.005$                      | $8.70\pm0.04$                            | 28.4              |
| 397        | J142136.51+532014.2                        | 215.4022                   | 53.3373                  | 2.017            | 21.497             | $45.068\pm0.004$                      | $8.18 \pm 0.02$                          | 34.0              |
| 401        | J140957.28+535047.0                        | 212.4887                   | 53.8464                  | 1.822            | 20.226             | $45.490 \pm 0.003$                    | $8.55 \pm 0.03$                          | 43.2              |
| 403        | J140758.42+525058.2                        | 211.9935                   | 52.8495                  | 1.612            | 20.444             | $44.940 \pm 0.002^*$                  |  | 32.6              |
| 405        | J142109.48+523800.1                        | 215.2895                   | 52.6334                  | 3.386            | 19.921             | $46.082 \pm 0.001$                    | $8.81 \pm 0.03$                          | 34.8              |
| 408<br>409 | J141409.85+520137.2<br>J140916.98+522535.0 | 213.5411<br>212.3208       | 52.0270<br>52.4264       | 1.734<br>2.110   | 19.630<br>18.765   | $45.708 \pm 0.001$ $46.181 \pm 0.001$ | $8.47 \pm 0.09$                          | 49.4              |
| 410        | J140944.88+535002.7                        | 212.4370                   | 53.8341                  | 1.819            | 20.773             | $45.579 \pm 0.001$                    | $9.05 \pm 0.02$<br>$9.04 \pm 0.01$       | 74.6<br>41.5      |
| 411        | J141252.35+540628.0                        | 213.2181                   | 54.1078                  | 1.734            | 20.773             | $44.887 \pm 0.007$                    | $8.29 \pm 0.02$                          | 24.7              |
| 412        | J141157.71+520624.1                        | 212.9905                   | 52.1067                  | 1.515            | 19.397             | $45.891 \pm 0.000^{*}$                |  | 43.2              |
| 413        | J141915.40+535522.7                        | 214.8142                   | 53.9230                  | 3.340            | 20.791             | $45.601 \pm 0.002$                    | $9.10 \pm 0.03$                          | 28.6              |
| 414        | J141402.78+540856.4                        | 213.5116                   | 54.1490                  | 1.457            | 21.554             | $44.988 \pm 0.003^*$                  |  | 42.5              |
| 416        | J140849.42+534050.9                        | 212.2059                   | 53.6808                  | 2.600            | 19.870             | $45.621\pm0.002$                      | $8.96 \pm 0.01$                          | 39.6              |
| 418        | J142148.21+525104.3                        | 215.4509                   | 52.8512                  | 1.418            | 21.464             | $45.040 \pm 0.003^*$                  |  | 62.5              |
| 423        | J141155.27+540435.6                        | 212.9803                   | 54.0766                  | 1.521            | 20.626             | $45.296 \pm 0.001^*$                  | •••                                      | 26.3              |
| 424        | J142141.25+524551.6                        | 215.4219                   | 52.7644                  | 2.660            | 19.829             | $45.580 \pm 0.003$                    | $8.98 \pm 0.02$                          | 22.6              |
| 425        | J141030.00+521307.5                        | 212.6250                   | 52.2188                  | 2.574            | 21.273             | $45.306 \pm 0.002$                    | $8.69 \pm 0.03$                          | 22.5              |
| 426<br>430 | J141032.32+535740.2                        | 212.6347                   | 53.9612<br>52.4087       | 1.544            | 20.679<br>20.416   | $45.190 \pm 0.002^*$                  | <br>0.01 ± 0.07                          | 37.6              |
| 430        | J142027.25+522431.4<br>J141551.60+520025.6 | 215.1136<br>213.9650       | 52.4087                  | 3.919<br>1.518   | 18.838             | $46.150 \pm 0.001 45.930 \pm 0.001^*$ | $9.01 \pm 0.07$                          | 41.1<br>34.8      |
| 431        | J142202.80+530034.1                        | 215.5117                   | 53.0095                  | 1.316            | 19.890             | $45.429 \pm 0.001^*$                  |  | 35.7              |
| 433        | J141413.27+541017.8                        | 213.5553                   | 54.1716                  | 1.627            | 20.952             | $44.942 \pm 0.003^*$                  |  | 22.2              |
| 434        | J140911.66+522350.1                        | 212.2986                   | 52.3973                  | 1.545            | 20.564             | $45.574 \pm 0.001^*$                  | •••                                      | 53.4              |
| 435        | J142102.17+533944.1                        | 215.2591                   | 53.6623                  | 2.295            | 19.987             | $45.765\pm0.001$                      | $8.58\pm0.01$                            | 35.3              |
| 436        | J142053.67+534145.2                        | 215.2236                   | 53.6959                  | 1.742            | 20.752             | $45.382\pm0.002$                      | $8.59\pm0.01$                            | 33.0              |
|            |  |                            |                          |                  |                    |                                       |  |                   |

Table 1 (Continued)

|            |  |                            |                          | (Continued)      |                    |  |                                    |              |
|------------|--|----------------------------|--------------------------|------------------|--------------------|--|------------------------------------|--------------|
|            | SDSS                                       | R.A. <sup>a</sup><br>(deg) | Decl. <sup>a</sup> (deg) |                  |                    | $\log \lambda L_{\lambda 1350}^{b}$      | $\log M_{ m BH,SE}^{ m b,c}$       |              |
| RMID       | Identifier                                 | (J2000)                    | (J2000)                  | $z^{\mathbf{b}}$ | i mag <sup>b</sup> | $(\text{erg s}^{-1})$                    | $(M_{\odot})$                      | S/N2d        |
| 441        | J141531.90+515906.4                        | 213.8829                   | 51.9851                  | 1.397            | 19.354             | $45.636 \pm 0.001^*$                     |                                    | 28.3         |
| 442        | J141225.72+540741.6                        | 213.1072                   | 54.1282                  | 2.152            | 20.355             | $45.244 \pm 0.003$                       | $7.58 \pm 0.15$                    | 24.3         |
| 445        | J141114.36+520629.2                        | 212.8098                   | 52.1081                  | 1.519            | 19.939             | $45.489 \pm 0.001^*$                     |                                    | 37.6         |
| 447        | J142201.29+524824.4                        | 215.5054                   | 52.8068                  | 1.707            | 21.088             | $45.199\pm0.002$                         | $8.53 \pm 0.04$                    | 22.3         |
| 448        | J140725.96+525554.8                        | 211.8582                   | 52.9319                  | 1.626            | 20.943             | $44.793 \pm 0.003^*$                     | •••                                | 38.9         |
| 451        | J140850.38+534611.9                        | 212.2099                   | 53.7700                  | 2.674            | 19.340             | $46.031 \pm 0.001$                       | $9.25 \pm 0.01$                    | 30.8         |
| 452        | J142214.08+531516.7                        | 215.5587                   | 53.2547                  | 2.028            | 20.609             | $45.755\pm0.001$                         | $9.08 \pm 0.01$                    | 51.2         |
| 454        | J142018.09+521924.9                        | 215.0754                   | 52.3236                  | 2.011            | 18.969             | $45.985 \pm 0.000$                       | $9.18 \pm 0.01$                    | 22.4         |
| 455        | J142206.84+524958.4                        | 215.5285                   | 52.8329                  | 1.809            | 21.303             | $45.145 \pm 0.003$                       | $8.51 \pm 0.02$                    | 31.4         |
| 456        | J141259.13+515925.0                        | 213.2464                   | 51.9903                  | 2.266            | 19.958             | $45.677 \pm 0.001$                       | $9.19 \pm 0.01$                    | 29.4         |
| 461<br>462 | J140830.45+534309.2<br>J140916.45+535149.3 | 212.1269<br>212.3186       | 53.7192<br>53.8637       | 2.272<br>1.633   | 20.699<br>21.448   | $45.769 \pm 0.001  44.822 \pm 0.003^*$   | 9.14 ± 0.04                        | 34.6<br>23.6 |
| 467        | J142140.19+523614.9                        | 215.4175                   | 52.6042                  | 1.887            | 20.898             | $45.155 \pm 0.003$                       | $8.47 \pm 0.02$                    | 20.5         |
| 468        | J140713.60+530200.8                        | 211.8067                   | 53.0336                  | 3.127            | 20.453             | $45.959 \pm 0.003$                       | $9.23 \pm 0.02$                    | 34.5         |
| 470        | J142047.48+534759.9                        | 215.1979                   | 53.8000                  | 1.879            | 21.392             | $44.821 \pm 0.006$                       | $8.26 \pm 0.02$                    | 21.5         |
| 482        | J141011.80+521002.1                        | 212.5492                   | 52.1673                  | 1.530            | 19.580             | $45.733 \pm 0.001^*$                     |                                    | 20.7         |
| 485        | J141912.47+520818.0                        | 214.8020                   | 52.1383                  | 2.562            | 19.677             | $46.119 \pm 0.001$                       | $9.33 \pm 0.01$                    | 32.0         |
| 486        | J140940.81+521337.2                        | 212.4201                   | 52.2270                  | 1.401            | 19.702             | $45.626 \pm 0.001^*$                     | •••                                | 33.6         |
| 487        | J142206.54+524317.7                        | 215.5273                   | 52.7216                  | 1.845            | 20.549             | $45.278 \pm 0.004$                       | $8.34 \pm 0.05$                    | 63.8         |
| 488        | J142138.60+523324.6                        | 215.4108                   | 52.5568                  | 2.604            | 20.250             | $45.712\pm0.002$                         | $8.66 \pm 0.04$                    | 42.5         |
| 490        | J141058.03+540535.9                        | 212.7418                   | 54.0933                  | 1.953            | 20.320             | $45.583\pm0.001$                         | $8.96 \pm 0.01$                    | 34.3         |
| 491        | J140920.50+535445.5                        | 212.3354                   | 53.9127                  | 1.961            | 20.927             | $45.421\pm0.003$                         | $8.76 \pm 0.03$                    | 49.4         |
| 493        | J142039.47+521928.4                        | 215.1645                   | 52.3246                  | 1.592            | 18.605             | $46.028 \pm 0.000^*$                     | •••                                | 39.0         |
| 494        | J142142.57+533752.3                        | 215.4274                   | 53.6312                  | 1.867            | 21.201             | $45.316 \pm 0.001$                       | $7.86\pm0.20$                      | 34.7         |
| 495        | J140806.04+534046.5                        | 212.0252                   | 53.6796                  | 2.263            | 21.253             | $45.499 \pm 0.002$                       | $9.21 \pm 0.01$                    | 31.3         |
| 496        | J141101.51+520402.1                        | 212.7563                   | 52.0673                  | 2.080            | 20.508             | $45.560 \pm 0.001$                       | $8.39 \pm 0.02$                    | 21.2         |
| 499        | J141004.22+540109.0                        | 212.5176                   | 54.0192                  | 2.325            | 21.238             | $45.058 \pm 0.003$                       | $8.37 \pm 0.04$                    | 32.7         |
| 500        | J141033.34+540411.4                        | 212.6389                   | 54.0699                  | 1.966            | 21.283             | $45.276 \pm 0.003$                       | $8.44 \pm 0.02$                    | 31.1         |
| 506<br>507 | J141336.30+541501.2<br>J140959.26+520912.0 | 213.4013<br>212.4969       | 54.2503<br>52.1533       | 1.736<br>2.575   | 20.609<br>19.780   | $45.075 \pm 0.003$ $46.212 \pm 0.001$    | $8.79 \pm 0.09$<br>$9.02 \pm 0.02$ | 59.2<br>26.2 |
| 508        | J142129.40+522752.0                        | 215.3725                   | 52.4644                  | 3.228            | 18.124             | $46.919 \pm 1.000$                       | 9.02 ± 0.02                        | 32.9         |
| 511        | J140755.91+523040.3                        | 211.9830                   | 52.5112                  | 1.982            | 20.624             | $45.136 \pm 0.003$                       | $8.62 \pm 0.06$                    | 29.2         |
| 512        | J141254.37+541410.8                        | 213.2266                   | 54.2363                  | 4.328            | 19.394             | $46.518 \pm 0.001$                       | $9.40 \pm 0.02$                    | 41.5         |
| 514        | J140945.30+521033.7                        | 212.4388                   | 52.1760                  | 1.515            | 19.014             | $45.612 \pm 0.001^*$                     |                                    | 54.2         |
| 517        | J142049.31+535211.5                        | 215.2055                   | 53.8699                  | 2.216            | 20.200             | $45.839 \pm 0.001$                       | $9.11 \pm 0.01$                    | 39.1         |
| 520        | J141924.26+540348.6                        | 214.8511                   | 54.0635                  | 3.268            | 19.532             | $46.344 \pm 0.000$                       | $9.45 \pm 0.01$                    | 28.0         |
| 522        | J142041.78+521701.6                        | 215.1741                   | 52.2838                  | 1.384            | 20.214             | $45.242\pm0.002^*$                       | •••                                | 32.3         |
| 527        | J142226.76+524246.6                        | 215.6115                   | 52.7130                  | 1.647            | 20.930             | $44.788 \pm 0.003^*$                     | •••                                | 39.0         |
| 528        | J140647.49+525956.1                        | 211.6979                   | 52.9989                  | 1.820            | 19.777             | $45.170 \pm 0.004$                       | $7.39 \pm 0.22$                    | 21.6         |
| 529        | J141317.34+541614.6                        | 213.3223                   | 54.2707                  | 2.780            | 21.412             | $45.342 \pm 0.003$                       | $8.78 \pm 0.01$                    | 41.9         |
| 530        | J142036.56+521455.0                        | 215.1523                   | 52.2486                  | 2.214            | 21.298             | $45.332 \pm 0.002$                       | $8.74\pm0.02$                      | 23.0         |
| 531        | J142129.53+534633.4                        | 215.3731                   | 53.7759                  | 1.584            | 21.590             | $44.606 \pm 0.004^*$                     |                                    | 33.2         |
| 532<br>533 | J140757.37+522722.2<br>J140749.14+522924.2 | 211.9891<br>211.9548       | 52.4562<br>52.4901       | 2.407<br>1.770   | 20.763<br>20.102   | $45.506 \pm 0.002  45.337 \pm 0.002$     | $8.04 \pm 1.09$                    | 30.8<br>43.4 |
| 535        | J140749.14+322924.2<br>J142201.46+523250.2 | 215.5061                   | 52.5473                  | 2.122            | 19.781             | $45.737 \pm 0.002$<br>$45.737 \pm 0.001$ | $8.81 \pm 0.01$<br>$8.85 \pm 0.01$ | 45.4         |
| 538        | J141806.36+515821.1                        | 214.5265                   | 51.9725                  | 1.640            | 21.459             | $45.219 \pm 0.001^*$                     | 0.05 ± 0.01                        | 20.9         |
| 540        | J140705.59+524250.7                        | 211.7733                   | 52.7141                  | 2.747            | 20.206             | $46.019 \pm 0.001$                       | $8.96 \pm 0.01$                    | 42.1         |
| 542        | J140908.91+535805.0                        | 212.2871                   | 53.9681                  | 1.824            | 21.698             | $44.501 \pm 0.025$                       | $7.50 \pm 0.01$                    | 21.5         |
| 543        | J142015.35+540014.5                        | 215.0640                   | 54.0040                  | 2.059            | 20.555             | $45.677 \pm 0.001$                       | $8.94 \pm 0.01$                    | 21.7         |
| 549        | J141631.45+541719.7                        | 214.1311                   | 54.2888                  | 2.275            | 21.605             | $45.369 \pm 0.002$                       | $8.67 \pm 0.02$                    | 37.5         |
| 550        | J142116.86+535114.5                        | 215.3203                   | 53.8540                  | 1.879            | 21.218             | $45.113 \pm 0.003$                       | $8.46 \pm 0.04$                    | 23.6         |
| 553        | J142301.67+531100.5                        | 215.7570                   | 53.1835                  | 1.869            | 21.652             | $45.054\pm0.003$                         | $8.60 \pm 0.05$                    | 20.6         |
| 554        | J141948.09 + 520610.5                      | 214.9504                   | 52.1029                  | 1.706            | 20.250             | $45.573\pm0.002$                         | $8.71\pm0.01$                      | 32.4         |
| 555        | J142242.59+524415.6                        | 215.6775                   | 52.7377                  | 2.179            | 19.656             | $45.906\pm0.001$                         | $9.15\pm0.01$                      | 36.4         |
| 556        | J142232.53+523938.0                        | 215.6356                   | 52.6606                  | 1.494            | 19.416             | $45.525\pm0.001^*$                       | •••                                | 34.9         |
| 557        | J142155.20+522749.4                        | 215.4800                   | 52.4637                  | 2.519            | 20.684             | $45.525 \pm 0.003$                       | $8.76 \pm 0.04$                    | 25.0         |
| 560        | J141849.37+515950.4                        | 214.7057                   | 51.9973                  | 1.867            | 20.927             | $45.131 \pm 0.005$                       | $8.57 \pm 0.01$                    | 34.9         |
| 561        | J140853.68+535757.0                        | 212.2237                   | 53.9658                  | 1.652            | 19.154             | $45.767 \pm 0.001^*$                     |                                    | 51.9         |
| 562        | J141453.01+541952.4                        | 213.7209                   | 54.3312                  | 2.786            | 19.392             | $46.302 \pm 0.001$                       | $9.41 \pm 0.01$                    | 39.1         |
| 563        | J142113.92+521747.0                        | 215.3080                   | 52.2964                  | 1.971            | 19.904             | $45.763 \pm 0.001$                       | $8.96 \pm 0.01$                    | 25.2         |
| 564<br>573 | J142306.05+531529.0                        | 215.7752                   | 53.2581                  | 2.471            | 18.241             | $46.484 \pm 0.000$                       | $9.42 \pm 0.01$                    | 78.4         |
| 573        | J142242.14+533251.9                        | 215.6756                   | 53.5478                  | 1.993            | 19.823             | $45.765\pm0.001$                         | $8.40 \pm 0.06$                    | 29.1         |

Table 1 (Continued)

|            |  |                      |                    | (                |                    |   |                                    |                   |
|------------|--|----------------------|--------------------|------------------|--------------------|---|------------------------------------|-------------------|
|            | SDSS                                       | R.A. <sup>a</sup>    | Decl.a             |                  |                    | log VI b  | $\log M_{\rm BH,SE}^{\rm b,c}$     |                   |
| RMID       | Identifier                                 | (deg)<br>(J2000)     | (deg)<br>(J2000)   | $z^{\mathbf{b}}$ | i mag <sup>b</sup> | $\log \lambda L_{\lambda 1350}^{\text{b}}$ (erg s <sup>-1</sup> ) | $(M_{\odot})$                      | S/N2 <sup>d</sup> |
| 574        | J142047.87+521158.7                        | 215.1995             | 52.1997            | 1.982            | 21.264             | $44.905 \pm 0.009$  | $7.95 \pm 0.02$                    | 31.1              |
| 575        | J140939.50+540532.3                        | 212.4146             | 54.0923            | 1.625            | 20.530             | $45.417 \pm 0.001^*$  | 7.93 ± 0.02                        | 23.8              |
| 578        | J142254.99+524424.9                        | 215.7291             | 52.7403            | 1.570            | 19.658             | $45.272 \pm 0.002^*$  |                                    | 22.9              |
| 579        | J140622.08+530102.0                        | 211.5920             | 53.0172            | 2.329            | 21.461             | $45.131 \pm 0.004$  | $8.43 \pm 0.03$                    | 27.7              |
| 583        | J140731.08+534447.2                        | 211.8795             | 53.7464            | 1.709            | 20.814             | $45.416\pm0.003$  | $8.77\pm0.02$                      | 44.0              |
| 584        | J140802.98+535154.2                        | 212.0124             | 53.8651            | 4.058            | 19.120             | $46.646\pm0.000$  | $9.59\pm0.01$                      | 44.4              |
| 585        | J141609.14+514926.2                        | 214.0381             | 51.8240            | 1.829            | 19.850             | $45.328\pm0.002$  | $8.74 \pm 0.04$                    | 38.0              |
| 586        | J140624.61+531739.7                        | 211.6026             | 53.2944            | 2.392            | 21.275             | $45.526 \pm 0.002$  | $8.83 \pm 0.02$                    | 40.7              |
| 591        | J140954.00+540827.6                        | 212.4750             | 54.1410            | 2.100            | 19.073             | $46.326 \pm 0.000$  | $9.58 \pm 0.01$                    | 41.6              |
| 594<br>595 | J141903.81+515800.7<br>J140613.50+530742.5 | 214.7659<br>211.5563 | 51.9669<br>53.1285 | 2.934<br>1.707   | 20.414<br>21.665   | $45.731 \pm 0.002  45.058 \pm 0.005$                              | $8.66 \pm 0.03$<br>$7.22 \pm 0.05$ | 22.3<br>21.7      |
| 596        | J140727.88+522530.9                        | 211.8662             | 52.4253            | 1.767            | 19.025             | $45.844 \pm 0.003^{*}$  | 7.22 ± 0.03                        | 27.9              |
| 600        | J140617.85+531930.4                        | 211.5744             | 53.3251            | 1.425            | 20.466             | $45.149 \pm 0.003^*$  |                                    | 33.3              |
| 602        | J140630.77+532753.2                        | 211.6282             | 53.4648            | 3.115            | 21.354             | $45.428 \pm 0.004$  | $8.93 \pm 0.06$                    | 38.4              |
| 609        | J141952.89+520116.8                        | 214.9704             | 52.0214            | 2.229            | 19.431             | $46.120 \pm 0.001$  | $9.13 \pm 0.01$                    | 26.0              |
| 611        | J142301.08+533311.8                        | 215.7545             | 53.5533            | 1.886            | 17.691             | $46.492\pm0.000$  | $9.60 \pm 0.01$                    | 60.7              |
| 612        | J142252.42+533648.8                        | 215.7184             | 53.6136            | 2.083            | 21.289             | $45.216\pm0.002$  | $8.55\pm0.03$                      | 25.5              |
| 613        | J141007.73+541203.4                        | 212.5322             | 54.2010            | 2.336            | 18.120             | $46.591 \pm 0.001$  | $9.10 \pm 0.01$                    | 55.3              |
| 614        | J140904.48+520549.0                        | 212.2687             | 52.0970            | 2.061            | 20.912             | $44.490 \pm 0.016$  | $8.24 \pm 0.03$                    | 29.6              |
| 616        | J141056.25+541608.5                        | 212.7344             | 54.2691            | 2.320            | 19.025             | $46.377 \pm 0.000$  | $9.46 \pm 0.01$                    | 53.5              |
| 620        | J140707.30+522636.4                        | 211.7804             | 52.4435            | 2.582            | 20.245             | $45.514 \pm 0.003$  | $8.84 \pm 0.01$                    | 23.1              |
| 621<br>623 | J140650.01+534023.2<br>J141727.16+514856.0 | 211.7084<br>214.3632 | 53.6731<br>51.8156 | 1.774<br>2.959   | 20.995<br>20.282   | $45.031 \pm 0.009 45.877 \pm 0.002$                               | $8.40 \pm 0.01$<br>$8.83 \pm 0.03$ | 30.7<br>26.1      |
| 629        | J142340.69+530143.1                        | 215.9196             | 53.0286            | 1.641            | 20.282             | $43.877 \pm 0.002$<br>$44.727 \pm 0.004^*$                        | 6.65 ± 0.05                        | 26.1              |
| 630        | J141838.99+515253.5                        | 214.6625             | 51.8815            | 1.889            | 19.326             | $45.969 \pm 0.000$  | $9.16 \pm 0.01$                    | 38.0              |
| 631        | J140554.87+530323.5                        | 211.4787             | 53.0565            | 2.717            | 19.828             | $46.188 \pm 0.001$  | $9.44 \pm 0.04$                    | 52.9              |
| 633        | J142337.51+531828.8                        | 215.9063             | 53.3080            | 2.439            | 20.579             | $45.311 \pm 0.002$  | $8.79 \pm 0.06$                    | 23.6              |
| 635        | J140726.67+522013.2                        | 211.8611             | 52.3370            | 2.595            | 18.908             | $46.405\pm0.001$  | $9.43 \pm 0.02$                    | 37.9              |
| 636        | J141102.59+541817.6                        | 212.7608             | 54.3049            | 2.232            | 20.789             | $45.657\pm0.001$  | $8.49 \pm 0.02$                    | 20.5              |
| 646        | J140813.16+540045.3                        | 212.0549             | 54.0126            | 1.409            | 20.716             | $45.147 \pm 0.002^*$  | •••                                | 21.9              |
| 647        | J142318.46+533252.5                        | 215.8269             | 53.5479            | 1.599            | 19.941             | $45.290 \pm 0.001^*$  |                                    | 22.8              |
| 648        | J140903.51+520307.1                        | 212.2646             | 52.0520            | 1.788            | 20.590             | $45.170 \pm 0.004$  | $8.06 \pm 0.10$                    | 23.7              |
| 651<br>658 | J142149.30+521427.8<br>J140916.26+520022.1 | 215.4554<br>212.3178 | 52.2411<br>52.0062 | 1.486<br>1.947   | 20.194<br>21.473   | $45.412 \pm 0.001^*$<br>$44.577 \pm 0.011$                        | $8.05 \pm 0.02$                    | 35.0<br>30.0      |
| 660        | J142342.66+524831.5                        | 215.9278             | 52.8088            | 1.852            | 19.302             | $45.831 \pm 0.001$  | $8.31 \pm 0.02$                    | 38.6              |
| 661        | J141959.93+541255.3                        | 214.9997             | 54.2154            | 2.411            | 20.864             | $45.628 \pm 0.002$  | $8.82 \pm 0.02$                    | 21.5              |
| 665        | J141604.84+542639.8                        | 214.0202             | 54.4444            | 1.944            | 20.132             | $45.440 \pm 0.002$  | $8.82 \pm 0.02$                    | 30.9              |
| 670        | J141534.44+542730.4                        | 213.8935             | 54.4585            | 2.021            | 21.340             | $45.388\pm0.002$  | $8.16 \pm 0.09$                    | 27.5              |
| 676        | J140904.15+541023.7                        | 212.2673             | 54.1733            | 2.515            | 18.530             | $46.527\pm0.001$  | $9.82 \pm 0.01$                    | 45.9              |
| 678        | J142103.25+520427.0                        | 215.2636             | 52.0742            | 1.462            | 19.620             | $45.519 \pm 0.001^*$  | •••                                | 29.9              |
| 680        | J141940.24+515437.2                        | 214.9177             | 51.9103            | 1.831            | 20.553             | $45.402 \pm 0.002$  | $8.38 \pm 0.04$                    | 27.8              |
| 682        | J142338.37+533057.4                        | 215.9099             | 53.5160            | 1.881            | 21.603             | $45.045 \pm 0.004$  | $8.17 \pm 0.02$                    | 41.0              |
| 686<br>687 | J140913.79+515841.6<br>J140532.25+530401.5 | 212.3075<br>211.3844 | 51.9782<br>53.0671 | 2.134<br>3.072   | 21.047<br>20.958   | $45.444 \pm 0.002$ $45.586 \pm 0.002$                             | $8.67 \pm 0.01$<br>$8.86 \pm 0.05$ | 40.5<br>36.3      |
| 688        | J140332.23+330401.3<br>J141129.65+514701.7 | 212.8735             | 51.7838            | 1.679            | 19.617             | $45.580 \pm 0.002$<br>$45.597 \pm 0.001$                          | $8.37 \pm 0.03$                    | 28.8              |
| 689        | J140542.53+532323.5                        | 211.4272             | 53.3899            | 2.005            | 21.303             | $45.223 \pm 0.003$  | $8.31 \pm 0.01$                    | 126.8             |
| 690        | J140616.09+533926.0                        | 211.5670             | 53.6572            | 1.504            | 19.462             | $45.594 \pm 0.001^*$  |                                    | 35.5              |
| 692        | J142308.03+522815.5                        | 215.7835             | 52.4710            | 1.642            | 19.260             | $45.729 \pm 0.001^*$  | •••                                | 33.6              |
| 693        | J142043.51+520038.7                        | 215.1813             | 52.0108            | 1.988            | 20.017             | $45.643\pm0.001$  | $8.82\pm0.02$                      | 28.1              |
| 695        | J140706.74+521836.3                        | 211.7781             | 52.3101            | 1.526            | 21.256             | $44.606 \pm 0.006^*$  |                                    | 24.4              |
| 698        | J142350.24+532929.3                        | 215.9594             | 53.4915            | 2.137            | 21.090             | $45.458\pm0.002$  | $8.82 \pm 0.02$                    | 26.6              |
| 699        | J141039.64+542102.9                        | 212.6652             | 54.3508            | 2.345            | 20.465             | $45.640 \pm 0.003$  | $8.35 \pm 0.03$                    | 30.4              |
| 703        | J142051.98+541029.2                        | 215.2166             | 54.1748            | 2.216            | 20.182             | $45.660 \pm 0.002$  | $8.72 \pm 0.01$                    | 33.2              |
| 704<br>705 | J140629.07+534625.9<br>J140607.57+523207.9 | 211.6212<br>211.5315 | 53.7739<br>52.5355 | 1.649<br>1.772   | 21.179<br>20.201   | $44.990 \pm 0.003^*$<br>$45.345 \pm 0.003$                        | 9.06 $\pm$ 0.01                    | 29.3<br>60.3      |
| 705<br>706 | J140540.19+532850.6                        | 211.3313             | 52.5555            | 1.774            | 20.201             | $45.345 \pm 0.003$<br>$45.316 \pm 0.003$                          | $9.08 \pm 0.01$<br>$8.68 \pm 0.02$ | 30.8              |
| 710        | J142418.21+530406.5                        | 216.0759             | 53.0685            | 2.868            | 19.396             | $46.432 \pm 0.001$  | $9.43 \pm 0.01$                    | 44.9              |
| 711        | J140617.56+522829.4                        | 211.5732             | 52.4748            | 1.426            | 20.544             | $45.152 \pm 0.002^*$  |                                    | 37.2              |
| 713        | J142411.08+532041.3                        | 216.0462             | 53.3448            | 2.370            | 20.114             | $45.865 \pm 0.001$  | $9.04 \pm 0.01$                    | 48.3              |
| 715        | J142017.80+541531.4                        | 215.0742             | 54.2587            | 1.701            | 19.684             | $45.513\pm0.002$  | $8.88\pm0.01$                      | 34.5              |
| 718        | J141915.05+542136.0                        | 214.8127             | 54.3600            | 3.189            | 20.539             | $46.071\pm0.001$  | $9.62\pm0.01$                      | 37.9              |
| 722        | J142419.18+531750.6                        | 216.0800             | 53.2974            | 2.509            | 19.494             | $45.799\pm0.002$  | $9.20\pm0.07$                      | 44.0              |

Table 1 (Continued)

| RMID | SDSS<br>Identifier  | R.A. <sup>a</sup><br>(deg)<br>(J2000) | Decl. <sup>a</sup><br>(deg)<br>(J2000) | z <sup>b</sup> | i mag <sup>b</sup> | $\log \lambda L_{\lambda 1350}^{b}$ (erg s <sup>-1</sup> ) | $\log M_{ m BH,SE}^{ m b,c} \ (M_{\odot})$ | S/N2 <sup>d</sup> |
|------|---------------------|---------------------------------------|--|----------------|--------------------|--|--|-------------------|
| 723  | J140844.48+515843.3 | 212.1854                              | 51.9787                                | 1.635          | 20.582             | 45.272 ± 0.002*  |  | 39.7              |
| 725  | J142322.50+522656.1 | 215.8438                              | 52.4489                                | 1.770          | 19.900             | $45.704 \pm 0.001$   | $9.19 \pm 0.01$                            | 22.2              |
| 729  | J142404.67+532949.3 | 216.0195                              | 53.4970                                | 2.768          | 19.563             | $46.074 \pm 0.001$   | $9.10 \pm 0.01$                            | 57.9              |
| 734  | J141425.95+513801.6 | 213.6081                              | 51.6338                                | 2.332          | 20.640             | $45.530 \pm 0.001$   | $9.06 \pm 0.02$                            | 30.5              |
| 735  | J141728.92+542849.8 | 214.3705                              | 54.4805                                | 1.829          | 21.147             | $45.081 \pm 0.004$   | $8.35 \pm 0.03$                            | 29.7              |
| 737  | J140648.14+535449.0 | 211.7006                              | 53.9136                                | 1.585          | 19.838             | $45.619 \pm 0.001^*$                                       |  | 35.3              |
| 738  | J142400.40+533347.0 | 216.0017                              | 53.5631                                | 1.599          | 19.986             | $45.478 \pm 0.001^*$                                       |  | 22.6              |
| 739  | J142047.88+515650.8 | 215.1995                              | 51.9475                                | 2.988          | 21.203             | $45.500 \pm 0.013$   | $8.80 \pm 0.06$                            | 21.8              |
| 743  | J142405.10+533206.3 | 216.0213                              | 53.5351                                | 1.730          | 19.181             | $45.389 \pm 0.002$   | $8.53 \pm 0.01$                            | 38.8              |
| 748  | J140906.84+515358.0 | 212.2785                              | 51.8995                                | 1.848          | 20.854             | $45.181 \pm 0.003$   | $9.02 \pm 0.02$                            | 21.2              |
| 749  | J140855.61+515512.2 | 212.2317                              | 51.9201                                | 2.561          | 20.981             | $45.401 \pm 0.003$   | $8.44 \pm 0.02$                            | 36.8              |
| 751  | J140711.71+521033.4 | 211.7988                              | 52.1760                                | 1.368          | 20.825             | $45.249 \pm 0.002^*$                                       |  | 21.3              |
| 752  | J142322.69+534913.5 | 215.8446                              | 53.8204                                | 1.864          | 20.867             | $45.321 \pm 0.002$   | $8.42 \pm 0.02$                            | 25.6              |
| 753  | J142435.26+531448.8 | 216.1470                              | 53.2469                                | 1.562          | 19.538             | $45.558 \pm 0.001^*$                                       |  | 35.0              |
| 754  | J142014.47+515124.3 | 215.0603                              | 51.8568                                | 1.891          | 20.434             | $45.334 \pm 0.002$   | $8.70 \pm 0.01$                            | 24.0              |
| 759  | J142434.46+525310.8 | 216.1436                              | 52.8863                                | 1.966          | 20.886             | $45.080 \pm 0.004$   | $8.88 \pm 0.03$                            | 23.9              |
| 763  | J140636.91+521614.0 | 211.6538                              | 52.2706                                | 1.634          | 20.282             | $45.196 \pm 0.002^*$                                       |  | 36.8              |
| 770  | J142106.86+533745.2 | 215.2786                              | 53.6292                                | 1.862          | 16.456             | $46.948 \pm 0.003$   | $9.31 \pm 0.10$                            | 59.7              |
| 771  | J141604.54+541039.5 | 214.0189                              | 54.1777                                | 1.492          | 18.642             | $45.841 \pm 0.000^*$                                       |  | 29.2              |
| 774  | J141031.12+520316.6 | 212.6297                              | 52.0546                                | 1.686          | 19.343             | $45.884 \pm 0.001$   | $8.90 \pm 0.00$                            | 58.4              |
| 777  | J141021.11+541452.5 | 212.5880                              | 54.2479                                | 1.402          | 17.680             | $46.170 \pm 0.000^*$                                       |  | 52.8              |
| 784  | J140903.64+541746.9 | 212.2652                              | 54.2964                                | 1.677          | 17.358             | $46.340 \pm 0.001$   | $9.30 \pm 0.01$                            | 78.8              |
| 794  | J141122.38+524154.4 | 212.8433                              | 52.6984                                | 2.386          | 20.899             | $45.350 \pm 0.002$   | $8.20 \pm 0.01$                            | 25.8              |
| 796  | J141807.61+534204.4 | 214.5317                              | 53.7012                                | 3.008          | 20.538             | $45.837 \pm 0.001$   | $8.92 \pm 0.07$                            | 41.6              |
| 801  | J140926.98+523933.3 | 212.3624                              | 52.6593                                | 1.772          | 20.970             | $44.680 \pm 0.011$   | $9.00 \pm 0.06$                            | 30.8              |
| 803  | J140854.31+524549.8 | 212.2263                              | 52.7639                                | 3.623          | 21.106             | $45.469 \pm 0.005$   | $8.23 \pm 0.03$                            | 27.9              |
| 809  | J141350.98+541028.9 | 213.4625                              | 54.1747                                | 1.659          | 20.750             | $45.204 \pm 0.005$   | $8.91 \pm 0.23$                            | 32.8              |
| 810  | J140735.62+524925.0 | 211.8984                              | 52.8236                                | 1.826          | 19.849             | $45.298 \pm 0.004$   | $8.22 \pm 0.02$                            | 62.2              |
| 811  | J141258.26+541058.8 | 213.2428                              | 54.1830                                | 1.964          | 19.625             | $46.056 \pm 0.000$   | $8.80 \pm 0.01$                            | 54.3              |
| 816  | J141656.69+541223.6 | 214.2362                              | 54.2066                                | 1.637          | 21.349             | $44.869 \pm 0.004^*$                                       |  | 21.6              |
| 818  | J141124.46+541121.3 | 212.8519                              | 54.1893                                | 1.954          | 19.643             | $45.863 \pm 0.001$   | $8.92 \pm 0.01$                            | 32.5              |
| 820  | J141739.09+541425.6 | 214.4129                              | 54.2405                                | 1.757          | 20.710             | $45.324 \pm 0.005$   | $8.76 \pm 0.01$                            | 49.2              |
| 821  | J141810.69+541301.1 | 214.5446                              | 54.2170                                | 3.511          | 20.720             | $45.978 \pm 0.002$   | $9.11 \pm 0.01$                            | 37.7              |
| 827  | J141218.03+541817.1 | 213.0751                              | 54.3048                                | 1.965          | 20.034             | $44.999 \pm 0.006$   | $7.99 \pm 0.02$                            | 63.7              |
| 828  | J141328.37+542052.8 | 213.3682                              | 54.3480                                | 2.782          | 20.902             | $45.636 \pm 0.002$   | $8.26 \pm 0.06$                            | 23.0              |
| 829  | J141151.56+515302.5 | 212.9648                              | 51.8841                                | 1.804          | 21.479             | $44.852 \pm 0.007$   | $8.24 \pm 0.05$                            | 26.0              |
| 831  | J141635.13+542141.8 | 214.1464                              | 54.3616                                | 2.130          | 19.419             | $46.043 \pm 0.001$   | $9.14 \pm 0.01$                            | 21.5              |
| 835  | J141302.73+542245.1 | 213.2614                              | 54.3792                                | 1.545          | 21.093             | $44.996 \pm 0.002^*$                                       | ).14 ± 0.01                                | 27.8              |

#### Notes

(This table is available in machine-readable form.)

PrepSpec also accounts for variations in seeing and small shifts in the wavelength solution. Various spectral measurements from PrepSpec using the first year of data only are presented by Shen et al. (2019b).

We use PrepSpec to improve our flux calibrations and subsequently to produce measurements of line fluxes, line widths, mean/rms profiles, and light curves for each emission line (and various continuum regions, depending on the wavelength ranges accessible for each object). We convolve our PrepSpec-corrected spectra with the SDSS filter response curves (Fukugita et al. 1996; Doi et al. 2010) to produce *g*- and *i*-band synthetic photometry for each quasar. To estimate the uncertainties in the synthetic

photometric fluxes, we sum in quadrature the spectral uncertainties and the errors in the flux-correction factors reported by PrepSpec.

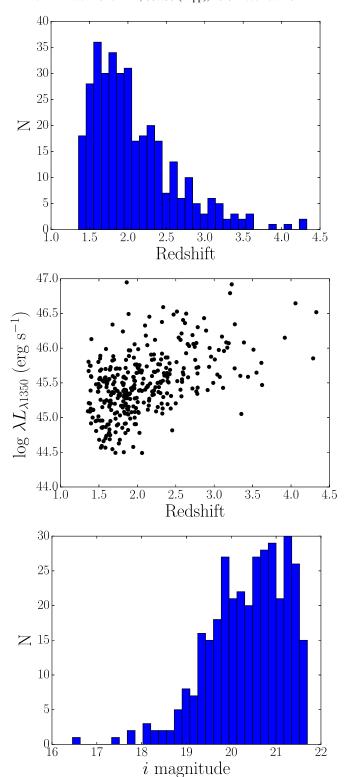
Before further analysis, we first removed any suspect epochs and outliers from our spectroscopic light curves. The seventh epoch is a significant outlier in a large fraction of the light curves; following Grier et al. (2017), we remove this epoch from all of our spectroscopic light curves. In addition, there are occasional spectra (roughly 4% of epochs) that have zero flux or are significant low-flux outliers in the light curves (these are cases where the BOSS spectrograph fibers were not plugged in correctly or the SDSS pipeline failed to extract a

<sup>&</sup>lt;sup>a</sup> These measurements were made as a part of the SDSS Data Release 10 (Ahn et al. 2014).

<sup>&</sup>lt;sup>b</sup> These measurements were retrieved from Shen et al. (2019b). The *i* magnitudes listed are PSF magnitudes, and have not been corrected for Galactic extinction. Luminosity measurements with asterisks (\*) indicate measurements where  $L_{1350}$  was not available. In these cases, we converted  $L_{1700}$  to  $L_{1350}$  using measurements from Richards et al. (2006).

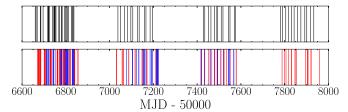
<sup>&</sup>lt;sup>c</sup> Black hole mass uncertainties listed here include measurement uncertainties only; the estimated systematic uncertainties beyond those listed is 0.4 dex.

 $<sup>^{\</sup>rm d}$  S/N2 measurements from PrepSpec (see Section 2.1).



**Figure 1.** The distributions of various properties of our quasar sample. From top to bottom: the redshift distribution,  $\lambda \log L_{\lambda 1350}$  (the continuum luminosity at 1350 Å) vs. redshift, and the distribution of *i*-magnitude. All quantities were measured by Shen et al. (2019b).

proper spectrum). We excluded all points with zero flux, as well as those that were offset from the median flux by more than five times the normalized median absolute deviation (NMAD) of the light curve (Maronna et al. 2006).



**Figure 2.** The distribution of MJD for the 2014–2017 spectroscopic observations from SDSS (top panel) and photometric observations from the Bok and CFHT (bottom panel). Each vertical line represents an observed epoch. Black lines indicate SDSS spectroscopic observations, blue lines represent CFHT observations, and red lines indicate Bok observations. The large spacings between sets of lines highlight the seasonal gap between each observing year.

#### 2.3. Photometric Data

To improve the cadence of our continuum light curves, we also monitored the SDSS-RM field in the g and i bands with the Steward Observatory Bok 2.3 m telescope on Kitt Peak from 2014 to 2017, and the 3.6 m CFHT on Maunakea from 2014 to 2016. We used the Bok/90Prime instrument (Williams et al. 2004) for our observations; it has a  $1^{\circ} \times 1^{\circ}$  field of view, mapping the observations onto a  $4k \times 4k$  CCD with a plate scale of 0.45 pixel-1. On the CFHT, we used the MegaCam instrument (Aune et al. 2003), which has a similar  $1^{\circ} \times 1^{\circ}$  field of view and a pixel scale of 0.187. The observing cadence of the photometric observations is provided in Figure 2.

Following Grier et al. (2017), we adopted the image subtraction method as implemented in the software package ISIS (Alard & Lupton 1998; Alard 2000) to produce the photometric light curves. The basic steps are as follows: (1) the images are aligned; (2) the images with the best seeing, transparency, and sky background are used to create a reference image; (3) for each epoch, the reference image point-spread function (PSF) is altered to match that of the epoch, and a flux-calibration scale factor is applied to the target image; (4) the epoch and the reference image are subtracted, yielding a "difference" image that has the same flux calibration as the reference image; (5) a residual-flux light curve is produced by placing a PSF-weighted aperture over each source to measure the flux in the subtracted image.

We performed the image subtraction separately for each individual telescope, field, filter, and CCD, to obtain *g*- and *i*-band light curves for each quasar. Before further analysis, we removed problematic epochs from the light curves, such as epochs where the source fell on or near the edge of the detector, epochs where the sources were saturated or too close to a nearby saturated star, or epochs affected by cirrus clouds. As with our spectroscopy, epochs were identified as outliers in the light curves that deviated from the median flux by >5 times the NMAD of the light curve within each individual observing season (i.e., the NMAD was calculated using only data taken within a specific observing season, and outliers excluded from that season based on that NMAD alone, rather than the entire four-year light curve). We visually inspected all of the resulting light curves to confirm that this procedure was effective.

# 2.4. Light-curve Intercalibration and Uncertainties

To improve the precision of our continuum light curves, we placed all of the light curves from different instruments,

telescopes, fields, and in different bands onto the same flux scale —we hereafter refer to this as light-curve "intercalibration." This approach accounts for differences in detector properties, telescope throughputs, and properties specific to the individual telescopes. We combine both *g*- and *i*-band light curves together to increase the number of data points, assuming that the time lag between these two bands is negligible. Interband continuum lags have been measured for some of the SDSS-RM sample by Homayouni et al. (2019), but the measured lags are generally on the order of a week or less, which is smaller than the uncertainties for our lag measurements.

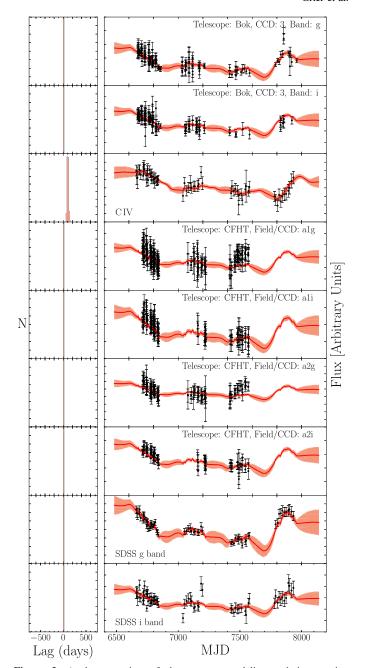
To combine our light curves, we use the Continuum REprocessing AGN MCMC (CREAM) software recently developed by Starkey et al. (2016). A brief overview of this technique is provided here; see Starkey et al. (2016) for details. CREAM models the light curves using Markov chain Monte Carlo (MCMC). The model assumes that the observed continuum emission is first emitted from a central "lamp post" and later reprocessed by more distant gas. Each telescope/ field/CCD light curve is fit to a model that includes an additive offset, scaling parameter, and transfer function (for intercalibration purposes, we set the parameters within CREAM such that it has a delta function response at zero lag). After optimization via the MCMC fitting process, the rescaled g and ilight curves are placed on the same scale as the reference light curve, and the resulting light curves are treated as a single light curve for all further analysis purposes. Figure 3 provides a demonstration of this procedure.

The final step in our light-curve preparation considers the uncertainties in our data. The ISIS image subtraction software reports only local Poisson error contributions and neglects additional systematic uncertainties; our photometric/continuum light-curve uncertainties are thus generally underestimated by a factor of a few. Similarly, PrepSpec includes only spectral uncertainties in its emission-line flux calculations. To address this, we use an additional feature of the CREAM software that allows it to adjust the nominal error bars of the light curves. We used CREAM to search for extra variance within the light curves and apply a multiplicative correction to the uncertainties when they are underestimated. For our quasar sample, CREAM applied a median scale factor of 3.5 to correct the uncertainties in the continuum light curves and 2.6 for the emission-line light curves. We adopt the CREAM-scaled light curves and their adjusted uncertainties for all further analysis. Table 2 provides the final, intercalibrated light curves for each source with adjusted uncertainties.

# 2.5. Emission-line Variability Contamination

Because we are using photometric light curves (including synthetic photometry produced from spectra) to represent the continuum light curves, we also investigate the emission lines that fall within the wavelength range covered by the *g*- and *i*-band filters. The broad emission lines are expected to be variable, and strongly variable emission lines falling within the wavelength range of the filters could have a significant impact on the photometric/continuum light curve. Significant variability contamination from the BLR would result in underestimated lag measurements, effectively making it more difficult to detect a lag.

Because the lag measurements depend on the observed variability, we need to know how much of that observed variability is due to the broad emission lines instead of the



**Figure 3.** A demonstration of the CREAM modeling technique, using SDSS J141250.39+531719.6 (RM 052) as an example. The left panels present the CREAM posterior distributions of observed-frame time lags; the right panels show the original light curves (black filled points) with the CREAM model fits and their uncertainty envelopes (red).

continuum. To estimate this, we use the PrepSpec measurements of intrinsic rms variability for the broad emission lines and continuum within the wavelength range covered by the g and i filters. The "variability contamination fraction" (hereafter  $f_{\text{var,BLR}}$ ) is the sum of the variability contributions from each emission line within the FWHM of the filter:  $f_{\text{var,BLR}} = \sum \left(\frac{\text{rms}_{\text{line}}}{\text{rms}_{\text{cont}}}\right) \left(\frac{\text{EW}_{\text{line}}}{\text{FWHM}}\right)$ . Here,  $\text{rms}_{\text{line}}$  and  $\text{rms}_{\text{cont}}$  are the PrepSpecmeasured fractional rms variability of each broad emission line and the continuum nearest the filter effective wavelength, and  $\text{EW}_{\text{line}}$  is the observed-frame equivalent width of the emission line measured by Shen et al. (2019b). In our sources, this quantity is generally small, matching the expectation that the

Table 2 RM 000 Light Curve

| MJD       |                   |                        |                   |                    |
|-----------|-------------------|------------------------|-------------------|--------------------|
| (-50000)  | Band <sup>a</sup> | Telescope <sup>b</sup> | Flux <sup>c</sup> | Error <sup>c</sup> |
| 6660.2090 | g                 | S                      | 0.99              | 0.06               |
| 6664.5132 | g                 | S                      | 1.11              | 0.07               |
| 6669.5005 | g                 | S                      | 1.21              | 0.08               |
| 6671.4697 | g                 | В                      | 0.93              | 0.18               |
| 6671.4717 | g                 | В                      | 0.87              | 0.17               |
| 6675.4595 | g                 | В                      | 1.39              | 0.21               |
| 6675.4619 | g                 | В                      | 1.46              | 0.20               |
| 6675.5303 | g                 | В                      | 1.10              | 0.12               |
| 6675.5327 | g                 | В                      | 1.23              | 0.13               |
| 6677.4727 | g                 | В                      | 1.31              | 0.14               |
| 6677.4751 | g                 | В                      | 1.02              | 0.15               |
| 6678.4312 | g                 | В                      | 1.08              | 0.09               |
| 6678.4336 | g                 | В                      | 1.06              | 0.09               |
| 6680.4292 | g                 | В                      | 1.15              | 0.13               |
| 6680.4316 | g                 | В                      | 1.20              | 0.13               |
| 6683.4800 | g                 | S                      | 0.98              | 0.06               |
| 6685.4228 | g                 | В                      | 1.13              | 0.05               |
| 6685.4248 | g                 | В                      | 1.14              | 0.05               |
| 6685.5239 | g                 | В                      | 1.17              | 0.04               |
| 6685.5264 | g                 | В                      | 1.18              | 0.04               |
| 6686.4736 | g                 | S                      | 1.14              | 0.07               |
| 6696.7783 | g                 | S                      | 1.09              | 0.07               |
| 6701.3901 | g                 | В                      | 0.76              | 0.21               |
| 6701.3921 | g                 | В                      | 0.76              | 0.21               |

#### Notes.

continuum is more variable than the emission lines (e.g., Sun et al. 2015). We find a median variability contamination fraction of 9.1% in the g band and 1.4% in the i band in our quasar sample. In other words, the BLR contamination is negligible for most of our sources, and will generally be smaller than the measured lag uncertainties.

# 3. Time-series Analysis

## 3.1. Lag Measurements

We follow Grier et al. (2017), hereafter G17, and employ three lag detection methods to analyze our sample: The JAVELIN software (Zu et al. 2011), traditional cross-correlation functions (CCF; e.g., Peterson et al. 2004), and the CREAM software (Starkey et al. 2016). Details of each of these methods are provided in each of these works as listed; we provide only a brief synopsis of each method here.

Our primary method for time-lag detection is the JAVE-LIN code (Zu et al. 2011, 2013). We model the light curves as autoregressive processes using a damped random walk (DRW) model, which has been demonstrated to be a good description of quasar behavior on the timescales relevant to our study (e.g., Kelly et al. 2009; Kozłowski et al. 2010; MacLeod et al. 2010, 2012; Kozłowski 2016). JAVELIN accounts for all of the likely behavior of the light curves during gaps in the light

curve, and applies uncertainties to the model accordingly. JAVELIN builds a model of both the continuum and emission-line light curves while simultaneously fitting a transfer function using Markov Chain Monte Carlo techniques. We assume that the emission-line light curves are smoothed, lagged versions of the continuum light curve, and adopt a top-hat transfer function that is parameterized by a scaling factor, width, and time delay. We allow JAVELIN to explore a range of observed lags from -750 to 750 days, which is about 60% of the total length of our campaign. We then determine  $\tau_{\rm JAV}$ , the best-fit time delay, from the posterior distribution of lags produced by the MCMC chain, after some modifications that are described below (Section 3.2).

Accurately modeling the light curves requires a wellconstrained damping timescale ( $\tau_{DRW}$ ), and for the time baseline covered by our data, this quantity is not fit well by JAVELIN—for example, using simulated light curves, Kozłowski (2017) found that the light curves must span at least 10 times  $au_{\mathrm{DRW}}$  in order to obtain a reliable measurement. Prior RM studies using JAVELIN have fixed the value to be longer than the length of the observing campaign (e.g., Fausnaugh et al. 2016; Grier et al. 2017), which effectively negates the impact of this on the time-lag measurements. Because the time baseline of the data in this work is longer than the expected damping timescales, however, we here allow this parameter to vary in JAVELIN, but place a strong constraint on the  $au_{
m DRW}$ parameter. For each source, we calculate the expected  $au_{\mathrm{DRW}}$ value based on Table 1 and Equation (7) of MacLeod et al. (2010), which relates the damping timescale to the luminosity of the quasar; this expected value (typically on the order of  $\sim$ 400–600 days for our sample) is fed into JAVELIN as a starting point, with small allowable uncertainties, for the MCMC step. This prevents the software from fitting unphysically small damping timescales to the data. However, the lag measurements are quite insensitive to the  $\tau_{DRW}$  value fit by JAVELIN; lag measurements obtained with and without setting this constraint are almost always consistent with one another. In addition, we also fixed the width of the top-hat transfer function to 20 observed-frame days; this helps keep JAVELIN from fitting unphysical values when the top-hat width cannot be constrained by our data. We tested several different top-hat widths (ranging from 10 to 40 days), and the lag results came out consistent with one another regardless of the width chosen: Fixing the top-hat width produces more clean posterior lag distributions than when it is allowed to vary, but the exact value of the chosen width has a negligible effect on our results.

Historically, CCF methods have been used most frequently to measure RM lags, so we include these measurements for completeness and ease of comparison with prior results. However, we note that these methods have been reported to perform less well on data sets with quality similar to ours (e.g., G17; Li et al. 2019); these data have more sparse time sampling and noisy light curves, compared to much of the RM data for local AGNs. This class of methods includes the interpolated cross correlation function (ICCF; e.g., Peterson et al. 1998), the discrete correlation function (DCF; Edelson & Krolik 1988) and z-transformed DCF (zDCF; Alexander 1997). We adopted the ICCF method, as it has been used most often in previous studies and has also been shown to perform better than the DCF in cases of low sampling (White & Peterson 1994). The ICCF linearly interpolates between data points on a

<sup>\*</sup>Light curves for all 348 quasars can be found online. A portion are shown here for guidance in formatting.

<sup>&</sup>lt;sup>a</sup> CIV = C IV emission line, g = g band, and i = i band.

 $<sup>^{</sup>b}$  C = CFHT, B = Bok, S = SDSS.

<sup>&</sup>lt;sup>c</sup> Continuum Flux densities and uncertainties are in units of  $10^{-17}$  erg s<sup>-1</sup> cm<sup>-2</sup> Å<sup>-1</sup>. Integrated emission-line fluxes are in units of  $10^{-17}$  erg s<sup>-1</sup> cm<sup>-2</sup>. (This table is available in its entirety in machine-readable form.)

user-specified grid, and the CCF is constructed by calculating the Pearson coefficient r between the two light curves at each possible lag. The centroid of the CCF ( $\tau_{\rm cent}$ ) is measured using points surrounding the maximum correlation coefficient  $r_{\rm max}$  of the CCF. We used the PyCCF code<sup>30</sup> (Peterson et al. 1998; Sun et al. 2018) to perform our ICCF calculations with an interpolation grid spacing of two days, and again restricted our lag search to lags between -750 and 750 days. We calculate the best lag measurement and its uncertainties via the flux randomization/random subset sampling method, using Monte Carlo simulations, as discussed by Peterson et al. (2004). We perform 5000 realizations to obtain the cross correlation centroid distribution (CCCD) and adopt the median of the distribution; the uncertainties in either direction are set to the 68th percentile of the distribution.

As an additional check, we report the lags measured by CREAM, which also measures time delays while performing the intercalibration of the light curves discussed above. CREAM is similar to JAVELIN in many ways, but it assumes a random walk model (where the Fourier transform of the time series is inversely proportional to the square of the frequency) instead of a DRW model to interpolate the light curves (Starkey et al. 2016). During the intercalibration process, CREAM fits a tophat transfer function to the emission lines and reports the posterior probability distribution of lag values, from which we measure the best-fit lag ( $\tau_{\text{CREAM}}$ ).

#### 3.2. Alias Identification and Removal

One of the hazards of obtaining RM data with regular seasonal gaps is the potential for lag-detection algorithms to prefer lags that result in the light curves being shifted into the seasonal gaps in the data; i.e., because RM lag detection algorithms interpolate or model within these gaps, they often end up associating features in the real continuum light curves with "fake" (i.e., model or interpolated) data in the shifted emission-line light curves. Inopportune features in the light curves can cause various lag-detection methods to latch onto incorrect lags (e.g., Grier et al. 2008). In addition, these data (and single-season data) often possess multiple significant peaks in their lag posterior distributions that can easily be identified as aliases of a primary lag solution; including the entire posterior distribution in the lag calculation in these cases often results in a skewed lag measurement and/or uncertainties that are unreasonably large.

To remedy these issues, we require additional procedures beyond simply measuring the lags from the entire posterior distributions for each method. We adopt a procedure similar to that used by G17 (see their Section 3.2), but modified to take into account the effects of seasonal gaps on the data. We apply a weight on the distribution of  $\tau$  measurements in the posterior probability distributions—this weight is used to search for the primary peak of the distribution and establish a range of lags within the posterior distribution that are included in the final lag and uncertainty calculations. Our weighting procedure has two components:

1. The first component takes into account the number of overlapping spectral epochs at each time delay. Applying a time lag  $\tau$  to the emission-line light curve will shift the data such that fewer "real" points will overlap. If the time

lag is such that the shift results in little or no overlap between the two data sets (for example, a  $\tau$  of 180 days in data sets with regular seasonal gaps of six months), detecting that lag will be very difficult. Any potential detection of such a lag in our data has a relatively high probability of being spurious, therefore we downweight such lags in the posterior distribution. We calculate the function  $P(\tau) = [N(\tau)/N(0)]^2$ , where  $N(\tau)$  is the number of real emission-line data points that overlap in date ranges with the continuum data and N(0) is the number of overlapping points at  $\tau = 0$ . Thus, the weight on a lag measurement is 1 at  $\tau = 0$  and decreases each time a data point moves outside the data overlap regions. Because our data have regular annual gaps of six months,  $P(\tau)$ rises and falls as each segment of the light curve is shifted into and out of the overlapping ranges of each year of data.

2. The second component accounts for the effect our seasonal gaps will have on our ability to detect certain lags. To characterize this phenomenon, we compute the autocorrelation function (ACF) of the continuum variations. If the ACF declines rapidly, the annual gaps will have a significant effect on our sensitivity because we are less likely to account correctly for the light-curve behavior during the gaps. In cases where the ACF declines slowly away from zero lag, it is straightforward to interpolate across the seasonal gaps, and the gaps are thus less likely to have an effect on our lag measurements.

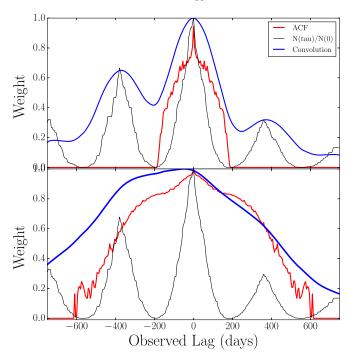
The final weight that we apply to the posterior distributions is thus a convolution of the continuum ACF and the  $P(\tau)$ function, with one small adjustment: if the ACF drops below zero within our lag range, we set its value at that lag to zero before the convolution. Figure 4 shows two examples of these functions (one with a rapidly declining ACF and one with a slowly declining ACF). We smooth the weighted posterior lag distributions (for JAVELIN and CREAM, this is the posterior lag distribution, and in the case of the cross-correlation function, this is the CCCD) by a Gaussian kernel with a width of 15 days, and identify the tallest peak within this smoothed distribution as the "primary" peak. We identify local minima in the distribution to either side of the peak and adopt these minima as the minimum and maximum lags to be included in our final lag calculation. We then return to the unweighted posteriors, reject all lag samples that lie outside the determined range, and use the remaining samples to calculate the final lag and its uncertainties.

The best lag is taken to be the median of the distribution, with the uncertainty in either direction calculated using samples within the 68th percentile of the distribution. Figure 5 provides a demonstration of this procedure for one of the quasars in our sample. We tested this alias removal approach with mock light curves (with known lags) that mimic the SDSS-RM data, and found that this approach is very efficient in removing alias lags (Li et al. 2019).

# 3.3. Lag-significance Criteria

While our alias-removal procedure above mitigates the problem of lag aliases and seasonal gaps, these methods are not foolproof. The fact remains that, in some cases, the lags are just not well-measured, despite the models reporting their best solutions. Following G17, we thus impose a number of

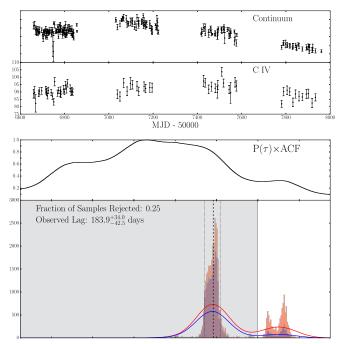
<sup>&</sup>lt;sup>30</sup> The PyCCF code is available for download at https://bitbucket.org/cgrier/python\_ccf\_code.



**Figure 4.** A demonstration of the adopted weighting scheme used in our alias removal procedure. The black line indicates  $P(\tau)$ , the red line shows the continuum ACF (set to zero wherever it is originally less than zero), and the thick blue line is the convolution of the two, which is our final adopted weight. The top panel shows an example where the continuum ACF declines rapidly (thus making it more unlikely that we detect spurious lags within the gaps in overlapping points); the bottom panel demonstrates a case where the continuum ACF declines slowly.

additional criteria on our measurements for a lag to be considered a significant detection:

- 1. The lag can be positive or negative, but must be inconsistent with zero at  $1\sigma$  significance.
- 2. Less than half of the posterior lag samples can be removed by our alias-removal procedure described in Section 3.2. If this procedure eliminates a larger fraction of samples, it indicates that most of the samples lie outside of the primary peak that we identified, suggesting that we lack a solid measurement of  $\tau$ .
- 3. The behavior of the light curves must be well-correlated at or near the measured lag, as characterized by the Pearson correlation coefficient r measured by the ICCF. We include only measurements of quasars for which r reaches a value greater than 0.5 within  $\pm 1\sigma$  of the reported lag (see below for a discussion of how this threshold was chosen).
- 4. When selecting our quasar sample, we required that the emission-line light curves showed some variability (see Section 2.1). However, after merging the light curves and adjusting the uncertainties of the light curves, some sources are no longer significantly variable. We thus require that both the continuum and emission lines are still considered significantly variable after the intercalibration process. To quantify this variability, we follow G17 and measure the rms variability S/Ns in the merged/adjusted light curves. We require that the continuum and emission-line rms variability S/N (S/N<sub>con</sub> and S/N<sub>line</sub>) are greater than 6.5 and 2.0, respectively. This criterion effectively eliminates cases where the light curves are consistent with little-to-no real variability, which can result in the lag

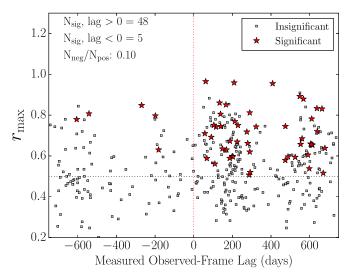


**Figure 5.** A demonstration of our alias removal procedure. The top two panels are the light curves for RM 119 (SDSS J141135.55+524814.4), with continuum flux density in units of in units of  $10^{-17}$  erg s<sup>-1</sup> cm<sup>-2</sup> Å<sup>-1</sup> and integrated emission-line fluxes in units of  $10^{-17}$  erg s<sup>-1</sup> cm<sup>-2</sup>. Third panel shows the adopted weighting scheme. Bottom panel shows the original JAVELIN posterior distribution for this object (pink histogram) and the weighted posterior distribution after applying the calculated weight (blue histogram). Solid red and blue lines indicate the smoothed posterior distribution of the original and weighted posteriors, respectively. Shaded gray region highlights the range of lags included in the final lag calculation. Dashed black vertical line indicates the measured lag, and black dotted lines show the measured uncertainties.

detection methods latching onto monotonic trends or spurious correlations between noisy light curves. Roughly 20% of the 348 quasars do not meet this criterion for  $\rm S/N_{line}.$  However, all but two of those sources also fail additional criteria, and would thus not have been selected as significant lags regardless.

Detailed simulations addressing the quality of lag detections yielded by our procedures are presented by Li et al. (2019). To determine the thresholds for  $r_{\rm max}$ , S/N<sub>con</sub>, and S/N<sub>line</sub>, we utilize a positive/negative false-positive test as implemented by Shen et al. (2016), G17, and Li et al. (2019). We assume that there is no physical reason to measure a negative lag; if all lag measurements were due to spurious correlations rather than physical processes, we would expect to measure equal numbers of positive and negative lags in our sample (the nonuniform temporal sampling pattern in our data does not bias our results toward either positive or negative lags<sup>31</sup>). We can thus use the number of negative lag measurements to estimate the rate of false-positive detections at positive lags in our sample. We

<sup>31</sup> To verify this, we ran simulations using mock light curves. First, a random walk model was used to generate a continuum light curve, sampled at one-day intervals. Shifting the continuum light curve with a delay in the range -1.5 to +1.5 yr then provided a line light curve. These were sampled with 32 epochs in Year 1 and 12 epochs in each of Years 2–4, to approximate the SDSS-RM sampling. Synthetic data were then generated with Gaussian noise for various assumed S/N ratios. For each pair of synthetic light curves, the ICCF was computed and its peak located. The above was repeated for 1000 random-walk realizations. There is no significant difference in lag detections between positive and negative lags, indicating that our assumption above is reasonable.



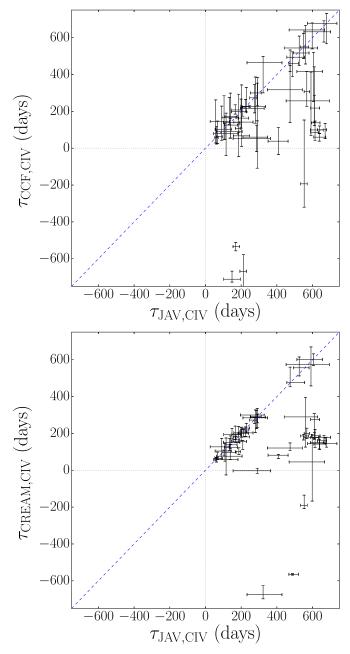
**Figure 6.** The measured time lag vs.  $r_{\rm max}$  for all quasars in our sample. Those measurements that do not meet the criteria for significant lags are shown as gray points; those that meet all of the significance criteria are represented by red stars. The vertical dotted red line indicates a lag of zero, to guide the eye, and the horizontal dotted black line indicates the threshold of  $r_{\rm max}=0.5$  used to select our significant lag sample.

define the "false-positive rate" as the ratio of negative lags to positive lags. Even including all of our lowest-quality measurements, we see a strong preference for positive lags: without imposing any selection criteria at all, we have 253 positive measurements and 95 negative measurements (see Figure 6), which indicates a false-positive rate of 37%. We provide all 348 measurements, as well as the quantities via which we measure their significance, in the Appendix in Table 5.

We choose the thresholds for our selection criteria described above in order to lower our false-positive rate to an acceptable level while maximizing the number of positive lag detections. We choose a maximum acceptable false-positive rate of 10%. Figure 6 shows the resulting distribution of lags for both those deemed "insignificant" and those passing our selection criteria. By downselecting the sample to a false-positive rate of 10%, we exclude many true lags: based on the false-positive rate without imposing our additional constraints, we expect that our sample has on the order of  $\sim 100$  additional measurable lags. Such lags may be recoverable with additional years of data.

We adopt JAVELIN as our primary lag-detection method and therefore require that all of our significance criteria are satisfied specifically for the JAVELIN measurements. This results in 48 positive lag detections and five negative measurements in our full "primary" sample of lag detections.

For comparison purposes, we apply these selection criteria separately to the lags measured with all three methods. In about 2/3 of our lag measurements, the resulting lags from all three methods are consistent with one another (see Figure 7). As reported by G17 and others (e.g., Li et al. 2019), the ICCF generally produces larger uncertainties than JAVELIN and CREAM, and the ICCF is less sensitive than JAVELIN to lag detection with light-curve qualities similar to SDSS-RM (Li et al. 2019). There has been some discussion in the literature (e.g., Edelson et al. 2019) regarding the uncertainties reported by JAVELIN; i.e., it has been suggested that JAVELIN uncertainties are underestimated. However, recent work by two independent groups suggests that the JAVELIN lag uncertainties are actually more representative of the true uncertainties than



**Figure 7.** A comparison of the observed-frame lag measurements made using the different detection methods for our 48 positive lag detections. The top panel shows the lags measured by the ICCF vs. the <code>JAVELIN</code> measurements, and the bottom panel presents lags measured by <code>CREAM</code> vs. the <code>JAVELIN</code> measurements.

those reported by the ICCF method, provided that the JAVELIN assumption of Gaussian light-curve uncertainties is satisfied (Li et al. 2019; Yu et al. 2019). In addition, we note that 41 out of 48 of our significant lags were also formally detected by the ICCF method, which has been found to *overestimate* the lag uncertainties, and while we chose  $1\sigma$  as our detection threshold, all but four of them are  $>\!\!2\sigma$  detections. Our detections are thus robust against the possibility that the uncertainties reported by JAVELIN are underestimated to within a reasonable extent.

For about a third of our measurements, the ICCF or CREAM software reported different alias lags than JAVELIN; in these cases, a different primary peak was identified, resulting in lag disagreements. In all of these cases, we see the same

peaks present for all three methods, but their strengths vary, causing different lags to be preferred by different methods. In these cases, the different lags are frequently one-year aliases of one another. We have visually inspected all of the cases where the three measurement methods disagree, and can confirm that the peaks identified by JAVELIN are reliable in most cases. Those cases where the JAVELIN lags appear to be incorrect are taken into account with our lag measurement quality ratings (discussed in Section 3.4).

# 3.4. Lag Measurement Quality and the "Gold" Sample

#### 3.4.1. Quality Ratings

Though our false-positive test (Figure 6) indicates that the majority of our lag measurements are robust, because our lag-selection procedure uses statistical arguments and we apply our criteria to achieve a false-positive rate of 10%, it is statistically likely that the lag sample presented here contains false detections. A subset of our lag detections have characteristics indicating that they are more likely to be real than others. Thus, we follow G17 and assign quality ratings to each of our measurements, in order to help readers assess the results. We use a scale of 1–5, with 1 representing the lowest-quality measurements and 5 representing the highest-quality measurements. We took into account a variety of criteria when assigning these quality ratings:

- 1. There are variability features visible in the continuum light curve that also appear in the emission-line light curve; i.e., it is possible to pick out a "lag" between the two light curves by eye.
- 2. There is clearly defined structure corresponding to the C IV emission line in the rms line profile (see Figure 12 in the Appendix).
- 3. The model fits from JAVELIN and CREAM match the light-curve data well, and there is general agreement in the models between the two methods.
- 4. The ICCF has a clear, well-defined peak on or around the measured lag.
- 5. There is general agreement between the three different methods used.
- 6. Unimodality of the posterior lag distribution: If there are several other peaks with strengths comparable to that of the peak that was determined to be the primary one, this reduces our confidence in a lag measurement.

We include these quality ratings, assigned by the first author of this work, in Table 3. In addition, we place all of the measurements with quality ratings of 4 and 5 into a "gold sample" of lag measurements that represent our highest-confidence individual measurements. Our gold sample includes 16 sources. We note that the criteria used to rate the lag measurements are subjective and based primarily on our prior experience with RM measurements. Thus, our gold sample is not statistically meaningful and should not be interpreted as such.

# 3.4.2. Broad Absorption-line Contamination

Because we are focused on the C IV region of the spectrum, we must also consider the possible presence of broad and narrow absorption features. PrepSpec does not currently fit absorption profiles; for narrow absorption lines, it generally has little issue interpolating across the absorption line. This will not

Table 3
SDSS-RM Observed-frame Lag Detections

|      |       |  |   |  | 0 11: 8                        |
|------|-------|--|---|--|--------------------------------|
| RMID | z     | $	au_{ m JAV} \  m (days)$                     | $	au_{	ext{CCF}}$ (days)                        | $	au_{	ext{CREAM}}$ (days)               | Quality <sup>a</sup><br>Rating |
|      |       | <u> </u>                                       |   |  |                                |
| 000  | 1.463 | $322.8^{+105.6}_{-90.1}$                       | $463.9^{+33.7}_{-163.4}$                        | $-675.2^{+48.4}_{-22.6}$                 | 2                              |
| 032  | 1.720 | 62.0 <sup>+9.5</sup> <sub>-9.8</sub>           | $57.5^{+61.7}_{-34.8}$                          | $67.4^{+2.1}_{-22.8}$                    | 5                              |
| 036  | 2.213 | $605.2^{+50.1}_{-93.1}$                        | $416.4^{+104.2}_{-162.5}$                       | $601.1^{+30.8}_{-31.9}$                  | 1                              |
| 052  | 2.311 | $187.1^{+10.4}_{-19.4}$                        | $107.9^{+22.8}_{-21.7}$                         | $100.3^{+21.7}_{-14.4}$                  | 4                              |
| 057  | 1.930 | $610.4^{+31.2}_{-16.5}$                        | $137.6^{+150.0}_{-14.8}$                        | $187.1^{+16.8}_{-19.2}$                  | 1                              |
| 058  | 2.299 | $614.0^{+19.5}_{-24.4}$                        | 84.8 <sup>+62.5</sup><br>621.8 <sup>+59.7</sup> | $177.4^{+43.9}_{-53.0}$                  | 1                              |
| 130  | 1.960 | 663.8 <sup>+36.8</sup> 501.2 <sup>+102.9</sup> | $631.8^{+59.7}_{-55.6}$                         | $178.9^{+10.9}_{-29.4}$                  | 2                              |
| 144  | 2.295 | 591.2 <sup>+102.9</sup> <sub>-139.3</sub>      | 256.9 <sup>+156.3</sup> 256.9 <sup>+109.4</sup> | 573.6 <sup>+96.1</sup> <sub>-115.7</sub> | 2                              |
| 145  | 2.138 | 567.8 <sup>+14.7</sup> -14.9                   | $306.9^{+109.4}_{-79.5}$                        | $200.0^{+28.5}_{-28.4}$                  | 3                              |
| 158  | 1.477 | $91.0^{+46.0}_{-64.6}$                         | $145.1^{+83.4}_{-102.1}$                        | $127.0^{+46.0}_{-66.3}$                  | 3                              |
| 161  | 2.071 | $553.0^{+17.2}_{-19.5}$                        | $-193.4^{+346.4}_{-126.7}$                      | $-190.0^{+55.0}_{-17.4}$                 | 2                              |
| 181  | 1.678 | $274.9^{+13.3}_{-27.1}$                        | $273.3^{+71.8}_{-81.6}$                         | $272.6^{+13.5}_{-19.7}$                  | 4                              |
| 201  | 1.797 | $115.5^{+89.6}_{-54.4}$                        | $90.8^{+99.6}_{-131.3}$                         | $76.4^{+98.9}_{-101.7}$                  | 3                              |
| 231  | 1.646 | $212.8^{+16.6}_{-20.0}$                        | $-668.1^{+90.1}_{-84.1}$                        | $208.2^{+15.8}_{-26.9}$                  | 3                              |
| 237  | 2.394 | $169.4^{+22.4}_{-15.0}$                        | $-534.1^{+22.9}_{-22.9}$                        | $165.0^{+20.7}_{-14.5}$                  | 2                              |
| 245  | 1.677 | $286.6^{+61.4}_{-76.6}$                        | $60.1^{+64.9}_{-78.3}$                          | $284.6^{+39.4}_{-58.2}$                  | 2                              |
| 249  | 1.721 | $67.8^{+26.5}_{-8.3}$                          | $62.0^{+85.3}_{-36.8}$                          | $64.3^{+34.3}_{-5.5}$                    | 4                              |
| 256  | 2.247 | $139.5^{+52.9}_{-38.7}$                        | $140.0^{+159.0}_{-84.7}$                        | $151.6^{+34.7}_{-34.7}$                  | 5                              |
| 269  | 2.400 | $670.3_{-42.8}^{+8.0}$                         | $100.0^{+34.0}_{-47.9}$                         | $160.1^{+15.2}_{-12.5}$                  | 1                              |
| 275  | 1.580 | $209.1^{+21.0}_{-63.0}$                        | $198.0^{+25.8}_{-24.5}$                         | $156.6^{+4.9}_{-43.0}$                   | 5                              |
| 295  | 2.351 | $549.0^{+27.4}_{-17.9}$                        | $549.7^{+72.5}_{-62.7}$                         | $186.4^{+8.9}_{-21.9}$                   | 3                              |
| 298  | 1.633 | $279.5^{+49.3}_{-83.5}$                        | $216.6^{+169.9}_{-80.9}$                        | $299.9^{+27.4}_{-95.1}$                  | 4                              |
| 312  | 1.929 | $166.7^{+33.4}_{-19.5}$                        | $207.6^{+28.1}_{-22.4}$                         | $196.4^{+43.4}_{-29.1}$                  | 4                              |
| 332  | 2.580 | $292.1^{+20.0}_{-40.9}$                        | $299.9^{+83.3}_{-69.5}$                         | $292.8^{+12.3}_{-35.3}$                  | 4                              |
| 346  | 1.592 | $186.2^{+61.6}_{-29.3}$                        | $67.1^{+225.9}_{-111.9}$                        | $181.1^{+56.5}_{-30.2}$                  | 3                              |
| 362  | 1.857 | $224.9^{+17.9}_{-27.2}$                        | $227.9^{+36.8}_{-30.8}$                         | $218.6^{+16.9}_{-34.1}$                  | 2B                             |
| 386  | 1.862 | $109.4^{+37.7}_{-55.2}$                        | $103.1^{+32.9}_{-55.5}$                         | $104.5^{+40.8}_{-55.2}$                  | 2                              |
| 387  | 2.427 | $104.0^{+67.3}_{-11.7}$                        | $165.9^{+118.8}_{-118.1}$                       | $97.5^{+12.0}_{-15.8}$                   | 4                              |
| 389  | 1.851 | $639.5^{+20.3}_{-51.4}$                        | $99.1^{+21.8}_{-19.7}$                          | $149.6^{+31.9}_{-36.6}$                  | 2                              |
| 401  | 1.823 | $133.8^{+43.0}_{-25.0}$                        | $171.1^{+103.7}_{-41.5}$                        | $138.1^{+35.7}_{-29.8}$                  | 4                              |
| 408  | 1.742 | $487.9_{-20.5}^{+32.7}$                        | $460.8^{+62.4}_{-73.0}$                         | $-564.7_{-4.4}^{+3.7}$                   | 3B                             |
| 411  | 1.734 | $678.8^{+57.7}_{-106.6}$                       | $677.9^{+53.2}_{-111.0}$                        | $144.7^{+34.7}_{-19.4}$                  | 2                              |
| 418  | 1.419 | $199.6^{+66.9}_{-40.9}$                        | $141.8^{+124.9}_{-32.9}$                        | $203.1^{+28.9}_{-43.5}$                  | 4                              |
| 470  | 1.883 | $57.5^{+124.6}_{-11.4}$                        | $79.1^{+183.2}_{-50.8}$                         | $58.4^{+5.2}_{-7.1}$                     | 4                              |
| 485  | 2.557 | $474.3^{+80.5}_{-18.5}$                        | $494.0^{+39.0}_{-78.2}$                         | $476.3^{+83.3}_{-23.2}$                  | 3                              |
| 496  | 2.079 | $609.4^{+29.9}_{-20.2}$                        | $217.9^{+223.9}_{-76.0}$                        | $275.4^{+32.4}_{-103.1}$                 | 1                              |
| 499  | 2.327 | $560.8^{+67.8}_{-119.5}$                       | $544.1^{+123.1}_{-86.9}$                        | $289.6^{+106.4}_{-163.6}$                | 2                              |
| 506  | 1.753 | $637.6^{+36.5}_{-30.6}$                        | $60.1^{+19.7}_{-21.7}$                          | $142.2^{+25.3}_{-27.0}$                  | 1                              |
| 527  | 1.651 | $138.6^{+40.1}_{-32.3}$                        | $125.4^{+35.3}_{-71.7}$                         | $123.7^{+17.2}_{-64.7}$                  | 5                              |
| 549  | 2.277 | $228.9_{-23.6}^{+17.4}$                        | $225.7^{+103.6}_{-29.0}$                        | $229.2^{+25.5}_{-21.3}$                  | 4                              |
| 554  | 1.707 | $525.1^{+55.2}_{-33.0}$                        | $517.0_{-69.3}^{+91.7}$                         | $556.2^{+58.7}_{-44.1}$                  | 3                              |
| 562  | 2.773 | $597.9^{+68.7}_{-129.2}$                       | $642.0^{+37.9}_{-103.0}$                        | $45.2^{+150.2}_{-212.5}$                 | 2                              |
| 686  | 2.130 | $202.6_{-19.8}^{+39.4}$                        | $163.3^{+180.0}_{-153.5}$                       | $200.2^{+21.6}_{-20.2}$                  | 2                              |
| 689  | 2.007 | $474.0^{+68.7}_{-126.9}$                       | $317.1^{+131.7}_{-178.2}$                       | $120.8^{+27.5}_{-12.5}$                  | 2                              |
| 722  | 2.541 | $148.7^{+46.4}_{-46.6}$                        | $-711.1^{+43.6}_{-15.8}$                        | $193.5^{+34.1}_{-23.4}$                  | 1B                             |
| 734  | 2.324 | $289.9^{+46.1}_{-36.5}$                        | $225.9^{+127.1}_{-76.8}$                        | $288.0^{+47.3}_{-55.6}$                  | 5                              |
| 809  | 1.670 | $290.1^{+73.9}_{-135.3}$                       | $52.7^{+95.3}_{-161.3}$                         | 2.0 + 13.9                               | 1                              |
| 827  | 1.966 | 408.4 <sup>+54.4</sup> <sub>-57.6</sub>        | $38.3^{+73.2}_{-72.8}$                          | $-2.9_{-13.6}$<br>$81.8_{-17.6}^{+3.8}$  | 3                              |
|      | 1.700 | .00.1-5/.6                                     | 20.2-72.8                                       | 01.0-1/.0                                |                                |

#### Note.

affect our variability measurements, though the actual integrated emission-line flux measurements may be offset from the true values. However, BALs are a potential issue. When there

<sup>&</sup>lt;sup>a</sup> Lag quality rating (see Section 3.4). Quasars with significant BAL presence that affected our line width measurements (see Section 3.4.2) are identified with a "B" following their numerical rating.

are BALs superimposed on the C IV emission line, PrepSpec is often unable to correctly interpolate over the feature and the result is that the BAL is fit as part of the continuum or emission line.

BALs are known to be variable, and they may vary simultaneously with the continuum (e.g., Barlow 1993; Lundgren et al. 2007; Filiz Ak et al. 2013; Wang et al. 2015). This may cause a light curve to be biased toward zero (or at least shorter) lags. Though studies have generally avoided BALs that are superimposed onto emission lines, due to difficulties in disentangling the two, detached BALs that are at lower velocities have been reported to be less likely to vary than those at higher velocities (e.g., Capellupo et al. 2011; Filiz Ak et al. 2013, 2014). Low-velocity troughs are also sometimes highly saturated and thus have depths that are unaffected by quasar variability. Assuming that these trends hold true for BALs at low enough velocities to overlap with the emission lines, we can expect any effect on lag measurements to be minimal in our sample (and we find that, in most cases, we measure consistent lags both with and without masking out the BAL. However, an improper fit to the CIV line profile due to the presence of a BAL will result in incorrect line width measurements, both for the mean line profile and for the rms line profile. This will in turn affect our  $M_{\rm BH}$  measurements (see Section 4.3), which rely on accurate characterization of the line widths. Thus,  $M_{\rm BH}$  measurements for objects whose rms profile is significantly impacted by the fit around the BAL are potentially suspect, though we note that the uncertainties in the  $M_{\rm BH}$  measurements are large and the BALs may not cause deviations outside of the measurement uncertainties.

There were ten quasars in our lag-detected sample that have significant BAL components that overlap with the C IV emission line (see Figure 12). In these sources, we masked out the BAL region when fitting the spectra with PrepSpec. In three sources, we found that the C IV rms line profiles were too weak to reliably measure line widths; however, we were still able to measure a time lag in these sources. In Tables 3 and 4 and all subsequent figures, we flag these three quasars to indicate the higher uncertainty and potential for error in their measurements. In addition, the severity of the BAL contamination in all ten sources was taken into consideration when assigning the quality ratings that are reported in Table 3. These sources do not deviate systematically from the positions of the non-BAL quasars, which suggests that any effects of the BALs on our results are minimal.

#### 4. Results and Discussion

# 4.1. Lag Results

We identify significant positive lags in 48 quasars in our primary sample. Of these, 16 are deemed to be high-confidence lags that constitute our "gold sample" of lag detections. All 48 positive lag measurements that constitute our sample are listed in Table 3. Light curves, model fits, and posterior lag distributions are shown for all of our positive lag detections in Figure 8.

## 4.2. The C IV Radius-Luminosity Relation

To place our measurements on the C IV  $R_{\rm BLR}-L$  relationship, we measure  $\log \lambda L_{\lambda 1350}$ , the luminosity at 1350 Å, from the PrepSpec model fits. In our 10 lowest-redshift sources, 1350 Å was not covered by the spectrum; in these sources, we

measure the luminosity at 1700 Å and convert the values to  $\log \lambda L_{\lambda 1350}$  by multiplying  $L_{\lambda 1700}$  by factor of 1.09, which was computed from the mean quasar luminosities reported in Table 3 of Richards et al. (2006). The uncertainties on the luminosity measurements provided in Table 1 include only statistical uncertainties; due to the variability of the quasars, the actual uncertainties in the average quasar luminosities are somewhat higher. To quantify this additional source of uncertainty, we calculate the standard deviation in the flux at 1350 Å for our targets and add it to the statistical uncertainties.

Figure 9 shows the location of our sources on the  $R_{\rm BLR}-L$  relation. Previous recent measurements of the relation included only  $\sim\!15$  sources (Lira et al. 2018; Hoormann et al. 2019); our measurements raise this number to 63. In addition, our measurements span two orders of magnitude in luminosity in a region that was previously unpopulated on the C IV  $R_{\rm BLR}-L$  relation. In general, our measurements lie fairly close to the locations expected based on previously measured  $R_{\rm BLR}-L$  relations.

We use the LINMIX procedure described by Kelly (2007) to fit a new relationship including our new measurements, which includes a measurement of the intrinsic scatter of the relation. We fit the relation in the form

$$\log \frac{R_{\rm BLR}}{\text{(light-days)}} = a + b \times \log \frac{\lambda L_{\lambda} (1350 \,\text{Å})}{10^{44} \,\text{erg s}^{-1}} + \epsilon, \quad (2)$$

where  $\epsilon$  is the intrinsic random scatter of the relation. The resulting line fits are shown in Figure 9. Including our entire sample of significant lags, we measure a slope of  $b=0.51\pm$ 0.05, an intercept of  $a = 1.15 \pm 0.08$ , and an rms intrinsic scatter  $\langle \epsilon^2 \rangle^{1/2} = 0.15 \pm 0.03$ . Our measured slope is consistent with the most recent measurements by Lira et al. (2018) and Hoormann et al. (2019), though somewhat shallower than earlier measurements by Peterson et al. (2005) and Kaspi et al. (2007). In addition, our measured intercept is larger than that measured by Hoormann et al. (2019). Previous studies used a variety of methods to measure the line fit; for comparison purposes, we also fit our relation using the Bivariate Correlated Errors and Intrinsic Scatter (BCES) method (Akritas & Bershady 1996), implemented with the publicly available code of Nemmen et al. (2012). Results from the BCES method are consistent with those using LINMIX.<sup>32</sup>

Because our full sample likely includes some false-positive measurements, we also fit the relation while including only the measurements in our gold sample (see Section 3.4) and the previously reported measurements. We measure a slope of  $b=0.52\pm0.04$ , an intercept of  $a=0.92\pm0.08$ , and  $\langle\epsilon^2\rangle^{1/2}=0.11\pm0.04$ . The slope is consistent with that measured using our full sample, as well as with that measured by Hoormann et al. (2019) and Lira et al. (2018).

We caution that the fit of the  $R_{\rm BLR}-L$  relation here (and in earlier work) does not take into account selection effects in the sample, which have several effects on the appearance of the  $R_{\rm BLR}-L$  relation. For example, visual inspection suggests that there is some tension between our results and those at higher luminosities from Lira et al. (2018) and Hoormann et al. (2019); our measurements, when separated from the others, would

 $<sup>\</sup>overline{^{32}}$  Using the BCES method, we measure a slope of 0.49  $\pm$  0.08 and an intercept of 1.15  $\pm$  0.13.

Table 4 Line Width, Virial Product, and  $M_{\rm BH}$  Measurements

| RMID <sup>a</sup> | z     | τ <sub>final</sub> <sup>b</sup><br>(days) | $\sigma_{\text{line,mean}}$ (km s <sup>-1</sup> ) | $\sigma_{\text{line,rms}}$ $(\text{km s}^{-1})$ | FWHM <sub>mean</sub> (km s <sup>-1</sup> ) | FWHM <sub>rms</sub> (km s <sup>-1</sup> ) | $\begin{array}{c} \text{VP} \\ (10^7 \ M_{\odot}) \end{array}$ | $\frac{{M_{\rm BH}}^{\rm c}}{(10^7~M_\odot)}$   |
|-------------------|-------|---|---|---|--|---|--|---|
| 000               | 1.463 | $131.1^{+42.9}_{-36.6}$                   | $1807 \pm 106$                                    | $2144 \pm 46$                                   | $3509 \pm 74$                              | $4380 \pm 87$                             | $11.8^{+5.8}_{-5.4}$   | $52.6^{+25.9}_{-24.3}$                          |
| 032               | 1.720 | $22.8_{-3.6}^{+3.5}$                      | $1805\pm15$                                       | $2017 \pm 10$                                   | $2768\pm22$                                | $5010 \pm 20$                             | $1.8^{+0.7}_{-0.7}$  | $8.1^{+3.2}_{-3.2}$                             |
| 036               | 2.213 | $188.4^{+15.6}_{-29.0}$                   | $2905\pm19$                                       | $3900 \pm 34$                                   | $4906\pm18$                                | $7975 \pm 129$                            | $55.9^{+21.1}_{-22.3}$   | $249.9^{+94.4}_{-99.8}$                         |
| 052               | 2.311 | $56.5^{+3.1}_{-5.9}$                      | $1397\pm7$  | $1322\pm22$                                     | $3258 \pm 11$                              | $3354 \pm 67$                             | $1.9^{+0.7}_{-0.7}$  | $8.6^{+3.2}_{-3.3}$                             |
| 057               | 1.930 | $208.3^{+10.6}_{-5.6}$                    | $1592\pm7$  | $1682\pm12$                                     | $2652\pm8$                                 | $3944 \pm 25$                             | $11.5^{+4.3}_{-4.2}$   | $51.4^{+19.1}_{-19.0}$                          |
| 058               | 2.299 | $186.1^{+5.9}_{-7.4}$                     | $2695\pm24$                                       | $3412\pm30$                                     | $3564\pm95$                                | $7512\pm121$                              | $42.3^{+15.6}_{-15.7}$   | $189.0^{+69.9}_{-70.0}$                         |
| 130               | 1.960 | $224.3_{-37.9}^{+12.4}$                   | $4084\pm18$                                       | $4324\pm36$                                     | $5986\pm25$                                | $7923\pm44$                               | $81.8^{+30.5}_{-33.2}$   | $365.8^{+136.3}_{-148.2}$                       |
| 144               | 2.295 | $179.4^{+31.2}_{-42.3}$                   | $2830\pm14$                                       | $2792\pm19$                                     | $4419\pm39$                                | $7222\pm74$                               | $27.3^{+11.1}_{-11.0}$   | $122.0^{+49.7}_{-53.4}$                         |
| 145               | 2.138 | $180.9^{+4.7}_{-4.7}$                     | $3321\pm25$                                       | $3408\pm16$                                     | $5220\pm65$                                | $7976\pm41$                               | $41.0^{+15.1}_{-15.1}$   | $183.3^{+67.7}_{-67.7}$                         |
| 158               | 1.477 | $36.7^{+18.6}_{-26.1}$                    | $2043\pm74$                                       | $2136\pm31$                                     | $3621\pm80$                                | $4888\pm40$                               | $3.3^{+2.0}_{-2.6}$  | $14.6^{+9.1}_{-11.7}$                           |
| 161               | 2.071 | $180.1^{+5.6}_{-6.4}$                     | $2342\pm16$                                       | $2524\pm20$                                     | $2938 \pm 17$                              | $4950 \pm 38$                             | $22.4_{-8.3}^{+8.3}$   | $100.1^{+37.0}_{-37.0}$                         |
| 181               | 1.678 | $102.6^{+5.0}_{-10.1}$                    | $2116 \pm 49$                                     | $2721 \pm 34$                                   | $3024 \pm 32$                              | $4533 \pm 49$                             | $14.8^{+5.5}_{-5.7}$   | $66.3^{+24.6}_{-25.3}$                          |
| 201               | 1.797 | $41.3^{+32.0}_{-19.5}$                    | $1861 \pm 6$                                      | $2408 \pm 117$                                  | $5413 \pm 39$                              | $4061 \pm 44$                             | $4.7^{+4.0}_{-2.8}$  | $20.9_{-12.5}^{+17.9}$                          |
| 231               | 1.646 | $80.4_{-7.5}^{+6.3}$                      | $3326\pm49$                                       | $3803\pm18$                                     | $6496\pm56$                                | $11792 \pm 35$                            | $22.7^{+8.5}_{-8.6}$   | $101.5^{+38.2}_{-38.6}$                         |
| 237               | 2.394 | $49.9_{-4.4}^{+6.6}$                      | $2711 \pm 13$                                     | $2779 \pm 23$                                   | $5428 \pm 34$                              | $6442 \pm 30$                             | $7.5^{+2.9}_{-2.8}$  | $33.6^{+13.2}_{-12.7}$                          |
| 245               | 1.677 | $107.1^{+22.9}_{-28.6}$                   | $3910 \pm 61$                                     | $3953 \pm 86$                                   | $6847 \pm 64$                              | $7031 \pm 64$                             | $32.6_{-14.9}^{+13.9}$   | $145.9^{+62.2}_{-66.4}$                         |
| 249               | 1.721 | $24.9_{-3.1}^{+9.7}$                      | $1461 \pm 10$                                     | $1640 \pm 15$                                   | $2388 \pm 14$                              | $2601 \pm 29$                             | $1.3^{+0.7}_{-0.5}$  | $5.8^{+3.1}_{-2.3}$                             |
| 256               | 2.247 | $43.0^{+16.3}_{-11.9}$                    | $1720 \pm 22$                                     | $1802 \pm 24$                                   | $2440 \pm 39$                              | $3565 \pm 49$                             | $2.7^{+1.4}_{-1.3}$  | $12.2^{+6.4}_{-5.6}$                            |
| 269               | 2.400 | $197.2^{+2.4}_{-12.6}$                    | $2671 \pm 27$                                     | $3547 \pm 30$                                   | $3575 \pm 25$                              | $6937 \pm 99$                             | $48.4^{+17.8}_{-18.1}$   | $216.4_{-80.9}^{+79.8}$                         |
| 275               | 1.580 | $81.0^{+8.2}_{-24.4}$                     | $2077 \pm 27$<br>$2027 \pm 7$                     | $2406 \pm 5$                                    | $2992 \pm 12$                              | $6943 \pm 22$                             | $9.2^{+3.5}_{-4.4}$  | $40.9^{+15.6}_{-19.5}$                          |
| 295               | 2.351 | $163.8^{+8.2}_{-5.3}$                     | $2434 \pm 20$                                     | $2446 \pm 19$                                   | $4139 \pm 32$                              | $6402 \pm 41$                             | $19.1^{+7.1}_{-7.1}$   | 85.5 <sup>+31.8</sup> <sub>-31.6</sub>          |
| 298               | 1.633 | $106.1^{+18.7}_{-31.7}$                   | $2045 \pm 20$                                     | $2549 \pm 35$                                   | $3176 \pm 22$                              | $5177 \pm 51$                             | $13.5^{+5.5}_{-6.4}$   | $60.2^{+24.6}_{-28.5}$                          |
| 312               | 1.929 | 56.9 <sup>+11.4</sup>                     | $4289 \pm 33$                                     | $4291 \pm 30$                                   | $8553 \pm 89$                              | $10248 \pm 53$                            | $20.5^{+8.6}_{-7.9}$   | $91.4^{+38.3}_{-35.3}$                          |
| 332               | 2.580 | $81.6^{+5.6}_{-11.4}$                     | $2945 \pm 100$                                    | $4277 \pm 33$                                   | $3813 \pm 290$                             | $7828 \pm 32$                             | $29.1^{+10.9}_{-11.5}$   | $130.2^{+48.8}_{-51.3}$                         |
| 346               | 1.592 | $71.9^{+23.8}_{-11.3}$                    | $2183 \pm 33$                                     | $3055 \pm 29$                                   | $3385 \pm 54$                              | $5864 \pm 57$                             | $13.1^{+6.5}_{-5.2}$   | $58.5^{+29.0}_{-23.4}$                          |
| 362*              | 1.857 | $78.7^{+6.3}_{-9.5}$                      | $3541 \pm 39$                                     | $4326 \pm 44$                                   | $5829 \pm 42$                              | $12041 \pm 151$                           | $28.7^{+10.8}_{-11.1}$   | $128.5^{+48.4}_{-49.8}$                         |
| 386               | 1.862 | $38.2^{+13.2}_{-19.3}$                    | $1839 \pm 26$                                     | $2187 \pm 41$                                   | $2935 \pm 31$                              | $3756 \pm 70$                             | $3.6^{+1.8}_{-2.2}$  | $15.9^{+8.0}_{-10.0}$                           |
| 387               | 2.427 | $30.2_{-19.3}$<br>$30.3_{-3.4}^{+19.6}$   | $2181 \pm 11$                                     | $2451 \pm 23$                                   | $3733 \pm 31$<br>$3733 \pm 18$             | $4797 \pm 30$                             | $3.6^{+2.6}_{-1.4}$  | $15.9^{+11.8}_{-6.1}$                           |
| 389               | 1.851 | $224.3_{-18.0}^{+7.1}$                    | $3790 \pm 12$                                     | $4064 \pm 15$                                   | $5014 \pm 49$                              | $7740 \pm 27$                             | $72.3^{+26.7}_{-27.3}$   | $323.2^{+119.5}_{-121.9}$                       |
| 401               | 1.823 | $47.4^{+15.2}_{-8.9}$                     | $2517 \pm 9$                                      | $3321 \pm 12$                                   | $3754 \pm 19$                              | $10120 \pm 497$                           | $10.2^{+5.0}_{-4.2}$   | $45.6^{+22.3}_{-18.8}$                          |
| 408*              | 1.742 | $177.9^{+11.9}_{-7.5}$                    | $2517 \pm 9$<br>$2519 \pm 22$                     | $3321 \pm 12$<br>$3872 \pm 29$                  | $4130 \pm 159$                             | $9227 \pm 536$                            | $52.1^{+19.5}_{-19.3}$   | $43.0_{-18.8}$ $232.7_{-86.3}^{+87.1}$          |
| 411               | 1.742 | $248.3_{-39.0}^{+21.1}$                   | $2379 \pm 22$<br>$2375 \pm 36$                    | $3872 \pm 29$<br>$2490 \pm 39$                  | $3535 \pm 35$                              | $6024 \pm 70$                             | $32.1_{-19.3}$ $30.0_{-12.0}^{+11.4}$                          |   |
| 411               | 1.734 | $82.5^{+27.6}_{-16.9}$                    | $2542 \pm 23$                                     | $2490 \pm 39$<br>$3110 \pm 23$                  | $2952 \pm 22$                              | $6024 \pm 70$<br>$6159 \pm 44$            | $15.6^{+7.8}_{-6.6}$   | $134.3^{+50.8}_{-53.8} \\ 69.6^{+34.7}_{-29.3}$ |
| 470               |       |   |   | $2317 \pm 60$                                   | $2932 \pm 22$<br>$3957 \pm 46$             |   |  |   |
|                   | 1.883 | $19.9^{+43.2}_{-4.0}$                     | $2401 \pm 31$                                     |   |  | $5028 \pm 70$                             | $2.1^{+4.6}_{-0.9}$  | $9.3^{+20.5}_{-3.9}$                            |
| 485               | 2.557 | $133.4^{+22.6}_{-5.2}$                    | $2919 \pm 26$                                     | $3961 \pm 41$                                   | $5422 \pm 37$                              | $8535 \pm 82$                             | $40.8^{+16.6}_{-15.1}$   | $182.5^{+74.0}_{-67.6}$                         |
| 496               | 2.079 | $197.9^{+9.7}_{-6.6}$                     | $2076 \pm 29$                                     | $2409 \pm 45$                                   | $2477 \pm 38$                              | $5620 \pm 73$                             | $22.4^{+8.3}_{-8.3}$   | $100.2^{+37.2}_{-37.1}$                         |
| 499               | 2.327 | $168.5^{+20.4}_{-35.9}$                   | $3007 \pm 32$                                     | $3085 \pm 26$                                   | $3233 \pm 33$                              | $6371 \pm 49$                             | 31.3 <sup>+12.1</sup> <sub>-13.3</sub>                         | 139.9+54.3                                      |
| 506               | 1.753 | $231.6^{+13.3}_{-11.1}$                   | $3378 \pm 24$                                     | $3510 \pm 24$                                   | $4174 \pm 21$                              | $9354 \pm 35$                             | $55.7^{+20.8}_{-20.7}$   | 248.9 <sup>+92.8</sup>                          |
| 527               | 1.651 | $52.3_{-12.2}^{+15.1}$                    | $3380 \pm 55$                                     | $3587 \pm 34$                                   | $5263 \pm 106$                             | $8306 \pm 53$                             | $13.1^{+6.1}_{-5.7}$   | $58.7^{+27.5}_{-25.6}$                          |
| 549               | 2.277 | $69.8^{+5.3}_{-7.2}$                      | $1840 \pm 64$                                     | $2176 \pm 21$                                   | $4081 \pm 54$                              | $4995 \pm 53$                             | $6.5^{+2.4}_{-2.5}$  | $28.8^{+10.9}_{-11.0}$                          |
| 554               | 1.707 | $194.0^{+20.4}_{-12.2}$                   | $2286 \pm 29$                                     | $2229 \pm 35$                                   | $3636 \pm 37$                              | 5609 ± 52                                 | $18.8^{+7.2}_{-7.0}$   | 84.1+32.2                                       |
| 562               | 2.773 | $158.5^{+18.2}_{-34.2}$                   | $2034 \pm 21$                                     | $2078 \pm 27$                                   | $4544 \pm 47$                              | $5189 \pm 37$                             | $13.4^{+5.2}_{-5.7}$   | $59.7^{+23.0}_{-25.5}$                          |
| 686               | 2.130 | $64.7^{+12.6}_{-6.3}$                     | $2126\pm20$                                       | $2203 \pm 27$                                   | $3839 \pm 26$                              | $4847\pm37$                               | $6.1^{+2.6}_{-2.3}$  | $27.4^{+11.4}_{-10.4}$                          |
| 689               | 2.007 | $157.6^{+22.9}_{-42.2}$                   | $1281\pm7$  | $1407\pm5$                                      | $2253 \pm 17$                              | $2791 \pm 17$                             | $6.1^{+2.4}_{-2.8}$  | $27.2^{+10.8}_{-12.4}$                          |
| 722*              | 2.541 | $42.0^{+13.1}_{-13.2}$                    | $3560 \pm 108$                                    | $8571 \pm 122$                                  | $6892 \pm 62$                              | $17233 \pm 4743$                          | $60.2^{+29.1}_{-29.1}$   | $269.1^{+130.0}_{-130.1}$                       |
| 734               | 2.324 | $87.2^{+13.9}_{-11.0}$                    | $2978\pm50$                                       | $3405\pm40$                                     | $6296\pm103$                               | $7042\pm65$                               | $19.7^{+7.9}_{-7.7}$   | $88.2^{+35.4}_{-34.4}$                          |
| 809               | 1.670 | $108.6^{+27.7}_{-50.7}$                   | $4748\pm42$                                       | $4749\pm96$                                     | $11172\pm92$                               | $11743 \pm 700$                           | $47.8^{+21.4}_{-28.4}$   | $213.7^{+95.7}_{-127.0}$                        |
| 827               | 1.966 | $137.7^{+18.3}_{-19.4}$                   | $995 \pm 9$                                       | $1443\pm13$                                     | $2772\pm19$                                | $2393\pm134$                              | $5.6^{+2.2}_{-2.2}$  | $25.0^{+9.8}_{-9.9}$                            |

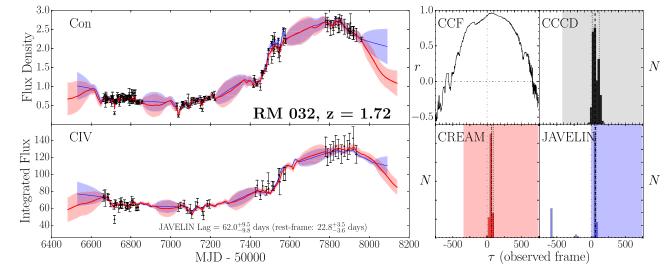
## Notes.

indicate a steeper slope of the relation. This tension is due to a selection effect: none of these studies is capable of measuring rest-frame lags in the 800-1000 days range within their quasar sample. Thus, the highest-luminosity end of this relation cannot currently include measurements above the measured relation and must be composed only of measurements that scatter below the

<sup>&</sup>lt;sup>a</sup> Quasars with significant BAL inference on the C IV emission line (see Section 3.4.2) are flagged with an asterisk. These sources may have incorrect line width measurements.

b Measurements are in the quasar rest frame.

<sup>&</sup>lt;sup>c</sup> Virial products were converted to  $M_{\rm BH}$  using f=4.47, as measured by Woo et al. (2015).



**Figure 8.** Light curves and posterior distributions for the quasars with significant C IV lags in our primary lag sample. The two left panels show the continuum (top) and C IV (bottom) light curves: black points are the data, blue lines show the JAVELIN model fit to the data (with the uncertainties shown as a blue envelope), and red lines show the CREAM model fit (with uncertainties shown as a red/pink envelope). For visualization purposes, data points within a single night were combined using a weighted average. Continuum flux density is provided in units of  $10^{-17}$  erg s<sup>-1</sup> cm<sup>-2</sup> Å<sup>-1</sup>, and integrated emission-line fluxes in units of  $10^{-17}$  erg s<sup>-1</sup> cm<sup>-2</sup>. The right panels indicate the time series analysis results: the top panels show the CCF (left) and CCCD (right), and the bottom panels show the CREAM and JAVELIN posterior distributions (left and right, respectively). The measured lag and its uncertainties are indicated as dashed and dotted lines, and the shaded regions indicate the range of lags considered in the final measurement, as per our alias rejection procedure. Figures for all of our significant lag detections are provided in the figure set. Sources that are affected by BALs (see Section 3.4.2) are flagged with red "BAL" text in the bottom-left panel.

(The complete figure set (48 images) is available.)

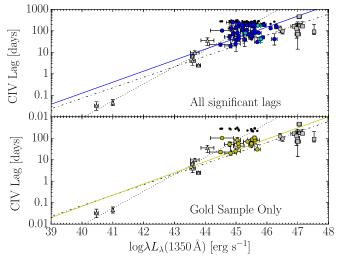


Figure 9. The CIV  $R_{\rm BLR}-L$  relation. Gray solid triangles represent measurements from Peterson et al. (2004), who reanalyzed C IV data from Reichert et al. (1994), Rodriguez-Pascual et al. (1997), Korista et al. (1995), O'Brien et al. (1998), and Wanders et al. (1997), and additional measurements from Peterson et al. (2005), and Kaspi et al. (2007). Gray squares represent data from Lira et al. (2018), and gray circles indicate the two measurements from Hoormann et al. (2019). The dashed black lines show the best-fit line from Peterson et al. (2005), while the dashed-dotted black lines indicate the most recent best-fit line from Hoormann et al. (2019). In the top panel, the blue filled circles represent all of our significant lag measurements and the blue solid line indicates the measured  $R_{\rm BLR}-L$  relation from the entire sample. In the bottom panel, the yellow filled circles represent only our measurements that we placed in the gold sample, and the yellow solid line represents the measured  $R_{\rm BLR}-L$ relation while including only gold-sample measurements. Cyan filled circles indicate sources that are affected by BALs (see Section 3.4.2). Black solid dots represent a 750 days observed-frame lag cutoff at the redshift of each of our sources; i.e., each of our measurements has a corresponding black dot that shows the longest lag we could have detected with our campaign at that quasar's redshift (see text in Section 4.2).

relation. To fully address this issue, we require additional data for such high-luminosity sources from campaigns with extended time baselines.

Similarly, our study is unable to detect lags longer than  $\sim$ 750 observed-frame days. At the luminosities of most of our sources, this is long enough for us to detect lags. However, at the high-luminosity end of our sample ( $\log \lambda_{L\lambda} > 45.5$ ), the expected rest-frame time lags based on the  $R_{\rm BLR}-L$  relation are on par with the rest-frame time lag threshold for the range of redshifts of our sample. It is thus likely that we are missing some of the lags at the high-luminosity end of our sample range, due to their likely scatter above the relation (and thus above our detection threshold; this causes the apparent "flattening" effect that is visible when considering only our measurements). However, the finite observation baseline is unlikely to be affecting the detected lag measurements themselves; Figure 9 shows that the majority of our measurements fall well below the rest-frame equivalent of our 750 days detection threshold (for example, 750 observed-frame days translates to 250 rest-frame days for a quasar at a redshift of 2). This suggests that our lag measurements themselves are unlikely to be biased low due to the observed-frame lag detection limit of 750 days; if this were the case, we would expect many of our measurements to lie close to the upper detection limit. While a more detailed treatment/investigation of these issues is beyond the scope of this work, Li et al. (2019) and Fonseca Alvarez et al. (2019) have investigated this issue for the H $\beta$ -detected lag sample using simulations, and both studies come to similar conclusions regarding selection effects for H $\beta$  lag measurements.

Future high-luminosity measurements from data spanning long timescales will continue to shed light on the slope and scatter of the relation; however, the lack of measurements at the low-luminosity end is also problematic. The only two measurements in

sources with luminosities below  $10^{43}$  erg s<sup>-1</sup> lie below our measured relation. It could be that these measurements are consistent with the relation to within the expected intrinsic scatter; additionally, there may be an intrinsic difference in the accretion and/or line-emission region between low-luminosity sources and the high-luminosity quasars that populate much of the relation. Future RM experiments in the UV focused on local, low-luminosity AGNs would be greatly beneficial in determining whether this is the case, as well as in more concretely constraining the slope of this relation.

A more detailed quantification of the selection effects on the measured  $R_{\rm BLR}-L$  relation is beyond the scope of this paper, and will be investigated with future SDSS-RM work that specifically focuses on the  $R_{\rm BLR}-L$  relation using simulations similar to those performed by Li et al. (2019) and Fonseca Alvarez et al. (2019). For this reason, the preliminary C IV  $R_{\rm BLR}-L$  relation presented here is primarily used as a sanity check on the bulk reliability of our C IV lags, and we do not recommend its usage for other applications (e.g., SE masses).

#### 4.3. Black Hole Mass Measurements

For each quasar, we measure  $M_{\rm BH}$  with Equation (1) using our adopted rest-frame time lags from JAVELIN and line widths measured by PrepSpec during the fitting process. We adopt  $\sigma_{\mathrm{line,rms}}$  as our line width measurement to compute the virial product, as past studies (e.g., Peterson 2011) have suggested that  $\sigma_{\text{line,rms}}$  is a less biased estimator for  $M_{\text{BH}}$  than the FWHM, for a number of reasons. For example, the relationship between FWHM and  $\sigma_{line}$  is not linear, which can cause the underestimation of low masses and the overestimation of high masses when FWHM is used. In addition, FWHM measurements can often be significantly affected by narrow line components; see, e.g., Wang et al. (2019) for a recent discussion on this topic. However, this issue is still in contention, so we include several different characterizations of line width in Table 4. We again note that some of our objects have significant BAL contamination that has affected the PrepSpec fits (see Section 3.4.2); we flag such cases in Table 4 and caution that  $M_{\rm BH}$  measurements for these sources may be

When calculating the uncertainties in the virial products, we follow G17 and add a 0.16 dex uncertainty in quadrature to the statistical uncertainties (which are calculated via standard propagation) to account for systematic uncertainties that have not been taken into account, following the 0.16 dex standard deviation among the many different mass determinations of NGC 5548 (Fausnaugh et al. 2017). To convert the virial products into  $M_{\rm BH}$ , we adopt f=4.47 (Woo et al. 2015). All virial products and  $M_{\rm BH}$  measurements are provided in Table 4. Our  $M_{\rm BH}$  measurements range from about  $10^8$  to  $10^{10}$  solar masses, and are among the most massive SMBHs to have RM mass measurements (see Figure 10).

Figure 11 compares our RM  $M_{\rm BH}$  measurements with SE  $M_{\rm BH}$  estimates from Shen et al. (2019b). We add systematic uncertainties of 0.4 dex to the SE measurements to the measurement uncertainties in the Shen et al. (2019b) values (e.g., Vestergaard & Peterson 2006; Shen 2013). The SE and RM measurements are largely consistent within their (large) uncertainties for many quasars; however, there is noticeable scatter around a one-to-one relation. Our C IV lags are consistent with the previously measured  $R_{\rm BLR}-L$  relation from

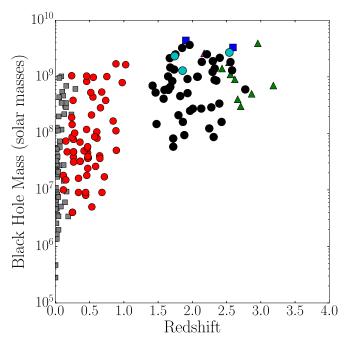


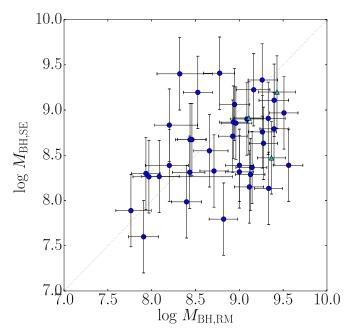
Figure 10. Black hole mass vs. redshift for reverberation-mapped AGNs. Gray squares represent H $\beta$  RM measurements, made prior to the SDSS-RM program, by Bentz & Katz (2015) with additions from Du et al. (2016a). Red circles indicate SDSS-RM measurements made using the H $\beta$  emission line by G17. Blue solid squares are C IV measurements by Hoormann et al. (2019), solid green triangles are C IV measurements by Lira et al. (2018), the solid magenta triangle is from Kaspi et al. (2007), and solid black circles represent C IV measurements from this work. Cyan circles indicate sources from this work that are affected by BALs (see Section 3.4.2).

which the SE estimators are derived, so we are unsurprised to see so many that are consistent; however, given the uncertainties around C IV SE  $M_{\rm BH}$  estimates (see Section 1), we are also unsurprised to see cases with inconsistencies. A detailed analysis of the reliability of SE mass measurements is beyond the scope of this work, but will be addressed thoroughly in future work dedicated to improving SE mass estimators.

#### 5. Summary

With four years of spectroscopic and photometric data from the SDSS-RM program, we searched for time delays between the continuum and the C IV emission-line in 348 quasars. Our main results are:

- 1. We measured significant positive lags in 48 quasars, with an expected false-positive detection rate of 10%. Lowering the false-positive rate threshold will yield more significant positive lags, but with increased false positives; including additional years of SDSS-RM monitoring will likely decrease the false-positive rate and lead to a larger set of lags (see Section 3.3).
- 2. We assigned quality ratings to each individual measurement, based on visual inspections. This led us to create a "gold sample" of 16 of our highest-confidence lag measurements (see Section 3.4). These measurements are consistent with the larger primary sample of 48 quasars, but are less likely to be false positives and so are the best sources for targeted follow-up of individual



**Figure 11.** Single-epoch  $M_{\rm BH}$  estimates from Shen et al. (2019b), compared to our new RM measurements. Filled blue circles represent sources without BAL contamination, and filled cyan triangles indicate sources with BALs (see Section 3.4.2). The SE values were computed using estimators from Vestergaard & Peterson (2006). We have increased the statistical uncertainties on the SE masses by 0.4 dex (see Section 4.3), to account for systematic uncertainties. The gray dotted line shows a 1:1 ratio.

quasars. We note again that the criteria used to determine this sample are subjective, and thus we caution against statistical interpretations using the gold sample.

- 3. We place our measurements on the C IV  $R_{\rm BLR}-L$  relation. They fill in a previously unexplored range of luminosities, and increase the number of sources included from 15–18 to  $\sim$ 65 (Section 4.2). We fit a new relation to our data while including the entire set of C IV RM results from the literature, and find a relation consistent with previous studies. We separately fit only the gold sample together with previous measurements, and measure a consistent relation. We caution that selection effects must be addressed before this relation can be widely used for other applications (such as designing SE mass recipes).
- 4. We use our time-lag measurements to obtain  $M_{\rm BH}$  measurements for our full sample of lags (see Section 4.3). These  $M_{\rm BH}$  values are at the high end of the distribution of RM mass measurements.
- 5. We have increased the sample of quasars with C IV RM lag measurements from  $\sim 18$  to  $\sim 65$ , adding quasars at redshifts ranging from 1.35 to 2.8. This is a significant increase in both sample size and redshift range spanned by the RM sample, demonstrating the utility of multi-object RM campaigns in expanding the parameter space covered by RM observations.

We have shown here that RM measurements in quasars at higher redshifts and higher luminosities are possible, using large survey-based data sets such as ours that span multiple years. Our work makes use of four years of spectroscopic monitoring with SDSS combined with accompanying photometry from the Bok and CFHT telescopes. The SDSS-RM program will continue to observe through 2020 as a part of the SDSS-IV program, and RM monitoring will continue through 2025 as a part of the SDSS-V Black Hole Mapper program (Kollmeier et al. 2017). The additional years of data will allow us to measure lags in quasars at higher luminosities and explore the SMBH population at unprecedented scales. In addition, we are also adding 4 yr PanSTARRS1 early light curves (2010–2014) for SDSS-RM quasars to effectively extend the baseline to measure longer lags (Shen et al. 2019a).

Beyond the SDSS-RM program and the upcoming Black Hole Mapper survey, there are several additional surveys and facilities that are planning or currently executing large RM programs using multiobject spectrographs, such as OzDES (King et al. 2015), 4MOST (Swann et al. 2019), and the Maunakea Spectroscopic Explorer (McConnachie et al. 2016). The SDSS-RM program, and our results here, serve as a proof-of-concept that such programs are not only feasible, but can have a dramatic impact on our knowledge of quasars and SMBHs across the observable universe.

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# **Appendix**

Here, we present the mean and rms spectra for our sample of significantly detected lags (Figure 12). In addition, we provide all of the measured quantities used as lag significance criteria for our entire quasar sample (Table 5).

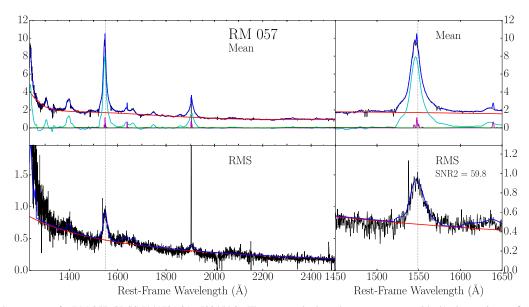


Figure 12. Mean and rms spectra for RM 057 (SDSS J141721.81+530454.3). The top panels show the mean spectrum (black), the continuum fit to the mean (red), the full model fit to the C IV emission line (blue), the BLR model (cyan), the Fe II model (green), and the narrow-line region model (magenta). The bottom panels show the rms spectra (black), the rms model (blue), and the continuum fit to the rms spectrum (red). Flux densities are in units of  $10^{-17}$  erg s<sup>-1</sup> cm<sup>-2</sup> Å<sup>-1</sup>. The left panels show a large portion of the observed spectrum, and the right panels show only the C IV emission-line region. Vertical dotted black lines indicate the rest-frame wavelength of the C IV emission line. Plots for all 48 of our quasars with C IV lag detections are provided in the figure set.

(The complete figure set (48 images) is available.)

Table 5
Observed-frame Lag Measurements and Significance Parameters for the Entire Sample

Table 5 (Continued)

|      |  | Sample               | <del></del> _ |                    |                     | -          | _   | E4!                  |               |                 |                     |
|------|--|----------------------|---------------|--------------------|---------------------|------------|---|----------------------|---------------|-----------------|---------------------|
| RMID | $	au_{ m JAV} \  m (days)$               | Fraction<br>Rejected | $r_{ m max}$  | S/N <sub>con</sub> | S/N <sub>line</sub> | RMID       | $	au_{ m JAV} 	ag{days}$  | Fraction<br>Rejected | $r_{\rm max}$ | $\rm S/N_{con}$ | S/N <sub>line</sub> |
| 000  | 322.8 <sup>+105.6</sup> <sub>-90.1</sub> | 0.23                 | 0.54          | 18.00              | 2.72                | 144        | $591.2^{+102.9}_{-139.3}$   | 0.13                 | 0.54          | 8.50            | 2.11                |
| 004  | $194.2^{+34.5}_{-23.5}$                  | 0.23                 | 0.54          | 8.00               | 0.54                | 145        | $567.8^{+14.7}_{-14.9}$   | 0.09                 | 0.79          | 21.00           | 3.92                |
| 006  | $-124.1^{+81.1}_{-139.8}$                | 0.07                 | 0.40          | 15.00              | 1.22                | 149        | $-131.5^{+65.4}_{-41.1}$  | 0.44                 | 0.33          | 9.00            | 1.42                |
| 011  | $245.4^{+89.1}_{-134.7}$                 | 0.61                 | 0.40          | 14.00              | 0.00                | 150        | $543.9^{+45.7}_{-31.1}$   | 0.35                 | 0.57          | 15.00           | 1.65                |
| 012  | $13.9^{+19.3}_{-137.5}$                  | 0.09                 | 0.43          | 11.00              | 2.95                | 153        | $557.7^{+72.7}_{-99.6}$   | 0.27                 | 0.56          | 10.00           | 0.00                |
| 013  | $-430.1^{+55.6}_{-39.6}$                 | 0.70                 | 0.46          | 7.00               | 0.56                | 154        | $-566.6^{+7.7}_{-5.7}$  | 0.09                 | -0.24         | 12.00           | 4.35                |
| 019  | $-124.1^{+117.9}_{-149.8}$               | 0.20                 | 0.44          | 6.00               | 1.04                | 155        | $498.8^{+114.3}_{-69.2}$  | 0.04                 | 0.38          | 12.00           | 0.51                |
| 024  | $524.9^{+112.3}_{-103.4}$                | 0.25                 | 0.48          | 11.00              | 2.93                | 156        | 498.8 <sup>+114.3</sup><br>498.8 <sup>+54.6</sup><br>555.6 <sup>+54.6</sup><br>118.0 <sup>+16.2</sup><br>118.0 <sup>+16.2</sup> | 0.21                 | 0.43          | 11.00           | 0.78                |
| 025  | $343.3^{+47.6}_{-69.9}$                  | 0.27                 | 0.72          | 7.00               | 1.44                | 157        | $118.0^{+16.2}_{-12.5}$   | 0.46                 | 0.31          | 9.50            | 1.55                |
| 028  | $157.7^{+47.8}_{-46.3}$                  | 0.13                 | 0.40          | 13.29              | 3.62                | 158        | $91.0^{+46.0}_{-64.6}$  | 0.10                 | 0.68          | 12.00           | 2.08                |
| 031  | $162.2^{+105.9}_{-123.8}$                | 0.06                 | 0.74          | 12.00              | 1.18                | 159        | $517.2^{+36.2}_{-15.8}$   | 0.31                 | 0.43          | 10.00           | 2.99                |
| 032  | $62.0_{-9.8}^{+9.5}$                     | 0.23                 | 0.96          | 16.00              | 4.84                | 161        | $553.0^{+17.2}_{-19.5}$   | 0.29                 | 0.54          | 7.50            | 2.56                |
| 034  | $396.5^{+132.3}_{-154.9}$                | 0.06                 | 0.39          | 14.00              | 2.33                | 164        | $598.5^{+18.3}_{-36.5}$   | 0.25                 | 0.41          | 0.00            | 4.89                |
| 035  | $102.9^{+110.4}_{-13.1}$                 | 0.06                 | 0.81          | 16.00              | 1.17                | 172        | 88.1 <sup>+411.2</sup> <sub>-108.5</sub>  | 0.27                 | 0.64          | 12.75           | 0.00                |
| 036  | $605.2^{+50.1}_{-93.1}$                  | 0.06                 | 0.56          | 11.25              | 4.01                | 176        | $-689.4^{+28.5}_{-28.3}$  | 0.29                 | 0.31          | 13.00           | 0.59                |
| 038  | $-472.7^{+151.4}_{-115.3}$               | 0.42                 | 0.42          | 11.00              | 0.00                | 178        | $329.7^{+277.4}_{-55.5}$  | 0.10                 | 0.44          | 11.50           | 2.86                |
| 039  | $-577.2^{+34.7}_{-49.6}$                 | 0.49                 | 0.69          | 0.00               | 4.75                | 179        | $-610.8^{+27.7}_{-22.2}$  | 0.65                 | 0.14          | 12.00           | 0.00                |
| 041  | $28.2^{+52.4}_{-15.6}$                   | 0.01                 | 0.70          | 15.67              | 1.58                | 180        | $-437.3^{+31.6}_{-57.9}$  | 0.64                 | 0.13          | 11.00           | 1.82                |
| 045  | $-82.2^{+142.1}_{-73.4}$                 | 0.00                 | 0.41          | 0.00               | 1.79                | 181        | $274.9^{+13.3}_{-27.1} 228.2^{+191.3}_{-19.8}$  | 0.13                 | 0.72          | 13.00           | 3.38                |
| 049  | $-412.9^{+48.8}_{-79.7}$                 | 0.50                 | 0.46          | 11.00              | 0.05                | 182        | $228.2_{-19.8}^{+191.3}$  | 0.05                 | 0.56          | 26.00           | 1.53                |
| 051  | 535.6 <sup>+8.5</sup> <sub>-8.3</sub>    | 0.32                 | 0.30          | 7.50               | 3.54                | 186        | $623.6^{+67.4}_{-111.5}$  | 0.55                 | 0.24          | 9.00            | 2.46                |
| 052  | $187.1^{+10.4}_{-19.4}$                  | 0.29                 | 0.51          | 9.50               | 3.42                | 190        | $-200.7^{+4.9}_{-4.9}$  | 0.71                 | 0.60          | 9.00            | 5.41                |
| 055  | $698.9^{+41.7}_{-161.7}$                 | 0.31                 | 0.71          | 10.00              | 0.00                | 194        | $80.2^{+29.8}_{-7.2}$   | 0.80                 | 0.87          | 21.00           | 1.19                |
| 057  | $610.4^{+31.2}_{-16.5}$                  | 0.37                 | 0.57          | 11.67              | 2.46                | 196        | $-538.8^{+24.0}_{-29.8}$  | 0.47                 | 0.23          | 6.00            | 0.00                |
| 058  | $614.0^{+19.5}_{-24.4}$                  | 0.31                 | 0.58          | 9.00               | 3.05                | 201        | 115.5 <sup>+89.6</sup> -54.4  | 0.01                 | 0.72          | 16.50           | 3.23                |
| 059  | $219.9^{+89.0}_{-26.4}$                  | 0.63                 | 0.38          | 15.33              | 0.16                | 202        | $495.7^{+28.0}_{-29.5}$   | 0.36                 | 0.37          | 14.00           | 2.68                |
| 063  | $509.5^{+72.2}_{-46.0}$                  | 0.47                 | 0.55          | 0.00               | 1.92                | 205        | $484.6^{+31.0}_{-51.9}$   | 0.10                 | 0.29          | 21.00           | 4.11                |
| 064  | $627.3^{+21.6}_{-52.6}$                  | 0.04                 | 0.42          | 7.50               | 2.14                | 207        | $-718.6^{+35.3}_{-18.6}$  | 0.60                 | 0.74          | 14.50           | 2.37                |
| 065  | $316.6^{+30.1}_{-58.5}$                  | 0.09                 | 0.53          | 9.00               | 1.66                | 208        | $-144.6^{+42.5}_{-49.5}$  | 0.61                 | 0.38          | 3.00            | 2.80                |
| 066  | $-604.9^{+10.9}_{-17.0}$                 | 0.70                 | -0.04         | 23.00              | 4.97                | 210        | $154.7^{+223.1}_{-232.6}$   | 0.42                 | 0.24          | 9.00            | 0.00                |
| 069  | $155.5^{+193.8}_{-88.1}$                 | 0.06                 | 0.34          | 11.00              | 1.11                | 213        | 269.9 <sup>+182.0</sup> 572.0 <sup>+42.3</sup>  | 0.34                 | 0.29          | 0.00            | 1.57                |
| 071  | $554.1^{+83.8}_{-107.1}$                 | 0.06                 | 0.65          | 12.25              | 1.54                | 216        | $573.0^{+42.3}_{-51.4}$   | 0.04                 | 0.36          | 14.00           | 2.01                |
| 072  | $22.0_{-194.3}^{+34.3}$                  | 0.09                 | 0.50          | 12.50              | 1.71                | 217        | $40.8^{+142.9}_{-23.9}$   | 0.49                 | 0.49          | 6.50            | 2.51                |
| 075  | $-179.3^{+298.9}_{-142.1}$               | 0.09                 | 0.37          | 12.50              | 1.55                | 218<br>220 | $233.3_{-52.5}^{+73.1} \\ 11.8_{-107.7}^{+129.4}$   | 0.42<br>0.57         | 0.45<br>0.47  | 11.00           | 0.00<br>0.97        |
| 076  | $218.8^{+17.7}_{-16.8}$                  | 0.57                 | 0.59          | 14.50              | 4.86                | 222        | $624.5_{-40.7}^{+45.6}$   | 0.37                 | 0.47          | 13.00           | 0.97                |
| 079  | $-330.9^{+13.0}_{-16.9}$                 | 0.26                 | 0.41          | 14.00              | 2.04                | 225        | $59.5^{+35.7}_{-29.2}$  | 0.11                 | 0.73          | 16.00<br>9.00   | 1.75                |
| 080  | $547.1^{+50.7}_{-31.3}$                  | 0.64                 | 0.44          | 7.50               | 3.98                | 226        | 9.5 <sub>-29.2</sub><br>9.5+85.5  | 0.20                 | 0.59          | 1.50            | 1.75                |
| 081  | $-167.7^{+105.2}_{-46.0}$                | 0.41                 | 0.59          | 12.50              | 0.21                | 227        | $-8.5^{+85.5}_{-124.5}$ $652.2^{+11.6}_{-9.1}$  | 0.54                 | 0.53          | 10.50           | 2.81                |
| 086  | $-577.1^{+13.4}_{-10.0}$                 | 0.58                 | 0.24          | 23.00              | 3.29                | 230        | $202.3_{-40.2}^{+67.2}$   | 0.09                 | 0.33          | 16.50           | 1.40                |
| 087  | $143.1^{+137.3}_{-66.6}$                 | 0.68                 | 0.23          | 7.00               | 0.00                | 231        | $212.8^{+16.6}_{-20.0}$   | 0.47                 | 0.54          | 17.00           | 4.71                |
| 092  | $172.4^{+14.9}_{-17.8}$                  | 0.20                 | 0.47          | 20.00              | 1.00                | 237        | $169.4^{+22.4}_{-15.0}$   | 0.40                 | 0.59          | 20.00           | 2.90                |
| 095  | $508.4^{+31.3}_{-34.6}$                  | 0.04                 | 0.60          | 0.00               | 1.94                | 238        | $7.7^{+130.9}_{-127.5}$   | 0.14                 | 0.65          | 18.50           | 1.46                |
| 097  | $182.6^{+40.1}_{-62.0}$                  | 0.73                 | 0.85          | 14.00              | 3.40                | 241        | $7.7_{-127.5}$ $713.8_{-24.2}^{+15.9}$  | 0.14                 | 0.03          | 16.00           | 4.11                |
| 098  | $-742.5^{+20.5}_{-6.5}$                  | 0.00                 | 0.75          | 6.00               | 4.86                | 242        | $69.7^{+69.2}_{-67.5}$  | 0.47                 | 0.49          | 8.00            | 1.34                |
| 107  | $-713.7^{+19.5}_{-7.5}$                  | 0.27                 | 0.26          | 7.00               | 1.31                | 244        | $125.1^{+10.9}_{-8.4}$  | 0.28                 | 0.53          | 0.00            | 4.75                |
| 108  | $199.1^{+29.3}_{-40.8}$                  | 0.60                 | 0.34          | 14.00              | 3.28                | 245        | $286.6^{+61.4}_{-76.6}$   | 0.23                 | 0.53          | 12.00           | 2.30                |
| 110  | $182.9^{+47.5}_{-36.4}$                  | 0.14                 | 0.45          | 14.00              | 0.76                | 249        | $67.8^{+26.5}_{-8.3}$   | 0.36                 | 0.51          | 8.50            | 3.98                |
| 112  | $101.2^{+8.9}_{-14.6}$                   | 0.52                 | 0.67          | 10.00              | 3.04                | 251        | $162.7^{+54.2}_{-16.5}$   | 0.74                 | 0.35          | 11.00           | 3.09                |
| 116  | $170.8^{+60.6}_{-24.7}$                  | 0.69                 | 0.52          | 13.00              | 1.84                | 253        | $646.4_{-48.2}^{+53.6}$   | 0.74                 | 0.33          | 13.00           | 2.24                |
| 117  | $-565.8^{+77.0}_{-128.1}$                | 0.05                 | 0.44          | 18.00              | 0.00                | 256        | $139.5^{+52.9}_{-38.7}$   | 0.20                 | 0.71          | 15.00           | 3.42                |
| 119  | $186.5^{+35.3}_{-42.3}$                  | 0.19                 | 0.56          | 15.50              | 1.35                | 257        | $20.6_{-35.9}^{+30.4}$  | 0.14                 | 0.71          | 8.33            | 1.40                |
| 124  | $-601.9_{-4.7}^{+4.5}$                   | 0.56                 | 0.21          | 14.00              | 4.06                | 259        | $572.3^{+29.0}_{-24.5}$   | 0.11                 | 0.23          | 11.00           | 0.43                |
| 128  | $565.3^{+18.7}_{-21.9}$                  | 0.16                 | 0.44          | 19.00              | 2.77                | 262        | $-492.4^{+15.7}_{-58.5}$  | 0.12                 | 0.39          | 3.50            | 2.04                |
| 130  | $663.8^{+36.8}_{-112.1}$                 | 0.13                 | 0.83          | 16.50              | 2.45                | 264        | $-492.4_{-58.5}$ $549.6_{-10.1}^{+10.7}$  | 0.30                 | 0.20          | 15.00           | 3.62                |
| 137  | $269.0^{+21.3}_{-70.2}$                  | 0.01                 | 0.47          | 6.00               | 4.21                | 266        | $-664.4^{+93.0}_{-6.2}$   | 0.66                 | 0.04          | 12.00           | 2.26                |
| 142  | $88.2^{+113.6}_{-132.6}$                 | 0.00                 | 0.77          | 14.00              | 0.00                | 269        | $-604.4_{-6.2}$ $670.3_{-42.8}^{+8.0}$  | 0.00                 | 0.20          | 8.00            | 4.33                |
|      |  |                      |               |                    |                     | 209        | $070.3_{-42.8}$   | 0.14                 | 0.51          | 0.00            | 4.33                |

Table 5 (Continued)

Table 5 (Continued)

| RMID       | $	au_{ m JAV} \  m (days)$                        | Fraction<br>Rejected | $r_{ m max}$ | $S/N_{con}$ | S/N <sub>line</sub> | RMID | $	au_{ m JAV} \  m (days)$                         | Fraction<br>Rejected | $r_{ m max}$ | S/N <sub>con</sub> | S/N <sub>line</sub> |
|------------|---|----------------------|--------------|-------------|---------------------|------|--|----------------------|--------------|--------------------|---------------------|
| 275        | $209.1^{+21.0}_{-63.0}$                           | 0.42                 | 0.95         | 18.33       | 4.73                | 412  | 368.9 <sup>+97.5</sup> <sub>-34.9</sub>            | 0.01                 | 0.75         | 16.67              | 0.15                |
| 279        | $-548.6_{-28.0}^{+26.4}$                          | 0.52                 | 0.40         | 17.00       | 1.21                | 413  | $523.1_{-19.4}^{+17.8}$                            | 0.42                 | 0.34         | 2.00               | 3.11                |
| 280        | $55.2^{+88.9}_{-136.2}$                           | 0.39                 | 0.60         | 14.20       | 0.00                | 414  | $219.5_{-40.2}^{+47.2}$                            | 0.07                 | 0.62         | 21.00              | 1.93                |
| 282        | $386.1^{+25.2}_{-38.0}$                           | 0.22                 | 0.29         | 4.50        | 0.00                | 416  | $-699.1^{+36.2}_{-31.2}$                           | 0.72                 | 0.43         | 10.50              | 0.93                |
| 283        | $193.6^{+69.5}_{-33.5}$                           | 0.06                 | 0.38         | 8.50        | 3.62                | 418  | $199.6^{+66.9}_{-40.9}$                            | 0.20                 | 0.60         | 12.00              | 2.33                |
| 284        | $-34.2^{+34.9}_{-28.8}$                           | 0.47                 | 0.68         | 6.00        | 2.06                | 423  | $-625.2^{+52.0}_{-32.6}$                           | 0.18                 | 0.45         | 11.00              | 4.16                |
| 286        | $260.9^{+35.4}_{-29.0}$                           | 0.23                 | 0.34         | 0.00        | 4.38                | 424  | $433.4_{-60.7}^{+73.7}$                            | 0.55                 | 0.53         | 3.00               | 3.04                |
| 293        | $584.4^{+34.7}_{-30.3}$                           | 0.18                 | 0.43         | 13.00       | 2.79                | 425  | $142.3^{+153.3}_{-122.5}$                          | 0.44                 | 0.26         | 0.00               | 1.32                |
| 295        | $549.0^{+27.4}_{-17.9}$                           | 0.45                 | 0.89         | 18.00       | 2.88                | 426  | $216.2^{+330.7}_{-354.3}$                          | 0.00                 | 0.47         | 19.00              | 0.00                |
| 298        | $279.5^{+49.3}_{-83.5}$                           | 0.08                 | 0.66         | 17.00       | 3.18                | 430  | $158.4^{+60.1}_{-62.1}$                            | 0.20                 | 0.62         | 5.50               | 3.02                |
| 304        | $284.2^{+76.5}_{-18.6}$                           | 0.22                 | 0.25         | 10.00       | 0.00                | 431  | $116.5^{+385.2}_{-261.2}$                          | 0.20                 | 0.28         | 12.00              | 0.00                |
| 310        | $-703.6^{+18.8}_{-24.8}$                          | 0.60                 | 0.21         | 16.00       | 2.33                | 432  | $-699.7^{+24.9}_{-6.4}$                            | 0.47                 | 0.56         | 15.00              | 1.87                |
| 312        | $166.7^{+33.4}_{-19.5} \\ 126.8^{+65.2}_{-12.9}$  | 0.28                 | 0.85         | 22.00       | 4.90                | 433  | $214.3_{-52.9}^{+43.7} \\ -580.7_{-16.4}^{+22.8}$  | 0.45                 | 0.46         | 17.00              | 1.58                |
| 317        | $126.8^{+65.2}_{-12.9}$                           | 0.24                 | 0.49         | 12.00       | 1.10                | 434  | $-580.7^{+22.8}_{-16.4}$                           | 0.62                 | 0.25         | 7.00               | 2.97                |
| 318        | $215.8^{+70.3}_{-66.8}$                           | 0.43                 | 0.48         | 18.67       | 1.72                | 435  | $-195.9_{-21.1}^{+14.5}$                           | 0.16                 | 0.18         | 15.50              | 3.42                |
| 319        | $197.1^{+43.8}_{-40.1}$                           | 0.07                 | 0.69         | 10.00       | 0.53                | 436  | $487.7^{+147.2}_{-162.5}$                          | 0.13                 | 0.35         | 6.50               | 1.08                |
| 321        | $55.8^{+63.4}_{-73.0}$                            | 0.62                 | 0.29         | 10.33       | 1.37                | 441  | $570.3^{+24.7}_{-22.9}$                            | 0.09                 | 0.67         | 11.33              | 0.58                |
| 322        | $200.7^{+33.7}_{-32.1}$                           | 0.41                 | 0.60         | 4.00        | 1.62                | 442  | $-599.9^{+10.3}_{-37.2}$                           | 0.52                 | 0.50         | 8.00               | 2.65                |
| 327        | $-626.4^{+69.3}_{-79.1}$                          | 0.56                 | 0.46         | 20.67       | 0.82                | 445  | $189.8^{+15.4}_{-12.2}$                            | 0.50                 | 0.34         | 15.00              | 3.73                |
| 330        | $423.3^{+90.6}_{-81.9}$                           | 0.14                 | 0.50         | 16.75       | 0.00                | 447  | $-643.2^{+40.5}_{-35.5}$                           | 0.59                 | 0.49         | 8.50               | 0.48                |
| 332        | $292.1^{+20.0}_{-40.9}$                           | 0.09                 | 0.52         | 9.50        | 4.54                | 448  | $-535.0^{+46.7}_{-95.1}$                           | 0.65                 | 0.41         | 10.00              | 1.02                |
| 334        | $135.0^{+85.0}_{-162.2}$                          | 0.17                 | 0.76         | 11.00       | 1.67                | 451  | $-424.4^{+102.3}_{-95.7}$                          | 0.67                 | 0.49         | 11.33              | 0.00                |
| 335        | $236.7_{-30.3}^{+15.6} 441.0_{-404.1}^{+193.7}$   | 0.53                 | 0.78         | 11.00       | 3.89                | 452  | $-624.6^{+72.2}_{-36.3}$                           | 0.31                 | 0.48         | 13.00              | 1.44                |
| 339        | $441.0^{+193.7}_{-404.1}$                         | 0.14                 | 0.49         | 10.00       | 0.87                | 454  | $99.0^{+388.6}_{-51.9}$                            | 0.03                 | 0.33         | 7.67               | 1.63                |
| 342        | $498.6^{+157.1}_{-166.6}$                         | 0.02                 | 0.60         | 7.00        | 0.82                | 455  | $579.1^{+24.1}_{-19.2}$                            | 0.27                 | 0.00         | 11.50              | 4.39                |
| 343        | $660.9^{+49.5}_{-119.8}$                          | 0.22                 | 0.64         | 13.00       | 0.00                | 456  | $174.6^{+28.4}_{-13.5}$                            | 0.74                 | 0.62         | 8.00               | 2.94                |
| 344        | $205.3^{+153.1}_{-91.6}$                          | 0.00                 | 0.72         | 9.00        | 0.00                | 461  | $174.6^{+28.4}_{-13.5} \\ -431.1^{+69.5}_{-116.0}$ | 0.47                 | 0.40         | 8.00               | 0.52                |
| 345        | $171.8^{+80.7}_{-56.3}$                           | 0.66                 | 0.67         | 4.00        | 2.46                | 462  | $662.0^{+19.4}_{-138.0}$                           | 0.32                 | 0.33         | 7.00               | 2.76                |
| 346        | $186.2^{+61.6}_{-29.3}$                           | 0.00                 | 0.58         | 7.00        | 2.41                | 467  | $-657.0^{+85.3}_{-46.7}$                           | 0.57                 | 0.44         | 15.00              | 1.47                |
| 348        | $-547.5^{+35.8}_{-29.0}$                          | 0.55                 | 0.42         | 5.00        | 3.12                | 468  | $-569.5^{+56.2}_{-47.5}$                           | 0.25                 | 0.64         | 6.50               | 2.09                |
| 349        | $-537.9^{+196.7}_{-87.7}$                         | 0.40                 | 0.38         | 0.00        | 0.31                | 470  | $57.5^{+124.6}_{-11.4}$                            | 0.04                 | 0.71         | 17.00              | 2.72                |
| 351        | $662.4_{-19.4}^{+12.7}$                           | 0.14                 | 0.36         | 8.00        | 3.72                | 482  | $186.3^{+28.7}_{-20.5}$                            | 0.48                 | -0.07        | 12.40              | 2.58                |
| 353        | $-566.1^{+14.4}_{-13.8}$                          | 0.54                 | 0.04         | 17.00       | 1.46                | 485  | $474.3^{+80.5}_{-18.5}$                            | 0.21                 | 0.74         | 12.33              | 2.20                |
| 358        | $216.4^{+46.9}_{-47.7}$                           | 0.57                 | 0.72         | 7.00        | 1.21                | 486  | $242.9^{+86.6}_{-48.0}$                            | 0.38                 | 0.23         | 17.67              | 1.76                |
| 359        | $-636.5^{+119.9}_{-100.5}$                        | 0.62                 | 0.41         | 8.67        | 0.35                | 487  | $51.2^{+103.4}_{-14.3}$                            | 0.57                 | 0.84         | 10.50              | 3.81                |
| 361        | $-154.8^{+144.3}_{-59.3}$                         | 0.04                 | 0.66         | 11.50       | 1.58                | 488  | $209.3_{-37.3}^{+71.8}$                            | 0.10                 | 0.16         | 12.00              | 1.95                |
| 362        | $224.9_{-27.2}^{+17.9}$                           | 0.21                 | 0.67         | 15.50       | 3.92                | 490  | $553.0_{-30.4}^{+25.1}$                            | 0.15                 | 0.15         | 12.67              | 1.77                |
| 363        | $-245.8^{+31.1}_{-39.2}$                          | 0.08                 | 0.26         | 10.50       | 2.44                | 491  | $725.6^{+18.1}_{-51.9}$                            | 0.66                 | 0.31         | 0.00               | 0.77                |
| 366        | $-527.3_{-21.3}^{+28.9}$                          | 0.55                 | 0.52         | 9.00        | 2.95                | 493  | $-661.2^{+46.5}_{-34.1}$                           | 0.45                 | 0.46         | 8.80               | 0.00                |
| 372        | $185.3_{-33.2}^{+45.2}$                           | 0.60                 | 0.76         | 15.67       | 3.92                | 494  | $-577.3^{+2.9}_{-3.3}$                             | 0.52                 | -0.55        | 4.00               | 0.00                |
| 379        | $-158.7^{+15.8}_{-33.0}$                          | 0.35                 | 0.59         | 12.00       | 1.01                | 495  | $-429.3^{+302.9}_{-203.4}$                         | 0.34                 | 0.43         | 11.00              | 0.19                |
| 380        | $160.0^{+10.5}_{-9.3}$                            | 0.34                 | 0.59         | 15.00       | 1.91                | 496  | $609.4^{+29.9}_{-20.2}$                            | 0.20                 | 0.53         | 11.50              | 4.86                |
| 381        | $288.4^{+122.1}_{-64.8}$                          | 0.01                 | 0.65         | 16.00       | 1.07                | 499  | $560.8^{+67.8}_{-119.5}$                           | 0.07                 | 0.69         | 7.00               | 2.12                |
| 383        | $230.3^{+29.4}_{-41.3}$                           | 0.37                 | 0.23         | 0.00        | 1.50                | 500  | $167.3^{+80.5}_{-35.0}$                            | 0.19                 | 0.38         | 14.00              | 0.00                |
| 386        | $109.4^{+37.7}_{-55.2}$                           | 0.49                 | 0.56         | 11.00       | 2.21                | 506  | $637.6^{+36.5}_{-30.6}$                            | 0.22                 | 0.57         | 11.50              | 3.59                |
| 387        | $104.0^{+67.3}_{-11.7}$                           | 0.30                 | 0.75         | 12.00       | 2.26                | 507  | $576.6^{+98.6}_{-188.4}$                           | 0.13                 | 0.52         | 9.50               | 0.00                |
| 389        | $639.5^{+20.3}_{-51.4}$                           | 0.10                 | 0.52         | 12.67       | 3.08                | 508  | $-651.1^{+11.0}_{-9.7}$                            | 0.74                 | 0.28         | 9.11               | 2.27                |
| 394        | $-231.4^{+76.3}_{-109.1}$                         | 0.27                 | 0.34         | 5.00        | 1.13                | 511  | $249.2^{+132.1}_{-99.0}$                           | 0.74                 | 0.41         | 5.00               | 1.59                |
| 396        | $-675.4^{+97.5}_{-67.5}$                          | 0.80                 | 0.26         | 2.50        | 0.00                | 512  | $-535.1^{+121.5}_{-100.0}$                         | 0.14                 | 0.08         | 0.00               | 1.52                |
| 397        | $708.5^{+11.4}_{-11.8}$                           | 0.24                 | 0.13         | 5.00        | 3.17                | 514  | $462.2^{+176.9}_{-293.1}$                          | 0.23                 | 0.49         | 9.00               | 0.00                |
| 401        | $133.8^{+43.0}_{-25.0}$                           | 0.33                 | 0.84         | 12.00       | 3.39                | 517  | $227.1^{+81.6}_{-125.3}$                           | 0.09                 | 0.66         | 11.33              | 1.52                |
| 403        | $723.5^{+12.4}_{-55.0}$                           | 0.66                 | 0.65         | 8.00        | 3.56                | 520  | $604.2^{+92.9}_{-101.3}$                           | 0.29                 | 0.65         | 9.00               | 0.00                |
| 405        | $722.5^{+18.5}_{-62.9}$                           | 0.27                 | 0.46         | 16.00       | 1.72                | 522  | $237.8^{+63.0}_{-77.4}$                            | 0.36                 | 0.52         | 8.00               | 0.36                |
| 408        | $487.9^{+32.7}_{-20.5}$                           | 0.07                 | 0.60         | 10.00       | 4.47                | 527  | $138.6^{+40.1}_{-32.3}$                            | 0.00                 | 0.81         | 10.00              | 4.22                |
|            | -20.3   |                      |              | 10.75       | 2.72                | 528  | $-592.6^{+97.9}_{-87.2}$                           | 0.66                 | 0.35         | 6.00               | 0.00                |
|            | $126.3^{+21.9}_{-20.2}$                           | 0.29                 | 0.35         | 10.75       | 4.14                | 240  | - JJZ.U 07 1                                       | 0.00                 | 0.55         | 0.00               | 0.00                |
| 409<br>410 | $126.3_{-20.2}^{+21.9} \\ -542.1_{-45.6}^{+26.4}$ | 0.29<br>0.10         | 0.35<br>0.81 | 15.33       | 3.39                | 529  | $-392.0_{-87.2}$ $439.5_{-13.0}^{+17.1}$           | 0.53                 | 0.32         | 7.00               | 3.32                |

Table 5 (Continued)

Table 5 (Continued)

| (Continued) |  |                      |              |                |                     | (Continued) |   |                      |              |                    |                     |  |
|-------------|--|----------------------|--------------|----------------|---------------------|-------------|---|----------------------|--------------|--------------------|---------------------|--|
| RMID        | $	au_{ m JAV} \  m (days)$   | Fraction<br>Rejected | $r_{ m max}$ | $S/N_{con}$    | S/N <sub>line</sub> | RMID        | $	au_{ m JAV} \  m (days)$                          | Fraction<br>Rejected | $r_{ m max}$ | S/N <sub>con</sub> | S/N <sub>line</sub> |  |
| 531         | $157.4_{-30.8}^{+18.0}  633.1_{-148.0}^{+26.9}  239.9_{-19.8}^{+26.2}$ | 0.71                 | 0.67         | 7.50           | 3.40                | 665         | $198.5^{+21.6}_{-68.2} \\ -512.8^{+226.3}_{-155.0}$ | 0.26                 | 0.78         | 11.50              | 1.76                |  |
| 532         | $633.1^{+26.9}_{-148.0}$   | 0.01                 | 0.31         | 0.00           | 3.08                | 670         | $-512.8^{+226.3}_{-155.0}$                          | 0.56                 | 0.52         | 21.00              | 1.55                |  |
| 533         | $239.9^{+26.2}_{-19.8}$  | 0.59                 | 0.37         | 7.00           | 2.56                | 676         | $-600.5^{+170.4}_{-115.6}$                          | 0.64                 | 0.32         | 14.20              | 0.00                |  |
| 535         | $-597.1^{+19.0}_{-30.9}$   | 0.32                 | -0.03        | 14.20          | 3.00                | 678         | $179.7^{+46.6}_{-94.7}$                             | 0.00                 | 0.41         | 13.50              | 0.84                |  |
| 538         | $-422.1^{+51.7}_{-72.4}$   | 0.31                 | 0.30         | 11.00          | 3.94                | 680         | $18.7^{+81.8}_{-68.2}$                              | 0.65                 | 0.47         | 12.50              | 1.75                |  |
| 540         | $310.0^{+88.6}_{-154.4}$   | 0.31                 | 0.56         | 11.00          | 0.00                | 682         | $648.9^{+12.7}_{-27.9}$                             | 0.10                 | 0.29         | 13.00              | 2.64                |  |
| 542         | $72.3^{+92.4}_{-82.5}$   | 0.37                 | 0.42         | 6.00           | 1.20                | 686         | $202.6^{+39.4}_{-19.8}$                             | 0.19                 | 0.58         | 8.00               | 3.09                |  |
| 543         | $161.9^{+93.7}_{-135.1}$   | 0.19                 | 0.18         | 9.00           | 1.21                | 687         | $508.6^{+171.0}_{-149.4}$                           | 0.31                 | 0.45         | 10.00              | 1.78                |  |
| 549         | $228.9_{-23.6}^{+17.4}$  | 0.02                 | 0.74         | 16.00          | 3.41                | 688         | $-102.1^{+189.9}_{-173.6}$                          | 0.32                 | 0.56         | 22.00              | 1.10                |  |
| 550         | $463.9^{+36.5}_{-82.2}$  | 0.02                 | 0.46         | 8.00           | 3.04                | 689         | $474.0^{+68.7}_{-126.9}$                            | 0.00                 | 0.58         | 8.00               | 3.02                |  |
| 553         | $655.5^{+80.2}_{-50.7}$  | 0.43                 | 0.47         | 8.00           | 1.65                | 690         | $144.0^{+40.2}_{-41.9}$                             | 0.31                 | 0.61         | 16.25              | 0.71                |  |
| 554         | $525.1^{+55.2}_{-33.0}$  | 0.05                 | 0.59         | 7.33           | 2.42                | 692         | $-316.7^{+630.6}_{-307.6}$                          | 0.00                 | 0.45         | 11.67              | 0.29                |  |
| 555         | $-696.1^{+100.7}_{-14.5}$  | 0.52                 | 0.49         | 13.00          | 3.85                | 693         | $252.5^{+15.2}_{-28.5}$                             | 0.42                 | 0.39         | 11.00              | 1.78                |  |
| 556         | $-269.7^{+92.7}_{-106.9}$  | 0.07                 | 0.85         | 13.50          | 2.29                | 695         | $249.3^{+90.5}_{-62.7}$                             | 0.43                 | 0.54         | 7.00               | 1.82                |  |
| 557         | $325.8^{+53.0}_{-69.3}$  | 0.44                 | 0.66         | 12.00          | 0.00                | 698         | $145.0^{+36.8}_{-25.3}$                             | 0.77                 | 0.70         | 19.00              | 2.83                |  |
| 560         | $582.6_{-15.0}^{+14.9}$ $316.7_{-91.4}^{+140.5}$                       | 0.25                 | -0.02        | 13.00          | 2.70                | 699         | $240.9^{+25.4}_{-45.2}$                             | 0.03                 | 0.64         | 13.50              | 0.00                |  |
| 561         | $316.7^{+140.3}_{-91.4}$   | 0.59                 | 0.44         | 13.20          | 1.52                | 703         | $583.6^{+66.3}_{-72.5}$                             | 0.09                 | 0.61         | 12.00              | 1.72                |  |
| 562         | $597.9^{+68.7}_{-129.2}$   | 0.40                 | 0.54         | 9.00           | 2.01                | 704         | $-567.9^{+61.9}_{-45.4}$                            | 0.57                 | 0.49         | 14.00              | 1.48                |  |
| 563         | $488.2^{+142.1}_{-51.2}$   | 0.01                 | 0.34         | 7.67           | 2.64                | 705         | $202.0_{-27.9}^{+37.7}$                             | 0.49                 | 0.47         | 14.67              | 3.12                |  |
| 564         | $602.1^{+104.8}_{-138.9}$  | 0.23                 | 0.34         | 10.67          | 1.04                | 706         | $-68.1^{+26.6}_{-10.4}$                             | 0.45                 | 0.43         | 14.50              | 0.49                |  |
| 573         | 565.1 <sup>+44.9</sup> <sub>-180.7</sub>                               | 0.14                 | 0.29         | 13.00          | 2.06                | 710         | 480.5 <sup>+214.5</sup> <sub>-195.2</sub>           | 0.16                 | 0.28         | 11.00              | 1.10                |  |
| 574         | $652.0^{+37.9}_{-47.8}$  | 0.21                 | 0.13         | 7.50           | 2.68                | 711         | $-663.5^{+110.6}_{-30.8}$                           | 0.53                 | 0.63         | 12.00              | 1.98                |  |
| 575         | 540.9 <sup>+22.8</sup> -35.6   | 0.33                 | 0.37         | 10.33          | 4.04                | 713         | $68.4^{+99.5}_{-78.2}$                              | 0.14                 | 0.74         | 9.00               | 1.96                |  |
| 578         | $429.0^{+140.6}_{-75.7}$   | 0.12                 | 0.50         | 14.00          | 0.70                | 715         | $-602.5^{+14.5}_{-90.9}$                            | 0.59                 | 0.31         | 8.67               | 1.28                |  |
| 579         | $148.9^{+183.3}_{-13.5}$   | 0.04                 | 0.50         | 19.00          | 2.64                | 718         | $89.9^{+398.9}_{-279.0}$                            | 0.30                 | 0.44         | 12.00              | 0.00                |  |
| 583         | $249.9^{+16.8}_{-14.8}$  | 0.48                 | 0.18         | 15.00          | 2.70                | 722         | $148.7^{+46.4}_{-46.6}$                             | 0.11                 | 0.52         | 16.00              | 4.16                |  |
| 584         | $-591.9^{+41.5}_{-89.1}$   | 0.31                 | 0.18         | 7.00           | 2.85                | 723         | $209.3^{+75.6}_{-197.5}$                            | 0.27                 | 0.38         | 15.50              | 0.00                |  |
| 585         | $65.3_{-18.8}^{+65.1} \\ -69.4_{-199.7}^{+48.2}$                       | 0.05                 | 0.66         | 14.00          | 0.67                | 725         | $-1.0^{+8.1}_{-9.7}$                                | 0.46                 | 0.53         | 8.25               | 1.56                |  |
| 586         | -69.4 <sub>-199.7</sub>  | 0.16                 | 0.47         | 10.00          | 2.80                | 729<br>724  | $112.7^{+86.9}_{-57.0}$                             | 0.62                 | 0.66         | 8.50               | 0.63                |  |
| 591<br>594  | $-249.1^{+38.4}_{-45.6}$   | 0.87<br>0.04         | 0.35<br>0.49 | 11.00<br>11.50 | 0.76<br>1.97        | 734         | $289.9^{+46.1}_{-36.5}  637.6^{+52.9}_{-111.5}$     | 0.02<br>0.34         | 0.81<br>0.39 | 8.50<br>11.00      | 2.37<br>2.34        |  |
| 595         | $192.1^{+31.1}_{-19.9} \\ -619.6^{+76.1}_{-27.9}$                      |                      | 0.49         | 0.00           | 0.81                | 735<br>737  | $-534.4^{+55.1}_{-109.5}$                           | 0.54                 | 0.39         | 9.67               | 0.00                |  |
| 596         | $-619.0_{-27.9}$ $649.1_{-208.8}^{+83.8}$                              | 0.58<br>0.55         | 0.10         | 13.00          | 1.45                | 737         | $-334.4_{-109.5}$ $146.7_{-10.6}^{+11.4}$           | 0.08                 | 0.22         | 11.00              | 0.00                |  |
| 600         | $636.3^{+28.9}_{-54.0}$  | 0.07                 | 0.08         | 14.67          | 2.93                | 739         | $214.1^{+40.9}_{-38.2}$                             | 0.29                 | 0.15         | 6.00               | 2.63                |  |
| 602         | $-390.8^{+47.2}_{-24.2}$   | 0.07                 | 0.08         | 9.00           | 2.93                | 743         | $191.1^{+67.3}_{-65.8}$                             | 0.19                 | 0.33         | 4.00               | 3.78                |  |
| 609         | $-189.4^{+9.5}_{-9.2}$   | 0.79                 | 0.11         | 13.00          | 2.13                | 748         | $621.4_{-86.0}^{+33.4}$                             | 0.12                 | 0.33         | 10.00              | 2.12                |  |
| 611         | $-79.5^{+241.4}_{-196.4}$  | 0.77                 | 0.41         | 12.41          | 0.53                | 749         | $707.2^{+36.9}_{-51.4}$                             | 0.17                 | 0.33         | 12.00              | 0.85                |  |
| 612         | $715.7^{+14.6}_{-41.9}$  | 0.56                 | 0.39         | 6.00           | 1.56                | 751         | $-690.9^{+47.7}_{-23.5}$                            | 0.80                 | 0.48         | 12.00              | 1.93                |  |
| 613         | $651.2^{+45.5}_{-42.1}$  | 0.43                 | 0.44         | 0.00           | 2.61                | 752         | $187.8^{+17.4}_{-26.4}$                             | 0.49                 | 0.22         | 17.00              | 1.64                |  |
| 614         | $92.5^{+99.6}_{-7.2}$  | 0.53                 | 0.68         | 10.00          | 4.90                | 753         | $-102.5^{+52.5}_{-56.6}$                            | 0.22                 | 0.33         | 9.50               | 1.60                |  |
| 616         | $684.9^{+48.8}_{-113.4}$   | 0.24                 | 0.35         | 12.33          | 0.90                | 754         | $-198.5^{+22.4}_{-36.7}$                            | 0.07                 | 0.79         | 10.00              | 2.33                |  |
| 620         | $-196.5^{+26.6}_{-28.3}$   | 0.32                 | 0.23         | 8.00           | 2.51                | 759         | $233.2^{+142.1}_{-73.8}$                            | 0.28                 | 0.40         | 8.00               | 0.00                |  |
| 621         | $358.2^{+44.6}_{-73.9}$  | 0.30                 | 0.37         | 14.00          | 1.29                | 763         | $-181.6^{+15.7}_{-32.0}$                            | 0.33                 | 0.63         | 10.50              | 3.41                |  |
| 623         | $573.0^{+76.9}_{-134.6}$   | 0.01                 | 0.60         | 10.00          | 0.52                | 770         | $-8.7^{+71.5}_{-135.0}$                             | 0.57                 | 0.32         | 4.20               | 0.00                |  |
| 629         | $168.5^{+27.2}_{-18.7}$  | 0.30                 | 0.23         | 0.00           | 0.69                | 771         | $363.0^{+80.5}_{-96.2}$                             | 0.14                 | 0.58         | 13.38              | 0.00                |  |
| 630         | $163.0^{+217.7}_{-186.5}$  | 0.54                 | 0.27         | 7.33           | 0.46                | 774         | 86.6 <sup>+39.7</sup> -51.2                         | 0.00                 | 0.79         | 15.60              | 1.14                |  |
| 631         | $-683.1^{+82.2}_{-55.1}$   | 0.02                 | 0.74         | 15.00          | 0.00                | 777         | $260.2^{+51.5}_{-61.6}$                             | 0.65                 | 0.32         | 10.75              | 0.00                |  |
| 633         | $220.5^{+110.3}_{-29.4}$   | 0.67                 | 0.57         | 8.50           | 1.69                | 784         | $-4.0^{+38.5}_{-25.7}$                              | 0.04                 | 0.62         | 5.10               | 0.00                |  |
| 635         | $592.5^{+73.7}_{-89.3}$  | 0.13                 | 0.43         | 13.00          | 2.62                | 794         | $-606.9^{+29.2}_{-5.0}$                             | 0.57                 | 0.06         | 7.00               | 1.74                |  |
| 636         | $95.8^{+70.6}_{-146.9}$  | 0.33                 | 0.55         | 8.00           | 0.00                | 796         | $-375.6^{+151.8}_{-65.1}$                           | 0.19                 | 0.39         | 6.00               | 0.00                |  |
| 646         | $640.5^{+13.3}_{-39.9}$  | 0.14                 | 0.09         | 8.00           | 0.00                | 801         | $601.1^{+29.5}_{-35.6}$                             | 0.11                 | 0.01         | 9.00               | 3.85                |  |
| 647         | $273.9^{+93.2}_{-186.6}$   | 0.12                 | 0.33         | 26.00          | 0.73                | 803         | $203.1_{-34.9}^{+34.1}$                             | 0.01                 | 0.70         | 6.00               | 1.62                |  |
| 648         | $557.7^{+19.5}_{-72.8}$  | 0.13                 | 0.31         | 7.00           | 2.58                | 809         | $290.1_{-135.3}^{+73.9}$                            | 0.42                 | 0.62         | 9.00               | 2.36                |  |
| 651         | $196.9^{+21.5}_{-38.5}$  | 0.51                 | 0.76         | 12.67          | 3.53                | 810         | $-351.0^{+51.6}_{-67.6}$                            | 0.58                 | 0.40         | 11.00              | 0.33                |  |
| 658         | $139.8^{+102.5}_{-24.0}$   | 0.43                 | 0.56         | 7.00           | 1.50                | 811         | $-219.2^{+46.0}_{-33.6}$                            | 0.39                 | 0.38         | 10.00              | 0.80                |  |
| 660         | $54.6^{+67.8}_{-41.0}$   | 0.26                 | 0.60         | 11.67          | 0.21                | 816         | $168.8^{+23.3}_{-25.9}$                             | 0.29                 | 0.34         | 11.00              | 1.32                |  |
| 661         | $479.6^{+63.6}_{-42.0}$  | 0.23                 | 0.22         | 13.00          | 1.65                | 818         | $219.4_{-29.2}^{+16.8}$                             | 0.17                 | 0.30         | 17.60              | 2.42                |  |
| 001         | 4/9.0_42.0   | 0.23                 | 0.22         | 13.00          | 1.03                | 010         | 419.4 <sub>-29.2</sub>                              | 0.1/                 | 0.30         | 17.00              |                     |  |

Table 5 (Continued)

| RMID | $	au_{ m JAV} \ 	ag{days}$              | Fraction<br>Rejected | $r_{ m max}$ | $S/N_{con}$ | S/N <sub>line</sub> |
|------|---|----------------------|--------------|-------------|---------------------|
| 820  | 647.9 <sup>+53.5</sup> <sub>-95.6</sub> | 0.17                 | 0.54         | 11.00       | 0.00                |
| 821  | $736.8^{+9.7}_{-28.5}$                  | 0.65                 | 0.69         | 13.00       | 1.57                |
| 827  | $408.4^{+54.4}_{-57.6}$                 | 0.26                 | 0.91         | 14.00       | 3.08                |
| 828  | $311.1^{+21.5}_{-22.7}$                 | 0.43                 | 0.32         | 14.00       | 0.95                |
| 829  | $159.3^{+48.8}_{-55.1}$                 | 0.06                 | 0.46         | 5.00        | 3.00                |
| 831  | $-605.8^{+72.3}_{-86.9}$                | 0.43                 | 0.56         | 11.80       | 3.10                |
| 835  | $475.6^{+85.5}_{-32.5}$                 | 0.32                 | 0.46         | 10.00       | 0.19                |

(This table is available in machine-readable form.)

#### **ORCID** iDs

C. J. Grier https://orcid.org/0000-0001-9920-6057 Yue Shen https://orcid.org/0000-0003-1659-7035 Keith Horne https://orcid.org/0000-0003-1728-0304 W. N. Brandt https://orcid.org/0000-0002-0167-2453 J. R. Trump https://orcid.org/0000-0002-1410-0470 P. B. Hall https://orcid.org/0000-0002-1763-5825 K. Kinemuchi https://orcid.org/0000-0001-7908-7724 Luis C. Ho https://orcid.org/0000-0001-6947-5846 Y. Homayouni https://orcid.org/0000-0002-0957-7151 Jennifer I-Hsiu Li https://orcid.org/0000-0002-0311-2812 Ian D. McGreer https://orcid.org/0000-0002-3461-5228 B. M. Peterson https://orcid.org/0000-0001-6481-5397 Dmitry Bizyaev https://orcid.org/0000-0002-3601-133X K. S. Dawson https://orcid.org/0000-0002-0553-3805 Siyao Jia https://orcid.org/0000-0001-5341-0765 Linhua Jiang https://orcid.org/0000-0003-4176-6486 Kaike Pan https://orcid.org/0000-0002-2835-2556 Kara A. Ponder https://orcid.org/0000-0002-8207-3304 Jesse Rogerson https://orcid.org/0000-0002-7078-1776 Tianmeng Zhang https://orcid.org/0000-0002-8531-5161 Hu Zou https://orcid.org/0000-0002-6684-3997

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