

# The Surface Detector System of the Pierre Auger Observatory

I. Allekotte<sup>a</sup>, A. F. Barbosa<sup>d</sup>, P. Bauleo<sup>ℓ</sup>, C. Bonifazi<sup>d</sup>,  
B. Civit<sup>c</sup>, C. O. Escobar<sup>e</sup>, B. García<sup>c</sup>, G. Guedes<sup>f</sup>,  
M. Gómez Berisso<sup>a</sup>, J. L. Harton<sup>ℓ</sup>, M. Healy<sup>k</sup>, M. Kaducak<sup>j</sup>,  
P. Mantsch<sup>j</sup>, P. O. Mazur<sup>j</sup>, C. Newman-Holmes<sup>j</sup>, I. Pepe<sup>g</sup>,  
I. Rodríguez-Cabo<sup>i</sup>, H. Salazar<sup>h</sup>, N. Smetniansky-De Grande<sup>b</sup>,  
D. Warner<sup>ℓ</sup>, for the Pierre Auger Collaboration<sup>m</sup>

<sup>a</sup>*Instituto Balseiro and Centro Atómico Bariloche (U.N. Cuyo and CNEA,  
CONICET), 8400 Bariloche, Argentina*

<sup>b</sup>*Laboratorio Tandem, Comisión Nacional de Energía Atómica and CONICET, Av.  
Gral. Paz 1499 (1650) San Martín, Buenos Aires, Argentina*

<sup>c</sup>*Universidad Tecnológica Nacional Regional Mendoza, Mendoza, Argentina*

<sup>d</sup>*CBPF, Rua Xavier Sigaud 150, Rio de Janeiro, Brazil*

<sup>e</sup>*Universidade Estadual de Campinas, Instituto de Física, Departamento de Raios  
Cosmicos, CP 6165, 13084-971, Campinas SP, Brazil*

<sup>f</sup>*Universidade Estadual de Feira de Santana (UEFS), Av. Universitaria Km 03 da  
BR 116, Campus Universitario, 44031-460 Feira de Santana BA, Brazil*

<sup>g</sup>*Universidade Federal da Bahia, Campus de Odina, 40210-340 Salvador BA,  
Brazil*

<sup>h</sup>*Benemérita Universidad Autónoma de Puebla (BUAP), Ap. Postal J-48, 72500  
Puebla, Puebla, Mexico*

<sup>i</sup>*Dpto. Física de Partículas, Universidad de Santiago de Compostela, 15706  
Santiago de Compostela, Spain*

<sup>j</sup>*Fermi National Accelerator Lab., Batavia IL, U.S.A.*

<sup>k</sup>*University of California, Los Angeles (UCLA), Department of Physics and  
Astronomy, Los Angeles, CA 90095, U.S.A.*

<sup>ℓ</sup>*Colorado State University, Fort Collins, CO 80523, U.S.A.*

<sup>m</sup>*Pierre Auger Collaboration, Av. San Martín Norte 306, 5613 Malargüe,  
Mendoza, Argentina*

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## Abstract

The Pierre Auger Observatory is designed to study cosmic rays with energies greater than  $10^{19}$  eV. Two sites are envisaged for the observatory, one in each hemisphere,

for complete sky coverage. The southern site of the Auger Observatory, now approaching completion in Mendoza, Argentina, features an array of 1600 water-Cherenkov surface detector stations covering 3000 km<sup>2</sup>, together with 24 fluorescence telescopes to record the air shower cascades produced by these particles. The two complementary detector techniques together with the large collecting area form a powerful instrument for these studies. Although construction is not yet complete, the Auger Observatory has been taking data stably since January 2004 and the first physics results are being published. In this paper we describe the technical characteristics and performance of the Surface Detector Stations of the Pierre Auger Observatory.

*Key words:* Pierre Auger Observatory; high-energy cosmic rays; surface detector array; water-Cherenkov detectors

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## 1 Introduction

Cosmic rays with energies near 10<sup>20</sup> eV have been a continuing mystery since Linsley reported the first such event in 1963 [1]. As yet there are no identified sources and no convincing mechanisms for accelerating particles to these energies. Interaction with the cosmic microwave background (CMB) constrains protons of  $\sim 10^{20}$  eV to come from distances not greater than about 50 Mpc [2,3]. Similarly constrained are other primaries: heavier nuclei lose energy by photo-disintegration and pair production, and photons due to pair creation [4]. Furthermore, the flux of cosmic rays at these highest energies is very low (less than one event per km<sup>2</sup> per century per sr), so that their detailed study requires detectors covering large areas.

The Pierre Auger Observatory was designed for a high statistics, full sky study of cosmic rays at the highest energies [5]. It utilizes an array of surface water-Cherenkov detectors combined with air fluorescence telescopes, which together provide a powerful instrument for air shower reconstruction. Energy, direction and composition measurements are intended to illuminate the mysteries of the most energetic particles in nature.

On dark moonless nights, air fluorescence telescopes record the development of what is essentially the electromagnetic shower that results from the interaction of the primary particle with the upper atmosphere. The surface array measures the particle densities as the shower strikes the ground just beyond

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*Email address:* [ingo@cab.cnea.gov.ar](mailto:ingo@cab.cnea.gov.ar) (for the Pierre Auger Collaboration).  
*URL:* [www.auger.org.ar](http://www.auger.org.ar); [www.auger.org](http://www.auger.org) (for the Pierre Auger Collaboration).

22 its maximum development. By recording the light produced by the developing  
23 air shower, fluorescence telescopes can make a near calorimetric measurement  
24 of the energy. This energy calibration can then be transferred to the surface  
25 array with its nearly 100% duty factor and large event gathering power [6,7].  
26 Moreover, independent measurements with the surface array and the fluores-  
27 cence detectors alone have limitations that can be overcome by combining the  
28 results of their measurements.

29 The water-Cherenkov detector was chosen for use in the surface array because  
30 of its robustness and low cost. Furthermore, water-Cherenkov detectors exhibit  
31 a rather uniform exposure up to large zenithal angles and are sensitive to  
32 charged particles as well as to energetic photons which convert to pairs in  
33 the water volume. Their use in surface arrays was proven to be successful in  
34 previous experiments [8].

35 Each of the 1600 surface detector stations includes a 3.6 m diameter water  
36 tank containing a sealed liner with a reflective inner surface. The liner contains  
37 12 000 l of pure water. Cherenkov light produced by the passage of particles  
38 through the water is collected by three nine-inch-diameter photomultiplier  
39 tubes (PMTs) that are symmetrically distributed at a distance of 1.20 m  
40 from the center of the tank and look downwards through windows of clear  
41 polyethylene into the water. The surface detector station is self-contained. A  
42 solar power system provides an average of 10 Watts for the PMTs and elec-  
43 tronics package consisting of a processor, GPS receiver, radio transceiver and  
44 power controller. The components of the surface detector station are shown  
45 in Fig. 1.

46 In this paper we describe the design features and performance of the surface  
47 detector hardware. This description includes the detector tanks, liners and  
48 accessories and the pure water production, as well as the most relevant steps  
49 for assembly and deployment of the surface detectors. We conclude with an  
50 overview of the technical performance of the system. The electronics system  
51 of the surface detectors will be described in a companion paper [9].

52 The Southern site of the Auger Observatory, now under construction in the  
53 Province of Mendoza, Argentina, is over 85% completed. Active detectors have  
54 been recording events in a stable operation mode since January 2004 [10].

## 55 **2 Design Considerations**

56 The low event rate of the highest energy cosmic rays requires an area large  
57 enough to accumulate good statistics in a reasonable time. By covering an area  
58 of 3000 km<sup>2</sup> at the Southern Site, the aperture achieved with the surface array

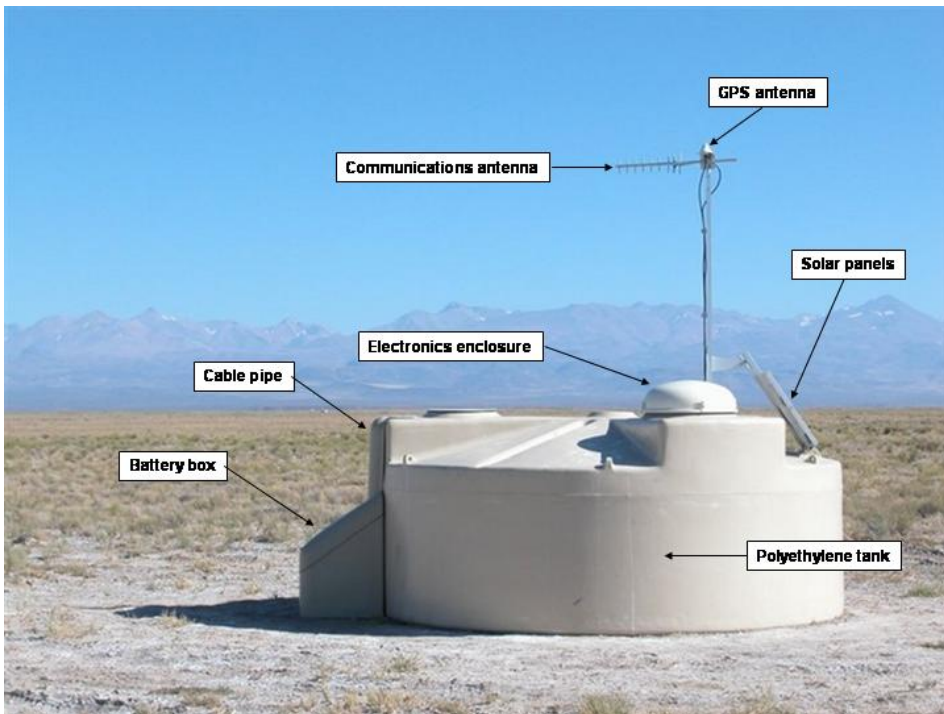


Fig. 1. A schematic view of a surface detector station in the field, showing its main components.

59 for zenith angles less than  $60^\circ$  will be  $7350 \text{ km}^2 \text{ sr}$ . By including events with  
60 larger zenith angles, up to  $80^\circ$ , the aperture can be increased by  $\sim 30\%$  [11].  
61 The detection efficiency at the trigger level reaches 100% for energies above  
62  $3 \times 10^{18} \text{ eV}$  [12]. This energy is determined from knowledge of the lateral distri-  
63 bution of showers and the single detector trigger probability, without recourse  
64 to Monte Carlo calculations. The spacing between the detector stations is the  
65 result of a compromise between cost considerations and the energy threshold  
66 (low enough to insure a good overlap with existing data.) Other important  
67 considerations are the need for sufficient sampling of the particle density away  
68 from the shower core, and the need for shower front timing in several locations.  
69 A minimum of five stations triggering at  $10^{19} \text{ eV}$  allows a maximum spacing  
70 of 1500 m on a triangular grid. At this spacing, approximately 10 stations  
71 are triggered by a nearly vertical shower with an energy of  $10^{20} \text{ eV}$ . At large  
72 zenith angles the multiplicity of stations triggered increases and at  $\sim 60^\circ$  it is  
73 typically over 20. Differential GPS systems allow the determination of position  
74 and altitude of the stations with an accuracy of less than 1 m, sufficient for a  
75 good shower reconstruction.

76 For the installation of this array, the site is required to be flat for good wireless  
77 communications. An altitude between 1000 and 1500 m above sea level is  
78 required for optimal development of the shower in the atmosphere. A large  
79 semi-desert area in the west of Argentina was chosen ( $35.0^\circ$  to  $35.3^\circ \text{ S}$ ,  $69.0^\circ$   
80 to  $69.4^\circ \text{ W}$ ) [13] next to the city of Malargüe . The chosen site has an average  
81 altitude of 1420 m, with detectors located at altitudes between 1340 m and  
82 1610 m. The site has suitable infrastructure nearby as well as clear night  
83 skies and minimal light pollution which enables good fluorescence detector  
84 performance.

## 85 *2.1 Energy and Angular Resolution and Composition Determination*

86 The shower energy is obtained by determination of the signal density at a par-  
87 ticular distance (typically 1000 m) from the shower axis. With the subset of  
88 events that the Observatory detects in hybrid mode (simultaneous measure-  
89 ment with both surface and fluorescence detectors), the nearly calorimetric  
90 energy determination which is possible with the fluorescence data can be used  
91 for an absolute calibration of the surface detector energy [6,7].

92 The signal densities measured with the surface detector array are affected  
93 by fluctuations from different origins: statistical fluctuations in the measured  
94 density, experimental uncertainties on the shower core position, incidence di-  
95 rection, and large physical fluctuations in the shower longitudinal development  
96 that lead to shower to shower fluctuations. The sampling fluctuations, which  
97 are dominated by the muon content of the showers, are determined by the

98 sampling area of the detector. At distances of around 1000 m from the shower  
99 core, the muon flux is of the order of  $\sim 1 \text{ m}^{-2}$  at  $10^{19}$  eV and corresponds  
100 to roughly a half of the total signal, the other half being due to the electro-  
101 magnetic component of the shower. Then, with a detector surface of  $10 \text{ m}^2$   
102 the sampling error in each detector is below 20%. For cylindrical detectors,  
103 this corresponds to a diameter of 3.6 m. The statistical uncertainty (including  
104 sampling and reconstruction fluctuations) in the determination of the signal  
105 density at 1000 m from the shower core is of 10% RMS for events with an  
106 energy of  $5 \times 10^{18}$  eV [14,15].

107 The direction of the primary is inferred from the relative arrival times of  
108 the shower front at different surface detectors. A weighted least squares fit  
109 is applied to the station triggering times. Fitting the station signal densities to  
110 the expected lateral distribution allows a refined core location determination.  
111 The angular resolution improves rapidly with energy and zenith angle because  
112 of the greater number of triggered stations. For the surface array alone, the  
113 angular precision is better than  $1^\circ$  for energies larger than  $\sim 10^{19}$  eV [16–18].

114 The height of the water-Cherenkov detector is chosen to get a clear muon  
115 signal [19] and optimize the separation of the muon and electromagnetic con-  
116 tributions to the signal. A vertical height of 1.2 m of water is sufficient to  
117 absorb 85% of the incident electromagnetic shower energy at core distances  
118 larger than 100 m, and gives a signal proportional to the energy of the elec-  
119 tromagnetic component. Muons passing through the tank generate a signal  
120 proportional to their geometric path length inside the detector and rather in-  
121 dependent of their zenith angle and position. Each PMT collects in excess of  
122 90 photoelectrons for each vertical muon [20].

## 123 *2.2 Physical and Environmental Requirements*

124 The Observatory will have an operating lifetime of 20 years and must be de-  
125 signed to survive the expected conditions at the site. The temperature ranges  
126 from  $-15^\circ\text{C}$  to  $50^\circ$  with large diurnal variation. The outdoor location ex-  
127 poses the detectors to intense solar ultraviolet radiation and wind of up to  
128  $160 \text{ km h}^{-1}$ . The detectors must be resistant to floods, rain, snow, dust, wind-  
129 blown sand and 2.5 cm diameter hail. Material selection is important because  
130 the local soils contain salts which can be corrosive to some materials. Mod-  
131 est seismic activity should not damage the detector units. The detector tanks  
132 must be robust and able to support a heavy person on top of the tank as well  
133 as to resist the action of insects, rodents and grazing animals.

134 The ground on which each detector station is placed must be leveled to prevent  
135 deformation of the tank and the area around the detector must be cleared of

136 heavy vegetation to avoid damage from bush fires.

### 137 *2.3 Design, Development and Production Control*

138 Each stage in the design, development and production of the surface detector  
139 station was marked by an appropriate technical review. Subsequent to the  
140 preliminary design review, 32 prototype detectors were built, deployed with  
141 standard spacing and operated in a small Engineering Array [21]. Every design  
142 feature of the detectors, the communications systems and data acquisition was  
143 tested during the two years allocated to the Engineering Array. Refinements  
144 resulting from this period were incorporated into the baseline design and sub-  
145 jected to a critical design review. A pre-production run of 100 detectors was  
146 then built to qualify the production process. Production readiness reviews  
147 initiated large scale component production. Assembly and deployment pro-  
148 cedures and associated quality assurance steps were also qualified during the  
149 Engineering Array and pre-production phases.

150 Individual assembly steps are documented in controlled written procedures,  
151 which are also used for training and guidance of the staff. A database was  
152 developed for the traceability of detector components and the results of the  
153 tests performed on them.

## 154 **3 The Tank System**

### 155 *3.1 Tanks*

156 The water-Cherenkov detectors have a cylindrical shape for the water volume,  
157 which is the simplest and least expensive to manufacture. The top of the  
158 tank is rather complex in order to provide rigidity both for mounting external  
159 components such as the solar panels and for people standing on top of it, and  
160 to provide space inside the tank for the photomultiplier assemblies and cabling.  
161 The tanks do not exceed 1.6 m in height so that they can be shipped over the  
162 roads within transportation regulations. The beige tank color is selected to  
163 blend in with the natural background of the site. Although the tank liner and  
164 photomultiplier assemblies are designed for opacity to keep any external light  
165 away from the PMTs, the tank is totally opaque to provide redundancy.

166 For the manufacture of the surface detector tanks, the technique of rotational  
167 molding (also called “rotomolding”) of high-density polyethylene was chosen  
168 for its low cost, tank uniformity and because polyethylene meets the require-

169 ments of robustness against the environmental elements.

170 In the rotomolding process, a predetermined amount of light beige powdered  
171 polyethylene is deposited inside a steel or stainless steel mold. The inside  
172 of the mold has the shape desired for the outside of the tank. The mold is  
173 closed and rotated about two axes simultaneously inside a 300°C oven. The  
174 beige powdered polyethylene melts and forms a coating on the inside surface  
175 of the mold. Heating and rotation continues until all the powder has been  
176 deposited on the surface of the mold. The rotation is briefly stopped and a  
177 predetermined amount of black powdered polyethylene is put inside the mold,  
178 which is immediately re-closed and the rotation in the oven continues until all  
179 of this powder has been deposited on the surface. Then the mold is removed  
180 from the oven and cooled while the rotation continues. Finally, the mold is  
181 opened and the tank removed.

182 This process, which requires between four and six hours, produces tanks with  
183 a light-beige outer layer of 1/3 of the thickness, and an opaque black inner  
184 layer guaranteeing that the tank itself will be opaque. Care in the manufac-  
185 turing process results in a nearly uniform wall thickness of the desired (13  
186  $\pm$  3) mm and minimal warping. The nominal weight of each tank is 530 kg,  
187 varying slightly with each manufacturer. Four companies produced tanks for  
188 this project.

189 Lugs are molded into the tank for lifting it and for supporting the solar panels.  
190 The solar panel bracket lugs are drilled to the correct diameter after molding  
191 and access hatches are cut into the tank.

192 The 20-year lifetime of the tanks under outdoor conditions is a challenging  
193 specification. However, discussions with consultants and experts in the field  
194 convinced us that this can be achieved using high-quality polyethylene resins.  
195 To greatly reduce damage due to ultraviolet exposure, modern polyethylenes  
196 contain hindered amine light stabilizers (HALS). In addition, ultraviolet light  
197 is absorbed by titanium dioxide found in the beige pigment of the outer layer  
198 and by the 1% carbon black pigment of the inner layer. The polyethylene  
199 resins used for tank production are prepared in two stages. The first one is the  
200 manufacture of the base resin by polymerizing selected alkenes with suitable  
201 catalysts. This stage of manufacture also includes the addition of the light  
202 stabilizers and anti-oxidants. The character and quality of the resin are de-  
203 termined in this stage. The second stage is “compounding”. The polyethylene  
204 resin thus manufactured is melted and the required pigments are extruded into  
205 the resin in such a way that they mix very finely with the base polyethylene.  
206 Other additives, like HALS and antioxidants, can be mixed in at this stage as  
207 well. Then the resin is cooled and ground into a powder ready for the molding  
208 process.



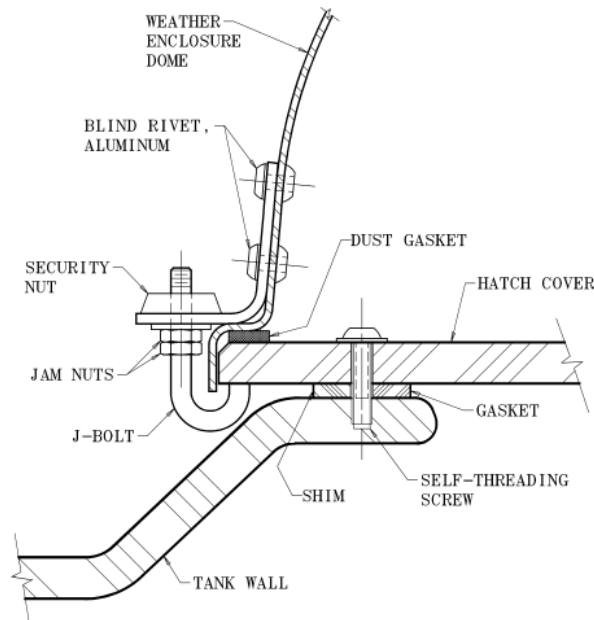


Fig. 2. Details of the hatchcover sealing system and the electronics weather enclosure dome attachment

209 Creep over the 20 years lifetime might also cause the tank to deform. Creep  
 210 measurements of samples of our resins and extensive finite element analysis  
 211 indicate that creep would not be a problem. Indeed, no evidence of either creep  
 212 distortion or ultraviolet degradation have been observed in any tank, some of  
 213 which have been in service for over five years.

### 214 3.2 Hatch Covers and Electronics Enclosure

215 As can be seen in Figs. 1 and 2, the tank hatches are elevated, to prevent  
 216 rainwater from accumulating around the hatchcover and leaking into the tank.

217 The hatchcover assemblies for the three hatch openings (one large, 560 mm  
 218 diameter, and two small, 450 mm diameter) consist of hatchcovers, gaskets,  
 219 shims between the tank and hatchcover, and fastening screws. They seal and  
 220 protect the tank contents, keeping out light, water and dust. They are easily  
 221 removable for access to the tank contents. The large hatchcover is the mount-

222 ing location for the electronics and has penetrations for cable feed-throughs.

223 The hatchcovers are of similar material to the tank itself so that stresses in the  
224 attaching screws are minimized. Hatchcovers are machined from 12.7 mm high-  
225 density, two-layer polyethylene (HDPE) sheets with beige on the outer side  
226 and opaque black on the inner side. The shape of the hatchcover is a simple  
227 disk with 24 equally spaced holes around the outer edge for the attaching  
228 screws.

229 The purpose of the shim is to control the spacing between the tank top and the  
230 hatchcover at the location of the gasket, to limit its amount of compression.  
231 The shims (polyethylene) and gaskets (foam polyurethane) are bonded to the  
232 hatchcover using 3M 9472 acrylic adhesive transfer tape<sup>1</sup> which is particularly  
233 good at bonding to low surface energy materials, including polyethylene.

234 The hatchcovers are attached to the tanks using self threading screws designed  
235 for thermoplastics, identified as Plastite 48-2. The 5.3 mm diameter screws are  
236 made from stainless steel and have a tamper-resistant (pin-in-head) Torx head  
237 for increased security.

238 The detector electronics enclosure is mounted on the large hatchcover and  
239 protected by a weather enclosure, a dome that provides rain and dust pro-  
240 tection and the outer security layer. The dome can be seen in Fig. 1. The  
241 dome itself is spun from 2.3 mm soft aluminum. A foam polyurethane dust  
242 gasket is installed inside the lower lip so that it compresses against the large  
243 hatchcover. The dome is painted beige to match the color of the tank. The  
244 hold-down system for the weather enclosure consists of a bracket riveted to  
245 the dome, a J-bolt which engages the large hatchcover, two jam-nuts and one  
246 security nut, which can be opened only with a special tool.

### 247 *3.3 Battery Box System*

248 Attached to the Surface Detector is a rotational molded polyethylene box  
249 containing the batteries and charge regulator for the solar power system. The  
250 battery box, visible in Fig. 1, is placed on the southern side of the tank, where  
251 the tank protects it from direct sunlight to keep the temperature low and thus  
252 increase the lifetime of the batteries. A polyethylene plate is screwed to the  
253 bottom of the box and extends below the tank to anchor the box, deterring  
254 theft or displacement by large animals. The box has a rounded back with  
255 radius of curvature equal to the tank radius to fit close to the tank. The  
256 corners of the box are rounded to discourage rubbing by cows. The interior of  
257 the box is lined with 50 mm polystyrene foam sheets as thermal insulation.

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<sup>1</sup> 3M, St. Paul, Minnesota, U.S.A., [www.3m.com](http://www.3m.com)

258 The top of the box has a slope to deter its use as a step to get on the tank.  
259 The lid is held on with security-head screws. A protective cover is mounted  
260 to the tank to shield the power system cables that run from the inside of the  
261 tank, above the water level, to the interior of the battery box.

## 262 4 Solar Power System

### 263 4.1 Solar panels and batteries

264 Power for the electronics is provided by a solar photovoltaic system. The power  
265 system provides the required 10 W average power. A 24-V system has been  
266 selected for efficient power conversion for the electronics.

267 Using the available insolation data for the Auger site, it was found that a  
268 suitable power system can be obtained with two 55 Wp panels<sup>2</sup> and two  
269 105 Ampere-hour (Ah), 12 V batteries. Power is expected to be available over  
270 99% of the time. Even if after long-term operation the capacities of the solar  
271 panels and batteries are degraded to 40 Wp and 80 Ah, respectively, power  
272 would be available 97.8% of the time.

273 The batteries<sup>3</sup> selected for the project are a new type of lead acid battery  
274 designed for solar power applications. They have a selectively permeable mem-  
275 brane and do not require maintenance. Other lead-acid battery technologies  
276 are being considered for replacement batteries as these wear out.

277 The charge controller<sup>4</sup> was selected for robust design and construction, to  
278 maximize the lifetime expectations. An encapsulated, epoxy potted model  
279 with robust surge protection was found in the solar power market. The con-  
280 troller is pulse width modulated and operates by applying pulses of current of  
281 varying width to the batteries, as their state of charge varies with battery volt-  
282 age and temperature. This is considered to be the best method of charging for  
283 maintaining battery efficiency and lifetime. There have been no observations  
284 of electronics interference arising from the charge controller.

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<sup>2</sup> Wp is a unit expressed in watts for solar panel output with a standard solar irradiation applied.

<sup>3</sup> Model 12MC105, Acumuladores Moura S.A., Brazil, [www.moura.com.br](http://www.moura.com.br)

<sup>4</sup> SunSaver SS-10-24V, Morningstar Corporation, U.S.A.,  
[www.morningstarcorp.com](http://www.morningstarcorp.com)

## 285 4.2 *Solar Panel Support Brackets and Masts*

286 The solar panel bracket supports the solar panels and includes the mast that  
287 supports the communications antenna and the GPS antenna. The bracket sys-  
288 tem is designed to withstand  $160 \text{ km h}^{-1}$  winds. The brackets are built using  
289 aluminum 38 mm square tubing with aluminum blind rivets, and the alu-  
290 minium alloys used were selected for good corrosion resistance. The brackets  
291 are prepared by cutting, drilling and riveting most of the assembly in a factory.  
292 A few of the rivet holes are not drilled until the bracket is test-fitted to the  
293 tank, so that the variability in the dimensions from tank to tank is compen-  
294 sated for. The assembly of the solar panels to the brackets and of the brackets  
295 to the tank is completed before the detectors are taken out into the field, but  
296 the brackets are left in a collapsed configuration for ease of transportation.  
297 When the detector is in its final position the panels and mast are raised and  
298 locked in place by a single bolt.

## 299 4.3 *Power Cabling*

300 By mounting the electronics directly on the hatchcover, the length of cables  
301 and the number of connections and feed-throughs are minimized. The power  
302 cables run from the solar panels to the electronics enclosure and from there  
303 through the interior of the tank to the battery box. They penetrate the large  
304 hatchcover and the tank with light- and water-tight cable feedthroughs. The  
305 only cables exposed to the outside world are the two antenna cables and the  
306 solar power cable coming from the bracket assembly and entering the electron-  
307 ics enclosure. They are UV protected for outside use. Heavy gauge wiring was  
308 selected for robustness rather than for electrical resistance considerations.

309 Sensor cables are installed with the power cables. Voltage of the individual  
310 batteries, their charge and discharge current as well as the temperatures of  
311 the batteries and the bases of the PMTs are monitored and registered in 6-  
312 minute intervals. The monitoring of the batteries is also required as the tank  
313 power control board is designed with the capability of setting the local station  
314 in hibernation mode if the voltage drops too low after many days without  
315 sunshine. After a period of prolonged cloudiness, all stations of the array can  
316 be shut down simultaneously rather than shutting down individual stations,  
317 minimizing recovery times and maximizing data integrity. Power system con-  
318 nectors are automotive grade, gold-plated for long durability in the harsh field  
319 conditions.

320 A grounding rod is driven into the ground at the opening between the bat-  
321 tery box and the tank and connected to the negative terminal to provide the

322 electronics system grounding.

## 323 **5 Liners**

### 324 *5.1 Development and Design*

325 Tank liners are right circular cylinders made of a flexible plastic material  
326 conforming approximately to the inside surface of the tanks. The liners fulfill  
327 three functions: they enclose the water volume, preventing contamination or  
328 the loss of water and providing a barrier against any light that enters the  
329 closed tank; they diffusively reflect light traversing the water; and they provide  
330 optical access to the water volume for the PMTs, such that PMTs can be  
331 replaced without exposing the water to the environment.

332 The liners also must not contaminate the pure water themselves. Three dome  
333 windows and five fill ports with screw caps are hermetically sealed to the liner.  
334 The window assemblies allow for the mounting of the PMTs. The fill ports  
335 allow for filling and venting the tank, as well as providing a window for an  
336 LED flasher used for initial testing.

337 Although the tanks provide the primary light barrier for external light sources,  
338 it is necessary that the liners be completely opaque to act as a secondary  
339 protection against small light leaks. Initial tests were performed to ensure  
340 that the laminate and the seals are completely opaque against single-photon  
341 level light transmission, i.e., a 0% light transmission for light of wavelengths  
342 between 300 and 700 nm, as measured by counting single-photon detection  
343 rates.

344 Although the mass of water moderates temperature fluctuations, the temper-  
345 ature range to which the liner is exposed is from nearly  $-10^{\circ}\text{C}$  to  $+50^{\circ}\text{C}$ . Up to  
346 10 cm of ice could form at the upper surface or sides of the water volume. The  
347 liner is designed to be sufficiently strong and flexible that it is not damaged  
348 by such ice formation. Ice is prevented from forming near the PMT windows  
349 by mounting insulating rings of polystyrene foam. Strength and flexibility are  
350 also required to withstand the formation of waves up to 15 cm high on the  
351 surface of the water produced by eventual seismic activity. The Observatory  
352 is located in an area rated for moderate seismic activity and the detector was  
353 designed to resist damage from such activity.

354 Liner materials require strength, opacity to external light, diffuse reflectivity  
355 of inner surface, sealability, resistance to chemicals from the environment and  
356 to biological activity and minimal extractables from the material which might

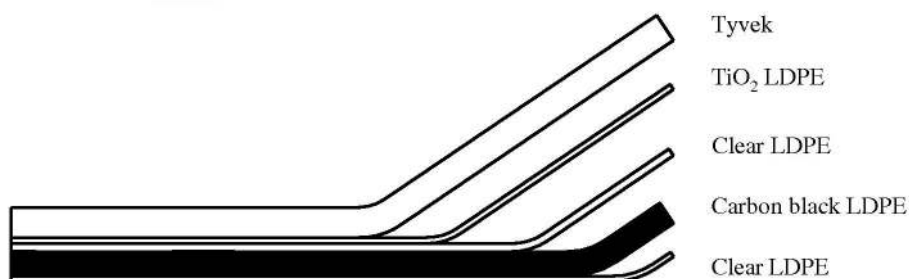


Fig. 3. A sketch of the laminate, showing the outer Tyvek<sup>®</sup> layer, the medium TiO<sub>2</sub> LDPE layer and the 3-layer with clear LDPE, LDPE with carbon-black and clear LDPE.

357 contaminate the water volume enclosed.

358 The liners are produced from a laminate composed of an opaque three-layer  
 359 co-extruded low-density polyethylene (LDPE) film bonded to a 5.6 mils thick  
 360 layer of Dupont Tyvek<sup>®</sup> 1025-BL<sup>5</sup> by a layer of Titanium-dioxide pigmented  
 361 LDPE of 1.1 mils thickness (see Fig. 3). The three-layer co-extruded film consists  
 362 of a 4.5 mils thick carbon black loaded LDPE formulated to be opaque to  
 363 single photons, sandwiched between layers of clear LDPE to prevent any carbon  
 364 black from migrating into the water volume. The LDPE was metallocene  
 365 catalized linear low-density polyethylene (LLDPE) with excellent strength  
 366 and flexibility. Tyvek<sup>®</sup> 1025-BL was chosen as the reflective layer due to its  
 367 strength and excellent diffuse reflectivity for Cherenkov light in the near ultra-  
 368 violet [22,23]. Tyvek<sup>®</sup> 1025-BL is an untreated polyolefin non-woven material,

<sup>5</sup> E.I. du Pont de Nemours and Co., Wilmington, Delaware, U.S.A.,  
 www.dupont.com

369 which minimizes the chemicals available to leach into the water volume. It is  
370 the thinnest of the “biological grade” Tyvek<sup>®</sup> commercially available, which  
371 simplifies the bonding processes used in manufacturing liners.

372 Polyolefin film has a strong tendency to pick up electrostatic charge when un-  
373 rolled or pulled over a surface and even in a very clean assembly environment  
374 would collect significant dust during the hours involved in liner assembly. The  
375 method for controlling contamination of the liners centers on minimizing food  
376 sources for microbes by eliminating hair and skin contact with the lamination  
377 and working in a reasonably clean environment. Although the Auger lamina-  
378 tion is not produced in a “clean room” environment, the extruders, lamination  
379 machines and slitting machines are all cleaned prior to production of the Auger  
380 lamination, and hair restraints and gloves are worn during all handling of the  
381 film.

## 382 *5.2 Assembly and Testing*

383 Liners are assembled by first manufacturing three separate sections of laminate  
384 and then sealing them together. The separate sections are the bottom, side  
385 strip, and top. The liner top is the most complex section since it includes  
386 the PMT and LED windows and fill/vent ports. Seals are made by welding  
387 the layers together under pressure with custom designed impulse heat seal  
388 machines. The liner tops were assembled using the same cleanliness procedures  
389 as for laminate manufacture mentioned above. Final liner assemblies were done  
390 in a class 100 000 clean room specially set up for this project.

391 All liners were tested for leaks and flaws, and any defects were repaired before  
392 packing and shipping to the site. The same tests were repeated at the assembly  
393 site prior to installation.

394 For testing, the liner is inflated to a pressure of 20 millibar over atmospheric  
395 pressure, see Fig. 4. Then all the seals are tested using a soap bubble solution,  
396 looking for visible signs of bubbling. The liner is then examined in a darkened  
397 room with bright lights covering the window ports such that they only illu-  
398 minate the interior of the liner. Any visible light leaking out from the liner  
399 indicates a fault requiring repair. The testing procedures described above were  
400 determined to be sensitive to leaks smaller than those which could cause a loss  
401 of 10% of the detector volume in 20 years.



Fig. 4. An inflated liner during testing.



403 The PMT enclosures have been designed to allow the PMT to collect Cherenkov  
404 light from the water detector volume while providing for a cover to shield the  
405 PMT from external light and protecting it from the external environment (see  
406 Fig. 5).

407 The foundation of the PMT assembly is an annular, LLDPE flange that is  
408 heat-sealed directly to a hole in the top of the liner using a custom circular  
409 heat impulse welder. The window through which the PMT views the water  
410 is made of UV-transparent LLDPE. The windows are vacuum formed to fit  
411 approximately the nominal PMT face. The window is heat sealed to the flange.  
412 Using heat seals rather than any adhesive insures that the only material in  
413 contact with the water is polyethylene. The PMT is protected on the top  
414 from light by an injection-molded ABS plastic cover called the “fez”. For  
415 installation the PMT is indexed with respect to the fez using an internal  
416 polystyrene foam collar that is bonded to the PMT neck. The variance in  
417 the PMT face shape results in a few millimeters uncertainty on the space  
418 between the window and the PMT face, and that space is filled with 150 ml of  
419 the silicone optical compound GE6136 RTV<sup>6</sup>. Without the optical coupling  
420 approximately half the light from the tank is lost due to total internal reflection  
421 and direct reflection from the interfaces. The fez, with PMT in place, is sealed  
422 to the flange using black GE 123 RTV<sup>6</sup> at the time that the optical seal is  
423 made. The fez has four ports. One port is a light-tight air vent to prevent  
424 pressure buildup due to temperature changes. The other three ports are for  
425 cable feed-throughs. These are custom molded two-piece parts (identical left  
426 and right parts) that clip around the cables and clip to flat annular regions on  
427 the fez. There are similar feed-throughs to pass cables through the bottom of  
428 the hatch cover into the electronics enclosure. Finally there are two annular  
429 polystyrene foam insulation pieces that fit inside the fez to prevent ice buildup  
430 near the PMT. One insulation piece is the same one that fits on the PMT neck  
431 to fix its position with respect to the fez. The other fits at about water level  
432 and fills the space between the inside of the flange and the top of the bulb of  
433 the PMT glass. Tests show that ice will form in extreme years on the water  
434 surface, but with the insulation in place it will not stress the optical coupling  
435 or the PMT itself.

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<sup>6</sup> General Electric Company, U.S.A., [www.gesilicones.com](http://www.gesilicones.com)

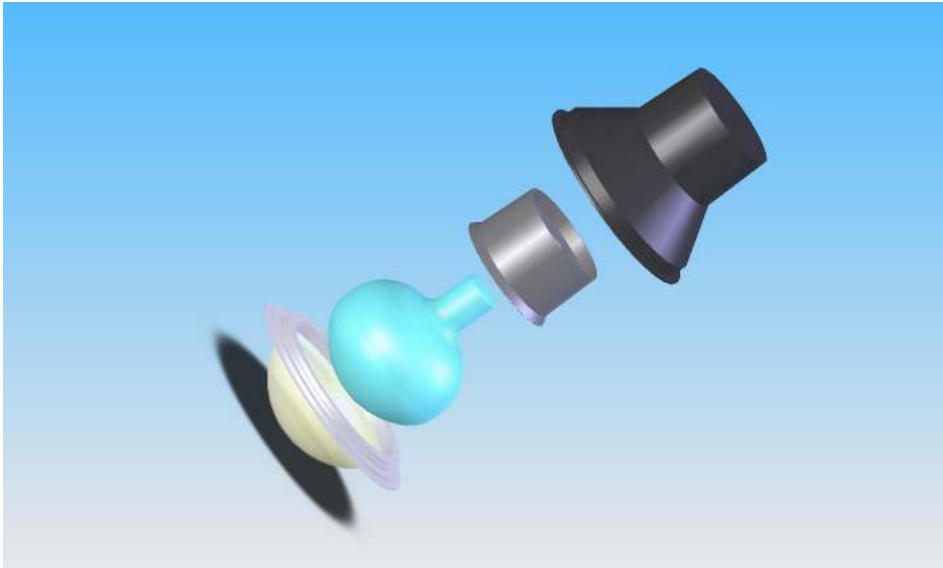


Fig. 5. Mechanical housing for the PMT (top to bottom): Outer ABS plastic housing; insulating plug affixed to the PMT neck that centers the PMT and sets the distance of the PMT face to the window; PMT; flange to which the housing is glued with a room- temperature RTV; UV-transparent window which is fixed to the PMT using a UV-transparent optical coupling.

## 436 6 Water

### 437 6.1 Water Quality Specification

438 Each surface detector contains 12 000 l of ultra-pure water. The high water  
439 purity is required for two purposes: to achieve the lowest possible attenuation  
440 for UV Cherenkov light, and to guarantee stability of the water during the  
441 20 years of operation of the detectors.

442 For these reasons, the detector water needs to be deionized and completely  
443 free of microorganisms and nutrients. After consulting experts in pure water  
444 production, it was established that the best achievable water quality requires  
445 a water treatment that gives an output water of resistivity above 15 M $\Omega$ -cm.

446 The production rate of the water plant has to be high enough to ensure that  
447 it can provide water to the detectors at the same rate as they are deployed.  
448 This requirement corresponds to up to 36 000 l/day, which would allow us to  
449 fill up to 90 detectors per month.

### 450 6.2 Water Production

451 The pure water required for the surface detectors is produced at a plant owned  
452 and operated by the Auger Observatory and installed at the Central Campus  
453 in Malargüe.

454 Water is provided both from a local well at 80 m depth and from the city of  
455 Malargüe water network and pumped to a cistern with 60 m<sup>3</sup> capacity where  
456 it is chlorinated and stored. The water plant is fed from this cistern. As the  
457 quality of the city water is considerably better than the underground water  
458 but more expensive, the admixture allows an increased production rate and  
459 reduced contamination in the effluents at the lowest cost.

460 The water purification follows four stages:

- 461 (1) Pre-processing:
- 462 • Prefiltering, to eliminate particles greater than 40  $\mu\text{m}$ .
  - 463 • Softening with a resin bed for strong cationic exchange, with regenera-  
464 tion by sodium chloride, to eliminate Ca<sup>++</sup>, Mg<sup>++</sup> and Fe ions.
  - 465 • Addition of antiscaling solution, to avoid deposit of silicates on the reverse  
466 osmosis membranes (see below).
  - 467 • Addition of chlorine reducer to eliminate active chlorine.
  - 468 • Microfiltering with two pairs of polypropylene microfilters to eliminate

- 469 particles greater than 5  $\mu\text{m}$ .
- 470 • Ultraviolet disinfection with a 254-nm UV unit (64 W power), to elim-  
471 inate microorganisms from the water.
- 472 (2) Reverse osmosis: A high-pressure centrifugal pump pressurizes the wa-  
473 ter and pumps it to the reverse osmosis unit, consisting of two modules  
474 in parallel with 4 membranes each and, in series at their output, a third  
475 module with 4 membranes. Maximum input flow is 4500 l/h, with a max-  
476 imum output of 2800 l/h. The output water resistivity is  $\sim 100 \text{ k}\Omega\text{-cm}$ .
- 477 (3) Ultraviolet purification: an ultraviolet source of 185 nm eliminates micro-  
478 biological residues and removes Total Organic Carbon (TOC).
- 479 (4) Continuous Electrodeionization (EDI): To achieve the required final water  
480 quality (resistivity above 15  $\text{M}\Omega\text{-cm}$ ), the product of the reverse osmosis  
481 process is fed to an EDI unit<sup>7</sup>, which consists of a set of membranes with  
482 cationic and anionic transfer. The production capacity of this unit is up  
483 to 3400 l/h.

484 The high-purity output water is stored in a 50 000 l storage tank. A recircu-  
485 lation system, which also permits quality improvement through a mixed resin  
486 bed and UV treatment (254 nm, 151 W), can recirculate up to 5 500 l/h. The  
487 pumping system of this recirculation is also used to fill the transport tank.

488 The water plant is fully automated. Instruments monitor the working param-  
489 eters of the water plant: a chlorine monitor at the entrance of the reverse  
490 osmosis membranes, pressure gauges, flux gauges, flow meters and resistivity  
491 meters. A programmable logical controller (PLC) records the relevant produc-  
492 tion parameters.

### 493 6.3 Water Testing and Handling

494 The two most relevant parameters that give information about water quality  
495 are its resistivity and biological activity. Resistivity can be measured contin-  
496 uously at the output of the water plant and in the storage tank with the  
497 instruments incorporated at the water plant. Resistivity of the water in the  
498 transport tank and in the detectors is determined with hand-held conductivity  
499 meters. Although the water resistivity degrades during transportation, prob-  
500 ably due to absorption of carbon dioxide, tanks in the production phase are  
501 filled with water of 8 to 10  $\text{M}\Omega\text{-cm}$ . During the initial phases of the project,  
502 Engineering Array tanks were filled with water of less than 1  $\text{M}\Omega\text{-cm}$  quality  
503 and they worked as required for nearly 4 years [21].

504 The TOC, i.e., potential nutrients for bacteria, is removed by the short wave-

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<sup>7</sup> Model E-Cell MK-1 PHARMA, General Electric Company, U.S.A.,  
www.gewater.com

505 length UV exposure followed by deionization. The plant manufacturer specifies  
506 that 10 ppb should be achieved. It is not feasible to measure TOC in the tanks  
507 deployed in the field with the required accuracy, so TOC was only measured  
508 a few times at the output of the water plant, yielding values below 100 ppb.

509 To determine the biological activity in the water, samples are taken periodi-  
510 cally from the storage tank, the transport tank and the detectors themselves.  
511 These samples are kept in a sterile container and sent to a biochemists' lab-  
512 oratory to perform the corresponding analysis and search for aerobe meso-  
513 phylls, coliforms, faecal coliforms, coliforms in Koser citrate, yeasts and fungi  
514 in Agar Saboreaud medium. In most of the cases, no biological activity has  
515 been found. Some isolated tanks showed contamination with low quantities of  
516 aerobe mesophylls, identified as being of the genus "Serratia", which might  
517 originate from contamination during sampling or during sample transporta-  
518 tion. In all cases, the initially detected bacterial contamination was low (below  
519 2000 colony forming bacteria per ml) and these tanks were monitored period-  
520 ically and in no case could a large or steady increase in bacterial activity be  
521 detected.

#### 522 6.4 Long-Term Stability

523 The long-term trends in water quality are tracked using the on-line tank cal-  
524 ibration and monitoring system that is active for every station and updates  
525 every four hours [20]. In this application, the time structure of the collected  
526 Cherenkov light produced by through-going muons is recorded to measure the  
527 water purity indirectly [24]. Use of the calibration and monitoring system has  
528 the advantage that every station in the array can be followed and the great  
529 quantity of data collected allows some predictive power even if the measure-  
530 ment lacks the directness of water sampling.

531 The charge registered in the fast analog-to-digital converter from single muons  
532 rises rapidly, peaks, and then decreases exponentially. The decay time depends  
533 on the rate of Cherenkov light absorption and on the reflectivity of the interior  
534 of the liner. Measuring the time constant quantifies the amount of Cherenkov  
535 light that is absorbed in a way that is largely unrelated to the absolute photo-  
536 electron count. An absolute photon count depends on more than just the  
537 amount of absorption in a station. Although it is possible to fit the muon  
538 traces directly and obtain the time constant, this method is dependent on  
539 the precise details of the fitting procedure. For this reason  $Q_{VEM}$  (the total  
540 charge deposit by a vertical muon) divided by  $I_{VEM}$  (the signal maximum for  
541 a vertical muon) is used as a substitute for the actual time constant. That  
542 ratio can then be examined as a function of time to search for trends that  
543 have time scales in the range of a few months to several years.

544 Application of this technique allowed us to observe a decline by 10% in the  
545  $Q_{VEM}/I_{VEM}$  ratio in the first several months after deployment, at which time  
546 it reaches an equilibrium. The origin of this behaviour is still under inves-  
547 tigation. After this the water quality is nearly constant with a small annual  
548 oscillation of less than 1% in the  $Q_{VEM}/I_{VEM}$  ratio, linked to seasonal changes.

## 549 7 Detector Assembly and Deployment

### 550 7.1 Detector Assembly

551 The assembly of the surface detector stations is done in the Assembly Building  
552 located at the Central Campus of the Observatory in Malargüe. The differ-  
553 ent components are received and assembled into a complete detector in this  
554 building, which provides workspace for eight detectors at a time.

555 When received, tanks are unloaded and inspected. Using a template, holes are  
556 drilled to guide the hatchcover screws and the hatches are closed to keep water  
557 and dirt out of the tank during outdoor storage. Dimensional measurements,  
558 including ultrasonic measurements of the tank wall thickness, are performed  
559 to ensure tank quality. After cleaning, the tank interior is checked for imper-  
560 fections that could damage the liner. Holes for venting, water drain and cable  
561 feed-throughs are drilled into the tank, cables are passed through the interior  
562 of the tank and the liner is inserted and inflated with filtered air. PMTs are  
563 installed and glued to the liner window domes using optical RTV. Fezzes are  
564 mounted over the PMTs to ensure a light-tight seal. The remaining items are  
565 mounted to the tank: the half-pipe to protect the cables running outside the  
566 tank, the solar panel brackets with solar panels and the electronics enclosure  
567 dome. The liner is kept inflated with air for safe transportation to the field,  
568 and foam pads are inserted between the PMT fezzes and the hatchcovers to  
569 provide cushioning of PMTs during transportation. Six full time technicians,  
570 one foreman and an administrative assistant (for data entry, inventory and  
571 parts receiving and management) can assemble eight tanks every two days.  
572 This includes the assembly of the solar panel brackets and the preparation of  
573 the battery boxes. PMTs are tested in the Assembly Building after installa-  
574 tion, and serial numbers of the main detector parts are recorded and entered  
575 into the parts management database.

576 Detector deployment involves survey and site preparation, delivery of the de-  
577 tector units to their prepared locations, delivery of water and installation of  
578 the components necessary to complete the detector. The main challenge for  
579 deployment is transportation over difficult and variable road conditions, par-  
580 ticularly with heavy loads of water. Access to detector locations is affected by

581 seasonal and daily weather conditions.

## 582 *7.2 Site Survey and Preparation*

583 Prior to detector deployment, the ground for each surface detector location is  
584 prepared following these steps:

- 585 • A contract surveyor marks the location where each detector is to be deployed  
586 with two stakes oriented north-south at a distance of roughly 10 m from each  
587 other. The surveyor provides the Project with information on the positioning  
588 of both stakes (including altitude) with centimeter precision, as well as  
589 information on ground conditions.
- 590 • A circular area of 6 m radius is cleared of vegetation. At locations with pam-  
591 pas grass (“cortadera”) or heavy brush, the circular cleared area is increased  
592 to 10 m radius to reduce the seasonal fire hazard. Local environmental reg-  
593 ulations and procedures are observed.
- 594 • A central circular area of 2.5 m radius is prepared by clearing it of stones,  
595 roots and other sharp objects and irregularities to avoid damage to the tank  
596 bottom. the ground is leveled to within 3 cm to avoid overloading the walls  
597 of the detector tank and to provide a uniform water depth and PMT height.

598 The aim was to place all of the detectors on a hexagonal grid of 1500 m  
599 spacing. However, for practical reasons, deviations from this ideal have been  
600 inevitable although the median location is within 12 m of the optimum po-  
601 sition. Only 4% of the detector positions are more than 50 m away from the  
602 ideal location, with 0.4% of the detectors being displaced more than 100 m.  
603 These large displacements (which have little impact on reconstruction accu-  
604 racy) were necessary because of a cultivated area, a riverbed or a swamped  
605 and inaccessible area.

## 606 *7.3 Deployment*

607 The deployment procedure starts with loading assembled tanks and transport-  
608 ing them to a staging area at the site. Tank transport to the staging area is  
609 done with flatbed tractor-trailer trucks carrying four tanks at a time. Staging  
610 areas are selected to be approximately equidistant from the four deployment  
611 locations and in an area where the truck transporting the tanks can easily  
612 maneuver. An escort vehicle carries other components for deployment.

613 Loading at the Assembly Building is done with a forklift truck. All tank lifting  
614 is performed using the lifting lugs molded into the top of the tanks along with  
615 clevises and straps. Unloading and further transportation at the site requires

616 a truck capable of carrying a single tank and equipped with a hydraulic crane.  
617 Such trucks are commonly used for transporting bricks, drywall, roofing ma-  
618 terials and other construction supplies. While being unloaded and positioned,  
619 the tank is oriented such that the solar panel will face north ( $5^\circ$  tolerance) as  
620 determined with a compass. Once the tank is positioned, the battery box is  
621 installed at the south side of the tank and batteries and charge regulator are  
622 installed and connected.

623 Water is delivered to the detector as discussed in the following section. During  
624 water filling, the water delivery team installs the communications antenna kit  
625 and the GPS antenna and mounts them to the mast.

626 Finally, installation of the electronics kit is performed by a team of two elec-  
627 tronics technicians. The electronics for the detector station are tested and the  
628 detector is commissioned. Contact via a mobile radio system to a data ac-  
629 quisition technician at the Central Campus allows the deployment technician  
630 to check that the detector is performing correctly and sending triggers to the  
631 central data acquisition system at the Central Campus before leaving the field.  
632 At this stage the detector is fully integrated into the data taking system.

#### 633 7.4 *Water Delivery*

634 Water is delivered to each detector tank (12 000 l) in one filling, with a sin-  
635 gle hose connection. Only a single connection is used in an effort to prevent  
636 contamination by bacteria and/or potential nutrients.

637 A water delivery system is composed of two 12 500 l tanks, one mounted on  
638 the back of a truck and one mounted on a trailer. Each tank has an electrically  
639 powered pump, a gasoline powered generator, hoses, connections and acces-  
640 sories. The trailer is pulled by the truck on easy access roads and tracks. To  
641 access the more difficult areas, the trailer or the truck are pulled by a large  
642 front-end loader. The front-end loader is also used to even out irregular roads  
643 and to compact the ground in wet areas.

644 The transport tank system has the following characteristics:

- 645 • The first transport tank that was acquired for water delivery was made of  
646 fiberglass-reinforced polyester resin with food-grade protective coatings on  
647 the inside. The maximum allowable working differential pressure of the tank  
648 is 100 cm of water. For full scale deployment, three additional tanks were  
649 purchased, made of stainless steel (AISI 304 with 2-b sanitary finishing) as  
650 this is more robust to damage in the harsh field conditions and can be kept  
651 clean more easily. Two of these tanks were mounted on trucks and two on  
652 trailers.



- 653 ● A 0.2  $\mu\text{m}$  bacteriological filter is connected to the air inlet of the tank to  
654 filter the air that is sucked into the transport tank as the water is pumped  
655 out. A valve is installed below the filter, to ensure that the water cannot  
656 splash the filter during truck movements because the filter has a very high  
657 pressure drop when wet. The valve is opened when the tank is being emptied  
658 to allow inflow of air.
- 659 ● Each tank has a manway to allow access for cleaning. A pressure relief valve  
660 is installed at the manway to avoid damage to the tank by overpressure  
661 during filling.
- 662 ● There is a transparent plastic window on the tank for direct visual inspec-  
663 tion.
- 664 ● A 50 mm hose and associated valves are installed to transfer the water  
665 from the transport tank to the detector. The end of the hose is connected  
666 to a bayonet that has a valve to regulate water flow and a freely rotating  
667 cap that can be screwed to the liner opening. During transportation, the  
668 bayonet is protected with a stainless steel scabbard which can be screwed  
669 to the bayonet with an airtight seal.
- 670 ● The electrically driven stainless steel centrifugal pump installed to transfer  
671 the water has a capacity of 120-300  $\text{l min}^{-1}$ .
- 672 ● All accessories in contact with water are stainless steel with a sanitary finish  
673 to prevent corrosion and formation of bacterial colonies.

674 The recirculation system of the water plant is used to fill the transport tank.  
675 This allows a flow of 12 500 l in 50 minutes. Before filling the tank the water  
676 conductivity is tested with a hand-held conductivity meter. To fill the detec-  
677 tors, hatch covers are removed after cleaning the tank surface, one liner cap  
678 is opened and the bayonet, after being rinsed thoroughly, is introduced into  
679 the liner and screwed to the liner opening, and the pump is turned on. A  
680 second liner port is opened for air release. The filling of the detector takes  
681 approximately 45 minutes. The height of the water column is determined by  
682 measuring the height of the tank and subtracting the height of the water  
683 level, measured from the top of the tank. This gives a precision of 1-2 cm. The  
684 level is measured at different hatch openings to avoid systematic errors due  
685 to any possible tank tilt. After filling, any remaining air is pumped out of the  
686 liners with a vacuum cleaner. Once deployed, water level measurements can  
687 be obtained from the slope of the charge histogram from single muon tracks  
688 [25,24].

689 After pauses in water deployment of five to six days, the transport tanks and  
690 all accessories are cleaned and disinfected, and filters are checked and replaced  
691 as required. Cleaning is done with detergent, bleach and a very thorough rinse.

## 692 8 Performance and Conclusions

### 693 8.1 Performance, Maintenance and Operation

694 As of July 2007, more than 1300 surface detector stations are operational.  
695 Typically more than 98.5% of the stations are operational at any time. The  
696 technical staff distributes its time between deployment of new detectors and  
697 maintenance and repair of down stations.

698 Only seven liners were observed to leak shortly after installation. In these  
699 cases, which constitute the worst failure mode, the tank is emptied and brought  
700 back to the Assembly Building for replacement of the interior components.

701 There have been very few instances of human interference with the surface  
702 detectors. During 5 years of operation, only 12 solar panels have been damaged  
703 and two have been removed (both from locations along side a paved road).

704 Solar power system parameters are recorded and analyzed using the central  
705 data acquisition system. Failures are treated on an individual basis. Moni-  
706 toring software for the solar power system has been developed to make this  
707 monitoring routine for operating personnel and scientists either on shift at the  
708 site or elsewhere by internet access. The lifetime of batteries is estimated to  
709 be four years. The batteries will be monitored along with the rest of the solar  
710 power system. The condition of the batteries can be determined from the data  
711 (voltages, currents, and temperatures) that are being monitored and the weak  
712 batteries can therefore be identified weeks or even months before complete  
713 failure occurs. Batteries can then be scheduled for replacement by the routine  
714 maintenance process.

715 In conclusion, with over 1300 commissioned detectors in the field, some of  
716 which have already been operational for over five years, much insight on their  
717 performance has been gained. All components of the above-described detector  
718 hardware have fully met our design expectations. The design has proven suf-  
719 ficiently robust to withstand the adverse field conditions and failure rates are  
720 less than expected. Data taking is ongoing and the first scientific results have  
721 already been published. The physics performance has met or exceeded all of  
722 our requirements.

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740 Ministerium für Wissenschaft und Forschung Nordrhein Westfalen, Ministerium  
741 für Wissenschaft, Forschung und Kunst Baden-Württemberg, Germany; Istit-  
742 tuto Nazionale di Fisica Nucleare and Ministero dell'Istruzione, dell'Università  
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## 755 References

- 756 [1] J. Linsley, Phys. Rev. Lett. **10**, 146-148 (1963)  
757 [2] K. Greisen, Rev. Lett. **16**, 748 (1966)  
758 [3] G.T. Zatsepin, V.A. Kuz'min, JETP Letters **4**, 78 (1966)  
759 [4] M. Nagano, A.A. Watson, Rev. Mod. Phys. **72**, 689 (2000)

- 760 [5] Pierre Auger Observatory Design Report (March 1997), [www.auger.org/admin](http://www.auger.org/admin)
- 761 [6] The Pierre Auger Collaboration, "First Estimate of the Primary Cosmic Ray  
762 Energy Spectrum Above 3 EeV from the Pierre Auger Observatory", Proceedings  
763 of the 29th International Cosmic Ray Conference, Pune, India, **7**, 387 (2005)
- 764 [7] M. Roth for the Pierre Auger Collaboration, "Measurement of the UHECR  
765 energy spectrum using data from the Surface Detector of the Pierre Auger  
766 Observatory", Proceedings of the 30th International Cosmic Ray Conference,  
767 Merida, Mexico (2007), H.E. 1.4.A - 313. arXiv:0706.2096v1 [astro-ph]
- 768 [8] M.A. Lawrence, R.J.O. Reid and A.A. Watson, *J. Phys. G* **17**, 733 (1991)
- 769 [9] T. Suomijarvi et. al. for the Pierre Auger Collaboration, "The Electronics System  
770 of the Surface Detectors of the Pierre Auger Observatory", in preparation
- 771 [10] T. Suomijarvi for the Pierre Auger Collaboration, "Performance of the  
772 Pierre Auger Observatory Surface Detector", Proceedings of the 30th  
773 International Cosmic Ray Conference, Mérida, Mexico (2007), H.E. 1.4.A - 299.  
774 arXiv:0706.4322v1 [astro-ph]
- 775 [11] P. Facal San Luis for the Pierre Auger Collaboration, "Measurement of the  
776 UHECR spectrum above  $10^{19}$  eV at the Pierre Auger Observatory using showers  
777 with zenith angles greater than  $60^\circ$ ", Proceedings of the 30th International Cosmic  
778 Ray Conference, Mérida, Mexico (2007), H.E. 1.4.A - 319. arXiv:0709.1823v1  
779 [astro-ph]
- 780 [12] D. Allard et. al. for the Pierre Auger Collaboration, "Aperture calculation of the  
781 Pierre Auger Observatory surface detector", Proceedings of the 29th International  
782 Cosmic Ray Conference, Pune, India, **7**, 71 (2005)
- 783 [13] I. Allekotte et. al, *J. Phys. G: Nucl. Part. Phys.* **28**, 1499 (2002)
- 784 [14] P. Ghia for the Pierre Auger Collaboration, "Statistical and systematic  
785 uncertainties in the event reconstruction and S(1000) determination by the Pierre  
786 Auger surface detector", Proceedings of the 29th International Cosmic Ray  
787 Conference, Pune, India, **7**, 167 (2005)
- 788 [15] M. Ave et. al. for the Pierre Auger Collaboration, *Nucl. Inst. & Meth.* **A578**,  
789 180 (2007)
- 790 [16] C. Bonifazi for the Pierre Auger Collaboration, "Angular Resolution of the  
791 Pierre Auger Observatory", Proceedings of the 29th International Cosmic Ray  
792 Conference, Pune, India, **7**, 17 (2005)
- 793 [17] M. Ave for the Pierre Auger Collaboration, "Reconstruction accuracy of the  
794 surface detector array of the Pierre Auger Observatory", Proceedings of the 30th  
795 International Cosmic Ray Conference, Merida, Mexico (2007), H.E. 1.4.A - 297.
- 796 [18] C. Bonifazi, A. Letessier-Selvon and E. M. Santos, *subm. to Astrop. Phys.*,  
797 astro-ph 0705.1856.

- 798 [19] M. Aglietta et. al. for the Pierre Auger Collaboration, "Response of the Pierre  
799 Auger Observatory Water Cherenkov Detectors to Muons", Proceedings of the  
800 29th International Cosmic Ray Conference, Pune, India, **7**, 83 (2005)
- 801 [20] X. Bertou et. al for the Pierre Auger Collaboration, Nuclear Instruments and  
802 Methods in Physics Research **A568** 839 (2006)
- 803 [21] The Pierre Auger Collaboration, Nucl. Instr.& Meth. A **523** 50-95 (2004)
- 804 [22] A. Filevich et. al, Nucl. Inst. & Meth. **A423**, 69 (1999)
- 805 [23] J. Ogwoka Gichaba, "Measurements of Tyvek Reflective Properties for  
806 the Pierre Auger Project," University of Mississippi Masters Thesis (1998).  
807 <http://lss.fnal.gov/archive/masters/fermilab-masters-1998-05.pdf>
- 808 [24] I. Allekotte et. al. for the Pierre Auger Collaboration, "Observation of the  
809 Long Term Stability of Water Stations in the Pierre Auger Surface Detector",  
810 Proceedings of the 29th International Cosmic Ray Conference, Pune, India, **8**,  
811 287 (2005)
- 812 [25] P. Allison et. al. for the Pierre Auger Collaboration, "Observing muon decays  
813 in water Cherenkov detectors at the Pierre Auger Observatory", Proceedings of  
814 the 29th International Cosmic Ray Conference, Pune, India, **8**, 299 (2005)