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### Theoretical atomic structure and electron scattering data for ions in the nitrogen isoelectronic sequence: Mg VI, Si VIII, S x, A XII and Ca XIV

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 $2s^2 2p^3$ ,  $2s 2p^4$  of Mg VI, Si VIII, Sx, AXII and CaXIV. The electron scattering problem was solved using the 'distorted wave' approximation. The statistical equilibrium equations for level populations were solved including all relevant excitation and de-excitation mechanisms. The level populations spectral lines are tabulated for conditions appropriate to the solar atmosphere. configurations ground configuration and theoretical intensity ratios for the strengths oscillator been computed for the Summary. Intermediate coupling energy levels, strengths have collision electron

### 1 Introduction

sequences (Mg VII, Si IX and S XI - Mason & Bhatia 1978; A XIII, Ca XV, A XIV, et al. 1979). In this paper we report calculations for several ions in the package developed at University College, London. In Section 2 we tabulate the atomic data for MgVI, Si VIII, S x, A XII, Ca XIV and compare our results with publications by other nitrogen iso-electronic sequence. All these atomic data have been obtained using a computer In previous papers we have tabulated new atomic data for ions in the boron and carbon iso-Ca xvi – Dere electronic authors.

separate paper (Feldman et al. 1978). Using available EUV observations from the quiet Sun These calculations are useful in the analysis of solar spectra. We have discussed the theoretical and observed intensity ratios for transitions in the ground configuration in a and active regions, we found that the ion S x is most useful for electron density diagnostics.

Transitions between configurations  $2s^2 2p^3$  and  $2s 2p^4$  give rise to lines in the wavelength region 100-500 Å. Identifications of these lines has been made in laboratory spectra and solar spectra. We discuss the theoretical intensity ratios and line identifications in Section 3.

### 2 Atomic data

The configurations included in the solution of the atomic structure and electron scattering codes were  $2s^2 2p^3$ ,  $2s 2p^4$  and  $2p^5$ . Atomic data for all transitions between terms in these configurations was computed but we tabulate only the radiative and electron collisional

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data within the  $2s^2 2p^3$  configuration and between the  $2s^2 2p^3$  and  $2s 2p^4$  configurations. The data connected with  $2p^5$  and within  $2s 2p^4$  is available on request. The configuration interaction effects between  $2s^2 2p^3$  and  $2p^5$  are fully allowed for.

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## 2.1 ATOMIC STRUCTURE

coupling, allowing for spin-orbit and other relativistic effects. The Slater state expansion method was used and interaction between configurations was allowed for. The radial wavefunctions for the one electron orbitals were obtained using a Thomas-Fermi statistical model potential. The scaling parameters  $(\lambda_l)$  for the potential were determined by minimizing the sum of the energies of the terms in  $2s^2 2p^3$  and  $2s 2p^4$ . The computer The energy levels (Table 1) and radiative data (Tables 2(a)—(e)) were computed in intercode is called SSTRUCT. The theoretical methods used are discussed in Eissner, Jones & Nussbaumer (1974). Tables 1-4 are on Microfiche MN 190/2.

Kastner (1967), Froese (1967), Nicolaides & Beck (1973). Kastner and Froese used the optimized wavefunctions. His transition probabilities are about 15 per cent different from between  $2s^2 2p^3$  and  $2p^5$ . Froese (1967) lists multiplet oscillator strengths for only three transitions of Si vIII. Her values for  $2s^2 2p^3 ^2D - 2s 2p^4 ^2D$  (1.28) and  $2s^2 2p^3 ^2D - 2s 2p^4 ^2D$ between our results and his is better than 25 per cent for all large oscillator strengths intensity ratios but emphasize that more accurate results could be obtained using the atomic dipole operator, which are usually neglected, and could be important for higher members of Previous atomic structure calculations for the ions considered have been carried out by Hartree-Fock program of Froese (1963). They did not allow for configuration interaction  $2s 2p^{44}P$  (1.32) is very different from ours (0.86). To facilitate comparison with Kastner, we ran SSTRUCT including only the configurations  $2s^2 2p^3$  and  $2s 2p^4$ . The agreement (>0.1), including the transitions  $2s^2 2p^3 4S_{3/2} - 2s 2p^4 4p_J$ . Our wavelengths are substantially closer to the experimental values than are Kastner's. Nicolaides & Beck have also calculated oscillator strengths for Si viii. They use wavefunctions containing all the important non-Fock results are in excellent agreement with our structure results, including only two configurations. Their high accuracy calculations agree to within 25 per cent with our three configuration calculations. Their wavelengths are in better agreement with the experimental values than ours. We consider our results to be adequate for calculating the theoretical structure code by including a more elaborate set of correlation configurations. Forbidden transition probabilities are very sensitive to errors in energy separations. Zeippen (1977) configuration of OII. Using a modified form of SSTRUCT, he carried out sophisticated calculations involving configuration interaction, semi-empirical term energy corrections and previous calculations. He also considered the effect of higher order terms in the magnetic the nitrogen isoelectronic sequence. Kastner, Bhatia & Cohen (1977) published results for the ground configuration (and  $2s^2 2p^2 3s$ ,  $2s^2 2p^2 3d$ ) of Mg VI, Si VIII and S x. They used the same computer program as ourselves but for expediency they used a scaling parameter of value one for the Thomas-Fermi potential. We optimized the scaling parameter as indicated (1.63) agree well with ours (1.27 and 1.65 respectively) but her value for  $2s^2 2p^{34}S$ . dynamical correlation effects in the non-closed shell many electron theory. Their Hartreecomputed the transition probabilities  $A(^2D_{5/2} - ^4S_{3/2})$  and  $A(^2D_{3/2} - ^4S_{3/2})$  in the above, consequently our results are more accurate.

# 2.2 ELECTRON SCATTERING

based on the 'distorted wave' The electron scattering program uses the same target wavefunctions as the atomic structure code, including configurations  $2s^2 2p^3$ ,  $2s 2p^4$  and  $2p^5$ . For low partial wave values of the incoming electron  $(l \le 7)$  we used the program COLLDW

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atoms is even better. Davis et al. used a 'distorted wave' approximation to compute electron excitation rates in L-S coupling. They tabulate results for a couple of transitions in Mg vi approximation (theoretical methods discussed in Eissner & Seaton 1972). The R matrices, computed in the L-S coupling scheme, are transformed into pair coupling using algebraic re-coupling coefficients which allow for spin-orbit interaction and other relativistic effects momentum values (l > 7) a 'Bethe' approximation code, developed by Burgess & Shoerey (1975, private communication) was used. Convergence between the 'distorted wave' and 'Bethe' results was checked by plotting the collision strengths in L-S coupling as a function of partial wave value. The final collision strengths  $(\Omega_{ij})$  are given in Tables 2(a)—(e) for three values of the energy of the incident electron appropriate to each ion. Previous calculations of electron-scattering from these ions have been published by Blaha (1969) and Davis, (1976). Blaha only tabulated results for the transition between  $2s^2 2p^3(^2P_{1/2}-^2P_{3/2})$ . He used a weak coupling approximation, with exchange and quotes an accuracy of a factor 2 for low z and up to 50 per cent for highly ionized atoms. His results and ours agree to 25 per cent for Mg vI and agreement for the more highly ionized in the target system. The program used is called JJOM (Saraph 1972). For large and Si vIII and agreement with our L-S coupled results is better than 5 per cent. & Blaha Kepple

# 3 Level populations and line intensities

1975), electron excitation and de-excitation and radiative transitions. For these ions, proton excitations were found to be negligible in comparison to electron excitations (see Feldman The statistical equilibrium equations were solved including all relevant processes (see Mason et al. 1978). The level populations

$$N_i/N$$
,  $N=\sum_{i=1}^5 N_i$ 

in the ground configuration. The wavelength and intensity ratios of transitions within the observed EUV wavelengths for Mg vI correspond to a different energy ordering than that listed in Table 1. In particular, the positions of the  $2s^2$  2p  $^3$   $^2$  $D_{5/2}$  and  $^2$  $D_{3/2}$  are observed to be (1975, private communication), A xII  $-2.5 \times 10^6 \, \mathrm{K}$ , Ca xIV  $-3 \times 10^6 \, \mathrm{K}$ ). The dilution factor [D(h)] for the radiation field is taken as 0.5. For low electron densities the population of the ion is primarily in the ground level, but as the electron density increases, the excited levels become populated and eventually Boltzmann equilibrium is reached between all the levels ground configuration were discussed in Feldman et al. (1978) so we will discuss only the transitions between levels in configurations  $2s^2 2p^3 - 2s 2p^4$ . We note, however, that the 55 350 and 55 370 cm<sup>-1</sup> respectively, above the  $2s^2 2p^3 4S_{3/2}$  level. These levels are very close together in both the experimental and theoretical results. The splitting of the  $2s^2$   $\stackrel{?}{ extstyle 2}p^3$   $^3$   $^3$ levels for Si viii and more highly ionized ions has a consistent energy ordering for the for the ground configuration are given in Table 3 for each ion as a function of electron density. These values correspond to the temperature of maximum abundance  $(T_{max})$  for each ion (Jordan (1969),  $MgvI - 5 \times 10^5 K$ ,  $SivIII - 8 \times 10^5 K$ ,  $Sx - 1.3 \times 10^6 K$ ; Storey observed and theoretical values.

intensity for this transition is relatively weak. Assuming Kelly & Palumbo's identification the Mg vI transition  $2s^2 2p^3 ^2 D_{3/2} - 2s 2p^4 ^2 D_{3/2}$  has a strong intensity. A line is listed (by Kelly & Palumbo) at 387.787 Å as transition  $2s^2 2p^3 ^2 P_{1/2} - 2s 2p^4 ^2 D_{3/2}$ , but the theoretical Si viii, (1973). We comment below on uncertain or new wavelengths. From Table 4 we see that to be correct, the predicted wavelength for the transition  $2s^2 2p^3 2D_{3/2} - 2s 2p^4 2D_{3/2}$  is Sx, AxII, CaxIv are given in Table 4. The wavelengths are taken from Kelly & Palumbo Theoretical intensity ratios for the strongest UV lines from the ions Mg VI,

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349.14 Å. For Si viii, Table 4, Kelly & Palumbo iist a product a wavelength of 277.11 Å the transition  $2s^2 2p^{32} p_{3/2} - 2s 2p^{42} p_{5/2}$ . From this we predict a wavelength of 277.11 Å the transition  $2s^2 2p^{32} p_{3/2} - 2s 2p^{42} p_{5/2}$ . From this we predict a wavelength of 277.11 Å -2s  $2p^4 {}^2D_{5/2}$ . For A XII and Ca XIV, Table 4, only Palumbo do not list the wavelengths for transitions  $2s^2 2p^3 2D_{3/2} - 2s 2p^4 2D_{3/2}$  or  $2s^2 2p^3 2D_{5/2} - 2s 2p^4 2D_{5/2}$ . Using other wavelengths listed by Kelly & Palumbo and the EUV wavelengths listed in Feldman et al. (1978), we predict these lines to lie at 192.44 and 193.91 Å respectively. the six strongest transitions are listed. For A XII, Kelly & for the strong transition at  $2s^2 2p^{32}D_{5/2}$ 

listed is at 403.299 Å but it is blended with a Ne vI line. For Si vIII, lines are listed at 319.830 Å (22, wide line), 316.216 Å (10), 314.350 Å (6), 276.850 Å (8), 216.90 Å (5, blended) and 214.76 Å (-). The numbers in parentheses indicate the intensities as listed by intensity of the 276.85 Å line relative to the 314.35 Å line indicates an electron density just above  $10^{10}$  cm<sup>-3</sup>. For S x, Behring *et al.* list lines at 264.233 Å (20, blended), 259.494 Å (17), isoelectronic sequence are relatively weak (compared to lines from iron ions), however, it reliably measured, the presence of the lines at 228.16 and 228.70 Å is indicative of a high electron density. The instrument sensitivity falls very rapidly below 200 Å and we therefore Some of these lines are listed in Behring et al. (1976). This was a full Sun rocket spectrum lines which are intense for electron densities less than  $10^{10} \mathrm{cm}^{-3}$ . For Mg vI, the only line Behring et al. We see that they are reasonably consistent with our theoretical values. The 257.136 Å (5), 228.167 Å (11) and 177.593 Å (-, wide line). Again the intensities are relative to the rest indicates an electron density just above  $10^{10}\,\mathrm{cm}^{-3}$ . No A XIII lines are Malinovsky & Heroux (1973) also obtained a full Sun rocket spectrum (150-300 Å, spectral resolution of 0.25 Å). They observed only a few Si vIII lines at 216.9, 214.75, 235.55 Å and Sx lines at 264.27 and 259.50 Å. A compilation of lines from solar flare spectra in the wavelength region 171-630 Å has recently been published by Dere (1978). These data were The wavelength resolution was limited by the spatial extent of the emitting region, the highest resolution being about 0.1 Å. Several of the UV lines from ions in the nitrogen isoelectronic sequence were recorded. Mg vI lines were identified at 403.32 Å (blended with Ne vI), 400.68, 399.27, 349.13, 270.34 and 269.00 Å. Most of these lines in the nitrogen relative to 400.68 Å was measured as 4.3. This is twice as high as that predicted for the high of 277.10 relative to 316.20 Å was measured as 1.4 for the August 9 flare (Dere et al. 1978). This indicates an electron density of  $3 \times 10^{10} \, \mathrm{cm}^{-3}$ . The S x lines identified by Dere lie at 264.24, 259.49, 228.16 and 228.70 Å. Although the intensities for these lines cannot be do not expect to see the Ca xIV lines. If one could measure the intensity of these lines, they could be very useful for determining the electron density in solar flare conditions, where the electron density can reach values in excess of  $10^{11}\,\mathrm{cm}^{-3}$ . (160-770 Å) with a spectral resolution of 0.06 Å. With this data we expect only to observe reasonably consistent with the theoretical values and the intensity of the line 228.167 Å identified by Behring et al., but two Ca XIV lines are listed, 193.872 Å (-) and 185.605 Å (5). obtained using the Naval Research Laboratory's (NRL) spectroheliograph aboard Skylab. 1973 August 9, in the data from the NRL spectroheliograph. Details of these intensity are given in Dere et al. (1979). The Mg vi intensity ratio for line 349.16 density limit which would indicate that there is some unaccounted for blend. Several Si vIII lines are listed in Dere (1978), they are 319.84, 316.19, 314.31, 276.85, 277.04 Å (blended with Mg VII), 216.88 Å (blended with Fe xIII) and 214.77 Å. The intensity ratio for Si VIII has been possible to measure the intensity of a few of the lines for a compact intense flare measurements

### 4 Conclusion

Our atomic structure results are in good agreement with previous publications. The amount of electron scattering data available in the literature for these systems is very sparse. In

theoretical intensity ratios for the EUV (see Feldman et al. 1978) and UV lines for conditions appropriate to the solar corona. We have commented on the available line identifications both in aboratory and solar spectra. Although these lines are relatively weak in the solar spectrum, some of them are potentially very useful for electron density diagnostics in different solar this paper we have tabulated a comprehensive set of electron collision strengths for several compute data to these nsed We sednence. in the nitrogen isoelectronic ions

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coronal holes, quiet Sun, active regions and solar flares.

phenomena

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electron scattering sedneuce: VIX g isoelectronic and and atomic structure the (/2 7 ions 77 02 for Theoretical <u>ದೆಭಿಕೆ</u>

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Configurations		$2s^22p^3$					2s2p							
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Table 1

Transition	3.4 m .4	A.j.		S.	
			10 Ryd	15 Ryd	20 Ryd
- 2		1.45-11	0.1897	0.1300	0.0936
m		 	0.2188	0.1526	0.1118
47		4.92+0	0.0582	0.0371	0.0249
<b>ኒ</b> ግ		1.20+1	0.101.0	0.0649	0.0439
9	0.520	3.52+9	3.0794	3,3999	3.6508
	0.349	3.5849	2.0408	2.2538	2.4217
<b>∞</b>	0.175	3.62+9	1.0594	1.1556	1.2336
6		2.12+4	0.0016	0.0008	0.0005
10		2.91+3	0.0020	0.0010	9000°0
्रक्तावर्ष श्रीवरवर्ष		3.14+6	0.0003	0.0002	0.0002
1.2		5.62+6	0.0538	0.0394	0.0297
13		1.66+6	0.0338	0.0236	0.0173
2 - 3			0.2777	0.1944	0.1432
<b>†</b> 7		1.85+0	0.1531	0.1520	0.1521
٧.		2.9940	0.1933	0.1765	0.1674
9		6.53+4	0.0136	0.0102	0.0077
		4.29+4	0.0476	0.0337	0.0248
<b>∞</b>		3.95+4	0.0338	0.0238	0.0175
6	0.578	8.31+9	2.6621	2.9365	3,1630
2	0.045	4.28+8	0.2477	0.2711	0.2783
ganağ ganağ	0.007	3.09+8	0.0267	0.0304	0.0327
1.2	0.167	4.1349	0.4937	0.5551	0.6042
<u>~~</u>	0.630	3.14+10	1.8377	2.0711	2.2644

4         10 Rgd         15 Rgd         20 Rgd           4         1,67-2         0.1423         0.1278         0.1197           5         1,69+0         0.3746         0.1278         0.1197           6         1,69+0         0.3746         0.3640         0.3588           6         1,89+4         0.0314         0.0661         0.0464           8         1,83+4         0.0314         0.0233         0.0146           9         0.056         8.30+9         0.0350         0.0146         0.0463           10         0.866         8.30+9         0.03107         0.0334         0.0463           11         0.866         8.30+9         0.03107         0.0314         0.0463           12         1.224         3.02440         4.0903         0.0416           13         1.1645         0.0213         0.0416         0.0119           14         1.1645         0.0214         0.0103         0.0119           15         1.1645         0.0213         0.0167         0.0119           16         0.031         0.0210         0.0210         0.0119           17         1.6749         0.2623         0.0210         0.	Transition	$\omega_{i}$ fjj	424 44.2		ä	
6         7.67-2         0.1423         0.1278           8         1.69+0         0.3746         0.3640           9         3.47+5         0.0801         0.0601           9         0.056         8.00+8         0.0114         0.0233           9         0.056         8.00+8         0.01107         0.0334           1         1.83+4         0.01107         0.0034           0         0.056         8.00+8         0.0034         0.0034           1         0.056         8.00+8         0.01107         0.0034           2         1.224         3.02+10         3.8703         4.3040           3         1.224         3.02+10         0.0113         0.0016           4         4.36-6         0.0113         0.0016         0.0017           5         4.36-6         0.0203         0.0026           6         1.16+5         0.0204         0.0017           9         0.031         0.164         0.0401           1         0.149         0.0201         0.0201           1         0.149         0.0201         0.0201           1         0.149         0.0202         0.0203				10 Ryd	15 Ryd	20 Ryd
6         1.6940         0.3466         0.3640           6         3.47+5         0.0801         0.0601           7         1.8344         0.0314         0.0233           8         0.056         8.00+8         0.0314         0.0233           9         0.056         8.00+8         0.0107         0.0334           1         0.2866         8.30+9         3.8103         4.3640           2         1.224         3.02+10         0.0113         0.0015           3         1.224         3.02+10         3.6444         4.0903           4         4.36-6         0.0113         0.0015         0.0015           5         4.36-6         0.1224         4.0903         0.0026           6         4.36-6         0.1224         4.0903         0.0026           7         4.36-6         0.0204         0.0047         0.0204         0.0047           9         0.039         1.10+9         0.5103         0.0206         0.0316           1         0.134         5.89+9         0.4451         0.4451         0.4987           1         0.134         1.3444         0.0172         0.0149           2 <th< td=""><td>7</td><td></td><td>7.67-2</td><td>0.1423</td><td>0.1278</td><td>0.1197</td></th<>	7		7.67-2	0.1423	0.1278	0.1197
6         3.47+5         0.08011         0.0601           7         1.83+4         0.0314         0.0233           8         0.056         8.00+8         0.0050         0.0034           9         0.056         8.30+9         3.8703         4.3040           1         0.866         8.30+9         3.8703         4.3040           2         0.266         8.30+9         3.8703         4.3040           3         0.240         3.6444         4.0003           4         4.36-6         0.0113         0.0016           9         0.091         1.10+9         0.0129         0.0077           9         0.099         1.10+9         0.2024         0.0203           10         0.199         7.10+9         0.2024         0.0477           11         0.194         0.10+9         0.2625         0.2937           12         0.134         5.89+9         0.4451         0.4587           13         1.57+3         0.02530         0.0269           14         0.134+         0.134+         0.0451         0.0269           15         1.24+9         0.0452         0.0269         0.0269           1	S		1.69+0	0.3746	0.3640	0.3588
8         1.8344         0.0314         0.0223           8         0.056         0.0050         0.0034           9         0.056         8.00+8         0.3107         0.0334           1         0.0866         8.30+9         3.8703         4.3040           2         0.0866         8.30+9         3.8703         4.3040           2         1.224         3.02+10         0.0113         0.0016           3         1.224         3.02+10         3.6444         4.0903           4         4.36-6         0.0113         0.0016           5         1.57+3         0.0213         0.0077           9         1.16+5         0.0204         0.0203           9         1.16+5         0.0204         0.0204           10         0.199         1.10+9         0.5010         0.0201           11         0.199         1.10+9         0.5010         0.0201           12         0.031         0.0204         0.0201         0.0201           13         0.134         5.89+9         0.4451         0.0459           14         0.134         1.34+4         0.0607         0.0649           15         1.24+	S		3.4745	0.0801	0.0601	0.0463
8         0.0050         0.0034           9         0.056         8.00+8         0.3107         0.3330           1         0.0866         8.30+9         3.8703         4.3040           2         0.0866         8.30+9         3.8703         4.3040           3         1.224         3.02+10         3.6444         4.0903           4         1.224         3.02+10         0.0113         0.0016           5         4.36-6         0.1524         4.0903           6         1.57+3         0.0129         0.0077           9         0.091         1.10+9         0.2020         0.0092           1         0.134         1.67+9         0.2103         0.0203           1         0.134         1.67+9         0.2625         0.2937           2         0.077         1.67+9         0.2625         0.2937           3         0.134         5.89+9         0.4451         0.4987           4         0.077         1.34+4         0.0172         0.0166           8         0.147         0.0607         0.0649           9         0.330         1.27+10         0.4451         0.4464           1	~		1.83+4	0.0314	0.0223	0.0166
9         0.0566         8.00+8         0.3107         0.3330           1         0.0866         8.30+9         3.8703         4.3040           1         0.0866         8.30+9         3.8703         4.3040           2         1.224         3.02+10         3.6444         4.0903           3         1.224         3.02+10         0.0013         0.0016           4         4.36-6         0.1524         4.0903           5         1.57+3         0.0129         0.0077           9         0.091         1.10+9         0.0204         0.0147           9         0.097         1.10+9         0.2023         0.0205           1         0.199         7.10+9         0.2625         0.2937           2         0.077         1.67+9         0.2625         0.2937           3         0.134         5.89+9         0.4451         0.4987           4         3.57+5         0.0330         0.0269           9         0.134+         0.0451         0.0669           9         0.182         1.47+9         0.0669         0.0669           1         0.350         1.25+10         0.0669         0.01669	හ			0.0050	0.0034	0.0024
0.866       8.30+9       3.8703       4.3040         1.224       3.02+10       3.6444       4.0903         1.224       3.02+10       3.6444       4.0903         1.224       3.02+10       0.0113       0.0015         1.24       3.24-6       0.1524       0.1053         1.57+3       0.0293       0.0092         1.16+5       0.0204       0.0147         0.091       1.10+9       0.5103       0.0205         0.077       1.67+9       0.2603       0.0210         0.077       1.67+9       0.2625       0.2937         0.134       5.89+9       0.4451       0.4987         0.134       5.89+9       0.4451       0.4987         1.34+4       0.0373       0.0269         0.182       1.47+9       0.0449       0.0649         0.330       1.25+10       0.0449       0.0649         0.331       7.17+9       0.4404       0.4404       0.4992	S	0.056	8.00+8	0.3107	0.3330	0.3423
1.224       3.02+10       3.6444       4.0903         2       1.224       3.02+10       3.6444       4.0903         3       6.01       0.0113       0.0007         4       4.36-6       0.1524       0.1053         6       1.57+3       0.0129       0.0002         7       1.57+3       0.0203       0.0002         8       0.091       1.10+9       0.0204       0.0147         9       0.077       1.67+9       0.2625       0.2937         10       0.199       7.10+9       0.2625       0.2937         11       0.134       5.89+9       0.4451       0.4987         12       1.67+9       0.2625       0.2937         13       1.34+4       0.0333       0.0269         1       1.34+4       0.0172       0.0116         1       0.350       1.47+9       0.9951       1.0628         1       0.350       1.25+10       1.4759       1.5569         1       0.331       7.17+9       0.4406       0.4406       0.4492	0	0.866	8.3049	3.8703	4.3040	4.6553
2       1.224       3.02+10       3.6444       4.0903         3       0.0113       0.0077         4       0.0113       0.0077         5       4.36-6       0.1524       0.1053         6       0.05       0.0129       0.0092         7       1.57+3       0.0204       0.0205         8       0.091       1.10+9       0.0204       0.0147         9       0.097       1.67+9       0.2625       0.2937         10       0.199       7.10+9       0.2625       0.2937         12       0.077       1.67+9       0.2625       0.2937         13       0.134       5.89+9       0.4451       0.4987         13       0.134       5.89+9       0.4451       0.4987         13       0.134+       0.0339       0.0269         1       1.34+4       0.0172       0.0166         1       0.350       1.47+9       0.9531       1.0628         1       0.350       1.25+10       1.4250       1.5569         2       0.331       7.17+9       0.4404       0.4404       0.4492	poor)			0.0019	0.0016	0.0013
3       4.36-6       0.01524       0.0053         6       0.157+3       0.0129       0.0092         7       1.57+3       0.0293       0.0092         8       1.16+5       0.0204       0.0147         9       0.091       1.10+9       0.5103       0.5467         10       0.199       7.10+9       0.5103       0.5467         1.       0.077       1.67+9       0.2625       0.2937         2.       0.077       1.67+9       0.2625       0.2937         3       0.134       5.89+9       0.4451       0.4987         4       0.0134       5.89+9       0.6451       0.4987         5       0.134+       0.0530       0.0396         8       0.1+7       0.0673       0.0166         9       1.34+4       0.0172       0.0116         9       0.354+5       0.0530       0.0649         10       0.350       1.25+10       1.47+9       0.9951       1.0628         1       0.350       1.25+10       1.0745       1.2147         2       0.331       7.17+9       0.4404       0.4992	2	1.224	3.02+10	3.6444	4.0903	8075.7
5       4.36-6       0.1524       0.1053         6       0.0129       0.0092         7       1.57+3       0.0293       0.0205         8       1.16+5       0.0204       0.0147         9       0.091       1.10+9       0.5103       0.5467         10       0.199       7.10+9       0.0201       0.0210         12       0.077       1.67+9       0.2625       0.2937         13       0.134       5.89+9       0.4451       0.4987         14       0.037       0.0530       0.0396         15       3.57+5       0.0373       0.0269         16       3.57+5       0.0373       0.0649         10       0.182       1.47+9       0.9607       0.0649         10       0.350       1.25+10       1.4250       1.5569         11       0.350       1.25+10       1.4250       1.5569         12       0.331       7.17+9       0.4404       0.4992	ci.			0.0113	0.0077	0.0057
6       0.0129       0.0092         7       1.57+3       0.0293       0.0205         8       1.16+5       0.0204       0.0147         9       0.091       1.10+9       0.5103       0.5467         10       0.199       7.10+9       0.0201       0.0210         12       0.077       1.67+9       0.2625       0.2937         13       0.134       5.89+9       0.4451       0.4987         14       2.26+5       0.0530       0.0396         15       1.34+4       0.0172       0.0169         10       0.182       1.47+9       0.0607       0.0649         10       0.350       1.25+10       1.4250       1.5569         10       0.350       1.25+10       1.0745       0.4992	n		4.36-6	0.1524	0.1053	0.0765
7       1.57+3       0.0293       0.0205         8       1.16+5       0.0204       0.0147         9       0.091       1.10+9       0.5103       0.5467         10       0.199       7.10+9       0.5103       0.5467         11       0.199       7.10+9       0.8016       0.8891         12       0.077       1.67+9       0.2625       0.2937         13       0.134       5.89+9       0.4451       0.4987         14       0.134       0.0530       0.0396         15       1.34+4       0.0172       0.01669         10       0.182       1.47+9       0.0607       0.0649         11       0.350       1.25+10       1.4250       1.5569         11       0.350       1.25+10       1.0745       1.2569         12       0.0331       7.17+9       0.4404       0.4992	9			0.0129	0.0092	0.0069
8       1.16+5       0.0204       0.0147         9       0.091       1.10+9       0.5103       0.5467         10       0.199       7.10+9       0.0201       0.0210         1       0.199       7.10+9       0.8016       0.8891         2       0.077       1.67+9       0.2625       0.2937         3       0.134       5.89+9       0.4451       0.4987         4       2.26+5       0.0530       0.0396         7       3.57+5       0.0333       0.0649         8       1.34+4       0.0607       0.0649         9       8.01+7       0.0607       0.0649         9       1.47+9       0.9551       1.0628         1       0.350       1.25+10       1.4250       1.5569         1       0.335       1.17+9       1.0745       1.2147         2       0.331       7.17+9       1.6746       0.4992	_		1.57+3	0.0293	0.0205	0.0
0.091       1.10+9       0.5103       0.5467         0.199       7.10+9       0.8016       0.8891         0.077       1.67+9       0.2625       0.2937         0.134       5.89+9       0.4451       0.4987         2.26+5       0.0530       0.0396         3.57+5       0.0373       0.0269         1.34+4       0.0172       0.0166         0.182       1.47+9       0.9067       0.0649         0.350       1.25+10       1.4250       1.5569         0.331       7.17+9       1.0745       1.2147         0.135       5.91+9       0.4404       0.4992	œ		1.16+5	0.0204	0.0147	0.0109
0.199       7.10+9       0.8016       0.8891         0.077       1.67+9       0.2625       0.2937         0.134       5.89+9       0.4451       0.4987         2.26+5       0.0530       0.0396         3.57+5       0.0373       0.0269         1.34+4       0.0172       0.0166         8.01+7       0.0607       0.0649         0.350       1.25+10       1.4250       1.5569         0.331       7.17+9       1.0745       1.2147         0.135       5.91+9       0.4404       0.4992	ο,	0.091	1.10+9	0.5103	0.5467	6.5818
0.199       7.10+9       0.8016       0.8891         0.077       1.67+9       0.2625       0.2937         0.134       5.89+9       0.4451       0.4987         2.26+5       0.0530       0.0396         3.57+5       0.0373       0.0269         1.34+4       0.0172       0.01669         0.182       1.47+9       0.0607       0.0649         0.350       1.25+10       1.4250       1.5569         0.331       7.17+9       1.0745       1.2147         0.135       5.91+9       0.4404       0.4992	0			0.0201	0.0210	0.0160
0.077       1.67+9       0.2625       0.2937         0.134       5.89+9       0.4451       0.4987         2.26+5       0.0530       0.0396         3.57+5       0.0373       0.0269         1.34+4       0.0172       0.0116         8.01+7       0.0607       0.0649         0.182       1.47+9       0.9751       1.0628         0.350       1.25+10       1.4250       1.5569         0.331       7.17+9       1.0745       1.2147         0.135       5.91+9       0.4404       0.4992	-4	0.199	7.10+9	0.8016	0.8891	0.9539
0.134       5.89+9       0.4451       0.4987         2.26+5       0.0530       0.0396         3.57+5       0.0373       0.0269         1.34+4       0.0172       0.0116         8.01+7       0.0607       0.0649         0.182       1.47+9       0.9751       1.0628         0.350       1.25+10       1.4250       1.5569         0.331       7.17+9       1.0745       1.2147         0.135       5.91+9       0.4404       0.4992	2	0.077	1.67+9	0.2625	0.2937	0.3167
6       2.26+5       0.0530       0.0396         7       3.57+5       0.0373       0.0269         8       1.34+4       0.0172       0.0116         9       8.01+7       0.0607       0.0649         0       0.182       1.47+9       0.9751       1.0628         1       0.350       1.25+10       1.4250       1.5569         2       0.331       7.17+9       1.0745       1.2147         3       0.135       5.91+9       0.4404       0.4992	eg.	0.134	5.89+9	24.0	1867.0	0.5415
3.57+5       0.0373       0.0269         1.34+4       0.0172       0.0116         8.01+7       0.0607       0.0649         0.182       1.47+9       0.9751       1.0628         0.350       1.25+10       1.4250       1.5569         0.331       7.17+9       1.0745       1.2147         0.135       5.91+9       0.4404       0.4992	9		2.26+5	0.0530	0.0396	0.0304
1.34+4       0.0172       0.0116         8.01+7       0.0607       0.0649         0.182       1.47+9       0.9751       1.0628         0.350       1.25+10       1.4250       1.5569         0.331       7.17+9       1.0745       1.2147         0.135       5.91+9       0.4404       0.4992	-		3.57+5	0.033	0.0269	1020.0
8.01+7 0.0667 0.0649 0.182 1.47+9 0.9751 1.0628 0.350 1.25+10 1.4250 1.5569 0.331 7.17+9 1.0745 1.2147 0.135 5.91+9 0.4404 0.4992	∞		7+76	0.0172	0.0116	0.0085
0.182       1.47+9       0.9751       1.0628         0.350       1.25+10       1.4250       1.5569         0.331       7.17+9       1.0745       1.2147         0.135       5.91+9       0.4404       0.4992	0		8.01+7	0.0607	6,0649	0.0614
0.350     1.25+10     1.4250     1.5569       0.331     7.17+9     1.0745     1.2147       0.135     5.91+9     0.4404     0.4992	0	0.182	1.47+9	0.9751	1.0628	000 000 000 000 000 000
0.331 7.17+9 1.0745 1.2147 0.135 5.91+9 0.4404 0.4992	person di	0.350	2.25+10	1.4250	1.5569	1.6667
0.135 5.91+9 0.4404 0.4992	~	ë o	7.17+5	37.0.7	7777	
	ed.	S	5.9149	0.440%	7667.0	70.0

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Transition	3 **** **** ****	epronj epronj	10 Ryd	$\Omega_{i,j}$ 15 Ryd	20 Ryd
		1.96+0	0.1505	0.1142	0.0890
		3.75-2	0.1759	5	0.1066
		2.99+1	0.0483	0.0347	0.0258
		7.12+1	0.0845	0.0612	0.0456
	0.436	4.70+9	2.0657	2.2444	2.3893
	0.294	4.85+9	1.3647	1.4829	1.5795
	0.148	6+56.7	0.710	0.7628	0.8070
		1.77+5	0.0011	0.0007	0.0005
		2.73+4	0.0013	0.0008	0.0005
		1.12+7	9000.0	0.0005	0.0005
		2.22+7	0.0403	0.0325	0.0265
		6.1846	0.0247	0.0192	0.0152
		3.54-4	0.2191	0.1691	0.1343
		thereof to the total total	0.1044	0.1023	0.1016
		1.90-1	0.1331	0.1214	0.1142
		3.9945	0.0131	0.0105	0.0086
		5+10.	0.0351	0.0273	0.0217
		2.16+5	0.0242	0.0187	0.0149
	0.493	O mid the part of	2000	7.001	2.1324
	0.029	4.30+8	· 155	0.1515	0.1526
	0.019		0.0549	0.0596	0.0634
	5	5,84+9	.3833	0.4224	0.4537
	787.0	3.72+10	2888	1.3085	1.4053

ransition	3 *** ***	۸ نیز نیز	10 Ryd	Ω <sub>i,j</sub> 15 Ryd	20 Ryd
3 - 4		-61	0.1017	0.0921	0.0860
S		1.05+1	0.2573	0.2482	0.2432
Ø		9+67°T	0.0596	0.0489	0.0405
7		8.65+4	0.0235	0.0185	0.0149
œ			0.0037	0.0028	0.0022
σ	0.042	9.55+8	0.2085	0.2118	0.2155
0	0.722	1.09+10	2.6137	2.8609	3.0615
paral paral			0.0010	0.0008	0.0007
12	6.0.1	3.82+10	2.5565	2.7948	2.9905
<u>م</u>			0.0079	0.0061	0.0048
4 - 5		1.29-3	0.1196	0.0915	0.0720
9			0.0000	0.0072	0.0058
•		7.05+3	0.0217	0.0168	0.0133
<b>∞</b>		5.15+5	0.0	0.0125	0000
0	0.076	1.43+9	0.3438	0.3688	3888 3888 0
10			0.0207	0.0167	0.0136
èreo é	0.175	9.72+9	0.5864	0.6352	0.6737
12	0.067	2.19+9	0.1935	0.2119	0.2248
<b>~</b>	0.102	6.86+9	0.2828	0.3120	97.80
9 .		8.34+5	0.0370	0.0302	0.0249
		1.48+6	0.0298	0.0236	510.0
<b>00</b>		3.4744	0.0139	8070	0.0086
5	0.002	3.50+7	0.0343	0.0298	0.0265
9	0.162	2.03+9	0.6995	0.7582	0.8054
turd hered	0.267	1,48+10	0.9037	0.9711	2970-1
77	0.255	8.38+9	6.7031	1277.0	0.83
(m)	0.157	1,05+10	0.4367	0.4781	0.5114
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30 Ryd	0.0555	0.0685	0.0159	0.0286	1.8339	1.2101	0.6157	0.0003	0.0002	0.0007	0.0174	0.0090	0.0870	0.0724	0.0742	0.0073	0.0129	7800.0	1.6859	0.0818	0.1147	0.4021	0.9743
Stj 20 Ryd	0.0781	0.0947	0.0241	0.0428	1.6837	1.1096	0.5688	0.0005	0.0004	6000.0	0.0230	0.0124	0.1179	0.0733	0.0810	0.0095	0.0178	0.0116	7875.I	0.0825	0.1056	0.3669	48880
15 Ryd	0.0946	0.1137	0.0303	0.0536	1.5942	965.1	0.5417	0.0007	0.0006	0.00.0	0.0268	0.0148	0.1403	0.0745	0.0865	0	0.0212	0.0138	1.4668	0.0833	0.1002	0.3457	0.8390
Aj.	1,7841	777.0	1.35+2	3.06+2	5.9349	6.26+9	6+97.9	1.27+6	1.44+5	3.18+7	7.13+7	1.78+7	2.42-2	Ž	# # 6	1.96+6		9.62+5	07+77-1	3.5948	4	8.02+9	4.07+10
23 and and and and					0.376	0.255	0.129												0.435	0.016	0.038	0.149	0.366
Transition	1 - 2	e	4	5	9	7	∞	6	0	guessé guessé	CZ proof	<u>~</u>	7	4	\$	9	<i>l.</i> ,	œ	6	0	poordi gravej	house)	enné Tago

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Transition	12 12 12 12 12 12 12 12 12 12 12 12 12 1	°≓ ≪	15 Ryd	A <sub>ij</sub> 30 Ryd	45 Ryd
- 2		1.13+2	0.0774	0.0507	0.0355
m		2.49+0	0.0944	0.0631	0.0450
7		4.94+2	0.0260	0.0156	0.0101
5		1.04+3	0.0453	0.0275	0.0180
9	0.331	7.25+9	1.1893	1.3500	1.4689
-	0.227	7.85+9	0.7808	0.8879	0.9679
œ	0.116	8.22+9	0,4040	0.4536	0.4915
5		7.46+6	0.0009	0.0005	0.0004
2		5.56+5	0.0004	0.0002	0.0001
samoné ervandy		7.81+7	0.0018	0.0013	0.0010
CV pusasi	0.002	1.98+8	0.0230	0.0166	0.0125
~		1+11.4	0.0112	0.0076	0.0054
			ć,	90.0	o o
·		75. 5	C. 1149	05/0°0	350°0°0°0°0°0°0°0°0°0°0°0°0°0°0°0°0°0°0°
*		1.01+2	0.0572	0.0545	0.0535
<b>S</b>		3.70+2	0.0630	0.0531	0.0480
9		8.10+6	0.0122	0.0089	0.0068
_		3.07+3	0.0164		0.0079
\$		3.6946	0.0100	0.0068	0.0049
0	0.392	1.80+10	~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~	1.2727	1.3847
9	0.008	2.41+8	0.0444	0.0414	0.03%
Steward	0.062	8	0.1419	0.1604	0.1743
C.J.	0,143	01+90-1	0.2896	0.3306	0.3615
<u>~</u>	0.266	4.11+10	0.5267	0.5987	0.6538
			*		

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ransition	C. Frank C. Call C. Ca	A i.j	15 Ryd	$a_{ m ij}$	45 Ryd
2		5.28+2	0.0643	0.0457	0.0340
ಣ		e brood	0.0785	0.0568	0.0430
7		1.5743	0.0224	0.0148	0.0103
٧		2.91+3	0.0372	0.0250	0.0176
9	0.295	8.65+9	0.9188	1.0289	1.1140
7	0.205	9.72+9	0.6020	0.6753	0.7327
<b>∞</b>	0.106	1.04+10	0.3130	0.3470	0.3743
6		3.67+7	0.0015	0.0011	0.0009
<u> </u>		1.72+6	0.0003	0.0002	0.0001
Street,		1.78+8	0.0026	0.0021	0.0017
C. C	0.004	4.93+8	0.0217	0.0185	0.0162
2		7.95+7	0.0082	0900.0	9700.0
e 1		5.07+0	0.0943	0.0708	0.0561
*/		5.33+2	9570.0	0.0427	0.0414
5		1.35+3	0.0476	0.0396	0.0349
9		2.87+7	0.0143	0.0113	0.0092
يسم		6.71+5	0.0131	9600.0	0.0073
<b>3</b> 0		1.27+7	0.0075	0.0055	0.0042
<b>o</b> ∿	0.361	2.25+10	0.8940	0.9966	1.0780
2	0.003	1.20+8	0.0223	0.0175	0.0141
garanti; garanti;	0.087	0,715	0.1731	0.1915	0.2065
<u>~</u>	**************************************	3.110	0.2359	0.2682	0.2913
(College)	0.186	3.88+10	0.3209	0.3576	0.3871

						D	ownloa	ided fro	om http	s://acaden	nic.oup.	.com/m	nras/a	rticle/1	90/4/9	25/103	7765 b	y gues	t on 20 A	August 2	2022							
45 Ryd	0.0355	0.0962	0.0181	0.0057	0.0008	0.0545	1.4580	0.0002	1.5163	0.0014	0.0280	0.0017	0.0045	0.0047	0.1717	0.0049	0.4088	0.1357	0.0898	0.0076	0.0108	0.0045	0.0129	0.4539	0.2412	0.2913	0.6272	
Lij 30 Ryd	0.0383	0.1004	0.0225	0.0074	0.0010	0.0543	1.3416	0.0003	1.4010	0.0019	0.0357	0.0022	09000	0.0061	0.1604	0.0064	0.3812	0.1302	0.0829	0.0095	0.0136	0.0059	0.0157	0.4204	0.2265	0.2692	0.5802	•
15 Ryd	0.0434	0.1084	0.0285	0.0099	0.0014	0.0551	1.1946	0.0005	1.2597	0.0026	0.0480	0.0029	0.0082	0.0081	0.1461	0.0084	0.3459	0.1142	0.0741	0.0121	0.0177	0.0080	0.0197	0.3773	0.2091	0.2409	0.5212	:
A	2.87-1	5.73+2	3.30+7	2.91+6		8.73+8	1.99+10		6.58+10		1.07+1		2.16+5	1.59+7	2.42+9		2.15+10	4.45+9	6.75+9	9.92+6	3.03+7	3.47+2	2.01+8	4.13+9	1.19410	9.28+9	4.51+10	1
a, f.j						0.014	0.490		0.687						0.048		0.148	0.054	0.038				0.004	0.128	0.085	0.116	0.261	
Transition	3 - 4	Ŋ	9	_	80	Ø	10	prod prod	12	E.	5 - 7	9	5-	∞	o,	10	yand gand	2	<b>~</b>	5 6	7	œ	σ	2 - 5	tracefy from	C	ennel Energy	1

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