

Tsunami waves generated by submarine landslides of variable volume: analytical solutions for a basin of variable depth

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Abstract. Tsunami wave generation by submarine landslides of a variable volume in a basin of variable depth is studied within the shallow-water theory. The problem of landslide induced tsunami wave generation and propagation is studied analytically for two specific convex bottom profiles ($h \sim x^{4/3}$ and $h \sim x^4$). In these cases the basic equations can be reduced to the constant-coefficient wave equation with the forcing determined by the landslide motion. For certain conditions on the landslide characteristics (speed and volume per unit cross-section) the wave field can be described explicitly. It is represented by one forced wave propagating with the speed of the landslide and following its offshore direction, and two free waves propagating in opposite directions with the wave celerity. For the case of a near-resonant motion of the landslide along the power bottom profile $h \sim x^\gamma$ the dynamics of the waves propagating offshore is studied using the asymptotic approach. If the landslide is moving in the fully resonant regime the explicit formula for the amplitude of the wave can be derived. It is demonstrated that generally tsunami wave amplitude varies non-monotonically with distance.

At least, two special workshops specialized on this problem should be mentioned (Keating et al., 2000; Yalciner et al., 2003).

For example, an underwater landslide on 17 July 1998 caused the destructive Papua New Guinea tsunami, when the 15-m wave at the coast devastated three villages and took more than 2200 lives (McSaveney et al., 2000; Synolakis et al., 2002). On 17 August 1999 a shore slump in the Izmit Bay (Turkey) generated a 2.5 m high tsunami (Altinok et al., 2001). The problem of tsunami generation by landslides has also been actively discussed in the Atlantic and Caribbean. In particular, three tsunamis in the Lesser Antilles were generated by avalanche flows from the Montserrat volcano in 1997, 2003 and 2006 (O'Loughlin and Lander, 2003; Pelinovsky et al., 2004; Zahibo, 2006). Deplus et al. (2001) reported large-scale debris avalanche deposits around the Lesser Antilles. Particularly, a large area covered by mega blocks up to 2.8 km long and 260 m high is located off Dominica. Large coastal landslides and associated tsunami hazard in the Caribbean are described in (Teeuw et al., 2009). According to their study possible tsunami waves in the vicinity of Dominica can reach 3–10 m due to probable collapse of coastal blocks. Thus, the problem of tsunami generation by landslides is of current scientific interest.

For description of tsunami wave generation by submarine and aerial landslides various numerical models, which take into account the rheological properties of landslide body and real bathymetry are used (see, for instance, Imamura and Gica, 1996; Heinrich et al., 1999; Assier-Rzadkiewicz et al., 2000; Mangeney et al., 2000; Fine et al., 2003, 2005; Kuo et al., 2008; among others). In all these numerical models the volume of the landslide is conserved. However, Pudasaini and Hutter (2007) in their book pointed out the importance

1 Introduction

The landslide motion is now recognized as an important source of tsunami wave generation, since it is the second most frequent tsunami source after earthquakes responsible for about 10% of all tsunami waves (Gusiakov, 2009).



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of the erosion processes in avalanches, so that the deposited mass in the runout zone can be much larger than the initial mass in the starting zone. This effect of variable volume of the landslide has never been analyzed in the problem of tsunami wave generation and the given study is focused on this problem.

The number of analytical methods for analysis of tsunami wave generation by submarine landslides is limited even for the cases when the landslide is moving with a constant speed and conserves its volume. 1-D wave field around landslide moving with a constant speed in a basin of constant depth is computed in (Pelinovsky, 1996, 2003; Tinti and Bortolucci, 2000; Tinti et al., 2001; Okal and Synolakis, 2003). The 2-D and 3-D motion of a constant-speed landslide is studied analytically for shallow-water approximation in the framework of the potential theory in (Novikova and Ostrovsky, 1978; Pelinovsky and Poplavsky, 1997; Ward, 2001). The landslide tsunami generation along a sloping beach in 1-D and 2-D cases is discussed in (Liu et al., 2003; Sammarco and Renzi, 2008), in the last case the landslide also induces edge waves propagating along a plane beach.

An interesting analytical example of tsunami wave generation in the shallow water basin of variable depth is given in (Tinti et al., 2001). It was shown that in the case of bottom profile $h \sim x^{4/3}$ (h is the water depth and x is coordinate directed offshore) the wave equation with an external force can be simplified and the same methods as for a constant depth basin can be applied. It was found later in (Didenkulova et al., 2009) that this bottom profile can be interpreted as a “non-reflecting” one. Waves propagating along this profile in the opposite directions do not interact between each other and are able to transfer the wave energy over large distances. At the same time there is another quartic bottom profile, $h \sim x^4$, which has the same “non-reflecting” nature (Didenkulova and Pelinovsky, 2010) and the analytical solution of the tsunami wave generation by landslides along this profile is studied below in detail. In fact, the number of “non-reflecting” profiles in 1-D geometry exceeds two, but other bottom configurations lead to the wave dispersion even in the shallow-water approximation (Grimshaw et al., 2010).

At the same time real bathymetries in the coastal zone can be well approximated by these two “non-reflecting” profiles. For example, Fig. 1 demonstrates the applicability of “non-reflecting” approximation to bottom profiles near Guadeloupe, Caribbean Sea (Gusiakov, 2002).

Here we present an analytical study of tsunami wave generation by landslides of a variable volume moving with a variable speed in 1-D case. The mathematical model that is linear shallow-water theory is briefly described in Sect. 2. The process of tsunami wave generation along a special beach profile $h \sim x^{4/3}$ is studied in Sect. 3. Here, in contrast to Tinti et al. (2001) the landslide is assumed to have a volume variable per unit cross-section and velocity variable during its motion. The runup of generated tsunami waves

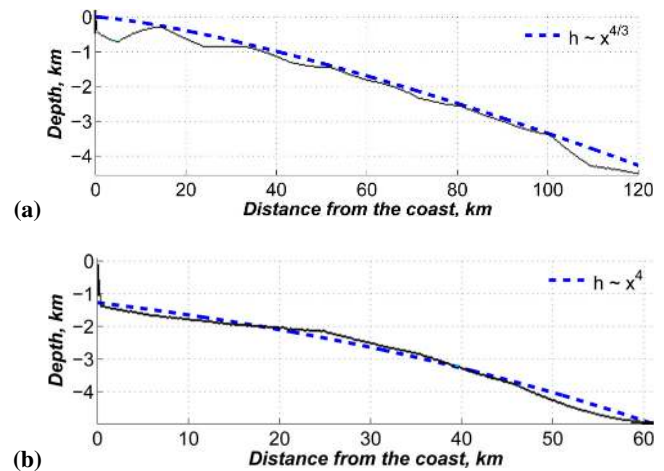


Fig. 1. Bottom profiles near Guadeloupe, Caribbean Sea (solid line) and their “non-reflecting” approximations (dashed line); (a) Marie-Galante and (b) La Desirade.

on this beach is also analyzed. The generation of tsunami waves along a quartic bottom profile $h \sim x^4$ is discussed in Sect. 4 and the new analytical solution for landslide induced tsunamis is studied in detail. The case of the resonant generation of tsunami waves by landslides above slowly varying “power” bottom profile and its propagation offshore is considered in Sect. 5. Using the asymptotic approach, the wave field is expressed analytically in the integral form and discussed for various scenarios, when the volume of the landslide increases, decreases or stays constant with time. It is shown that generally the wave amplitude varies with offshore distance non-monotonically due to competing effects of the resonant growth and the wave attenuation with a depth. The main results are summarized in Sect. 6.

2 Basic model

The governing equations of 1-D linear shallow-water theory for tsunami wave generation by underwater landslides are (Pelinovsky, 1996; Tinti et al., 2001; Liu et al., 2003):

$$\frac{\partial \eta}{\partial t} + \frac{\partial}{\partial x} [h(x)u] = W(x, t) = \frac{\partial z_b}{\partial t}, \quad (1)$$

$$\frac{\partial u}{\partial t} + g \frac{\partial \eta}{\partial x} = 0, \quad (2)$$

where $\eta(x, t)$ is the water displacement, $u(x, t)$ is the depth-averaged flow velocity, g is the gravity acceleration, $W(x, t)$ is the vertical velocity of the moving bottom boundary $z_b(x, t)$; see Fig. 2.

Initial conditions for the shallow-water system (1)–(2) are applied to both the water displacement $\eta(x, t)$ and depth-averaged flow velocity $u(x, t)$. If at the initial moment the ocean rests, they are

$$\eta(x, 0) = 0, \quad u(x, 0) = 0. \quad (3)$$

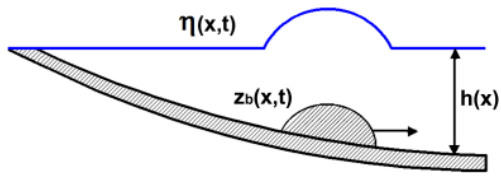


Fig. 2. The geometry of the problem: the water displacement $\eta(x,t)$ is generated by the landslide with the shape $z_b(x,t)$ above the variable bottom profile $h(x)$.

These initial conditions (3) are used in (Tinti et al., 2001; Liu et al., 2003). Meanwhile, if the vertical velocity of the landslide, W , is nonzero at the initial moment, that is a typical approximation in this kind of a problem. It follows from Eq. (1) that the vertical velocity of the fluid ($\partial\eta/\partial t$) is also nonzero. In fact, flow distribution around the body with nonzero velocity is more complicated and should be found by solving the full system of hydrodynamic equations. So the ratio between vertical and horizontal components of velocity is not evident in the shallow-water approximation. For example, Pelinovsky (1996, 2003) assumed that the vertical velocity ($\partial\eta/\partial t$) is zero at the initial moment.

Here we consider the situation of the landslide movement triggered by the earthquake that in the initial moment the landslide body lifts up and then slides down. Of course, the shallow water theory does not give a correct representation of the early fluid motion from rest. In the literature this paradox has been specially studied for the piston-model of tsunami wave motion. As it has been shown by (Kajiura, 1963) and then reproduced by (Kervella et al., 2007), if the size of the landslide is four times larger than the water depth, in shallow water theory and in full hydrodynamic model the shape of the free water surface (for the most part of the initial disturbance) coincide. The study was based on the rectangular initial disturbance and the only discrepancy between these two models was found at the sharp ends of the rectangular pulse, and this discrepancy can be smoothed by filtering. This explains why the shallow water theory is widely used for the description of the initial stage of the landslide motion. In all our calculations below we consider only smooth initial disturbances that justify the applicability of the shallow water model.

In this case the appropriate initial conditions should be derived from the assumption that the landslide velocity is zero at the initial moment as it is rigorously applied to the problem of wave generation by a moving bottom (“piston” model). Using the analogy with the piston model of tsunami generation let us consider the following approximation of the moving bottom:

$$z_b(x,t) = Y(t)Z_b(x,t), \quad (4)$$

where $Z_b(x,t)$ is a “smooth” function, that describes the landslide motion (for example, constant-speed motion), and

$Y(t)$ is almost the step function, which reflects the transition process when the landslide suddenly starts its motion. After integrating Eqs. (1) and (2) over an infinitesimal time interval the new initial conditions for the system (1)–(2) with an external forcing $W = \partial Z_b/\partial t$ can be obtained

$$\eta(x,0) = Z_b(x,0), \quad u(x,0) = 0. \quad (5)$$

These effective initial conditions (5) are well known for the piston shift of the bottom during the earthquake. Mathematically, nonzero initial conditions appear in the hyperbolic equations with an external forcing if the Cauchy problem is posed in the class of generalized functions (in our case it is a step function, which reflects sudden motion of the landslide) (Courant and Hilbert, 1989).

Equations (1) and (2) of the shallow-water system can be reduced to the wave equation for the water displacement (Z_b is replaced by z_b)

$$\frac{\partial^2 \eta}{\partial t^2} - \frac{\partial}{\partial x} \left[c^2(x) \frac{\partial \eta}{\partial x} \right] = \frac{\partial^2 z_b}{\partial t^2}, \quad c = \sqrt{gh(x)}, \quad (6)$$

which satisfies the following initial conditions

$$\eta(x,0) = z_b(x,0), \quad \frac{\partial \eta}{\partial t}(x,0) = \frac{\partial z_b}{\partial t}(x,0). \quad (7)$$

Alternatively, the wave equation for the flow velocity

$$\frac{\partial^2 u}{\partial t^2} - \frac{\partial^2}{\partial x^2} [c^2(x)u] = -g \frac{\partial^2 z_b}{\partial t \partial x}, \quad (8)$$

satisfies the initial conditions

$$u(x,0) = 0, \quad \frac{\partial u}{\partial t}(x,0) = -g \frac{\partial z_b}{\partial x}(x,0). \quad (9)$$

We would like to stress that both initial conditions (7) and (9) are derived from a more general assumption (5) and are equivalent.

Each form of the wave equation: Eq. (6) or Eq. (8) has its advantages in different problems and for different bottom configurations. Analytical solutions of both Eqs. (6) and (8) are discussed in Sects. 3 and 4, respectively. It is also important to mention here that the landslide described by the function $z_b(x,t)$ can have a variable volume and move with a variable speed. Different scenarios of the landslide body change, when its volume increases, decreases or stays constant are studied in Sect. 5.

3 Tsunami generation by the landslide motion along the bottom profile $h \sim x^{4/3}$

Let us consider here the bottom profile described by

$$h(x) = px^{4/3}, \quad (10)$$

where p is an arbitrary coefficient with a dimension $m^{-1/3}$. Here as before axis x is directed offshore and the point

$x = 0$ corresponds to the shoreline. As it has been shown in Didenkulova et al. (2009), long waves propagating along a bottom profile (10) do not interact between each other and conserve their shape, while their amplitude satisfies the Green's law ($h^{-1/4}$). In comparison with the water displacement, the velocity field has a more complicated form: the shape of the wave of velocity changes in time and its amplitude does not satisfy the Green's law. Formally, the water displacement disturbance can be considered as a traveling wave transferring the potential wave energy over large distances. The detailed analysis of the long wave dynamics along the bottom profile (10) including the process of the wave runup on the coast is given in (Didenkulova et al., 2009) for various initial disturbances.

Mathematically, this “non-reflecting” behavior is related to the possibility of reduction of the variable-coefficient wave equation to the constant-coefficient wave equation. In the case of the bottom profile (10) this reduction was first applied to the problem of tsunami generation by a moving landslide by (Tinti et al., 2001). The transformation (x_0 and h_0 represent the coordinate and the depth of the initial landslide location, respectively)

$$\eta(x, t) = A(x)H(\tau(x), t), \quad \tau = \int_{x_0}^x \frac{dx'}{c(x')},$$

$$A(x) = A_0 \left[\frac{h_0}{h(x)} \right]^{1/4}, \quad (11)$$

reduces Eq. (6) to the constant-coefficient wave equation with an external forcing

$$\frac{\partial^2 H}{\partial t^2} - \frac{\partial^2 H}{\partial \tau^2} = \frac{\partial^2}{\partial t^2} \left[\frac{z_b(\tau, t)}{A(\tau)} \right]. \quad (12)$$

The solution of Eq. (12) satisfying the initial conditions (7) can be expressed in the Duhamel integral form (Courant and Hilbert, 1989):

$$H(\tau, t) = \frac{1}{2} \left[\frac{z_b(\tau - t)}{A(\tau - t)} + \frac{z_b(\tau + t)}{A(\tau + t)} \right]$$

$$+ \frac{1}{2} \int_{\tau-t}^{\tau+t} \frac{1}{A(\sigma)} \frac{\partial z_b}{\partial t}(\sigma, 0) d\sigma$$

$$+ \frac{1}{2} \int_0^t d\rho \int_{\tau-(t-\rho)}^{\tau+(t-\rho)} \frac{1}{A(\zeta)} \frac{\partial^2 z_b}{\partial \rho^2}(\zeta, \rho) d\zeta. \quad (13)$$

Similar solution with some modifications due to other initial conditions was used in (Tinti et al., 2001) for tsunami waves generated by the landslide moving with a constant speed. Obtained results were compared with those for a flat bottom and the difference was relatively small.

Equation (13) can be presented in the explicit form for the following landslide motion:

$$z_b(\tau, t) = A(\tau)Z(\tau - Fr \cdot t), \quad (14)$$

where Fr is the constant Froude number, which determines the variable speed of the landslide

$$V(x) = \frac{dx}{dt} = c(x) \cdot Fr. \quad (15)$$

The landslide body according to Eq. (14) has the variable volume (mass) per unit cross-section

$$M(t) = \int z_b(x, t) dx = \int c(\tau) A(\tau) Z(\tau - Fr \cdot t) d\tau. \quad (16)$$

If $Z(\tau)$ is defined as a stepwise function, where τ_0 and T are arbitrary constants, which define the location and the length of the landslide,

$$Z(\tau) = \begin{cases} 0, & \tau < \tau_0, \\ 1, & \tau_0 < \tau < \tau_0 + T, \\ 0, & \tau > \tau_0 + T, \end{cases} \quad (17)$$

Eq. (16) simplifies to

$$M(t) = M_0 \left[1 + \frac{Fr}{\tau_0 + T/2} t \right]. \quad (18)$$

Thus, the landslide moves with acceleration proportional to t ($\sim x^{1/3}$ or $\sim h^{1/4}$), its height decreases with time as t^{-1} ($\sim x^{-1/3}$), but the volume grows with time and with distance ($\sim x^{1/3}$). The length of the landslide also increases ($\sim x^{2/3}$). Therefore not all the points of the landslide move at the same speed. The growth of the landslide volume can be connected to the bottom sediment friction; so that the landslide “absorbs” the surrounding materials and makes bottom particles “cling” to it. This physical process is well known for avalanches and described in (Pudasaini and Hutter, 2007). It is important to emphasize that variations of the landslide parameters (its acceleration, height and volume) with the depth are relatively slow ($\sim h^{1/4}$) and therefore, the process of the wave generation by the landslides along the bottom profile (10) can be considered as qualitatively the same as in the basin of constant depth.

Equation (13) for the special landslide shape (14) transforms into

$$H(\tau, t) = \frac{Fr^2}{Fr^2 - 1} Z(\tau - Fr \cdot t) - \frac{1}{2(Fr - 1)} Z(\tau - t)$$

$$+ \frac{1}{2(Fr + 1)} Z(\tau + t). \quad (19)$$

Solutions, similar to Eq. (19) are known for tsunami waves induced by landslides moving with a constant speed in a basin of constant depth (Pelinovsky, 1996, 2003; Tinti et al., 2001). In physical variables the solution (19) has the following form

$$\eta(x, t) = \frac{Fr^2}{Fr^2 - 1} A(x) Z \left[\int \frac{dx}{c(x)} - Fr \cdot t \right]$$

$$- \frac{A(x)}{2(Fr - 1)} Z \left[\int \frac{dx}{c(x)} - t \right] + \frac{A(x)}{2(Fr + 1)} Z \left[\int \frac{dx}{c(x)} + t \right], \quad (20)$$

and represents three waves. The first one is the forced wave, which is located above the landslide and moves with the variable velocity (15); its length increases with a distance and its amplitude is proportional to the landslide height and decreases with a distance. The forced wave is positive (wave of elevation) in super-critical regime ($Fr > 1$) and negative (wave of depression) in sub-critical regime ($Fr < 1$). The second wave is a free wave, which moves with a variable velocity $c(x)$ behind the landslide in the super-critical regime ($Fr > 1$) and in front of it in sub-critical regime ($Fr < 1$). Its amplitude decreases and its length increases in time. The third (free) wave moves shoreward with an increase in its amplitude and decrease in length. The relation between amplitudes of these waves for different values of the Froude number at the moment of wave generation is illustrated in Fig. 3.

Here the amplification factor is the ratio H/Z marked in dashed blue for the first term, dash-dotted red – for the second and solid black – for the third. The resonance between waves and the landslide ($Fr \approx 1$) dramatically increases amplitudes of waves moving offshore (in the direction of the landslide). At the same time these waves do not split in space in the vicinity of the resonance and, therefore, the resulting amplitude also stays bounded for a long time. For exact resonance ($Fr = 1$) Eq. (20) transforms into

$$\eta(x, t) = -\frac{A(x)t}{2} \frac{\partial Z}{\partial \tau} [\tau(x) - t] + \frac{3A(x)}{4} Z[\tau(x) - t] + \frac{A(x)}{4} Z[\tau(x) + t]. \quad (21)$$

The forced wave propagating offshore has a sign-variable shape. Taking into account that in the vicinity of the resonance $\tau(x) \approx t$, the resonant wave can be written as

$$\eta_{res}(x, t) = -\frac{A(x)\tau(x)}{2} \frac{\partial Z}{\partial \tau} [\tau(x) - t]. \quad (22)$$

As a result, wave amplitude grows with the distance and tends to the asymptotic value

$$A_{\infty} = \frac{3x_0}{c_0} A_0 \max(\partial Z / \partial \tau). \quad (23)$$

In contrast to the basin of a constant depth, where the resonance leads to the infinite growth of the wave amplitude, the resonant effect in the basin of a variable depth can be bounded. Detailed study of these effects is given in Sect. 5.

The wave dynamics along the beach profile (10) with the same parameter p as for the coast of Marie-Galante (Fig. 1a) is calculated below for the initial landslide shape (Fig. 4), described by

$$z_b(x, t = 0) = \frac{A(x)}{2} \left[\tanh\left(\frac{\tau(x) - \tau_0 + T/2}{a}\right) - \tanh\left(\frac{\tau(x) - \tau_0 - T/2}{a}\right) \right], \quad (24)$$

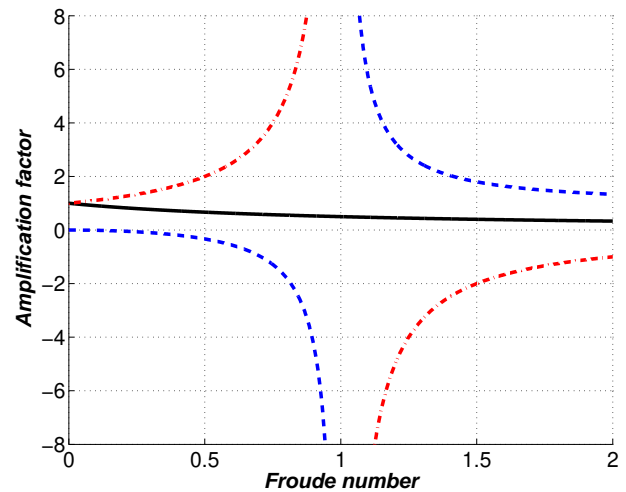


Fig. 3. Amplification factor for generated tsunami waves along the bottom profile $h \sim x^{4/3}$ plotted against the Froude number: the forced wave (dashed blue line) and free waves propagating offshore (dash-dotted red line) and onshore (solid black line).

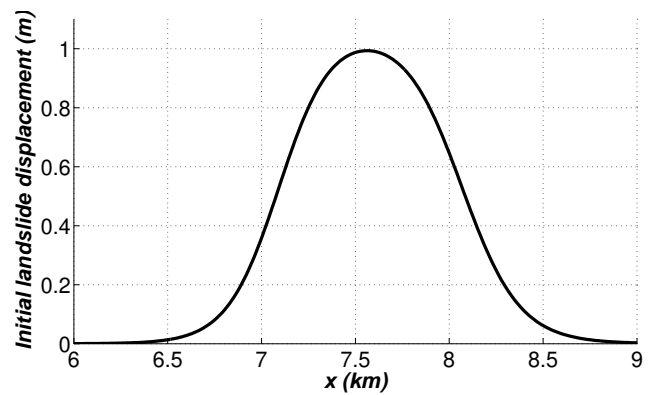


Fig. 4. Initial landslide shape (24) along the bottom profile $h \sim x^{4/3}$.

where $T = 30$ s and $\tau_0 = 11$ min, providing the location of 2 km long and 1 m high landslide at the distance 7.5 km offshore at the water depth 100 m. Parameter $a = 0.3T$ is chosen to provide smoothing of the landslide shape. Similar parameters of the landslide were used in the paper by Tinti et al. (2001), and they are also in agreement with estimations of possible and real submarine landslides in the Lesser Antilles (Ten Brink et al., 2006; Teeuw et al., 2009).

The results of calculation are presented in Fig. 5 for two different regimes of the wave motion: subcritical ($Fr < 1$) and supercritical ($Fr > 1$). In the case of the supercritical regime ($Fr = 1.2$) the forced wave, described by the first term in Eq. (19), propagates with the same velocity as the landslide body and represent the leading wave of elevation. In the case of the subcritical regime ($Fr = 0.8$) it is the second wave of depression moving offshore. Waves propagating offshore become longer with time (Fig. 5). The variations

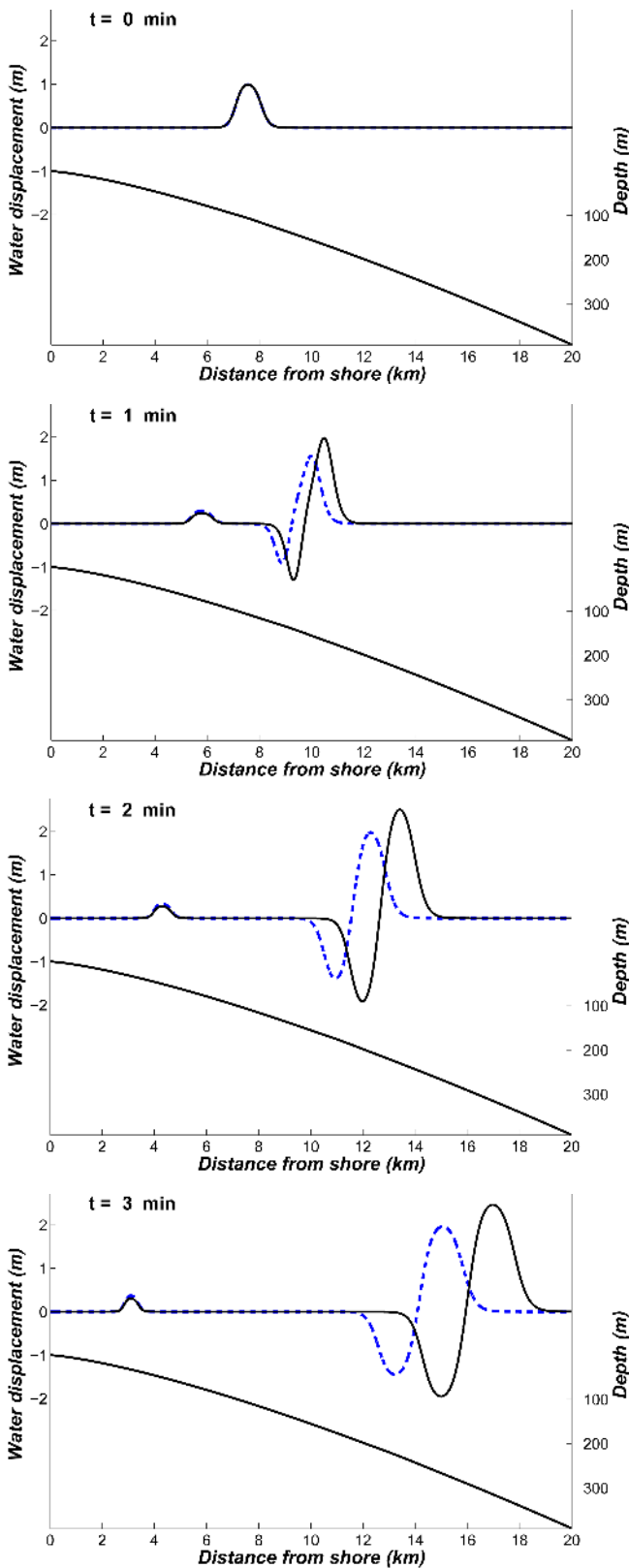


Fig. 5. Wave dynamics along the bottom profile $h \sim x^{4/3}$ in subcritical (blue dashed line) and supercritical (black line) regimes.

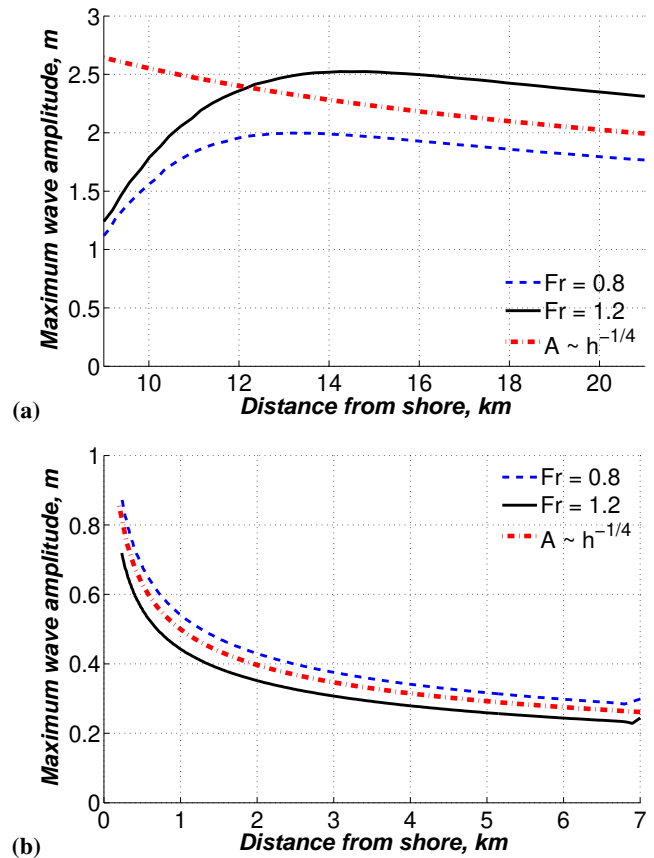


Fig. 6. Variations of the maximum amplitude of tsunami waves during its propagation along the bottom profile $h \sim x^{4/3}$: for positive waves propagating offshore (a) and onshore (b).

of their amplitudes are presented in Fig. 6a. In the beginning for a short time amplitudes of individual waves propagating offshore are increased by the resonant effect up to the factor of 2.5 in the case of the supercritical regime ($Fr = 1.2$) but at the distance of about 2–3 wavelengths they start to be determined by the function $A(x) \sim h(x)^{-1/4} \sim x^{-1/3}$, which reflects the Green’s law (Fig. 6a). The main difference between two studied regimes is that waves propagating offshore are higher and faster in the case of the supercritical regime even if the deviation from the critical value of the Froude number is the same.

The free wave of the third term in Eq. (19) moves onshore with a weak initial amplitude that grows when the wave approaches the coast (Fig. 7). The wave approaching the beach increases in its amplitude according to the Green’s law (Fig. 6b) and reduces in length. The wave amplitude is higher in the subcritical regime rather than in supercritical one. The shoaling effect becomes significant near the shore and gives wave amplification in several times (2–3 times).

There are two possible scenarios of the runoff of this wave on a beach: with or without breaking. Formally, there is no rigorous criterion of the wave breaking on the beach,

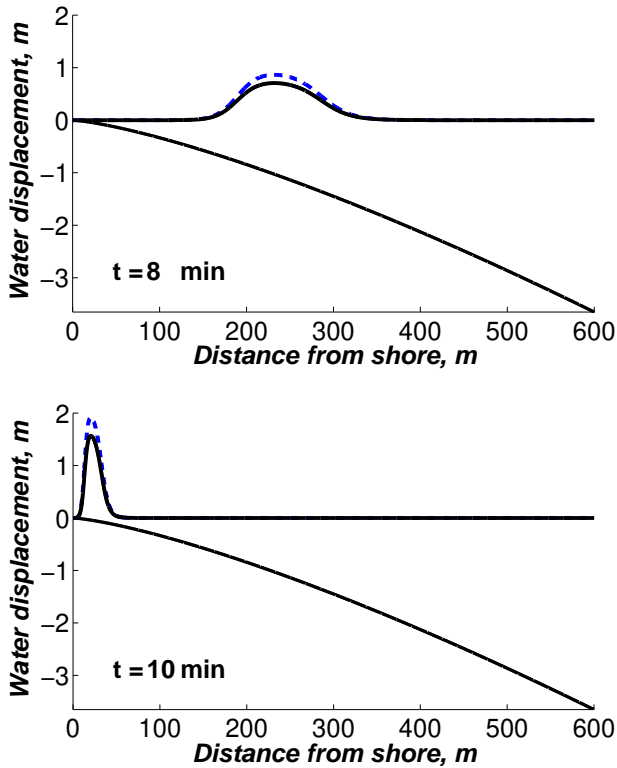


Fig. 7. Tsunami wave runup on the beach $h \sim x^{4/3}$ in subcritical (blue dashed line) and supercritical (black line) regimes.

described by Eq. (10) in comparison with a plane beach (Synolakis, 1987; Didenkulova et al., 2007, 2008), since the linear wave equation is solved. Estimates of the wave runup on the beach, described by Eq. (10), give unfeasibly high runup height (Didenkulova et al., 2009). That is why we match the non-reflecting beach (Eq. 10) with the beach of constant slope, for which the nonlinear problem of runup is solved, in the point, where the wave amplitude is small in comparison with the water depth. In our case it is the distance $X_1 \sim 500 - 600$ m from the shore. The process of the wave runup on a plane beach is well-studied (Synolakis, 1987; Didenkulova et al., 2007, 2008) and the runup height can be determined (Didenkulova et al., 2008)

$$R_{\text{plane}} \approx 3.5A\sqrt{X_1/\lambda}, \quad (25)$$

where A and λ are amplitude and wavelength of the approaching wave at the distance X_1 from the shore respectively. Taking into account wave parameters at the distance $X_1 \sim 500$ m from the shore: amplitude $A \sim 0.7$ m and wavelength is $\lambda \sim 200$ m, the runup height can be estimated from Eq. (25) as 3.9 m. It follows from Eq. (20) that amplitude of incoming wave decreases with an increase in the Froude number. Hence, the runup height also decreases with an increase in the Froude number as $\sim 1/(Fr+1)$.

At the same time, since the water depth in the near shore is too small (a few meters) it is reasonable that the dissipation of wave energy in the near-bottom turbulent flow and the wave breaking lead to the decrease in the tsunami runup height. As it is shown in (Didenkulova et al., 2010) usually landslide generated tsunami waves break at the coast. Thus, the results presented here can be considered as the upper estimate for the possible tsunami runup heights.

4 Tsunami generation by the landslide motion along the quartic bottom profile $h \sim x^4$

Another bottom profile, which allows analytical solution for the problem of tsunami wave generation by landslides, is

$$h(x) = qx^4, \quad (26)$$

where q is an arbitrary coefficient with the dimension m^{-3} .

As it has been recently shown in (Didenkulova and Pelinovsky, 2010), similarly to the wave dynamics along the bottom profile (10) discussed in Sect. 3, long waves of the flow velocity do not interact between each other along the quartic bottom profile, described by Eq. (1). These propagating waves of flow velocity do not change their shape in time and their amplitudes satisfy the Green's law for velocity ($h^{-3/4}$). In contrast to the case of the bottom profile, described by Eq. (10), the water displacement along the quartic bottom profile does not have a simple representation: the wave shape is not conserved and its amplitude does not satisfy the Green's law. The detailed analysis of the wave dynamics in this case for various initial disturbances is given in (Didenkulova and Pelinovsky, 2010).

Similarly to the case discussed in Sect. 3, the simplified behavior along the quartic bottom profile is related to the possibility of reduction of the variable-coefficient wave equation to the constant-coefficient wave equation. The following transformation

$$u(x, t) = B(x)U(\tau(x), t), \quad (27)$$

$$\tau = - \int \frac{dx}{c(x)}, \quad B(x) = bh^{-3/4}(x),$$

where b is an arbitrary constant with dimension $m^{7/4} s^{-1}$, reduces the wave equation for the flow velocity with an external forcing (8) to the inhomogeneous constant-coefficient wave equation

$$\frac{\partial^2 U}{\partial t^2} - \frac{\partial^2 U}{\partial \tau^2} = - \frac{g}{B(\tau)c(\tau)} \frac{\partial^2 z_b(\tau, t)}{\partial t \partial \tau}. \quad (28)$$

Initial conditions for Eq. (3) follow from Eqs. (9) for velocity flow that is identical to Eqs. (7) for water displacement

$$U(\tau, 0) = 0, \quad \frac{\partial U}{\partial t}(\tau, 0) = - \frac{g}{B(\tau)c(\tau)} \frac{\partial z_b}{\partial \tau}(\tau, 0). \quad (29)$$

Here the spatial domain ($0 < x < \infty$) transforms to the new domain ($\infty < \tau < 0$) with an opposite direction that differs

from the previous case of the beach (10), described in Sect. 3. It means that in the new variables the landslide moves to the left.

Similarly to the case described in Sect. 3, the solution of Eq. (3) satisfying the initial conditions (4) can be represented in the form of the Duhamel integral (Courant and Hilbert, 1989):

$$U(\tau, t) = -\frac{1}{2} \int_{\tau-t}^{\tau+t} \frac{g}{B(\sigma)c(\sigma)} \frac{\partial z_b}{\partial \sigma}(\sigma, 0) d\sigma - \frac{1}{2} \int_0^t d\rho \int_{\tau-(t-\rho)}^{\tau+(t-\rho)} \frac{g}{B(\zeta)c(\zeta)} \frac{\partial^2 z_b}{\partial \rho \partial \zeta}(\zeta, \rho) d\zeta. \quad (30)$$

The new forcing function

$$P(\tau, t) = \int \frac{g}{B(\tau)c(\tau)} \frac{\partial z_b(\tau, t)}{\partial \tau} d\tau, \quad (31)$$

simplifies Eqs. (28) and (29) and transforms them to

$$\frac{\partial^2 U}{\partial t^2} - \frac{\partial^2 U}{\partial \tau^2} = -\frac{\partial^2 P(\tau, t)}{\partial t \partial \tau}, \quad (32)$$

$$U(\tau, 0) = 0, \quad \frac{\partial U}{\partial t}(\tau, 0) = -\frac{\partial P}{\partial \tau}(\tau, 0). \quad (33)$$

If the new forcing function (31) of the landslide motion can be presented in the following way

$$P(\tau, t) = P(\tau + Fr \cdot t), \quad (34)$$

Eq. (30) transforms into a simple explicit solution for the velocity field

$$U(\tau, t) = -\frac{Fr}{Fr^2 - 1} P(\tau + Fr \cdot t) + \frac{1}{2(Fr - 1)} P(\tau + t) + \frac{1}{2(Fr + 1)} P(\tau - t), \quad (35)$$

which represents three waves of velocity, the first of which is the forced one propagating offshore (the first term in Eq. 35), and other two are free waves propagating offshore and onshore respectively. The amplitude of the forced wave propagating offshore in dimensionless variables varies linearly with time in the vicinity of the resonance ($Fr = 1$)

$$U(\tau, t) = -\frac{t}{2} \frac{\partial P(\tau + t)}{\partial \tau} - \frac{1}{4} P(\tau + t) + \frac{1}{4} P(\tau - t). \quad (36)$$

The water displacement can be found from Eq. (2)

$$\frac{\partial \eta}{\partial \tau} = -bq^{1/4} \tau \frac{\partial U}{\partial t}, \quad (37)$$

using the condition of zero displacement at infinity $x \rightarrow \infty$ that corresponds to $\tau = 0$.

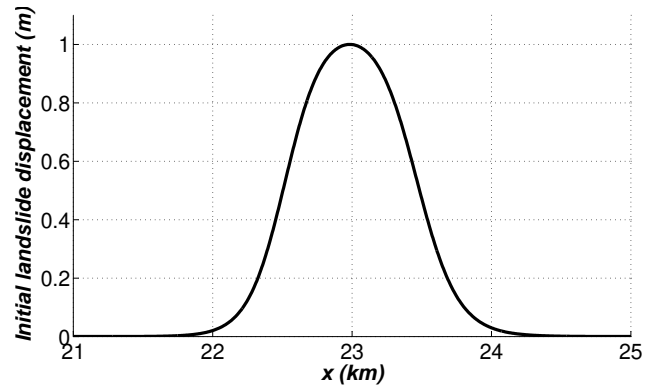


Fig. 8. Initial landslide shape (38) along the quartic bottom profile $h \sim x^4$.

The long wave dynamics along the quartic bottom profile is discussed for the landslide shape (Fig. 8) given by

$$z_b(x, t = 0) = \frac{A_0}{2} \left[\tanh\left(\frac{\tau(x) - \tau_0 + T/2}{a}\right) - \tanh\left(\frac{\tau(x) - \tau_0 - T/2}{a}\right) \right], \quad (38)$$

where τ_0 represents the travel time to the deep water. The landslide shape in Eq. (38) differs from the one discussed in Sect. 3 (Eq. 24) by the amplitude A . It is constant in Eq. (38), while in Eq. (24) it is a function of coordinate $A(x)$, representing the Green's law. Though the solution (Eq. 35) describing the long wave dynamics along the quartic profile is very similar to the one, discussed in Sect. 3, there are some differences, which should be mentioned. The depth of a quartic bottom profile is a rapid function of the distance far from the coast that leads to the fact that long waves cross the deep water in a fixed time. It is evident that the shallow-water approximation breaks down on large depths and the solution given by Eq. (35) does not work there.

At the same time the water depth becomes very shallow in the near shore and very soon the wave amplitude starts to be comparable with the water depth and the wave should break due to the nonlinearity. The reflection from such a beach is also very small and almost negligible. At the same time it can be significant if we place the vertical wall at some distance from the shore and study the wave dynamics in this new bottom geometry. This situation of a sudden change of the depth just at the shore occurs quite often for rocky and cliffy coasts. One of such examples is shown on Fig. 1b for Desirade. In this case the wave can be reflected from the vertical wall without breaking. Such a situation is considered in (Didenkulova and Pelinovsky, 2010). Anyhow we are not going to do it here and consider our solution given by Eqs. (35) and (36) only in the main part of the basin, excluding deep water part and the vicinity of the shoreline.

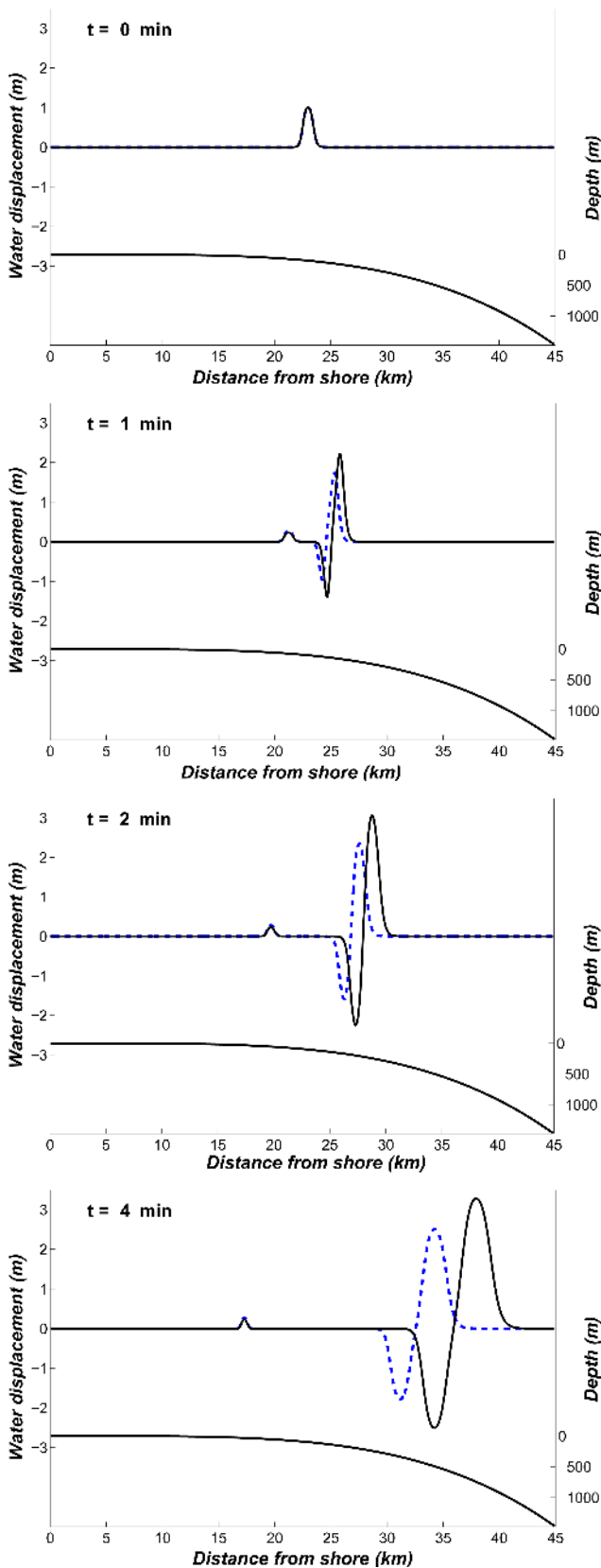


Fig. 9. Wave dynamics along the quartic bottom profile $h \sim x^4$ in subcritical (blue dashed line) and supercritical (black line) regimes.

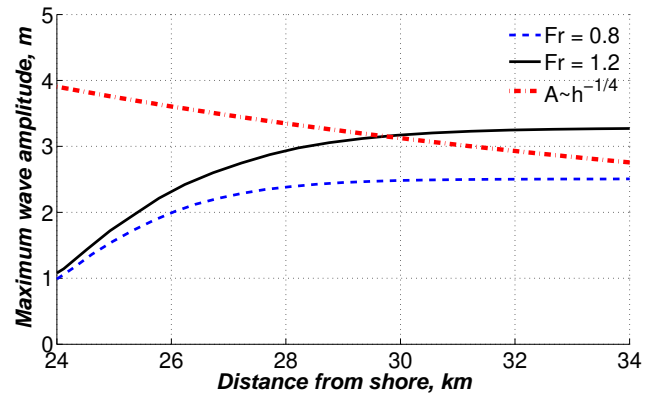


Fig. 10. Variations of the maximum amplitude of tsunami waves during its propagation along the quartic bottom profile $h \sim x^4$ for positive waves propagating offshore.

The calculated long wave dynamics along the quartic bottom profile with the parameter q taken from the bathymetry near Desirade (Fig. 1b) for the landslide shape (38) is illustrated in Fig. 9 for sub- ($Fr=0.8$) and supercritical ($Fr=1.2$) regimes. The landslide of 1 m high and 2 km long is located at the distance of 23 km from the shore at the depth of 100 m, the travel time to the deep water τ_0 is 12 min, T is 30 s and $a = 0.3T$.

In the initial moment the water displacement has the same shape as the landslide and initial velocity is zero. As it has been discussed for the beach profile (10) in Sect. 3, the waves that travel upward the quartic bottom profile are larger and faster in case of supercritical regime.

Variations of wave amplitudes with the distance are presented in Fig. 10. In the beginning amplitudes of waves propagating offshore grow due to the resonant effect and then stabilize with some value at deep waters. It can be seen that the wave amplitude does not follow the Green’s law (Fig. 10). As it has been mentioned above, it is related to very fast changes of the water depth offshore that is contradictory to the shallow water theory.

Thus, generally the wave dynamics along the quartic bottom profile is very similar to the one, discussed in Sect. 3 for the beach profile, described by Eq. (10). The landslide motion generates three waves, two of which propagate offshore in the direction of the landslide and one propagates onshore. Amplitudes of offshore propagating waves grow due to the resonance effect and reach 3.3 m in subcritical and 2.5 m in supercritical regimes. For comparison, in the case of the bottom profile (10), discussed in Sect. 3, for the similar shape of the landslide, located at the same depth, the maximum values of the offshore propagating waves are 2.5 m in subcritical and 2 m in supercritical regimes. Hence two analytical solutions presented here give similar estimates for amplitudes of landslide generated waves.

We should mention that rigorous analytical solutions discussed here are found within shallow water theory and do not take into account wave dispersion. However in the case of a weak dispersion the processes of tsunami wave generation and propagation can be considered independently. The process of tsunami wave generation can be studied in the framework of the shallow water theory, while the wave propagation over long distances, when dispersive effects start to be significant, can be studied within Bousinesq-type models. Here we focus on the process of tsunami wave generation and obtained solutions of the shallow water theory are adequate.

5 Tsunami generation by the resonantly moving landslide along an arbitrary bottom profile

Two analytical examples of tsunami wave generation by the landslides, described in Sects. 3 and 4, demonstrate the important role of the resonance, when the landslide and the sea waves are moving with the same speeds ($Fr = 1$). As it has been shown in Sect. 3 the resonant wave amplitude can be bounded in the basin of variable depth, whereas it tends to infinity if the depth of the basin is constant. It makes clear that the resonance phenomenon should be considered not only for specific bottom configurations but for a more general case that should give us understanding about the sensitivity of these results to variations of the bottom profile and landslide characteristics.

Here this effect is studied for a basin of a slowly varying depth. Anyhow we do not analyze the full wave field, since the dynamics of the “non-resonant” wave approaching the coast is not related to the landslide motion and we do not expect large variations of its amplitude for all other regimes of tsunami generation by the landslide. Here we concentrate on the “resonant” waves propagating offshore. In the vicinity of the resonance these waves propagate with speeds close to the local wave celerity $c(x)$, which slowly changes with a distance, since the depth is a slow function of the distance. For this case let us introduce new adequate coordinates in Eq. (6)

$$s = \tau(x) - t, \quad x' = x, \tag{39}$$

where $\tau(x)$ is a travel time as before. After substitution of Eq. (39) the wave equation (6) has the following form

$$2c(x') \frac{\partial^2 \eta}{\partial s \partial x'} + \frac{dc}{dx'} \frac{\partial \eta}{\partial s} + \frac{\partial}{\partial x'} \left[c^2(x') \frac{\partial \eta}{\partial x'} \right] = - \frac{\partial^2 z_b}{\partial s^2}. \tag{40}$$

The last term in LHS of Eq. (40) is small according to the assumptions given above and can be neglected. After integration of Eq. (40) and some simple manipulations the solution for the water displacement can be found (prime is omitted):

$$\eta(x, s) = - \frac{1}{2\sqrt{c(x)}} \int_{x_0}^x \frac{1}{\sqrt{c(y)}} \frac{\partial z_b(y, s)}{\partial s} dy + \eta(x_0, s), \tag{41}$$

where the location ($x = x_0$) is chosen at the right border of the initial location of the landslide and the function $\eta(x_0, s)$ is the tsunami time series in this location. Eq. (41) corresponds to the first two terms in Eq. (21), describing the waves propagating offshore along the bottom profile $h \sim x^{4/3}$. Here we focus on the dynamics of the resonant wave, described by

$$\eta_{res}(x, s) = - \frac{1}{2\sqrt{c(x)}} \int_{x_0}^x \frac{1}{\sqrt{c(y)}} \frac{\partial z_b(y, s)}{\partial s} dy. \tag{42}$$

Equation (42) can be used for study of tsunami wave generation by the landslide of a variable volume (mass) moving with an arbitrary speed. It is restricted by the speed of the landslide, which should be close to the wave speed.

Let us consider the resonantly moving landslide of an arbitrary shape and variable volume

$$z_b(x, t) = Q(x)Z(s) = Q(x)Z[\tau(x) - t], \tag{43}$$

which according to Eq. (41) generates tsunami waves of variable amplitude $D(x)$

$$\eta_{res}(x, t) = -D(x) \frac{\partial Z(\tau - t)}{\partial \tau}, \quad D(x) = \frac{1}{2\sqrt{c(x)}} \int_{x_0}^x \frac{Q(y)dy}{\sqrt{c(y)}}, \tag{44}$$

along a general “power” bottom profile

$$h(x) = h_0 \left(\frac{x}{x_0} \right)^\gamma, \quad \gamma > 0. \tag{45}$$

As it has been mentioned above the resonant wave has a sign-variable shape for any kind of the bottom profile. For understanding of all possible regimes of the tsunami wave generation it is important to consider different scenarios of the landslide volume variations.

The first case is when the landslide height changes with depth according to the Green’s law (this assumption is used in Sect. 3)

$$Q_{Gr}(x) = Q_0 \left(\frac{h}{h_0} \right)^{-1/4} = Q_0 \left(\frac{x}{x_0} \right)^{-\gamma/4}. \tag{46}$$

In this case the wave amplitude $D(x)$ is

$$D_{Gr}(x) = \frac{Q_0 x_0}{2\sqrt{gh_0}} N_{Gr}(x),$$

$$N_{Gr}(x) = \begin{cases} \frac{1}{1 - \gamma/2} \left[(x/x_0)^{1-3\gamma/4} - (x/x_0)^{-\gamma/4} \right], & \gamma \neq 2 \\ \ln(x/x_0) / (x/x_0)^{1/2}, & \gamma = 2 \end{cases}, \tag{47}$$

where the function $N_{Gr}(x)$ is displayed in Fig. 11. It follows

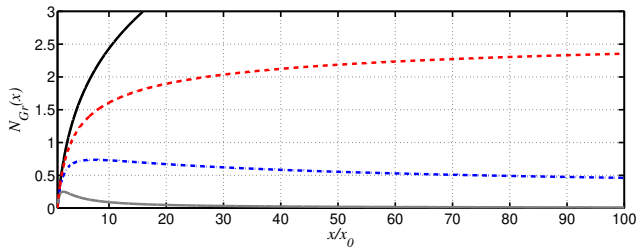


Fig. 11. Wave amplitude variations versus distance (Eq. 47) for $\gamma = 1$ (black solid line), $\gamma = 4/3$ (red dashed line), $\gamma = 2$ (blue dash-dotted line), $\gamma = 4$ (green dotted line).

from Eq. (47) that the wave amplitude grows up to infinity for $\gamma < 4/3$, but slower than in the basin of constant depth. In the case of the “non-reflecting” beach ($\gamma = 4/3$) discussed in Sect. 3, the wave amplitude asymptotically tends to its maximum. For all values $\gamma > 4/3$, the competition of two effects: resonance and increasing water depth leads to a non-monotonic behavior of the wave amplitude. If the depth increases with distance more rapidly the amplification becomes smaller and the amplification zone becomes narrower.

For analysis to be completed we need to calculate the volume of the landslide. In the case of $\gamma < 2$ the volume of the landslide can be computed explicitly

$$M_{Gr}(t) = \int z_b(x, t) dx = \int c(\tau) Q(\tau) Z(\tau - t) d\tau \sim \int \tau^{\frac{\gamma}{2(2-\gamma)}} Z(\tau - t) d\tau \sim t^{\frac{\gamma}{2(2-\gamma)}}. \quad (48)$$

It increases as $t^{1/2}$ along the plane beach and as t along the “non-reflecting” beach. So, the landslide volume grows with the distance while the wave amplitude decreases for $\gamma > 4/3$.

The second case is the landslide of a constant volume, which height and length vary with a distance. It follows from Eq. (48) that this can be realized if $Q \sim c^{-1}$:

$$Q_C(x) = Q_0 \left(\frac{h}{h_0}\right)^{-1/2} = Q_0 \left(\frac{x}{x_0}\right)^{-\gamma/2}, \quad (49)$$

for which

$$N_C(x) = \begin{cases} \frac{1}{1-3\gamma/4} \left[(x/x_0)^{1-\gamma} - (x/x_0)^{-\gamma/4} \right], & \gamma \neq 4/3 \\ \frac{\ln(x/x_0)}{(x/x_0)^{1/3}}, & \gamma = 4/3 \end{cases}. \quad (50)$$

The function $N_C(x)$ is bounded for $\gamma \geq 1$, and for all $\gamma > 1$ the wave amplitude decreases with the distance (Fig. 12). The maximum amplification along the plane beach ($\gamma = 1$) is $N_C(x \rightarrow \infty) = 4$.

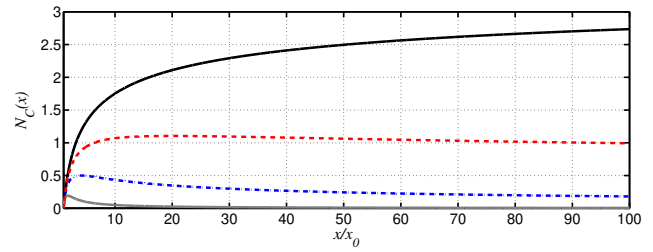


Fig. 12. Wave amplitude variations versus distance (Eq. 50) for $\gamma = 1$ (black solid line), $\gamma = 4/3$ (red dashed line), $\gamma = 2$ (blue dash-dotted line), $\gamma = 4$ (green dotted line).

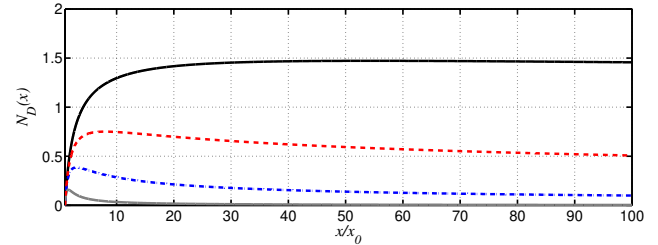


Fig. 13. Wave amplitude variations versus distance (Eq. 53) for $\gamma = 1$ (black solid line), $\gamma = 4/3$ (red dashed line), $\gamma = 2$ (blue dash-dotted line), $\gamma = 4$ (green dotted line).

And the third case is the landslide motion with the decrease in its volume, which we study on the following example:

$$Q_D(x) = Q_0 \left(\frac{h}{h_0}\right)^{-3/4} = Q_0 \left(\frac{x}{x_0}\right)^{-3\gamma/4}. \quad (51)$$

For the “non-reflecting” bottom profile (10) and $Z(\tau)$ defined by Eq. (17) the volume of the landslide can be calculated explicitly.

$$M_D(t) = Q_0 x_0 \ln \left[1 + \frac{T}{\tau_0 + t} \right]. \quad (52)$$

As before, the wave amplitude is described by the function $N_D(x)$

$$N_D(x) = \begin{cases} \frac{1}{1-\gamma} \left[(x/x_0)^{1-5\gamma/4} - (x/x_0)^{-\gamma/4} \right], & \gamma \neq 1 \\ \frac{\ln(x/x_0)}{(x/x_0)^{1/4}}, & \gamma = 1 \end{cases}. \quad (53)$$

Now the wave amplitude decreases for all $\gamma > 4/5$ including the plane beach (Fig. 13).

Thus, we demonstrate that the joint action of the resonance and increasing depth generally leads to non-monotonic variations of the wave amplitude with a distance. The result is sensitive to the landslide volume variations in time and the amplification zone reduces with a decrease in the landslide volume.

6 Conclusions

The tsunami wave generation by submarine landslides of a variable volume moving with a variable speed in a basin of variable depth is studied analytically.

The theory of tsunami wave generation by landslides is developed for basins of “non-reflecting” bottom configurations $h \sim x^{4/3}$ and $h \sim x^4$. For such bottom configurations the shallow-water system can be reduced to the constant-coefficient wave equation with an external forcing, and its analytical solution can be expressed in the form of the Duhamel integral. Analytical solutions for tsunami wave generation by landslides of variable volume and speed are obtained and discussed. They consist of three waves: the forced wave propagating in the same direction as the landslide and two free waves propagating in the opposite directions. The forced wave is located above the landslide and propagates with a variable velocity; its length increases with a distance and its amplitude is proportional to the landslide height and decreases with a distance. The forced wave is presented by the wave of elevation in supercritical regime ($Fr > 1$) and by the wave of depression in sub-critical regime ($Fr < 1$). One of the free waves propagates offshore with a variable velocity $c(x)$. It moves behind the landslide in the supercritical regime ($Fr > 1$) and in front of it in sub-critical regime ($Fr < 1$). In the beginning its amplitude increases due to the resonant effect and then decreases according to the Green’s law for the beach $h \sim x^{4/3}$ or stabilizes at deep waters for the beach $h \sim x^4$. The wavelengths of the waves propagating offshore increase in time. Another free wave propagates onshore with an increase in its amplitude and decrease in its length.

The runup of the landslide generated wave approaching the coast $h \sim x^{4/3}$ is studied analytically assuming that the wave does not break at the shoreline. The runup characteristics depend on the Froude number.

The process of the resonant generation of tsunami waves by landslides is studied in a basin of slowly varying depth. Using the asymptotic approach, the wave field can be expressed analytically in the integral form. The main result here is that even for the landslide moving with the resonant speed, generally the wave amplitudes remain bounded and decrease at large distances for most of “power-like” beaches.

Since the resonance leads to the maximum amplification, the obtained expressions can be used for evaluation of prognostic tsunami waves generated by the submarine landslides of variable volume and speed. These analytical results can also be used for testing numerical schemes.

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