



Shah, Y. D. , Grant, J. , Hao, D., Kenney, M. , Pusino, V. and Cumming, D. R.S. (2018) Ultra-narrow line width polarization-insensitive filter using a symmetry-breaking selective plasmonic metasurface. *ACS Photonics*, 5(2), pp. 663-669.

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*ACS Photonics*, **Just Accepted Manuscript** • DOI: 10.1021/acsp Photonics.7b01011 • Publication Date (Web): 12 Dec 2017

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# Ultra-narrow linewidth polarization-insensitive filter using a symmetry-breaking selective plasmonic metasurface

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## Abstract

Plasmonic metasurfaces provide unprecedented control of the properties of light. By designing symmetry-breaking nanoholes in a metal sheet and engineering the optical properties of the metal using geometry, highly selective transmission and polarisation control of light is obtained. To date such plasmonic filters have exhibited broad ( $> 200$  nm) transmission linewidths in the NIR and as such are unsuitable for applications requiring narrow passbands, e.g. multi-spectral imaging. Here we present a novel sub-wavelength elliptical and circular nanohole array in a metallic film that simultaneously exhibits high transmission efficiency, polarisation insensitivity and narrow linewidth. The experimentally obtained linewidth is 79 nm with a transmission efficiency of 44%. By examining the electric and magnetic field distributions for various incident polarisations at the transmission peak we show that the narrowband characteristics are due

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3 to a Fano resonance. Good agreement is obtained between the experimental data, sim-  
4 ulations and analytical calculations. Our design can be modified to operate in other  
5 6 regions of the electromagnetic spectrum and these filters may be integrated with suit-  
7 8 able detectors such as photodiodes and single photon avalanche diode (SPAD) arrays.  
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12 Keywords: (plasmonics; Fano resonance; metasurface; nanophotonics; surface plasmon po-  
13 laritons; subwavelength optics)

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16 Nanophotonics encompasses a broad field that deals with quantum and classical light-matter  
17 interaction that can yield devices used for applications such as imaging,<sup>1-3</sup> spectroscopy and  
18 bio-sensing.<sup>4-6</sup> In recent years significant progress has been made in nanophotonics based  
19 on the phenomena of surface plasmon resonance<sup>7,8</sup> and plasmonic metasurfaces.<sup>9-12</sup> There  
20 has been growing interest in these two-dimensional metasurfaces,<sup>13-17</sup> since their introduc-  
21 tion, for manipulating the propagation of electromagnetic waves.<sup>18</sup> The thickness of these  
22 structures is far smaller than the operational wavelength, which allows the miniaturization  
23 and integration of various optical components and systems. Plasmonic metasurfaces have  
24 gained prominence in this field due to their ability to control individually and simultaneously  
25 the phase,<sup>19</sup> momentum,<sup>20</sup> amplitude<sup>21</sup> and polarization of light<sup>19</sup> and hence promise great  
26 utility in the realization of compact photonic devices through tuneable resonant properties  
27 controlled by near field coupling.<sup>22</sup> In addition, there has been particular interest in ultra-  
28 thin metasurfaces operating in transmission mode, but these metasurfaces are still in their  
29 infancy because of their low efficiency.  
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44 The periodic arrangement of nanoholes in a metal sheet leads to resonant coupling be-  
45 tween the surface plasmon polaritons (SPP) on the surface of the corrugated metal surface  
46 and the incident light leading to extraordinary optical transmission (EOT).<sup>22-28</sup> It has been  
47 demonstrated that both the period and the geometry of the nanoholes (localised surface  
48 plasmon resonance) play a role in determining the transmission characteristics.<sup>22</sup> Plasmonic  
49 filters consist of circular or rectangular nanoholes<sup>21,22,29-31</sup> or gratings in a thin metal film  
50 arranged in a periodic array.<sup>23,32,33</sup> Such plasmonic bandpass filters are a simple and elegant  
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3 alternative to the more complex and challenging to fabricate dichroic film filters. Moreover,  
4 the resonance transmission passband of a plasmonic metasurface filter can be shifted to a  
5 desired frequency by altering the size and period of the nanoholes. Although the use of  
6 metals results in losses in the SPP, several strategies have been presented to overcome this  
7 deficiency.<sup>7,34</sup> For a single layer filter with a regular triangular circular hole lattice on glass,  
8 the transmission observed was between 30-35% with a linewidth of >100 nm in the visible  
9 spectrum.<sup>30</sup> Similar devices made in the near infrared (NIR) region achieved a transmission  
10 coefficient of 65%<sup>31</sup> with a broad linewidth of 220 nm. High transmission has been observed  
11 for multilayer Fabry-Prot type designs (multiple stacks of alternating metallic and dielectric  
12 structures) that increase the transmission coefficient to 60-65% with a linewidth of 110 nm  
13 in the visible.<sup>35</sup> These designs, however, generally require sophisticated fabrication processes  
14 and complicated variations of unit cells. The combination of high transmission and narrow  
15 linewidth has to date proved difficult to achieve. Moreover, plasmonic filters typically suffer  
16 from poor out-of-band suppression with unwanted transmission peaks observed at longer  
17 wavelengths. Narrow linewidth, high transmission efficiency, low-cost and miniaturizable fil-  
18 ters suitable for monolithic integration with detectors are desirable for multispectral imaging  
19 applications as well as gas detection due to the narrow spectral response of molecules such  
20 as CO, NO and CH<sub>4</sub>.<sup>35,36</sup>

## 41 Results and discussion

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44 In this letter we present a novel NIR filter yielding high transmission, narrow linewidth,  
45 and polarisation insensitivity using an array, wherein elliptical nanoholes are made alongside  
46 circular ones, with a hexagonal lattice to form a supercell. An advantage of this design is that  
47 because it is a single layer fabrication process, it can be tuned to any desirable wavelength by  
48 scaling the elliptical and circular nanohole sizes and period. Hexagonal lattice arrangements  
49 of nanoholes have been shown to provide sharper EOT resonances and a higher confinement of  
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3 E-field which make this arrangement suitable for sensing applications.<sup>37,38</sup> Elliptical nanohole  
4 arrays<sup>39,40</sup> have been investigated to provide an efficient polarisation dependent,<sup>41</sup> broadband  
5 response<sup>42,43</sup> and have found applications in biosensing due to the high sensitivity to changes  
6 in refractive index.<sup>44</sup> Two designs are presented in our investigation, the unit cells of which  
7 are highlighted in Figure 1. In the first instance we have a design optimised with ellipses  
8 oriented all at the same angle of 135° to the x-axis, as shown in Figure 1(A)(i), and in the  
9 second instance we have a design with ellipses alternately oriented in 45° and 135°, as shown  
10 in Figure 1(A)(ii) .

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13 Due to the permittivity discontinuity at metal-dielectric surfaces, SPPs have an in-plane  
14 momentum. Under normally incident light, the free-space radiation cannot couple to surface  
15 plasmons directly but it is feasible, with the help of a grating, to provide the additional  
16 momentum. The SPP momentum vector is given by,  $\mathbf{k}_{spp} = \mathbf{k}_{sin\theta} + \mathbf{k}_{i,j}$ , where  $\mathbf{k}_{sin\theta}$  is the  
17 momentum from light incident on the device and  $\mathbf{k}_{i,j}$  is dependent on the diffraction grating  
18 order. For normally incident light,  $\mathbf{k}_{sin\theta}$  is 0 and hence  $\mathbf{k}_{spp}$  is given as Equation 1;

$$k_{spp} = k_{i,j} = \frac{a^*}{\sqrt{\frac{4}{3}(i^2 + ij + j^2)}} \sqrt{\frac{\epsilon_m \epsilon_d}{\epsilon_m + \epsilon_d}} \quad (1)$$

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21 where  $a^*$  is the period of the nanoholes in the metal sheet, (i,j) signify the diffraction grating  
22 order and  $\epsilon_m$  and  $\epsilon_d$  are the permittivities of metal and dielectric respectively. To obtain a  
23 value of  $\mathbf{k}_{spp}$  corresponding to a transmission minimum<sup>45,46</sup> of 1.52  $\mu\text{m}$  we calculated that  
24 the lattice period  $a^*$  should be 1.17  $\mu\text{m}$  for the (1,0) diffraction order.

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27 The thickness of the gold was selected to be 80 nm as it gave a good trade-off between  
28 linewidth and transmission for the calculated period (See Figure S1 in the Supplementary  
29 information). The ratio of the short axis to long axis (b/a) of the ellipses was selected to  
30 be 0.8. Figure 1(B) shows the variation in simulated transmission spectrum for the design  
31 with ellipses orientated at 45° and 135°. The linewidths for several b/a ratios are also  
32 labelled. Assuming an E-field dependency such that  $(\mathbf{E}_b/\mathbf{E}_a)^2 \propto (b/a)$ ,  $\mathbf{E}_a$  and  $\mathbf{E}_b$  should  
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be approximately equal for  $b/a$  ratios in the range 0.75 - 0.85.<sup>41</sup> Owing to subwavelength confinement of the E-field mode, the dimensions of the nanoholes were limited to  $\lambda/4$ . The dimensions of the ellipses were 430 nm by 346 nm (long axis and short axis respectively with a  $b/a$  ratio of 0.8) and the circles have a diameter of 404 nm. A 300 nm thick cap layer of  $\text{SiO}_2$  was deposited on the perforated metal layer.

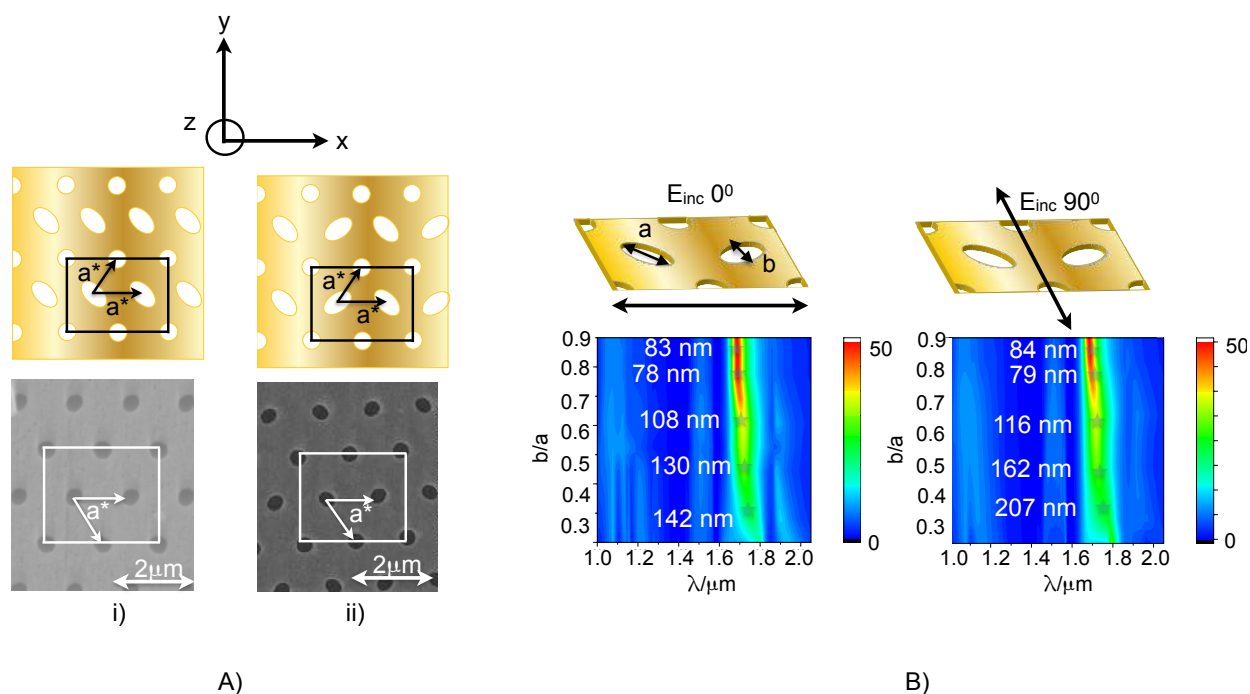


Figure 1: (A)(i) and (ii) Schematic and the corresponding SEM images of two plasmonic metasurfaces with elliptical and circular nanoholes arranged periodically.  $a^*$  is the period. (B) For  $\mathbf{E}_{inc}$  at  $0^\circ$  and  $90^\circ$  polarisations, the transmission spectra were simulated as a function of the ratio:  $b/a$  i.e. ratio of short axis to long axis. It can be seen from the dispersion colour plots that the linewidth narrows with increasing  $b/a$  in the range 0.3 – 0.9.

The fabrication of these devices is described in the Methods section. The transmission spectra were measured in a CRAIC 20/30 PV<sup>TM</sup> micro-photo-spectrometer system with a polariser and condenser lens. The aperture for the incident light has a diameter of 0.5 mm and the objective lens has a NA of 0.25.

Figure 2 plots the transmission spectra measured from the designs with unit cell highlighted in the SEM insets. Figure 2(A), shows the experimental transmission spectrum for the design with the ellipses oriented at  $135^\circ$  for incident light polarised at  $0^\circ$ ,  $45^\circ$ ,  $90^\circ$  and

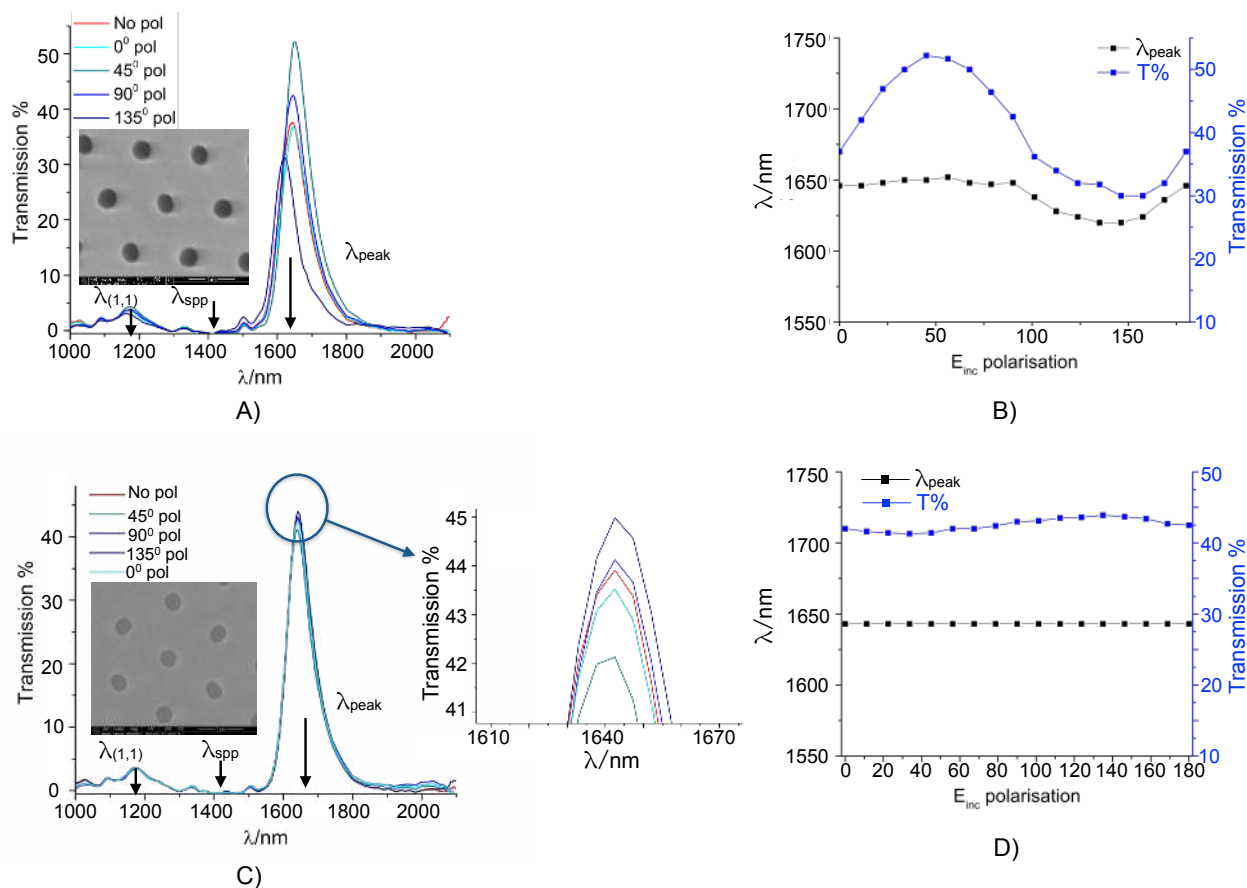


Figure 2: (A) The transmission spectra from the design with ellipses oriented at 135° to the x-axis for  $E_{inc}$  at 0°, 45°, 90° and 135° and unpolarised light (red). (B) A variation  $\Delta\lambda/\lambda$  of 1.9% and  $\Delta T$  of 23% is observed. (C) A high transmission of 44% and a narrow linewidth of 79 nm is observed for all  $E_{inc}$  polarisations for the design with ellipses oriented at 45° and 135° to the x-axis. (D) The transmission efficiency from this design are polarisation insensitive as  $\Delta\lambda/\lambda$  is 0% and  $\Delta T$  is 2.5%. Both designs have a high out of band rejection.

135°. The transmission data for unpolarised incident light is also shown. A maximum transmission of 53% is observed for  $E_{inc}$  polarised at 45° with a narrow linewidth of 92 nm. This can be attributed to the plasmon resonance excited along the shorter axis (b) of the ellipses. However the metasurface is sensitive to the incident polarization - there is a change of 1.9% in wavelength ( $\Delta\lambda/\lambda$ ) and a large change in transmission ( $\Delta T$ ) of 23%, as highlighted in Figure 2(B). However, unlike previously reported plasmonic filters, we observe a suppression of higher order modes with the mode at  $\lambda_{(1,1)}$  as small as 4%. The out of band rejection at other wavelengths is below this level. For the device design with the alternate ellipses



oriented at  $45^\circ$  and  $135^\circ$  (unit cell highlighted in the SEM inset in Figure 2(C)) we observe that  $\lambda_{peak}$  is insensitive to variations in the  $\mathbf{E}_{inc}$  polarisation, and that the transmission remains the same. We observe a very narrow FWHM of 79 nm (Q factor of 26) which is, to the best of our knowledge, the narrowest recorded from a plasmonic metasurface filter.

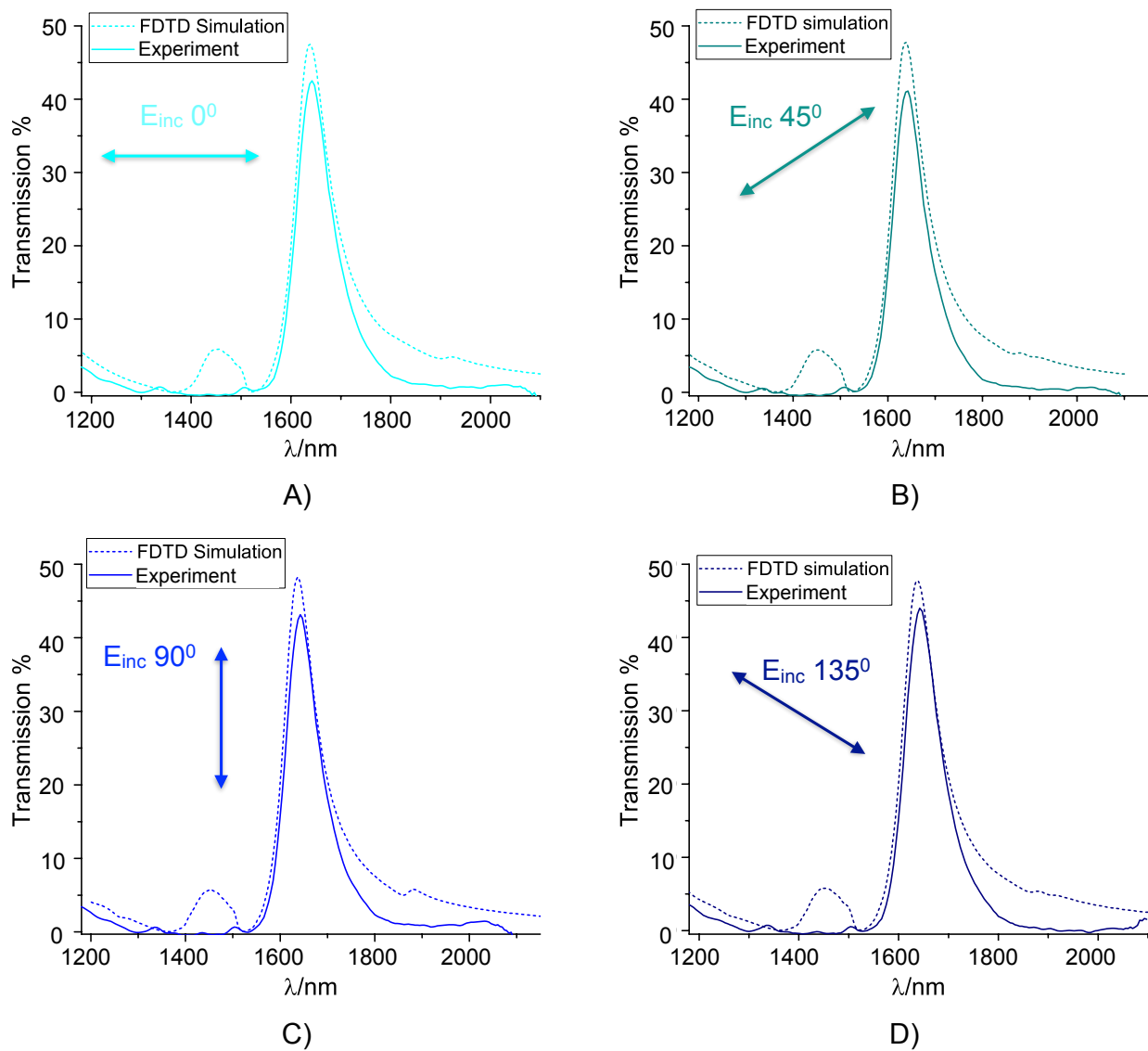


Figure 3: (A), (B), (C) and (D) show the FDTD simulation overlaid with the experimental data for  $\mathbf{E}_{inc}$  polarisation of  $0^\circ$ ,  $45^\circ$ ,  $90^\circ$  and  $135^\circ$  respectively, for the design shown in Figure 1(A)(ii).

Figure 2(D) shows the variation in the transmission coefficient as a function of  $\mathbf{E}_{inc}$ . It can be seen that the range is within 2.5% over a rotation of  $180^\circ$ . Similarly, we find

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3 that the variation in the peak transmission wavelength is so small as to be immeasurable  
4 with our equipment. The suppression of high order modes and high out of band radiation  
5 is also observed for this device design. To demonstrate the robustness and reproducibility  
6 of the designs two more devices were fabricated and characterised (see Figure S2 in the  
7 Supplementary Information). Our data shows a reproducibility of the characteristics we  
8 have described for the two designs.  
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11 As seen from the experimental results, the design with the ellipses oriented at 45° and  
12 135° exhibit insensitivity to  $\mathbf{E}_{inc}$  polarisations while maintaining a high transmission. To  
13 understand this phenomenon we carried detailed FDTD simulations. All simulations were  
14 performed using the commercially available Lumerical FDTD software using the settings and  
15 parameters described in the Methods section. The simulations show excellent agreement  
16 with the experimental results for incident light with polarisations of 0°, 45°, 90° and 135°,  
17 as shown in Figure 3. For comparison with characterisation of simple circular hole and  
18 elliptical hole design, see Supporting Information Figures S3 and S4. From the simulations  
19 and experimental data we observe that the transmission peak is asymmetric - indicative of  
20 a Fano resonance.<sup>47</sup> The Fano resonance has been observed in plasmonic devices<sup>48,49</sup> and  
21 can be induced by symmetry breaking inside the unit cell,<sup>50</sup> interference between dark and  
22 bright modes excited by the incident light<sup>51-53</sup> or interference between dipole and quadrupole  
23 modes in the structure.<sup>54</sup>  
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41 The Fano lineshape from the equation,  $I\alpha \frac{(q(\frac{\gamma}{2})^2 + \omega - \omega_0)^2}{(\omega - \omega_0)^2 + (\frac{\gamma}{2})^2}$ , is fitted to both the FDTD  
42 simulation and the experimental results in Figure 4.  $I$  is the intensity,  $q$  is the Fano factor  
43 that is slightly larger than 1 in our case,  $\omega$  is the angular frequency,  $\omega_0$  is the angular resonant  
44 frequency and  $\gamma$  is the FWHM of the resonant peak. The simulation artefact at 1.44  $\mu\text{m}$  is  
45 attributed the (2,1) reflection mode. The (2,1) reflection mode is confined in the substrate.  
46 The 2D planar sections in the xz-plane in Figure 4 reveal that at  $\lambda_{peak}$ , higher electric field  
47 confinement is observed in elliptical nanoholes than in circular nanoholes.  
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55 Figure 5 illustrates the origin of the Fano resonance, in the sample with the ellipses  
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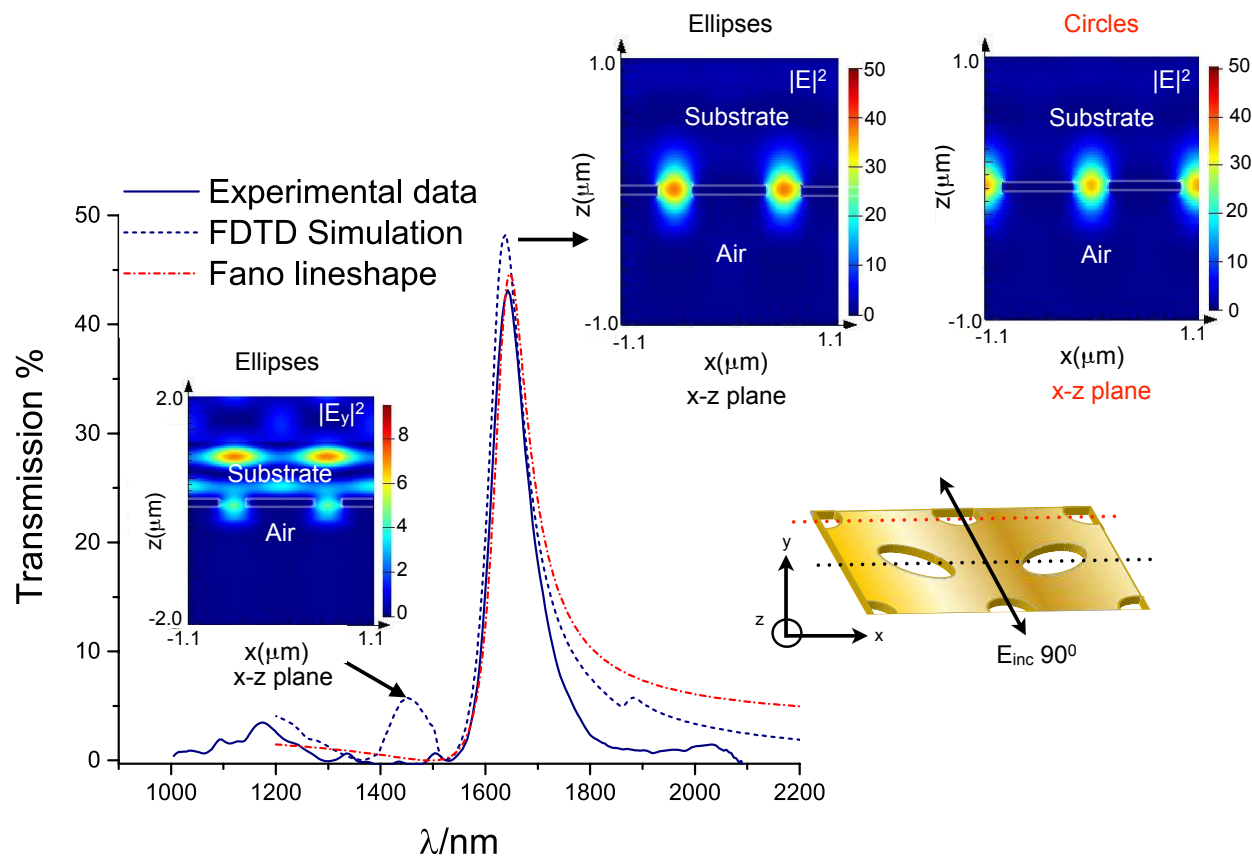


Figure 4: The analytical Fano lineshape compared to the FDTD simulation and the experimental results at  $\mathbf{E}_{inc} = 90^\circ$ . Electric field monitors were placed as indicated in the schematic. At  $\lambda_{peak} = 1.642 \mu\text{m}$ ,  $|E|^2$  is higher in elliptical holes than circular holes. The E-field monitor at  $1.44 \mu\text{m}$  shows a reflection into the substrate.

alternately oriented at  $45^\circ$  and  $135^\circ$ , for each incident polarisation. When the incident light is linearly polarized parallel to the y-axis, one would expect, in a circular aperture, to see the electric field reach a maximum in intensity at opposing sides of the circle, on the y-axis, forming a dipole. However, in both of the alternately angled ellipses, the charge distribution forms a quadrupole (see Figure 5(A)(i)). The field pattern looks to be identical (but a mirror image) in both ellipses. The modal changes in the elliptical holes and circular holes were analysed at resonance and off resonance.<sup>55</sup> Off resonance, at  $\lambda = 1.68 \mu\text{m}$ , the modal distribution in the elliptical holes is a quadrupole that is indicative of a subradiant mode as shown in Figure 5(A)(ii). However, at  $\lambda_{peak}$  the out of plane E-field along the z-axis ( $\mathbf{E}_z$ ) shows a quadrupole for the alternating elliptical holes (subradiant mode) and a dipole for

circular holes (super-radiant mode), as seen in Figures 5(A)(iv) and (v). This indicates that  $\mathbf{E}_{inc}$  cannot excite the dark resonance directly, but only through an interaction involving the dipole resonance that via near-field coupling, excites the sub-radiant mode.<sup>56</sup> When the

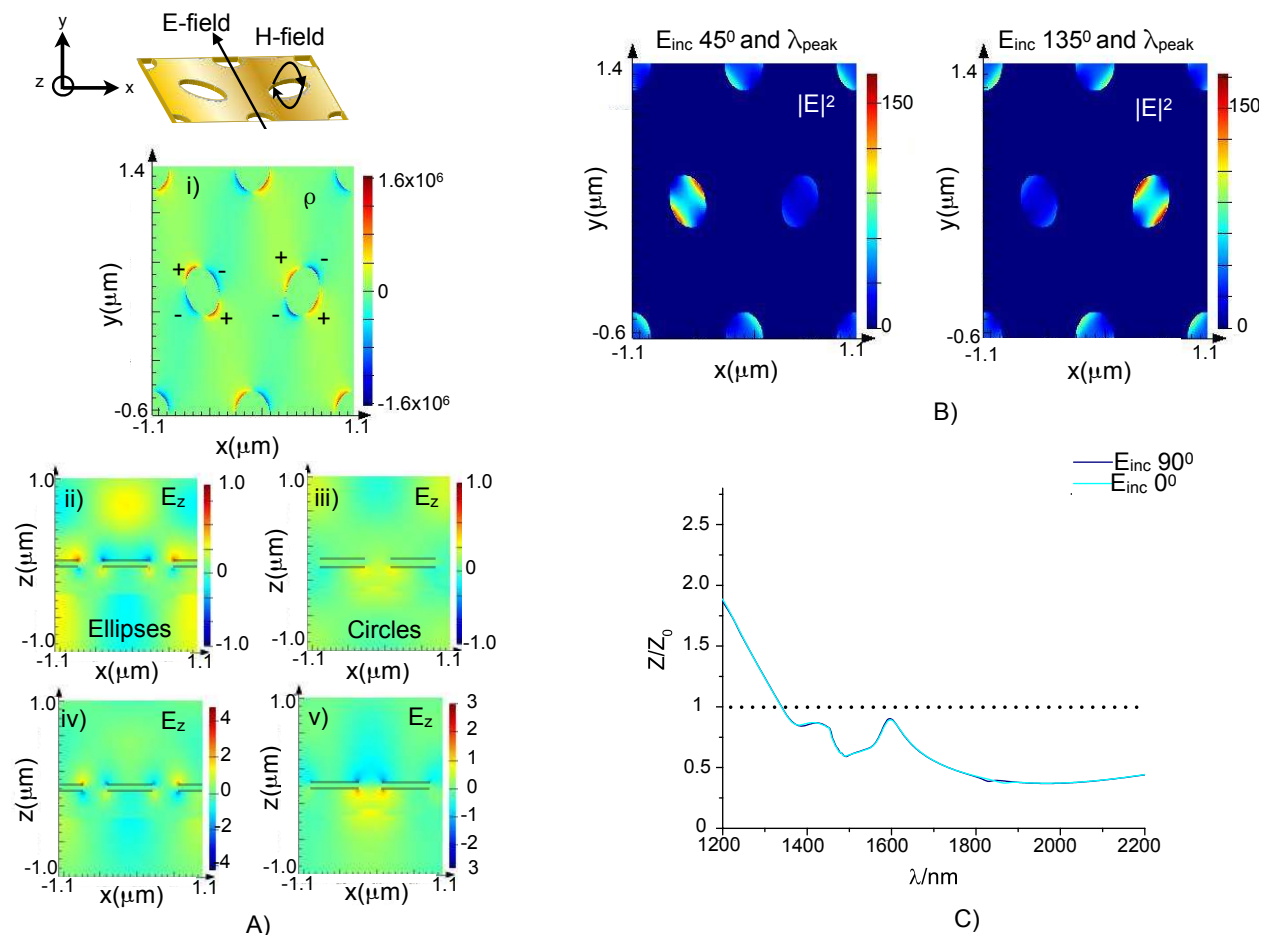


Figure 5: (A) Simulated E-fields for  $\mathbf{E}_{inc}$   $90^\circ$ . (i) At  $\lambda_{peak}$ , the surface charge density distribution shows a quadrupolar for the elliptical holes and a dipolar for the circular holes. (ii) and (iii) Simulated out of plane E-fields:  $\mathbf{E}_z$  field at  $1.68 \mu\text{m}$  (off resonance) that show a clear quadrupole for the elliptical holes only. This is the subradiant mode. However as seen at  $\lambda_{peak}$  in (iv) and (v) the E-field in the ellipses (quadrupole) is the subradiant mode which interacts with the super-radiant mode in the circular holes (dipole), explaining the Fano lineshape. (B) The  $|\mathbf{E}|^2$  intensity for  $\mathbf{E}_{inc}$   $45^\circ$  and  $135^\circ$  show that only one ellipse contributes to the EOT which results in asymmetry in the design that leads to a Fano lineshape. (C) Calculated normalized impedance ( $Z/Z_0$ ) plots at  $\mathbf{E}_{inc}$   $0^\circ$  and  $90^\circ$  that shows at  $\lambda_{peak}$ , the value is nearly 1.

incident light is linearly polarized parallel to the y-axis, i.e.  $\mathbf{E}_{inc}$  at  $0^\circ$  polarisation, the E-fields in the ellipses are opposite to what is discussed for  $\mathbf{E}_{inc}$   $90^\circ$ . For  $\mathbf{E}_{inc}$  at  $45^\circ$  and  $135^\circ$ ,

only one of the ellipses has a modal confinement contributing to the EOT as shown in Figure 5(B). This creates asymmetry in the structure and hence we observe the Fano resonance for these polarisations of incident light. Figures S5 and S6 in the Supplementary Information show the difference in mode confinement in the ellipses for  $\mathbf{E}_{inc}$  at  $45^\circ$  and  $135^\circ$ , respectively. We also calculated the optical impedance of the device from the s-parameters extracted with incident light polarized along the x and y axis. A normalised optical impedance ( $Z/Z_0$ : where  $Z_0$  is the impedance of free space) of unity would indicate high efficiency transmission with no reflection from the metasurface. Due to the asymmetry of the design,  $S_{11}$  and  $S_{21}$  were calculated with the light incident through the substrate and  $S_{22}$  and  $S_{12}$  were calculated with light incident from the opposite direction (through air).<sup>57,58</sup> The optical impedance  $z$  is calculated from Equation 2:

$$z^2 = \frac{T_{12}}{T_{21}} = \frac{(1 + S_{11})(1 + S_{22}) - S_{21}S_{12}}{(1 - S_{11})(1 + S_{22}) - S_{12}S_{21}} \quad (2)$$

This is normalized to  $Z_0$  for  $\mathbf{E}_{inc}$   $0^\circ$  and  $90^\circ$  with the plots shown in Figure 5(C). For both polarisations of incident light we observe that at resonance ( $1.61 \mu\text{m}$  for the S parameter calculation) the value is almost 1.

In conclusion, we have demonstrated a novel plasmonic metasurface design with arrays of elliptical and circular nanoholes in a metallic film to obtain an unprecedented high transmission efficiency of 44% and narrow FWHM of 79 nm. Polarisation insensitivity is observed with a  $\Delta\lambda/\lambda$  of 0 and  $\Delta T$  of 2.5%. The experimental transmission spectra are matched well with FDTD simulations. We have shown that the narrow linewidth is due to an interplay between the Fano resonance and the EOT. The Fano resonance arises due to the symmetry breaking of the design with respect to the  $\mathbf{E}_{inc}$  polarization: being anti-symmetric in the x-axis and symmetric in the y-axis, leading to dark modes interacting with the incident light. At  $\mathbf{E}_{inc}$  of  $0^\circ$  and  $90^\circ$  a negligible mismatch in optical impedance with the free space was observed around  $\lambda_{peak}$  with the normalized impedance value being almost 1. The narrow

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3 linewidth and high out of band rejection is comparable to state-of-the-art dichroic filters  
4 which makes our metasurface filters ideal for integration with appropriate photodetectors.  
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## 8 9 **Methods**

### 10 11 **Fabrication**

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14 The substrate used is a borosilicate glass slide of dimensions 20 mm  $\times$  20 mm and thickness  
15 515  $\mu\text{m}$ . A lift-off process was employed to obtain the elliptical and circular nanohole designs.  
16 A bilayer of polymethyl methacrylate (PMMA) was spin coated onto the substrates and the  
17 designs patterned into the resist using a Vistec VB6 electron beam lithography (EBL) tool.  
18 80 nm of Au is deposited using a Plassys electron beam evaporator and the sample placed  
19 in warm acetone maintained at 50° overnight. After lift-off, the sample was then cleaned  
20 in acetone and isopropyl alcohol. The devices were annealed in a furnace in an atmosphere  
21 of  $N_2$  gas at a temperature of 605° for 3 hours. After annealing, 300 nm of silicon dioxide  
22 was deposited on top of the Au layer using a plasma enhanced chemical vapour deposition  
23 (PECVD) process. The addition of the cap layer enhances the transmission.<sup>30</sup>  
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### 36 **Simulation setup**

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38 The plasmonic filter simulations are set up as follows: a 80 nm gold layer was placed between  
39 a semi-infinite borosilicate layer and a 300 nm silicon dioxide ( $\text{SiO}_2$ ) cap layer. The gold was  
40 patterned with the two different unit cell design (discussed in Figure 1(A)) and the silicon  
41 dioxide cap layer was patterned with "etch" holes to replicate the cap layer topography  
42 after deposition of silicon dioxide. A mesh grid with a maximum cell size of 5 nm was  
43 defined in the vicinity of the holes. For  $\mathbf{E}_{inc}$  of 0° and 90°, anti-symmetric and symmetric  
44 boundary conditions were used, respectively, to form the unit cells highlighted in Figure  
45 1(A), and perfectly matched layers (PML) were used in the  $z$  boundaries. For  $\mathbf{E}_{inc}$  of  
46 45° and 135° polarisation, periodic boundary conditions were used in the x and y axes.  
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48 The gold parameters were selected using a plasma resonance ( $\omega_p$ ) of  $1.37 \times 10^{16}$  rad/s and  
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3 collision frequency ( $\omega_c$ ) of  $1.224 \times 10^{16}$  rad/s with the refractive index ( $\eta$ ) of borosilicate  
4 glass substrate as 1.52 and SiO<sub>2</sub> cap of 1.49 (extrapolated from spectroscopic ellipsometry  
5 analysis). Steep angle boundary conditions were used in the FDTD simulation to absorb  
6 all the light at the boundaries and prevent any spurious reflections. The gold surface was  
7 illuminated by a 1.2  $\mu\text{m}$  to 2.1  $\mu\text{m}$  plane-wave source from within the substrate and the  
8 transmission spectra were recorded by a monitor placed on the opposite side of the metal  
9 film.  
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## 19 Acknowledgement

20  
21 The authors thank the James Watt Nanofabrication Centre (JWNC) staff for their expertise  
22 and assistance in fabrication processes. This work was supported by the Engineering and  
23 Physical Sciences Research Council of the United Kingdom, Grant Nos. EP/M01326X/1  
24 and EP/J018678/1.  
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## 31 Supporting Information Available

32  
33 A file called Supplementary Information is included. This file contains simulation results of  
34 the variation of metal thickness on the proposed design for  $\mathbf{E}_{inc}$  at 0° and 90°. A comparison  
35 between the proposed design and simple circular holes and elliptical holes only design is  
36 shown. The simulations supporting the origin of Fano resonance when  $\mathbf{E}_{inc}$  is 45° and 135°  
37 is explicitly shown.  
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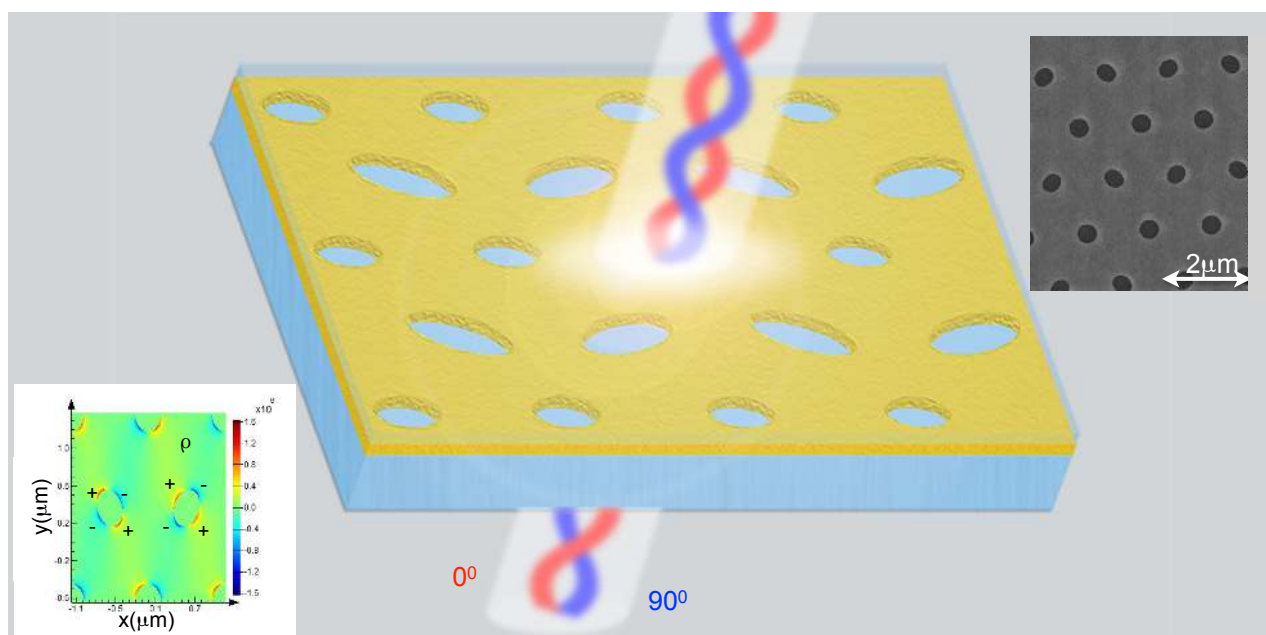
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3 **ToC: Ultra-narrow linewidth polarization-insensitive filter using a**  
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8 Yash D. Shah,\* James Grant, Danni Hao, Mitchell

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