



Del Din S, Godfrey A, Rochester L. <u>Validation of an accelerometer to quantify a comprehensive battery of gait characteristics in healthy older adults and Parkinson's disease: toward clinical and at home use</u>. *IEEE Journal of Biomedical and Health Informatics* 2015, (99).

Copyright:

© 2015 IEEE. Translations and content mining are permitted for academic research only. Personal use is also permitted, but republication/redistribution requires IEEE permission.

DOI link to article:

http://dx.doi.org/10.1109/JBHI.2015.2419317

Date deposited:

02/06/2015

Validation of an accelerometer to quantify a comprehensive battery of gait characteristics in healthy older adults and Parkinson's disease: toward clinical and at home use.

Silvia Del Din-IEEE Member, Alan Godfrey-IEEE Member and Lynn Rochester

Abstract-Measurement of gait is becoming important as a tool to identify disease and disease progression, yet to date its application is limited largely to specialist centres. Wearable devices enables gait to be measured in naturalistic environments however questions remain regarding validity. Previous research suggests that when compared with a laboratory reference, measurement accuracy is acceptable for mean but not variability or asymmetry gait characteristics. Some fundamental reasons for this have been presented (e.g. synchronisation, different sampling frequencies) but to date this has not been systematically examined. The aims of this study were to: (i) quantify a comprehensive range of gait characteristics measured using a single tri-axial accelerometerbased monitor, (ii) examine outcomes and monitor performance in measuring gait in older adults and those with Parkinson's disease (PD) and (iii) carry out a detailed comparison with those derived from an instrumented walkway to account for any discrepancies. Fourteen gait characteristics were quantified in 30 people with incident PD and 30 healthy age-matched controls. Of the 14 gait characteristics compared, agreement between instruments was excellent for 4 (ICCs 0.913 - 0.983); moderate for 4 (ICCs 0.508 - 0.766); and poor for 6 characteristics (ICCs -0.637 - 0.370). Further analysis revealed that differences reflect an increased sensitivity of accelerometry to detect motion, rather than measurement error. This is most likely because accelerometry measures gait as a continuous activity rather than discrete footfall events, per instrumented tools. The increased sensitivity shown for these characteristics will be of particular interest to researchers keen to interpret 'real world' gait data. In conclusion, use of a body worn monitor is recommended for the measurement of gait but is likely to yield more sensitive data for asymmetry and variability features.

Index Terms — Accelerometer, algorithm, body worn monitor, Instrumented gait, instrumented walkway.

I. INTRODUCTION

Gait is emerging as a powerful tool in neurodegenerative disease to identify surrogate markers of incipient disease manifestation or disease progression [1-5].

However, its widespread adoption for clinical and research purposes has been limited to date. This is largely

The research was supported by funding from the National Institute for Health Research (NIHR), Newcastle Biomedical Research Unit based at Newcastle Hospitals NHS Foundation Trust and Newcastle University and GlaxoSmithKline (GSK). The views expressed are those of the authors and not necessarily those of the NHS, the NIHR or the Department of Health.

S. Del Din, A. Godfrey and L. Rochester are with the Institute of Neuroscience, Newcastle University, Clinical Ageing Research Unit, Campus for Ageing and Vitality, Newcastle upon Tyne, NE4 5PL, UK (Corresponding author: L. Rochester phone: +441912081291, fax: +441912081251, e-mail: lynn.rochester@ncl.ac.uk).

because the majority of studies have been carried out using specialised gait analysis equipment (most commonly instrumented walkways such as pressure-sensor activated, e.g. GaitRite) [6-9] which limits work to specialised centres and a sparse number of gait cycles [10]. In order to develop the use of quantitative gait analysis for clinical screening and research, low-cost tools are required that facilitate measurement in the clinic and home. This has driven an interest in the use of accelerometer-based body worn monitors (BWM) for measuring gait.

BWM can provide a continuous sampling of whole body movement in controlled or habitual environments [11]. A BWM worn on the lower back implementing single/numerous algorithm(s) can provide a simple method to quantify gait; the adoption of the inverted pendulum model to evaluate step length and the use of appropriate filtering procedures to identify initial/final contact events within the gait cycle [12-14]. However, it is essential to validate the combination of BMW and implemented algorithms to accurately capture gait outcomes before widespread adoption. Evidence suggests suitable validity and reliability of estimated mean values of gait outcomes to a trusted laboratory reference (GaitRite) [12, 13, 15-19]. Yet moderate to poor agreement has been reported for step-to-step fluctuations (variability) and bilateral coordination (asymmetry) [12, 14, 15, 17, 20-22]. This leaves the role of BWM to comprehensively quantify gait in ageing and pathology unclear.

A comprehensive examination of systems is lacking within the literature, which is critical to further understand and explain the poor agreement for asymmetry and variability gait characteristics. Previous studies have tried to provide a rationale for the poor agreement such as: difference in rates; misalignment sampling due device orientation/placement; and poor synchronization [12, 13, 15, 23]. However, questions still remain. Furthermore, weaknesses of previous studies [12-15, 21] include: (i) limited and inconsistent reporting of gait characteristics [12-15]; (ii) introduction of newly derived variables [23-25] which are difficult to interpret making mainstream use problematic; (iii) restricted testing on a single (small) cohort (ranging on average from 10 to 23 participants [12, 13, 15, 20, 23]), often with a lack of consideration for the effects of pathology on BWM performance; and (iv) lack of BWM signal examination compared to video recordings. Evaluation of a comprehensive set of gait characteristics is therefore needed while undertaking a systematic examination of all data acquired during a validation-based study of a BWM.

The purpose of this study was therefore to take a systematic approach to address gaps in the literature. Firstly we aimed to characterise a broad range of gait characteristics using a low cost BWM in a large cohort of participants. Whilst multiple

characteristics can describe gait, studies have helped to provide a simplified framework for selection of important gait characteristics [5, 26, 27]. In this study characteristics were selected based on our previous work [27, 28] which identified a comprehensive range of 16 core gait characteristics (using GaitRite) recognised as indicative of healthy ageing and pathology (Parkinson's disease, PD). Here, we used a BWM and adopted a novel combination of two algorithms to quantify gait grouped by the properties they measure such as summary mean values, variability and asymmetry and including phases of the gait cycle. Secondly, we wanted to compare results in PD and older adults to see if the performance of the BWM remained stable in pathology. The adoption of two cohorts is a key feature of this work, providing contrasting features of gait, where asymmetric and variability characteristics are known to differ. Finally, we compared the findings from the BWM to a common laboratory reference for comparability with previous work and where possible carried out a detailed evaluation where differences were found between systems in order to characterise the source of error. In adopting this process we wished to determine the ability of a low cost BWM to accurately measure a comprehensive set of core gait characteristics in normal and pathological conditions for confidence in more widespread adoption. This forms part of our ongoing work to quantify gait simply and effectively within laboratory-based instrumented testing sessions, with a view to quantifying gait in real world environments.

II. METHODS

A. Participants

Thirty PD patients within 4 months of diagnosis and 30 healthy aged matched control subjects (HC) were recruited from the Incidence of Cognitive Impairment in Cohorts with Longitudinal Evaluation—GAIT (ICICLE-GAIT) study. This is a collaborative study with ICICLE-PD, an incident cohort study (Incidence of Cognitive Impairment in Cohorts with Longitudinal Evaluation—Parkinson's disease) conducted between June 2009 and December 2011 [29]. This study was conducted according to the declaration of Helsinki and had ethical approval from the Newcastle and North Tyneside research ethics committee. All participants signed an informed consent form prior to testing.

B. Demographic and Clinical Measures

Age, gender and body mass index (BMI) were recorded for each participant. Cognition was assessed with the Montreal Cognitive Assessment (MoCA) [30]. Balance confidence was measured using the self-rated Activities Balance Self Confidence Scale [31]. The severity of PD motor symptoms in the PD participants was measured using the Hoehn and Yahr scale [32], which ranges from 0 (no symptoms) to 5 (wheelchair bound or bedridden if unaided), and section III of the modified Movement Disorder Society version of the Unified Parkinson's Disease Rating Scale (MDS-UPDRS [33]), which ranges from 0 (no motor symptoms) to 132 (severe motor symptoms). The Postural Instability and Gait Disorder (PIGD) and Tremor phenotype subscales were also calculated from the MDS-UPDRS [34]. Levodopa equivalent daily doses were calculated according to established methods [35].

C. Equipment

Each participant was asked to wear a low cost (\leq £100) triaxial accelerometer-based device (Axivity AX3, dimensions: $23.0 \times 32.5 \times 7.6$ mm, weight: 9g) located on the fifth lumbar vertebrae (L5), Figure 1. It is a generic movement monitor that is non-specific for gait or ambulatory assessment and was held in place by double sided tape (Wig Tape, Natural Image, UK) and Hypafix (BSN Medical Limited, Hull, UK). The device measures vertical (a_v), anteroposterior (a_a) and mediolateral (a_m) accelerations and was programmed to capture data at 50Hz and 100Hz (16-bit resolution) and at a range of \pm 8g. The change in sampling frequency was due to upgrading of the device during the longitudinal ICICLE-PD Gait study where updated versions had increased memory and sampling capabilities. However, for consistency of analysis all data were down-sampled, where necessary, to 50 Hz

Gait assessment was conducted concurrently as part of the ICICLE-GAIT study using a 7.0m long \times 0.6m wide instrumented walkway (Platinum model GaitRite, software version 4.5, CIR systems, NJ, USA) which was synchronised with a video camera (Logitech, Webcam Pro 9000, CA, USA) recording at 25 Hz. The instrumented walkway had a spatial accuracy of 1.27cm and temporal accuracy of 1 sample (240Hz, \sim 4.17ms).

The quartz stabilised real time clock of the accelerometer (accuracy: 20 parts per million) was synchronised with the computer used for the walkway recordings and for each walking trial the start and stop time were recorded by the assessor. Start and stop times were subsequently input to a bespoke MATLAB® program that automatically segmented and analysed the accelerometer data. Digital synchronization to identify exact steps (left/right steps) between systems was not used due to the short distance traversed and lack of gyroscope within the BWM. However, the variability and asymmetry equations adopted in this study accounted for all steps to be used interchangeably (Section D. Laboratory reference: Instrumented walkway).

C. Protocol and Data Collection

Participants were asked to walk at their preferred speed, performing four intermittent straight line walking trials over 10.0m. The 7.0m instrumented walkway was placed in the centre of the 10.0m (Figure 1) to ensure gait was captured at a steady speed. In addition synchronised video of frontal plane motion was recorded during each walk. PD participants who were on medication were tested approximately 1 hour after medication intake.

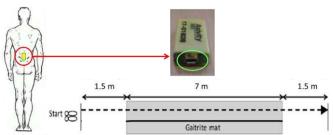


Figure 1. The tri-axial accelerometer-based device and site of attachment on the lower back (L5) and laboratory set up for testing intermittent walks.

D. Data Analysis

BWM (accelerometer) data processing

The BWM data were downloaded to a computer, segmented into the 4 different straight line passes using time stamps and analysed by the MATLAB® program. Accelerometer signals were transformed to a horizontal-vertical coordinate system [36], and filtered with a 4th order Butterworth filter at 20 Hz [12, 14] using the MATLAB functions: *detrend*, *butter*, and *filtfilt*. For the purposes of this study the program utilised the novel application of a combination of gait algorithms that have been previously developed for a single sensor attached to L5 on a cohort of healthy older adults:

Gait algorithm #1

The first algorithm estimated the initial contact (IC) and final contact (FC) events within the gait cycle (Figure 2), and is described in detail elsewhere [12]. In brief the algorithm consisted of the following:

• The IC and FC events are estimated from a continuous wavelet transform (CWT, using the *cwt* MATLAB® function) of *a_ν* which was first integrated (*cumtrapz*) and then differentiated using a Gaussian CWT: the IC events were detected as the local minima of the CWT (*findpeaks*), Figure 3a. A further differentiation resulted in the local maxima being defined as the FC events (Figure 3a, Figure 4).

Previously, the algorithm has been used to estimate step and stride times only [12]. However, in order to fully replicate the core characteristics of gait we needed to derive stance and swing time. This was achieved through the sequence of IC and FC events in relation to the double support phase of the gait cycle, Figure 2. From the sequence (i) of IC and FC events both left and right (opposite) events were identified where stride and subsequently stance and swing time were estimated, Equations (1, 2 & 3). For direct comparison to the steps quantified by the instrumented walkway, the initial and final 4 steps (walk to/from the walkway) of the accelerometer data (as determined by the IC/FC algorithm) were excluded from analysis.

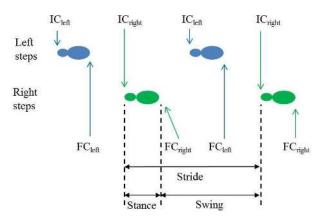


Figure 2. Identification of stride, stance and swing times from the double support phase of the IC and FC algorithm

Stance time =
$$FC(i + 1) - IC(i)$$
 (1)

Stride time =
$$IC(i + 2) - IC(i)$$
 (2)

Swing time = Stride time
$$-$$
 Stance time (3)

Gait algorithm #1: optimisation

Upon initial inspection of the signal traces, spurious IC events (i.e. non-IC events, Figure 4a) were detected in 37% and 58% of the HC and PD groups, respectively. As a result, the algorithm to detect IC and FC events was refined to include a previous methodology for improved step detection: the updated algorithm only included IC peaks within a predetermined timed interval similar to Najafi et al. [17]. The optimisation procedure required IC events to be identified during a predefined interval (0.25-2.25s) from a previous IC event. Figure 4b shows an example of the updated algorithm with the correct estimation of IC and FC events.

Gait algorithm #2

The second gait algorithm estimated step length using the inverted pendulum model described by Zijlstra et al. [14] (Equation 4, Figure 3b) where h represents the change in height (vertical position) of the centre of mass (CoM) derived using double integration (*cumtrapz*) of a_v ,, and l the pendulum length (sensor height from ground).

Step Length =
$$2\sqrt{2lh - h^2}$$
 (4)

Gait algorithm #2: optimisation

We evaluated step length using 2 methods: (i) l estimated using leg length × correction factor [14] and (ii) l estimated from the height of the BWM located at L5, i.e. the ratio of the participants' height (l = height × 0.53) [37]. Preliminary analysis revealed better agreement between systems for the second method compared with using the correction factor and as a result was adopted in this study.

Gait algorithm #3

To estimate a value for step velocity we utilised algorithm #1 and #2 and the simple ratio between distance (length) and time, Equation 5.

Step Velocity = Step Length/Step Time
$$(5)$$

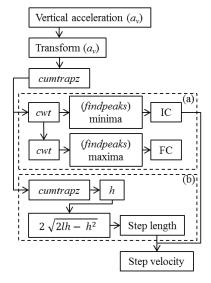


Figure 3. Flowchart of MATLAB® analysis: algorithm #1 (a), algorithm #2 (b) and algorithm #3 (step velocity).

We replicated 14/16 [27] clinically relevant gait characteristics (step width and step width variability could not be measured due to the adoption of a single tri-axial accelerometer). The mean, variability and asymmetry values of the gait characteristics were then calculated for direct comparison to gait characteristics determined by the instrumented walkway (see following section for details). Right and left IC's were previously identified by the sign of the filtered vertical angular velocity at the instant of IC with the use of a gyroscope [12]. In this study right and left IC's in the accelerometer signal were automatically selected from the MATLAB® program consistently assigning right steps to the first detected step and alternating with left step assignment.

Laboratory reference: Instrumented walkway

Data for individual steps for each walk were extracted from the instrumented walkway database using Microsoft Access 2007 (Microsoft Corp., Redmond, WA, USA). Mean gait values were calculated for step time, stance time (duration the stance foot was in contact with the ground for a given stride), swing time (duration a foot was not in contact with the ground for a given stride), step length and step velocity. To calculate step variability, the standard deviation (SD) from all steps (left and right combined) was calculated, Equation 6. SD was selected as a measure of variability due to its robustness and dual use with both the BWM and walkway. Other measures of variability (harmonic ratio, coefficient of variation) have been suggested but have shown low to moderate agreement between systems [23, 24, 38, 39] and are not all quantifiable by an instrumented walkway.

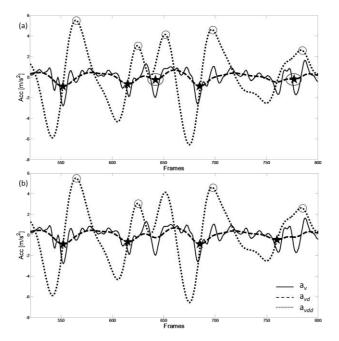


Figure 4. An example of ICs (squares) and FCs (circles) detection during a single pass on the walkway. The black solid line represents a_v , the dashed line the differentiated with Gaussian CWT of $a_v(a_{vd})$, and the dotted line the differentiated with Gaussian CWT of $a_{vd}(a_{vdd})$. Panel (a) shows the IC/FC algorithm with spuriously detected IC events (circled squares). Panel (b) shows the correct detection of the ICs and FCs with the optimised technique.

We considered each walking pass separately and as a result, right and left steps were interchangeable. This method has no impact on evaluation of variability values which were described as the SD of all steps within walking trials, Equation 6. Asymmetry was determined as the absolute difference between left and right steps (alternating) for each walking pass, averaged across all passes, Equation 7. As asymmetry represents the absolute mean difference between right and left steps, it does not depend on the detection of the "true" right and left steps.

$$Variability = SD (Steps)$$
 (6)

$$Asymmetry = |Average_{Left} - Average_{Right}|$$
 (7)

E. Statistical Analysis

Statistical analysis was carried out using SPSS v19 (IBM). Descriptive statistics (means and standard deviations (SD)) were calculated for all gait characteristics, in PD and HC pooled across the 4 passes. Normality of data was tested with a Shapiro-Wilk test. Bland-Altman plots were used to visually check for non-linear or heteroscedastic distributions of error between the two systems (instrumented walkway v. BWM) as a function of the participants' mean gait performance.

Absolute agreement between the two systems was formally tested using Intraclass Correlation Coefficients (ICC_{2,1}) and limits of agreement (LoA) expressed both as absolute values and as a percentage of the mean. Relative agreement between the two systems was also established using Pearson's correlations (r). Independent t-tests were used to examine the difference between groups for demographical data and systems' outcomes (p) value <0.05 was considered as significant).

III. RESULTS

Demographic data

Participant demographic, clinical and cognitive descriptors are shown in Table I. Compared to HC, PD participants were aged matched; included proportionally less women (CL: 50%, PD: 33%); presented with lower confidence in their balance (ABCs), and poorer cognition (MoCA). No differences were found between HC and PD participants for both height and BMI. Participants with PD were in the early stages of the disease with mild motor symptoms.

BWM and Instrumented walkway: agreement

Table II shows the agreement between the two systems for ICC, r values and LoA (%). There was excellent agreement between the systems for all the mean gait variables (step velocity, step time, stance time and step length) except for swing time. In contrast asymmetry of steps (bilateral co-ordination) and variability (step to step fluctuations) showed poor agreement.

Table III shows the results obtained from the derived gait parameters for both the BWM and instrumented walkway. Results show that the BWM had systematic longer/greater gait characteristics and this is significant for 10 of the 14 and 9 of the 14 variables for HC and PD, respectively.

TABLE I. CLINICAL AND DEMOGRAPHIC CHARACTERISTICS

Characteristic	HC (n = 30) Mean ± SD	PD $(n = 30)$ Mean \pm SD	p
M/F (n)	15/15	20/10	0.197
Age (years)	66.6 ± 7.7	66.9 ± 9.4	0.891
Height (m)	1.7 ± 0.1	1.7 ± 0.1	0.795
BMI (Kg/m ²)	28.0 ± 4.6	28.7 ± 5.4	0.585
MoCA (0-30)	27.9 ± 1.7	24.7 ± 3.1	<0.001
ABCs (0-100%)	91.3 ± 12.7	81.7 ± 20.0	0.031
Hoehn & Yahr (n)	-	HY I - 8 HY II - 20 HY III - 2	-
Levodopa Equivalent Daily Dose (mg/day)	-	163.3 ± 137.2 HY I - 137 ± 112.9 HY II - 177 ± 153.1 HY III - 130 ± 14.1	-
MDS-UPDRS III	-	29.5 ± 10.7 HY I - 17.5 ± 5.7 HY II - 32.9 ± 8.2 HY III - 43.5 ± 3.5	-
Motor Phenotype (n)	-	PIGD 10 ID 4 TD 16	-

BMI: Body Mass Index; MoCA: Montreal Cognitive Assessment; ABC: Activities specific balance confidence scale; UPDRS: Unified Parkinson's Disease Rating Scale; PIGD: Postural instability and gait disorder phenotype; ID: indeterminate phenotype; TD: Tremor dominant phenotype. *p* difference between HC and people with PD.

TABLE II. AGREEMENT BETWEEN INSTRUMENTED WALKWAY AND BWM

LoA expressed as a percentage (%) of the mean; Step vel.: Step velocity.

Variable		HC			PD			
variable	ICC _{2,1}	r	LoA	ICC ₂	, ₁ r	LoA		
Mean gait characteristics								
Step time (s)	0.983	0.998	1.2	0.981	0.997	1.4		
Stance time (s)	0.927	0.912	9.5	0.913	0.854	1.4		
Swing time (s)	0.766	0.708	18.0	0.511	0.618	19.5		
Step length (m)	0.913	0.867	13.9	0.869	0.850	15.6		
Step vel. (m/s)	0.952	0.906	14.7	0.928	0.890	16.7		
Variability (var) gait characteristics								
Step time var (s)	0.508	0.429	100.9	0.627	0.633	132.6		
Stance time var (s)	0.645	0.747	159.9	0.529	0.576	164.2		
Swing time var (s)	0.307	0.302	206.7	0.366	0.512	171.1		
Step length var (m)	0.060	0.102	126.3	0.216	0.254	83.3		
Step vel. var (m/s)	-0.143	-0.086	110.2	0.225	0.229	107.5		
Asymmetry (asy) gait characteristics								
Step time asy (s)	-0.637	-0.349	268.2	0.811	0.757	130.2		
Stance time asy (s)	0.370	0.249	177.2	0.318	0.473	362.3		
Swing time asy (s)	-0.229	-0.111	316.1	0.448	0.304	259.7		
Step length asy (m)	0.132	0.078	243.5	-0.223	-0.120	225.4		

BWM and Instrumented walkway: examination #1

To explore differences between systems for variability and asymmetry an analysis was conducted to check the potential impact of the quality of the measured filtered acceleration a_{ν} on the differences observed. For exploratory purposes we decided to examine step time variability obtained by both systems.

A range of features based on the filtered a_v were calculated and averaged across the 4 passes: mean, standard deviation, root mean square values (RMS), number of peaks (maxima of a_v) and valleys (minima of a_v), number of zero crossing (ZC), and frequency below which is the 95% of the signal power spectrum (f95%). Pearson's correlations explored the association between each of these features and the differences in step time variability of the two systems. None of the extracted features showed a strong positive correlation in either group (r < 0.353, Table IV), demonstrating that the poor agreement for the variability results could not be explained by the nature of the acceleration signal.

BWM and Instrumented walkway: examination #2

As no correlations were found between a_{ν} and the mean differences between the systems, further analyses of the filtered a_{ν} signal, estimated step times and instrumented walkway data were carried out to explore the source of discrepancy for asymmetry and variability.

In first instance we explored the impact of the height of the participants on the evaluation of the gait characteristics. Pearson's correlations revealed that only the HC stance time asymmetry (r = 0.435, p = 0.016) and the PD swing time variability (r = -0.362, p = 0.049) showed a poor correlation with height. Subsequently our analysis uncovered two key findings:

 Inspection of the filtered signal confirmed that the BWM identified each step, but with a greater range of step time values (Figure 5 and Figure 6). This accounted for higher variability and low agreement; moreover variability is evaluated considering all the steps (left and right combined).

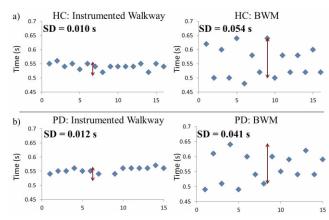


Figure 5. Step time and steptime variability (SD) evaluated with the instrumented walkway and the BWM for HC and PD participant. The BWM show higher step time variability for both (a) HC and (b) PD.

Table III. Mean ± SD values and mean differences of 14 Gait parameters evaluated with an Instrumented Walkway and BWM

	НС				PD			
Characteristic	Instrumented walkway	BWM	Mean Difference, %	p	Instrumented walkway	BWM	Mean Difference, %	P
Mean gait characteristics								
Step time (s)	0.554 ± 0.051	0.567 ± 0.054	0.013, 2.4%	<0.001	0.543 ± 0.045	0.555 ± 0.047	0.012, 2.2%	<0.001
Stance time (s)	0.715 ± 0.080	0.731 ± 0.062	0.016, 2.2%	0.018	0.706 ± 0.072	0.717 ± 0.063	0.011, 1.6%	0.119
Swing time (s)	0.393 ± 0.031	0.404 ± 0.051	0.011, 2.7%	0.116	0.380 ± 0.029	0.394 ± 0.044	0.014, 3.7%	0.052
Step length (m)	0.692 ± 0.094	0.718 ± 0.099	0.026, 3.7%	0.009	0.638 ± 0.100	0.681 ± 0.089	0.043, 6.7%	<0.001
Step vel. (m/s)	1.266 ± 0.219	1.275 ± 0.220	0.009, 0.7%	0.606	1.187 ± 0.223	1.242 ± 0.218	0.055, 4.6%	0.007
Variability (var) gait characteristics								
Step time var (s)	0.017 ± 0.008	0.024 ± 0.011	0.007, 32.8%	0.002	0.022 ± 0.012	0.031 ± 0.023	0.009, 41.8%	0.009
Stance time var (s)	0.022 ± 0.012	0.026 ± 0.015	0.005, 21.8%	0.039	0.023 ± 0.010	0.033 ± 0.022	0.011, 46.3%	0.003
Swing time var (s)	0.016 ± 0.009	0.027 ± 0.024	0.011, 66.3%	0.015	0.019 ± 0.007	0.031 ± 0.025	0.013, 65.9%	0.004
Step length var (m)	0.023 ± 0.007	0.043 ± 0.021	0.021, 92.6%	<0.001	0.025 ± 0.008	0.040 ± 0.015	0.015, 57.6%	<0.001
Step vel. var (m/s)	0.058 ± 0.017	0.043 ± 0.021	-0.015. 25.4%	0.008	0.062 ± 0.023	0.040 ± 0.015	-0.022, 35.8%	<0.001
Asymmetry (asy) gait characteristics								
Step time asy (s)	0.010 ± 0.006	0.015 ± 0.014	0.005, 38.2%	0.151	0.023 ± 0.027	0.023 ± 0.044	-0.0001, 0.3%	0.990
Stance time asy (s)	0.020 ± 0.012	0.014 ± 0.013	-0.006, 30.9%	0.035	0.022 ± 0.009	0.023 ± 0.045	0.001, 6.9%	0.846
Swing time asy (s)	0.010 ± 0.010	0.013 ± 0.015	0.003, 29.7%	0.387	0.018 ± 0.016	0.019 ± 0.024	0.001, 4.8%	0.848
Step length asy (m)	0.022 ± 0.016	0.014 ± 0.017	-0.008, 37.8%	0.049	0.024 ± 0.017	0.014 ± 0.015	-0.010, 4.6%	0.023

Mean difference: BWM - Instrumented walkway; Step vel.: Step velocity.

ii) Where gait was clearly asymmetrical (e.g. PD), asymmetry results were comparable (Figure 6a), while more subtle asymmetric gait patterns (e.g. HC) were detected by the BWM but not instrumented walkway (Figure 6b). This may explain the higher agreement for PD participants' asymmetry results compared to HC (step time asymmetry, Table II and Table III: people with PD often show a clear asymmetric gait pattern, whilst asymmetry is not as pronounced a feature in HC. This was confirmed in individual patient videos which were used as a reference to identify subtle features of gait identified by expert physiotherapists and biomechanists.

Table IV: Results between a_{ν} features and differences between Instrumented Walkway and BWM step varibility

Features	НС		PD	
	Mean ± SD	r	Mean ± SD	r
Mean a_v	-0.990 ± 0.067	0.094	-1.001 ± 0.037	< 0.001
$SD a_{\nu}$	0.127 ± 0.050	0.353	0.166 ± 0.058	< 0.001
RMS a_v	1.006 ± 0.067	0.003	1.026 ± 0.040	0.015
# of peaks	128 ± 42	0.095	162 ± 61	0.048
# of valleys	108 ± 29	< 0.001	132 ± 39	0.077
ZC	131 ± 37	0.009	167 ± 57	0.042
f95%	10.660 ± 2.372	0.108	11.518 ± 2.269	0.003

RMS: Root Mean Square values; SD: Standard Deviations; #: number; ZC: Zero crossing; f95%: frequency below which is the 95% of the signal power spectrum

IV. DISCUSSION

This study replicated 14 core characteristics of gait from a generic tri-axial accelerometer-based movement monitor using a novel combination of gait algorithms (BWM) to segment the gait cycle into discrete events. It is the largest and most comprehensive evaluation to date which incorporates comparison of pathological and non-pathological cohorts.

We compared the BWM results to a known laboratory reference (instrumented walkway, GaitRite) and were able to explain the systematic differences between systems unresolved by previous research.

Mean characteristics and effect of pathology

Excellent (ICCs > 0.900, LoA < 15.0%) agreement was found for mean step time, stance time, step length, and step velocity for HC (ICCs_{2,1} \geq 0.913) and for step time, stance time, and step velocity for PD (ICCs \geq 0.913), similar to other studies [12, 15]. Good agreement (ICCs 0.751 – 0.899, LoA > 15.0%) was found for swing time for HC (ICC_{2,1} = 0.766) and step length for PD (ICCs_{2,1} = 0.869) similar to previous findings [15]. In contrast we only found moderate agreement (ICCs 0.500 – 0.750) for swing time for PD (ICCs = 0.511).

The poorer agreement for mean swing time could be related to the limitation of the FC/IC algorithm where swing time was not accounted for in its design. Though the

algorithm [12] evaluated IC and FC events, the authors presented step and stride time values, which is based on IC estimation only. However, the detection of FCs allowed us to derive stance and swing time with contrasting results for both. Moreover, error is inherently assumed as swing time was computed in our study from the difference between stride and stance time, where small inaccuracies may also exist. Swing time estimation may be improved from direct IC and FC analysis rather than the method adopted here based on the relationship between stance, swing and stride time within the gait cycle.

Good agreement was found for step length within the PD group while the HC had excellent agreement (ICC_{2.1} = 0.913), similar to another study [15]. LoA for HC and PD were < 16.0% and mean percentage difference 3.7% for HC and 6.7% for PD which equates to longer estimated distances of 0.026m and 0.043m, respectively, which we consider acceptable [15]. Traditionally, high reproducibility has been problematic with step length due to adoption of the inverted pendulum model on which it is based [14, 40, 41]. The model assumes a compass gait cycle (circular trajectory) [14], which is not the case in an asymmetric disease (PD). Moreover, the model also assumes straight line walking at a constant pace which makes it problematic when testing within pathology or during laboratory-based protocols where continuous walking for better gait variability estimation is the recommendation [42]. Thus, there is a need to better refine step length estimation where the calculation of vertical displacement (h), pendulum length (l) or the adoption of a generic correction factor are sources of error.

Algorithms independent of site specific variables (h, l) and correction factors will allow for more robust quantification of step length. To date individualised correction factors have been recommended for improved step length estimation rather than generic or group specific values [18, 20]. However, these would be time consuming and difficult to implement in day-to-day clinical practice or in large scale clinical/intervention-based studies where instrumentation of gait is often time constraint [43]. We were unable to estimates for the remaining calculate core characteristics, i.e. step width and step width variability due to the limitations of the BWM and adoption of a single triaxial accelerometer. Moreover, step width estimation is yet to be determined from a single accelerometer-based BWM due to the bipedal dynamics of human locomotion and relative mediolateral placement of feet.

Variability and asymmetry characteristics and effect of pathology

We found poor to moderate agreement between systems for all variability and asymmetry characteristics, similar to previous studies [23, 24, 38, 39, 44]. Therefore we conducted an analysis to explore the lack of agreement to offer new insight into gait quantification with these systems. We hypothesised that corrupt features of the filtered acceleration signal would impact on the error between systems. However, there were no significant correlations in any of the extracted features, verifying that the standard filtering procedure (4th order Butterworth, cut off 20Hz) and resulting signal were

robust. Further exploration of the all the filtered acceleration signals together with all participant videos highlighted subtle asymmetries in gait that were only evident in the BWM signal and not instrumented walkway. A number of possible explanations account for these differences:

- i) We found that height of the participants had an impact on the error of the estimation of stance time asymmetry and swing time variability and this can be related to the limitation of the FC/IC algorithm.
 - Asymmetry was more comparable between instruments for PD because it is a more prominent feature of pathological gait. Asymmetry in HC is subtle and more difficult to detect with an instrumented walkway due to slight variations in dynamics of the CoM rather than discrete footfalls. These results impact on variability which was not comparable. Greater asymmetry increases the estimation of variability for accelerometry given its sensitivity to detecting this feature of gait.
- ii) An instrumented walkway detects footfalls but an accelerometer-based BWM continuously tracks the position of the body resulting in a continuous signal (Figure 4 and 6). The resulting peak therefore represents the trajectory of the CoM rather than actually heel strike (IC) or toe off (FC) events determined by an instrumented walkway.
- iii) Gait algorithms are dependent on the signal characteristics (e.g. peaks reliant on polynomial coefficients or local maxima to locate the maximum of a peak). Thus, delay in the location of maximum/minimum due to peak detection methods or smoothness of peak as a result of filtering or processing can introduce timing differences between the BWM signal and instrumented walkway to a resolution required for variability/asymmetric outcomes (ms).

Instrumented walkway: functionality and sources of error

The instrumented walkway used in this study (GaitRite) has been previously shown to be a reliable method for measuring mean gait characteristics [45], but less so for asymmetry and variability [23, 24, 38, 39]. Another plausible explanation for these discrepancies is the operational functionality of the walkway itself. Specifically the walkway is an array of pressure sensors that activate or trigger a footfall event when a load is applied. These events usually occur as a collective to define the entire surface area of the foot and subsequently IC and FC events. However, spurious contacts may result due to scuffing or a shuffling walk introducing false IC events. As a result, technician/researcher can review the series of contacts (activated pressure sensors) for each footfall and subjectively include or exclude an individual sensor (within the array defining a foot) if they deem it suitable during a walk. With a spatial accuracy of 1.27cm this (subjective) inclusion/exclusion of sensors can be the difference of approximately 0.009s based on an estimated stepping speed (step velocity 142cm/s). With variability and asymmetry quantified at a similar resolution (Table III), the inclusion/exclusion of a single pressure sensor in the

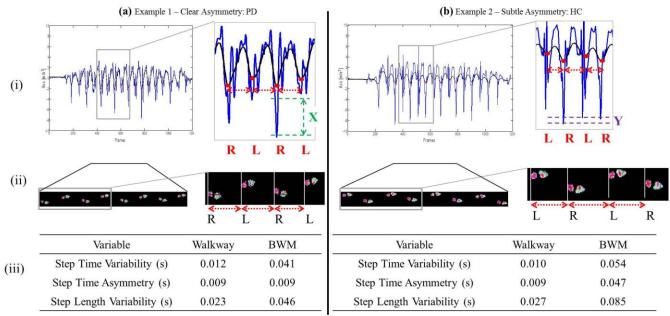


Figure 6. (a) Example of clear asymmetric gait pattern of a PD participant (regular alternating of higher and lower absolute peak values of the accleration signal, X) and (b) subtle asymmetric pattern of a HC (less regular alternating of higher and lower absolute peak values of the accleration signal, Y). Each panel (a), (b) displays (i) accelerometer sensor waveform and a zoomed example of 4 consecutive steps (red dots/arrows), (ii) corresponding data from the instrumented walkway and a zoomed example of same 4 consecutive steps (red arrows) and (iii) mean results from the 2 systems for each example

walkway can be a further source of disagreement between systems.

Alternative laboratory reference

Previous work has used continuous tracking of the CoM with a 3D motion analysis system [21, 46, 47]. Direct comparison of vertical acceleration, velocity, and position (displacement) traces together with spatial-temporal parameters showed good agreement between the optical motion capture system and an inertial measurement unit (BWM) [21, 46]. Despite good agreement, the comparison of an accelerometer-based BWM to a 3D system, though more similar in quantification of gait, measure different components; acceleration and displacement, respectively. Though acceleration and displacement can be related through single and double integration/derivation, that process introduces error through drift, where the error in the signal after each integration increases by $\varepsilon = t^{1.5}$, where t is integration time and ε is error [21, 48].

Therefore systematic errors will always remain between systems (instrumented walkway vs. accelerometer-based BWM on the lower back (L5) vs. 3D motion analysis system) even when measuring related components explaining why in our study there is lower agreement for the mean swing time, higher variability of step time (Figure 6) and estimation of (subtle) symmetry differences. This however does not infer that one system is less valid, rather that both systems are valid but differences can be explained by different methodological approaches used to estimate gait events.

BWM tend to have greater estimates for gait characteristics (a feature of the adopted algorithms), but was systematic in its nature and the values remained within expected ranges for both PD and HC. Importantly,

pathology did not influence our findings although this may change with increased disease severity and gait impairment.

Study limitations and future work

This study achieved its aims of quantifying 14 core gait characteristics while also deriving a new rationale to account for poor agreement between a BWM (worn at L5) and an instrumented walkway. However, some limitations do exist and therefore we make recommendations for future research. For instance, the methodology presented has been tested in a laboratory environment, considering walking at self-selected speed on a group of healthy participants and those with PD. Therefore before being able to generalize our results in these groups, further analysis would be required to test the robustness of the combination of algorithms across different gait speeds.

Moreover, our PD group had mild motor symptoms and more severe motor symptoms may influence the gait pattern and algorithm performance. For instance, lack of clearly identifiable signal characteristics (peaks/troughs) within the filtered signal may result in the miss or no detection of IC/FC events. While we included a range of PD participants (PIGD, ID, TD) there was no major (visually observant) limitation within their gait such as shuffling.

The addition of a gyroscope sensor within the BWM would allow the complete quantification of the 16 gait characteristics identified as important [27, 28]. Additionally, the extra sensor would allow the correct identification and allocation of left/right steps. The improved step recognition methodology would allow the variance of left and right steps to be calculated separately and then be combined to find SD, Equation 8. This method

avoids confounding step-to-step variability with variation originating from asymmetry between left and right steps [42]. Moreover, the correct identification of each left/right step could then be directly compared between systems

$$SD_{left or right} = \sqrt{\frac{(Variance_{left} + Variance_{right})}{2}}$$
 (8)

V. CONCLUSION

A simple tri-axial accelerometer device is able to replicate 14 clinically relevant core gait characteristics. Agreement with a laboratory reference system ranged from excellent (mean) to poor (variability and asymmetry), which we interpreted as primarily an intrinsic limitation of the comparison between two systems which measure different properties: continuous motion (BWM) vs. single footfall events (instrumented walkway). Despite this, we feel confident from our results that a single tri-axial accelerometer-based BWM is accurate for measuring gait variability and asymmetry.

Accelerometer-based BWM may offer advantages over standard laboratory systems for select characteristics potentially making them a more sensitive device to detect any subtle changes in gait pattern due to ageing and/or pathology. When compared to an instrumented walkway, systematically greater values of mean gait characteristics need to be taken into consideration. However, a system currently doesn't exist which: captures a broad range of gait outcomes sensitive to early pathology, is low-cost (<£100), and capable of being deployed in multi-centre large scale studies for instrumented testing or within the community for real-world continuous data collection. This approach (use of a generic movement monitor and algorithms from the literature) may therefore offer a lowcost solution for quantitative gait evaluation in PD and HC during instrumented testing and in a wide variety of environments (including at home). Further work is ongoing to optimise gait quantification algorithms as well as explore step width estimation and the impact of algorithm sensitivity on disease progression and disease severity.

ACKNOWLEDGMENT

We would like to acknowledge Dr. Brook Galna for his assistance in data analysis and interpretation and Dr. Sue Lord for critical examination of the manuscript.

REFERENCES

- S. Lord, B. Galna, and L. Rochester, "Moving forward on gait measurement: toward a more refined approach," *Mov Disord*, vol. 28, pp. 1534-43, Sep 15 2013.
- [2] J. M. Hausdorff, "Gait dynamics in Parkinson's disease: common and distinct behavior among stride length, gait variability, and fractal-like scaling," *Chaos*, vol. 19, p. 026113, Jun 2009.
- [3] M. K. Mak and M. Y. Pang, "Fear of falling is independently associated with recurrent falls in patients with Parkinson's disease: a 1-year prospective study," *J Neurol*, vol. 256, pp. 1689-95, Oct 2009.
- [4] L. Rochester, K. Baker, A. Nieuwboer, and D. Burn, "Targeting dopa-sensitive and dopa-resistant gait dysfunction in Parkinson's disease: selective responses to internal and external cues," *Mov Disord*, vol. 26, pp. 430-5, Feb 15 2011.
- [5] J. Verghese, C. Wang, R. B. Lipton, R. Holtzer, and X. Xue, "Quantitative gait dysfunction and risk of cognitive decline and

- dementia," *J Neurol Neurosurg Psychiatry*, vol. 78, pp. 929-35, Sep 2007.
- [6] L. Rochester, B. Galna, S. Lord, and D. Burn, "The nature of dualtask interference during gait in incident Parkinson's disease," *Neuroscience*, 2014.
- [7] C. A. Lohnes and G. M. Earhart, "The impact of attentional, auditory, and combined cues on walking during single and cognitive dual tasks in Parkinson disease," *Gait & Posture*, vol. 33, pp. 478-483, 3// 2011.
- [8] A. J. Williams, D. S. Peterson, and G. M. Earhart, "Gait coordination in Parkinson disease: Effects of step length and cadence manipulations," *Gait & Posture*, vol. 38, pp. 340-344, 6// 2013.
- [9] S.-L. Chien, S.-Z. Lin, C.-C. Liang, Y.-S. Soong, S.-H. Lin, Y.-L. Hsin, et al., "The efficacy of quantitative gait analysis by the GAITRite system in evaluation of parkinsonian bradykinesia," Parkinsonism & Related Disorders, vol. 12, pp. 438-442, 10// 2006.
- [10] K. L. Paterson, N. D. Lythgo, and K. D. Hill, "Gait variability in younger and older adult women is altered by overground walking protocol," *Age Ageing*, vol. 38, pp. 745-8, Nov 2009.
- [11] A. Godfrey, J. Lara, C. A. Munro, C. Wiuff, S. A. Chowdhury, S. Del Din, et al., "Instrumented assessment of test battery for physical capability using an accelerometer: a feasibility study," *Physiological Measurement*, vol. In Press, 2015.
- [12] J. McCamley, M. Donati, E. Grimpampi, and C. Mazzà, "An enhanced estimate of initial contact and final contact instants of time using lower trunk inertial sensor data," *Gait & Posture*, vol. 36, pp. 316-318, 2012.
- [13] R. C. González, A. M. López, J. Rodriguez-Uría, D. Álvarez, and J. C. Alvarez, "Real-time gait event detection for normal subjects from lower trunk accelerations," *Gait & posture*, vol. 31, pp. 322-325, 2010.
- [14] W. Zijlstra and A. L. Hof, "Assessment of spatio-temporal gait parameters from trunk accelerations during human walking," *Gait & posture*, vol. 18, pp. 1-10, 2003.
- [15] A. Hartmann, S. Luzi, K. Murer, R. A. de Bie, and E. D. de Bruin, "Concurrent validity of a trunk tri-axial accelerometer system for gait analysis in older adults," *Gait & posture*, vol. 29, pp. 444-448, 2009.
- [16] A. Godfrey, A. K. Bourke, G. M. Ólaighin, P. Van De Ven, and J. Nelson, "Activity classification using a single chest mounted tri-axial accelerometer," *Medical engineering & physics*, vol. 33, pp. 1127-1135, 2011.
- [17] B. Najafi, K. Aminian, A. Paraschiv-Ionescu, F. Loew, C. J. Bula, and P. Robert, "Ambulatory system for human motion analysis using a kinematic sensor: monitoring of daily physical activity in the elderly," *Biomedical Engineering, IEEE Transactions on*, vol. 50, pp. 711-723, 2003.
- [18] A. Zijlstra and W. Zijlstra, "Trunk-acceleration based assessment of gait parameters in older persons: A comparison of reliability and validity of four inverted pendulum based estimations," *Gait & posture*, 2013.
- [19]E. Sejdic, K. A. Lowry, J. Bellanca, M. S. Redfern, and J. S. Brach, "A comprehensive assessment of gait accelerometry signals in time, frequency and time-frequency domains," *IEEE Trans Neural Syst Rehabil Eng*, vol. 22, pp. 603-12, May 2014.
- [20]P. Esser, H. Dawes, J. Collett, M. G. Feltham, and K. Howells, "Assessment of spatio-temporal gait parameters using inertial measurement units in neurological populations," *Gait Posture*, vol. 34, pp. 558-60, Oct 2011.
- [21]P. Esser, H. Dawes, J. Collett, M. G. Feltham, and K. Howells, "Validity and inter-rater reliability of inertial gait measurements in Parkinson's disease: A pilot study," *Journal of neuroscience methods*, vol. 205, pp. 177-181, 2012.
- [22] R. Moe-Nilssen and J. L. Helbostad, "Estimation of gait cycle characteristics by trunk accelerometry," *Journal of biomechanics*, vol. 37, pp. 121-126, 2004.
- [23] R. Moe-Nilssen, M. K. Aaslund, C. Hodt-Billington, and J. L. Helbostad, "Gait variability measures may represent different constructs," *Gait & posture*, vol. 32, pp. 98-101, 2010.
- [24] J. S. Brach, S. Perera, S. Studenski, and A. B. Newman, "The reliability and validity of measures of gait variability in communitydwelling older adults," *Arch Phys Med Rehabil*, vol. 89, pp. 2293-6, Dec 2008.
- [25] A. Weiss, M. Brozgol, M. Dorfman, T. Herman, S. Shema, N. Giladi, et al., "Does the evaluation of gait quality during daily life provide insight into fall risk? A novel approach using 3-day accelerometer

- recordings," Neurorehabil Neural Repair, vol. 27, pp. 742-52, Oct 2013
- [26] J. H. Hollman, E. M. McDade, and R. C. Petersen, "Normative spatiotemporal gait parameters in older adults," *Gait Posture*, vol. 34, pp. 111-8, May 2011.
- [27] S. Lord, B. Galna, J. Verghese, S. Coleman, D. Burn, and L. Rochester, "Independent domains of gait in older adults and associated motor and nonmotor attributes: validation of a factor analysis approach," *The Journals of Gerontology Series A: Biological Sciences and Medical Sciences*, vol. 68, pp. 820-827, 2013.
- [28] B. Galna, S. Lord, D. J. Burn, and L. Rochester, "Progression of gait dysfunction in incident Parkinson's disease: Impact of medication and phenotype," *Mov Disord*, Dec 27 2014.
- [29] T. K. Khoo, A. J. Yarnall, G. W. Duncan, S. Coleman, J. T. O'Brien, D. J. Brooks, et al., "The spectrum of nonmotor symptoms in early Parkinson disease," *Neurology*, vol. 80, pp. 276-281, 2013.
- [30]Z. S. Nasreddine, N. A. Phillips, V. Bedirian, S. Charbonneau, V. Whitehead, I. Collin, et al., "The Montreal Cognitive Assessment, MoCA: a brief screening tool for mild cognitive impairment," J Am Geriatr Soc, vol. 53, pp. 695-9, Apr 2005.
- [31] L. E. Powell and A. M. Myers, "The Activities-specific Balance Confidence (ABC) Scale," *J Gerontol A Biol Sci Med Sci*, vol. 50A, pp. M28-34, Jan 1995.
- [32] M. M. Hoehn and M. D. Yahr, "Parkinsonism: onset, progression and mortality," *Neurology*, vol. 17, pp. 427-42, May 1967.
- [33] C. G. Goetz, B. C. Tilley, S. R. Shaftman, G. T. Stebbins, S. Fahn, P. Martinez-Martin, et al., "Movement Disorder Society-sponsored revision of the Unified Parkinson's Disease Rating Scale (MDS-UPDRS): scale presentation and clinimetric testing results," Mov Disord, vol. 23, pp. 2129-70, Nov 15 2008.
- [34] G. T. Stebbins, C. G. Goetz, D. J. Burn, J. Jankovic, T. K. Khoo, and B. C. Tilley, "How to identify tremor dominant and postural instability/gait difficulty groups with the movement disorder society unified Parkinson's disease rating scale: comparison with the unified Parkinson's disease rating scale," *Mov Disord*, vol. 28, pp. 668-70, May 2013.
- [35] C. L. Tomlinson, R. Stowe, S. Patel, C. Rick, R. Gray, and C. E. Clarke, "Systematic review of levodopa dose equivalency reporting in Parkinson's disease," *Mov Disord*, vol. 25, pp. 2649-53, Nov 15 2010.
- [36] R. Moe-Nilssen, "A new method for evaluating motor control in gait under real-life environmental conditions. Part 1: The instrument," *Clinical Biomechanics*, vol. 13, pp. 320-327, 1998.
- [37] D. A. Winter, "Biomechanics and motor control of human movement," ed: Wiley (New York), 1990.
- [38] O. Beauchet, E. Freiberger, C. Annweiler, R. W. Kressig, F. R. Herrmann, and G. Allali, "Test-retest reliability of stride time variability while dual tasking in healthy and demented adults with frontotemporal degeneration," *J Neuroeng Rehabil*, vol. 8, p. 37, 2011.
- [39]M. D. Lewek and E. P. Randall, "Reliability of spatiotemporal asymmetry during overground walking for individuals following chronic stroke," *J Neurol Phys Ther*, vol. 35, pp. 116-21, Sep 2011.
- [40] W. Zijlstra, "Assessment of spatio-temporal parameters during unconstrained walking," Eur J Appl Physiol, vol. 92, pp. 39-44, Jun 2004.
- [41] R. C. Gonzalez, D. Alvarez, A. M. Lopez, and J. C. Alvarez, "Ambulatory estimation of mean step length during unconstrained walking by means of COG accelerometry," *Comput Methods Biomech Biomed Engin*, vol. 12, pp. 721-6, Dec 2009.
- [42] B. Galna, S. Lord, and L. Rochester, "Is gait variability reliable in older adults and Parkinson's disease? Towards an optimal testing protocol," *Gait & posture*, 2012.
- [43] J. Lara, A. Godfrey, E. Evans, B. Heaven, L. J. Brown, E. Barron, et al., "Towards measurement of the Healthy Ageing Phenotype in lifestyle-based intervention studies," *Maturitas*, vol. 76, pp. 189-99, Oct 2013.
- [44] A. Godfrey, S. Del Din, G. Barry, J. C. Mathers, and L. Rochester, "Instrumenting gait with an accelerometer: A system and algorithm examination," *Med Eng Phys*, vol. 37, pp. 400-7, Apr 2015.
- [45] H. B. Menz, M. D. Latt, A. Tiedemann, M. Mun San Kwan, and S. R. Lord, "Reliability of the GAITRite ® walkway system for the quantification of temporo-spatial parameters of gait in young and older people," *Gait & posture*, vol. 20, pp. 20-25, 2004.

- [46]M. H. Cole, W. van den Hoorn, J. K. Kavanagh, S. Morrison, P. W. Hodges, J. E. Smeathers, et al., "Concurrent Validity of Accelerations Measured Using a Tri-Axial Inertial Measurement Unit while Walking on Firm, Compliant and Uneven Surfaces," PLoS One, vol. 9, p. e98395, 2014.
- [47] D. Trojaniello, A. Cereatti, and U. Della Croce, "Accuracy, sensitivity and robustness of five different methods for the estimation of gait temporal parameters using a single inertial sensor mounted on the lower trunk," *Gait Posture*, vol. 40, pp. 487-92, Sep 2014.
- [48] J. Farrell and M. Barth, *The global positioning system and inertial navigation* vol. 61: McGraw-Hill New York, 1999.



Silvia Del Din (M'14) received the BEng degree in information engineering in 2006, MEng in bioengineering in 2008 and the PhD degree in bioengineering in 2012 from the University of Padova, Italy.

Her early career as a Postdoctoral Researcher began at the Department of Information Engineering, University of Padova, where her work involved fMRI-Gait analysis assessment and Fugl-Meyer clinical scores estimation through wearable sensors.

Dr Del Din is a member of the Institute of Engineering and Technology (MIET). Dr Del Din received the BTS Bioengineering/SIMFER award in 2010 and the Prof Sergio Gambi Award, Second Edition in 2012.



Alan Godfrey (M'08) received the BEng degree in electronic engineering and the PhD degree in biomedical electronics from the University of Limerick, Ireland in 2004 and 2008, respectively.

After research positions at the University of Limerick and University of Reading, UK, he moved to the Institute of Neuroscience, Newcastle University, UK as a Research Associate. His current research interests include gait and ambulatory analysis using wearable devices with novel algorithm and signal

processing techniques. He is an adjunct lecturer in Electronic Engineering at the National University of Ireland, Galway and an Associate Fellow of the Faculty of Medical Science, Newcastle University.

Dr Godfrey is a member of the IEEE Engineering in Medicine and Biology Society (EMBS), a member of the Institute of Engineering and Technology (MIET).



Lynn Rochester graduated as a physiotherapist in 1983 specialising in neuro-rehabilitation and completed a PhD in 1992 in neuroscience.

She joined the Institute of Neuroscience, Newcastle University in 2008 as Professor of Human Movement Science and set up a research programme focussed on age related gait and mobility disorders and leads a multidisciplinary team of clinicians, clinical scientists and clinical

engineers. She is based in the Clinical Ageing Research Unit, a translational clinical research platform, where she is Deputy Director. Her main research interests are in neurodegenerative disease focused on the motor and non-motor mechanisms of gait and falls, surrogate markers of disease and disease progression, development and evaluation of novel interventions, and technological applications in healthcare.

Prof Rochester serves on various National and International committees and takes a key role in professional leadership within the university developing clinical academic careers for healthcare professionals. She also leads an academic physiotherapy team which is integrated into the Regional Movement Disorders Service.